REGIONE EMILIA ROMAGNA

PROVINCIA DI BOLOGNA

COMUNE DI SAN GIOVANNI IN PERSICETO

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Opera	Progetto di realizzazione di un impianto agrivoltaico e opere connesse nel Comune di San Giovanni in Persiceto (BO) denominato Biancolina.		
Oggetto	Codice elaborato: BNCSS0R01-00		
	Titolo elaborato: Relazione geologico-sismica		

00	13/02/2024	Emissione per progetto definitivo	Dott. Geol. Giulia Gardosi	Ing. D. Tubertini	Ing. Fabio Domenico Amico
Rev.	Data	Oggetto della revisione	Elaborazione	Verifica	Approvazione

Comune di San Giovanni in Persiceto (BO)

Località: Biancolina
Via Puglia

Oggetto: Studio geologico*) relativo alla realizzazione di un campo agrivoltaico nel comune di San Giovanni in Persiceto (progetto denominato "Biancolina").
- Relazione geologica-
- Modellazione geofisica -

febbraio 2024

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- carta geologica:

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Tav.3b - sezioni stratigrafiche interpretative:

-------- **Allegati:**

- **Prove penetrometriche** –

Cptm: - diagrammi di resistenza; - tabelle valori di resistenza; - valutazioni litologiche; - parametri geotecnici;

Cptu: - diagrammi di resistenza; - valutazioni litologiche; - parametri geotecnici;

- **Prove di laboratorio** - taglio diretto CD;
- **Sismica** - report indagini sismiche; - parametri sismici;

- **report verifica liquefazione**

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1. Premessa

Su incarico della committenza, è stato svolto il presente studio geologico, di modellazione geofisica a corredo del progetto per la realizzazione di un campo agrivoltaico nel comune di San Giovanni in Persiceto (progetto denominato "Biancolina").

Al fine di verificare l'idoneità geologica e geomorfologia del sito è stato eseguito un primo sopraluogo sull'area, i cui risultati, unitamente alle conoscenze desunte dalla bibliografia ed a dati in possesso dello scrivente relativi all'area in esame, hanno permesso di definire una prima conoscenza dell'area. Inoltre è stata condotta una iniziale campagna di indagini geognostiche e geofisiche, al fine di definire la caratterizzazione litostratigrafia, geofisica del terreno.

Scopo dello studio è dunque fornire l'inquadramento geologico, idrologico, idrogeologico nonché sismico necessario per effettuare le necessarie valutazioni di compatibilità dell'opera in progetto con le peculiarità dei luoghi. Per quanto riguarda l'aspetto sismico il presente studio fa riferimento alla classificazione sismica dei Comuni, definita nell'allegato 1- punto 3, dell'O.P.C.M. 3274 del 20/03/2003, nel quale il comune di San Giovanni in Persiceto è classificato di zona sismica 3.

2. Quadro normativo di riferimento adottato

- R.D. n. 3267 del 30 dicembre 1923 "*Riordinamento e riforma della legislazione in materia di boschi e di terreni montani*";
- R.D. n. 1126 del 16 maggio 1926 "*Approvazione del regolamento per l'applicazione del regio decreto 30 dicembre 1923, n. 326, concernente il riordinamento e la riforma della legislazione in materia di boschi e di terreni montani*";
- R.D. n. 1775 del 11 dicembre 1933 "*Approvazione del testo unico delle disposizioni di legge sulle acque e sugli impianti elettrici*";
- Legge n. 64 del 2 febbraio 1974 "*Provvedimenti per le costruzioni con particolari prescrizioni per le zone sismiche*";
- AGI – Associazione Geotecnica Italiana, giugno 1977 "*Raccomandazioni sulla programmazione ed esecuzione delle indagini geotecniche*";
- D.Min.LL.PP. 11 marzo 1988 "*Norme tecniche riguardanti le indagini sui terreni e sulle rocce, la stabilità dei pendii naturali e delle scarpate, i criteri generali e le prescrizioni per la progettazione, l'esecuzione e il collaudo delle opere di sostegno delle terre e delle opere di fondazione*";
- Circ. LL.PP. n. 30483 del 24/09/1988 "*Istruzioni riguardanti le indagini sui terreni e sulle rocce, la stabilità dei pendii naturali e delle scarpate, i criteri generali e le prescrizioni per la progettazione, l'esecuzione ed il collaudo delle opere di sostegno delle terre e delle opere di*

fondazione";

- Legge n. 36 del 5 gennaio 1994 "*Disposizioni in materia di risorse idriche*";
- EN 1997 (2002) – Eurocode 7 "*Geotechnical Design*";
- EN 1998 (2003) – Eurocode 8 "*Design of structures for earthquake resistance*"
- Ordinanza n.3274 della Presidenza del Consiglio dei Ministri del 20 marzo 2003 "*Primi elementi in materia di criteri generali per la classificazione sismica del territorio nazionale e di normative tecniche per le costruzioni in zona sismica*" e successivi aggiornamenti:
    - Ordinanza n.3316 della Presidenza del Consiglio dei Ministri del 2 ottobre 2003;
    - Ordinanza n.3431 della Presidenza del Consiglio dei Ministri del 3 maggio 2005;
- D.Min.LL.PP. 14 settembre 2005 "*Norme tecniche per le costruzioni*";
- D. Lgs. n. 152 del 03 aprile 2006 "*Norme in materia ambientale*" e s.m.i.;
- D.Min.LL.PP. 14 gennaio 2008 "*Nuove norme tecniche per le costruzioni*";
- Circolare Min.LL.PP. 2 febbraio 2009 n. 617 "*Istruzioni per l'applicazione delle "Nuove norme tecniche per le costruzioni" di cui al D.M. 14 gennaio 2008*";
- D.Min.LL.PP. 17 gennaio 2018 "*Aggiornamento delle norme tecniche per le costruzioni*";

2.1. NORME REGIONALI

- Legge della Regione Emilia-Romagna n. 47 del 7 dicembre 1978 "*Tutela ed uso del territorio*";
- Legge della Regione Emilia-Romagna n. 20 del 24 marzo 2000 "*Disciplina generale sulla tutele e l'uso del territorio*";
- Legge della Regione Emilia-Romagna n. 17 del 18 luglio 1991 "*Disciplina delle Attività Estrattive"* e s.m.i.;
- Legge della Regione Emilia Romagna n 9 del 18 maggio 1999 "*Disciplina della procedura di valutazione dell'impatto ambientale*";
- Delibera della Giunta Regionale n. 1117 del 11 luglio 2000 "*Direttiva regionale concernente le procedure amministrative e le norme tecniche relative alla gestione del vincolo idrogeologico, redatta ai sensi ed in attuazione degli artt. 148, 149, 150 e 151 della L.R. 21 aprile 1999 n. 3 "Riforma del sistema regionale e locale'"*";
- Legge della Regione Emilia-Romagna n. 31 del 25 novembre 2002 "*Disciplina generale dell'edilizia"* e s.m.i;.
- Delibera di Giunta Regionale n.1677 del 24 ottobre 2005, "*Prime indicazioni applicative in merito al decreto ministeriale 14 settembre 2005 (pubblicato sul supplemento ordinario n.159 alla G.U. n.222 del 23 settembre 2005) recante* "Norme tecniche per le costruzioni"";
- Deliberazione dell'Assemblea legislativa n. 112 del 2 maggio 2007:"Approvazione dell'atto di indirizzo e coordinamento tecnico ai sensi dell'art. 16, comma 1, della L.R. 20/2000 "Disciplina

generale sulla tutela e l'uso del territorio", in merito a"indirizzi per gli studi di microzonazione sismica in Emilia-Romagna per la pianificazione territoriale e urbanistica". (Proposta della Giunta regionale in data 10 gennaio 2007, n.1);

- Legge della Regione Emilia Romagna n 19 del 30 ottobre 2008 "*Norme per la riduzione del rischio sismico*";
- Delibera di Giunta Regionale n.687 del 23 maggio 2011, "*Atto di indirizzo recante l'individuazione degli interventi privi di rilevanza per la pubblica incolumità ai fini sismici e delle varianti in corso d'opera, riguardanti parti strutturali, che non rivestono carattere sostanziale, ai ai sensi dell'articolo 9, comma 4 della L.R. n. 19 del 2008*".
- Delibera di Giunta Regionale n.2193 del 21 dicembre 2015, "*Atto di indirizzo e coordinamento tecnico ai sensi dell'art. 16, c. 1, della LR 20/2000 per "Indirizzi per gli studi di microzonazione sismica in Emilia-Romagna per la pianificazione territoriale e urbanistica"*.
- Delibera di Giunta Regionale n.630 del 29 aprile 2019, "*Atto di coordinamento tecnico sugli studi di microzonazione sismica per la pianificazione territoriale e urbanistica (artt. 22 e 49, della LR 24/2017)"*.
- Delibera di Giunta Regionale n.476 del 12 aprile 2021, "*Aggiornamento dell'"atto di coordinamento tecnico sugli studi di microzonazione sismica per la pianificazione territoriale e urbanistica (artt. 22 e 49, l.r. n. 24/2017)" di cui alla deliberazione della giunta regionale 29 aprile 2019, n. 630."*.

3. Inquadramento topografico, lineamenti geomorfologici

Il sito di futura realizzazione del campo agrivoltaico si localizza all'interno degli elementi C.T.R. C.T.R. N° 202112 – Lorenzatico e N° 202151 - Zenerigolo. Le aree di studio, individuata nella Tav. 1, sono censite al Catasto Urbano del Comune di San Giovanni Persiceto al foglio n. 75. L'area di futura realizzazione del campo agrivoltaico è individuata dai toponimi "*Biancolina*", "*Zenerigolo*" e "*Lorenzatico*", e sarà posto ad est del nucleo abitativo della Biancolina, tra via Puglia a sud e Via Boschi Mascellaro a est; l'accesso all'area potrà sia da via Biancolina (procedendo lungo Via Puglia), sia lungo Via Boschi Mascellaro e la quota media del piano campagna si aggira tra 19,3 e 20,7 m s.l.m..

Il contesto morfologico di entrambe le aree è di tipo sub pianeggiante; le quote topografiche degradano lievemente verso nord-est, senza particolari elementi che alterino la monotonia morfologica ad eccezione degli argini di fossi e scoli di natura antropica che corrono in direzione sud-ovest nord-est.

Il territorio in esame appartiene alla fascia della media pianura, al di fuori delle conoidi alluvionali (Reno, Savena-Idice) pede-appenniniche, costituitasi tra l'area dell'Alta Pianura Padana

Appenninica e la zona di Bassa Pianura Padana.

Le zone di pianura non costituiscono un'unità morfologica piatta ed uniforme; sono infatti caratterizzate da strisce rilevate, dette dossi, corrispondenti ad alvei antichi (paleoalvei) od attuali, alternati a zone depresse, dette valli, che, fino a quando i corsi d'acqua non sono stati regimati, raccoglievano le acque di esondazione.

Caratteristica comune a tutta la pianura del bolognese, è l'andamento morfologico che vede l'alternanza di dossi e conche morfologiche. I dossi veri e propri hanno forma allungata secondo l'asse del canale fluviale, profilo convesso e gradiente di pendenza, normale all'asse, in genere non superiore allo 0.2%; nei casi più marcati si percepisce anche visivamente che i dossi costituiscono le porzioni di pianura alluvionale più rilevate. Le conche morfologiche, invece, sono zone topograficamente più depresse della pianura alluvionale, in cui le acque di rotta o esondazione, con i loro sedimenti, non sono riuscite ad innalzare il livello del suolo in maniera adeguata rispetto alle aree limitrofe. La principale funzione idrologica di queste aree è quella di fungere da casse di espansione naturali alle piene eccezionali dei canali fluviali, quindi hanno funzione di regimazione ed equilibrio idraulico. Le conoidi dell'alta pianura sono frequentemente dotate di ridotte protezioni naturali delle sottostanti falde.

L'evoluzione della pianura olocenica è fondamentalmente governata sia dalla tettonica, quali le grandi pieghe del ferrarese che hanno determinato nel tempo uno spostamento verso nord-est del corso del Fiume Po, che dalla subsidenza (circa 2 cm/anno); i fenomeni ricorrenti di rotte e tracimazione depositano in sequenza prima i materiali più grossolani e successivamente i materiali più fini nelle aree interfluviali e di conca ove spesso decantano in acque stagnanti (paludi). Pertanto le continue modifiche dei corsi d'acqua, dovute sia alla strutturazione tettonica della pianura che alla subsidenza, hanno prodotto una variegata sovrapposizione di sedimenti rappresentati da lenti sabbiose e/o ghiaiose (paleo alvei) e da sedimenti a tessitura fine (riempimenti dei bacini interfluviali di esondazione).

Per la datazione ed attribuzione idrografica dei paleoalvei dei fiumi della Pianura Padana occorre fare riferimento agli autori più recenti che si sono occupati della ricostruzione paleoidrografica della zona: Pellegrini (1969), Veggiani (1947), Castaldini et Alii (1979), Cremaschi et Alii (1980), Gasperi e Pellegrini (1981, 1984). In base alle informazioni reperite in merito, recenti studi indicherebbero, per i paleoalvei principali presenti nell'area di studio, una datazione risalente al XIII secolo.

La frequente corrispondenza riscontrata nell'area esaminata tra dossi e paleoalvei è spiegabile analizzando, dal punto di vista dei processi di sedimentazione, il modello evolutivo della pianura olocenica, almeno nelle linee generali. I fiumi appenninici, a valle delle conoidi pedemontane, tendono a proseguire verso il collettore principale su alvei pensili formati da sedimenti che il corso d'acqua non è più in grado di portare a carico.

Nel caso di rotte e tracimazioni, le acque si espandono nella pianura depositando, nelle immediate vicinanze dell'alveo, i materiali più grossolani e più lontano, una volta cessato il flusso, i sedimenti più fini. Questi ultimi sedimenti si costipano di più di quelli costituenti l'alveo e si determinano così, già per processi naturali, dei notevoli dislivelli fra fiumi e territori circostanti.

Per i corsi d'acqua di pianura, non arginati artificialmente, rotte e tracimazioni sono un fenomeno ricorrente che favorisce i cambiamenti d'alveo; in un bacino subsidente l'accrescersi della pianura avviene perciò sia orizzontalmente, con il giustapporsi di diversi successivi corpi d'alveo, che verticalmente, con il sovrapporsi di successivi cicli di riempimento dei bacini di esondazione.

I corsi d'acqua principali hanno tendenzialmente un andamento da Sud a Nord e sono a carattere torrentizio nella zona montana a Sud, con portate massime nei mesi di Marzo e Novembre e portate minime nel periodo Luglio-Agosto; in pianura perdono i caratteri di corsi d'acqua naturali, avendo subito arginature, deviazioni e alterazioni di vario tipo legate ad opere di bonifica. Essi corrono generalmente in pensile; le loro torbide sono state impiegate per lungo tempo allo scopo di bonificare mediante le "casse di colmata", creando in tal modo le pianure bonificate a Nord.

L'alta pianura è essenzialmente caratterizzata dalla presenza dei conoidi alluvionali riferibili alla attività deposizionale del F. Reno, del T. Lavino e del T. Samoggia che hanno modellato la fascia pedecollinare rispettivamente in corrispondenza del settore orientale ed occidentale dell'area in esame. Fra le strutture di conoide principali si interpongono delle strutture minori.

In ultimo si ricorda l'intenso intervento antropico di bonifica del settore bolognese a partire dall'età preromana fino al XIV sec. con notevole variazione dei corsi d'acqua come la deviazione dell'alveo del fiume Reno e la bonifica delle paludi con l'attuale pensilità dei corsi d'acqua nella pianura bolognese.

4. Modello geologico

Come detto, l'area in esame appartiene alla fascia della Media-Bassa Pianura ed è costituita, come il restante comparto di pianura, da terreni di origine pluviale-fluvioglaciale, formati dai sedimenti che, dal periodo post-glaciale sino al periodo storico, fiumi e torrenti vennero via via depositando nel loro vagare.

Il territorio dell'Emilia Romagna è costituito dal versante padano dell'Appennino settentrionale e dalla Pianura Padana a sud del Fiume Po. Pur essendo due ambienti geomorfologici distinguibili, essi risultano strettamente correlati fra loro: il fronte della catena appenninica non coincide con il limite morfologico catena montuosa-pianura, ma è individuabile fra gli archi esterni delle Pieghe Emiliane e Ferraresi (Pieri & Groppi, 1981), sepolte dai sedimenti quaternari della Pianura Padana. Il fronte appenninico sovrascorre verso nord sulla piattaforma padano-veneta; di conseguenza l'evoluzione del territorio dell'Emilia Romagna risulta strettamente legata ai cambiamenti del settore esterno della

catena nord-appenninica. Le faglie derivanti dai movimenti dei sovrascorrimenti appenninici danno origine alle manifestazioni sismiche che interessano la Regione.

L'intero territorio del comune di San Giovanni in Persiceto risulta compreso fra il *Fronte di accavallamento pedeappenninico* ed il *Fronte di accavallamento esterno* che insiste sull'avampaese, rappresentato dalla Pianura Padana; la zona di alta pianura appartiene strutturalmente alla "Fascia Sepolta" caratterizzata da tettonica di embricazione (ancora attiva) coperta dai depositi continentali quaternari. La parte del territorio del Comune verso le zone pianeggianti, risulta all'interno nel bacino subsidente pliocenico-quaternario della Pianura Padana, costituito da una ampia depressione a stile compressivo colmata da sedimenti mesozoici, terziari e quaternari; da un punto di vista tettonico-sedimentario è importante la subsidenza, avvenuta nel Pleistocene inferiore, che ha provocato la sedimentazione di diverse centinaia di metri di argilla marina. Le strutture tettoniche più significative sono gli accavallamenti a notevole continuità laterale e senso di trasporto tettonico verso nord-est che descrivono una struttura arcuata con una zona frontale (parallela al fronte appenninico), una zona laterale collegata alla linea del Sillaro ed una zona di raccordo a direzione obliqua. Queste strutture sembrano essersi originate già nella fase tettonica del *Messiniano sup*. (*fase intramessiniana*) Ulteriori strutturazioni e riattivazioni, anche molto importanti, sono inoltre evidenti nel *Pliocene* e nel *Pleistocene*, dove gli eventi tettonici lungo la linea del Sillaro si sono invertiti (da trascorrenza destra a trascorrenza sinistra).

La strutturazione neogenica, che ha deformato in tempi "recenti" le Sabbie di Imola (Gialle), si interrompe bruscamente lungo la valle del F. Reno, dove si nota una sensibile dislocazione del fronte appenninico che, nella parte orientale, risulta spostato di 3 km a nord. Queste dislocazioni ad andamento antiappenninico, caratterizzate da una storia geologica assai complessa, sono presenti lungo altri allineamenti come la linea dell'Idice.

Lungo il bordo appenninico esterno e la fascia di pianura antistante, gli elementi traslati ed impilati vengono a formare un vero e proprio prisma di accrezione tettonica neogenico che, sia per l'entità dell'ampliamento, sia per la complessa interferenza dell'attività tettonica con la deposizione, conferiscono al sistema il carattere di una marcata fossa tettonica.

Più a sud il territorio circostante è caratterizzato dal contatto tettonico per faglia verticale fra i terreni delle Successioni Epiliguri, presenti con la F.ne di Pantano (PAT) e F.ne di Cigarello (CIG), con i sottostanti *mélanges* o olistostromi (corpi sedimentari caotici sin-tettonici a tessitura a blocchi in matrice con aspetto brecciato) dell'Oligocene superiore-Miocene inferiore, ed i terreni neoautoctoni rappresentati dalle Argille Azzurre e dalle Sabbie gialle.

Nella media pianura le alluvioni sono per lo più riferibili ai fiumi appenninici, caratterizzati da una rete drenante orientata da SW a NE. Gli apporti fluviali hanno ricoperto i sedimenti marini che, nel settore del margine appenninico tra il T. Samoggia ed il T. Lavino, sono in successione continua dalla base del Pliocene al Pleistocene inferiore.

Di notevole interesse appaiono le strutture tettoniche attive evidenziate nella “Carta Sismotettonica della regione Emilia-Romagna” (figura 1) Ovvero:

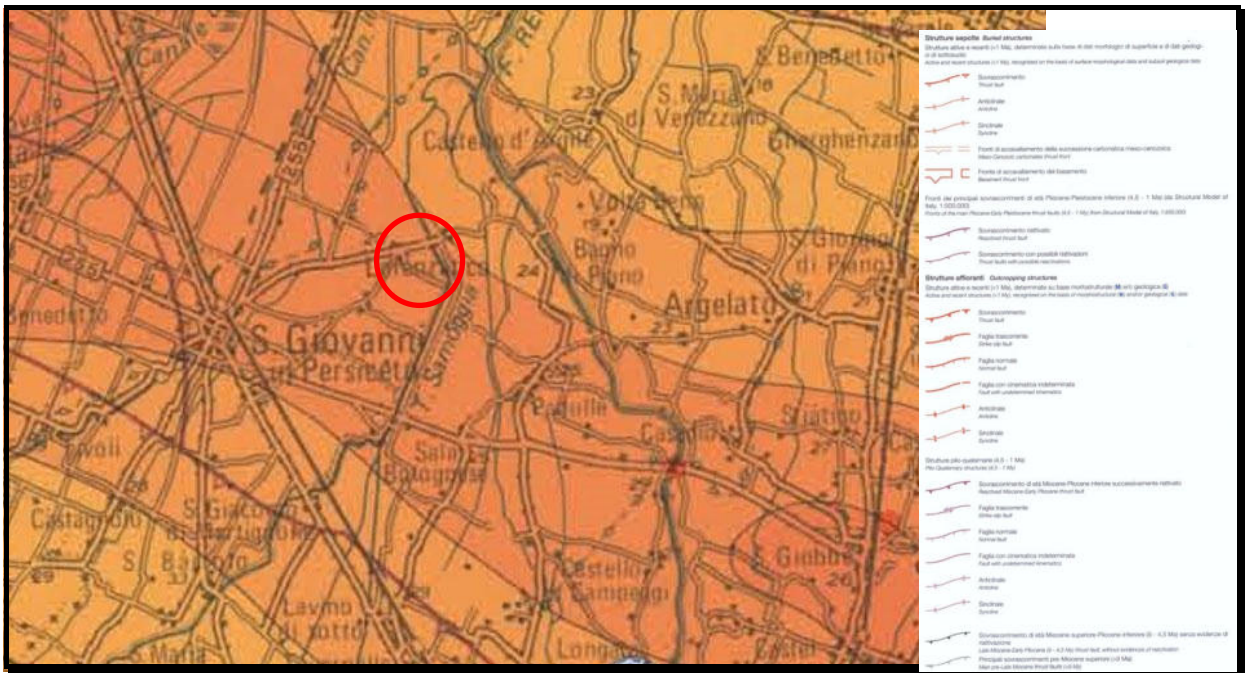


Figura 1: Estratto dalla Carta della Sismotettonica della Regione Emilia-Romagna –

STRUTTURE SEPOLTE

- Sovrascorrimento recente;
- Sovrascorrimento riattivati nell’area pedeappenninica;
- Sovrascorrimento con possibile riattivazione.

Queste strutture tettoniche sono aree sismogenetiche capaci di generare terremoti di cui si parlerà più avanti in testo.

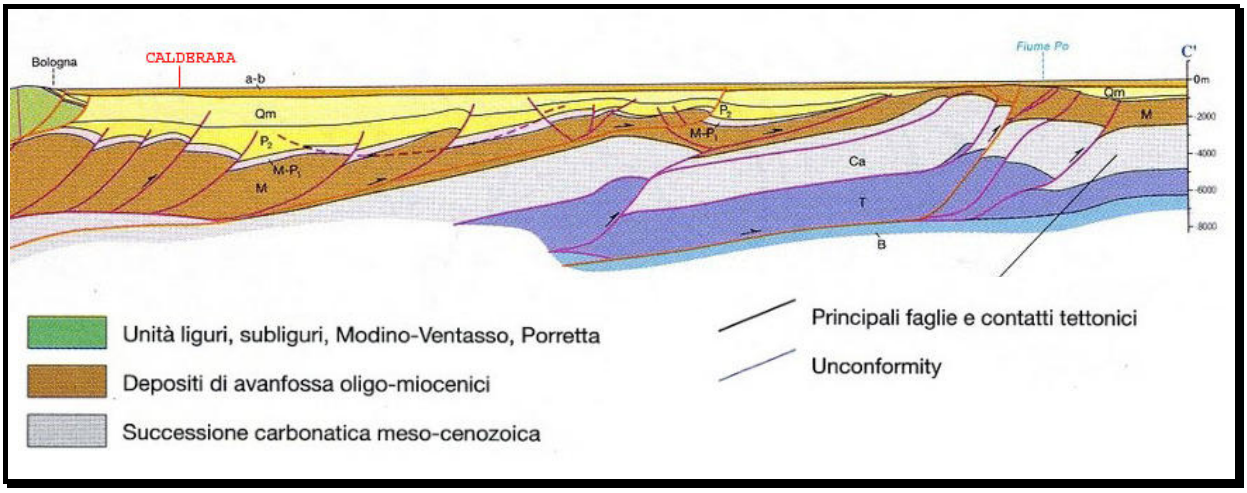


Figura 2: Estratto dalla sezione C-C’ della Carta Sismotettonica della Regione Emilia-Romagna.

4.1 LITOSTRATIGRAFIA QUATERNARIA E SUPERFICIALE

Per la descrizione della successione stratigrafica riguardante i depositi quaternari presenti nel settore della pianura bolognese s.l. ospitante il sito oggetto d'intervento, si fa riferimento al quadro stratigrafico del sottosuolo padano adriatico riportato in fig. 3. L'assetto schematizzato evidenzia le principali unita stratigrafiche, definendone la gerarchia in termini di Sequenze Deposizionali.

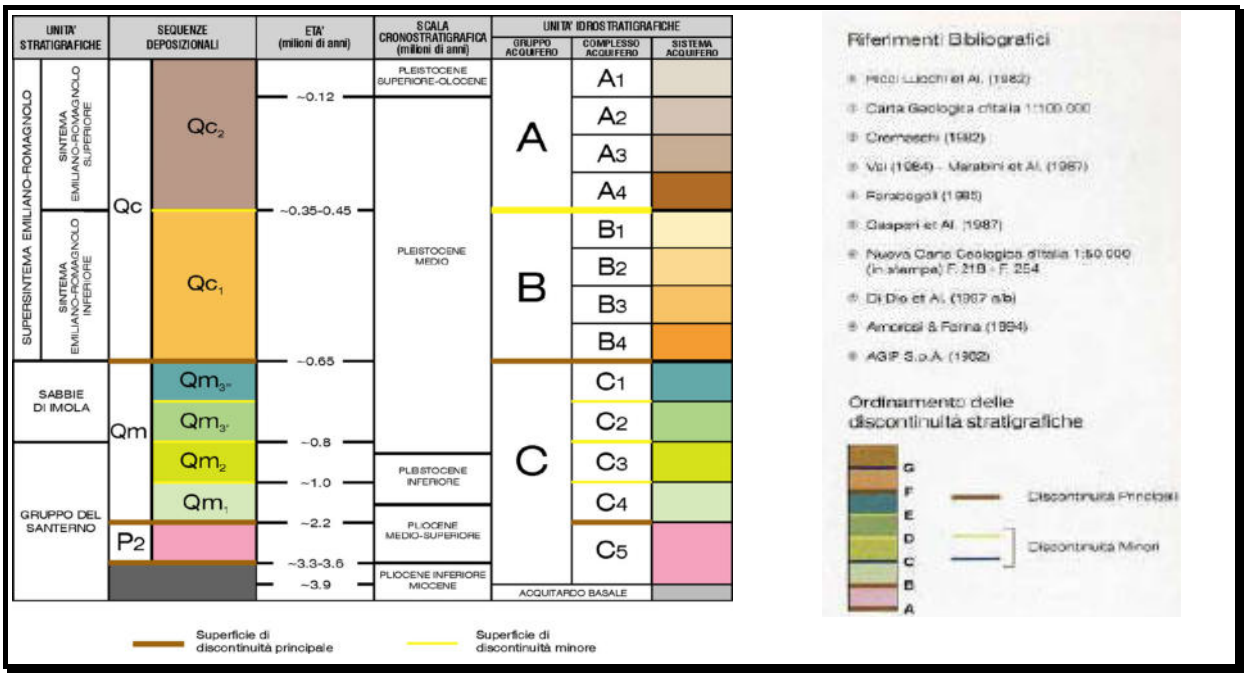


Figura 3: Gruppi acquiferi riferiti allo schema geologico-stratigrafico dell'Emilia-Romagna.

La suddivisione proposta tiene conto del fatto che i processi che hanno portato al riempimento del bacino padano, passando da una sedimentazione marina ad una continentale, sono avvenuti a seguito di eventi tettonico sedimentari generalmente molto intensi e discontinui, separati nel tempo da periodi di forte subsidenza bacinale e movimenti ridotti delle strutture compressive; la sussistenza e la successione di tali eventi è testimoniata dalle numerose superfici di discontinuità stratigrafica individuate e cartografate sul Margine Appenninico Padano. Attraverso i dati sismici e di pozzo, è stato possibile estendere tali superfici di discontinuità anche al sottosuolo della pianura e definirne, conseguentemente, il quadro stratigrafico. In tal senso, facendo riferimento allo schema di figura 2, i depositi plioquaternari di riempimento del bacino padano possono essere suddivisi, sulla base delle principali superfici di discontinuità riconosciute, in 3 Sequenze Principali, ovvero in 3 Supersintemi (o Allogruppi), secondo la terminologia delle Unconformity Bounded Stratigraphic Units (UBSU) utilizzata nella cartografia geologica di base della pianura (Carta Geologica in scala 1:50.000 della Regione Emilia Romagna):

1. Supersintema del Pliocene medio superiore;

2. Supersintema del Quaternario Marino;
3. Superintema Emiliano Romagnolo.

Tali sequenze rappresentano, da un punto di vista sedimentologico, la risposta alle tre principali fasi tettoniche di sollevamento regionale verificatesi, la prima tra circa 3.9 e 3.4 milioni di anni, la seconda tra 2.4 e 2.2 m.a., e la terza tra 0.80 e 0.65 m.a..

La presenza di superfici di discontinuità minori, legate a eventi tettonici secondari a carattere più locale, o ad oscillazioni climatiche eustatiche, hanno poi permesso di suddividere le Sequenze Principali in sequenze di rango inferiore, ovvero in Sintemi e Subsintemi. Tralasciando le due Sequenze Principali più antiche (Supersintema del *Pliocene medio-superiore* e Supersintema del Quaternario Marino), di scarso interesse per il presente studio data la loro profondità, si riportano di seguito i principali elementi caratterizzanti il Supersintema Emiliano Romagnolo (SER o AES), corrispondente alla porzione sommitale dei sedimenti di riempimento del bacino padano, la cui deposizione è avvenuta, come già ricordato, in risposta al sollevamento tettonico iniziato alla fine del *Pleistocene inferiore* e continuata nel *Pleistocene medio* fino a circa 0.65 m.a. Il Supesintema Emiliano Romagnolo, suddiviso nel Sintema Emiliano Romagnolo Inferiore (SERI o AEI), compreso tra 0.65 e 0.45 m.a., e nel Sistema Emiliano Romagnolo Superiore (SERS o AES), compreso tra 0.45 m.a. e l'attuale, è definito dall'insieme dei depositi quaternari di origine continentale affioranti sul margine appenninico padano e dai sedimenti ad essi correlati nel sottosuolo della pianura e del mare.

Delle due sequenze deposizionali di rango inferiore, il Sintema Emiliano Romagnolo Inferiore, il cui tetto è stato individuato a profondità mediamente comprese tra 220 e 280 metri, risulta essere caratterizzato da cicli deposizionali trasgressivo regressivi costituti da alternanze di depositi fini limoso argillosi e grossolani sabbioso ghiaiosi, riconducibili ad ambienti di piana alluvionale e, soprattutto, di piana fluvio-deltizia e piana costiera. Anche per quanto riguarda il Sintema Emiliano Romagnolo Superiore, i pertinenti depositi risultano essere organizzati in diversi cicli deposizionali sovrapposti, in cui sedimenti prevalentemente fini, riconducibili ad ambienti di argine e di piana inondabile, si alternano a sedimenti più grossolani, riconducibili ad ambienti di canale fluviale. Essendosi ormai esaurite le principali fasi tettoniche, la strutturazione deposizionale di tipo ciclico sopra schematizzata è da ricondurre, principalmente, a variazioni climatiche ed, in particolare, alle diverse fasi glaciali e interglaciali che si sono alternate durante il *Pleistocene*, nonché all'azione combinata della subsidenza, legata sia a cause tettoniche profonde, sia alla compattazione differenziale dei sedimenti plio-quaternari. Da un punto di vista paleogeografico le diverse fasi climatiche hanno determinato movimenti significativi della linea di costa adriatica, con avanzamenti massimi in corrispondenza delle fasi glaciali (regressione), ed arretramenti in corrispondenza delle fasi interglaciali (trasgressione). Al riguardo, si stima che durante la fase culminante dell'ultimo periodo glaciale (Wurm), iniziato circa 70.000 anni fa e terminato circa 15.000 anni fa, l'abbassamento del livello marino sia stato di quasi 100 metri rispetto al livello attuale; ciò ha portato ad una fase di forte alluvionamento dei corsi d'acqua

ed alla deposizione di ingenti spessori di sedimenti continentali terrestri, lacustri e fluvio palustri, con conseguente espansione della pianura su gran parte dell'Adriatico settentrionale.

Gli ambienti deposizionali prevalenti dei sedimenti presenti sono depositi di canale, argine e rotta fluviale, oltre che di piana inondabile in aree interfluviali.

Entrambe le aree di studio sono dunque dominate da depositi alluvionali riferibili al Sistema Emiliano Romagnolo superiore AES della "Nuova Carta Geologica della Regione Emilia-Romagna"; si tratta di ghiaie, sabbie, limi ed argille di piana intravalliva, di conoide e di piana alluvionale. Sintema parzialmente suddiviso in subsintemi limitati, in affioramento, da scarpate di terrazzo fluviale e paleosuoli e nel sottosuolo della pianura da bruschi contatti fra depositi fini alluvionali e palustri su depositi grossolani di conoide e di piana (*Pleistocene medio – Olocene*).

Come meglio precisato le aree si trovano all'interno dei terreni dell'Unità di Modena AES8a; l'AES8a è caratterizzato da ghiaie, sabbie, limi ed argille. Il limite superiore, sempre affiorante, è dato da un suolo calcareo di colore bruno olivastro e bruno grigiastro privo di reperti archeologici romani, o più antichi, non rimaneggiati. Il limite inferiore è dato da una superficie di erosione fluviale nelle aree intra, il cui spessore massimo in pianura risulta 7 metri, nel sottosuolo circa 10m (*Età post-romana (IV-VI sec. d.C. - Attuale; datazione archeologica)*).

I sedimenti neoautoctoni alluvionali poggiano in profondità sui sedimenti continentali della Successione neogenico - quaternaria del margine appenninico padano

Dal punto di vista stratigrafico, quindi, il territorio in esame si presenta di una complessità non trascurabile dovuta ad interazioni strutturali fra unità litostratigrafiche differenti mentre, dal punto di vista stratigrafico locale, l'area di futuro intervento è più facilmente definibile.

Da ricerche bibliografiche si rileva che la litologia di superficie è costituita da suoli a diffusa componente organica ed a grado di drenaggio interno medio basso che ricoprono con continuità l'area fino alla roccia alterata ed alla roccia madre sottostante.

Sono suoli derivati da sedimenti alluvionali e lacustri recenti ("Carta dei suoli argillosi d'Italia"), principalmente *Eutric Fluvisols*, *Calcaric Fluvisol*, *Eutric* e *Fluvi-Eutric Cambisols, Fluvi-Vertic Cambisols*.

4.2 IDROLOGIA SUPERFICIALE E IDROGEOLOGIA

Quanto di seguito riportato è stato in parte tratto dalla Relazione Tecnica contenuta nella pubblicazione "Riserve Idriche Sotterranee della Regione Emilia Romagna" (edizioni S.E.L.C.A.– Firenze).

Nel sottosuolo della Pianura Padana e sul Margine Appenninico Padano, sono stati riconosciuti tre Gruppi Acquiferi separati da barriere di permeabilità con estensione regionale, informalmente denominati Gruppo Acquifero **A**, **B** e **C** a partire da piano campagna. Il Gruppo Acquifero **A** è attualmente sfruttato in modo intensivo, il Gruppo Acquifero **B** è sfruttato solo localmente, il Gruppo

Acquifero **C**, isolato rispetto la superficie per gran parte della sua estensione, è raramente sfruttato.

I Gruppi Acquiferi **A**, **B**, **C** sono a loro volta suddivisi in tredici U.L.S. (Unità Litostratigrafico–Sequenziale), gerarchicamente inferiori, denominati Complessi Acquiferi.

La differenziazione gerarchica si basa su:

- volume complessivo di acquiferi utili in ciascuna Unità;
- spessore, continuità ed estensione areale del livello acquitardo o impermeabile di ciascuna Unità.

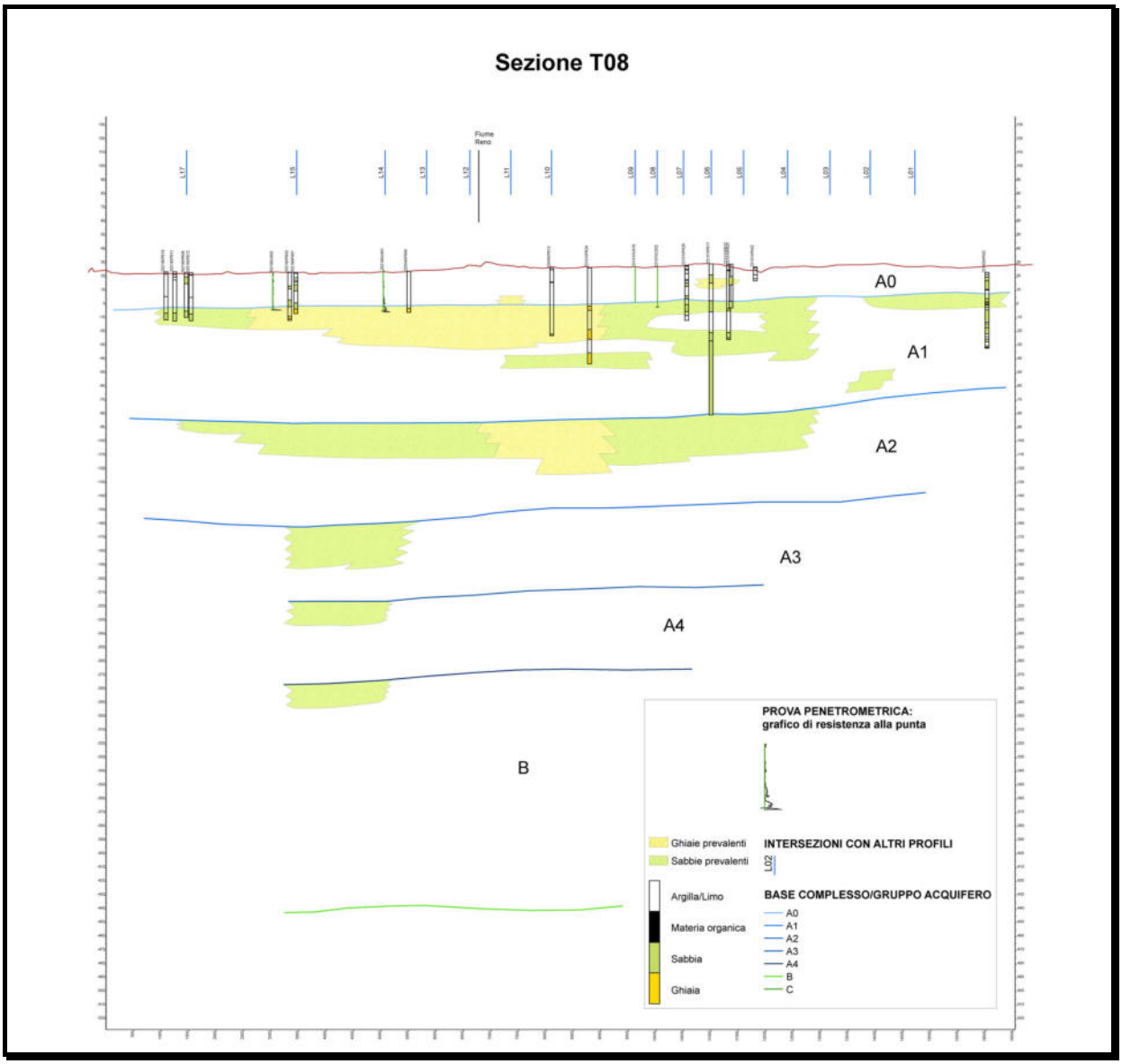


Figura 4: Schema dei rapporti stratigrafici della pianura Bolognese – Sezione T08.

Per quanto riguarda il sito di San Giovanni in Persiceto il limite dell'acquifero A è tra – 250 e -300 m, mentre per il B è a circa -300m.

Per quanto riguarda lo spessore cumulativo degli acquiferi utili relativi al gruppo acquifero **A**, intendendo per acquiferi utili quelli sfruttabili per uso idropotabile e/o per uso agricolo-industriale e la cui base corrisponde all'interfaccia tra acqua dolce e salmastra, i dati a disposizione evidenziano come, nella zona del territorio Comunale di San Giovanni in Persiceto, la potenza dell'acquifero A risulta tra 40,0 e 60,0 m e dell'acquifero B tra 0,0 e 20,0 m.

Per quanto riguarda lo spessore cumulativo degli acquiferi utili relativi al gruppo acquifero **C**, intendendo per acquiferi utili quelli sfruttabili per uso idropotabile e/o per uso agricolo-industriale e la cui base corrisponde all'interfaccia tra acqua dolce e salmastra, tra 80,0 e 100,0 m.

A migliore definizione si ricorda inoltre come, dal punto di vista idrogeologico, si intenda acquifero "*una formazione idrogeologica permeabile che permette il deflusso significativo di una falda idrica sotterranea e la captazione di quantità apprezzabili d'acqua con mezzi economici*".

In base alla definizione sopra riportata, la falda deve quindi avere un deflusso, il quale dovrà essere caratterizzato da spostamenti a prevalente componente orizzontale. Tale condizione è realizzabile in terreni dotati di adeguate caratteristiche di permeabilità e quindi, solo in tali casi, è identificabile una falda freatica in senso stretto. Nei restanti casi l'acqua presente corrisponde in realtà ad acqua di saturazione o di infiltrazione superficiale a movimento prevalentemente verticale anche se, di fatto, viene anch'essa comunemente definita "falda freatica".

Sulla base delle notizie bibliografiche, delle formazioni geologiche presenti e della posizione dell'area di studio (area di media pianura) la prima falda superficiale risulta a carattere stagionale, legata alle condizioni meteoclimatiche, e si trova nei primi metri a contatto fra litotipi diversi (sabbie e ghiaie permeate d'acqua a contatto con argille impermeabili); più probabile invece la presenza di falde più profonde determinate dal controllo tettonico (faglie e fessurazioni delle rocce sottostanti) e da contatti fra litotipi a differente grado di permeabilità che consentono il formarsi di riserve idriche sotterranee come nel caso delle Sabbie di Imola con l'acquifero del gruppo **C**; in considerazione dell'assetto morfologico e clivometrico del piano campagna non si rilevano settori con problemi di deflusso difficoltoso. Si rammenta comunque che, data la caratterizzazione litologica dei terreni presenti nell'area, sono <u>assai</u> probabili falde a carattere stagionale che permeano i primi metri di terreno. E' quindi consigliabile in fase di progettazione considerare queste acque di circolazione superficiale ed interagire con esse.

Si rammenta comunque, che, data la caratterizzazione litologica dei terreni presenti nell'area, sono pertanto <u>assai</u> probabili falde a carattere stagionale che permeano i primi metri di terreno. E' quindi consigliabile, in fase di progettazione, considerare queste acque di circolazione superficiale ed interagire con esse.

I litotipi presenti, sabbie, ghiaie, limi sabbiosi e argilla, sono caratterizzati i primi da un grado di

porosità alto ed una elevata permeabilità (dovuta al grado di addensamento della sabbia), con porosità totale compresa fra 5÷20%. I secondi (argille) sono caratterizzati da una porosità primaria alta ed una secondaria bassa; la permeabilità è data fondamentalmente dalla porosità (sono rocce tendenzialmente impermeabili).

La circolazione idrica superficiale deriva direttamente dalle acque di infiltrazione e di ruscellamento; sono dunque importanti i meccanismi di percolazione (discesa dell'acqua verso il basso attraverso il terreno), con movimenti d'acqua lungo gli interstrati fra i litotipi a grado di permeabilità differente, ed i fenomeni sia capillari che di evapotraspirazione (risalita dell'acqua verso l'alto).

La rete idrografica superficiale è rappresentata fossi naturali ed antropici (es. Scolo Dosolo e Canale Collettore Acque basse Bagnetto) che confluiscono a nord verso le reti di Bonifica o verso il Torrente Samoggia o il Torrente Lavino, quali collettori naturale principalie, ed è caratterizzata da corsi d'acqua a carattere stagionale con forti piene nei periodi di maggiori piovaschi, e portate quasi nulla nei periodi di magra.

In perfetta coerenza con quanto sopra riportato, per l'area in esame si possono indicare le seguenti caratteristiche idrogeologiche:

- profondità della falda freatica superficiale pari a circa -0,4 - -2,0 m dal p.c;
- direzione di deflusso: da Sud- Ovest verso Nord- Est;

Dai riscontri dei dati storici si può riscontrare come le aree in esame ed i suoi immediati dintorni possano essere interessate da fenomeni di alluvionamenti locali.

Alcune veloci considerazioni sullo stato degli acquiferi della pianura bolognese.

Gli acquiferi della pianura alluvionale costituiscono l'acquedotto naturale per eccellenza e sono utilizzati da millenni per rifornire d'acqua le comunità umane e le città. Il bolognese non fa eccezione: fino all'inizio del 1900 molte migliaia di pozzi freatici punteggiavano la pianura agricola e si concentravano nei paesi e nella città.

La prima ricostruzione del campo di moto del freatico bolognese è stata ottenuta nel 1994 (G. Viel, 1995), controllata per condizioni di piena nel 1996, successivamente arricchita di nuovi dati nel 1998 (G.P. Artioli et Al, 1997; G. Viel, 1998) e nel 2002 (G. Viel, S. Sangiorgi et Al, 2003). Il confronto tra le condizioni di piena e di magra dell'insieme delle falde superficiali è stato possibile solo nella pianura in destra Reno, fin poco oltre l'Idice, su un intervallo temporale di circa 6 anni. L'esito ottenuto mostra come le escursioni siano in genere di entità modesta (attorno o inferiori al metro), i valori negativi maggiori (fino oltre 4 metri) si distribuiscano lungo il Reno (Castel Maggiore, Calderara, Sala Bolognese), e tra Bentivoglio e Minerbio (Cà de Fabbri). Anche al confine orientale del Comune di Budrio si sono rilevate tendenze ad escursioni molto forti anche maggiori di 2 metri; qui però la falda superficiale è confinata e questi abbassamenti sono da connettere ad eccessivi prelievi locali.

Il campo di moto della falda superficiale risulta fortemente condizionato dalla presenza di 3

ampie aree, in cui il freatico è depresso fino alla sua scomparsa, che contengono i 5 maggiori campi di sollevamento dell'acquedotto bolognese. Ai margini settentrionali di queste 3 aree di abbassamento freatico si assiste all'inversione del senso di moto naturale delle acque sotterranee: sono dirette dalla pianura verso l'Appennino.

Dalla carta delle piezometrie medie relative agli anni 2005 e 2006 per la conoide del Reno-Savena (fig. 6, Progetto IA/RER_06_003), si osservano come le isopieze relative alla porzione centro orientale della conoide mostrano la situazione idrogeologica più profonda, in cui si osservano gli effetti dei prelievi dei campi pozzi acquedottistici che richiamando acqua da ovest generano una depressione piezometrica anche nella zona in esame con valori piezometrici fra -10,0 e 0,0 m s.l.m.

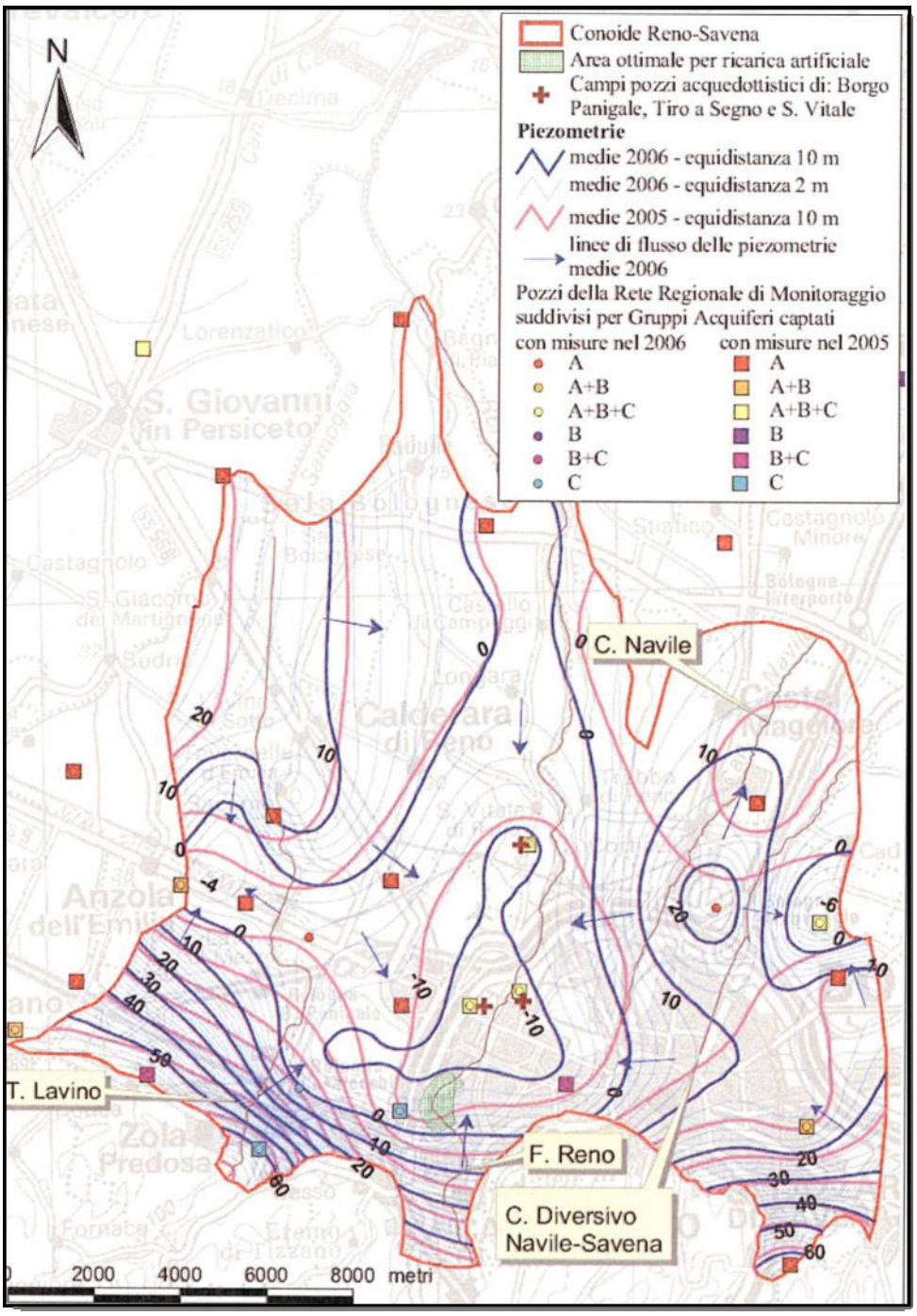


Figura 5: Estratto dalla Carta delle piezometrie medie relative agli anni 2005 e 2006 per la conoide del Reno-Savena (Progetto IA/RER_06_003)

Tutto ciò è il prodotto dall'eccessivo prelievo ed estrazione di acqua dalle falde che nell'area di studio ha evidenziato una grande area di forte soggiacenza (G. Viel) corrispondente agli apparati deposizionali del Reno, e del Lavino (oltre -70 metri). Si tratta di un immenso territorio corrispondente

ai Comuni di: Bologna (pianura ovest), Zola Predosa (pianura), Anzola, Calderara, Castel Maggiore (interamente), Casalecchio (pianura), Sala Bolognese, Argelato, Bentivoglio, S. Giorgio di Piano (in parte), caratterizzato da un cono dinamico prodotto dal prelievo delle stazioni di pompaggio HERA.

4.3 SUBSIDENZA

Nell'area, in considerazione dell'enorme spessore di sedimenti alluvionali a granulometria fine e degli elevati prelievi di acqua di falda idrica sotterranea, è soggetta ad una progressiva e continua subsidenza. Dagli studi più recenti eseguiti sull'abbassamento del suolo nella pianura bolognese (Figura 6) si evidenzia come, il valore della subsidenza in questo settore della pianura sia dell'ordine di 10÷30 mm/anno (2002-2006), con valori maggiori nel settore SO, nei pressi di Calderara di Reno (circa 30 mm/anno) e minori verso la parte nord. Per quanto concerne invece la Cartografia Interattiva di Arpae, nel periodo temporale 2011-2016 (Figura 9), l'area di San Giovanni in Persiceto è stata soggetta a un abbassamento medio fra -7,5 e -12,5 mm/anno. L'andamento delle isocinetiche di abbassamento del suolo è irregolare in quanto influenzato dalle maggiori quantità di acqua di falda prelevate in corrispondenza dei paleoalvei (maggiore concentrazione di emungimenti). Il fenomeno della subsidenza nella pianura bolognese è generato in minima parte da un progressivo costipamento dei sedimenti alluvionali (subsidenza naturale) e prevalentemente da un eccessivo emungimento delle acque sotterranee (subsidenza artificiale).

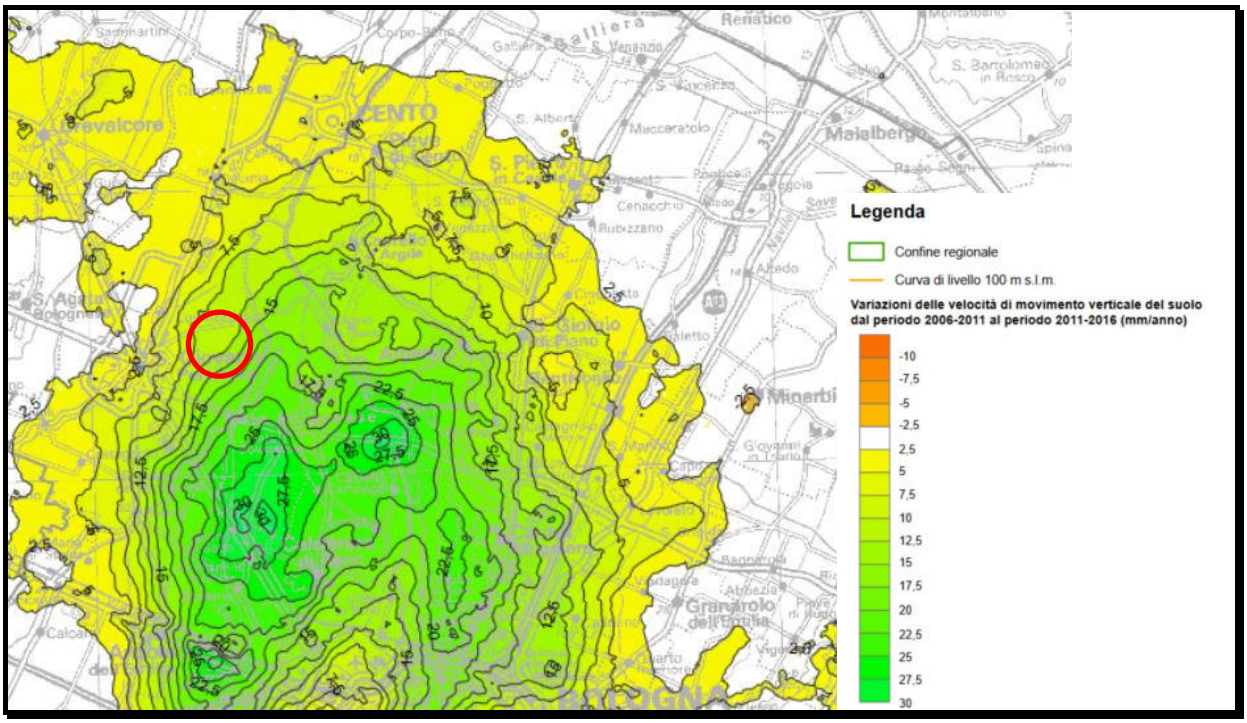


Figura 6: Estratto dalla Carta della velocità del movimento verticale del suolo nel periodo 2006-2016 "Cartografia Regione Emilia-Romagna"

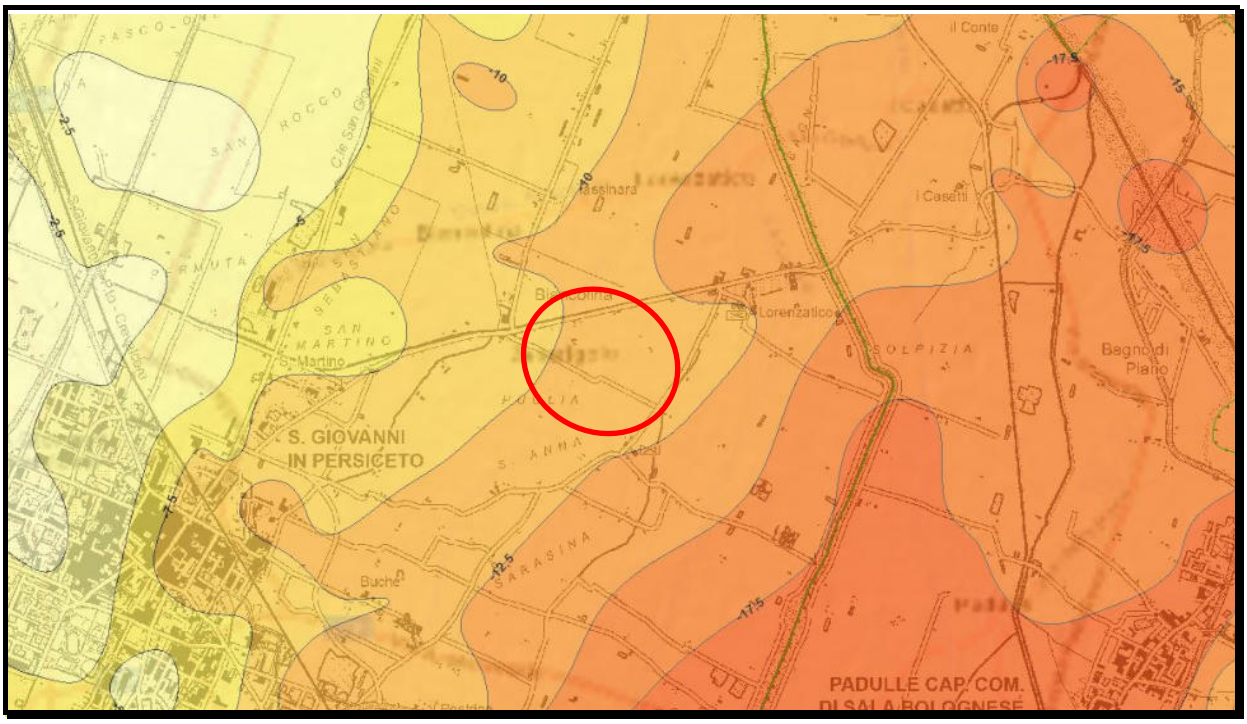


Figura 7: Estratto dalla Cartografia interattiva di ARPAE – Suolo-Subsidenza.

5. Vincoli Urbanistici

Secondo il P.T.M. – Piano Territoriale Metropolitano della Provincia di Bologna, aggiornato al 16 maggio 2022, l'area in esame si trova all'interno dei seguenti vincoli:

- Tav.1 "Carta della Struttura" – aree agricole della pianura alluvionale (art. 16 e 18);
- Tav.2 "Carta degli ecosistemi" – aree agricole della pianura alluvionale (art. 16 e 18);
- Tav.3 "Carta di area vasta del rischio idraulico, rischio da frana e dell'assetto dei versanti": area sottoposta a controllo degli apporti d'acqua di pianura, scenario P3 derivante dal Reticolo Naturale Principale e Secondario – RP (Art. 30);
- Tav.4 "Carta di area vasta delle aree suscettibili di effetti locali": Area C – sedimenti prevalentemente fini di pianura;

Va sottolineato come il percorso del cavidotto attraversi zone di attenzione per instabilità da liquefazione o densificazione (Area L), per cui è stata effettuata un'analisi di Risposta Sismica Locale di III livello.

Secondo il P.S.C. – Piano Strutturale Comunale dell'Unione Terre d'Acqua, nella carta QC.6/T2 inerente il Suolo – Sottosuolo – Acqua, l'area risulta interessata da:

- Aree caratterizzate da liquefazione dei terreni molto probabile in caso di sisma (FS<1);

- Subsidenza totale del periodo 1983 – 1999 → 600-800 mm.

Secondo il P.S.C. – Piano Strutturale Comunale del comune di San Giovanni in Persiceto, nella carta PSC.SG/T.2f inerente i vincoli, l'area risulta interessata da:

- Area a vulnerabilità naturale dell'acquifero elevata o estremamente elevata (art. 57 NTA PSC);
- Aree potenzialmente inondabili (art. 61 NTA PSC);
- Canali storici (art. 29 NTA PSC);
- Alvei attivi ed invasi dei bacini idrici (art. 49 NTA PSC);
- Fasce di tutela fluviale (PTCP) (art. 50 NTA PSC).

5. Indagini geognostiche, prospezioni geofisiche e prove di laboratorio

Come precedentemente indicato, per approfondire la conoscenza diretta della litologia, della geometria e delle caratteristiche meccaniche del sottosuolo, nel gennaio 2024 si è fatta eseguire una campagna indagini geognostiche formata da 10 indagini penetrometriche di tipo statico meccanico (Cone Penetration Test); per quanto riguarda le prove penetrometriche con punta elettrica e piezocono (CPTu) ne sono state effettuate 6. La campagna di indagini geognostiche è stata completata con tre prelievi di campioni indisturbati con fustella a pareti sottili tipo shelby destinati ad un laboratorio geotecnica per prove sui materiali che si andranno a sommare alle precedenti valutazioni fatte sui materiali. Per quanto riguarda l'indagine sismica, è stata effettuata un'indagine condotta con la metodologia M.A.S.W. associata a tomografo digitale TROMINO ENGY" (*Micromed* S.p.A.). Tutte le indagini sono ubicate nella planimetria di Tav. 2.

5.1 PROVE PENETROMETRICHE STATICHE MECCANICHE (CPT)

La prova penetrometrica statica CPT (di tipo meccanico), eseguita con uno strumento avente una spinta nominale pari a 200 kN, consiste essenzialmente nella misura della resistenza alla penetrazione di una punta meccanica di dimensioni e caratteristiche standardizzate, infissa nel terreno a velocità costante (v = 2 cm/s ± 0.5 cm/s).

La penetrazione avviene attraverso un dispositivo di spinta (martinetto idraulico) opportunamente zavorrato, che agisce su una batteria doppia di aste (aste esterne cave ed aste interne piene coassiali), alla cui estremità inferiore è collegata la punta. Lo sforzo necessario per l'infissione viene determinato a mezzo di un opportuno sistema di misura, collegato al martinetto idraulico.

Le caratteristiche del penetrometro da 200 kN utilizzato sono le seguenti:

- Punta conica meccanica ϕ =35.7 mm, angolo di apertura α=60° (area punta Ap = 10 cm²).

- Manicotto laterale di attrito tipo “Begemann” (ϕ =37.5 mm, h =133 mm, sup. lat. Am = 150 cm²).
- Velocità di avanzamento costante V = 2 cm/sec (± 0.5 cm/sec).

Sulla batteria di aste esterne può essere installato un anello allargatore per diminuire l’attrito sulle aste, facilitandone l’approfondimento.

Nei diagrammi di resistenza e nelle analoghe tabelle allegate sono riportati i seguenti valori di resistenza, rilevati ad intervalli regolari di 20 cm:

- Rp (kg/cm²) = resistenza alla punta (conica)
- RL (kg/cm²) = resistenza laterale (manicotto)

5.2 PROVE PENETROMETRICHE STATICHE ELETTRICHE CON PIEZOCONO (CPTU)

La prova con punta elettrica con piezocono (CPTu) è l'evoluzione della prova penetrometrica statica con punta meccanica (CPT). I valori di resistenza del terreno non vengono più rilevati con un sistema di aste scorrevoli che trasmettono i carichi (di rottura del terreno) ad un manometro (o cella di carico) di superficie, bensì con degli estensimetri posti direttamente all'interno della punta. Questi estensimetri, con deformazioni meno che millimetriche dei componenti della punta (cono e manicotto), producono dei segnali elettrici proporzionali alle variazioni di carico e quindi alle componenti di resistenza del terreno. I segnali elettrici (analogici) vengono digitalizzati con convertitori direttamente posti all'interno della punta (nel caso ormai più frequente di “digital cone”) e vengono memorizzati in un circuito interno. I segnali digitalizzati possono essere inviati direttamente in superficie dove è presente (oltre al circuito di sincronizzazione della profondità) una apposita “centralina” con funzioni di memorizzazione, stampante, salvataggio dati su dischetto ed eventuale trasmissione a PC.

Nella punta CPTu, oltre ai sensori che sono nella punta CPTE, è presente anche un sensore di pressione. Il sensore misura la pressione interstiziale attraverso un filtro poroso in bronzo, ubicato tra la base del cono ed il manicotto, disareato e saturato con olio siliconico.

Le caratteristiche del penetrometro elettrico sono identiche a quelle dello statico:

- Punta conica ϕ =35.7 mm, angolo di apertura α=60° (area punta Ap = 10 cm²).
- Manicotto laterale (ϕ =37.5 mm, h =133 mm, sup. lat. Am = 150 cm²).
- Velocità di avanzamento costante V = 2 cm/sec (± 0.5 cm/sec).

Inoltre il penetrometro statico elettrico è stato fatto oggetto di standardizzazione (ASTM, 1979).

5.3 INDAGINI GEOFISICHE

E’ stata condotta una seconda campagna di indagini di tipo geofisico per mezzo del tomografo digitale Tromino.

Il Tromino misura il rumore di fondo (microtremore) e lo utilizza come funzione di eccitazione per identificare in maniera passiva le frequenze di risonanza degli edifici e del suolo sede del futuro

intervento edilizio ed in prima approssimazione le Vseq. Le frequenze di risonanza, specie se combaciano quella del suolo con quella tipica del fabbricato in costruzione, sono in diretta relazione con l'amplificazione sismica considerata da molti la prima causa di danno e di distruzione durante un terremoto.

Il rumore di fondo (microtremore) presente ovunque sulla superficie terrestre ed associato sia a fenomeni atmosferici che all'attività antropica, è relativo ad oscillazioni molto piccole (10^{-15} m/s^2), con componenti spettrali che vengono scarsamente attenuate nello spazio e misurabili con tecniche di acquisizione passive.

Tutte le onde elastiche, dalla sorgente al sito, subiscono modifiche al loro tragitto ed attenuazioni in relazione alla natura del suolo attraversato; le informazioni stratigrafiche contenute nei microtremori sono sovrapposte al rumore casuale e possono essere estratte attraverso metodologie come quella di Nakamura dei rapporti spettrali (HVSR – horizontal to vertical spectral ratio).

Tale tecnica è utilizzata anche per la determinazione dell'amplificazione sismica locale e per stimare le frequenze principali di risonanza del sottosuolo, dati molto utili per la progettazione ingegneristica nelle strutture.

Il metodo considera i microtremori come composti in massima parte da onde di superficie (di Rayleigh) nelle componenti orizzontali e verticali, che vengono amplificate per effetto di sito a causa della presenza di discontinuità stratigrafiche nel sottosuolo. E' quindi possibile ricostruire la forma spettrale del microtremore, in cui i picchi alle diverse frequenze rappresentano il rapporto tra la componente orizzontale e verticale dei segnali registrati.

La frequenza dei diversi picchi è funzione della velocità delle onde sismiche nei diversi strati e del loro spessore, secondo la seguente relazione:

$$f = V_s/4h$$

La curva HVSR/f mostra quindi come massimi relativi le frequenze di risonanza dei vari strati alle diverse profondità, per cui conoscendo attraverso i sondaggi o prove penetrometriche gli spessori degli strati è possibile ottenere una stima della velocità delle onde sismiche nel sottosuolo e nello specifico anche una misura della Vseq.

Le indagini sono state inoltre condotte con la metodologia MASW (Multichannel Analysis of Surface Waves). Nella maggior parte delle indagini sismiche per le quali si utilizzano le onde compressive, più di due terzi dell'energia sismica totale generata viene trasmessa nella forma di onde di Rayleigh, la componente principale delle onde superficiali. Ipotizzando una variazione di velocità dei terreni in senso verticale, ciascuna componente di frequenza dell'onda superficiale ha una diversa velocità di propagazione (chiamata velocità di fase) che, a sua volta, corrisponde ad una diversa lunghezza d'onda per ciascuna frequenza che si propaga. Questa proprietà si chiama dispersione. Sebbene le onde superficiali siano considerate rumore per le indagini sismiche che utilizzano le onde

di corpo (riflessione e rifrazione), la loro proprietà dispersiva può essere utilizzata per studiare le proprietà elastiche dei terreni superficiali. La costruzione di un profilo verticale di velocità delle onde di taglio (Vs), ottenuto dall'analisi delle onde piane della modalità fondamentale delle onde di Rayleigh è una delle pratiche più comuni per utilizzare le proprietà dispersive delle onde superficiali. Questo tipo di analisi fornisce i parametri fondamentali comunemente utilizzati per valutare la rigidezza superficiale, una proprietà critica per molti studi geotecnici.

Nelle prospezioni sismiche per le quali si utilizzano le onde di tipo P, la maggior parte dell'energia sismica totale generata si propaga come onde superficiali di tipo Rayleigh. Ipotizzando una variazione di velocità dei terreni in senso verticale, ciascuna componente in frequenza di queste onde è caratterizzata da una diversa velocità di propagazione (chiamata velocità di fase) e quindi da una diversa lunghezza d'onda. Questa proprietà si chiama dispersione. Sebbene le onde superficiali siano considerate rumore per le indagini sismiche che utilizzano le onde di volume (riflessione e rifrazione), la loro proprietà dispersiva può essere utilizzata per studiare le proprietà elastiche dei terreni superficiali.

La costruzione di un profilo verticale di velocità delle onde di taglio (Vs), ottenuto dall'analisi delle onde piane della modalità fondamentale delle onde di Rayleigh è una delle pratiche più comuni per utilizzare le proprietà dispersive delle onde superficiali.

Per ottenere un profilo verticale di velocità Vs bisogna produrre un treno d'onde superficiali a banda larga e registrarlo minimizzando il rumore. Sono state utilizzate una molteplicità di tecniche diverse nel tempo per ricavare la curva di dispersione, ciascuna con i suoi vantaggi e svantaggi.

La configurazione base di campo e la routine di acquisizione per la procedura MASW sono generalmente le stesse utilizzate in una convenzionale indagine a rifrazione. MASW può essere efficace anche con solo dodici canali di registrazione collegati a geofoni verticali a bassa frequenza (4.5 Hz).

Le componenti a bassa frequenza (lunghezze d'onda maggiori), sono caratterizzate da forte energia e grande capacità di penetrazione, mentre le componenti ad alta frequenza (lunghezze d'onda corte), hanno meno energia e una penetrazione superficiale. Grazie a queste proprietà, una metodologia che utilizzi le onde superficiali può fornire informazioni sulle variazioni delle proprietà elastiche dei materiali prossimi alla superficie al variare della profondità. La velocità delle onde S (Vs) è il fattore dominante che governa le caratteristiche della dispersione.

La procedura MASW può sintetizzarsi in tre stadi distinti:

1 - acquisizione dei dati sperimentali;

2 - estrazione della curva di dispersione;

3 - inversione della curva di dispersione per ottenere il profilo verticale delle Vs (profilo 1-D), che descrive la variazione di Vs con la profondità.

Una mappa bidimensionale (mappa 2-D) può essere costruita accostando e sovrapponendo più

profili 1-D consecutivi.

Il principale vantaggio di un metodo di registrazione multicanale è la capacità di riconoscimento dei diversi comportamenti, che consente di identificare ed estrarre il segnale utile dall'insieme di varie e differenti tipologie di onde sismiche. Quando un impatto è applicato sulla superficie del terreno, tutte queste onde vengono simultaneamente generate con differenti proprietà di attenuazione, velocità e contenuti spettrali. Queste proprietà sono individualmente identificabili in una registrazione multicanale e lo stadio successivo del processo fornisce grande versatilità nell'estrazione delle informazioni utili.

5.4. PROVE DI LABORATORIO

In fase delle indagini, durante la campagna di prove penetrometriche, sono stati prelevati due campioni indisturbati di terreno con fustella a pareti sottili tipo shelby (per le profondità si rimanda alla tabella seguente) per le necessarie prove di laboratorio; oltre alla descrizione geotecnica è stata effettuata la prova di taglio diretto consolidata drenata (CD).

La prova di taglio diretto (CD) consiste nel sottoporre un campione di terreno, opportunamente preparato, a due forze poste su piani ortogonali tra di loro, una verticale ed una di taglio o orizzontale.

Il campione di terreno viene inserito all'interno di due telai quadrati sovrapposti (scatola di Casagrande) di cui uno è scorrevole rispetto all'altro. Attraverso il telaio superiore si applica uno sforzo di compressione verticale e uno sforzo orizzontale. Il campione di terreno si rompe per un valore dello sforzo orizzontale in corrispondenza del piano di separazione tra i due telai. Conoscendo le forze esterne e la sezione del campione si possono ricavare i valori delle tensioni σ e τ della retta di Coulomb. Eseguendo diverse prove si ottengono i corrispondenti valori di rottura di τ in base ai quali si può tracciare la retta di Coulomb $\tau = c + \sigma \text{ tg } \Phi$, dove Φ è l'angolo d'attrito critico del terreno. Durante la prova si controlla la velocità di applicazione del carico, misurando con un dinamometro il valore dello sforzo orizzontale al crescere della deformazione. Si può quindi tracciare il diagramma τ – deformazione per diversi valori dello sforzo verticale, e determinare quindi il massimo valore di τ. Generalmente si eseguono tre prove di taglio a carichi normali crescenti e si traccia su un grafico τ / σ la retta che media i tre punti trovati; la pendenza di questa retta rappresenta Φ e l'intercetta all'asse delle σ rappresenta c.

Di seguito, si elencano le prove effettuate (tabella 1) le cui risultanze (certificati) sono allegate in appendice:

campione	profondità campione (m)	descrizione geotecnica del campione	determinazione limiti	Colonna risonante	Analisi granulometrica combinata	Taglio diretto CD
CPT9 – C1	0,40 – 0,80	X				X
CPT9 – C2	1,00 – 1,40	X				X
CPT4 – C3	1,30 – 1,70	X				X

Tab. 1: riepilogo profondità e prove effettuate sui campioni indisturbati

6. Correlazioni adottate

6.1 INTERPRETAZIONI PER LE CPT

Di seguito vengono riportate le principali correlazioni per quanto riguarda le CPT meccaniche adottate tramite software di elaborazioni prove penetrometriche (es. Fondazioni 2011) per le valutazioni litologiche e geotecniche al fine di fornire utili indicazioni in merito al tipo di parametro utilizzato ed a come ci si è pervenuti.

6.1.1 INTERPRETAZIONI LITOLOGICHE

Valutazioni in base al rapporto: F = (Rp / RL) (Begemann 1965 - Raccomandazioni A.G.I. 1977) valide in via approssimata per terreni immersi in falda:

F = Rp / RL	NATURA LITOLOGICA	PROPRIETA'
F < 15	TORBE ED ARGILLE ORGANICHE	COESIVE
15 < F ≤ 30	LIMI ED ARGILLE	COESIVE
30 < F ≤ 60	LIMI SABBIOSI E SABBIE LIMOSE	GRANULARI
F > 60	SABBIE E SABBIE CON GHIAIA	GRANULARI

Vengono inoltre riportate le valutazioni stratigrafiche fornite da Schmertmann (1978), ricavabili in base ai valori di Rp e di FR = (RL / Rp) %:

- AO = argilla organica e terreni misti
- Att = argilla (inorganica) molto tenera
- At = argilla (inorganica) tenera
- Am = argilla (inorganica) di media consistenza
- Ac = argilla (inorganica) consistente
- Acc = argilla (inorganica) molto consistente
- ASL = argilla sabbiosa e limosa
- SAL = sabbia e limo / sabbia e limo argilloso
- Ss = sabbia sciolta
- Sm = sabbia mediamente addensata
- Sd = sabbia densa o cementata

- SC = sabbia con molti fossili, calcareniti

Secondo Schmertmann il valore della resistenza laterale da usarsi, dovrebbe essere pari a:

- 1/3 ± 1/2 di quello misurato per depositi sabbiosi
- quello misurato (inalterato) per depositi coesivi.

6.1.2 CORRELAZIONI GEOTECNICHE

PARAMETRI GEOTECNICI (validità orientativa) - simboli - correlazioni - bibliografia

- γ' = peso dell'unità di volume (efficace) del terreno [correlazioni: γ' - Rp - natura] (Terzaghi & Peck 1967 -Bowles 1982)
- $\sigma'vo$ = tensione verticale geostatica (efficace) del terreno (valutata in base ai valori di γ')
- Cu = coesione non drenata (terreni coesivi) [correlazioni: Cu - Rp]
- OCR = grado di sovra consolidazione (terreni coesivi) [correlazioni: OCR - Cu - $\sigma'vo$] (Ladd et al. 1972 / 1974 / 1977 - Lancellotta 1983)
- Eu = modulo di deformazione non drenato (terr.coes.) [correl.: Eu - Cu - OCR - Ip Ip= ind.plast.] Eu50 - Eu25 corrispondono rispettivamente ad un grado di mobilitazione dello sforzo deviatorico pari al 50-25% (Duncan & Buchigani 1976)
- E' = modulo di deformazione drenato (terreni granulari) [correlazioni: E' - Rp] E'50 - E'25 corrispondono rispettivamente ad un grado di mobilitazione dello sforzo deviatorico pari al 50-25% (coeff. di sicurezza F = 2 - 4 rispettivamente) (Schmertmann 1970 / 1978 - Jamiolkowski et al. 1983)
- Mo = modulo di deformazione edometrico (terreni coesivi e granulari) [correl.: Mo - Rp - natura] (Sanglerat 1972 - Mitchell & Gardner 1975 - Ricceri et al. 1974 - Holden 1973)
- Dr = densità relativa (terreni gran. N. C. - normalmente consolidati) [correlazioni: Dr - Rp - $\sigma'vo$] (Schmertmann 1976)
- Ø' = angolo di attrito interno efficace (terreni granulari N.C.) [correl.: – Meyerhof (1956/1976) ØMe - sabbie limose
- F.L. = accelerazione al suolo che può causare liquefazione (terreni granulari) (g = acc.gravità)(Seed & Idriss 1971 - Sirio 1976) [correlazioni : (Amax/g) - Dr]

7. Valutazioni geolitologiche

Nel sito di studio sono state riscontrate eteropie di facies tra litologie argillo limose e limo argillose, inorganiche, da mediamente a consistenti, con intercalazioni di sabbie medio-fini e argille/argille limose a tratti organiche. Inoltre, in tutta l'area di studio, è stato riscontrato un paleosuolo.

Tali terre ricoprono con continuità l'area; possiedono, nei periodi siccitosi, un grado di drenaggio interno medio.

Dall'analisi dei risultati delle prove penetrometriche, osservabili nei diagrammi e nelle tabelle allegate, si possono sintetizzare, per la porzione di sottosuolo in esame, le seguenti informazioni stratigrafiche ottenute mediante il già ricordato riconoscimento di massima dei terreni attraversati:

Punto 1 – Prova penetrometrica CPT 1

da p.c. a -0.6 m	terreno agricolo;
da -0,6 a -5,8 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -5,8 a -11,6 m	limo argilloso sabbioso, inorganico, consistente (paleosuolo);
da -11,6 a -15,0 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente.

Punto 2 – Prova penetrometrica CPT 2

da p.c. a -0,8 m	terreno agricolo;
da 0,8 a -4,4 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -4,4 a -5,2 m	limo argilloso sabbioso, inorganico, consistente (paleosuolo);
da -5,2 a -6,2 m	argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a consistente;
da -6,2 a -12,2 m	limo argilloso sabbioso, inorganico, consistente (paleosuolo);
da -12,2 a -15,0 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;

Punto 3 – Prova penetrometrica CPT 3

da p.c. a -0,2 m	terreno agricolo;
da -0,2 a -5,8 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -5,8 a -6,2 m	limo argilloso sabbioso, inorganico, consistente (paleosuolo);
da -6,2 a -8,4 m	limo argilloso, a tratti sabbioso (sabbie medio-fini) inorganico, consistente;
da -8,4 a -9,6 m	limo argilloso sabbioso, inorganico, consistente (paleosuolo);
da -9,6 a -12,0 m	limo argilloso, a tratti sabbioso (sabbie medio-fini) inorganico, consistente;
da -12,0 a -12,6 m	limo argilloso sabbioso, inorganico, consistente (paleosuolo);
da -12,6 a -15,0 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente.

Punto 4 – Prova penetrometrica CPT 4

da p.c. a -0.4 m	terreno agricolo;
da 0,4 a -6,2 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -6,2 a -8,4 m	limo argilloso sabbioso, inorganico, consistente (paleosuolo);
da -8,4 a -9,8 m	argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a consistente;
da -9,8 a -10,4 m	limo argilloso sabbioso, inorganico, consistente (paleosuolo);
da -10,4 a -11,8 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;

da -11,8 a -12,4 m limo argilloso sabbioso, inorganico, consistente (paleosuolo).

Punto 5 – Prova penetrometrica CPT 5

da p.c. a -0,8 m terreno agricolo;
da 0,8 a -1,2 m argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -1,4 a -2,0 m limo argilloso, a tratti sabbioso (sabbie medio-fini) inorganico, consistente;
da -2,0 a -3,4 m argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a consistente;
da -3,4 a -4,6 m argilla, argilla limosa, a tratti organica, poco consistente;
da -4,6 a -5,4 m argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a consistente;
da -5,4 a -5,8 m limo argilloso, a tratti sabbioso (sabbie medio-fini) inorganico, consistente;
da -5,8 a -6,6 m argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a consistente;
da -6,6 a -8,2 m limo argilloso sabbioso, inorganico, consistente (paleosuolo);
da -8,2 a -9,8 m limo argilloso, a tratti sabbioso (sabbie medio-fini) inorganico, consistente;
da -9,8 a -11,0 m limo argilloso sabbioso, inorganico, consistente (paleosuolo);
da -11,0 a -11,8 m limo argilloso, a tratti sabbioso (sabbie medio-fini) inorganico, consistente.

Punto 6 – Prova penetrometrica CPT 6

da p.c. a -0,2 m terreno agricolo;
da 0,2 a -8,2 m argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -8,2 a -10,6 m limo argilloso sabbioso, inorganico, consistente (paleosuolo);
da -10,6 a -12,0 m limo argilloso, a tratti sabbioso (sabbie medio-fini) inorganico, consistente.

Punto 7 – Prova penetrometrica CPT 7

da p.c. a -6,6 m argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a consistente;
da -6,6 a -9,2 m limo argilloso, a tratti sabbioso (sabbie medio-fini) inorganico, consistente;
da -9,2 a -9,8 m argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a consistente;
da -9,8 a -12,8 m limo argilloso, a tratti sabbioso (sabbie medio-fini) inorganico, consistente;
da -12,8 a -14,2 m argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a consistente.

Punto 8 – Prova penetrometrica CPT 8

da p.c. a -1,0 m terreno agricolo;
da 1,0 a -4,6 m argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -4,6 a -5,8 m limo argilloso sabbioso, inorganico, consistente (paleosuolo);
da -5,8 a -6,8 m argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a consistente;
da -6,8 a -8,8 m limo argilloso sabbioso, inorganico, consistente (paleosuolo);
da -8,8 a -11,2 m argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a consistente;
da -11,2 a -12,6 m limo argilloso sabbioso, inorganico, consistente (paleosuolo);
da -12,6 a -15,0 m argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a

consistente.

Punto 9 – Prova penetrometrica CPT 9

da p.c. a -0,6 m	terreno agricolo;
da 0,6 a -1,8 m	sabbie medio-fini, a tratti limose, da mediamente addensate a addendate;
da -1,8 a -2,4 m	argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a consistente;
da -2,4 a -4,0 m	sabbie medio-fini, a tratti limose, da mediamente addensate a addendate;
da -4,0 a -4,6 m	argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a consistente;
da -4,6 a -4,8 m	argilla, argilla limosa, a tratti organica, poco consistente;
da -4,8 a -5,8 m	sabbie medio-fini, a tratti limose, da mediamente addensate a addendate;
da -5,8 a -6,8 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -6,8 a -7,8 m	argilla, argilla limosa, a tratti organica, poco consistente;
da -7,8 a -9,4 m	sabbie medio-fini, a tratti limose, da mediamente addensate a addendate;
da -9,4 a -9,8 m	limo argilloso sabbioso, inorganico, consistente (paleosuolo);
da -9,8 a -15,0 m	limo argilloso, a tratti sabbioso (sabbie medio-fini) inorganico, consistente.

Punto 10 – Prova penetrometrica CPT 10

da p.c. a -0,2 m	terreno agricolo;
da 0,2 a -6,0 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -6,0 a -8,0 m	limo argilloso sabbioso, inorganico, consistente (paleosuolo);
da -8,0 a -15,0 m	limo argilloso, a tratti sabbioso (sabbie medio-fini) inorganico, consistente.

Punto 11 – Prova penetrometrica CPTu 1

da p.c. a -0,4 m	terreno agricolo;
da 0,4 a -1,8 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -1,8 a -3,3 m	argilla, argilla limosa, a tratti organica, poco consistente;
da -3,3 a -3,45 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -3,45 a -4,2 m	argilla, argilla limosa, a tratti organica, poco consistente;
da -4,2 a -10,3 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -10,3 a -11,6 m	argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a consistente;
da -11,6 a -14,2 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -14,2 a -15,4 m	argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a consistente;
da -15,4 a -17,2 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -17,2 a -17,9 m	limo argilloso sabbioso, inorganico, consistente (paleosuolo);
da -17,9 a -20,5 m	sabbie medio-fini, a tratti limose, da mediamente addensate a addendate.

Punto 12 – Prova penetrometrica CPTu 2

da p.c. a -0,6 m	terreno agricolo;
da 0,6 a -2,3 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente

	consistente;
da -2,3 a -3,3 m	argilla, argilla limosa, a tratti organica, poco consistente;
da -3,3 a -3,45 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -3,45 a -3,7 m	argilla, argilla limosa, a tratti organica, poco consistente;
da -3,7 a -4,4 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -4,4 a -4,7 m	argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a consistente;
da -4,7 a -6,0 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -6,0 a -6,6 m	argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a consistente;
da -6,6 a -7,2 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -7,2 a -8,3 m	limo argilloso sabbioso, inorganico, consistente (paleosuolo);
da -8,3 a -9,1 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -9,1 a -12,0 m	argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a consistente;
da -12,0 a -14,0 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -14,0 a -14,8 m	argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a consistente;
da -14,8 a -15,4 m	limo argilloso sabbioso, inorganico, consistente (paleosuolo);
da -15,4 a -16,9 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente.

Punto 13 – Prova penetrometrica CPTu 3

da p.c. a -0,8 m	terreno agricolo;
da 0,8 a -2,5 m	limo argilloso sabbioso, inorganico, consistente (paleosuolo);
da -2,5 a -3,2 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -3,2 a -4,6 m	argilla, argilla limosa, a tratti organica, poco consistente;
da -4,6 a -5,8 m	argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a consistente;
da -5,8 a -6,8 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -6,8 a -7,1 m	argilla, argilla limosa, a tratti organica, poco consistente;
da -7,1 a -8,5 m	argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a consistente;
da -8,5 a -8,7 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -8,7 a -9,8 m	limo argilloso sabbioso, inorganico, consistente (paleosuolo);
da -9,8 a -10,3 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -10,3 a -12,6 m	argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a consistente;
da -12,6 a -13,5 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -13,5 a -13,7 m	limo argilloso, a tratti sabbioso (sabbie medio-fini) inorganico, consistente;

da -13,7 a -14,0 m	argilla, argilla limosa, a tratti organica, poco consistente;
da -14,0 a -14,8 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -14,8 a -16,6 m	argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a consistente;
da -16,6 a -18,0 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -18,0 a -18,3 m	limo argilloso sabbioso, inorganico, consistente (paleosuolo);
da -18,3 a -18,7 m	limo argilloso, a tratti sabbioso (sabbie medio-fini) inorganico, consistente;
da -18,7 a -19,7 m	limo argilloso sabbioso, inorganico, consistente (paleosuolo).

Punto 14 – Prova penetrometrica CPTu 4

da p.c. a -0,8 m	terreno agricolo;
da 0,8 a -1,5 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -1,5 a -1,8 m	limo argilloso sabbioso, inorganico, consistente (paleosuolo);
da -1,8 a -2,1 m	argilla, argilla limosa, a tratti organica, poco consistente;
da -2,1 a -3,1 m	argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a consistente;
da -3,1 a -5,5 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -5,5 a -6,7 m	argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a consistente;
da -6,7 a -7,1 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -7,1 a -9,7 m	limo argilloso sabbioso, inorganico, consistente (paleosuolo);
da -9,7 a -10,1 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -10,1 a -10,4 m	limo argilloso sabbioso, inorganico, consistente (paleosuolo);
da -10,4 a -10,6 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -10,6 a -11,4 m	limo argilloso sabbioso, inorganico, consistente (paleosuolo);
da -11,4 a -12,4 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -12,4 a -14,1 m	argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a consistente.

Punto 15 – Prova penetrometrica CPTu 5

da p.c. a -0,4 m	terreno agricolo;
da 0,4 a -1,3 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -1,3 a -1,7 m	argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a consistente;
da -1,7 a -2,2 m	limo argilloso sabbioso, inorganico, consistente (paleosuolo);
da -2,2 a -2,6 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -2,6 a -4,1 m	argilla, argilla limosa, a tratti organica, poco consistente;
da -4,1 a -5,2 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -5,2 a -5,8 m	sabbie medio-fini, a tratti limose, da mediamente addensate a addendate;

da -5,8 a -6,0 m	limo argilloso, a tratti sabbioso (sabbie medio-fini) inorganico, consistente;
da -6,0 a -7,9 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -7,9 a -10,0 m	argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a consistente;
da -10,0 a -10,5 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -10,5 a -10,8 m	argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a consistente;
da -10,8 a -11,3 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -11,3 a -14,5 m	argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a consistente;
da -14,5 a -16,0 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -16,0 a -16,8 m	argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a consistente;
da -16,8 a -18,7 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -18,7 a -19,6 m	limo argilloso sabbioso, inorganico, consistente (paleosuolo);
da -19,6 a -20,3 m	limo argilloso, a tratti sabbioso (sabbie medio-fini) inorganico, consistente;
da -20,3 a -20,8 m	sabbie medio-fini, a tratti limose, da mediamente addensate a addendate.

Punto 16 – Prova penetrometrica CPTu 6

da p.c. a -0,2 m	terreno agricolo;
da 0,2 a -1,9 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -1,9 a -2,2 m	argilla, argilla limosa, a tratti organica, poco consistente;
da -2,2 a -4,6 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -4,6 a -5,1 m	argilla, argilla limosa, a tratti organica, poco consistente;
da -5,1 a -5,6 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -5,6 a -9,1 m	argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a consistente;
da -9,1 a -9,5 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -9,5 a -9,9 m	limo argilloso sabbioso, inorganico, consistente (paleosuolo);
da -9,9 a -10,1 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -10,1 a -10,5 m	limo argilloso sabbioso, inorganico, consistente (paleosuolo);
da -10,5 a -10,7 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -10,7 a -11,1 m	limo argilloso sabbioso, inorganico, consistente (paleosuolo);
da -11,1 a -11,4 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -11,4 a -12,0 m	argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a consistente;
da -12,0 a -13,4 m	limo argilloso sabbioso, inorganico, consistente (paleosuolo);

da -13,4 a -13,8 m	argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a consistente;
da -13,8 a -15,2 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente;
da -15,2 a -16,9 m	argilla limosa/limo argilloso a tratti sabbioso, inorganico, da mediamente a consistente;
da -16,9 a -18,2 m	argilla limosa, a tratti debolmente sabbiosa, inorganica, mediamente consistente.

Questo tipo di terreni fini spesso porta a mal distinguere la parte coesiva dalla parte granulare fine specialmente, come detto, con la punta meccanica begemann.

Si tratta nei primi metri di depositi alluvionali, costituiti da materiali coesivi prevalenti, ai primi stadi di alterazione pedogenetica, con fronte di alterazione < 1 m (50÷100 cm); al tetto sono presenti suoli calcarei con differenziazione in orizzonti A-C.

Le indicazioni riportate hanno ovviamente carattere generale ed indicativo e non possono in alcun modo sostituire gli opportuni approfondimenti necessari alle fasi esecutive.

8. Sismicità dell'area

8.1 MACROSISMICITA'

Un passo fondamentale nella valutazione del rischio sismico di un'area è l'identificazione delle faglie attive. Sebbene esistano, infatti, strutture a scorrimento lento asismico (*fault creep* o *tectonic creep*), molte delle faglie attive sono considerate sorgenti sismiche in quanto lo scorrimento istantaneo dei due lati delle stesse, che avviene allorché lo stress supera la resistenza delle rocce, genera il rilascio di onde elastiche che si propagano in tutte le direzioni. A tali faglie sismogenetiche è associato il maggior rischio.

Per la definizione di faglia attiva si fa normalmente riferimento alla possibilità che una faglia può attivarsi in un intervallo di tempo futuro che interessa la nostra società. D'altra parte le faglie che hanno la maggiore probabilità di muoversi in un futuro prossimo sono da ricercarsi tra quelle che si sono mosse nelle fasi più recenti della storia geologica. Così una delle definizioni più comunemente accettata è quella della U.S Nuclear Regulatory Commission (1982), che definisce attive le faglie che presentano un'attivazione negli ultimi 35.000 anni o almeno due negli ultimi 500.000 anni.

La Carta sismotettonica della Regione Emilia Romagna alla scala 1:250.000, oltre alla definizione della pericolosità sismica locale e all'individuazione di strutture potenzialmente sismogenetiche, offre anche un quadro delle relazioni fra attività tettonica attuale e i rischi naturali. In detto lavoro, infatti, l'analisi comparata della sismicità e delle strutture attive, evidenti per la loro espressione sia morfologica che geologica, unitamente ad una riconsiderazione dei dati disponibili sui movimenti verticali del suolo (sollevamento dei terrazzi alluvionali, subsidenza, evoluzione del reticolo idrografico) e alla ricostruzione delle isobate delle 2 principali e più recenti superfici di discontinuità del

sottosuolo (rispettivamente 450.000 anni, base del SERS, e 10.000 anni, base dell'Olocene), ha permesso di ottenere un quadro neotettonico e sismotettonico ben definito del territorio indagato.

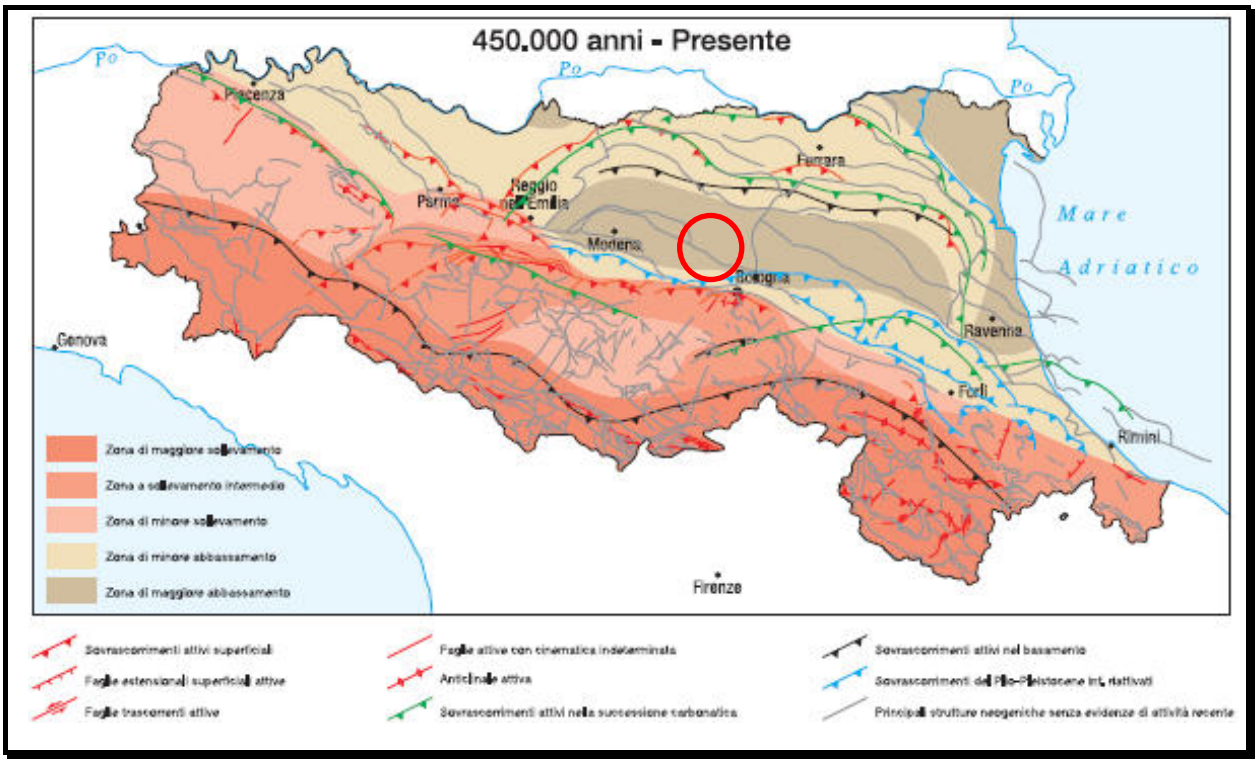


Figura 8: schema di sintesi sull'attività neotettonica in Emilia-Romagna.

Esaminando la Fig. 9.1 (fig. 8) delle Note Illustrative della Carta sismotettonica della Regione Emilia Romagna, che può essere considerata lo schema di sintesi sull'attività neotettonica in Emilia-Romagna, emerge che le zone a maggiore sollevamento, con tassi >1 mm/anno, sono individuabili nella parte alta della catena, corrispondente al settore a monte del principale raddoppio crostale a conferma dell'attività di questa struttura. L'area a sollevamento intermedio, con tassi mediamente ≥1 mm/anno, corrisponde al settore immediatamente retrostante la struttura superficiale del margine che da Bologna si estende verso NW fino alla valle del Taro. Le aree a minore sollevamento (<1 mm/anno) si collocano immediatamente a valle della struttura crostale. La zona di San Giovanni in Persiceto si trova a cavallo fra le zone a maggiore abbassamento e quelle a minor abbassamento. I meccanismi focali calcolati risultano compressivi e trascorrenti indicando direzioni di compressione sia NE-SW che NW-SE. I meccanismi focali distensivi sono nettamente secondari. Risulta quindi che la cinematica delle principali strutture attive superficiali è di tipo transpressivo.

La sismicità crostale, con ipocentri mediamente compresi tra 15 e 35 km, mostra una distribuzione simile a quella più superficiale ma con una densità inferiore. Anche in questo caso i meccanismi focali risultano compressivi e trascorrenti con direzioni di compressione sia NW-SE che

NE-SW ed i meccanismi distensivi sono rari e ben localizzati.

La sismicità più profonda, con ipocentri oltre i 35 km, fino ad oltre 50 km, è sempre diffusa nel settore di catena e in corrispondenza del margine appenninico-padano.

Risulta così un modello geodinamico attivo in cui le strutture superficiali della copertura, quelle crostali e quelle del mantello, sebbene tra loro distinte, sono tutte coerenti e inquadrabili in un sistema transpressivo che rispetto alle zone esterne dell'avampaese padano, relativamente stabili, assume il significato di un sistema di ordine inferiore all'interno di una zona di trascorrenza destra.

8.2 LA ZONAZIONE SISMOGENETICA ZS9

Nella zona di San Giovanni in Persiceto risultano all'interno dalla zona sismogenetica 912 denominata "*Dorsale Ferrarese*" non distante della zona sismogenetica 913 denominata "*Appennino Emiliano-Romagnolo*". La Fig. 9 (Zonazione sismogenetica ZS9) mostra il comportamento cinematico atteso delle strutture sismogenetiche nelle varie zone del territorio nazionale.

La zonazione sismogenetica ZS9 prodotta dal Gruppo Nazionale per la Difesa dai Terremoti rappresenta l'evoluzione di precedenti zonazioni prodotte dalla comunità scientifica nazionale con riferimento al territorio italiano e settori immediatamente confinanti. La ZS9 propone la suddivisione del territorio nazionale in fasce che presentano al loro interno requisiti di omogeneità in relazione alle caratteristiche geo-strutturali, cinematiche e sismiche. Le 42 zone-sorgente di ZS9 sono state identificate con un numero (da 901 a 936) o con una lettera (da A a F). Una base essenziale per la zonazione del territorio è rappresentata dal modello sismotettonico dell'area italiana, e contributi rilevanti per la definizione delle singole zone sono forniti dai cataloghi sismici disponibili. In particolare ZS9 è costruita facendo riferimento al modello sismotettonico di Meletti et al. (2000), rivisto ed integrato negli anni successivi alla sua formulazione. Inoltre ZS9 è definita sulla scorta delle informazioni disponibili dai cataloghi CPTI2 (catalogo parametrico dei terremoti italiani) e DISS (database delle sorgenti sismogenetiche). ZS9, come le versioni precedenti, è utilizzato per fornire i dati delle sorgenti-tipo e dei patterns sismici nei vari settori del territorio nazionale utili per le stime di pericolosità sismica.

La Zonazione ZS9 non introduce drastici elementi di novità rispetto alle precedenti zonazioni, in modo particolare rispetto a ZS4 che rappresenta una sorta di caposaldo nell'evoluzione del processo di zonazione. Infatti, il modello sismotettonico di riferimento di ZS9 è molto simile a quello utilizzato per la redazione di ZS4. Il vero elemento di novità è rappresentato dall'impiego di un catalogo sismico più aggiornato (CPTI2) e dall'introduzione delle conoscenze più recenti sulla geometria delle sorgenti sismogenetiche (database DISS).

Figura 9: Zonazione sismogenetica ZS9. Le diverse zone sono individuate da un numero; le zone individuate con una lettera non sono state utilizzate per la valutazione della pericolosità sismica.

Negli ultimi anni, infatti, la quantità di informazioni sulla sismogenesi del territorio italiano (sia per quanto riguarda gli aspetti geometrici delle sorgenti che per quanto attiene al loro comportamento atteso) è notevolmente aumentata rispetto a quella disponibile nel periodo in cui i ricercatori procedevano alla realizzazione di ZS4. Tali conoscenze rappresentano uno degli elementi chiave per il tracciamento delle nuove zone.

Un altro elemento di novità rispetto al passato è rappresentato dall'utilizzo del database delle soluzioni dei meccanismi focali dei terremoti italiani (EMMA; Vannucci e Gasperini, 2003). Tale database contiene meccanismi tratti da cataloghi on-line (come il catalogo CMT dell'Università di Harvard, il catalogo dell'ETH di Zurigo e il catalogo RCMT dell'INGV) o dalla letteratura cartacea

pubblicata. Tra tutti i meccanismi contenuti nel database sono stati selezionati quelli che ricadono all'interno delle zone sorgente di ZS9: si tratta di 1051 records relativi a terremoti avvenuti tra il 1905 ed il 2003, con magnitudo Mw compresa tra 1.9 e 6.6. Il numero di eventi per zona sorgente è estremamente variabile, poiché si va da zone per le quali si hanno solo 1 o 2 meccanismi disponibili a zone con diverse decine di meccanismi; solo in 12 zone sulle 36 utilizzate per il calcolo della pericolosità sismica si hanno meno di 10 soluzioni di meccanismi focali. Per ogni zona di ZS9 sono state determinate le somme delle componenti del momento tensore, utilizzando tutti i dati disponibili e avendo cura di scegliere il meccanismo più affidabile nel caso di soluzioni multiple per lo stesso evento. Ogni zonizzazione sismogenetica è caratterizzata da un definito modello cinematico il quale sfrutta una serie di relazioni di attenuazione stimate sulla base di misurazioni accelerometriche effettuate sia sul territorio nazionale che europeo. Sulla base di tali zone, per tutto il territorio italiano, sono state sviluppate le carte della pericolosità sismica.

Nella Zona Sismogenetica 913 sono previsti, sulla base dei meccanismi focali, valori di massima magnitudo pari a M_{wmax} = 5,91±6.14 mentre nella Zona Sismogenetica 912 sono previsti, sulla base dei meccanismi focali, valori di massima magnitudo pari a M_{wmax} = 6,14.

8.3 SISMICITA' DEL TERRITORIO

Ai sensi della legge 02.02.1974 n. 64, secondo il DM del 03.06.1981, si rileva che in base all'Elenco dei Comuni ad alto rischio sismico (Legge 22.12.1997 n. 449, art. 12) allegato all'Ordinanza P.C.M.12.06.1998 il territorio comunale di San Giovanni in Persiceto non era classificato.

Alla luce nuova normativa sismica, con l'entrata in vigore del O.P.C.M 3274 del 20 marzo 2003 ed in relazione alle emanazioni delle delibere della Giunta regionale 2329/2004 e 1677/2005, i territori comunali diventano entrambi "zona 3" e nello specifico alla zona 3. La storia sismica dei due comuni è stata desunta dal "DBMI15, un database di osservazioni macrosismiche di terremoti italiani utilizzati per la compilazione del catalogo parametrico CPTI15, database realizzato dal Gruppo Nazionale per la Difesa dei Terremoti che contiene i dati macrosismici provenienti da studi dello stesso GNDT e di altri enti.

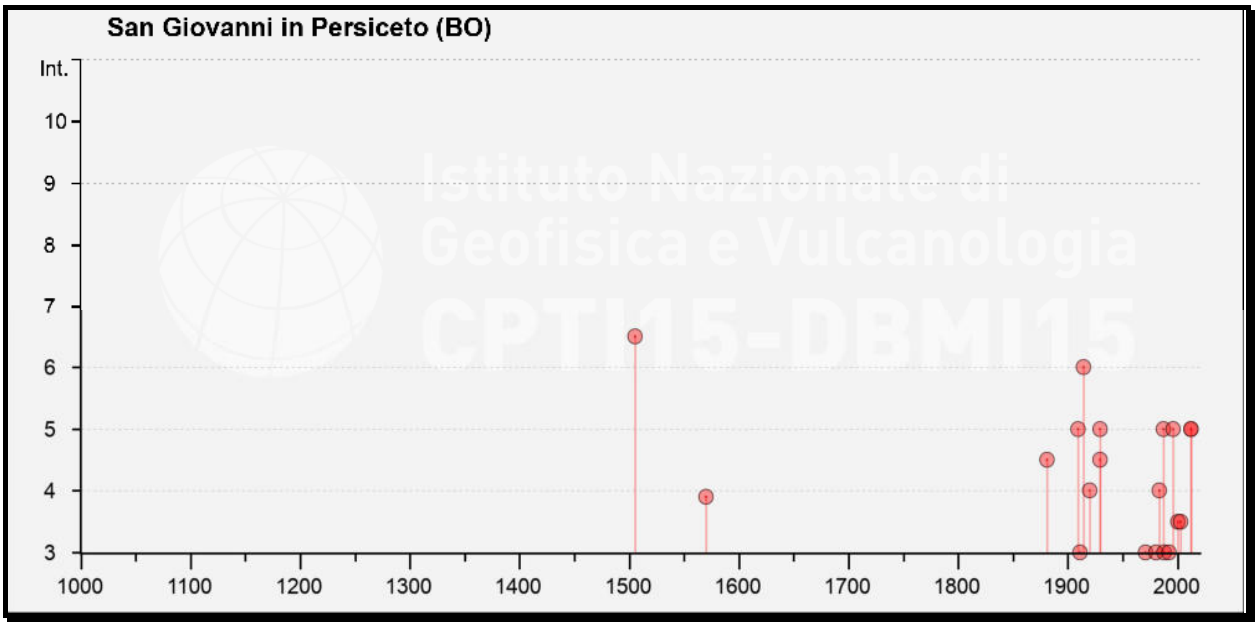


Fig.10: grafico rappresentante la storia sismica di San Giovanni in Persiceto.

In figura 10 viene riportato il diagramma del comune di San Giovanni in Persiceto, mentre in Tab. 2 sono elencati gli eventi di maggior intensità al sito.

Seismic history of	San Giovanni in Persiceto
PlaceID	IT_40181
Coordinates (lat, lon)	44.638, 11.187
Municipality (ISTAT 2015)	San Giovanni in Persiceto
Province	Bologna
Region	Emilia-Romagna
No. of reported earthquakes	27

Int. at place	Year	Mo	Da	EpicentralArea	DepDef	IoDef	MwDef
6-7	1505	1	3	Bolognese		8	5.62
F	1570	11	17	Ferrarese		7-8	5.44
4-5	1881	1	24	Bolognese		7	5.22
NF	1908	6	28	Finale Emilia		4-5	3.93
NF	1908	7	10	Carnia		7-8	5.31
5	1909	1	13	Emilia Romagna orientale		6-7	5.36
3	1911	2	19	Forlivese		7	5.26
6	1914	10	27	Lucchesia		7	5.63
4	1920	9	7	Garfagnana		10	6.53
4-5	1929	4	10	Bolognese		6	5.05
5	1929	4	20	Bolognese		7	5.36
3	1971	7	15	Parmense		8	5.51
3	1980	11	23	Irpinia-Basilicata		10	6.81
4	1983	11	9	Parmense		6-7	5.04
NF	1984	4	29	Umbria settentrionale		7	5.62
NF	1986	12	6	Ferrarese	23.5	6	4.43
5	1987	5	2	Reggiano	0.1	6	4.71
3	1988	3	15	Reggiano	0.1	6	4.57
3	1992	4	17	Appennino bolognese	0.1	4-5	4.11
5	1996	10	15	Pianura emiliana	1.3	7	5.38
NF	1998	3	26	Appennino umbro-marchigiano	44.8		5.26
3-4	2000	6	18	Pianura emiliana	25.6	5-6	4.4
NF	2002	6	8	Frignano	32.4	4	4.23
NF	2002	6	18	Frignano	32.1	4	4.3
3-4	2003	9	14	Appennino bolognese	8.3	6	5.24
5	2012	5	20	Pianura emiliana	9.5	7	6.09
5	2012	5	29	Pianura emiliana	8.1	7-8	5.9

Tab. 2: eventi sismici i cui effetti si sono sentiti nel territorio di San Giovanni in Persiceto

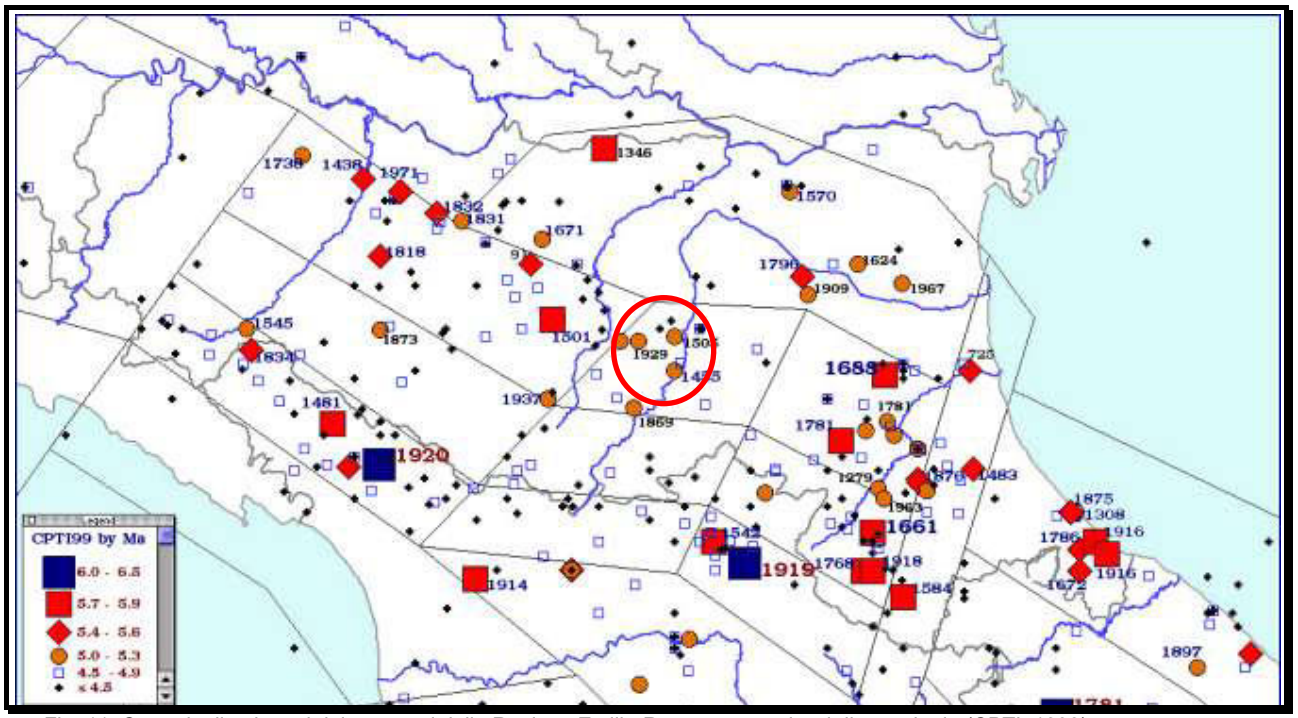


Fig. 11: Carta degli epicentri dei terremoti della Regione Emilia-Romagna per classi di magnitudo (CPTI, 1999)

Dalla lettura di Tab. 3 si evidenzia che il massimo evento sismico censito nel comune San Giovanni in Persiceto si è verificato il 10 maggio 2000. L'epicentro è indicato genericamente in Emilia Romagna. Il terremoto è stato caratterizzato da una magnitudo momento, calcolata sulle onde di superficie (Mw) pari a 4,86 ed una intensità epicentrale pari a 5-6. Non sono ancora inseriti nel database gli ultimi recenti eventi

Sopra viene riportata la mappa (figura 11) con l'indicazione degli epicentri dei terremoti storici della regione Emilia-Romagna con individuata l'area di studio, coincidente quasi con l'epicentro del terremoto del 1929 e non distante dall'epicentro dei terremoti occorso nel bolognese del 1505 e nel modenese nel 1501.

Come precedentemente indicato, l'area di studio si trova vicino al confine delle zone sismogenetica 913 con valori di massima magnitudo attesa pari a M_{wmax} = 5,91 e 912 con valori di massima magnitudo attesa pari a M_{wmax} = 6,14; aumentando il dettaglio delle informazioni disponibili dal catalogo delle sorgenti sismogenetiche italiane DISS 3.2.1 si evince che l'area di studio si colloca a ridosso della fascia sismogenetica ITCS047 "*Castelvetro di Modena-Castel San Pietro Terme*" a cui viene attribuita una magnitudo momento massima pari a M_{wmax} = 5,60 non lontana da un'altra importante fascia sismogenetica quale la ITCS051 "*Novi-Poggio Renatico*", a cui viene attribuita una magnitudo momento massima pari a M_{wmax} = 5,90. Inoltre sono state individuate non lontano dall'area di studio due faglie sismogenetiche identificate con ITIS103 "*Crespellano*" con una magnitudo momento massima attribuita pari a M_{wmax} = 5,60 e ITIS091 "*Casalecchio di Reno*" con una magnitudo

momento massima attribuita pari a M_{wmax} = 5,50. Si ricorda velocemente che una sorgente sismogenetica composita è una regione allungata, contenente un numero imprecisato di sorgenti sismogenetiche allineate che non possono essere individuate singolarmente.

Pertanto il territorio sismicamente è stato interessato da eventi significativi di cui bisognerà tenere conto in fase progettuale.

8.4 VALUTAZIONE DELLA VS_{EQ}

E' possibile calcolare il valore della V_{seq} in più modi:

1. con misure dirette di V_s (da prove Down Hole, ReMI, ecc.);
2. con misure indirette di V_s (mediante la V_p di indagini sismiche di superficie, previa conoscenza del Modulo di Poisson per gli strati investigati);
3. con indagini SPT o comunque prove penetrometriche correlabili alle SPT, mediante la correlazione di Ohta e Goto (1978) tra N_{spt} e V_s;
4. con indagini SPT o comunque prove penetrometriche correlabili alle SPT, mediante la correlazione di Motonori e Yoshida (1988) tra N_{spt} e V_s.

e nel caso in cui non si abbia a disposizione misure dirette o bibliografiche, si utilizzano le procedure indicate ai punti 3 e 4; si deve comunque considerare che deriveranno indicazioni circa la categoria di suolo di fondazione e Vs affette da un certo margine di errore dovuto in parte alla schematizzazione della stratigrafia (normalizzazione).

FORMULA DI OHTA E GOTO (1978):

$V_s = 54.33 \times (N_{spt})^{0.173} \times \alpha \times \beta \times (Z / 0.303)^{0.193}$
α = fattore di età (Olocene = 1.000: Pleistocene = 1.303);
β = fattore geologico (argille = 1.000; sabbie = 1.086);
Z = profondità in metri;
N_{spt} = numero di colpi di una prova SPT.

FORMULA DI YOSHIDA E MOTONORI (1988)

$V_s = \beta \times (N_{spt})^{0.25} \times \sigma'_{v0}{}^{0.14}$
β = fattore geologico (qualunque terreno = 55; sabbia fine = 49);
σ'_{v0} = pressione verticale (γ' h);
N_{spt} = numero di colpi di una prova SPT.

Per correlare I dati delle CPT (qc) a quelli della S.P.T. (N_{spt}) utilizzeremo:

- N_{spt} = qc/4,5 (correlazione di Robertson et al. per sabbie – qc in kg/cm^2);
- N_{spt} = qc/5 (correlazione sperimentale relativa a terreni coesivi nel bolognese)

Essendo stata effettuata un'indagine sismiche con metodologia M.A.S.W. e tomografo digitale Tromino debitamente tarata sulle indagini penetrometriche effettuate, e confrontando il dato alla Tabella 3.2.II delle NTC2018, è stato pertanto possibile ricavare direttamente il valore della V_{s30}

La V_{sEQ} ricavata dalla formula:

$$V_{sEQ} = 30/ \Sigma h_i/v_i,$$

nel caso specifico è risultata: V_{sEQ} = 192,0 m/sec;

il sito esaminato presenta un suolo di fondazione di tipo **C** ovvero:

"*Depositi di terreni a grana grossa mediamente addensati o terreni a grana fina mediamente consistenti con profondità del substrato superiori a 30 m, caratterizzati da un miglioramento delle proprietà meccaniche con la profondità e da valori di velocità equivalente compresi tra 180 m/s e 360 m/s.".*

In relazione alla frequenza tipica di vibrazione dei terreni investigata la frequenza massima significativa riscontrata presenta un picco attorno a circa 0,63 Hz in quanto è ascrivibile a discontinuità stratigrafiche importanti e che possono quindi dare origine a modificazioni del segnale sismico. Meno significative, per l'opera in progetto, appaiono le altre frequenze superiori ai 10 Hz che non possono essere considerate rappresentative di una corretta interazione struttura/terreni, in quanto sono riconducibili a discontinuità molto superficiali.

Pertanto in considerazione della tipologia strutturale da realizzarsi, si dovranno evitare accoppiamenti fra le modalità di vibrazione delle strutture e le modalità di vibrazione dei terreni di fondazione di cui sopra ovvero evitare effetti di risonanza.

8.5 PERICOLOSITÀ SISMICA DI BASE E SISMICITA' DELL'AREA DI STUDIO

Per la verifica si deve partire dalle azioni sismiche di progetto, che si definiscono a partire dalla "**Pericolosità sismica di base**" del sito di costruzione che costituisce l'elemento di conoscenza primario per la determinazione delle azioni sismiche ed è funzione delle coordinate geografiche del sito di realizzazione dell'opera e del Tempo di Ritorno.

Per pericolosità sismica di base si intende la probabilità (denominata Probabilità di eccedenza o di superamento nel periodo di riferimento P_{VR}) che, in un fissato lasso di tempo (periodo di riferimento V_R espresso in anni) nel sito si verifichi un evento sismico di entità almeno pari ad un valore prefissato

La pericolosità sismica è definita da:

a_g = accelerazione sismica massima attesa di un sito di riferimento rigido con superficie topografica orizzontale;

F_0 = valore massimo di amplificazione dello spettro in accelerazione orizzontale.

I valori dei parametri a_g ed F_0 relativi alla pericolosità sismica su reticolo geografico di riferimento sono forniti nelle tabelle riportate nell'ALLEGATO B al Testo unico 2008.

Sulla scorta del D.M 17 gennaio 2018 "*NORME TECNICHE PER LE COSTRUZIONI*" ed in base alla nuova classificazione sismica dei comuni italiani (allegato 1, punto 3 dell'OPCM 3274 del 20 marzo 2003) per i comuni appartenenti alla categoria sismica 3 la valutazione della a_g viene ora definita dal sito in base alla Latitudine ed alla longitudine che nello specifico:

WGS84
Latitudine 44.650147°
Longitudine 11.226755°

ED50
Latitudine 44,651083°
Longitudine 11,227753°

Il sito dell'INGV fornisce un a_g su suolo rigido per il comparto in questione compreso fra 0.150÷0.175 (nello specifico 0,160g), considerando un tempo di ritorno di 475 anni (VN = 50 anni, opera di classe II, cfr indicata per la pianificazione) con probabilità di eccedenza del 10% in 50 anni (50° percentile). In allegato sono riportate i valori di a_g (accelerazione massima orizzontale del terreno), F_o (valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale) e T_c (periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale) per i vari Stati Limite di Esercizio SLE (di Operatività (SLO) e di Danno (SLD)) e Stati Limite Ultimi SLU (di Salvaguardia della Vita (SLV) e di prevenzione al Collasso (SLC)) con relative probabilità di superamento nella Vita di Riferimento V_R della costruzione.

9. Modellazione sismica

9.1 Periodo di Riferimento, Vita Nominale e Classe d'uso

Il tempo di ritorno è valutato in funzione della Periodo di riferimento V_R ed in base alla corrispondente probabilità di del suo superamento allo stato limite che si intende verificare.

Il Periodo di riferimento viene calcolata in funzione della Vita nominale V_N per coefficiente d'uso C_U

$$V_R = V_N \times C_U$$

Vita nominale V_N indica in numero di anni nel quale la struttura deve essere usata per lo scopo per cui è progettata.

	Tipi di costruzione	Vita nominale V_N (in anni)
1	Opere provvisorie – Opere provvisionali - Strutture in fase costruttiva1 °	**≤10**
2	Opere ordinarie, ponti, opere infrastrutturali e dighe di dimensioni contenute o di importanza normale	**≥50**
3	Grandi opere, ponti, opere infrastrutturali e dighe di grandi dimensioni o di importanza strategica	**≥100**

Tabella 3: Tab. 2.4.I Norme Tecniche 2018

Coefficiente d'uso C_U: parametro definito in base alla classe d'uso della struttura in funzione del livello di affollamento e dell'interesse strategico.

	Classe d'uso	Coefficiente d'uso C_U
I	Costruzioni con presenza solo occasionale di persone, edifici agricoli.	**0.7**
II	Costruzioni il cui uso preveda normali affollamenti, senza contenuti pericolosi per l'ambiente e senza funzioni pubbliche e sociali essenziali. Industrie con attività non pericolose per l'ambiente. Ponti, opere infrastrutturali, reti viarie non ricadenti in Classe d'uso III o in Classe d'uso IV, reti ferroviarie la cui interruzione non provochi situazioni di emergenza. Dighe il cui collasso non provochi conseguenze rilevanti.	**1.0**
III	Costruzioni il cui uso preveda affollamenti significativi. Industrie con attività pericolose per l'ambiente. Reti viarie extraurbane non ricadenti in Classe d'uso IV. Ponti e reti ferroviarie la cui interruzione provochi situazioni di emergenza. Dighe rilevanti per le conseguenze di un loro eventuale collasso.	**1.5**
IV	Costruzioni con funzioni pubbliche o strategiche importanti, anche con riferimento alla gestione della protezione civile in caso di calamità. Industrie con attività particolarmente pericolose per l'ambiente. Reti viarie di tipo A o B, di cui al D.M. 5 novembre 2001, n. 6792, "Norme funzionali e geometriche per la costruzione delle strade", e di tipo C quando appartenenti ad itinerari di collegamento tra capoluoghi di provincia non altresì serviti da strade di tipo A o B. Ponti e reti ferroviarie di importanza critica per il mantenimento delle vie di comunicazione, particolarmente dopo un evento sismico. Dighe connesse al funzionamento di acquedotti e a impianti di produzione di energia elettrica.	**2.0**

Tabella 4: Tab. 2.4.II Norme Tecniche 2018

Nei confronti delle azioni sismiche gli stati limite ultimi (SLU) e gli stati limite di esercizio (SLE) sono definitivi riferendosi alle prestazioni della costruzione nel suo complesso includendo elementi strutturali, non strutturali ed impianti.

Stato limite di operatività (SLO)

Stato limite di danno (SLD)

Stato limite Ultimo di salvaguardia della vita (SLV)

Stato limite Ultimo di prevenzione del collasso (SLC)

La probabilità di superamento nel periodo di riferimento le PVR sono definite in funzione degli stati limite considerati.

Stati limite		P_{VR}: Probabilità di superamento nel periodo di riferimento V_R
SLE	**SLO**	**81 %**
	SLD	**63 %**
SLU	**SLV**	**10 %**
	SLC	**5 %**

Tabella 5: Tab. 3.2.I Norme Tecniche 2018

Fissata quindi la vita di riferimento e lo stato limite si ricava il tempo di ritorno:

$$T_R = - V_R / (\ln (1- P_{VR}))$$

Nel caso di studio, in quanto pianificazione, si terrà conto di un tempo di ritorno di 332 anni come da "Atto di indirizzo n. e coordinamento tecnico n. 112/2007 ai sensi dell'art. 16, c. 1, della L. R. 20/2000 per "Indirizzi per gli studi di microzonazione sismica in Emilia-Romagna per la pianificazione territoriale e urbanistica"":

V_N (1) $\geq$ 50

C_U (I) = 0,7

V_R = 50 anni

9.2 AZIONE SISMICA DI PROGETTO

Per definire l'azione sismica di progetto è necessario valutare la "Risposta Sismica Locale" e cioè quelle modifiche che un segnale sismico subisce rispetto a quello di base di un sito di riferimento rigido e con superficie topografica orizzontale.

$$a_{max} = a_g \times S_t \times S_s$$

S_s = Coefficiente di Amplificazione Stratigrafica
S_t = Coefficiente di Amplificazione Topografica

In condizioni sismiche la norma prescrive le stesse verifiche da realizzarsi in condizioni statiche con l'introduzione dei coefficienti sismici kh e kv che devono essere calcolati mediante le espressioni:

$$\mathbf{k}_h = \beta_s (a_{max} / g)$$

$$\mathbf{k}_v = \pm 0.5\, \mathbf{k}_h$$

β_S= coefficiente di riduzione dell'accelerazione massima attesa al sito

il coefficiente di riduzione si calcola in funzione della categoria del sottosuolo e della zona geografica tramite il valore di a_g (SLV).

	Categoria del sottosuolo	
	A	**B, C, D, E**
	β_s	β_s
$0.2 < a_g \leq 0.4$	0.30	0.28
$0.1 < a_g \leq 0.2$	0.27	0.24
$a_g \leq 0.1$	0.20	0.20

Tabella 6: Tab. 7.11.I - Norme Tecniche 2018

Entrambi i siti sono soggetti ad un coefficiente di amplificazione sismica locale di PGA S=1.45, dato da:

$$S = S_S \times S_T$$

In quanto la categoria topografica del sito inerente il sito di studio ricade nella T1 (S_T= 1,0 coefficiente di amplificazione topografica in quanto l'area di studio si trova in area sub-pianeggiante "*Superfici pianeggianti*, p*endii e rilievi isolati con inclinazione media ≤ 15°*", ed S_S (coefficiente di amplificazione stratigrafica in SLV per terreni in categoria suoli **C**) = 1.45.

Nel caso di studio si rileva che per sottosuoli di categoria **C** l'**SLD** sarà:

Prob. Sup. %	Tr (anni)	ag (g)	Fo	Tc (sec)	Cc	Ss	St	Kh	Kv	a_{maz} (m/s^2)	β
63	50	0,059	2,515	0,271	1,62	1,5	1,0	0,018	0,009	0,862	0,20

e per l'**SLV**:

Prob. Sup. %	Tr (anni)	ag (g)	Fo	Tc (sec)	Cc	Ss	St	Kh	Kv	a_{maz} (m/s^2)	β
10	475	0,160	2,563	0,276	1,61	1,45	1,0	0,056	0,028	2,280	0,24

9.3 ANALISI DI RISPOSTA SISMICA LOCALE RSL - ANALISI DI II LIVELLO

Dai dati della Regione Emilia Romagna, nell'atto di "*indirizzo e coordinamento tecnico ai sensi dell'art. 16, comma 1, della L.R. 20/2000 "Disciplina generale sulla tutela e l'uso del territorio", in merito a "Atto di indirizzo e coordinamento tecnico ai sensi dell'art. 16, c. 1, della LR 20/2000 per "Indirizzi per gli studi di microzonazione sismica in Emilia-Romagna per la pianificazione territoriale e urbanistica (DGR 476/2021)*", si evidenzia per le porzioni di territorio comunale riferite a San Giovanni in Persiceto vi sia un valore di accelerazione massima orizzontale di picco al suolo rigido, cioè per T = 0, espressa in frazione dell'accelerazione di gravità g (a_{refg}) = 0.161 e, in caso di substrato profondo

(significativo contrasto di impedenza a circa 100 m da p.c. e dal tetto del substrato rigido a circa 150 m da p.c. – PIANURA 2), utilizzando le relative tabelle, riportate nell'Allegato 2 degli Indirizzi regionali per la microzonazione sismica, sono così calcolati i seguenti fattori di amplificazione F.A sismica rispetto ad un suolo di riferimento:

- 1,7 = fattore di amplificazione in termini di rapporto di accelerazione massima orizzontale (PGA/PGA_0)
- 2,0 = fattore di amplificazione in termini di rapporto di Intensità di Housner (SI/SI0) per $0.1s < T_o < 0.5s$
- 3,0 = fattore di amplificazione in termini di rapporto di Intensità di Housner (SI/SI0) per $0.5s < T_o < 1.0s$
- 3,3 = fattore di amplificazione in termini di rapporto di Intensità di Housner (SI/SI0) per $0.5s < T_o < 1.5s$

Adottando i parametri forniti nell'atto di indirizzo della regione Emilia-Romagna l'accelerazione massima attesa al sito per lo stato limite SLV sarà data da:

$$a_{max} = a_{refg} \times FA = 2,684$$

con:

$a_{refg} = 0,161$

$FA = 1,70$

e i coefficienti sismici kh e kv avranno valore:

$$k_h = (\beta_s \times a_{max}) / g = 0.066$$

$$k_v = 0.033$$

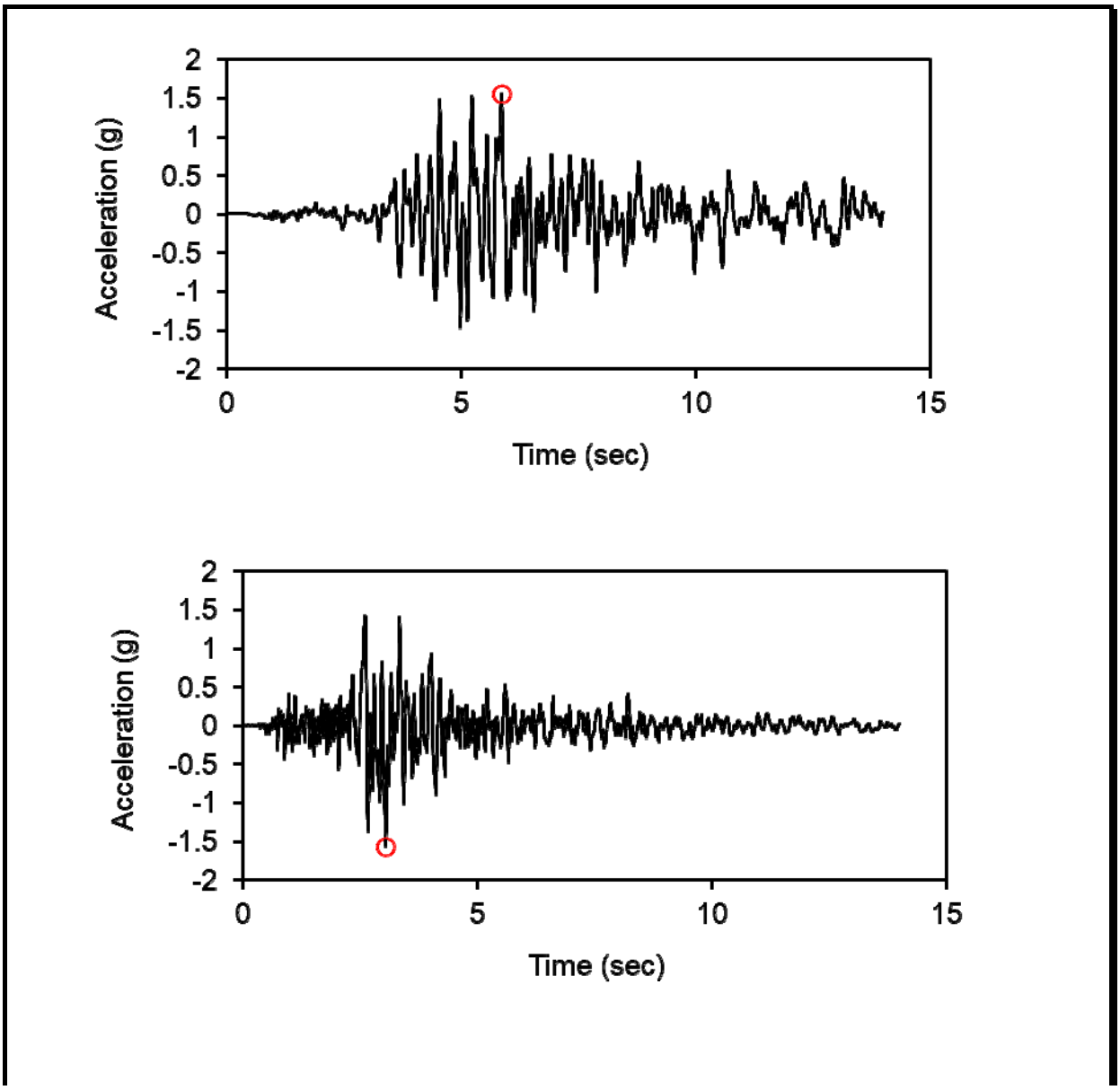
9.4 ANALISI DI RISPOSTA SISMICA LOCALE RSL - ANALISI DI III LIVELLO

Qui di seguito viene effettuato lo studio di risposta sismica locale al fine di determinare i coefficienti di amplificazione sismica rispetto al suolo di riferimento, in termini di rapporto di accelerazione massima orizzontale (PGA/PGA_0). Questo studio rientra in un'analisi di III livello a norma NTC2018 e sulla base di quanto indicato nel" *Atto di indirizzo e coordinamento tecnico ai sensi dell'art. 16, c. 1, della L. R. 20/2000 per "Indirizzi per gli studi di microzonazione sismica in Emilia-Romagna per la pianificazione territoriale e urbanistica"*".

Per l'input sismico sono stati utilizzati i dati forniti dalla Regione Emilia-Romagna per il territorio di San Giovanni in Persiceto e, nello specifico, sono stati impiegati sette segnali di riferimento (figura 15), già scalati che sono stati selezionati dalla banca dati accelerometrica "European Strong Motion database" attraverso una procedura che valuta la similarità tra una forma spettrale di riferimento e la forma degli spettri di risposta dei segnali contenuti nella banca dati ISESD e ITACA.

Magnitude (Mw)	Epic. Distance (km)	Scaling_Factor	Source File_Name
6.2	29.9	2.08%	ESM EU.HRZ..HNE.D.19790524.172317.C.ACC.ASC
5.74	12.57	1.36%	NGA RSN146_COYOTELK_G01320.AT2
5.99	54.21	2.57%	NGA RSN703_WHITTIER.A_A-VAS000.AT2
6.93	83.53	1.51%	NGA RSN804_LOMAP_SSF205.AT2
6.69	38.07	1.14%	NGA RSN1091_NORTHR_VAS090.AT2
6.6	31	0.64%	KiKnet SMNH100010061330.EW2
5.9	14.4	2.71%	ESM IT.SLO..HGE.D.20161026.191806.C.ACC.ASC

Tabella 7: Elenco accelerogrammi tratti da Rexel.



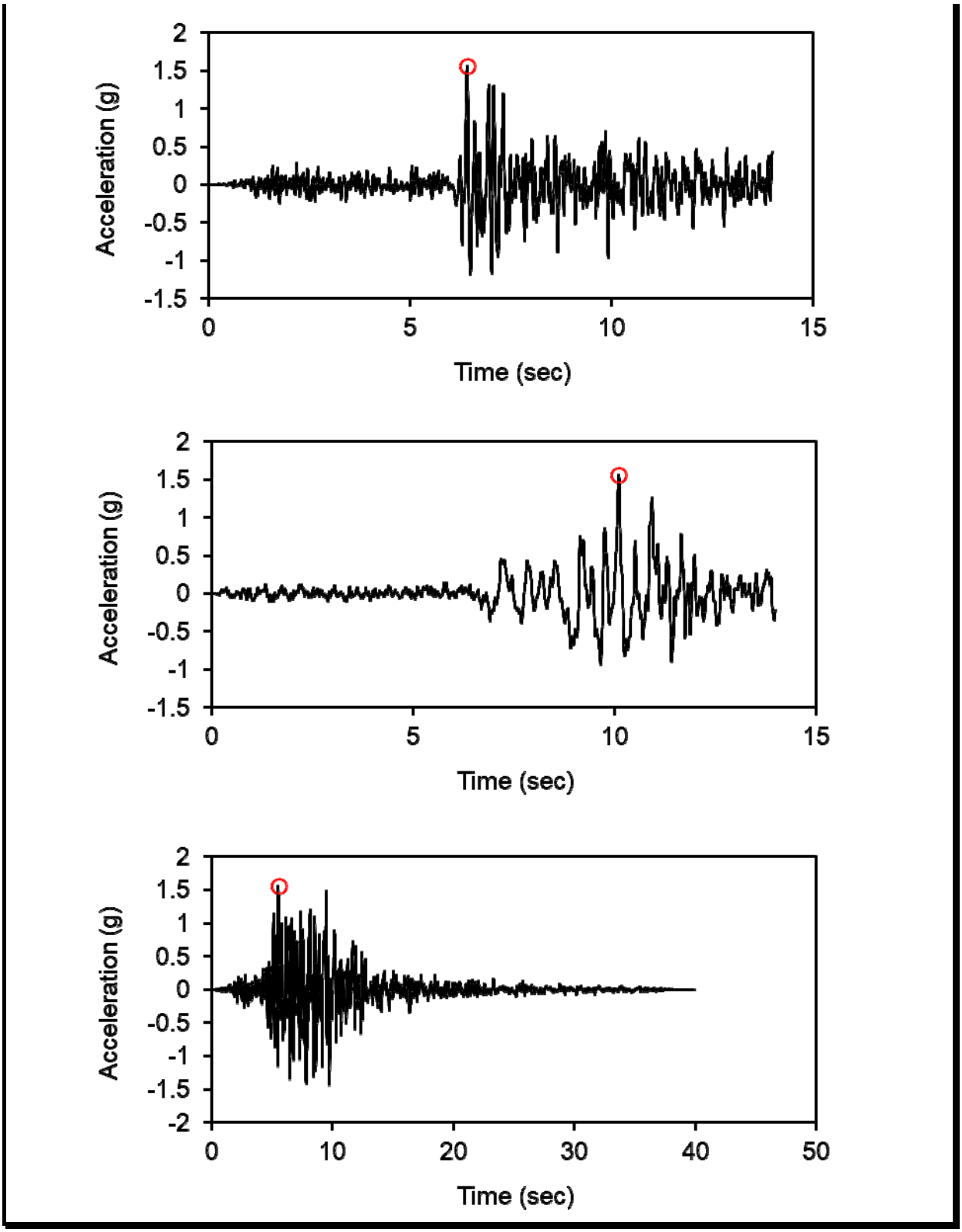


Fig. 12: accelerogrammi dei segnali di riferimento per San Giovanni in Persiceto forniti dalla Regione Emilia Romagna

Come programma numerico di analisi si è optato per il programma EERA (Equivalent-linear Earthquake site Response Analisys of Layered Soil Deposits), basato sul codice SHAKE 91 per quanto concerne le soluzioni relative alle propagazioni delle onde di taglio.

Il codice di calcolo EERA valuta la risposta sismica di un deposito di terreno, schematizzandolo come un sistema di N strati orizzontali omogenei, isotropi e visco-elastici, sovrastanti un semispazio uniforme, attraversati da un treno di onde di taglio che incidono verticalmente le superfici. Ogni strato è descritto per mezzo dello spessore H, del modulo di taglio massimo G_{max} o dalla corrispondente velocità massima V_{max}, dal valore dello smorzamento D, dal peso dell'unità di volume γ (o dalla densità di massa $\rho = \gamma / g$) e dalle curve di decadimento del modulo di rigidezza a taglio normalizzato (G / G_0 - γ) e le corrispondenti curve dello smorzamento (D - γ) con la deformazione di taglio γ.

L'analisi di tipo lineare equivalente che consiste nell'esecuzione di una sequenza di analisi lineari complete con aggiornamento successivo dei parametri di rigidezza e smorzamento fino al soddisfacimento di un prefissato criterio di convergenza. Il calcolo è stato eseguito inserendo come segnale di input, i sette segnali precedentemente identificati (fig. 12), provvedendo al taglio delle frequenze superiori ai 25 Hz, scalati sulla base di un valore di accelerazione massima orizzontale di picco (PGA) su un suolo di riferimento di tipo A, per T=0, espressa in frazione dell'accelerazione di gravità (a_{refg} - 10% di probabilità di superamento in 50 anni) pari a **0.160g**.

Per le curve di variazione del modulo di rigidezza a taglio G e del fattore di smorzamento D (damping ratio) in funzione della deformazione per le diverse tipologie di materiali, sono state impiegate quelle già presenti nel codice di calcolo in quanto ritenute sufficientemente assimilabili alla modellazione dell'area di studio.

Per la verifica della risposta sismica locale, in base alle indagini svolte sia di tipo geotecnico che di tipo geofisico, è stato modellato il sottosuolo fino al bedrock dedotto dalle sezioni geologiche disponibili, dalle indagini geofisiche effettuate e dalle indicazioni di letteratura in merito. Di seguito viene schematizzato il modello utilizzato per l'analisi:

Inserito il modello nel programma di calcolo, l'elaborazione, svolta sui n. 7 terremoti di riferimento, ha fornito i seguenti risultati, in termini di spettro di risposta elastico in accelerazione massima orizzontale in superficie per un valore di smorzamento critico pari al 5% (figura 13 e 14):

livello	profondità banco	spessore banco	litologia prevalente	Vs (m/s)
1	24,0	24,0	Argille limose	175
2	102,0	78,0	Argille limose	320
3	150,0	48,0	Limi Argillosi	520
4	inf	inf	Ghiaie	800

Tabella 8: modello geologico di riferimento

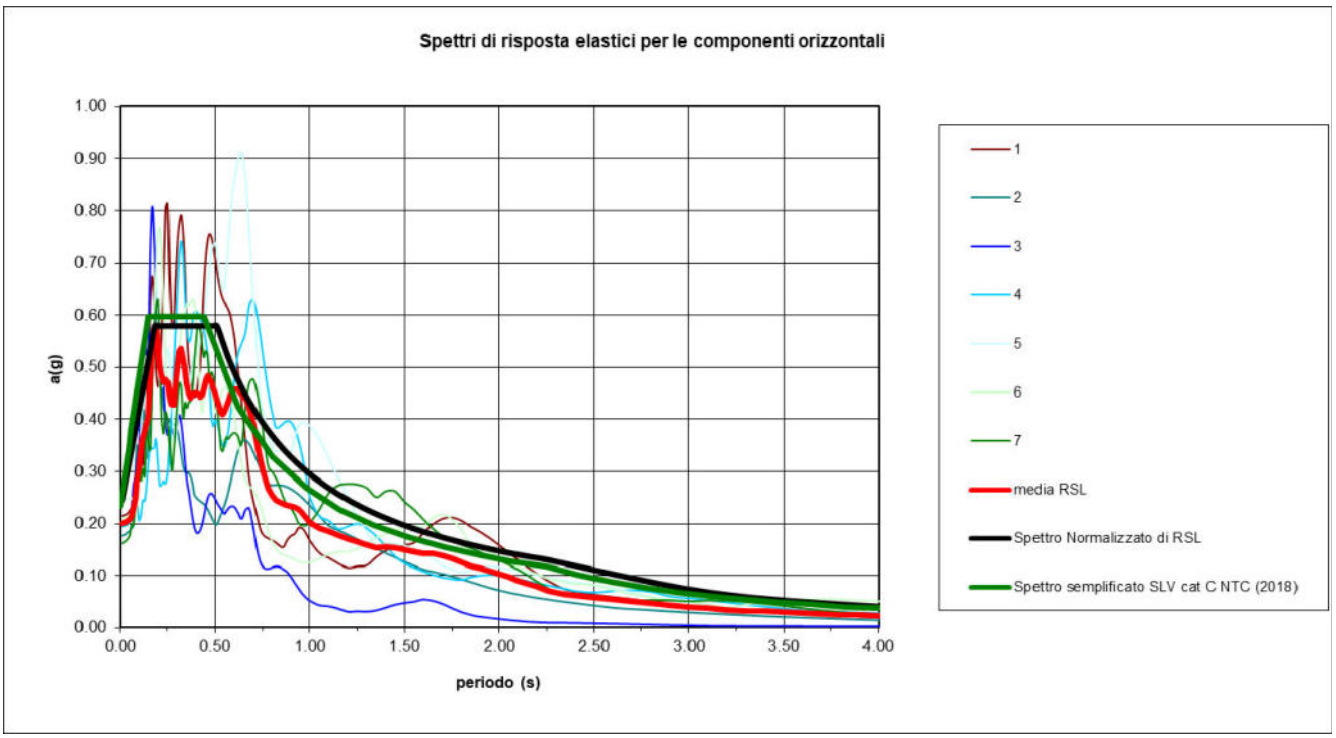


Fig. 13: risultato dell'analisi di risposta sismica locale per gli spettri di risposta con periodo di ritorno di 475 anni e smorzamento pari al 5%

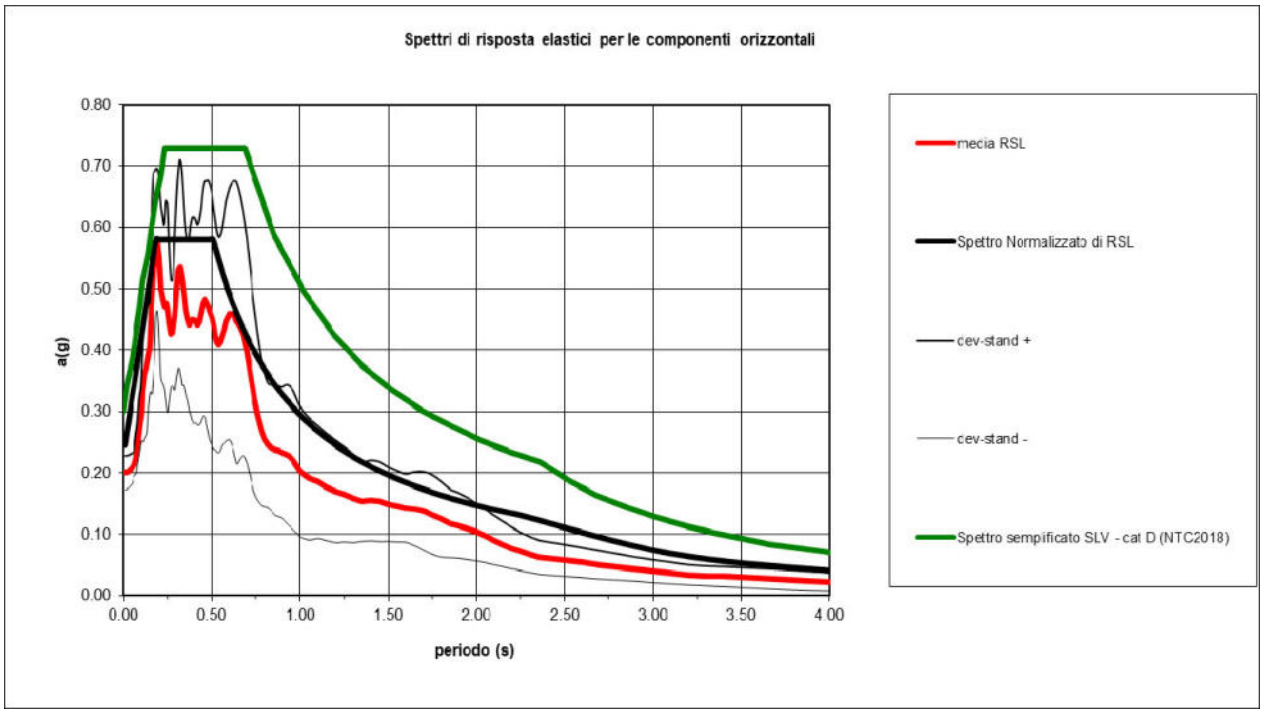


Fig. 14: risultato dell'analisi di risposta sismica locale per gli spettri di risposta con periodo di ritorno di 475 anni e smorzamento pari al 5% con spettro medio su 10 accelerogrammi e relativa deviazione standard

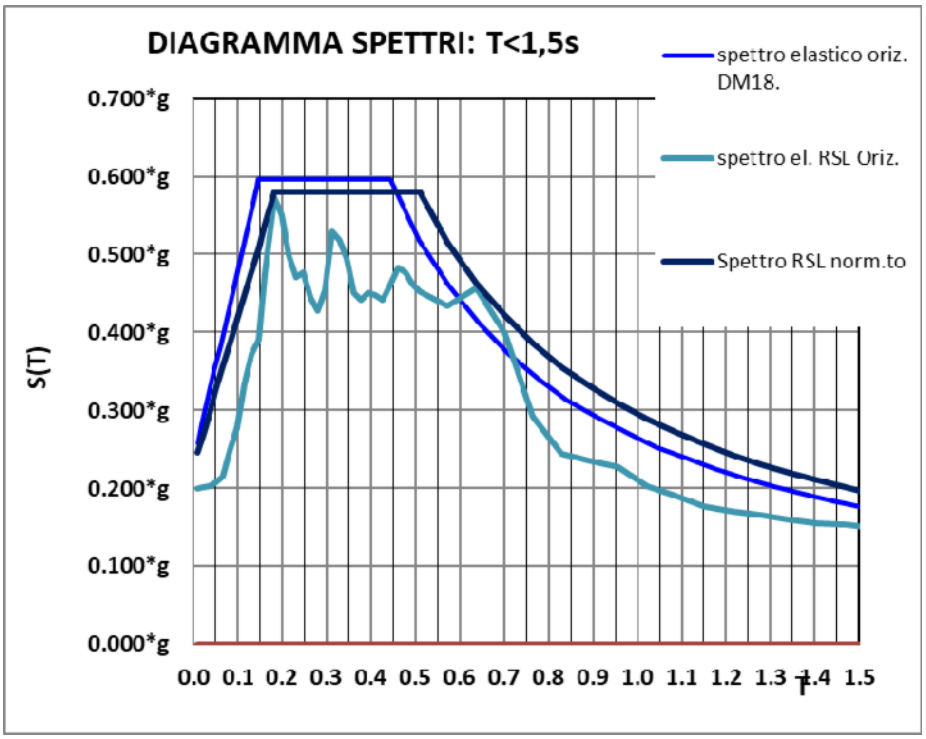


Fig. 15: raffronto fra lo spettro medio della RSL lo spettro normalizzato di RSL e lo spettro elastico da NTC2018 per suoli di categoria C (SLV) per un periodo 0.0 < T < 1,5 s.

Come si può notare (fig.15) l'analisi di risposta sismica locale (RSL) restituisce uno spettro **medio** più severo rispetto allo spettro di normativa per un suolo di categoria **C**.

L'analisi di risposta sismica locale RSL fornisce una PGA sulla superficie pari a 0.226g, come quella calcolata in base ai dati (accelerogrammi) regionali e leggermente inferiore a quanto previsto da normativa, ovvero 0.232g (NTC 2018).

In base all'analisi della Risposta Sismica Locale (figura 16 e 17) risulta che i fattori di amplificazione F.A sismici rispetto ad un suolo di riferimento risultano:

- 1,415 = fattore di amplificazione in termini di rapporto di accelerazione massima orizzontale (PGA/PGA_0) rispetto allo spettro di RSL Normalizzato e lo Spettro Semplificato NTC 2018 su suolo rigido (TR 475 anni);
- 1,407 = fattore di amplificazione in termini di rapporto di Intensità di Housner (SI/SI_0) per $0.1s < T_o < 0.5s$
- 1,949 = fattore di amplificazione in termini di rapporto di Intensità di Housner (SI/SI_0) per $0.5s < T_o < 1.0s$

Appare evidente che in questo caso i valori di normativa appaiono meno severi e conservativi rispetto a quelli di RSL; si rimanda pertanto al progettista la scelta del modello da seguire.

Di notevole interesse appare inoltre il fattore di amplificazione massima in funzione della frequenza (figura 16) ovvero è risultato un fattore di amplificazione massima (F.A.) pari a 2,28 alla frequenza di 0,6 Hz, abbastanza in accordo con quanto evidenziato dalla registrazione strumentale con tomografo digitale Tromino che indicava frequenze di sito possibili di amplificazione a circa 0,63 Hz. Pertanto si consiglia di evitare accoppiamenti in frequenza riguardante i fabbricati in progetto riferiti alle frequenze sopra indicate per evitare fenomeni di risonanza che risulterebbero sensibilmente più distruttivi di quanto ci si potrebbe attendere. In questo senso, una generale relazione empirica che lega la frequenza di vibrazione di un edificio e la sua altezza è la seguente: f = (10÷12)/n.piani.

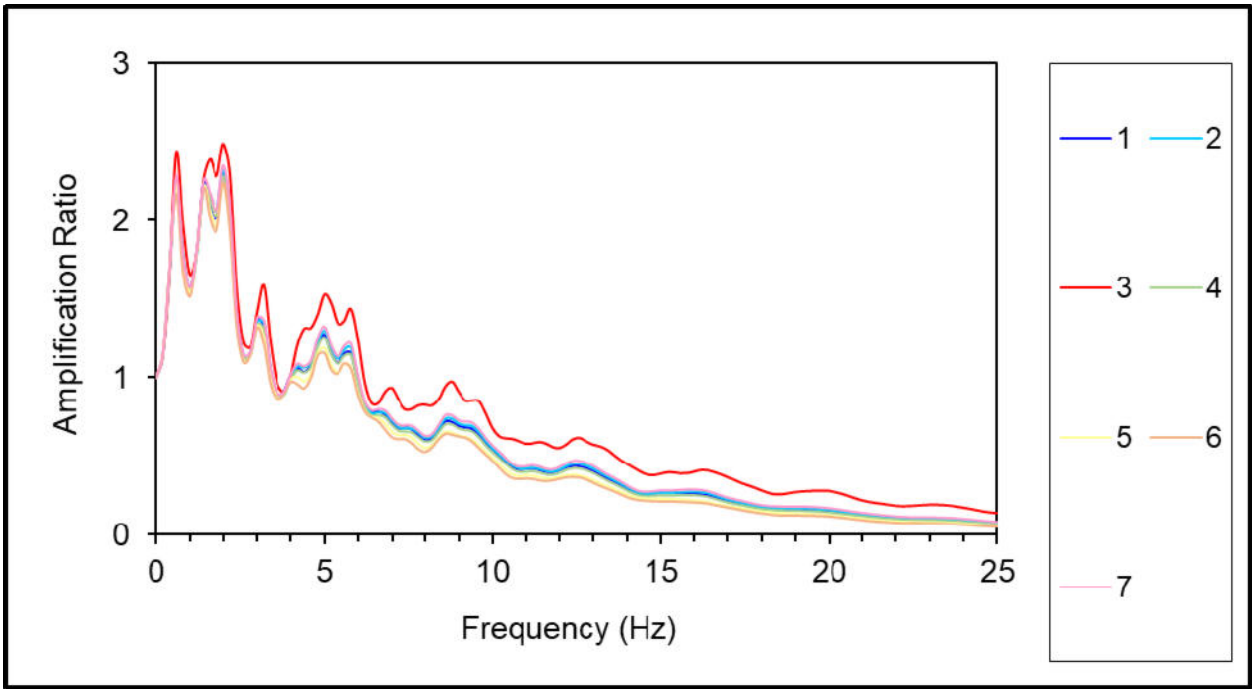


Fig. 16: fattore di amplificazione F.A. in funzione della frequenza

In ultimo vengono di seguito forniti i parametri indipendenti (per un periodo di ritorno di 475 anni), sia da NTC 2018 che da riferimento regionale e i parametri dipendenti riferiti allo spettro normalizzato di RSL, utili ai fini dei calcoli ingegneristici.

PARAMETRI INDIPENDENTI:

a_{refg} = 0,160 g (fornito dalla regione Emilia Romagna e dall'NTC 2018)

F_0 = 2,563

T^*_c = 0,276 s

PARAMETRI DIPENDENTI:

S = 1,415 (da RSL)

S = 1,45 (da NTC 2018)

Tb = 0,18	Se(T) = 0,580 g
Tc = 0,51	Se(T) = 0,580 g
Td = 2,24	Se(T) = 0,132 g

9.5 VALUTAZIONE DELLA POSSIBILITÀ DI OCCORRENZA DI FENOMENI DI LIQUEFAZIONE

Con riferimento all'Atto di indirizzo e coordinamento tecnico ai sensi dell'art. 16, c. 1, della L. R. 20/2000 per "Indirizzi per gli studi di micro zonizzazione sismica in Emilia-Romagna per la pianificazione territoriale e urbanistica" del 2 maggio 2007 (progr. 112) dell'Assemblea legislativa della

Regione Emilia-Romagna ed in particolare in relazione all'allegato 3 della stessa, è stata condotta una valutazione sulla possibilità di fenomeni di liquefazione dei terreni presenti nell'area di studio.

Il fenomeno della liquefazione (termine coniato da Mogani e Kubo nel 1953) interessa quei depositi sabbiosi saturi che, nel corso di un terremoto o più genericamente durante e immediatamente dopo una sollecitazione di tipo ciclico, subiscono una drastica riduzione della resistenza al taglio, a seguito della quale le condizioni di stabilità non sono più garantite e la massa di terreno interessata dal fenomeno comincia ad assestarsi (nel caso di un deposito orizzontale) fino a che la nuova configurazione del terreno non è compatibile con la nuova diminuita resistenza al taglio. In condizioni di sisma, vi possono anche essere effetti di "riordino" dei sedimenti, con possibilità di cedimenti significativi e che possono coinvolgere sia i depositi granulari poco addensati e recenti (olocenici), sia i sedimenti fini poco coesivi.

Risulta di fondamentale importanza la corretta conoscenza geologica di tutte quelle strutture suscettibili alla liquefazione di cui tutt'ora sono presenti notevoli lacune; studi relativamente aggiornati (Youd e Perkins - 1978; Mori et al. - 1978; CNR - 1983) hanno evidenziato come i sedimenti alluvionali e deltizi sono maggiormente suscettibili alla liquefazione se sono di deposizione recente o recentissima (depositi olocenici o addirittura minori di 500 anni). Dalle informazioni ottenute dal PTM – Piano Territoriale Metropolitano del Comune di Bologna, Tavola 4 *Carta di area vasta delle aree suscettibili di effetti locali* (Fig. 17) possiamo notare come il sito di studio siano interessati da terreni "C – sedimenti prevalente fini di pianura; tuttavia, le due aree vengono collegate da un cavidotto (linea blu) che attraversa aree "L – zone di attenzione per instabilità da liquefazione o densificazione".

Tuttavia, nella tavola QC.6/T2 del PSC Terre d'acqua – Vincoli (Fig. 18), possiamo notare come l'area in cui verrà realizzato il campo agrivoltaico in località Biancolina risulti "area caratterizzata da liquefazione dei terreni molto probabile in caso di sisma (FS<1). Anche se il sito risulta al di fuori della zona di indagine del PSC, è altamente plausibile che la zona di instabilità sia presente anche nell'area di interesse.

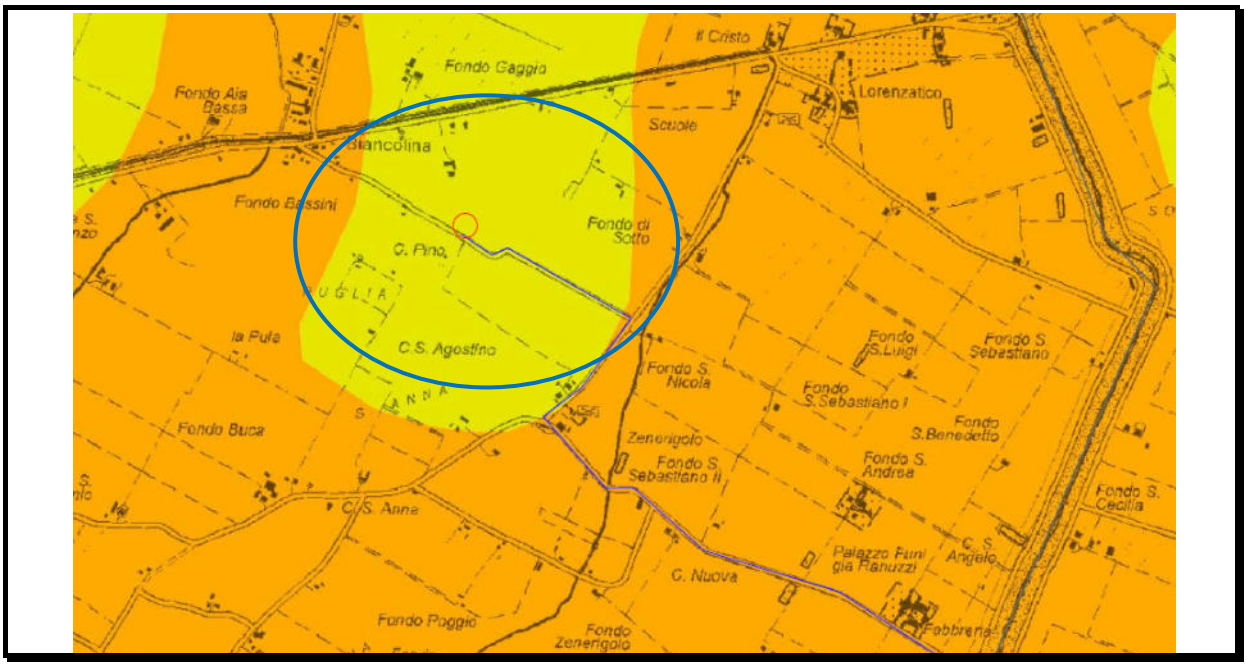


Figura 17: Estratto dalla Tav. 4 – "Carta delle aree suscettibili di effetti locali" del PTM di Bologna.

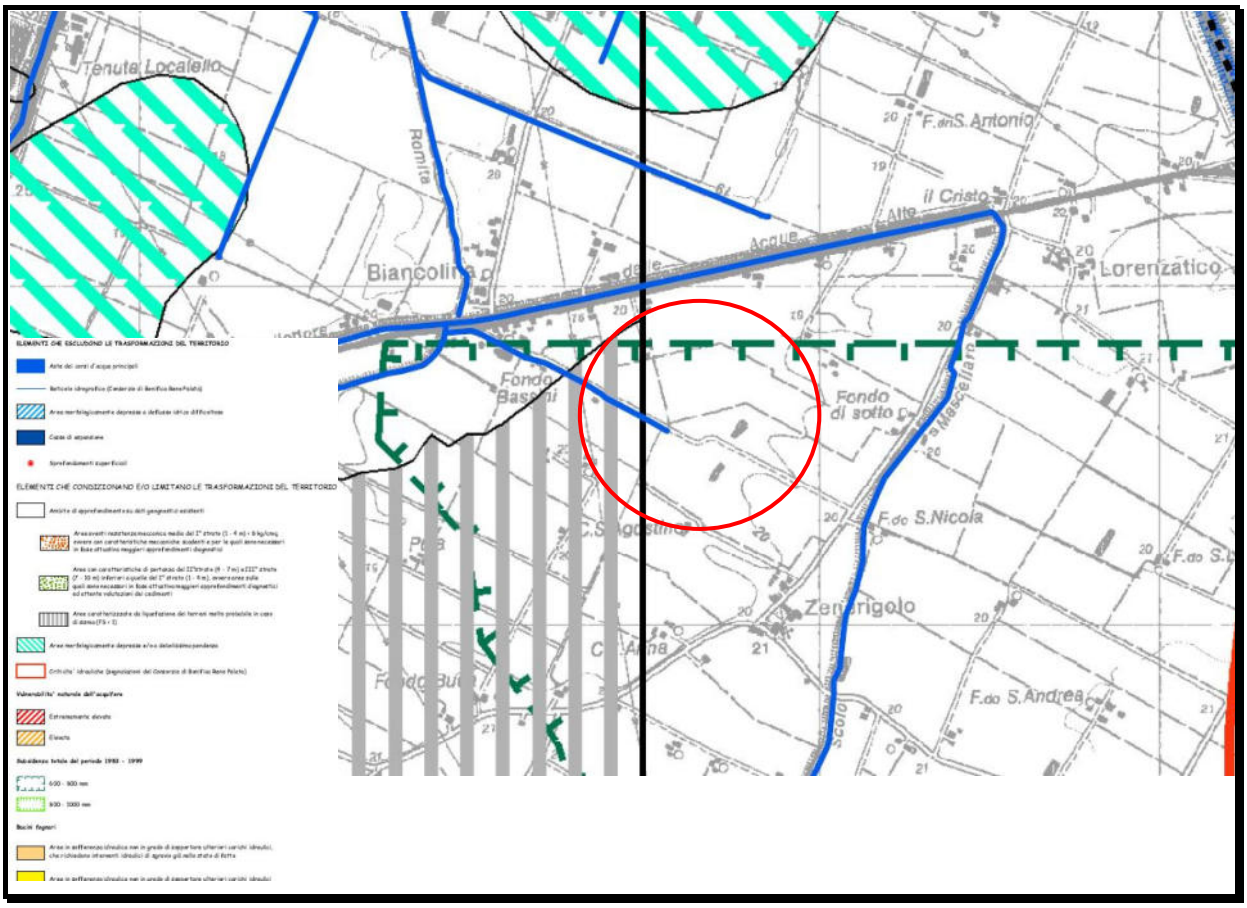


Figura 18: Estratto dalla Tav. QC.6/T2 del PSC Unione Terre d'acqua inerente il Suolo-Sottosuolo-Acque.

In base alle elaborazioni delle indagini svolte nei siti, la litologia di superficie prevalente risulta essere limo argilloso e argillo limosa con lenti decimetriche (raramente metriche) di materiali granulari (prevalentemente sabbia); pertanto, da queste informazioni le indicazioni preliminari sulla pericolosità del potenziale di liquefazione in relazione alle litologie riscontrate risulterebbe da moderata ad alta.

Tuttavia, nel recente terremoto del maggio 2012, nell'area di studio non si sono verificati fenomeni di liquefazione.

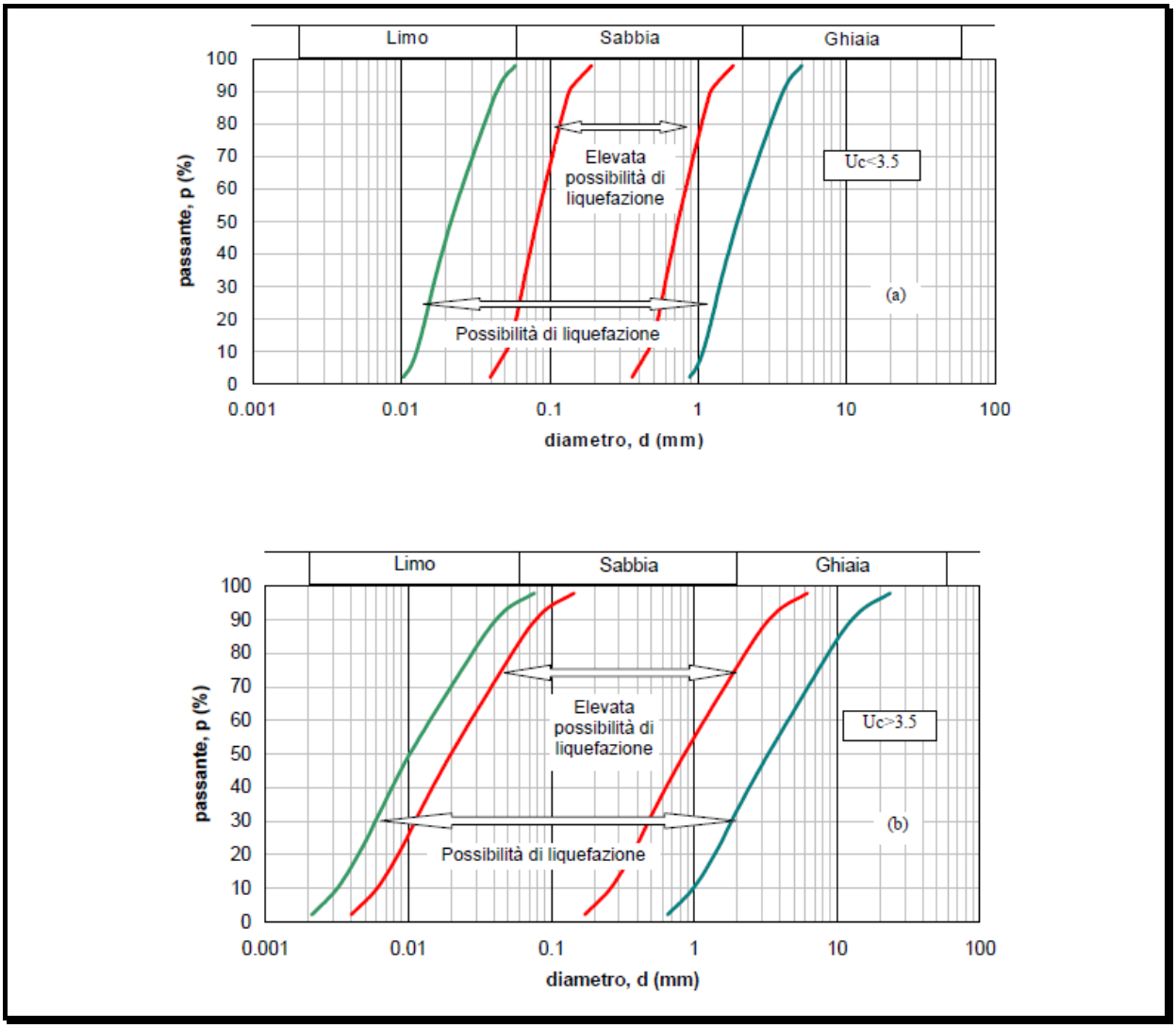


Fig. 19: Fasce granulometriche per la valutazione preliminare della suscettibilità alla liquefazione di un terreno per i terreni a granulometria uniforme (a) ed estesa (b) (da AGI 2005)

La probabilità che nei terreni sabbiosi saturi si verifichino fenomeni di liquefazione è bassa o nulla se si verifica almeno una delle seguenti condizioni:

1. Accelerazione massima attesa in superficie in condizioni *free-field* minore di 0,1g;

2. Accelerazione massima attesa in superficie in condizioni *free-field* minore di 0,15g e terreni con caratteristiche ricadenti in una delle tre seguenti categorie:

- − frazione di fine, FC, superiore al 20%, con indice di plasticità PI > 10;
- − FC ≥ 35% e resistenza $(N_1)_{60}$ > 20;
- − FC ≤ 5% e resistenza $(N_1)_{60}$ > 25

dove $(N_1)_{60}$ è il valore normalizzato della resistenza penetrometrica della prova SPT, definito dalla relazione: $(N_1)_{60} = N_{SPT}C_N$ in cui il coefficiente C_N è ricavabile dall'espressione

$$C_N = \left(\frac{p_a}{\sigma'_v}\right)^{0.5}$$

essendo p_a la pressione atmosferica e σ'v la pressione efficace verticale.

3. Distribuzione granulometrica esterna alle zone indicate nella Figura 19(a) nel caso di materiale con coefficiente di uniformità Uc < 3.5 ed in Figura 19(b) per coefficienti di uniformità Uc > 3.5.

4. Profondità media stagionale della falda superiore ai 15 m dal piano campagna.

Molti Autori hanno evidenziato una correlazione positiva tra età e tipo di deposito alluvionale continentale, riguardo la propensione alla liquefazione:

1) Youd e Perkins, 1978 – hanno composto una tabella che sintetizza i dati raccolti durante terremoti "strong motion" dell'area di S. Diego (California), da cui risulta che i sedimenti deposti da corsi d'acqua (piana alluvionale di esondazione, canale fluviale, delta fluviali, estuari) dimostrano una probabilità di liquefazione da alta a molto alta se di età minore di 500 anni o Olocenica, gli stessi depositi se di età pleistocenica o pre-pleistocenica hanno invece una "bassa" probabilità di liquefarsi. Cioè l'osservazione dimostra che sono solamente i sedimenti di deposizione recente (olocene) e recentissima (meno di 500 anni) a presentare un'alta pericolosità per la liquefazione.

2) Mori et Al, 1978 – dimostrano che la suscettibilità alla liquefazione decresce nei sedimenti di età maggiore di 500 anni, con scarti anche molto alti (maggiori del 50%). Tolno, 1975 dimostra l'incremento di densità secca (stato di addensamento) del sedimento in relazione all'aumento di vetustà (dall'Olocene al terziario)

3) Iwasaki et Al, 1982 – dimostra per terremoti giapponesi la correlazione diretta tra probabilità di liquefazione e letti di fiumi recenti e antichi;

4) CNR, 1983 – ripropone la correlazione diretta tra sedimenti fluviali e deltizi continentali ed età del deposito (i più recenti sono più suscettibili alla liquefazione).

In conclusione la letteratura geologica, ormai ben consolidata e verificata, indica che le maggiori probabilità di liquefazione si hanno nei sedimenti granulari saturi recenti e recentissimi. Ciò significa che gli alvei abbandonati e sepolti dei corsi d'acqua possono costituire fonte di pericolo di liquefazione

anche per sismi di magnitudo modesta come quelli previsti per il territorio bolognese (M=5,5÷5.6).

Per ogni verticale di indagine effettuata la stima del potenziale di liquefazione potrà essere effettuata con i metodi semplificati e a tal fine in ogni verticale dovrà essere valutato il picco di accelerazione a_{max} alla superficie del deposito; facendo riferimento a quanto esposto nel capitolo 9.4 in merito alla categoria di suolo, le verifiche verranno effettuate nei confronti della situazione più cautelativa, ovvero quella di normativa in quanto la verifica di RSL ha dato valori di F.A. sensibilmente inferiori rispetto alla norma.

Le verifiche della suscettibilità alla liquefazione e dei cedimenti potenziali indotti da sisma vengono valutati utilizzando correlazioni empiriche basate sui risultati della prova CPTu (es. P.K Robertson 1990; 1998; 2009-2010).

I dati ricavati dalle prove penetrometriche sono stati elaborati secondo le procedure semplificate di verifica della liquefacibilità e stima dei cedimenti sismici attualmente più accreditate, basate sulle esperienze di Seed e Idriss (1971), Imai & Tonouchi (1982), Robertson e Campanella (1985) e di Robertson & Wride (1998), recentemente aggiornate dallo stesso P.K. Robertson (2009-2010). Le analisi svolte seguono, inoltre, le note procedure di riferimento dettate dall'NCEER. Questo approccio valuta la propensione alla liquefazione e stima i cedimenti post sisma sia nei sedimenti granulari saturi e insaturi, sia nei sedimenti fini, poco coesivi. Per la verifica alla propensione alla liquefazione dei sedimenti e dei cedimenti post sisma dell'area di sedime si è ricorsi al software "Cliq", sviluppato dalla GeoLogiki Geotechnical Engineers in collaborazione con lo stesso P.K. Roberson.

Si è inoltre tenuto conto di una quota piezometrica da sisma saliente fino a un massimo pari a quota campagna (così come si è verificato nel recente terremoto Emiliano del 20 e 29 maggio 2012).

Per il metodo semplificato sono riportati sia in testo che negli elaborati allegati le metodologie semplificate che utilizzano le prove CPTu di seguito indicate:

- metodo di Robertson e Wride (1998) e Robertson (2009);

I metodi semplificati prevedono la verifica di un coefficiente di sicurezza dato da:

$$F_L = \frac{CRR}{CSR} \cdot MSF$$

dove, da Seed & Idriss (1971):

- $CRR = \frac{\tau_{ult}}{\sigma'_{v0}}$ è la resistenza normalizzata (rispetto alla pressione efficace verticale iniziale (σ'_{v0})) valutabile tramite abachi o prove quali SPT e CPT e da misure della velocità delle onde di taglio Vs;

- $CSR = \frac{\tau_{media}}{\sigma'_{v0}} = 0.65 \frac{a_{max\,s}}{g} \frac{\sigma_v}{\sigma'_v} r_d$ è la tensione indotta dal terremoto;

- a_{max} è l'accelerazione di gravità

- σ_v e σ'_v sono rispettivamente la tensione verticale e la tensione efficace verticale alla profondità considerata;
- r_d è un coefficiente riduttivo dell'azione sismica che porta in conto la deformabilità del sottosuolo e che può essere determinato con la relazione semplificata $r_d = 1 – 0.015z$;
- *MSF* è un fattore di scala che può essere valutato in funzione della magnitudo dei terremoti attesi.

In anni recenti l'aumento della base statistica di dati CPT ha reso possibile lo sviluppo di tecniche di analisi del potenziale di liquefazione direttamente basate sui risultati di prove CPT e molto affidabili come il metodo semplificato di Robertson e Wride (1998). A riprova della bontà di tale metodo si rimanda al lavoro del dicembre 2004 che vedeva come responsabile la Prof.ssa ing. Teresa Crespellani "R*elazione generale, descrittiva dei criteri seguiti nella programmazione e nell'esecuzione delle prove geotecniche dinamiche effettuate in laboratorio e in sito, e contenente i risultati dell'attività di ricerca svolta per la caratterizzazione dei terreni in campo statico e dinamico*" in cui si è potuto verificare che esiste una buona corrispondenza tra i valori del rischio di liquefazione ottenuti nel lavoro effettuato con la procedura semplificata di Robertson e Wride e quelli ottenuti con la metodologia basata su prove triassiali cicliche condotte su provini ricostruiti in laboratorio in condizioni simulanti da vicino quelle in sito durante il terremoto di progetto.

Si chiarisce comunque che il metodo elaborato da Robertson e Wride (1998), aggiornato dallo stesso Robertson (2009), si basa sull'elaborazioni di dati provenienti da CPTE e/o CPTU e un po' meno per le Cpt meccaniche.

La curva base per sabbia pulita della figura 24 può essere approssimata dalla seguente equazione (Robertson e Wride, 1998)

se $(q_{c1N})_{cs} < 50$

$$CRR_{7.5} = 0.833\left[\frac{(q_{c1N})_{cs}}{1000}\right] + 0.05$$

se $50 \leq (q_{c1N})_{cs} < 160$

$$CRR_{7.5} = 93\left[\frac{(q_{c1N})_{cs}}{1000}\right]^3 + 0.08$$

dove $(q_{c1N})_{cs}$ rappresenta la resistenza alla punta penetrometrica normalizzata a 1 atm (100 kPa). La procedura CPT richiede la normalizzazione della resistenza alla punta utilizzando le seguenti relazioni:

$$q_{c1N} = C_Q\left(\frac{q_c}{p_a}\right) \qquad C_Q = \left(\frac{p_a}{\sigma'_{v0}}\right)^n \quad (16b)$$

C_Q è il fattore di normalizzazione

p_a è la pressione atmosferica (1 atm) o comunque nella stessa unità di misura di σ'_{v0}

n è un esponente che varia col tipo di terreno

q_c è la resistenza alla punta del penetrometro statico.

A profondità basse C_Q diventa elevato per la bassa pressione verticale geostatica.

Comunque non vanno applicati valori di C_Q maggiori di 1.7. Il valore di n varia da 0.5 a 1.0 in funzione delle caratteristiche granulometriche del terreno (Olsen 1997).

Il rapporto di attrito (la resistenza laterale f_s divisa per la resistenza q_c) generalmente cresce al crescere del contenuto in fini e della plasticità del terreno, consentendo una stima approssimata del tipo di terreno e del contenuto in fini dai dati CPT.

Robertson e Wride (1998) hanno costruito l'abaco riprodotto in Figura 23 per la stima del tipo di terreno.

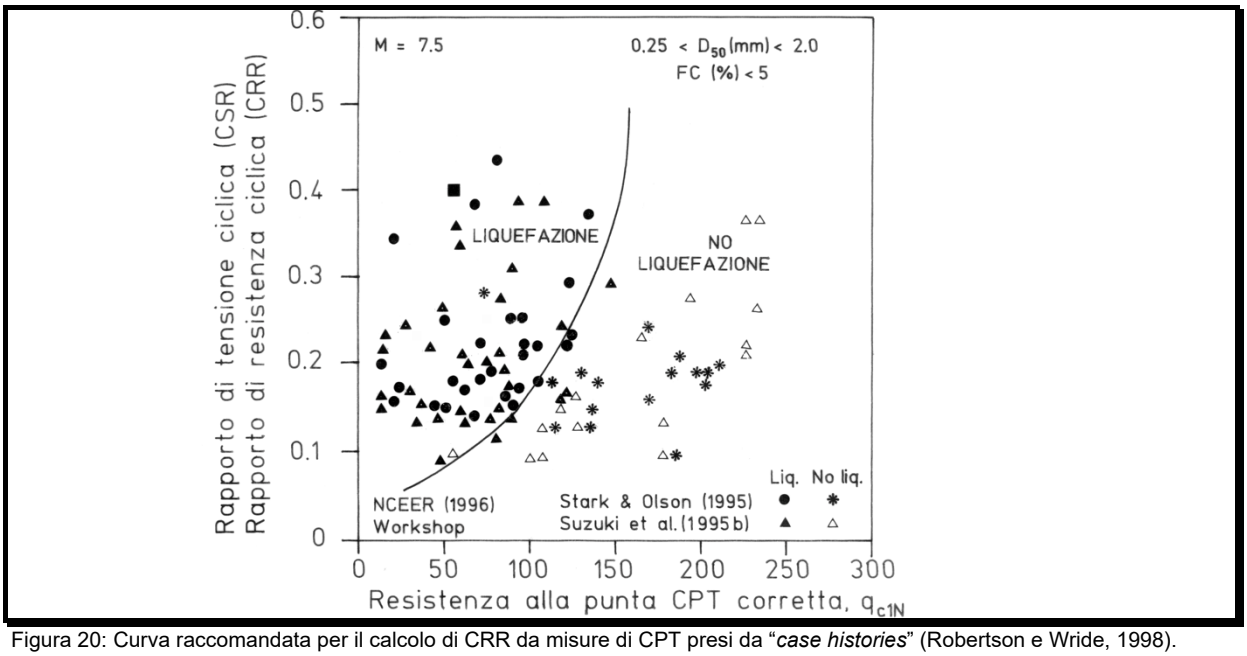


Figura 20: Curva raccomandata per il calcolo di CRR da misure di CPT presi da "*case histories*" (Robertson e Wride, 1998).

Per le verifiche a liquefazione del sito sono state perseguite tre metodologie per ottenere la Magnitudo del momento sismico (Mw) di riferimento per il calcolo:

1. tramite le zone sismogenetiche ZS9, che indicano una magnitudo massima per ogni zona (al più si può discretizzare in base al database DISS);
2. tramite la consultazione del Catalogo Parametrico dei Terremoti italiani (CPTI) (sito emidius.mi.ingv.it/cpti11) con individuazione del sito e il filtro di tutti i terremoti presenti in un'area circolare di 50 km di raggio (riferendosi al lavoro di Galli et *alli*, per cui sono da ritenersi poco probabili fenomeni di liquefazione ubicati oltre i 50 km di distanza dall'epicentro) oltre alla verifica del database DISS 3.1;

3. Tramite la mappa interattiva di pericolosità sismica dell'INGV (indirizzo esse1-gis.mi.ingv.it), in cui è possibile calcolare il terremoto di scenario basandosi sul concetto di disaggregazione della pericolosità sismica in cui si sommano i contributi dovuti alle singole coppie magnitudo-distanza degli epicentri ricadenti all'interno dell'area di riferimento (50 km).

Il primo metodo non considera il tempo di ritorno come da normativa pertanto risulta eccessivamente gravoso mentre il secondo metodo è sicuramente meno oneroso. Di seguito si riportano i valori di Mw ottenuti per ognuno dei metodi applicati:

1. Mw = 6,14 Zona sismogenetica 612;
2. SISMA DI RIFERIMENTO
   - 29 maggio 2012 con epicentro a Finale Emilia (MO) (lat. 44.905800– lon. 11.234248);
   - distanza dell'area di studio dall'epicentro ~ 13 Km;
   - magnitudo Mw riferita al terremoto di riferimento pari a ≈ 5.9;
   - $a_{max} = a_g \times S_t \times S_s = a_{refg} \times S_t \times S_s = 0.157 \times 1.59 \approx 0.25$ (per terreni di categoria C)
3. Mw = 5,06 con distanza epicentrale di 20,7km (metodo della disaggregazione)

Come anticipato è stato effettuato un campionamento, durante la campagna di indagini, con prelievo di un campione indisturbato con fustella a pareti sottili di tipo shelby e sottoposta ad analisi granulometrica per vagliatura e sedimentazione i cui esiti sono stati sovrapposti al fuso granulometrico di possibile liquefazione proposto da AGI e dalla Delibera regionale (Atto di indirizzo e coordinamento tecnico prog. 112). Gli esiti dimostrano che le sabbie del campione sono perfettamente comprese entro il fuso granulometrico suscettibile di liquefazione con Uc > 3,5 (fig. 21). Le verifiche sono state condotte secondo il metodo di Idriss e Boulanger (2014) tramite programma di calcolo automatico della liquefacibilità e dei cedimenti post sisma con il software "Cliq", sviluppato dalla GeoLogismiki Geotechnical Engineers in collaborazione con P.K. Roberson. Le verifiche sono state comunque condotte nelle condizioni peggiorative ovvero con Mw = 6,14 (zona sismogenetica 612) e a_{gmax} = 0.23 g (come da RSL) e falda durante l'evento sismico fino ad un massimo tra -0,4 e -2,00 m da p.c.. Di seguito si riportano le verifiche effettuate sulle prove CPTu-1, CPTu-2, CPTu-3, CPTu-4, CPTu-5 e CPTu-6 (fig.24).

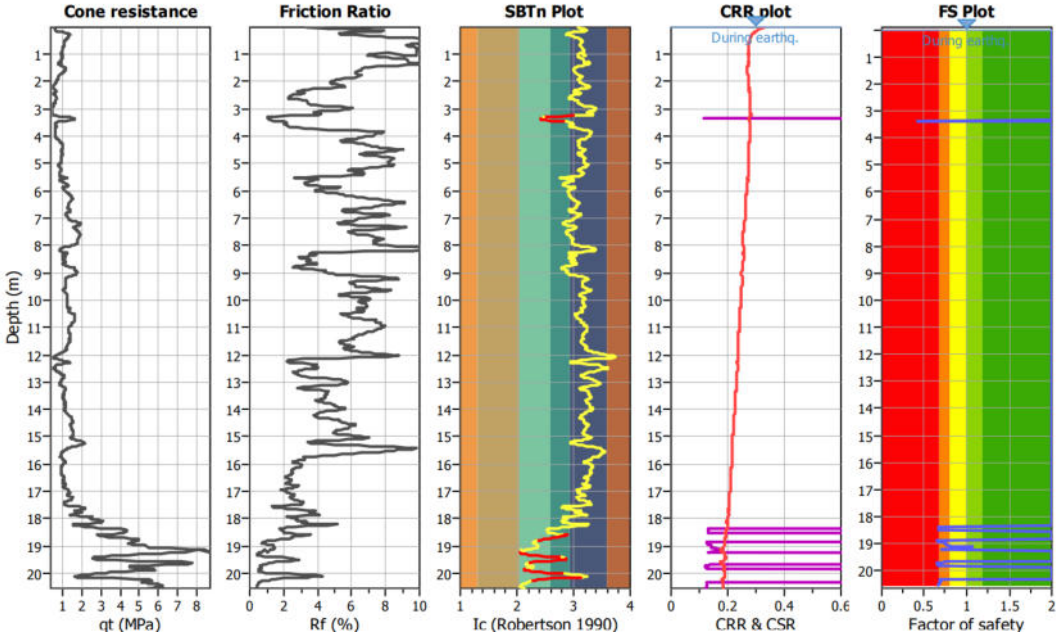
9.5.1 VERIFICA IN CONDIZIONI DI TERRENO DI CATEGORIA C (AMAX = 0.23g)

CPTu-1

CPT file : CPTu-01_Biancolina

Input parameters and analysis data

Analysis method:	B&I (2014)	G.W.T. (in-situ):	0.60 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	0.00 m	Fill height:	N/A	applied:	Sands only
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude M_w:	6.14	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.23	Unit weight calculation:	Based on SBT	K_σ applied:	Yes	MSF method:	Method based

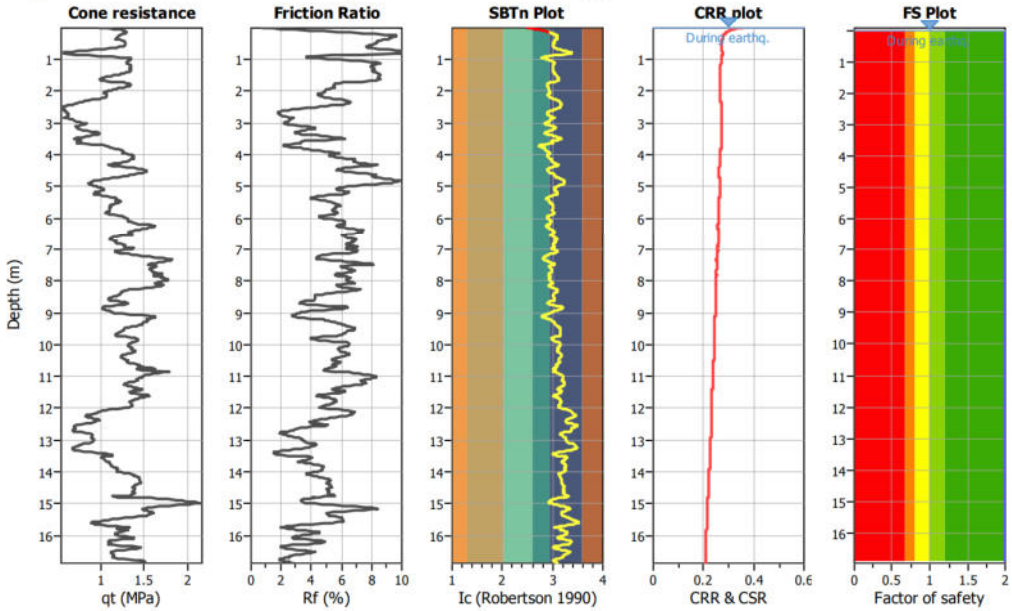


CPTu-2

CPT file : CPTu-02_Biancolina

Input parameters and analysis data

Analysis method:	B&I (2014)	G.W.T. (in-situ):	0.60 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	0.00 m	Fill height:	N/A	applied:	Sands only
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude M_w:	6.14	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.23	Unit weight calculation:	Based on SBT	K_σ applied:	Yes	MSF method:	Method based

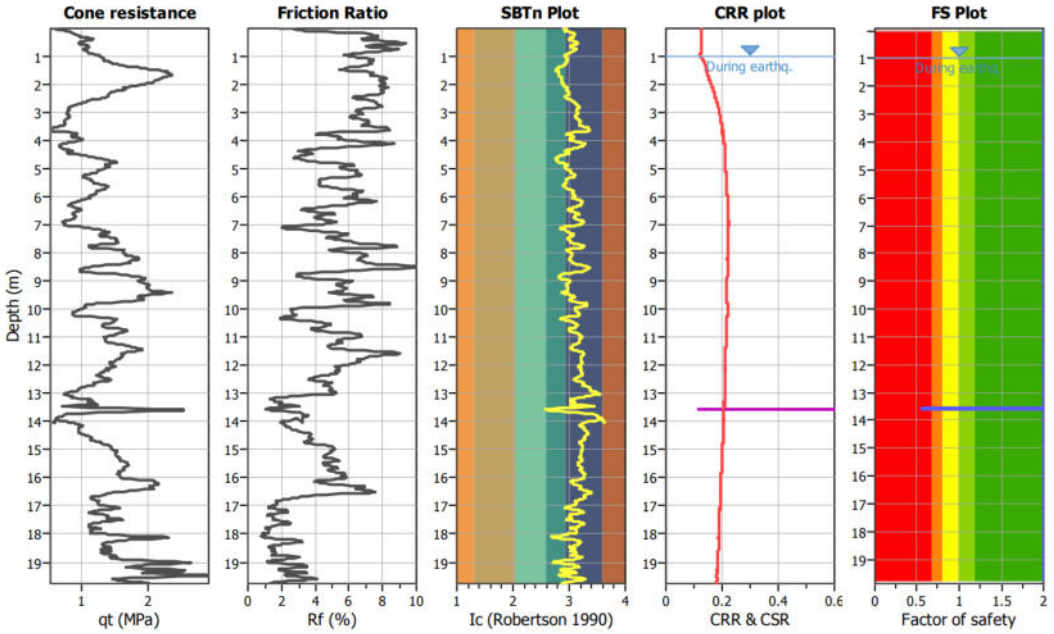


CPTu-3

CPT file : CPTu-03_Biancolina

Input parameters and analysis data

Analysis method:	B&I (2014)	G.W.T. (in-situ):	2.20 m	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.00 m	Fill height:	N/A	Limit depth applied:	No
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	N/A
Earthquake magnitude M_w:	6.14	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.23	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		

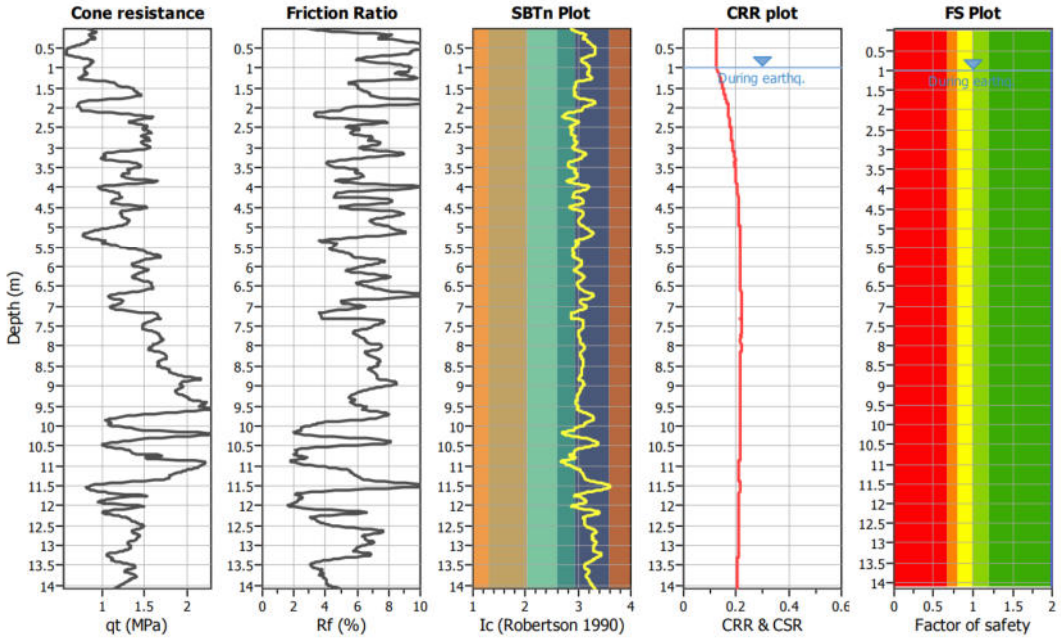


CPTu-4

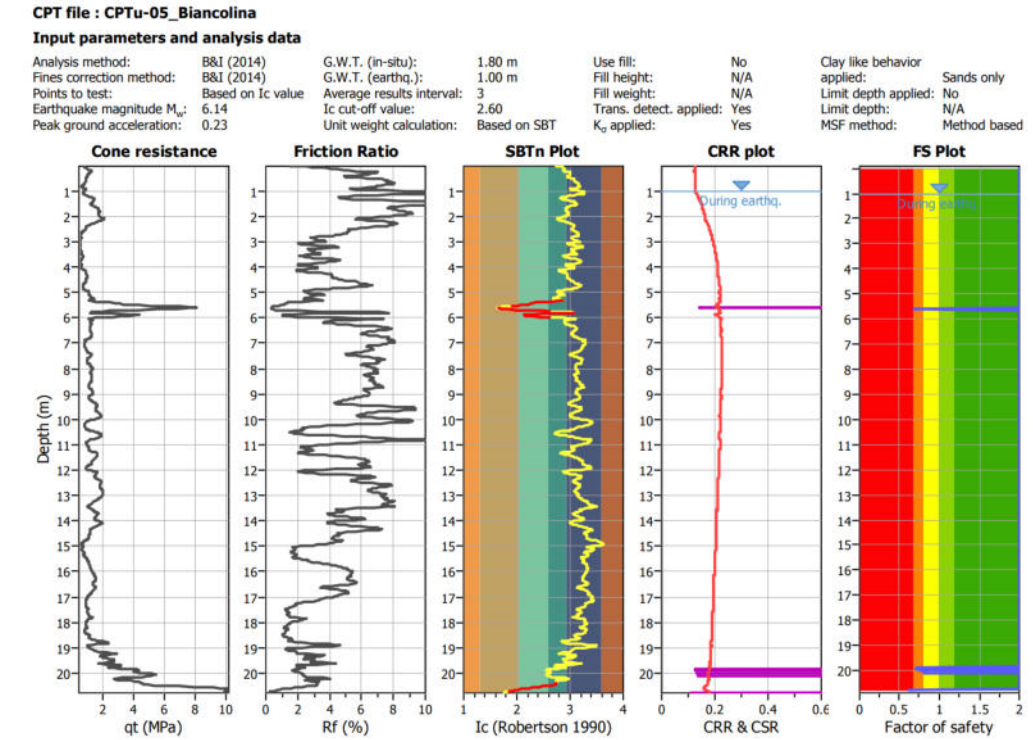
CPT file : CPTu-04_Biancolina

Input parameters and analysis data

Analysis method:	B&I (2014)	G.W.T. (in-situ):	2.20 m	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.00 m	Fill height:	N/A	Limit depth applied:	No
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	N/A
Earthquake magnitude M_w:	6.14	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.23	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		



CPTu-5



CPTu-6

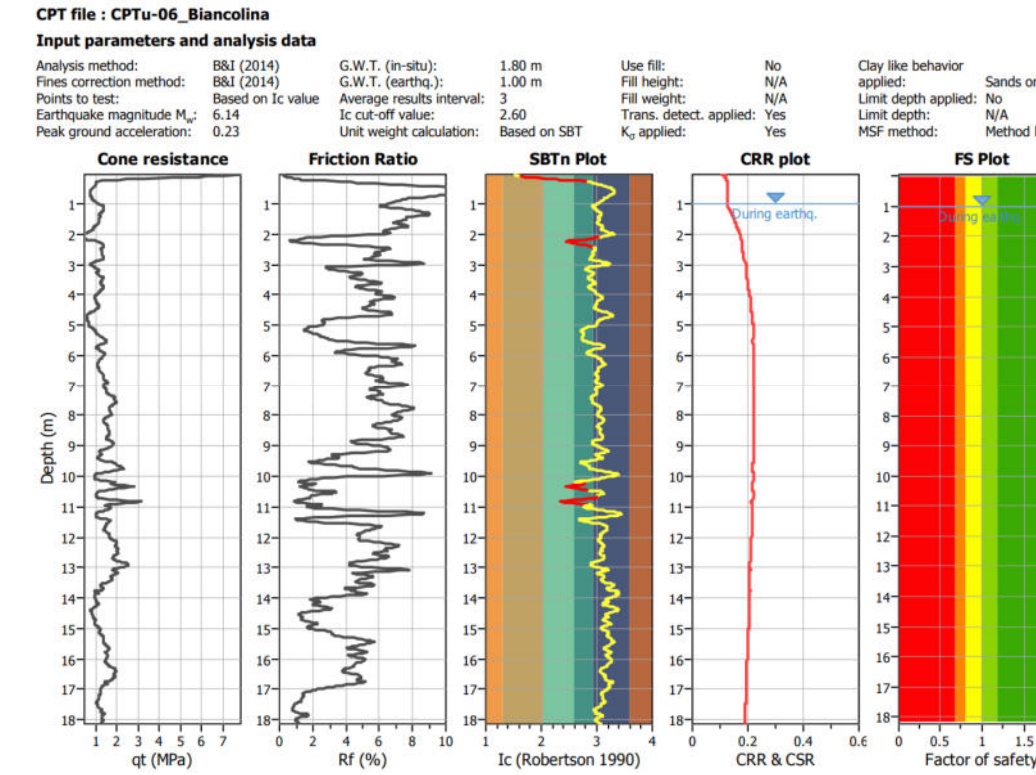


Figura 21: risultanza delle verifiche relative alla suscettibilità alla liquefazione.

Risulta, quindi, una pericolosità ed una propensione alla liquefazione bassa/nulla per quanto riguarda l'area di sedime del futuro campo agrivoltaico.

Pertanto, dati i valori certamente cautelativi della Mw (valore massimo attesa per la zona sismogenetica 912) e dell'a_{gmax}, ottenuto dalla RSL, l'area di studio risulta suscettibile alla liquefazione per l'area dell'agrivoltaico. Per queste aree si ritiene l'adozione di fondazioni superficiali a platea a garantire la sicurezza in caso di sisma per le opere connesse.

9.6 INDICE DEL POTENZIALE DI LIQUEFAZIONE E CEDIMENTI ATTESI

Per poter procedere alla rappresentazione del rischio di liquefazione occorre riferirsi a valori numerici associati ad ogni verticale di prova. Un indice sintetico, rappresentativo del rischio di liquefazione, applicabile a tutti i metodi che prevedono il calcolo del profilo del fattore di sicurezza, è l'indice del potenziale di liquefazione IP_L, introdotto da Iwasaki et al. (1978):

$$P_L = \int_0^{z_{crit}} F(z) \cdot w(z) \cdot dz$$

in cui F(z) è una funzione che per F.L. > 1 assume valore zero e per F.L. < 1 ne è il complemento ad 1, e $w(z) = 10 - 10 \cdot (z/z_{crit})$ è una funzione linearmente decrescente della profondità, z_{crit} è la profondità oltre la quale sono da escludersi fenomeni di liquefazione, il cui valore è per la maggior parte degli Autori = 20 m.

Valore di I_L	Rischio di liquefazione
$IP_L = 0$	Molto basso
$0 < IP_L \leq 2$	Basso
$2 < IP_L \leq 5$	Moderato
$5 < IP_L \leq 15$	Alto
$15 < IP_L$	Molto alto

Tabella 9: Indice di liquefazione e livello associato di rischio.

I risultati sul valore dell'indice del potenziale di liquefazione, sono stati calcolati con il metodo di Idriss & Boulanger (2014), mentre per la discretizzazione del potenziale di liquefazione, in base ai colloqui intercorsi, è stata assunta secondo le classi di pericolosità di Sonmerz (2003) e Riga (2007), già ripresa nella DGR 630/2019 per quanto riguarda la pianificazione territoriale; inoltre le indagini, elaborate con il software Cliq della Geologismiki in collaborazione con il prof. P.K. Robertson, sono state valutate con l'esclusione delle fasce di transizione; in questo caso sono stati esclusi dal calcolo del potenziale di liquefazione tutte le fasce tessiturali di transizione (es limi sabbiosi) con I_c compreso fra 1,7 e 3,0 e che nel contempo rispettino il criterio degli strati sottili così come indicato dallo stesso

Robertson. Il software elimina i dati quando il cono (la punta della prova penetrometrica elettrica) è in transizione da argilla a sabbia o viceversa. Per fare ciò il software richiede un intervallo di valori Ic oltre i quali verrà definita la transizione (in genere tra 1,80 <Ic <3,0) ed un tasso di variazione di Ic. Le transizioni si verificano in genere quando il tasso di variazione di Ic è rapido.

In questo caso il potenziale di liquefazione è elevato in quanto non siamo più in presenza di uno strato liquefacibile, intercalato da lenti di materiali fini che ne riducono il potenziale; di seguito le risultanze:

RISULTANZE VERIFICA DELL'INDICE DEL POTENZIALE DI LIQUEFAZIONE

Cptu-1:	IP_L = 0,19	Rischio di Liquefazione MOLTO BASSO
Cptu-2:	IP_L = 0,00	Rischio di Liquefazione MOLTO BASSO
Cptu-3:	IP_L = 0,06	Rischio di Liquefazione MOLTO BASSO
Cptu-4:	IP_L = 0,00	Rischio di Liquefazione MOLTO BASSO
Cptu-5:	IP_L = 0,13	Rischio di Liquefazione MOLTO BASSO
Cptu-6:	IP_L = 0,00	Rischio di Liquefazione MOLTO BASSO

RISULTANZE VERIFICA DEI CEDIMENTI POST SISMICI ATTESI

Cptu-1:	cedimento	3,56 cm
Cptu-2:	cedimento	0,00 cm
Cptu-3:	cedimento	0,16 cm
Cptu-4:	cedimento	0,00 cm
Cptu-5:	cedimento	1,03 cm
Cptu-6:	cedimento	0,00 cm

In questo caso viene dimostrata un indice del potenziale di Liquefazione MOLTO BASSO. Di seguito, figura 22, si riportano i grafici comparativi fra la verticale di indagine e con vari autori a confronto.

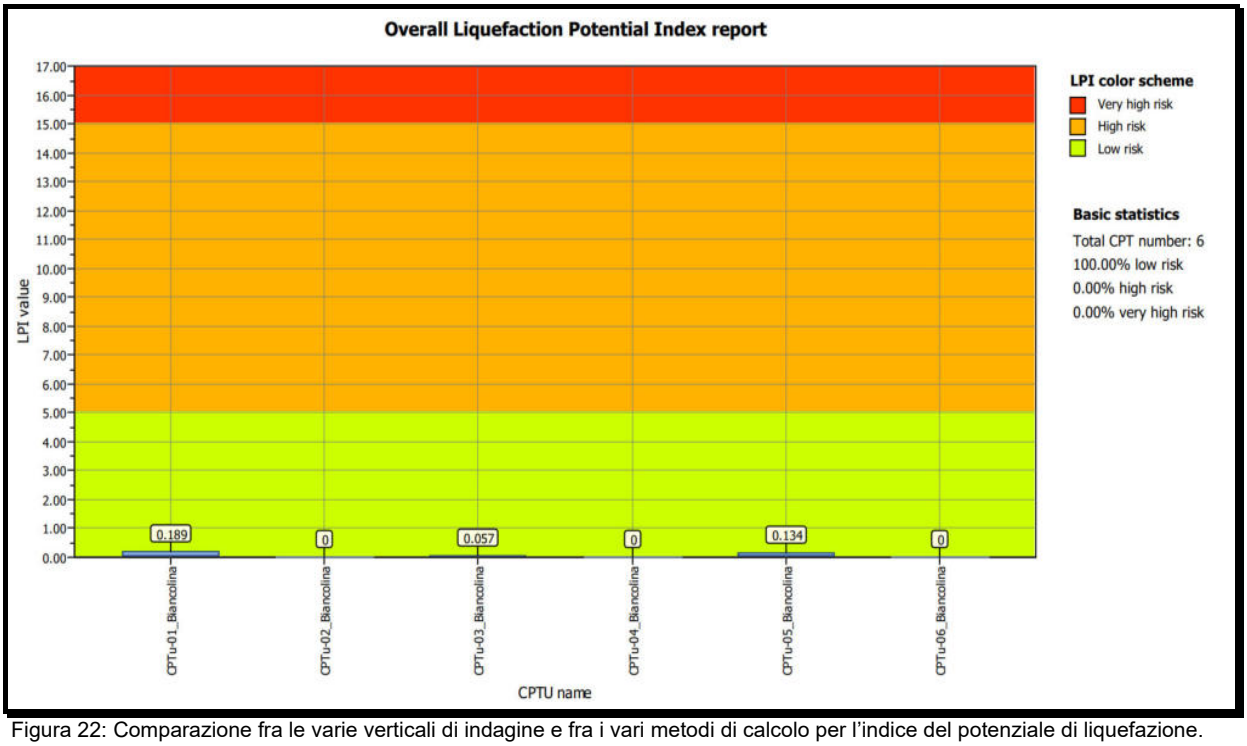


Figura 22: Comparazione fra le varie verticali di indagine e fra i vari metodi di calcolo per l'indice del potenziale di liquefazione.

Un altro parametro è l'indice di Severità di Liquefazione (Liquefaction Severity Number LSN) sulla base delle fasce di severità proposte da Tonkin e Taylor

0 < LSN < 10	Assenza di liquefazione/ minime espressioni di liquefazione
10 < LSN < 20	Minime espressioni di liquefazione
20 < LSN < 30	Moderate espressioni di liquefazione
30 < LSN < 40	Da moderate a severe espressioni di liquefazione
40 < LSN < 50	Maggiori espressioni di liquefazione
LSN > 50	Danni gravi

Tabella 10: Severità di liquefazione in base al parametro LSN (Tonkin e Taylor, 2013).

Le manifestazioni superficiali sono condizionate dal rapporto tra strati liquefacibili/non e dalla relativa posizione stratigrafica; ovvero viene messo in relazione al possibile danno superficiale atteso in relazione alla posizione dello strato liquefacibile.

I risultati sul valore dell'indice di severità di liquefazione, sono stati calcolati con il metodo di Idriss & Boulanger (2014); di seguito le risultanze:

RISULTANZE VERIFICA DELL'INDICE DI SEVERITÀ DI LIQUEFAZIONE

Cptu-1: LSN =2,025 Assenza di liquefazione/minime espressioni di liquefazione;
Cptu-2: LSN =0,00 Assenza di liquefazione/minime espressioni di liquefazione;
Cptu-3: LSN =0,121 Assenza di liquefazione/minime espressioni di liquefazione;
Cptu-4: LSN =0,00 Assenza di liquefazione/minime espressioni di liquefazione;
Cptu-5: LSN =0,749 Assenza di liquefazione/minime espressioni di liquefazione;
Cptu-6: LSN =0,00 Assenza di liquefazione/minime espressioni di liquefazione;

Correlando l'indice IPL con l'indice LSN si evince come, per l'area di studio, la suscettibilità alla liquefazione risulti assente/con minime espressioni.

Di seguito i grafici comparativi per la verticale di indagine e per le varie metodologie a confronto (figura 23).

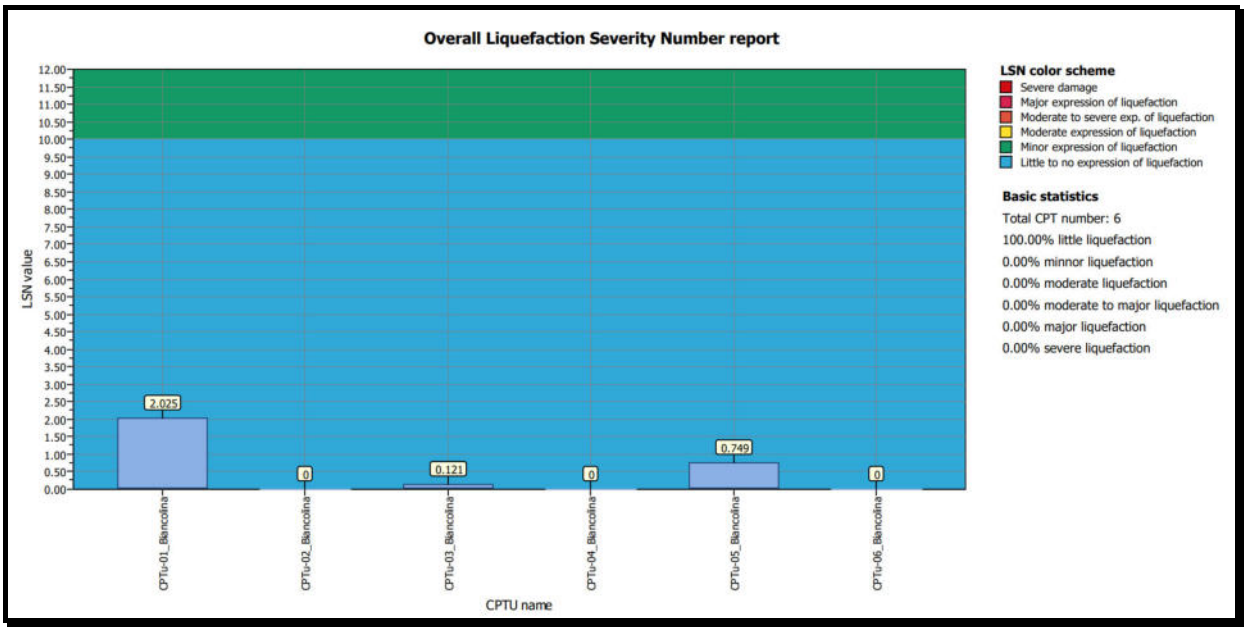


Figura 23: Comparazione fra le varie verticali di indagine e fra i vari metodi di calcolo per l'indice del potenziale di liquefazione.

Da tutte le verifiche effettuate si pone l'ovvio accento della BASSA/NULLA sensibilità dell'area di sedime alla liquefazione. Appare comunque corretta l'adozione di fondazioni a platea.

10. Considerazioni conclusive

In base a quanto sinora riportato, è possibile concludere che l'area in esame è situata in una zona avente elementi di pericolosità geologica e di conseguenza, nel complesso, vulnerabile.

Come precedentemente ricordato, impiegando prove geofisiche, sondaggi penetrometrici meccanici effettuati nell'area di studio, si è rilevato la presenza di eteropie di facies tra litologie argillo limose e limo argillose, inorganiche, da mediamente a consistenti, con intercalazioni di sabbie medio-fini e argille/argille limose a tratti organiche. Inoltre, in tutta l'area di studio, è stato riscontrato un paleosuolo.

Tali livelli, di natura alluvionale/tracimazione, sono poggianti su substrato (Pliocenico), rinvenibile a profondità elevata data la natura tettonica del cambio fra l'area pedecollinare e la Pianura.

Le criticità descritte nei capitoli precedenti evidenziano particolari problematiche intrinseche le aree; i siti di studio risultino potenzialmente allagabili in quanto si trovano in zone a forte depressione morfologica e ad alta subsidenza nelle vicinanze di torrenti soggetti a tracimazione (fonti storiche).

Per quanto riguarda la vulnerabilità degli acquiferi definita, dalle carte tematiche consultate e citate, risulta una vulnerabilità medio-bassa per la presenza di terreni coesivi impermeabili superficiali e di limi sabbiosi – sabbie limose (alternati ad argille limose) che aumentano la vulnerabilità.

Per quanto riguarda le verifiche alla propensione alla liquefazione dei terreni presenti, ci si rifà a quanto già affermato nei capitoli precedenti, ovvero l'area risulta con un potenziale di liquefazione basso/nullo; nonostante ciò, è consigliabile tenere conto dell'eventuale rischio associato a questo fenomeno. Si richiama l'attenzione solamente per quanto riguarda le problematiche inerenti la possibilità di occorrenza di fenomeni di liquefazione. E' stata effettuata una valutazione sulla probabilità di liquefazione dei terreni con il metodo di Idriss & Boulanger (2014) per la verticale di indagine effettuate; è risultata una propensione alla liquefazione BASSA/NULLA. Oltre all'indice del potenziale di liquefazione IPL, è stato valutato anche l'indice di severità a liquefazione LSN che fornisce importanti informazioni sulla reale espressione di fenomeni di liquefazione in relazione alle opere in superficie; in quest'ultimo caso è risultato una severità quasi nulla. E' evidente che per l'area di sedime l'indice di potenziale liquefazione sia basso/nullo e che vi sia uno scarso potenziale pericolo di liquefazione. Sono tuttavia consigliate fondazioni di tipo platea per le opere connesse.

Inoltre la caratterizzazione sismica dei luoghi (in accordo con le prove penetrometriche e con le

analisi svolte nelle schede di microzonazione) ha definito l'appartenenza dei suoli alla categoria **C** con Vs_{eq} ≈ 192,0 m/s con frequenze di sito pari a 0,63 Hz, indice di importanti contrasti di impedenza che possono dare origine a significative variazioni del moto dell'onda sismica. Va posta pertanto attenzione evitando effetti di risonanza fra le opere in progetto ed i terreni di fondazione.

Data la presenza di terreni superficiali agricoli, si consiglia l'appoggio delle fondazioni almeno al di sotto del primo strato (circa -0,8÷-1,0 m da p.c), al fine di evitare di appoggiare le strutture di fondazione al di sopra di terreni eccessivamente cedevoli; inoltre, dai dati ottenuti dalle CPTu, si è potuto notare come le temperature stagionali hanno avuto influenza sui terreni coesivi fino a circa -3,0 m dal piano campagna. Questo ad indicare che, in ragione della stagionalità, saranno presenti fenomeni di variazione volumetrica della frazione coesiva con abbassamenti e rigonfiamenti dell'intera successione stratigrafica fino a – 3,0 m.

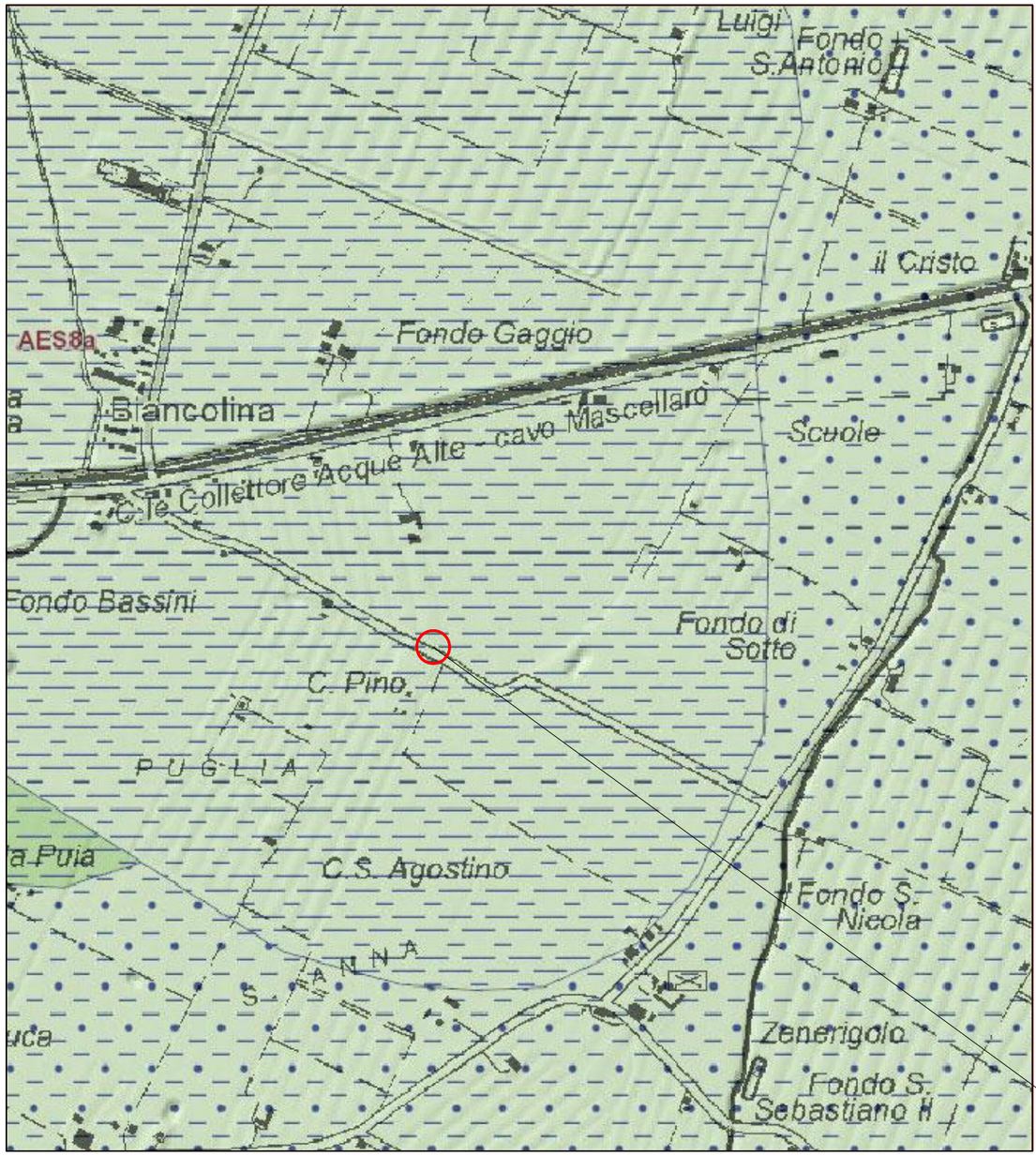
Grande attenzione si dovrà prestare agli eventuali cedimenti differenziali in relazione alle differenze riscontrate fra le varie verticali di indagine.

Sulla scorta di quanto rilevato nell'ambito del presente studio, osservando le prescrizioni precedentemente esposte, non si ravvedono elementi sfavorevoli dal punto di vista idrogeologico e geologico per l'area oggetto di studio e si ritiene fattibile la realizzazione delle opere in progetto.

Dott.ssa geol. Giulia Gardosi

Tavole

- corografia generale	1 : 25.000-
- corografia–	1 : 25.000-
- carta geologica	1 : 10.000-
- Tav-1 - inquadramento territoriale	1 : 5.000-
- Tav-2 – ubicazione indagini	1 : 300-
- Tav-3a– stratigrafia interpretativa	
- Tav-3b– stratigrafia interpretativa	



area di studio

AMOLA DEL PIANO **SEZIONE N° 202110 -scala 1:10.000-**

SAN GIOVANNI IN PERSICETO **SEZIONE N° 202150 -scala 1:10.000-**

SUCCESSIONE NEOGENICO-QUATERNARIA DEL MARGINE APPENNINICO PADANO

AES8 **Subsintema di Ravenna**

AES8a **Unità di Modena**

SEGNI CONVENZIONALI

60 Strati diritti.

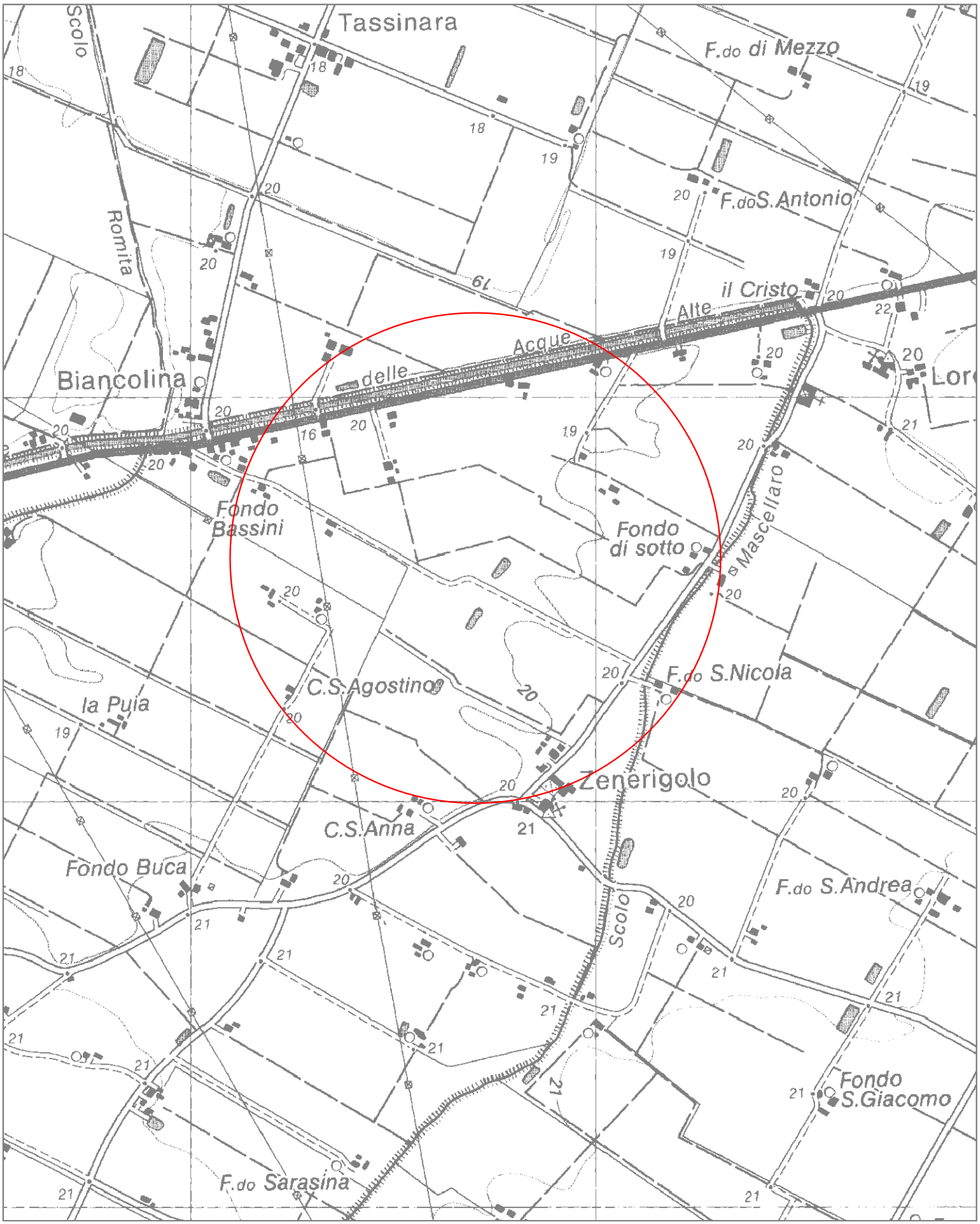
Limite stratigrafico.

Faglia certa

Faglia dedotta

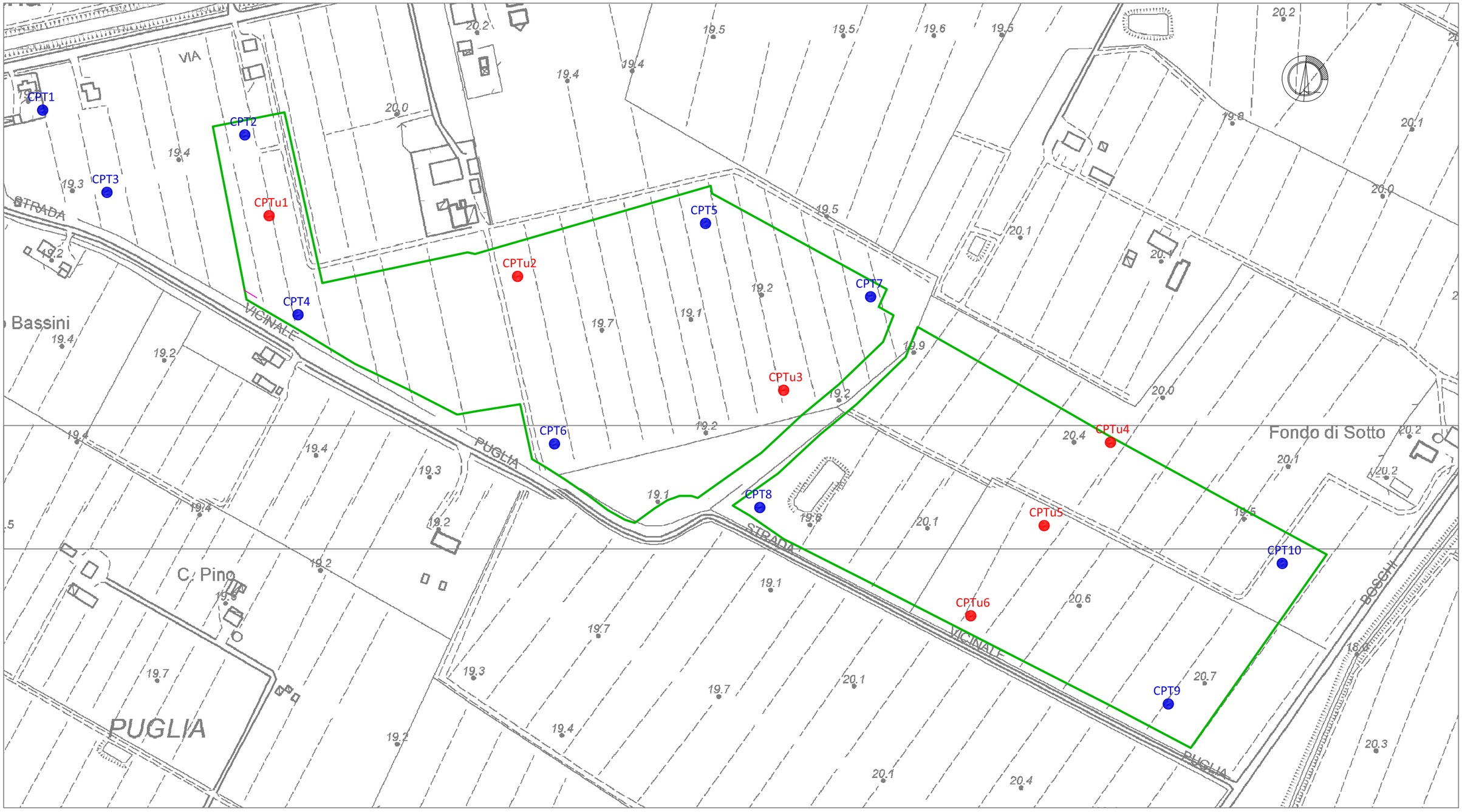
Sovrascorrimento certo

Corografia



Stralcio dalla Tavola. N° 202SE –SAN GIOVANNI IN PERSICETO–
con indicata l'area di intervento – scala 1:25.000 –

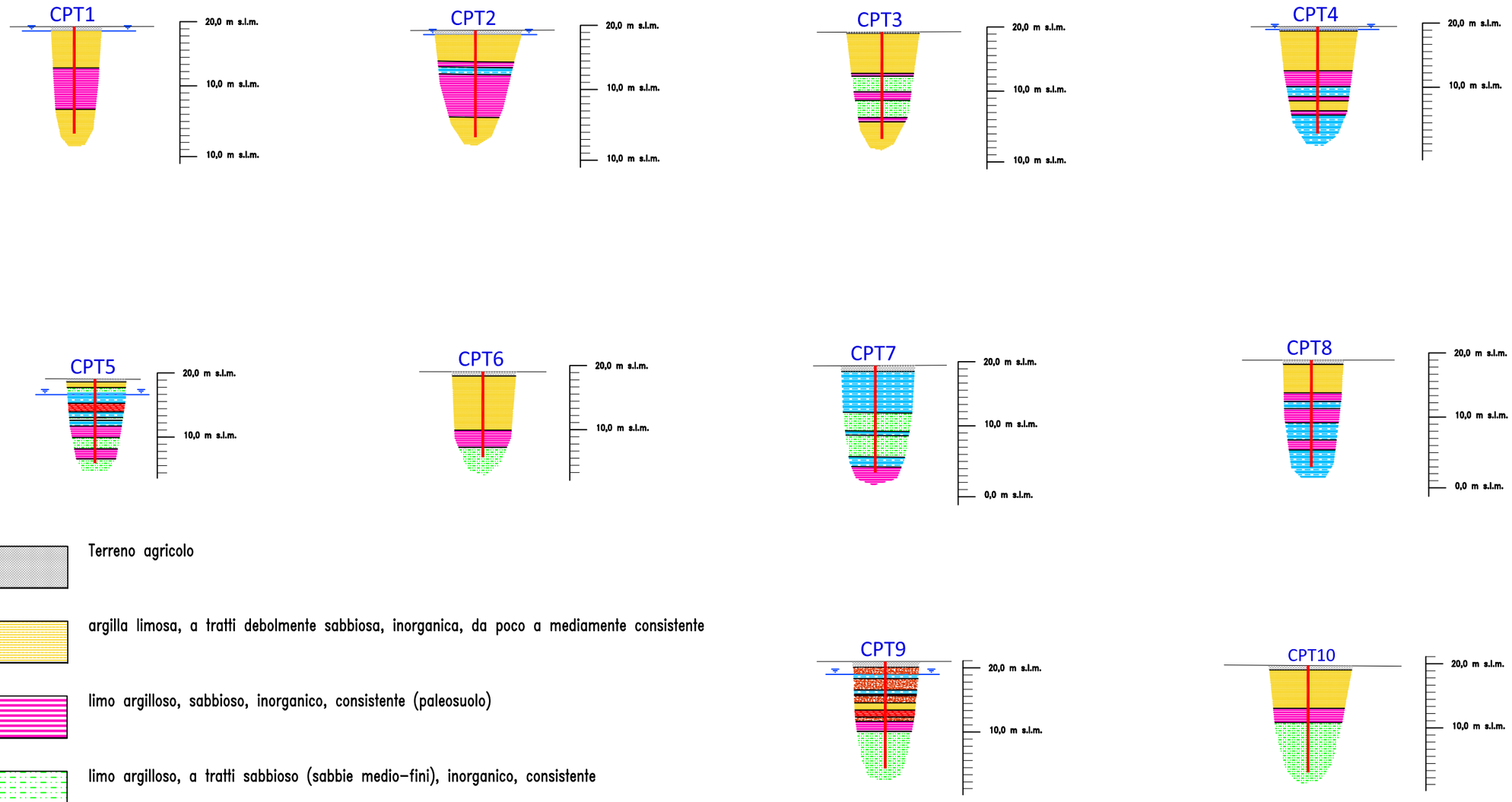
Stralcio dagli Elementi C.T.R. N° 202151 –ZENERIGOLO–
e N° 202112 –LORENZATICO– con indicata l'area di intervento – scala 1:5.000 –



Ubicazione sondaggi penetrometrici sulla planimetria di progetto – scala 1:3000

CPTu-1 *sondaggio penetrometrico statico con piezocono*

CPT-1 *sondaggio penetrometrico statico meccanico*



Terreno agricolo

argilla limosa, a tratti debolmente sabbiosa, inorganica, da poco a mediamente consistente

limo argilloso, sabbioso, inorganico, consistente (paleosuolo)

limo argilloso, a tratti sabbioso (sabbie medio-fini), inorganico, consistente

argilla limosa/limo argilloso, a tratti sabbioso, inorganico, da mediamente a consistente

argilla/argilla limosa, a tratti organica, poco consistente

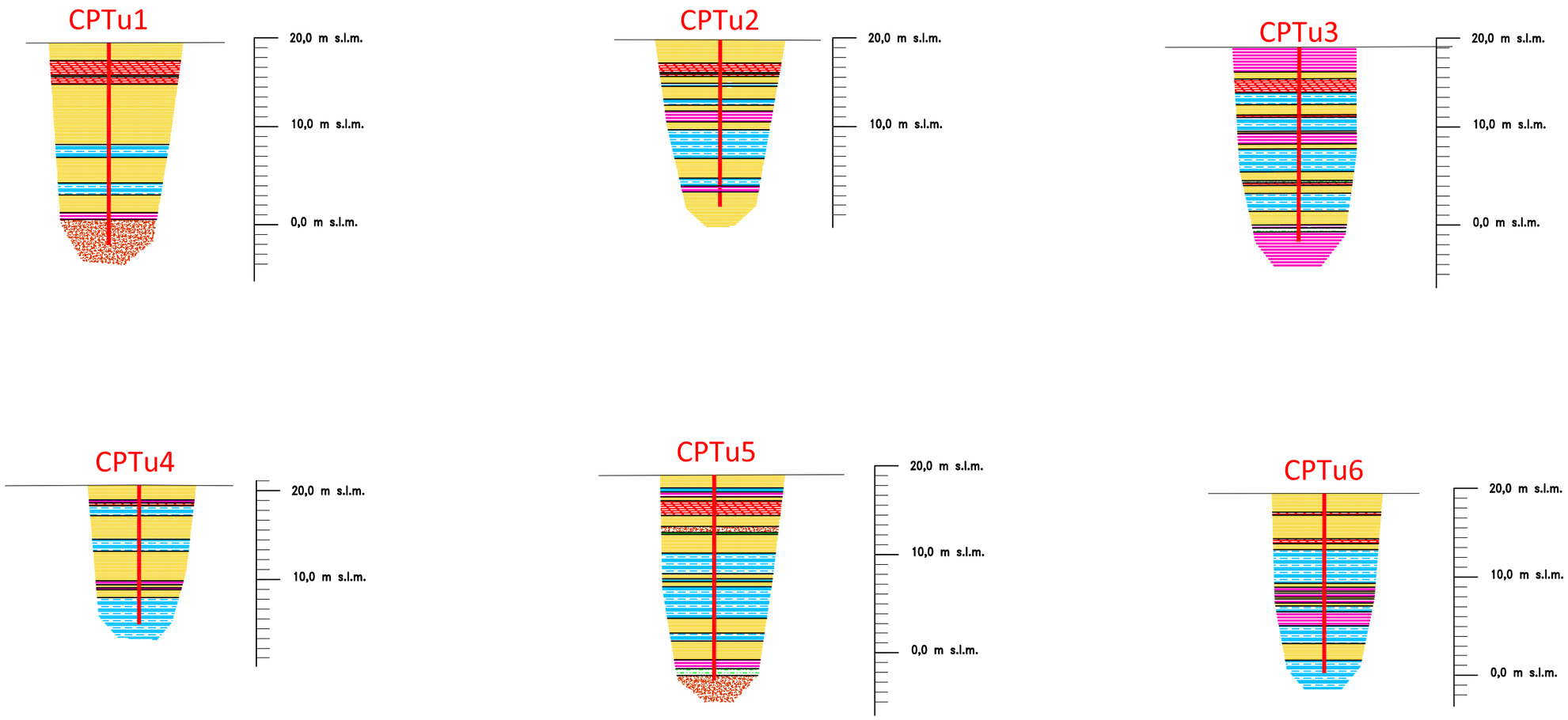
sabbie medio fini, a tratti limos, da moderatamente ad addensate

Sezione stratigrafica interpretativa

CPT-1 *prova penetrometrica statica meccanica*

CPTU-1 *prova penetrometrica statica elettrica con piezocono*

Tavola 3b



- Terreno agricolo
- argilla limosa, a tratti debolmente sabbiosa, inorganica, da poco a mediamente consistente
- limo argilloso, sabbioso, inorganico, consistente (paleosuolo)
- limo argilloso, a tratti sabbioso (sabbie medio-fini), inorganico, consistente
- argilla limosa/limo argilloso, a tratti sabbioso, inorganico, da mediamente a consistente
- argilla/argilla limosa, a tratti organica, poco consistente
- sabbie medio fini, a tratti limos, da moderatamente ad addensate

Sezione stratigrafica interpretativa

CPT-1 *prova penetrometrica statica meccanica*

CPTU-1 *prova penetrometrica statica elettrica con piezocono*

Elenco Allegati

Allegato 1: prove penetrometriche statiche meccaniche

Allegato 2: prove penetrometriche elettriche con piezocono

Allegato 3: prove di laboratorio

Allegato 4: indagini geofisiche

Allegato 5: report liquefazione

ALLEGATO I

- PROVE PENETROMETRICHE STATICHE MECCANICHE-

DIAGRAMMI DI RESISTENZA

--

TABELLE VALORI DI RESISTENZA

--

VALUTAZIONI LITOLOGICHE

--

PARAMETRI GEOTECNICI

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

LEGENDA VALORI DI RESISTENZA
FATTORI DI CONVERSIONE

Strumento utilizzato:
TG63-200 - Pagani - Piacenza

Caratteristiche:

- punta conica meccanica Ø 35.7 mm, area punta Ap = 10 cm²

- punta conica meccanica angolo di apertura: α = 60°

- manicotto laterale di attrito tipo 'Begemann' (Ø = 35.7 mm - h = 133 mm - Am = 150 cm²)

- velocità di avanzamento costante V = 2 cm/sec (± 0,5 cm / sec)

- spinta max nominale dello strumento Smax variabile a seconda del tipo

- costante di trasformazione CT = SPINTA (Kg) / LETTURA DI CAMPAGNA
  (dato tecnico legato alle caratteristiche del penetrometro utilizzato, fornito dal costruttore)

fase 1 - resistenza alla punta: qc (kg/cm²) = (L1) x CT /10

fase 2 - resistenza laterale locale: fs (kg/cm²) = [(L2) - (L1)] x CT / 150

fase 3 - resistenza totale : Rt (kg/cm²) = (Lt) x CT

- Prima lettura = lettura di campagna durante l' infissione della sola punta (fase 1)
- Seconda lettura = lettura di campagna relativa all'infissione di punta e manicotto (fase 2)
- Terza lettura = lettura di campagna relativa all'infissione delle aste esterne (fase 3)

N.B. : la spinta S (Kg) , corrispondente a ciascuna fase , si ottiene moltiplicando la corrispondente lettura di campagna L per la costante di trasformazione CT .

N.B. : causa la distanza intercorrente (20 cm circa) fra il centro del manicotto laterale e la punta conica del penetrometro , la resistenza laterale locale fs viene computata 20 cm sopra la punta .

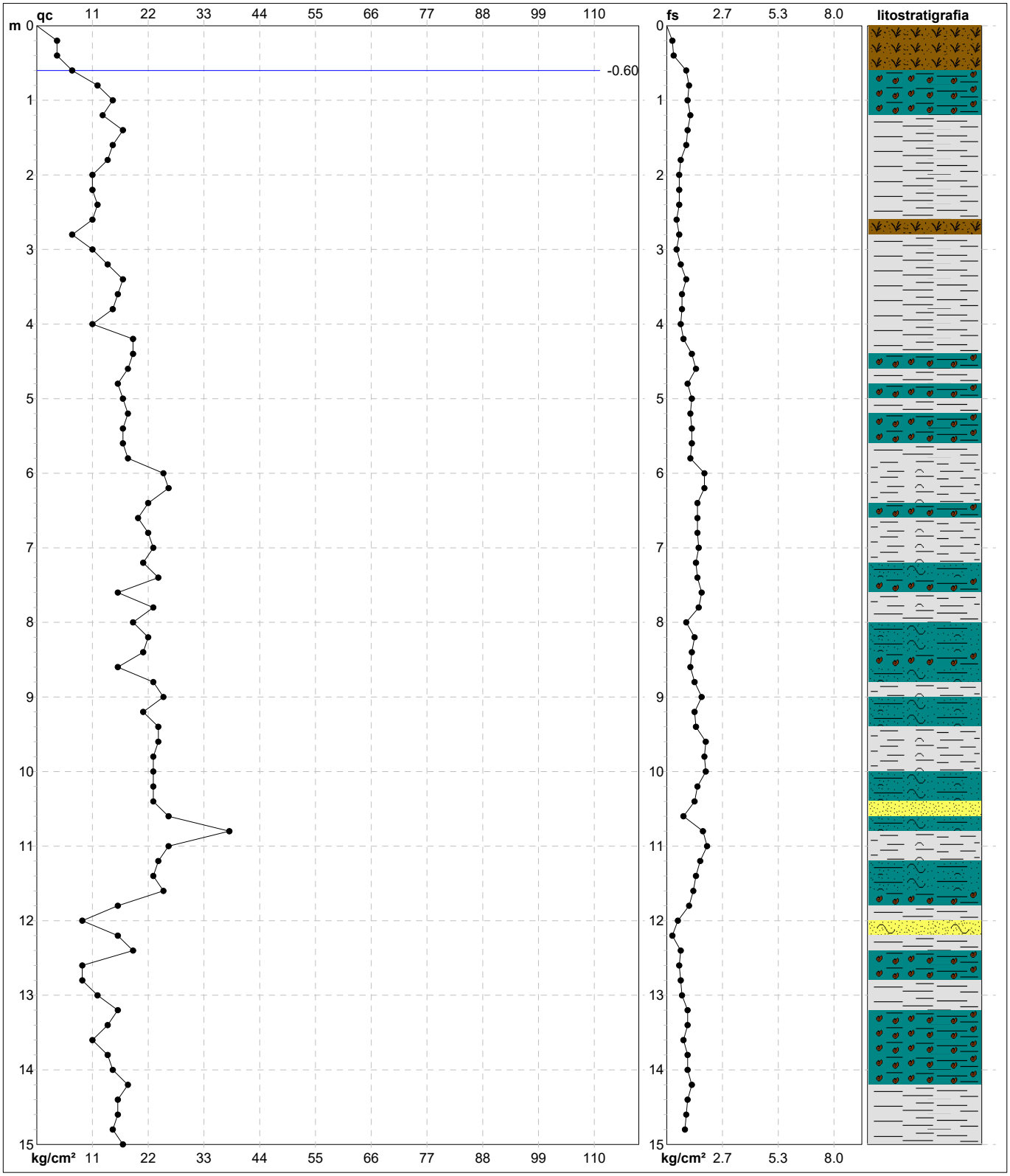
CONVERSIONI
1 kN (kiloNewton) = 1000 N $\approx$ 100 kg = 0,1 t
1 MN (megaNewton) = 1.000 kN = 1.000.000 N $\approx$ 100 t
1 kPa (kiloPascal) = 1 kN/m² = 0,001 MN/m² = 0,001 MPa $\approx$ 0,1 t/m² = 0,01 kg/cm²
1 MPa (megaPascal) = 1 MN/m² = 1.000 kN/m² = 1000 kPa $\approx$ 100 t/m² = 10 kg/cm²
1 kg/cm² = 10 t/m² $\approx$ 100 kN/m² = 100 kPa = 0,1 MN/m² = 0,1 MPa
1 t = 1000 kg $\approx$ 10 kN

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI DI RESISTENZA E LITOLOGIA

CPT	1
riferimento	110-2023

Committente:	**Green-go**	U.M.: **kg/cm²**	Data esec.: 01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Scala: 1:75	
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Pagina: 1	Quota inizio: Piano Campagna
		Elaborato:	Falda: -0.60 m Non rilevata



		Litologia: Begemann [qc + qc/fs] 4 Zone	Preforo: m
		Penetrometro: TG63-200	Corr.astine: kg/ml
		Responsabile: Servizi Geotecnici	Cod.ISTAT: 037053
		Assistente:	Cod. punta:

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
LETTURE CAMPAGNA E VALORI TRASFORMATI

CPT	1
riferimento	110-2023

Committente:	**Green-go**	U.M.: **kg/cm²**	Data esec.: 01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Pagina: 1	
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Elaborato:	Falda: -0.60 m Non rilevata

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %
0.20	4.0	9.0		4.00	0.27	15	6.8
0.40	4.0	8.0		4.00	0.33	12	8.3
0.60	7.0	12.0		7.00	0.93	8	13.3
0.80	12.0	26.0		12.00	1.07	11	8.9
1.00	15.0	31.0		15.00	1.00	15	6.7
1.20	13.0	28.0		13.00	1.13	12	8.7
1.40	17.0	34.0		17.00	1.00	17	5.9
1.60	15.0	30.0		15.00	0.93	16	6.2
1.80	14.0	28.0		14.00	0.67	21	4.8
2.00	11.0	21.0		11.00	0.60	18	5.5
2.20	11.0	20.0		11.00	0.60	18	5.5
2.40	12.0	21.0		12.00	0.60	20	5.0
2.60	11.0	20.0		11.00	0.47	23	4.3
2.80	7.0	14.0		7.00	0.60	12	8.6
3.00	11.0	20.0		11.00	0.47	23	4.3
3.20	14.0	21.0		14.00	0.67	21	4.8
3.40	17.0	27.0		17.00	0.93	18	5.5
3.60	16.0	30.0		16.00	0.73	22	4.6
3.80	15.0	26.0		15.00	0.73	21	4.9
4.00	11.0	22.0		11.00	0.67	16	6.1
4.20	19.0	29.0		19.00	0.80	24	4.2
4.40	19.0	31.0		19.00	1.20	16	6.3
4.60	18.0	36.0		18.00	1.40	13	7.8
4.80	16.0	37.0		16.00	1.00	16	6.3
5.00	17.0	32.0		17.00	1.20	14	7.1
5.20	18.0	36.0		18.00	1.13	16	6.3
5.40	17.0	34.0		17.00	1.20	14	7.1
5.60	17.0	35.0		17.00	1.20	14	7.1
5.80	18.0	36.0		18.00	1.13	16	6.3
6.00	25.0	42.0		25.00	1.80	14	7.2
6.20	26.0	53.0		26.00	1.80	14	6.9
6.40	22.0	49.0		22.00	1.47	15	6.7
6.60	20.0	42.0		20.00	1.47	14	7.4
6.80	22.0	44.0		22.00	1.47	15	6.7
7.00	23.0	45.0		23.00	1.53	15	6.7
7.20	21.0	44.0		21.00	1.40	15	6.7
7.40	24.0	45.0		24.00	1.47	16	6.1
7.60	16.0	38.0		16.00	1.67	10	10.4
7.80	23.0	48.0		23.00	1.53	15	6.7
8.00	19.0	42.0		19.00	0.93	20	4.9
8.20	22.0	36.0		22.00	1.33	17	6.0
8.40	21.0	41.0		21.00	1.20	18	5.7
8.60	16.0	34.0		16.00	1.13	14	7.1
8.80	23.0	40.0		23.00	1.33	17	5.8
9.00	25.0	45.0		25.00	1.67	15	6.7
9.20	21.0	46.0		21.00	1.33	16	6.3
9.40	24.0	44.0		24.00	1.40	17	5.8
9.60	24.0	45.0		24.00	1.87	13	7.8
9.80	23.0	51.0		23.00	1.80	13	7.8
10.00	23.0	50.0		23.00	1.87	12	8.1
10.20	23.0	51.0		23.00	1.47	16	6.4
10.40	23.0	45.0		23.00	1.33	17	5.8
10.60	26.0	46.0		26.00	0.80	33	3.1
10.80	38.0	50.0		38.00	1.73	22	4.6
11.00	26.0	52.0		26.00	1.93	13	7.4
11.20	24.0	53.0		24.00	1.60	15	6.7
11.40	23.0	47.0		23.00	1.40	16	6.1
11.60	25.0	46.0		25.00	1.27	20	5.1
11.80	16.0	35.0		16.00	1.07	15	6.7
12.00	9.0	25.0		9.00	0.53	17	5.9
12.20	16.0	24.0		16.00	0.27	59	1.7
12.40	19.0	23.0		19.00	0.67	28	3.5
12.60	9.0	19.0		9.00	0.60	15	6.7
12.80	9.0	18.0		9.00	0.67	13	7.4
13.00	12.0	22.0		12.00	0.73	16	6.1
13.20	16.0	27.0		16.00	1.00	16	6.3
13.40	14.0	29.0		14.00	1.00	14	7.1
13.60	11.0	26.0		11.00	0.80	14	7.3
13.80	14.0	26.0		14.00	1.00	14	7.1
14.00	15.0	30.0		15.00	1.00	15	6.7
14.20	18.0	33.0		18.00	1.20	15	6.7
14.40	16.0	34.0		16.00	1.00	16	6.3
14.60	16.0	31.0		16.00	0.93	17	5.8
14.80	15.0	29.0		15.00	0.87	17	5.8
15.00	17.0	30.0		17.00			

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %

H = profondità
L1 = prima lettura (punta)
L2 = seconda lettura (punta + laterale)
Lt = terza lettura (totale)
CT =10.00 costante di trasformazione

qc = resistenza di punta
fs = resistenza laterale calcolata alla stessa quota di qc
F = rapporto Begemann (qc / fs)
Rf = rapporto Schmertmann (fs / qc)*100

nota: FON053

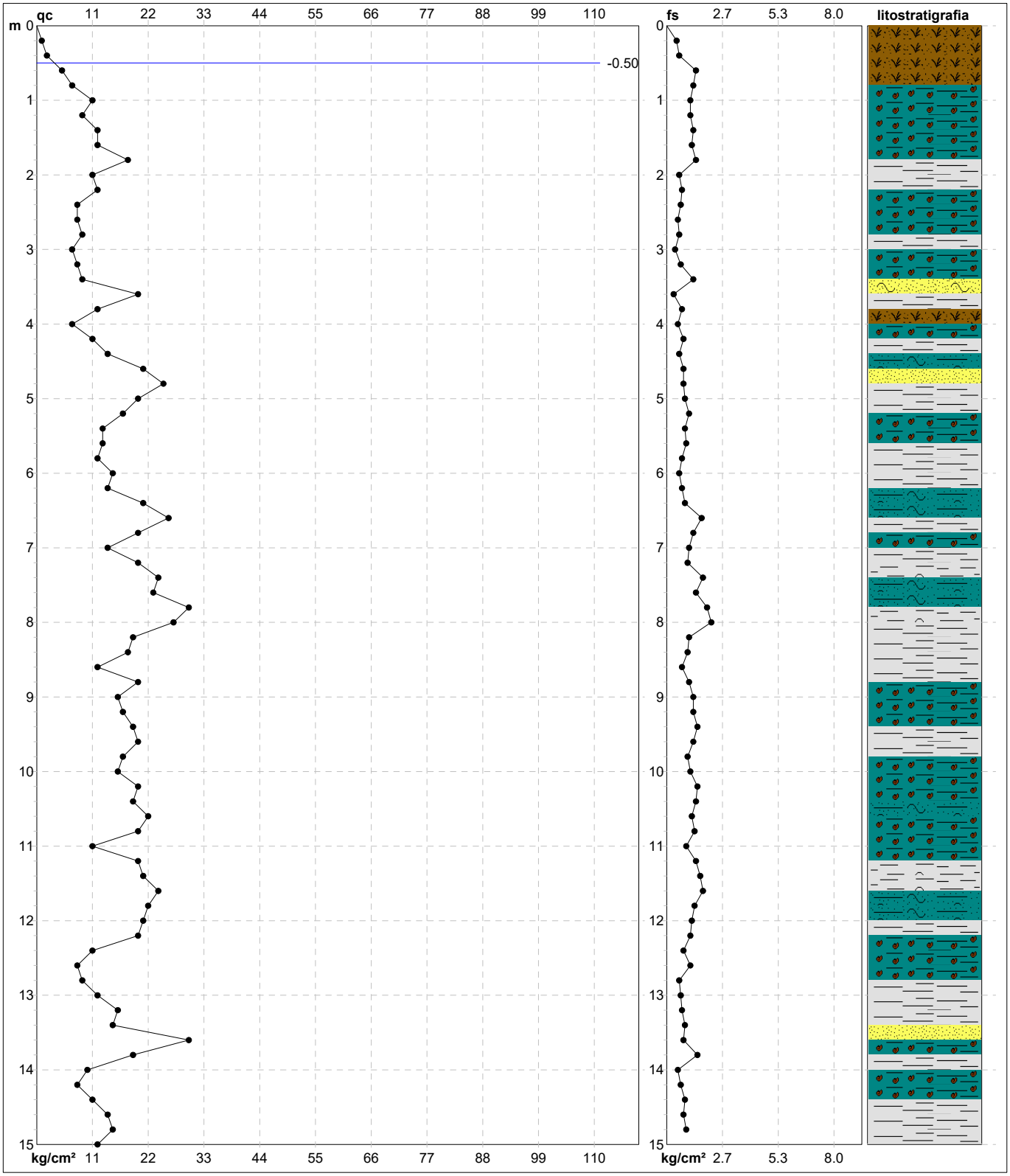
Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI DI RESISTENZA E LITOLOGIA

CPT	2
riferimento	110-2023

Committente:	**Green-go**	U.M.: **kg/cm²**	Data esec.: 01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Scala: 1:75	
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Pagina: 1	Quota inizio: Piano Campagna
		Elaborato:	Falda: -0.50 m da p.c.



		Litologia: Begemann [qc + qc/fs] 4 Zone	Preforo: m
		Penetrometro: TG63-200	Corr.astine: kg/ml
		Responsabile: Servizi Geotecnici	Cod.ISTAT: 037053
		Assistente:	Cod. punta:

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

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40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
LETTURE CAMPAGNA E VALORI TRASFORMATI

CPT	2
riferimento	110-2023

Committente:	**Green-go**	U.M.: **kg/cm²**	Data esec.: 01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Pagina: 1	
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Elaborato:	Falda: -0.50 m da p.c.

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %
0.20	4.0	8.0		1.00	0.47	2	47.0
0.40	5.0	12.0		2.00	0.60	3	30.0
0.60	8.0	17.0		5.00	1.40	4	28.0
0.80	10.0	31.0		7.00	1.27	6	18.1
1.00	14.0	33.0		11.00	1.13	10	10.3
1.20	12.0	29.0		9.00	1.13	8	12.6
1.40	15.0	32.0		12.00	1.27	9	10.6
1.60	15.0	34.0		12.00	1.20	10	10.0
1.80	21.0	39.0		18.00	1.40	13	7.8
2.00	14.0	35.0		11.00	0.60	18	5.5
2.20	15.0	24.0		12.00	0.73	16	6.1
2.40	11.0	22.0		8.00	0.67	12	8.4
2.60	11.0	21.0		8.00	0.53	15	6.6
2.80	12.0	20.0		9.00	0.60	15	6.7
3.00	10.0	19.0		7.00	0.40	18	5.7
3.20	11.0	17.0		8.00	0.67	12	8.4
3.40	12.0	22.0		9.00	1.27	7	14.1
3.60	23.0	42.0		20.00	0.33	61	1.7
3.80	15.0	20.0		12.00	0.73	16	6.1
4.00	10.0	21.0		7.00	0.53	13	7.6
4.20	14.0	22.0		11.00	0.80	14	7.3
4.40	17.0	29.0		14.00	0.60	23	4.3
4.60	24.0	33.0		21.00	0.80	26	3.8
4.80	28.0	40.0		25.00	0.80	31	3.2
5.00	23.0	35.0		20.00	0.87	23	4.4
5.20	20.0	33.0		17.00	1.07	16	6.3
5.40	16.0	32.0		13.00	0.87	15	6.7
5.60	16.0	29.0		13.00	0.93	14	7.2
5.80	15.0	29.0		12.00	0.73	16	6.1
6.00	18.0	29.0		15.00	0.60	25	4.0
6.20	17.0	26.0		14.00	0.73	19	5.2
6.40	24.0	35.0		21.00	0.87	24	4.1
6.60	29.0	42.0		26.00	1.67	16	6.4
6.80	23.0	48.0		20.00	1.27	16	6.4
7.00	17.0	36.0		14.00	1.07	13	7.6
7.20	23.0	39.0		20.00	1.00	20	5.0
7.40	27.0	42.0		24.00	1.73	14	7.2
7.60	26.0	52.0		23.00	1.40	16	6.1
7.80	33.0	54.0		30.00	1.93	16	6.4
8.00	30.0	59.0		27.00	2.13	13	7.9
8.20	22.0	54.0		19.00	1.07	18	5.6
8.40	21.0	37.0		18.00	1.00	18	5.6
8.60	15.0	30.0		12.00	0.73	16	6.1
8.80	23.0	34.0		20.00	1.07	19	5.4
9.00	19.0	35.0		16.00	1.27	13	7.9
9.20	20.0	39.0		17.00	1.27	13	7.5
9.40	22.0	41.0		19.00	1.47	13	7.7
9.60	23.0	45.0		20.00	1.27	16	6.4
9.80	20.0	39.0		17.00	1.00	17	5.9
10.00	19.0	34.0		16.00	1.13	14	7.1
10.20	23.0	40.0		20.00	1.47	14	7.4
10.40	22.0	44.0		19.00	1.40	14	7.4
10.60	25.0	46.0		22.00	1.20	18	5.5
10.80	23.0	41.0		20.00	1.33	15	6.7
11.00	14.0	34.0		11.00	0.93	12	8.5
11.20	23.0	37.0		20.00	1.40	14	7.0
11.40	24.0	45.0		21.00	1.60	13	7.6
11.60	27.0	51.0		24.00	1.73	14	7.2
11.80	25.0	51.0		22.00	1.33	17	6.0
12.00	24.0	44.0		21.00	1.20	18	5.7
12.20	23.0	41.0		20.00	1.13	18	5.7
12.40	14.0	31.0		11.00	0.80	14	7.3
12.60	11.0	23.0		8.00	1.13	7	14.1
12.80	12.0	29.0		9.00	0.60	15	6.7
13.00	15.0	24.0		12.00	0.67	18	5.6
13.20	19.0	29.0		16.00	0.73	22	4.6
13.40	18.0	29.0		15.00	0.87	17	5.8
13.60	33.0	46.0		30.00	0.80	38	2.7
13.80	22.0	34.0		19.00	1.47	13	7.7
14.00	13.0	35.0		10.00	0.53	19	5.3
14.20	11.0	19.0		8.00	0.67	12	8.4
14.40	14.0	24.0		11.00	0.87	13	7.9
14.60	17.0	30.0		14.00	0.80	18	5.7
14.80	18.0	30.0		15.00	0.93	16	6.2
15.00	15.0	29.0		12.00			

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %

H = profondità
L1 = prima lettura (punta)
L2 = seconda lettura (punta + laterale)
Lt = terza lettura (totale)
CT =10.00 costante di trasformazione

qc = resistenza di punta
fs = resistenza laterale calcolata alla stessa quota di qc
F = rapporto Begemann (qc / fs)
Rf = rapporto Schmertmann (fs / qc)*100

nota: FON053

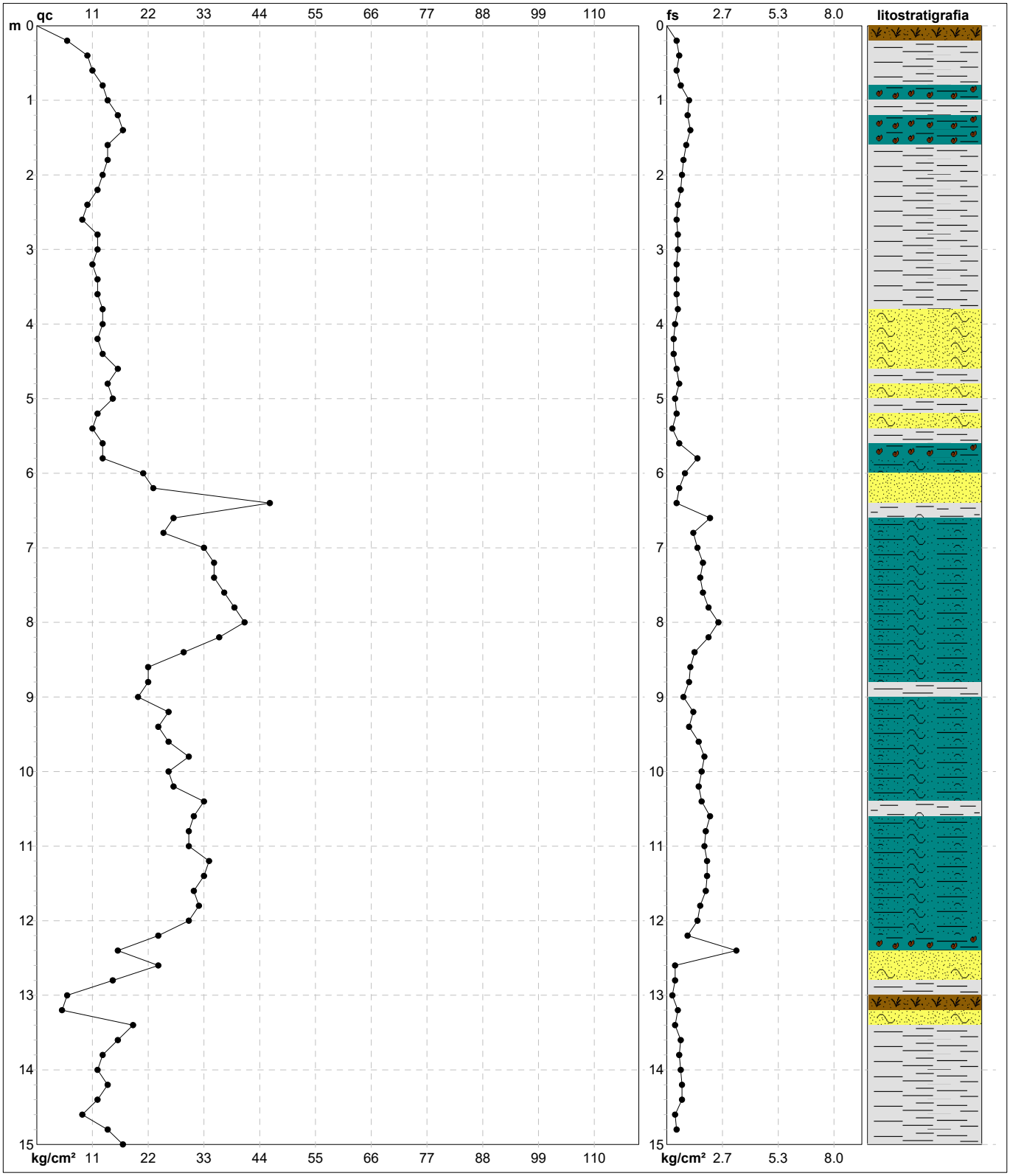
Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI DI RESISTENZA E LITOLOGIA

CPT	3
riferimento	110-2023

Committente:	**Green-go**	U.M.: **kg/cm²**	Data esec.: 01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Scala: 1:75	
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Pagina: 1	Quota inizio: Piano Campagna
		Elaborato:	Falda: Non rilevata



		Litologia:	Begemann [qc + qc/fs] 4 Zone
		Penetrometro:	TG63-200
		Responsabile:	Servizi Geotecnici
		Assistente:	

Preforo:	m
Corr.astine:	kg/ml
Cod.ISTAT:	037053
Cod. punta:	

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
LETTURE CAMPAGNA E VALORI TRASFORMATI

CPT	3
riferimento	110-2023

Committente:	**Green-go**	U.M.: **kg/cm²**	Data esec.: 01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Pagina: 1	
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Elaborato:	Falda: Non rilevata

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %
0.20	6.0	12.0		6.00	0.47	13	7.8
0.40	10.0	17.0		10.00	0.60	17	6.0
0.60	11.0	20.0		11.00	0.47	23	4.3
0.80	13.0	20.0		13.00	0.67	19	5.2
1.00	14.0	24.0		14.00	1.07	13	7.6
1.20	16.0	32.0		16.00	1.00	16	6.3
1.40	17.0	32.0		17.00	1.13	15	6.6
1.60	14.0	31.0		14.00	0.93	15	6.6
1.80	14.0	28.0		14.00	0.80	18	5.7
2.00	13.0	25.0		13.00	0.73	18	5.6
2.20	12.0	23.0		12.00	0.67	18	5.6
2.40	10.0	20.0		10.00	0.53	19	5.3
2.60	9.0	17.0		9.00	0.47	19	5.2
2.80	12.0	19.0		12.00	0.53	23	4.4
3.00	12.0	20.0		12.00	0.53	23	4.4
3.20	11.0	19.0		11.00	0.47	23	4.3
3.40	12.0	19.0		12.00	0.47	26	3.9
3.60	12.0	19.0		12.00	0.47	26	3.9
3.80	13.0	20.0		13.00	0.53	25	4.1
4.00	13.0	21.0		13.00	0.40	33	3.1
4.20	12.0	18.0		12.00	0.33	36	2.8
4.40	13.0	18.0		13.00	0.33	39	2.5
4.60	16.0	21.0		16.00	0.47	34	2.9
4.80	14.0	21.0		14.00	0.60	23	4.3
5.00	15.0	24.0		15.00	0.40	38	2.7
5.20	12.0	18.0		12.00	0.47	26	3.9
5.40	11.0	18.0		11.00	0.27	41	2.5
5.60	13.0	17.0		13.00	0.60	22	4.6
5.80	13.0	22.0		13.00	1.47	9	11.3
6.00	21.0	43.0		21.00	0.87	24	4.1
6.20	23.0	36.0		23.00	0.60	38	2.6
6.40	46.0	55.0		46.00	0.47	98	1.0
6.60	27.0	34.0		27.00	2.07	13	7.7
6.80	25.0	56.0		25.00	1.27	20	5.1
7.00	33.0	52.0		33.00	1.47	22	4.5
7.20	35.0	57.0		35.00	1.73	20	4.9
7.40	35.0	61.0		35.00	1.60	22	4.6
7.60	37.0	61.0		37.00	1.73	21	4.7
7.80	39.0	65.0		39.00	2.00	20	5.1
8.00	41.0	71.0		41.00	2.47	17	6.0
8.20	36.0	73.0		36.00	2.00	18	5.6
8.40	29.0	59.0		29.00	1.33	22	4.6
8.60	22.0	42.0		22.00	1.13	19	5.1
8.80	22.0	39.0		22.00	1.07	21	4.9
9.00	20.0	36.0		20.00	0.80	25	4.0
9.20	26.0	38.0		26.00	1.27	20	4.9
9.40	24.0	43.0		24.00	1.07	22	4.5
9.60	26.0	42.0		26.00	1.53	17	5.9
9.80	30.0	53.0		30.00	1.80	17	6.0
10.00	26.0	53.0		26.00	1.67	16	6.4
10.20	27.0	52.0		27.00	1.53	18	5.7
10.40	33.0	56.0		33.00	1.67	20	5.1
10.60	31.0	56.0		31.00	2.07	15	6.7
10.80	30.0	61.0		30.00	1.87	16	6.2
11.00	30.0	58.0		30.00	1.80	17	6.0
11.20	34.0	61.0		34.00	1.93	18	5.7
11.40	33.0	62.0		33.00	1.93	17	5.8
11.60	31.0	60.0		31.00	1.87	17	6.0
11.80	32.0	60.0		32.00	1.60	20	5.0
12.00	30.0	54.0		30.00	1.47	20	4.9
12.20	24.0	46.0		24.00	1.00	24	4.2
12.40	16.0	31.0		16.00	3.33	5	20.8
12.60	24.0	74.0		24.00	0.40	60	1.7
12.80	15.0	21.0		15.00	0.40	38	2.7
13.00	6.0	12.0		6.00	0.27	22	4.5
13.20	5.0	9.0		5.00	0.53	9	10.6
13.40	19.0	27.0		19.00	0.40	48	2.1
13.60	16.0	22.0		16.00	0.67	24	4.2
13.80	13.0	23.0		13.00	0.60	22	4.6
14.00	12.0	21.0		12.00	0.67	18	5.6
14.20	14.0	24.0		14.00	0.73	19	5.2
14.40	12.0	23.0		12.00	0.73	16	6.1
14.60	9.0	20.0		9.00	0.40	23	4.4
14.80	14.0	20.0		14.00	0.47	30	3.4
15.00	17.0	24.0		17.00			

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %

H = profondità
L1 = prima lettura (punta)
L2 = seconda lettura (punta + laterale)
Lt = terza lettura (totale)
CT =10.00 costante di trasformazione

qc = resistenza di punta
fs = resistenza laterale calcolata alla stessa quota di qc
F = rapporto Begemann (qc / fs)
Rf = rapporto Schmertmann (fs / qc)*100

nota:

FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
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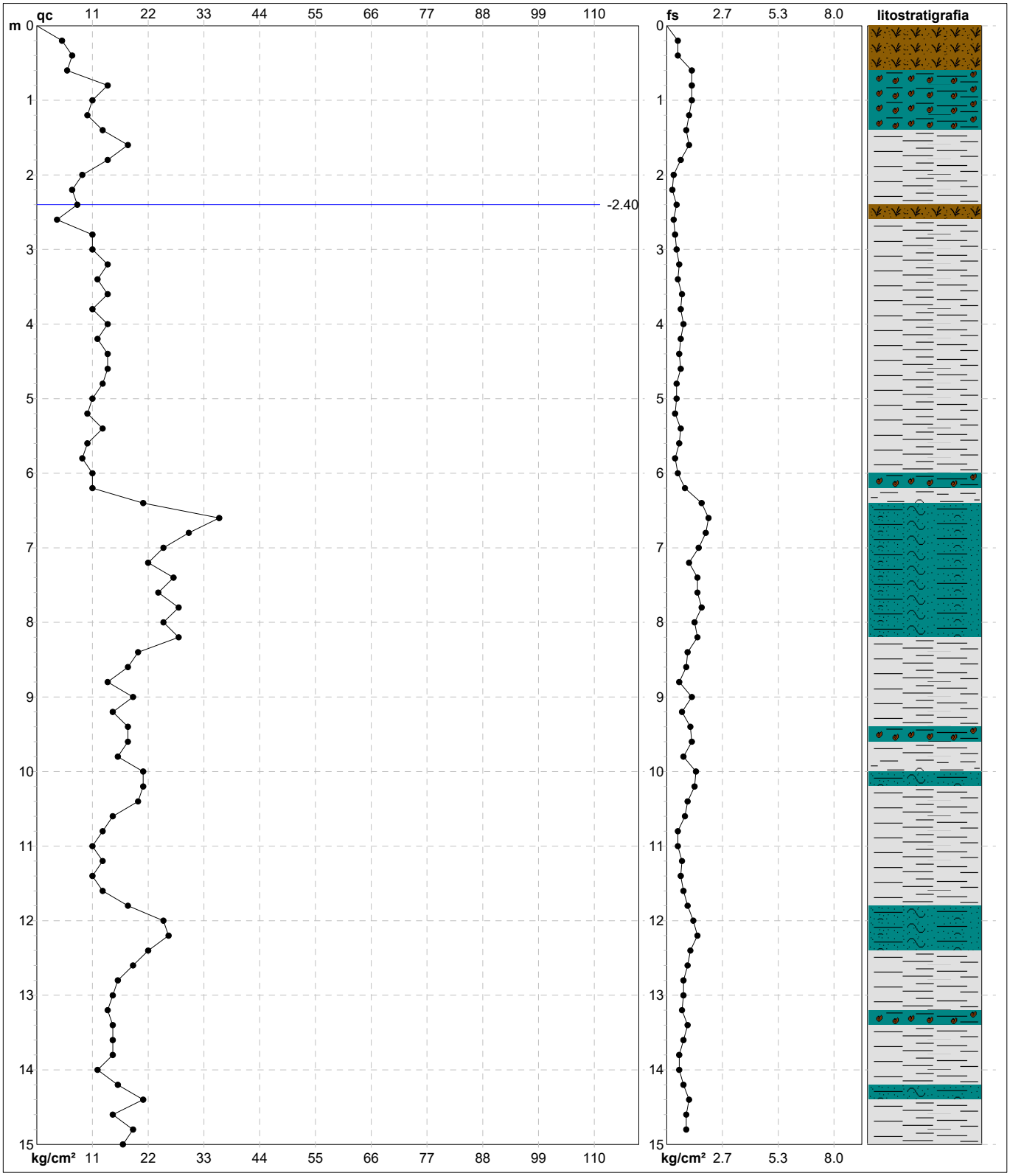
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI DI RESISTENZA E LITOLOGIA

CPT	4
riferimento	110-2023

Committente:	**Green-go**	U.M.: **kg/cm²**	Data esec.: 01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Scala: 1:75	
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Pagina: 1	Quota inizio: Piano Campagna
		Elaborato:	Falda: -2.40 m da p.c.



		Litologia:	Begemann [qc + qc/fs] 4 Zone
		Penetrometro:	TG63-200
		Responsabile:	Servizi Geotecnici
		Assistente:	

Preforo:	m
Corr.astine:	kg/ml
Cod.ISTAT:	037053
Cod. punta:	

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
LETTURE CAMPAGNA E VALORI TRASFORMATI

CPT	4
riferimento	110-2023

Committente:	**Green-go**	U.M.: **kg/cm²**	Data esec.: 01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Pagina: 1	
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Elaborato:	Falda: -2.40 m da p.c.

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %
0.20	5.0	10.0		5.00	0.53	9	10.6
0.40	7.0	15.0		7.00	0.53	13	7.6
0.60	6.0	14.0		6.00	1.20	5	20.0
0.80	14.0	32.0		14.00	1.20	12	8.6
1.00	11.0	29.0		11.00	1.20	9	10.9
1.20	10.0	28.0		10.00	1.07	9	10.7
1.40	13.0	29.0		13.00	0.93	14	7.2
1.60	18.0	32.0		18.00	1.07	17	5.9
1.80	14.0	30.0		14.00	0.67	21	4.8
2.00	9.0	19.0		9.00	0.33	27	3.7
2.20	7.0	12.0		7.00	0.27	26	3.9
2.40	8.0	12.0		8.00	0.47	17	5.9
2.60	4.0	11.0		4.00	0.33	12	8.3
2.80	11.0	16.0		11.00	0.40	28	3.6
3.00	11.0	17.0		11.00	0.47	23	4.3
3.20	14.0	21.0		14.00	0.60	23	4.3
3.40	12.0	21.0		12.00	0.53	23	4.4
3.60	14.0	22.0		14.00	0.73	19	5.2
3.80	11.0	22.0		11.00	0.67	16	6.1
4.00	14.0	24.0		14.00	0.80	18	5.7
4.20	12.0	24.0		12.00	0.67	18	5.6
4.40	14.0	24.0		14.00	0.60	23	4.3
4.60	14.0	23.0		14.00	0.67	21	4.8
4.80	13.0	23.0		13.00	0.47	28	3.6
5.00	11.0	18.0		11.00	0.47	23	4.3
5.20	10.0	17.0		10.00	0.40	25	4.0
5.40	13.0	19.0		13.00	0.67	19	5.2
5.60	10.0	20.0		10.00	0.60	17	6.0
5.80	9.0	18.0		9.00	0.40	23	4.4
6.00	11.0	17.0		11.00	0.53	21	4.8
6.20	11.0	19.0		11.00	0.87	13	7.9
6.40	21.0	34.0		21.00	1.67	13	8.0
6.60	36.0	61.0		36.00	2.00	18	5.6
6.80	30.0	60.0		30.00	1.87	16	6.2
7.00	25.0	53.0		25.00	1.53	16	6.1
7.20	22.0	45.0		22.00	1.07	21	4.9
7.40	27.0	43.0		27.00	1.47	18	5.4
7.60	24.0	46.0		24.00	1.47	16	6.1
7.80	28.0	50.0		28.00	1.67	17	6.0
8.00	25.0	50.0		25.00	1.33	19	5.3
8.20	28.0	48.0		28.00	1.47	19	5.3
8.40	20.0	42.0		20.00	1.00	20	5.0
8.60	18.0	33.0		18.00	0.93	19	5.2
8.80	14.0	28.0		14.00	0.60	23	4.3
9.00	19.0	28.0		19.00	1.20	16	6.3
9.20	15.0	33.0		15.00	0.73	21	4.9
9.40	18.0	29.0		18.00	1.13	16	6.3
9.60	18.0	35.0		18.00	1.20	15	6.7
9.80	16.0	34.0		16.00	0.80	20	5.0
10.00	21.0	33.0		21.00	1.40	15	6.7
10.20	21.0	42.0		21.00	1.33	16	6.3
10.40	20.0	40.0		20.00	1.00	20	5.0
10.60	15.0	30.0		15.00	0.87	17	5.8
10.80	13.0	26.0		13.00	0.53	25	4.1
11.00	11.0	19.0		11.00	0.53	21	4.8
11.20	13.0	21.0		13.00	0.73	18	5.6
11.40	11.0	22.0		11.00	0.67	16	6.1
11.60	13.0	23.0		13.00	0.80	16	6.2
11.80	18.0	30.0		18.00	1.00	18	5.6
12.00	25.0	40.0		25.00	1.27	20	5.1
12.20	26.0	45.0		26.00	1.47	18	5.7
12.40	22.0	44.0		22.00	1.13	19	5.1
12.60	19.0	36.0		19.00	1.00	19	5.3
12.80	16.0	31.0		16.00	0.80	20	5.0
13.00	15.0	27.0		15.00	0.80	19	5.3
13.20	14.0	26.0		14.00	0.73	19	5.2
13.40	15.0	26.0		15.00	1.00	15	6.7
13.60	15.0	30.0		15.00	0.80	19	5.3
13.80	15.0	27.0		15.00	0.60	25	4.0
14.00	12.0	21.0		12.00	0.60	20	5.0
14.20	16.0	25.0		16.00	0.80	20	5.0
14.40	21.0	33.0		21.00	1.07	20	5.1
14.60	15.0	31.0		15.00	0.93	16	6.2
14.80	19.0	33.0		19.00	0.93	20	4.9
15.00	17.0	31.0		17.00			

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %

H = profondità
L1 = prima lettura (punta)
L2 = seconda lettura (punta + laterale)
Lt = terza lettura (totale)
CT =10.00 costante di trasformazione

qc = resistenza di punta
fs = resistenza laterale calcolata alla stessa quota di qc
F = rapporto Begemann (qc / fs)
Rf = rapporto Schmertmann (fs / qc)*100

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
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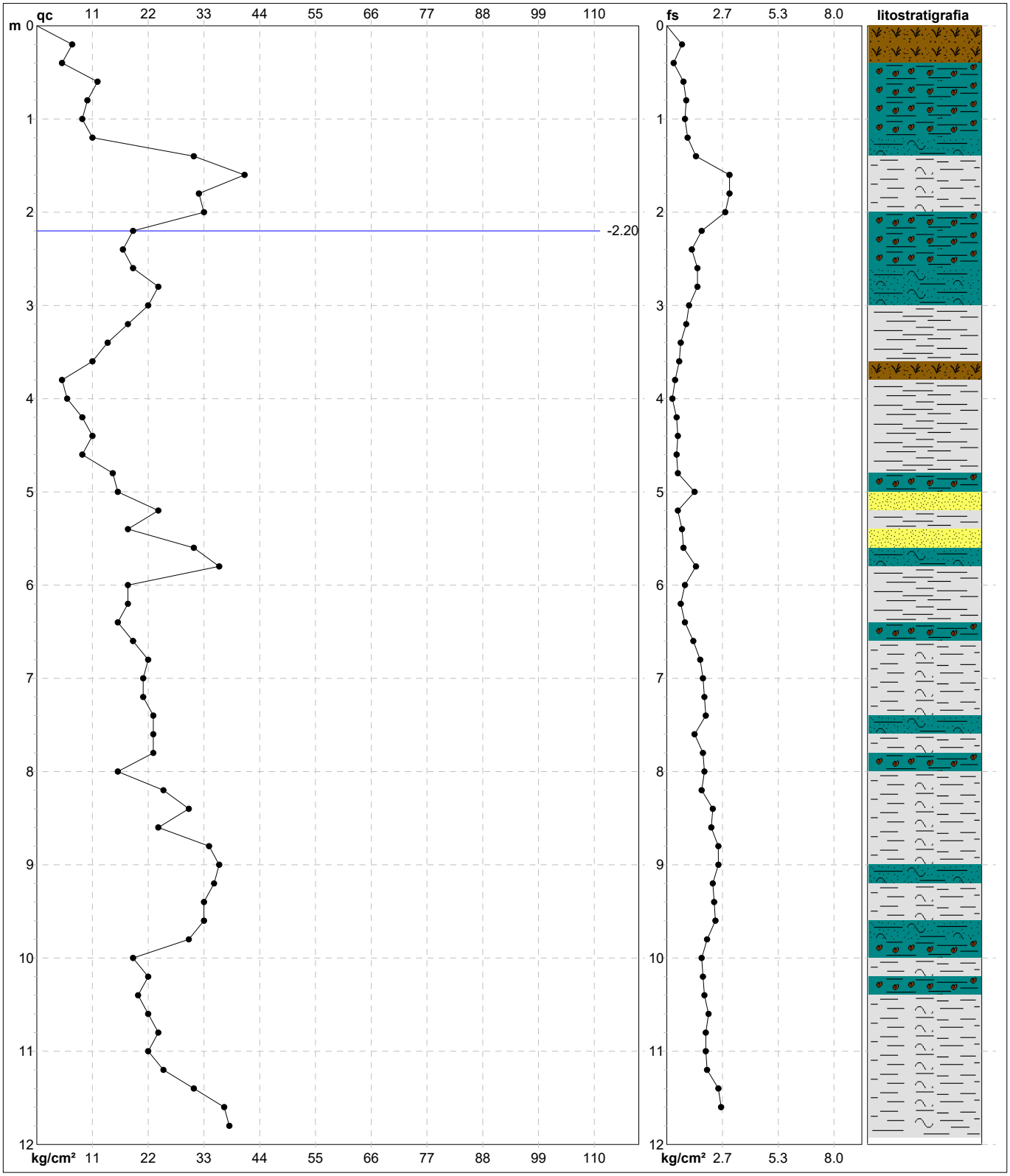
PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI DI RESISTENZA E LITOLOGIA

CPT	5
riferimento	110-2023

Committente:	**Green-go**	U.M.: **kg/cm²**	Data esec.: 01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Scala: 1:60	
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Pagina: 1	Quota inizio: Piano Campagna
		Elaborato:	Falda: -2.20 m da p.c.



		Litologia:	Begemann [qc + qc/fs] 4 Zone
		Penetrometro:	TG63-200
		Responsabile:	Servizi Geotecnici
		Assistente:	

Preforo:	m
Corr.astine:	kg/ml
Cod.ISTAT:	037053
Cod. punta:	

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
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PROVA PENETROMETRICA STATICA MECCANICA
LETTURE CAMPAGNA E VALORI TRASFORMATI

CPT	5
riferimento	110-2023

Committente:	**Green-go**	U.M.: **kg/cm²**	Data esec.: 01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Pagina: 1	
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Elaborato:	Falda: -2.20 m da p.c.

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %
0.20	7.0	13.0		7.00	0.73	10	10.4
0.40	5.0	16.0		5.00	0.33	15	6.6
0.60	12.0	17.0		12.00	0.80	15	6.7
0.80	10.0	22.0		10.00	0.93	11	9.3
1.00	9.0	23.0		9.00	0.87	10	9.7
1.20	11.0	24.0		11.00	1.00	11	9.1
1.40	31.0	46.0		31.00	1.40	22	4.5
1.60	41.0	62.0		41.00	3.00	14	7.3
1.80	32.0	77.0		32.00	3.00	11	9.4
2.00	33.0	78.0		33.00	2.80	12	8.5
2.20	19.0	61.0		19.00	1.67	11	8.8
2.40	17.0	42.0		17.00	1.20	14	7.1
2.60	19.0	37.0		19.00	1.47	13	7.7
2.80	24.0	46.0		24.00	1.47	16	6.1
3.00	22.0	44.0		22.00	1.07	21	4.9
3.20	18.0	34.0		18.00	0.93	19	5.2
3.40	14.0	28.0		14.00	0.67	21	4.8
3.60	11.0	21.0		11.00	0.60	18	5.5
3.80	5.0	14.0		5.00	0.40	13	8.0
4.00	6.0	12.0		6.00	0.27	22	4.5
4.20	9.0	13.0		9.00	0.47	19	5.2
4.40	11.0	18.0		11.00	0.53	21	4.8
4.60	9.0	17.0		9.00	0.47	19	5.2
4.80	15.0	22.0		15.00	0.53	28	3.5
5.00	16.0	24.0		16.00	1.33	12	8.3
5.20	24.0	44.0		24.00	0.53	45	2.2
5.40	18.0	26.0		18.00	0.73	25	4.1
5.60	31.0	42.0		31.00	0.80	39	2.6
5.80	36.0	48.0		36.00	1.40	26	3.9
6.00	18.0	39.0		18.00	0.87	21	4.8
6.20	18.0	31.0		18.00	0.67	27	3.7
6.40	16.0	26.0		16.00	0.87	18	5.4
6.60	19.0	32.0		19.00	1.27	15	6.7
6.80	22.0	41.0		22.00	1.60	14	7.3
7.00	21.0	45.0		21.00	1.73	12	8.2
7.20	21.0	47.0		21.00	1.80	12	8.6
7.40	23.0	50.0		23.00	1.87	12	8.1
7.60	23.0	51.0		23.00	1.33	17	5.8
7.80	23.0	43.0		23.00	1.73	13	7.5
8.00	16.0	42.0		16.00	1.80	9	11.3
8.20	25.0	52.0		25.00	1.67	15	6.7
8.40	30.0	55.0		30.00	2.20	14	7.3
8.60	24.0	57.0		24.00	2.13	11	8.9
8.80	34.0	66.0		34.00	2.47	14	7.3
9.00	36.0	73.0		36.00	2.47	15	6.9
9.20	35.0	72.0		35.00	2.20	16	6.3
9.40	33.0	66.0		33.00	2.27	15	6.9
9.60	33.0	67.0		33.00	2.33	14	7.1
9.80	30.0	65.0		30.00	1.93	16	6.4
10.00	19.0	48.0		19.00	1.67	11	8.8
10.20	22.0	47.0		22.00	1.73	13	7.9
10.40	20.0	46.0		20.00	1.80	11	9.0
10.60	22.0	49.0		22.00	2.00	11	9.1
10.80	24.0	54.0		24.00	1.87	13	7.8
11.00	22.0	50.0		22.00	1.87	12	8.5
11.20	25.0	53.0		25.00	1.93	13	7.7
11.40	31.0	60.0		31.00	2.47	13	8.0
11.60	37.0	74.0		37.00	2.60	14	7.0
11.80	38.0	77.0		38.00			

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %

H = profondità
L1 = prima lettura (punta)
L2 = seconda lettura (punta + laterale)
Lt = terza lettura (totale)
CT =10.00 costante di trasformazione

qc = resistenza di punta
fs = resistenza laterale calcolata alla stessa quota di qc
F = rapporto Begemann (qc / fs)
Rf = rapporto Schmertmann (fs / qc)*100

nota:

FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
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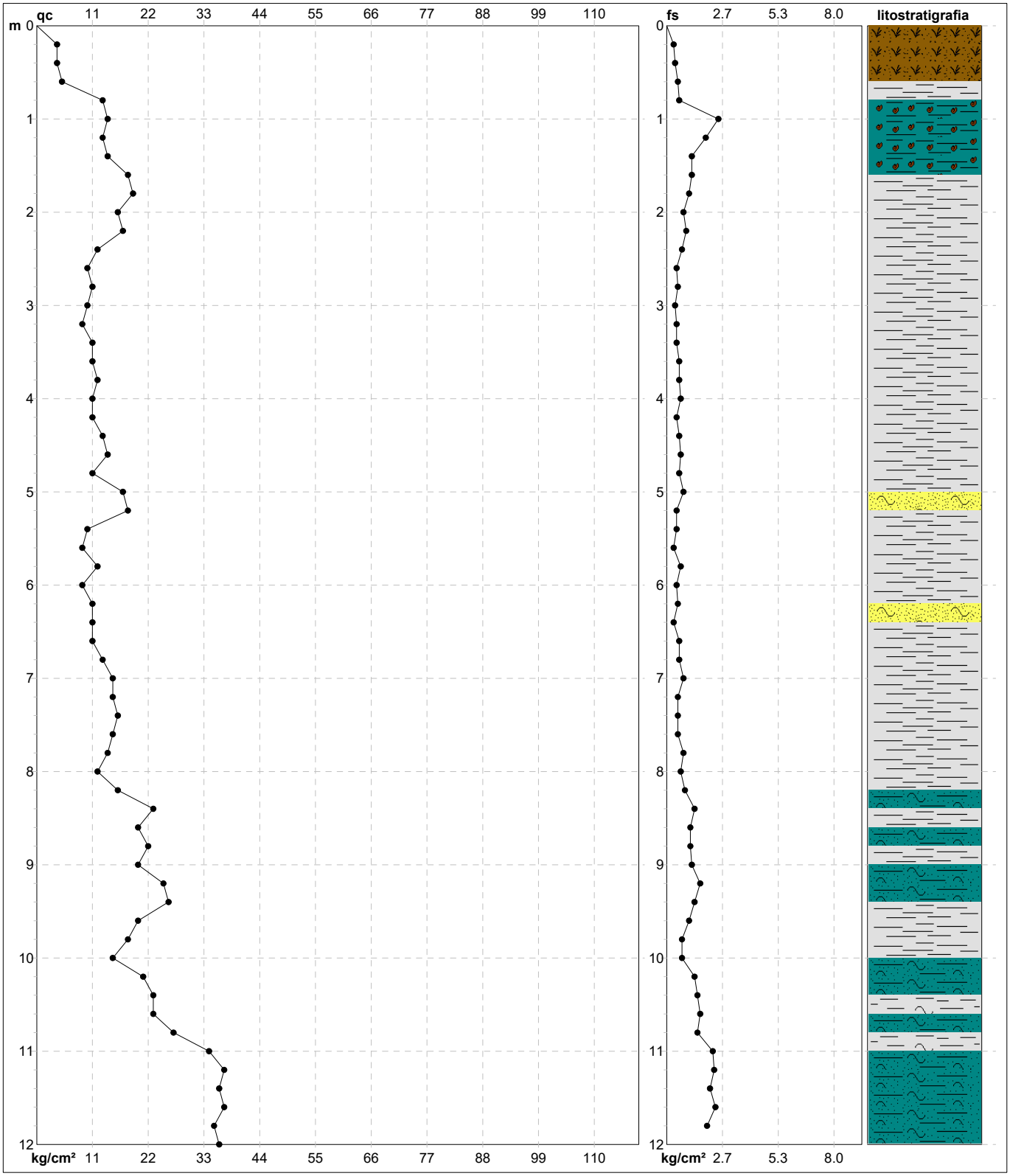
PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI DI RESISTENZA E LITOLOGIA

CPT	6
riferimento	110-2023

Committente:	**Green-go**	U.M.: **kg/cm²**	Data esec.: 01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Scala: 1:60	
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Pagina: 1	Quota inizio: Piano Campagna
		Elaborato:	Falda: Non rilevata



		Litologia:	Begemann [qc + qc/fs] 4 Zone
		Penetrometro:	TG63-200
		Responsabile:	Servizi Geotecnici
		Assistente:	

Preforo:	m
Corr.astine:	kg/ml
Cod.ISTAT:	037053
Cod. punta:	

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
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40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
LETTURE CAMPAGNA E VALORI TRASFORMATI

CPT	6
riferimento	110-2023

Committente:	**Green-go**	U.M.: **kg/cm²**	Data esec.: 01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Pagina: 1	
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Elaborato:	Falda: Non rilevata

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %
0.20	4.0	8.0		4.00	0.33	12	8.3
0.40	4.0	9.0		4.00	0.40	10	10.0
0.60	5.0	11.0		5.00	0.53	9	10.6
0.80	13.0	21.0		13.00	0.60	22	4.6
1.00	14.0	23.0		14.00	2.47	6	17.6
1.20	13.0	50.0		13.00	1.87	7	14.4
1.40	14.0	42.0		14.00	1.20	12	8.6
1.60	18.0	36.0		18.00	1.20	15	6.7
1.80	19.0	37.0		19.00	1.07	18	5.6
2.00	16.0	32.0		16.00	0.80	20	5.0
2.20	17.0	29.0		17.00	0.93	18	5.5
2.40	12.0	26.0		12.00	0.73	16	6.1
2.60	10.0	21.0		10.00	0.47	21	4.7
2.80	11.0	18.0		11.00	0.53	21	4.8
3.00	10.0	18.0		10.00	0.40	25	4.0
3.20	9.0	15.0		9.00	0.47	19	5.2
3.40	11.0	18.0		11.00	0.47	23	4.3
3.60	11.0	18.0		11.00	0.60	18	5.5
3.80	12.0	21.0		12.00	0.60	20	5.0
4.00	11.0	20.0		11.00	0.67	16	6.1
4.20	11.0	21.0		11.00	0.47	23	4.3
4.40	13.0	20.0		13.00	0.60	22	4.6
4.60	14.0	23.0		14.00	0.67	21	4.8
4.80	11.0	21.0		11.00	0.60	18	5.5
5.00	17.0	26.0		17.00	0.80	21	4.7
5.20	18.0	30.0		18.00	0.47	38	2.6
5.40	10.0	17.0		10.00	0.47	21	4.7
5.60	9.0	16.0		9.00	0.33	27	3.7
5.80	12.0	17.0		12.00	0.67	18	5.6
6.00	9.0	19.0		9.00	0.47	19	5.2
6.20	11.0	18.0		11.00	0.53	21	4.8
6.40	11.0	19.0		11.00	0.33	33	3.0
6.60	11.0	16.0		11.00	0.60	18	5.5
6.80	13.0	22.0		13.00	0.60	22	4.6
7.00	15.0	24.0		15.00	0.80	19	5.3
7.20	15.0	27.0		15.00	0.53	28	3.5
7.40	16.0	24.0		16.00	0.53	30	3.3
7.60	15.0	23.0		15.00	0.53	28	3.5
7.80	14.0	22.0		14.00	0.80	18	5.7
8.00	12.0	24.0		12.00	0.67	18	5.6
8.20	16.0	26.0		16.00	0.87	18	5.4
8.40	23.0	36.0		23.00	1.33	17	5.8
8.60	20.0	40.0		20.00	1.13	18	5.7
8.80	22.0	39.0		22.00	1.13	19	5.1
9.00	20.0	37.0		20.00	1.20	17	6.0
9.20	25.0	43.0		25.00	1.60	16	6.4
9.40	26.0	50.0		26.00	1.33	20	5.1
9.60	20.0	40.0		20.00	1.07	19	5.4
9.80	18.0	34.0		18.00	0.73	25	4.1
10.00	15.0	26.0		15.00	0.73	21	4.9
10.20	21.0	32.0		21.00	1.33	16	6.3
10.40	23.0	43.0		23.00	1.47	16	6.4
10.60	23.0	45.0		23.00	1.60	14	7.0
10.80	27.0	51.0		27.00	1.47	18	5.4
11.00	34.0	56.0		34.00	2.20	15	6.5
11.20	37.0	70.0		37.00	2.27	16	6.1
11.40	36.0	70.0		36.00	2.07	17	5.8
11.60	37.0	68.0		37.00	2.33	16	6.3
11.80	35.0	70.0		35.00	1.93	18	5.5
12.00	36.0	65.0		36.00			

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %

H = profondità
L1 = prima lettura (punta)
L2 = seconda lettura (punta + laterale)
Lt = terza lettura (totale)
CT =10.00 costante di trasformazione

qc = resistenza di punta
fs = resistenza laterale calcolata alla stessa quota di qc
F = rapporto Begemann (qc / fs)
Rf = rapporto Schmertmann (fs / qc)*100

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

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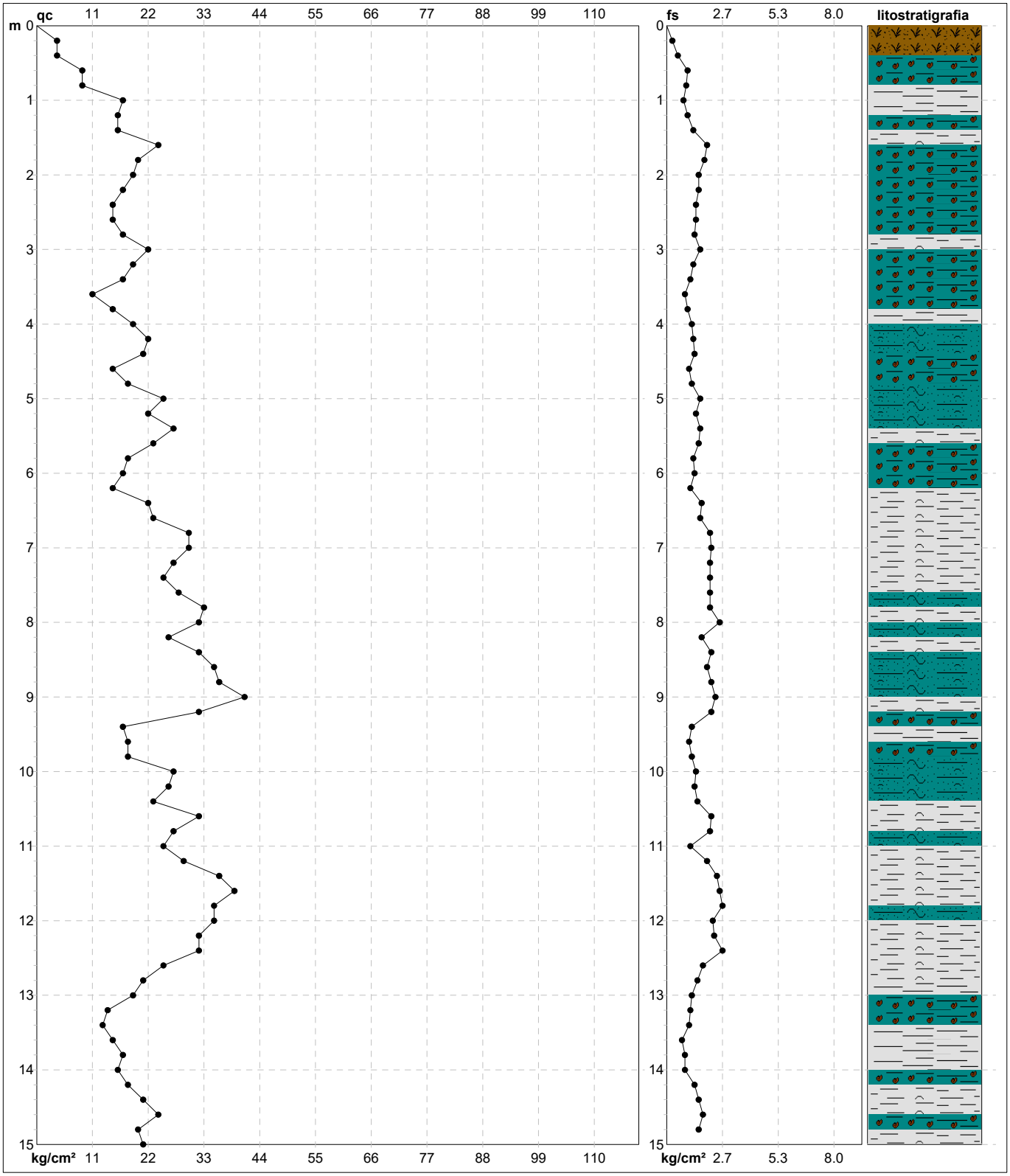
PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI DI RESISTENZA E LITOLOGIA

CPT	7
riferimento	110-2023

Committente:	**Green-go**	U.M.: **kg/cm²**	Data esec.: 01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Scala: 1:75	
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Pagina: 1	Quota inizio: Piano Campagna
		Elaborato:	Falda: Non rilevata



Litologia:	Begemann [qc + qc/fs] 4 Zone	Preforo:	m
Penetrometro:	TG63-200	Corr.astine:	kg/ml
Responsabile:	Servizi Geotecnici	Cod.ISTAT:	037053
Assistente:		Cod. punta:	

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
LETTURE CAMPAGNA E VALORI TRASFORMATI

CPT	7
riferimento	110-2023

Committente:	**Green-go**	U.M.: **kg/cm²**	Data esec.: 01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Pagina: 1	
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Elaborato:	Falda: Non rilevata

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %
0.20	4.0	6.0		4.00	0.27	15	6.8
0.40	4.0	8.0		4.00	0.53	8	13.3
0.60	9.0	17.0		9.00	1.00	9	11.1
0.80	9.0	24.0		9.00	0.93	10	10.3
1.00	17.0	31.0		17.00	0.80	21	4.7
1.20	16.0	28.0		16.00	1.00	16	6.3
1.40	16.0	31.0		16.00	1.27	13	7.9
1.60	24.0	43.0		24.00	1.93	12	8.0
1.80	20.0	49.0		20.00	1.80	11	9.0
2.00	19.0	46.0		19.00	1.53	12	8.1
2.20	17.0	40.0		17.00	1.53	11	9.0
2.40	15.0	38.0		15.00	1.40	11	9.3
2.60	15.0	36.0		15.00	1.40	11	9.3
2.80	17.0	38.0		17.00	1.33	13	7.8
3.00	22.0	42.0		22.00	1.60	14	7.3
3.20	19.0	43.0		19.00	1.27	15	6.7
3.40	17.0	36.0		17.00	1.13	15	6.6
3.60	11.0	28.0		11.00	0.87	13	7.9
3.80	15.0	28.0		15.00	1.00	15	6.7
4.00	19.0	34.0		19.00	1.20	16	6.3
4.20	22.0	40.0		22.00	1.27	17	5.8
4.40	21.0	40.0		21.00	1.33	16	6.3
4.60	15.0	35.0		15.00	1.07	14	7.1
4.80	18.0	34.0		18.00	1.20	15	6.7
5.00	25.0	43.0		25.00	1.60	16	6.4
5.20	22.0	46.0		22.00	1.40	16	6.4
5.40	27.0	48.0		27.00	1.60	17	5.9
5.60	23.0	47.0		23.00	1.53	15	6.7
5.80	18.0	41.0		18.00	1.27	14	7.1
6.00	17.0	36.0		17.00	1.33	13	7.8
6.20	15.0	35.0		15.00	1.13	13	7.5
6.40	22.0	39.0		22.00	1.67	13	7.6
6.60	23.0	48.0		23.00	1.60	14	7.0
6.80	30.0	54.0		30.00	2.07	14	6.9
7.00	30.0	61.0		30.00	2.13	14	7.1
7.20	27.0	59.0		27.00	2.07	13	7.7
7.40	25.0	56.0		25.00	2.07	12	8.3
7.60	28.0	59.0		28.00	2.07	14	7.4
7.80	33.0	64.0		33.00	2.07	16	6.3
8.00	32.0	63.0		32.00	2.53	13	7.9
8.20	26.0	64.0		26.00	1.67	16	6.4
8.40	32.0	57.0		32.00	2.13	15	6.7
8.60	35.0	67.0		35.00	1.93	18	5.5
8.80	36.0	65.0		36.00	2.13	17	5.9
9.00	41.0	73.0		41.00	2.33	18	5.7
9.20	32.0	67.0		32.00	2.13	15	6.7
9.40	17.0	49.0		17.00	1.20	14	7.1
9.60	18.0	36.0		18.00	1.07	17	5.9
9.80	18.0	34.0		18.00	1.20	15	6.7
10.00	27.0	45.0		27.00	1.40	19	5.2
10.20	26.0	47.0		26.00	1.33	20	5.1
10.40	23.0	43.0		23.00	1.47	16	6.4
10.60	32.0	54.0		32.00	2.13	15	6.7
10.80	27.0	59.0		27.00	2.07	13	7.7
11.00	25.0	56.0		25.00	1.13	22	4.5
11.20	29.0	46.0		29.00	1.93	15	6.7
11.40	36.0	65.0		36.00	2.40	15	6.7
11.60	39.0	75.0		39.00	2.53	15	6.5
11.80	35.0	73.0		35.00	2.67	13	7.6
12.00	35.0	75.0		35.00	2.20	16	6.3
12.20	32.0	65.0		32.00	2.27	14	7.1
12.40	32.0	66.0		32.00	2.67	12	8.3
12.60	25.0	65.0		25.00	1.73	14	6.9
12.80	21.0	47.0		21.00	1.47	14	7.0
13.00	19.0	41.0		19.00	1.20	16	6.3
13.20	14.0	32.0		14.00	1.13	12	8.1
13.40	13.0	30.0		13.00	1.07	12	8.2
13.60	15.0	31.0		15.00	0.73	21	4.9
13.80	17.0	28.0		17.00	0.87	20	5.1
14.00	16.0	29.0		16.00	0.87	18	5.4
14.20	18.0	31.0		18.00	1.33	14	7.4
14.40	21.0	41.0		21.00	1.53	14	7.3
14.60	24.0	47.0		24.00	1.73	14	7.2
14.80	20.0	46.0		20.00	1.53	13	7.7
15.00	21.0	44.0		21.00			

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %

H = profondità
L1 = prima lettura (punta)
L2 = seconda lettura (punta + laterale)
Lt = terza lettura (totale)
CT =10.00 costante di trasformazione

qc = resistenza di punta
fs = resistenza laterale calcolata alla stessa quota di qc
F = rapporto Begemann (qc / fs)
Rf = rapporto Schmertmann (fs / qc)*100

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
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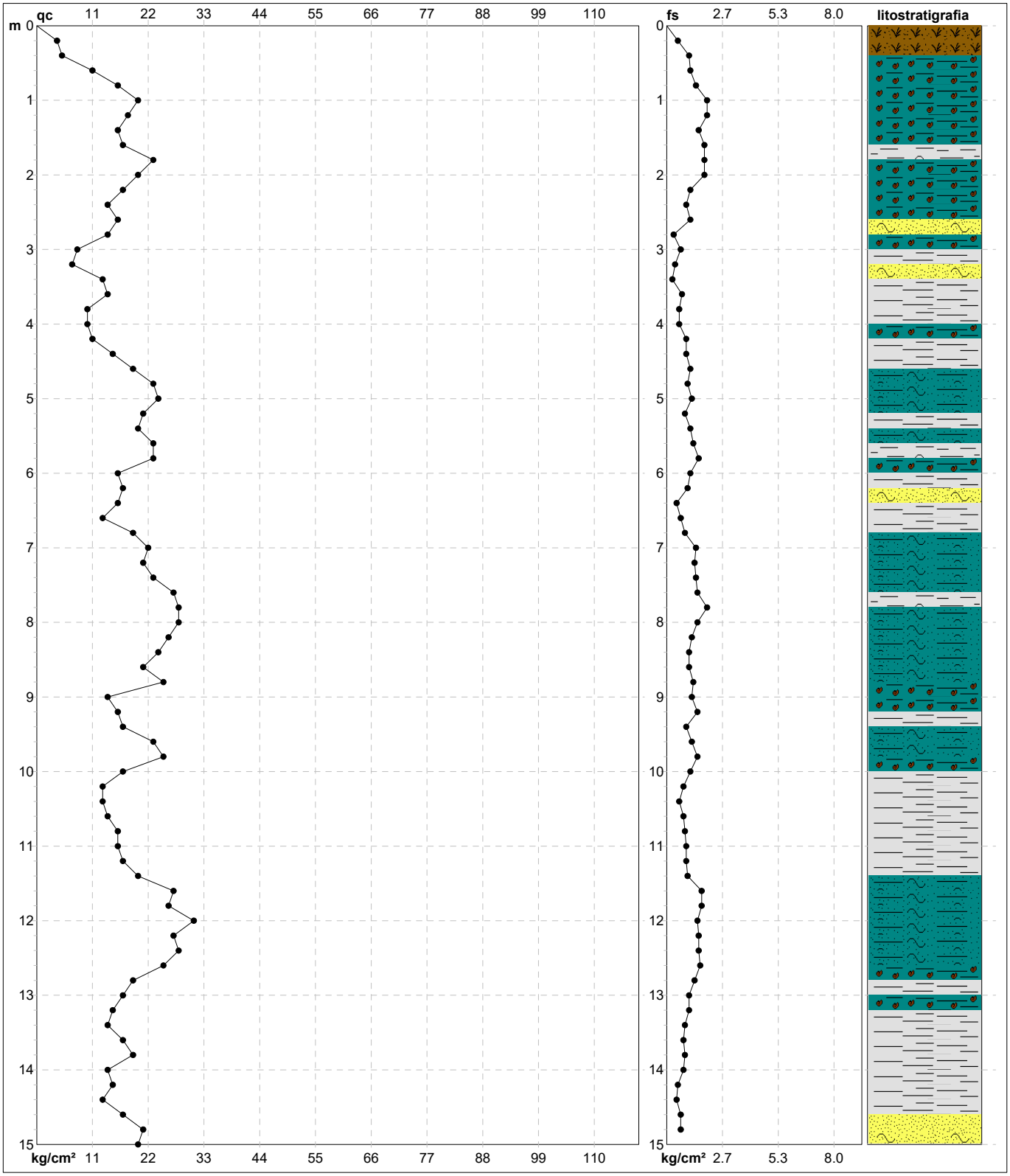
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI DI RESISTENZA E LITOLOGIA

CPT	8
riferimento	110-2023

Committente:	**Green-go**	U.M.: **kg/cm²**	Data esec.: 01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Scala: 1:75	
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Pagina: 1	Quota inizio: Piano Campagna
		Elaborato:	Falda: Non rilevata



Litologia:	Begemann [qc + qc/fs] 4 Zone	Preforo:	m
Penetrometro:	TG63-200	Corr.astine:	kg/ml
Responsabile:	Servizi Geotecnici	Cod.ISTAT:	037053
Assistente:		Cod. punta:	

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
LETTURE CAMPAGNA E VALORI TRASFORMATI

CPT	8
riferimento	110-2023

Committente:	**Green-go**	U.M.: **kg/cm²**	Data esec.: 01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Pagina: 1	
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Elaborato:	Falda: Non rilevata

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %
0.20	4.0	8.0		4.00	0.53	8	13.3
0.40	5.0	13.0		5.00	1.07	5	21.4
0.60	11.0	27.0		11.00	1.13	10	10.3
0.80	16.0	33.0		16.00	1.40	11	8.8
1.00	20.0	41.0		20.00	1.93	10	9.7
1.20	18.0	47.0		18.00	1.93	9	10.7
1.40	16.0	45.0		16.00	1.53	10	9.6
1.60	17.0	40.0		17.00	1.80	9	10.6
1.80	23.0	50.0		23.00	1.80	13	7.8
2.00	20.0	47.0		20.00	1.80	11	9.0
2.20	17.0	44.0		17.00	1.13	15	6.6
2.40	14.0	31.0		14.00	0.93	15	6.6
2.60	16.0	30.0		16.00	1.13	14	7.1
2.80	14.0	31.0		14.00	0.33	42	2.4
3.00	8.0	13.0		8.00	0.67	12	8.4
3.20	7.0	17.0		7.00	0.40	18	5.7
3.40	13.0	19.0		13.00	0.27	48	2.1
3.60	14.0	18.0		14.00	0.73	19	5.2
3.80	10.0	21.0		10.00	0.60	17	6.0
4.00	10.0	19.0		10.00	0.60	17	6.0
4.20	11.0	20.0		11.00	0.93	12	8.5
4.40	15.0	29.0		15.00	0.93	16	6.2
4.60	19.0	33.0		19.00	1.13	17	5.9
4.80	23.0	40.0		23.00	1.00	23	4.3
5.00	24.0	39.0		24.00	1.20	20	5.0
5.20	21.0	39.0		21.00	0.87	24	4.1
5.40	20.0	33.0		20.00	1.13	18	5.7
5.60	23.0	40.0		23.00	1.27	18	5.5
5.80	23.0	42.0		23.00	1.53	15	6.7
6.00	16.0	39.0		16.00	1.13	14	7.1
6.20	17.0	34.0		17.00	1.00	17	5.9
6.40	16.0	31.0		16.00	0.47	34	2.9
6.60	13.0	20.0		13.00	0.67	19	5.2
6.80	19.0	29.0		19.00	0.87	22	4.6
7.00	22.0	35.0		22.00	1.40	16	6.4
7.20	21.0	42.0		21.00	1.33	16	6.3
7.40	23.0	43.0		23.00	1.40	16	6.1
7.60	27.0	48.0		27.00	1.47	18	5.4
7.80	28.0	50.0		28.00	1.93	15	6.9
8.00	28.0	57.0		28.00	1.47	19	5.3
8.20	26.0	48.0		26.00	1.20	22	4.6
8.40	24.0	42.0		24.00	1.07	22	4.5
8.60	21.0	37.0		21.00	1.07	20	5.1
8.80	25.0	41.0		25.00	1.27	20	5.1
9.00	14.0	33.0		14.00	1.20	12	8.6
9.20	16.0	34.0		16.00	1.47	11	9.2
9.40	17.0	39.0		17.00	0.93	18	5.5
9.60	23.0	37.0		23.00	1.20	19	5.2
9.80	25.0	43.0		25.00	1.47	17	5.9
10.00	17.0	39.0		17.00	1.13	15	6.6
10.20	13.0	30.0		13.00	0.80	16	6.2
10.40	13.0	25.0		13.00	0.60	22	4.6
10.60	14.0	23.0		14.00	0.80	18	5.7
10.80	16.0	28.0		16.00	0.87	18	5.4
11.00	16.0	29.0		16.00	0.93	17	5.8
11.20	17.0	31.0		17.00	0.93	18	5.5
11.40	20.0	34.0		20.00	1.00	20	5.0
11.60	27.0	42.0		27.00	1.67	16	6.2
11.80	26.0	51.0		26.00	1.67	16	6.4
12.00	31.0	56.0		31.00	1.47	21	4.7
12.20	27.0	49.0		27.00	1.53	18	5.7
12.40	28.0	51.0		28.00	1.53	18	5.5
12.60	25.0	48.0		25.00	1.60	16	6.4
12.80	19.0	43.0		19.00	1.33	14	7.0
13.00	17.0	37.0		17.00	1.07	16	6.3
13.20	15.0	31.0		15.00	1.07	14	7.1
13.40	14.0	30.0		14.00	0.87	16	6.2
13.60	17.0	30.0		17.00	0.80	21	4.7
13.80	19.0	31.0		19.00	0.87	22	4.6
14.00	14.0	27.0		14.00	0.80	18	5.7
14.20	15.0	27.0		15.00	0.53	28	3.5
14.40	13.0	21.0		13.00	0.47	28	3.6
14.60	17.0	24.0		17.00	0.67	25	3.9
14.80	21.0	31.0		21.00	0.67	31	3.2
15.00	20.0	30.0		20.00			

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %

H = profondità
L1 = prima lettura (punta)
L2 = seconda lettura (punta + laterale)
Lt = terza lettura (totale)
CT =10.00 costante di trasformazione

qc = resistenza di punta
fs = resistenza laterale calcolata alla stessa quota di qc
F = rapporto Begemann (qc / fs)
Rf = rapporto Schmertmann (fs / qc)*100

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
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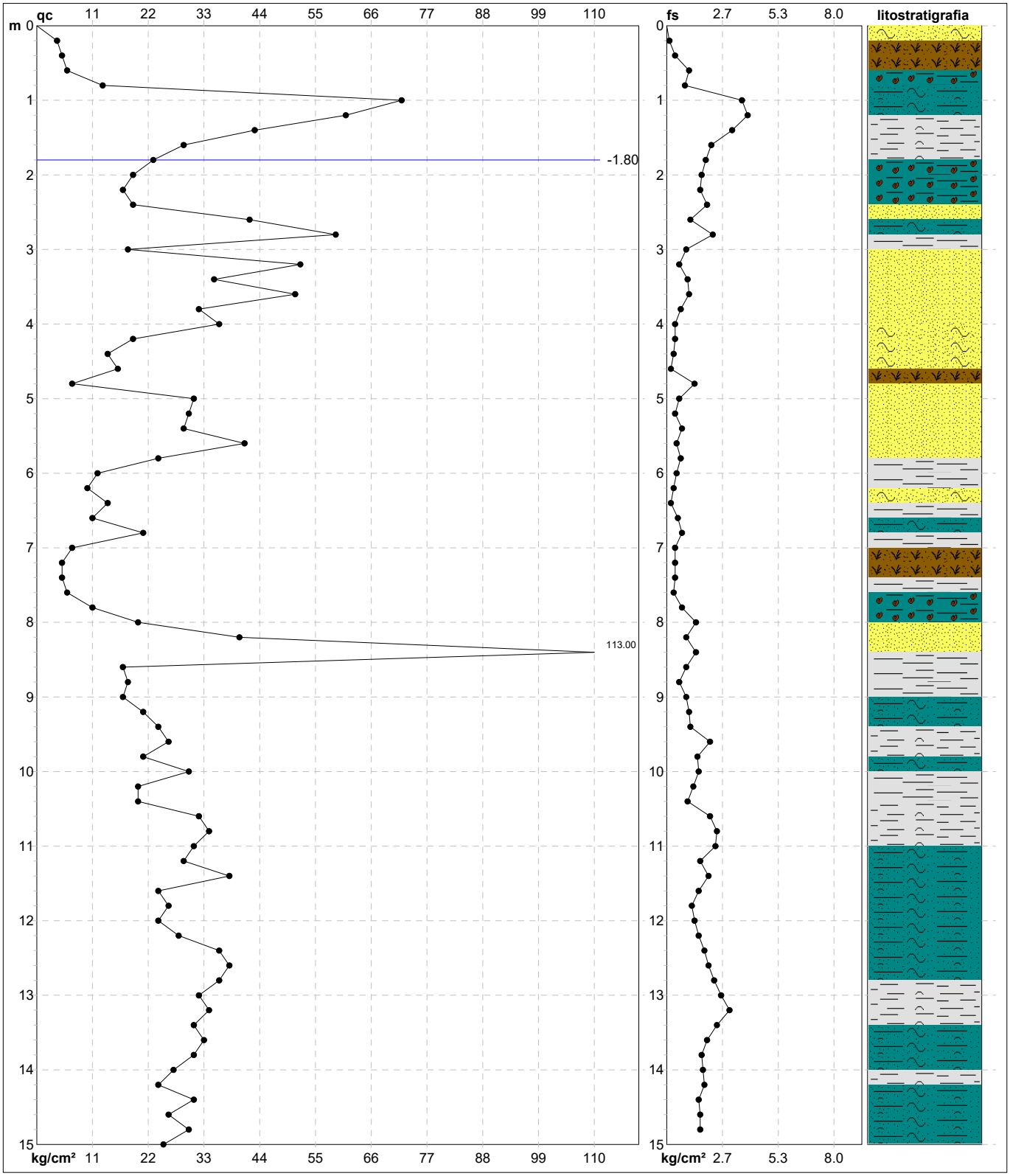
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI DI RESISTENZA E LITOLOGIA

CPT	9
riferimento	110-2023

Committente:	**Green-go**	U.M.: **kg/cm²**	Data esec.: 01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Scala: 1:75	
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Pagina: 1	Quota inizio: Piano Campagna
		Elaborato:	Falda: -1.80 m da p.c.



		Litologia: Begemann [qc + qc/fs] 4 Zone	Preforo: m
		Penetrometro: TG63-200	Corr.astine: kg/ml
		Responsabile: Servizi Geotecnici	Cod.ISTAT: 037053
		Assistente:	Cod. punta:

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
LETTURE CAMPAGNA E VALORI TRASFORMATI

CPT	9
riferimento	110-2023

Committente:	**Green-go**	U.M.: **kg/cm²**	Data esec.: 01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Pagina: 1	
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Elaborato:	Falda: -1.80 m da p.c.

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %
0.20	4.0	8.0		4.00	0.13	31	3.3
0.40	5.0	7.0		5.00	0.40	13	8.0
0.60	6.0	12.0		6.00	1.07	6	17.8
0.80	13.0	29.0		13.00	0.87	15	6.7
1.00	72.0	85.0		72.00	3.60	20	5.0
1.20	61.0	115.0		61.00	3.87	16	6.3
1.40	43.0	101.0		43.00	3.13	14	7.3
1.60	29.0	76.0		29.00	2.13	14	7.3
1.80	23.0	55.0		23.00	1.87	12	8.1
2.00	19.0	47.0		19.00	1.67	11	8.8
2.20	17.0	42.0		17.00	1.60	11	9.4
2.40	19.0	43.0		19.00	1.93	10	10.2
2.60	42.0	71.0		42.00	1.13	37	2.7
2.80	59.0	76.0		59.00	2.20	27	3.7
3.00	18.0	51.0		18.00	0.93	19	5.2
3.20	52.0	66.0		52.00	0.60	87	1.2
3.40	35.0	44.0		35.00	1.00	35	2.9
3.60	51.0	66.0		51.00	1.07	48	2.1
3.80	32.0	48.0		32.00	0.67	48	2.1
4.00	36.0	46.0		36.00	0.40	90	1.1
4.20	19.0	25.0		19.00	0.40	48	2.1
4.40	14.0	20.0		14.00	0.33	42	2.4
4.60	16.0	21.0		16.00	0.20	80	1.3
4.80	7.0	10.0		7.00	1.33	5	19.0
5.00	31.0	51.0		31.00	0.60	52	1.9
5.20	30.0	39.0		30.00	0.40	75	1.3
5.40	29.0	35.0		29.00	0.73	40	2.5
5.60	41.0	52.0		41.00	0.47	87	1.1
5.80	24.0	31.0		24.00	0.67	36	2.8
6.00	12.0	22.0		12.00	0.47	26	3.9
6.20	10.0	17.0		10.00	0.33	30	3.3
6.40	14.0	19.0		14.00	0.20	70	1.4
6.60	11.0	14.0		11.00	0.53	21	4.8
6.80	21.0	29.0		21.00	0.73	29	3.5
7.00	7.0	18.0		7.00	0.40	18	5.7
7.20	5.0	11.0		5.00	0.40	13	8.0
7.40	5.0	11.0		5.00	0.40	13	8.0
7.60	6.0	12.0		6.00	0.33	18	5.5
7.80	11.0	16.0		11.00	0.73	15	6.6
8.00	20.0	31.0		20.00	1.40	14	7.0
8.20	40.0	61.0		40.00	0.93	43	2.3
8.40	113.0	127.0		113.00	1.40	81	1.2
8.60	17.0	38.0		17.00	0.93	18	5.5
8.80	18.0	32.0		18.00	0.60	30	3.3
9.00	17.0	26.0		17.00	0.93	18	5.5
9.20	21.0	35.0		21.00	1.07	20	5.1
9.40	24.0	40.0		24.00	1.13	21	4.7
9.60	26.0	43.0		26.00	2.07	13	8.0
9.80	21.0	52.0		21.00	1.47	14	7.0
10.00	30.0	52.0		30.00	1.53	20	5.1
10.20	20.0	43.0		20.00	1.27	16	6.4
10.40	20.0	39.0		20.00	1.00	20	5.0
10.60	32.0	47.0		32.00	2.07	15	6.5
10.80	34.0	65.0		34.00	2.40	14	7.1
11.00	31.0	67.0		31.00	2.33	13	7.5
11.20	29.0	64.0		29.00	1.60	18	5.5
11.40	38.0	62.0		38.00	2.00	19	5.3
11.60	24.0	54.0		24.00	1.53	16	6.4
11.80	26.0	49.0		26.00	1.20	22	4.6
12.00	24.0	42.0		24.00	1.33	18	5.5
12.20	28.0	48.0		28.00	1.53	18	5.5
12.40	36.0	59.0		36.00	1.80	20	5.0
12.60	38.0	65.0		38.00	2.00	19	5.3
12.80	36.0	66.0		36.00	2.27	16	6.3
13.00	32.0	66.0		32.00	2.60	12	8.1
13.20	34.0	73.0		34.00	3.00	11	8.8
13.40	31.0	76.0		31.00	2.40	13	7.7
13.60	33.0	69.0		33.00	1.93	17	5.8
13.80	31.0	60.0		31.00	1.67	19	5.4
14.00	27.0	52.0		27.00	1.73	16	6.4
14.20	24.0	50.0		24.00	1.80	13	7.5
14.40	31.0	58.0		31.00	1.53	20	4.9
14.60	26.0	49.0		26.00	1.60	16	6.2
14.80	30.0	54.0		30.00	1.60	19	5.3
15.00	25.0	49.0		25.00			

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %

H = profondità
L1 = prima lettura (punta)
L2 = seconda lettura (punta + laterale)
Lt = terza lettura (totale)
CT =10.00 costante di trasformazione

qc = resistenza di punta
fs = resistenza laterale calcolata alla stessa quota di qc
F = rapporto Begemann (qc / fs)
Rf = rapporto Schmertmann (fs / qc)*100

nota:

FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
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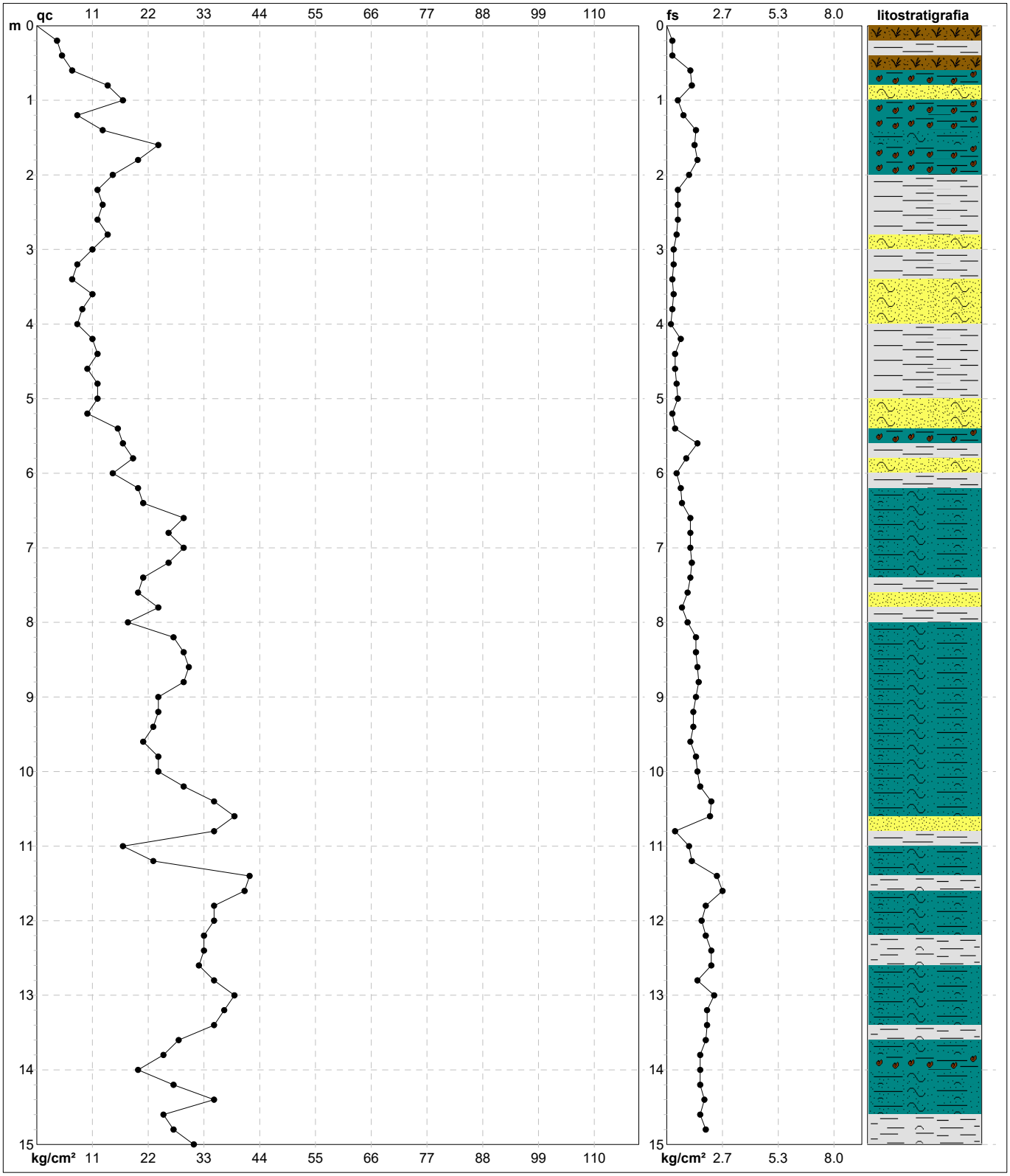
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI DI RESISTENZA E LITOLOGIA

CPT	10
riferimento	110-2023

Committente:	**Green-go**	U.M.: **kg/cm²**	Data esec.: 01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Scala: 1:75	
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Pagina: 1	Quota inizio: Piano Campagna
		Elaborato:	Falda: Non rilevata



		Litologia:	Begemann [qc + qc/fs] 4 Zone
		Penetrometro:	TG63-200
		Responsabile:	Servizi Geotecnici
		Assistente:	

Preforo:	m
Corr.astine:	kg/ml
Cod.ISTAT:	037053
Cod. punta:	

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
LETTURE CAMPAGNA E VALORI TRASFORMATI

CPT	10
riferimento	110-2023

Committente:	**Green-go**	U.M.: **kg/cm²**	Data esec.: 01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Pagina: 1	
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Elaborato:	Falda: Non rilevata

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %
0.20	4.0	8.0		4.00	0.27	15	6.8
0.40	5.0	9.0		5.00	0.27	19	5.4
0.60	7.0	11.0		7.00	1.13	6	16.1
0.80	14.0	31.0		14.00	1.20	12	8.6
1.00	17.0	35.0		17.00	0.53	32	3.1
1.20	8.0	16.0		8.00	0.80	10	10.0
1.40	13.0	25.0		13.00	1.40	9	10.8
1.60	24.0	45.0		24.00	1.33	18	5.5
1.80	20.0	40.0		20.00	1.47	14	7.4
2.00	15.0	37.0		15.00	1.07	14	7.1
2.20	12.0	28.0		12.00	0.53	23	4.4
2.40	13.0	21.0		13.00	0.53	25	4.1
2.60	12.0	20.0		12.00	0.53	23	4.4
2.80	14.0	22.0		14.00	0.47	30	3.4
3.00	11.0	18.0		11.00	0.33	33	3.0
3.20	8.0	13.0		8.00	0.33	24	4.1
3.40	7.0	12.0		7.00	0.27	26	3.9
3.60	11.0	15.0		11.00	0.33	33	3.0
3.80	9.0	14.0		9.00	0.27	33	3.0
4.00	8.0	12.0		8.00	0.20	40	2.5
4.20	11.0	14.0		11.00	0.67	16	6.1
4.40	12.0	22.0		12.00	0.40	30	3.3
4.60	10.0	16.0		10.00	0.40	25	4.0
4.80	12.0	18.0		12.00	0.47	26	3.9
5.00	12.0	19.0		12.00	0.53	23	4.4
5.20	10.0	18.0		10.00	0.27	37	2.7
5.40	16.0	20.0		16.00	0.40	40	2.5
5.60	17.0	23.0		17.00	1.47	12	8.6
5.80	19.0	41.0		19.00	0.93	20	4.9
6.00	15.0	29.0		15.00	0.47	32	3.1
6.20	20.0	27.0		20.00	0.67	30	3.4
6.40	21.0	31.0		21.00	0.73	29	3.5
6.60	29.0	40.0		29.00	1.13	26	3.9
6.80	26.0	43.0		26.00	1.13	23	4.3
7.00	29.0	46.0		29.00	1.13	26	3.9
7.20	26.0	43.0		26.00	1.20	22	4.6
7.40	21.0	39.0		21.00	1.13	19	5.4
7.60	20.0	37.0		20.00	1.00	20	5.0
7.80	24.0	39.0		24.00	0.73	33	3.0
8.00	18.0	29.0		18.00	1.00	18	5.6
8.20	27.0	42.0		27.00	1.40	19	5.2
8.40	29.0	50.0		29.00	1.40	21	4.8
8.60	30.0	51.0		30.00	1.47	20	4.9
8.80	29.0	51.0		29.00	1.53	19	5.3
9.00	24.0	47.0		24.00	1.40	17	5.8
9.20	24.0	45.0		24.00	1.27	19	5.3
9.40	23.0	42.0		23.00	1.27	18	5.5
9.60	21.0	40.0		21.00	1.13	19	5.4
9.80	24.0	41.0		24.00	1.40	17	5.8
10.00	24.0	45.0		24.00	1.47	16	6.1
10.20	29.0	51.0		29.00	1.60	18	5.5
10.40	35.0	59.0		35.00	2.13	16	6.1
10.60	39.0	71.0		39.00	2.07	19	5.3
10.80	35.0	66.0		35.00	0.40	88	1.1
11.00	17.0	23.0		17.00	1.07	16	6.3
11.20	23.0	39.0		23.00	1.20	19	5.2
11.40	42.0	60.0		42.00	2.40	18	5.7
11.60	41.0	77.0		41.00	2.67	15	6.5
11.80	35.0	75.0		35.00	1.87	19	5.3
12.00	35.0	63.0		35.00	1.67	21	4.8
12.20	33.0	58.0		33.00	1.87	18	5.7
12.40	33.0	61.0		33.00	2.13	15	6.5
12.60	32.0	64.0		32.00	2.13	15	6.7
12.80	35.0	67.0		35.00	1.47	24	4.2
13.00	39.0	61.0		39.00	2.27	17	5.8
13.20	37.0	71.0		37.00	1.93	19	5.2
13.40	35.0	64.0		35.00	1.93	18	5.5
13.60	28.0	57.0		28.00	1.87	15	6.7
13.80	25.0	53.0		25.00	1.60	16	6.4
14.00	20.0	44.0		20.00	1.60	13	8.0
14.20	27.0	51.0		27.00	1.60	17	5.9
14.40	35.0	59.0		35.00	1.80	19	5.1
14.60	25.0	52.0		25.00	1.60	16	6.4
14.80	27.0	51.0		27.00	1.87	14	6.9
15.00	31.0	59.0		31.00			

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %

H = profondità
L1 = prima lettura (punta)
L2 = seconda lettura (punta + laterale)
Lt = terza lettura (totale)
CT =10.00 costante di trasformazione

qc = resistenza di punta
fs = resistenza laterale calcolata alla stessa quota di qc
F = rapporto Begemann (qc / fs)
Rf = rapporto Schmertmann (fs / qc)*100

nota:

FON053

Software by dott. Geol. Diego Merlin 0425-840820

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LEGENDA VALUTAZIONI LITOLOGICHE CORRELAZIONI GENERALI

Valutazioni in base al rapporto: F = (qc / fs)
Begemann 1965 - Raccomandazioni A.G.I. 1977
Valide in via approssimata per terreni immersi in falda :

	F = qc / fs	NATURA LITOLOGICA	PROPRIETA'
	F ≤ 15 kg/cm²	TORBE ED ARGILLE ORGANICHE	COESIVE
15 kg/cm² <	F ≤ 30 kg/cm²	LIMI ED ARGILLE	COESIVE
30 kg/cm² <	F ≤ 60 kg/cm²	LIMI SABBIOSI E SABBIE LIMOSE	GRANULARI
	F > 60 kg/cm²	SABBIE E SABBIE CON GHIAIA	GRANULARI

Vengono inoltre riportate le valutazioni stratigrafiche fornite da Schmertmann (1978), ricavabili in base ai valori di qc e di FR = (fs / qc) % :

- AO = argilla organica e terreni misti
- Att = argilla (inorganica) molto tenera
- At = argilla (inorganica) tenera
- Am = argilla (inorganica) di media consistenza
- Ac = argilla (inorganica) consistente
- Acc = argilla (inorganica) molto consistente
- ASL = argilla sabbiosa e limosa
- SAL = sabbia e limo / sabbia e limo argilloso
- Ss = sabbia sciolta
- Sm = sabbia mediamente addensata
- Sd = sabbia densa o cementata
- SC = sabbia con molti fossili, calcareniti

Secondo Schmertmann il valore della resistenza laterale da usarsi, dovrebbe essere pari a:

- 1/3 ± - 1/2 di quello misurato , per depositi sabbiosi
- quello misurato (inalterato) , per depositi coesivi.

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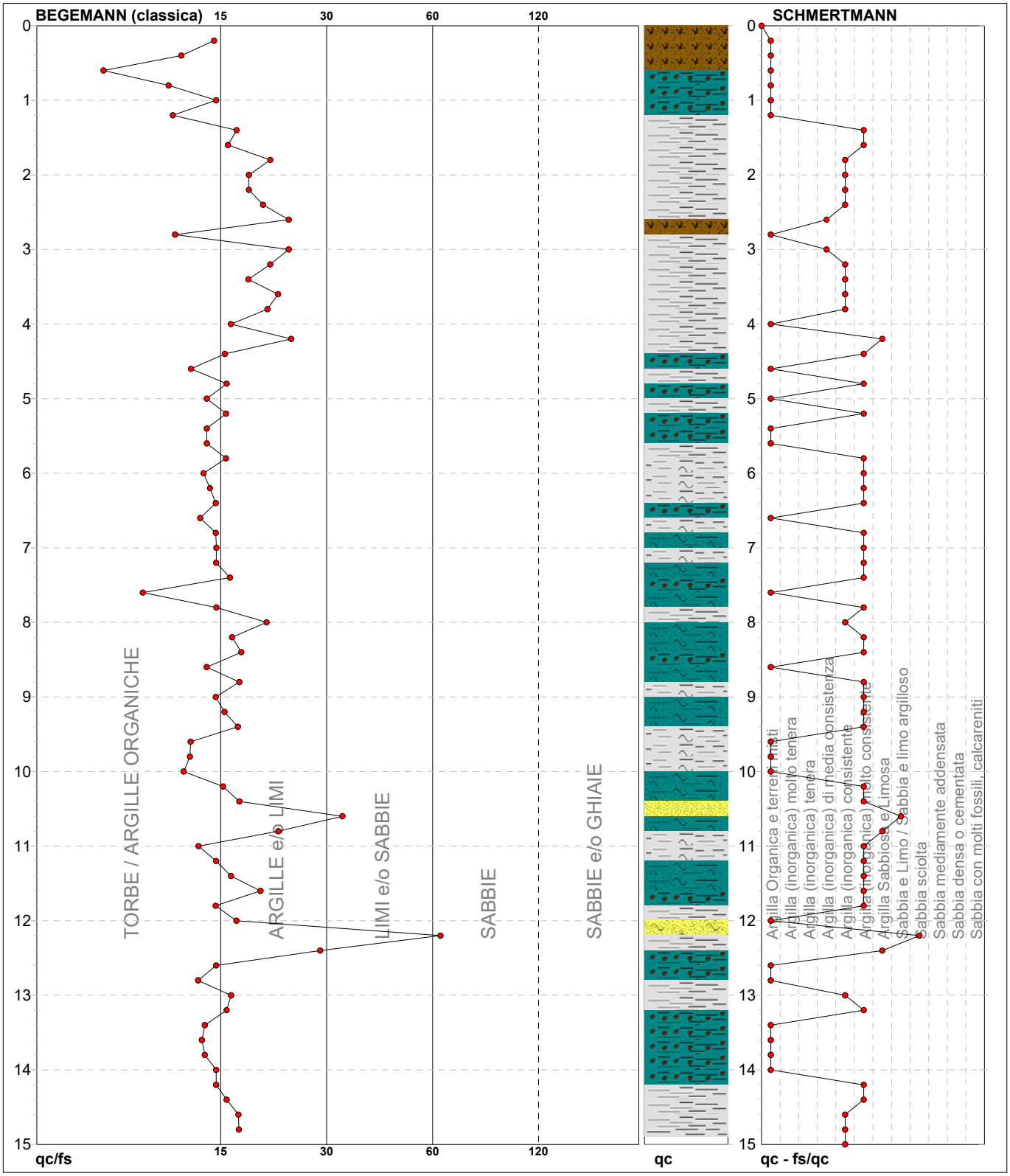
PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI LITOLOGIA

CPT	1
riferimento	110-2023

Committente:	**Green-go**	U.M.:	**kg/cm²**	Data esec.:	01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Scala:	1:75		
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Pagina:	1		
		Elaborato:		Falda: -0.60 m	Non rilevata



Torbe / Argille org. :	33 punti,	44.59%	Argilla Organica e terreni misti:	25 punti,	33.78%	Argilla Sabbiosa e Limosa:	3 punti, 4.05%
Argille e/o Limi :	39 punti,	52.70%	Argilla (inorganica) media consist.:	2 punti,	2.70%	Sabbia e Limo / Sabbia e limo arg.:	1 punti, 1.35%
Limi e/o Sabbie :	2 punti,	2.70%	Argilla (inorganica) consistente:	12 punti,	16.22%	Sabbia sciolta:	1 punti, 1.35%
			Argilla (inorganica) molto consist.:	30 punti,	40.54%		

nota: FON053

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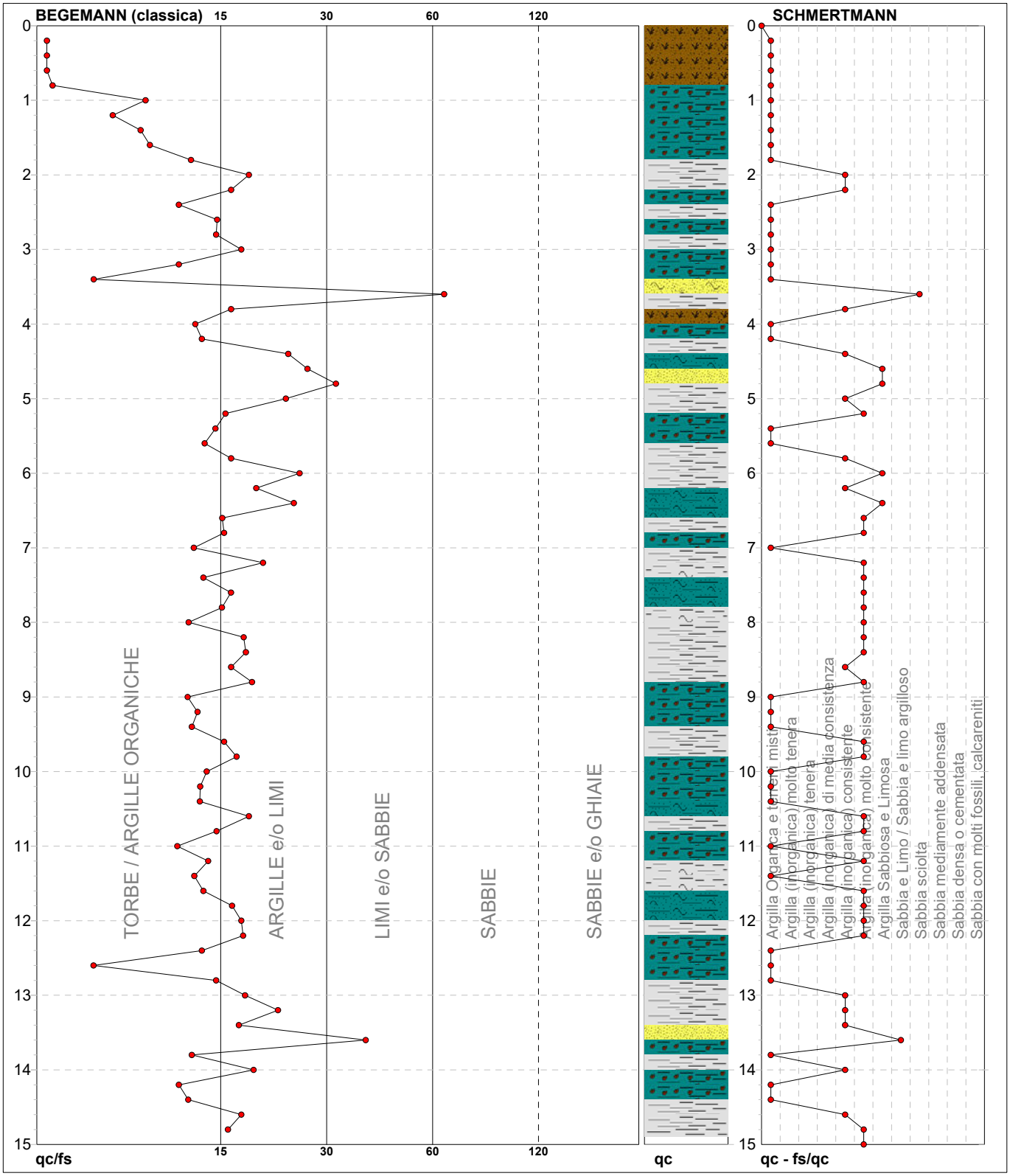
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI LITOLOGIA

CPT	2
riferimento	110-2023

Committente:	**Green-go**	U.M.: **kg/cm²**	Data esec.: 01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Scala: 1:75	
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Pagina: 1	
		Elaborato:	Falda: -0.50 m da p.c.



Torbe / Argille org. :	36 punti, 48.65%	Argilla Organica e terreni misti:	34 punti, 45.95%	Argilla Sabbiosa e Limosa:	4 punti, 5.41%
Argille e/o Limi :	35 punti, 47.30%	Argilla (inorganica) consistente:	13 punti, 17.57%	Sabbia e Limo / Sabbia e limo arg.:	1 punti, 1.35%
Limi e/o Sabbie :	2 punti, 2.70%	Argilla (inorganica) molto consist.:	21 punti, 28.38%	Sabbia sciolta:	1 punti, 1.35%
Sabbie:	1 punti, 1.35%				

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
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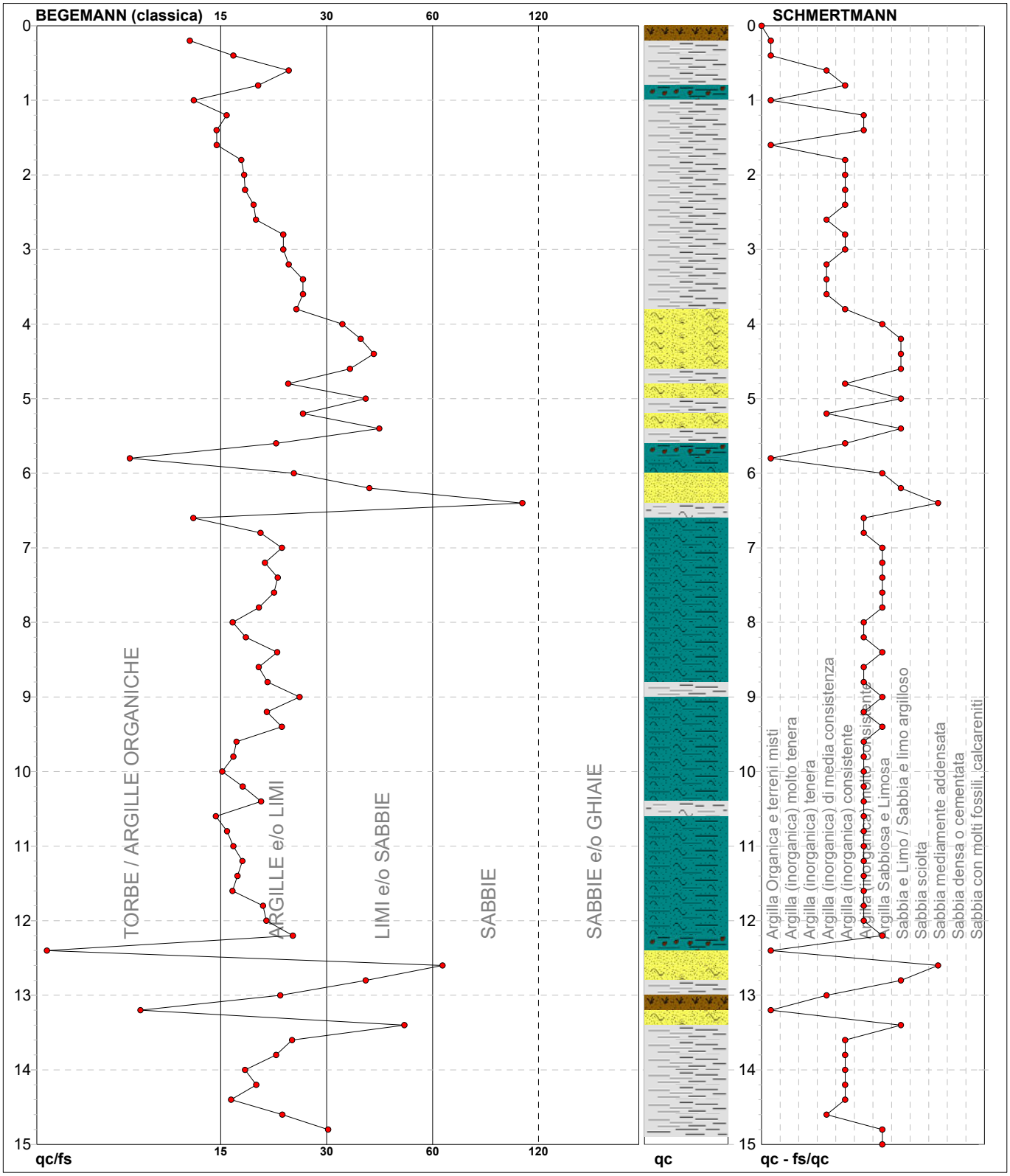
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI LITOLOGIA

CPT	3
riferimento	110-2023

Committente:	**Green-go**	U.M.:	**kg/cm²**	Data esec.:	01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Scala:	1:75		
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Pagina:	1		
		Elaborato:		Falda:	Non rilevata



Torbe / Argille org. :	7 punti,	9.46%	Argilla Organica e terreni misti:	7 punti,	9.46%	Argilla Sabbiosa e Limosa:	12 punti, 16.22%
Argille e/o Limi :	56 punti,	75.68%	Argilla (inorganica) media consist.:	8 punti,	10.81%	Sabbia e Limo / Sabbia e limo arg.:	8 punti, 10.81%
Limi e/o Sabbie :	10 punti,	13.51%	Argilla (inorganica) consistente:	15 punti,	20.27%	Sabbia mediamente addensata:	2 punti, 2.70%
Sabbie:	1 punti,	1.35%	Argilla (inorganica) molto consist.:	22 punti,	29.73%		

nota: FON053

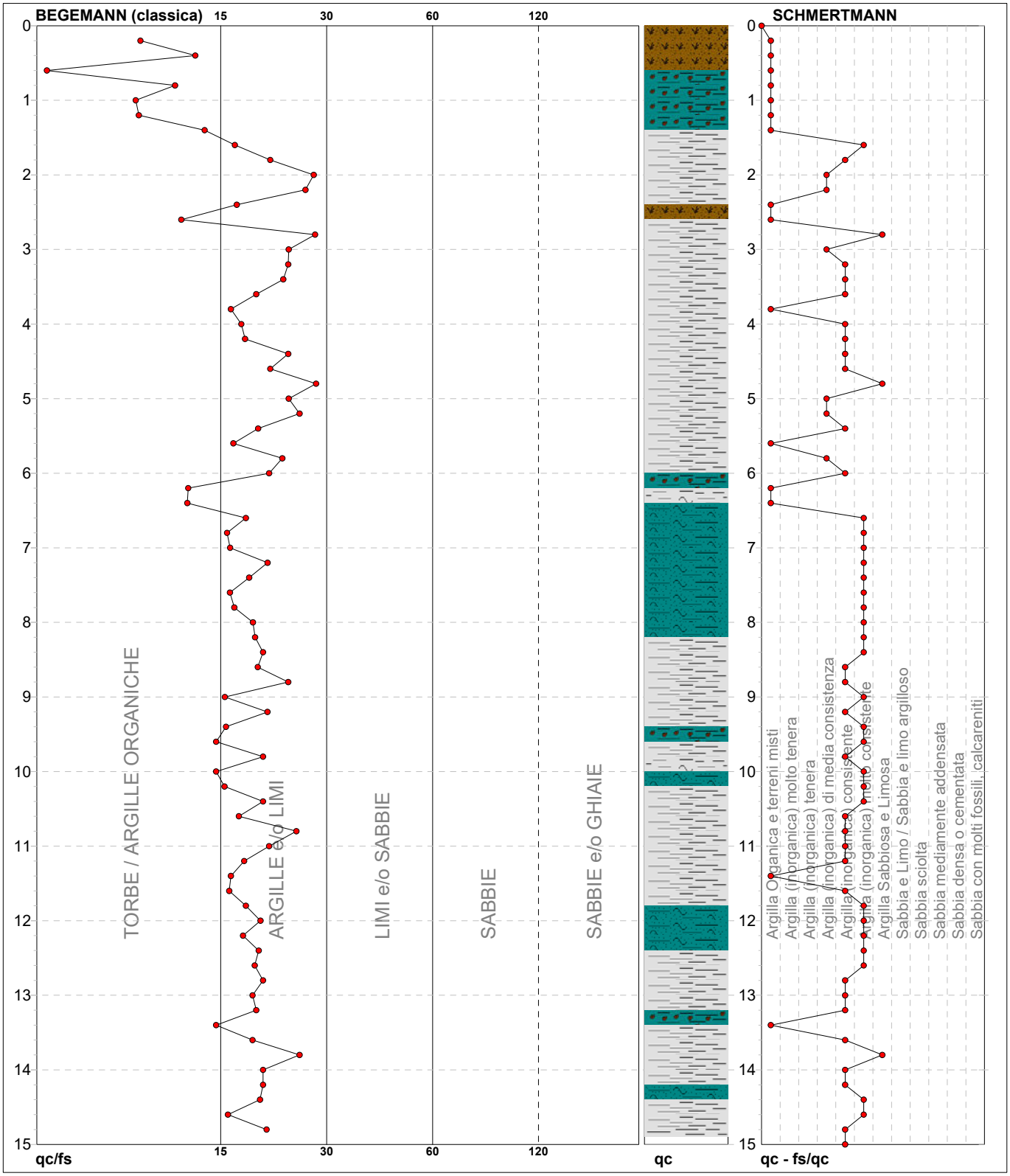
Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI LITOLOGIA

CPT	4
riferimento	110-2023

Committente:	**Green-go**	U.M.:	**kg/cm²**	Data esec.:	01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Scala:	1:75		
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Pagina:	1		
		Elaborato:		Falda:	-2.40 m da p.c.



Torbe / Argille org. :	13 punti, 17.57%	Argilla Organica e terreni misti:	15 punti, 20.27%	Argilla Sabbiosa e Limosa:	3 punti, 4.05%
Argille e/o Limi :	61 punti, 82.43%	Argilla (inorganica) media consist.:	6 punti, 8.11%		
		Argilla (inorganica) consistente:	26 punti, 35.14%		
		Argilla (inorganica) molto consist.:	24 punti, 32.43%		

nota: FON053

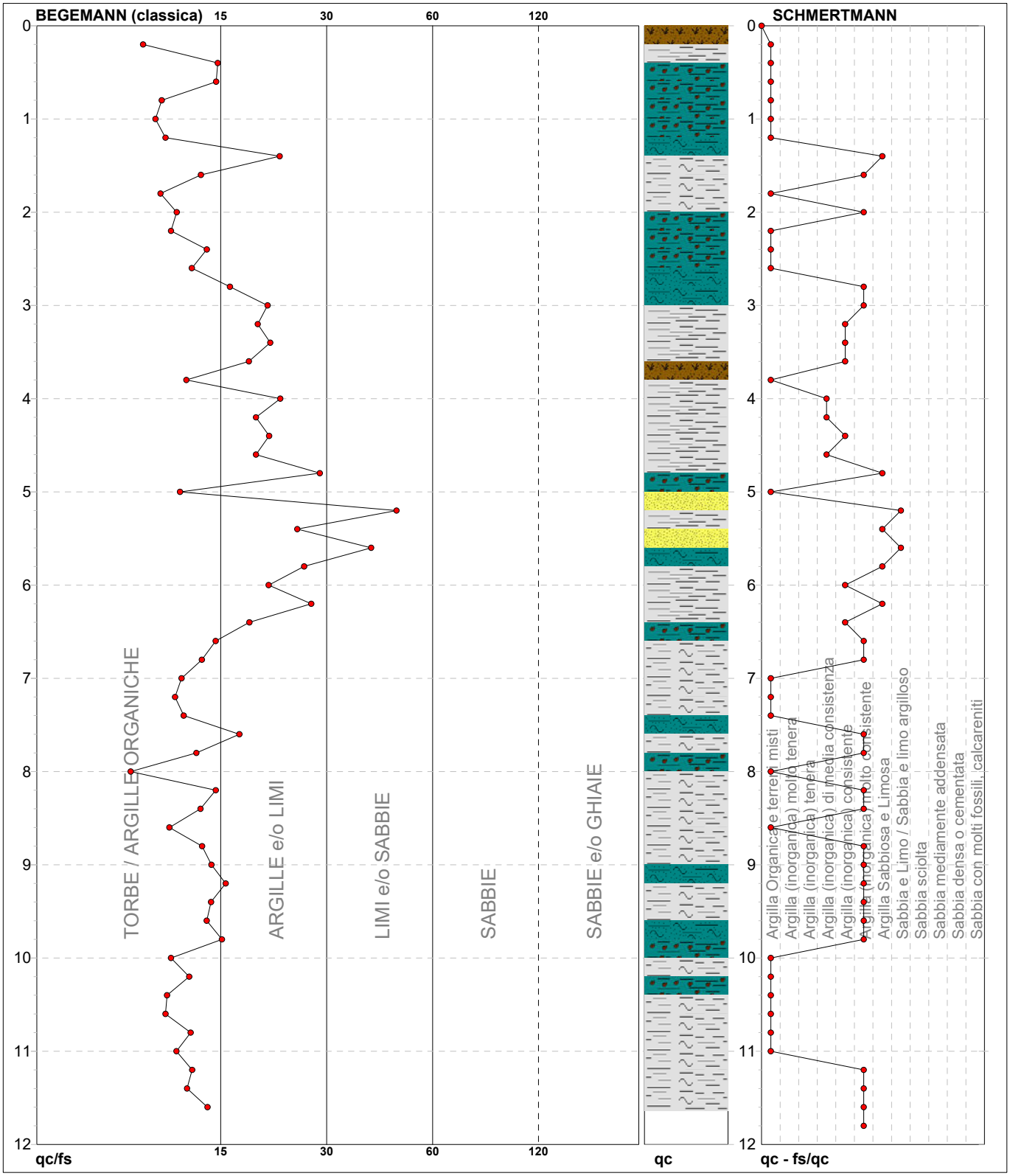
Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI LITOLOGIA

CPT	5
riferimento	110-2023

Committente:	**Green-go**	U.M.: **kg/cm²**	Data esec.: 01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Scala: 1:60	
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Pagina: 1	
		Elaborato:	Falda: -2.20 m da p.c.



Torbe / Argille org. :	36 punti,	61.02%
Argille e/o Limi :	20 punti,	33.90%
Limi e/o Sabbie :	2 punti,	3.39%

Argilla Organica e terreni misti:	23 punti,	38.98%
Argilla (inorganica) media consist.:	3 punti,	5.08%
Argilla (inorganica) consistente:	6 punti,	10.17%
Argilla (inorganica) molto consist.:	19 punti,	32.20%

Argilla Sabbiosa e Limosa:	5 punti,	8.47%
Sabbia e Limo / Sabbia e limo arg.:	2 punti,	3.39%

nota: FON053

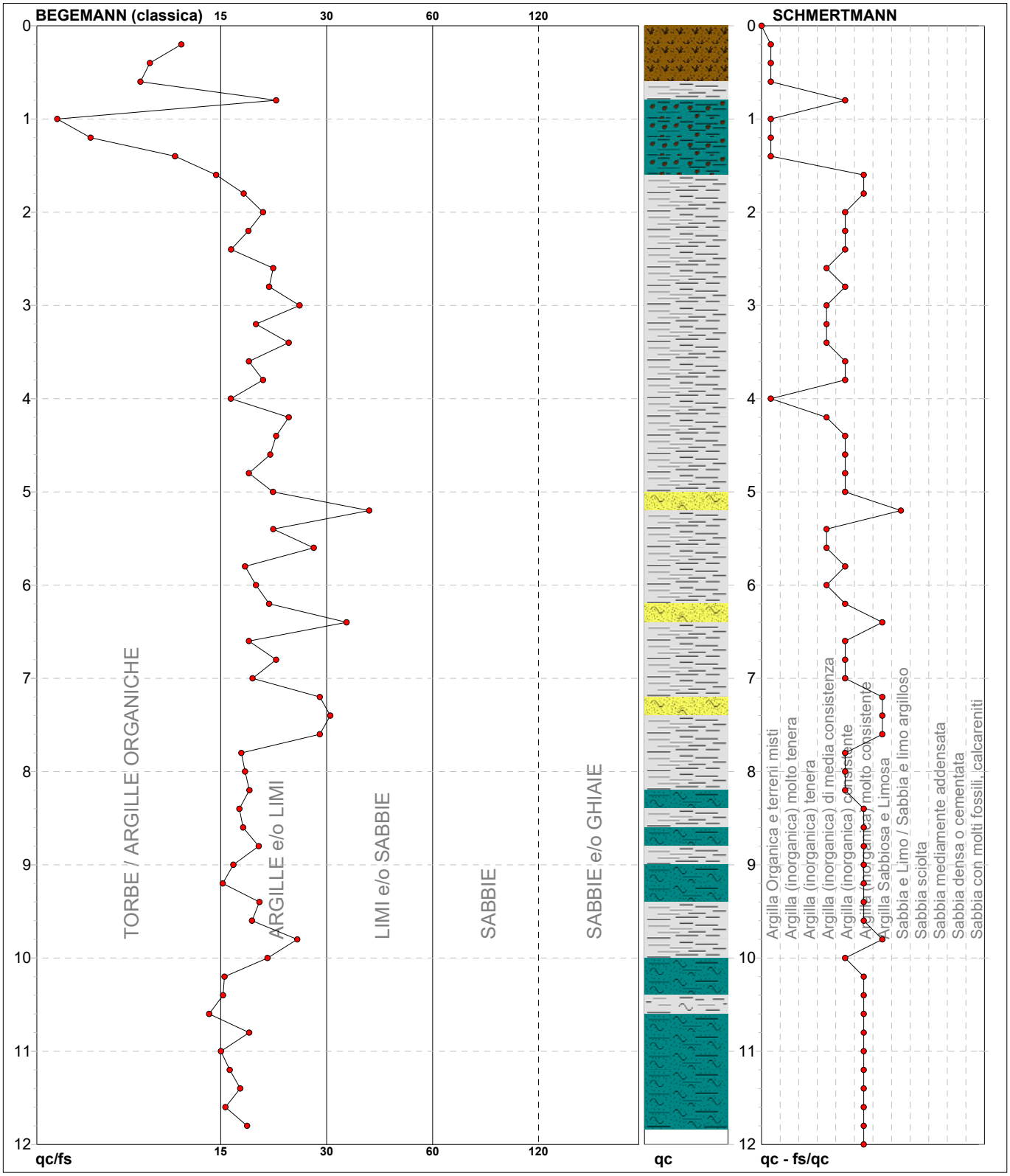
Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI LITOLOGIA

CPT	6
riferimento	110-2023

Committente:	**Green-go**	U.M.:	**kg/cm²**	Data esec.:	01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Scala:	1:60		
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Pagina:	1		
		Elaborato:		Falda:	Non rilevata



Torbe / Argille org. :	8 punti,	13.56%	Argilla Organica e terreni misti:	7 punti,	11.86%	Argilla Sabbiosa e Limosa:	5 punti, 8.47%
Argille e/o Limi :	48 punti,	81.36%	Argilla (inorganica) media consist.:	8 punti,	13.56%	Sabbia e Limo / Sabbia e limo arg.:	1 punti, 1.69%
Limi e/o Sabbie :	3 punti,	5.08%	Argilla (inorganica) consistente:	20 punti,	33.90%		
			Argilla (inorganica) molto consist.:	18 punti,	30.51%		

nota: FON053

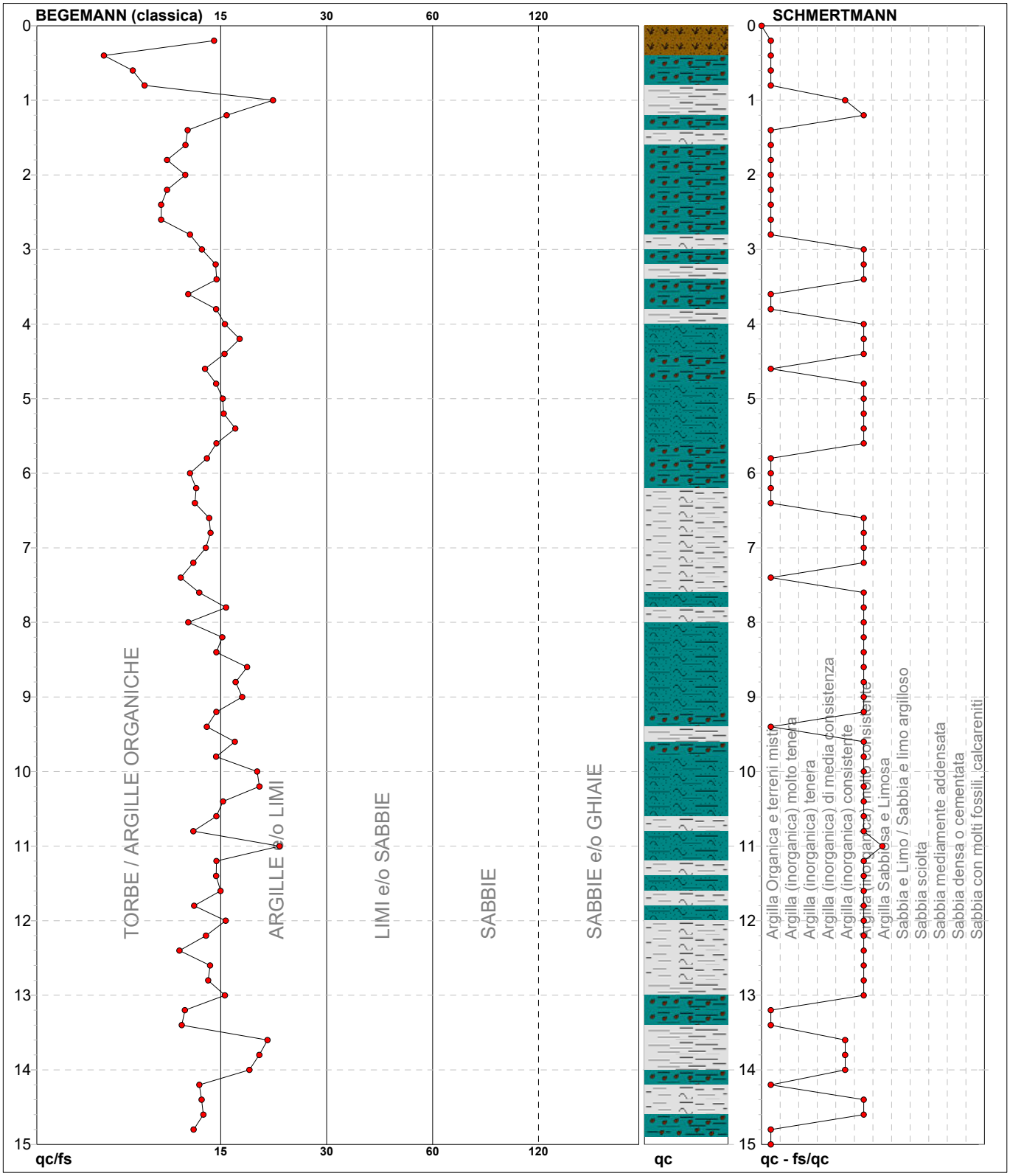
Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI LITOLOGIA

CPT	7
riferimento	110-2023

Committente:	**Green-go**	U.M.:	**kg/cm²**	Data esec.:	01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Scala:	1:75		
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Pagina:	1		
		Elaborato:		Falda:	Non rilevata



Torbe / Argille org. :	44 punti, 59.46%	Argilla Organica e terreni misti:	25 punti, 33.78%	Argilla Sabbiosa e Limosa:	1 punti, 1.35%
Argille e/o Limi :	30 punti, 40.54%	Argilla (inorganica) consistente:	4 punti, 5.41%		
		Argilla (inorganica) molto consist.:	44 punti, 59.46%		

nota: FON053

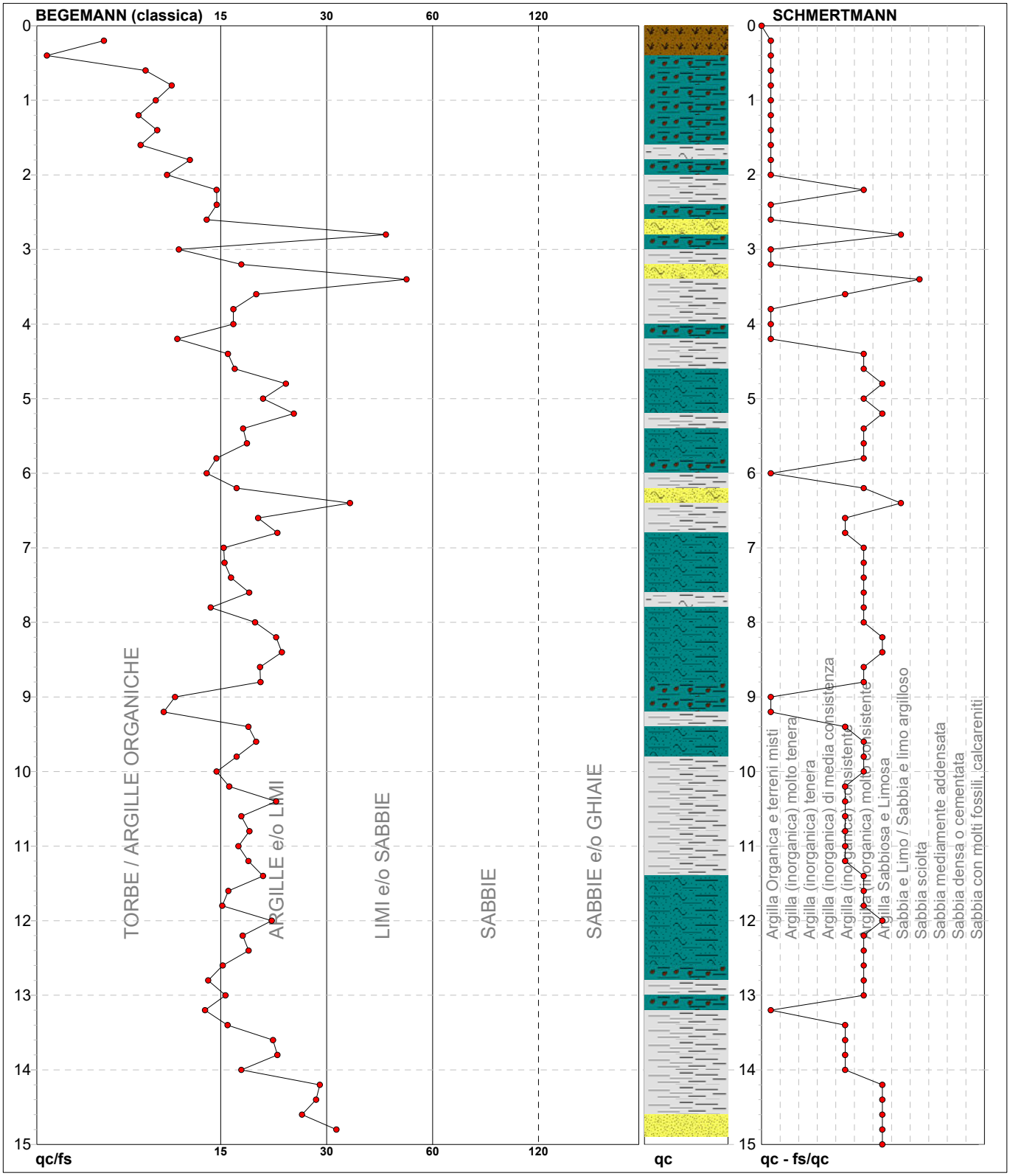
Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI LITOLOGIA

CPT	8
riferimento	110-2023

Committente:	**Green-go**	U.M.:	**kg/cm²**	Data esec.:	01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Scala:	1:75		
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Pagina:	1		
		Elaborato:		Falda:	Non rilevata



Torbe / Argille org. :	19 punti, 25.68%	Argilla Organica e terreni misti:	21 punti, 28.38%	Argilla Sabbiosa e Limosa:	9 punti, 12.16%
Argille e/o Limi :	51 punti, 68.92%	Argilla (inorganica) consistente:	14 punti, 18.92%	Sabbia e Limo / Sabbia e limo arg.:	2 punti, 2.70%
Limi e/o Sabbie :	4 punti, 5.41%	Argilla (inorganica) molto consist.:	27 punti, 36.49%	Sabbia sciolta:	1 punti, 1.35%

nota: FON053

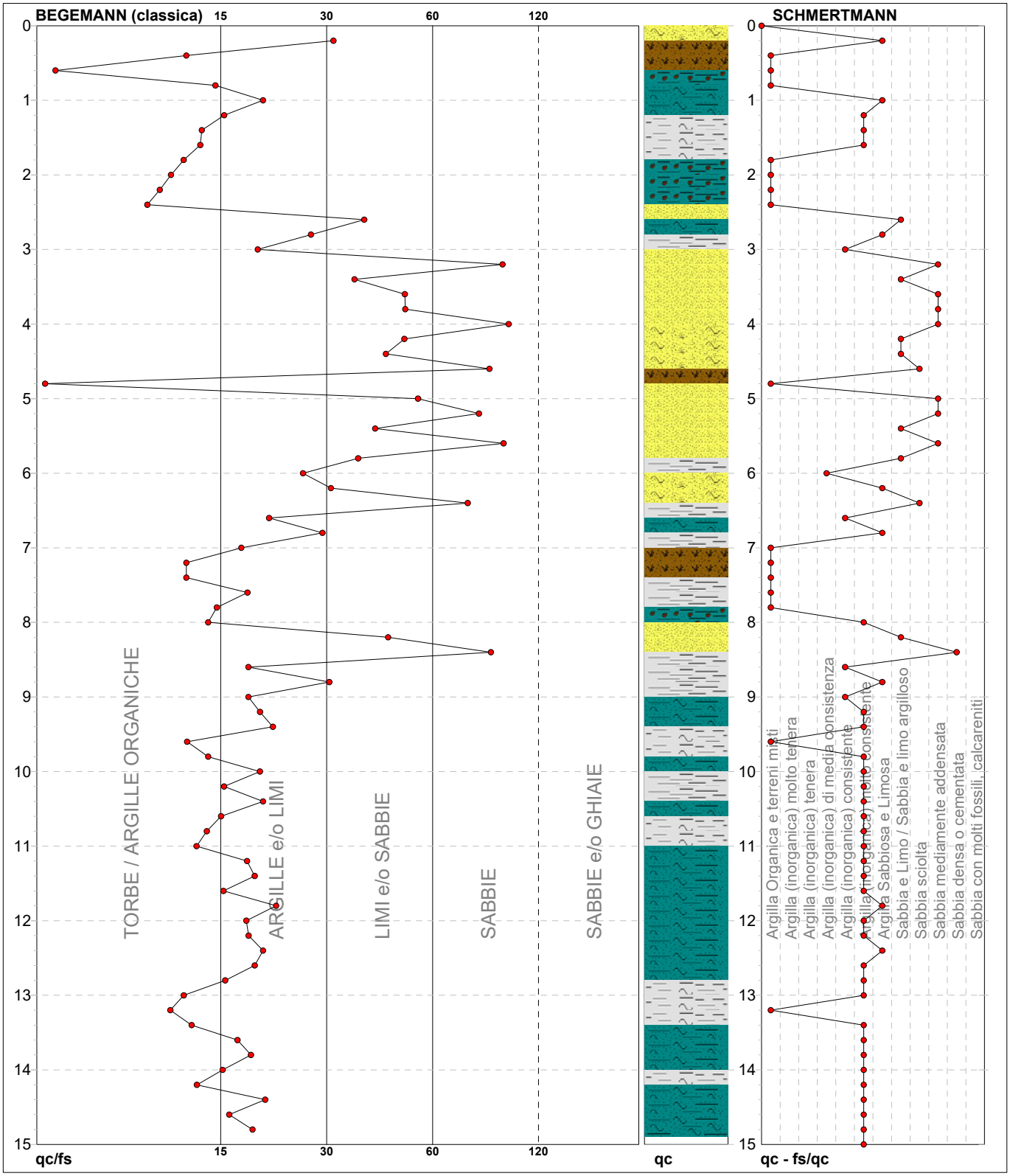
Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI LITOLOGIA

CPT	9
riferimento	110-2023

Committente:	**Green-go**	U.M.:	**kg/cm²**	Data esec.:	01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Scala:	1:75		
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Pagina:	1		
		Elaborato:		Falda:	-1.80 m da p.c.



Torbe / Argille org. :	21 punti, 28.38%	Argilla Organica e terreni misti:	15 punti, 20.27%	Argilla Sabbiosa e Limosa:	8 punti, 10.81%
Argille e/o Limi :	34 punti, 45.95%	Argilla (inorganica) media consist.:	1 punti, 1.35%	Sabbia e Limo / Sabbia e limo arg.:	7 punti, 9.46%
Limi e/o Sabbie :	12 punti, 16.22%	Argilla (inorganica) consistente:	4 punti, 5.41%	Sabbia sciolta:	2 punti, 2.70%
Sabbie:	7 punti, 9.46%	Argilla (inorganica) molto consist.:	29 punti, 39.19%	Sabbia mediamente addensata:	7 punti, 9.46%
				Sabbia densa o cementata:	1 punti, 1.35%

nota: FON053

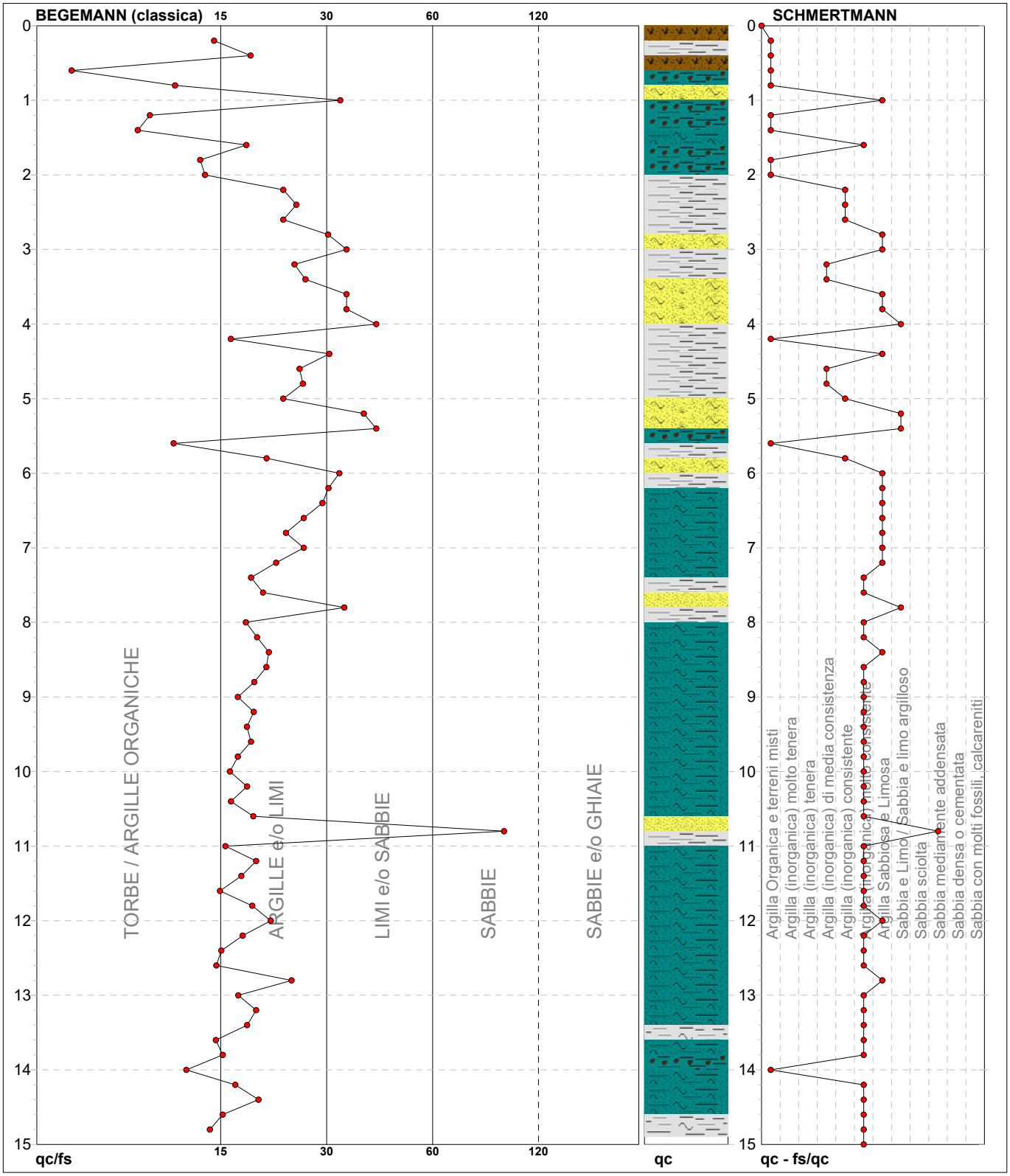
Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI LITOLOGIA

CPT	10
riferimento	110-2023

Committente:	**Green-go**	U.M.:	**kg/cm²**	Data esec.:	01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Scala:	1:75		
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Pagina:	1		
		Elaborato:		Falda:	Non rilevata



Torbe / Argille org. :	11 punti, 14.86%	Argilla Organica e terreni misti:	11 punti, 14.86%	Argilla Sabbiosa e Limosa:	16 punti, 21.62%
Argille e/o Limi :	53 punti, 71.62%	Argilla (inorganica) media consist.:	4 punti, 5.41%	Sabbia e Limo / Sabbia e limo arg.:	4 punti, 5.41%
Limi e/o Sabbie :	9 punti, 12.16%	Argilla (inorganica) consistente:	5 punti, 6.76%	Sabbia mediamente addensata:	1 punti, 1.35%
Sabbie:	1 punti, 1.35%	Argilla (inorganica) molto consist.:	33 punti, 44.59%		

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

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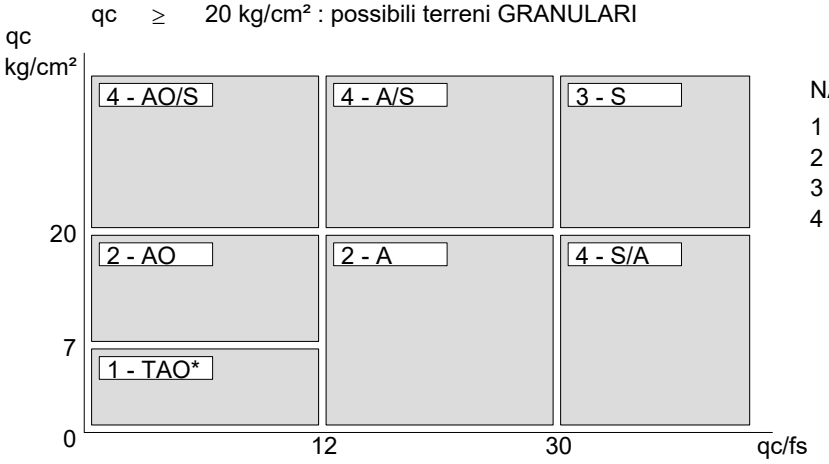
LEGENDA PARAMETRI GEOTECNICI
SPECIFICHE TECNICHE

Le scelte litologiche vengono effettuate in base al rapporto qc / fs (Begemann 1965 - A.G.I. 1977) prevedendo altresì la possibilità di casi dubbi :

qc ≤ 20 kg/cm² : possibili terreni COESIVI — anche se (qc / fs) > 30

qc ≥ 20 kg/cm² : possibili terreni GRANULARI — anche se (qc / fs) < 30



NATURA LITOLOGICA
1 - COESIVA (TORBOSA) ALTA COMPRIM.
2 - COESIVA IN GENERE
3 - GRANULARE
4 - COESIVA / GRANULARE

PARAMETRI GEOTECNICI (validità orientativa) - simboli - correlazioni - bibliografia

γ' = peso dell' unità di volume (efficace) del terreno [correlazioni : γ' - qc - natura]
(Terzaghi & Peck 1967 - Bowles 1982)

$\sigma'vo$ = tensione verticale geostatica (efficace) del terreno (valutata in base ai valori di γ')

Cu = coesione non drenata (terreni coesivi) [correlazioni : Cu - qc]

OCR = grado di sovra consolidazione (terreni coesivi) [correlazioni : OCR - Cu - σ 'vo]
(Ladd et al. 1972 / 1974 / 1977 - Lancellotta 1983)

Eu = modulo di deformazione non drenato (terreni coesivi) [correl. : Eu - Cu - OCR - Ip Ip= ind.plast.]
Eu50 - Eu25 corrispondono rispettivamente ad un grado di mobilitazione dello sforzo deviatorico pari al 50-25% (Duncan & Buchigani 1976)

E' = modulo di deformazione drenato (terreni granulari) [correlazioni : E' - qc]
E'50 - E'25 corrispondono rispettivamente ad un grado di mobilitazione dello sforzo deviatorico pari al 50-25% (coeff. di sicurezza F = 2 - 4 rispettivamente)
Schmertmann 1970 / 1978 - Jamiolkowski ed altri 1983)

Mo = modulo di deformazione edometrico (terreni coesivi e granulari) [correl. : Mo - qc - natura]
Sanglerat 1972 - Mitchell & Gardner 1975 - Ricceri et al. 1974 - Holden 1973)

Dr = densità relativa (terreni granulari N. C. - normalmente consolidati)
[correlazioni : Dr - Rp - σ 'vo (Schmertmann 1976)]

Ø' = angolo di attrito interno efficace (terreni granulari N.C.) [correl. : Ø' - Dr - qc σ 'vo)
ØCa - Caquot (1948) — ØKo - Koppejan (1948)
ØDB - De Beer (1965) — ØSc - Schmertmann (1978)
ØDM - Durgunoglu & Mitchell (1975) (sabbie N.C.) — ØMe - Meyerhof (1956 / 1976) (sabbie limose)

F.L. = fattore di liquefazione (F.L.s = Sabbie Pulite, F.L.l = Sabbie Limose)

Vs = velocità di propagazione delle onde sismiche (Iyisan 1996)

Dott. Geol. Maurizio Zamboni
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PROVA PENETROMETRICA STATICA MECCANICA
PARAMETRI GEOTECNICI

CPT	1
riferimento	110-2023

Committente:	**Green-go**	U.M.: **kg/cm²**	Data esec.: 01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Pagina: 1	
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Elaborato:	Falda: -0.60 m Non rilevata

							NATURA COESIVA					NATURA GRANULARE											
Prof.	qc	qc/fs	zone	γ'	σ'vo	Vs	Cu	OCR	Eu50	Eu25	Mo	Dr	Sc	Ca	Ko	DB	DM	Me	FLs	FLI	E'50	E'25	Mo
m	U.M.			t/m³	U.M.	m/s	U.M.	%	U.M.	U.M.	U.M.	%	(°)	(°)	(°)	(°)	(°)	(°)			U.M.	U.M.	U.M.
0.20	4.00	14.81	1	1.46	0.03	93	0.20	69.6	8.0	12.0	6.0	--	--	--	--	--	--	--	--	--	--	--	--
0.40	4.00	12.12	1	1.46	0.06	93	0.20	29.2	8.0	12.0	6.0	--	--	--	--	--	--	--	--	--	--	--	--
0.60	7.00	7.53	1	0.46	0.07	115	0.35	49.0	14.0	21.0	10.5	--	--	--	--	--	--	--	--	--	--	--	--
0.80	12.00	11.22	2	0.92	0.09	141	0.57	67.0	97.1	145.7	44.6	--	--	--	--	--	--	--	--	--	--	--	--
1.00	15.00	15.00	2	0.95	0.11	154	0.67	63.3	113.3	170.0	49.5	--	--	--	--	--	--	--	--	--	--	--	--
1.20	13.00	11.50	2	0.93	0.12	145	0.60	45.7	102.8	154.2	46.5	--	--	--	--	--	--	--	--	--	--	--	--
1.40	17.00	17.00	2	0.97	0.14	161	0.72	47.6	123.0	184.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
1.60	15.00	16.13	2	0.95	0.16	154	0.67	36.8	113.3	170.0	49.5	--	--	--	--	--	--	--	--	--	--	--	--
1.80	14.00	20.90	2	0.94	0.18	150	0.64	30.3	108.2	162.3	48.2	--	--	--	--	--	--	--	--	--	--	--	--
2.00	11.00	18.33	2	0.91	0.20	137	0.54	21.7	91.2	136.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
2.20	11.00	18.33	2	0.91	0.22	137	0.54	19.4	91.2	136.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
2.40	12.00	20.00	2	0.92	0.24	141	0.57	19.0	97.1	145.7	44.6	--	--	--	--	--	--	--	--	--	--	--	--
2.60	11.00	23.40	2	0.91	0.25	137	0.54	16.0	91.2	136.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
2.80	7.00	11.67	1	0.46	0.26	115	0.35	9.0	14.8	22.2	10.5	--	--	--	--	--	--	--	--	--	--	--	--
3.00	11.00	23.40	2	0.91	0.28	137	0.54	14.1	91.2	136.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
3.20	14.00	20.90	2	0.94	0.30	150	0.64	16.1	108.2	162.3	48.2	--	--	--	--	--	--	--	--	--	--	--	--
3.40	17.00	18.28	2	0.97	0.32	161	0.72	17.4	123.0	184.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
3.60	16.00	21.92	2	0.96	0.34	157	0.70	15.4	118.3	177.4	51.8	--	--	--	--	--	--	--	--	--	--	--	--
3.80	15.00	20.55	2	0.95	0.36	154	0.67	13.7	113.3	170.0	49.5	--	--	--	--	--	--	--	--	--	--	--	--
4.00	11.00	16.42	2	0.91	0.38	137	0.54	9.8	91.5	137.3	42.5	--	--	--	--	--	--	--	--	--	--	--	--
4.20	19.00	23.75	2	0.99	0.40	168	0.78	14.6	131.8	197.8	58.1	--	--	--	--	--	--	--	--	--	--	--	--
4.40	19.00	15.83	2	0.99	0.42	168	0.78	13.7	131.8	197.8	58.1	--	--	--	--	--	--	--	--	--	--	--	--
4.60	18.00	12.86	2	0.98	0.44	164	0.75	12.4	127.5	191.3	56.2	--	--	--	--	--	--	--	--	--	--	--	--
4.80	16.00	16.00	2	0.96	0.45	157	0.70	10.7	118.3	177.4	51.8	--	--	--	--	--	--	--	--	--	--	--	--
5.00	17.00	14.17	2	0.97	0.47	161	0.72	10.7	123.0	184.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
5.20	18.00	15.93	2	0.98	0.49	164	0.75	10.6	127.5	191.3	56.2	--	--	--	--	--	--	--	--	--	--	--	--
5.40	17.00	14.17	2	0.97	0.51	161	0.72	9.7	123.9	185.9	54.1	--	--	--	--	--	--	--	--	--	--	--	--
5.60	17.00	14.17	2	0.97	0.53	161	0.72	9.2	126.6	189.9	54.1	--	--	--	--	--	--	--	--	--	--	--	--
5.80	18.00	15.93	2	0.98	0.55	164	0.75	9.2	131.3	196.9	56.2	--	--	--	--	--	--	--	--	--	--	--	--
6.00	25.00	13.89	4	0.94	0.57	186	0.91	11.2	154.5	231.8	75.0	38	36	29	25	24	32	28	0.73	1.11	41.7	62.5	75.0
6.20	26.00	14.44	4	0.95	0.59	189	0.93	11.1	157.9	236.8	78.0	39	36	29	25	24	32	28	0.74	1.12	43.3	65.0	78.0
6.40	22.00	14.97	4	0.93	0.61	177	0.85	9.5	145.9	218.9	66.0	32	35	28	24	23	31	28	0.69	1.04	36.7	55.0	66.0
6.60	20.00	13.61	4	0.93	0.63	171	0.80	8.5	148.7	223.1	60.0	28	35	27	24	22	31	27	0.67	1.00	33.3	50.0	60.0
6.80	22.00	14.97	4	0.93	0.65	177	0.85	8.8	152.9	229.3	66.0	31	35	27	24	23	31	28	0.68	1.03	36.7	55.0	66.0
7.00	23.00	15.03	4	0.94	0.66	180	0.87	8.8	157.3	236.0	69.0	31	35	27	24	23	31	28	0.69	1.04	38.3	57.5	69.0
7.20	21.00	15.00	4	0.93	0.68	174	0.82	7.9	164.3	246.4	63.0	28	35	27	24	22	30	27	0.67	1.00	35.0	52.5	63.0
7.40	24.00	16.33	4	0.94	0.70	183	0.89	8.4	166.6	250.0	72.0	32	35	27	24	23	31	28	0.69	1.04	40.0	60.0	72.0
7.60	16.00	9.58	2	0.96	0.72	157	0.70	6.0	190.7	286.0	51.8	--	--	--	--	--	--	--	--	--	--	--	--
7.80	23.00	15.03	4	0.94	0.74	180	0.87	7.7	179.7	269.5	69.0	29	35	27	24	22	30	28	0.67	1.02	38.3	57.5	69.0
8.00	19.00	20.43	2	0.99	0.76	168	0.78	6.4	196.2	294.4	58.1	--	--	--	--	--	--	--	--	--	--	--	--
8.20	22.00	16.54	4	0.93	0.78	177	0.85	7.0	195.5	293.2	66.0	26	34	26	23	22	30	28	0.66	0.99	36.7	55.0	66.0
8.40	21.00	17.50	4	0.93	0.80	174	0.82	6.5	204.8	307.2	63.0	24	34	26	23	21	30	27	0.65	0.98	35.0	52.5	63.0
8.60	16.00	14.16	2	0.96	0.82	157	0.70	5.1	224.1	336.1	51.8	--	--	--	--	--	--	--	--	--	--	--	--
8.80	23.00	17.29	4	0.94	0.83	180	0.87	6.6	214.0	320.9	69.0	26	34	26	23	22	30	28	0.66	1.00	38.3	57.5	69.0
9.00	25.00	14.97	4	0.94	0.85	186	0.91	6.8	216.4	324.7	75.0	28	35	27	23	22	30	28	0.68	1.02	41.7	62.5	75.0
9.20	21.00	15.79	4	0.93	0.87	174	0.82	5.8	232.5	348.8	63.0	22	34	26	22	21	29	27	0.64	0.96	35.0	52.5	63.0
9.40	24.00	17.14	4	0.94	0.89	183	0.89	6.3	232.5	348.8	72.0	26	34	26	23	22	30	28	0.67	1.00	40.0	60.0	72.0
9.60	24.00	12.83	4	0.94	0.91	183	0.89	6.1	239.5	359.2	72.0	25	34	26	23	21	30	28	0.67	1.00	40.0	60.0	72.0
9.80	23.00	12.78	4	0.94	0.93	180	0.87	5.8	248.4	372.7	69.0	23	34	26	22	21	29	28	0.66	0.99	38.3	57.5	69.0
10.00	23.00	12.30	4	0.94	0.95	180	0.87	5.6	255.1	382.7	69.0	23	34	26	22	21	29	28	0.66	0.99	38.3	57.5	69.0
10.20	23.00	15.65	4	0.94	0.97	180	0.87	5.5	261.7	392.6	69.0	22	34	26	22	21	29	28	0.66	1.00	38.3	57.5	69.0
10.40	23.00	17.29	4	0.94	0.98	180	0.87	5.4	268.2	402.3	69.0	22	34	25	22	21	29	28	0.66	1.00	38.3	57.5	69.0
10.60	26.00	32.50	3	0.87	1.00	189	--	--	--	--	--	26	34	26	23	21	29	28	0.69	1.04	43.3	65.0	78.0
10.80	38.00	21.97	4	0.99	1.02	218	1.27	8.2	243.7	365.6	114.0	38	36	28	25	23	31	30	0.79	1.19	63.3	95.0	114.0
11.00	26.00	13.47	4	0.95	1.04	189	0.93	5.4	282.6	423.9	78.0	25	34	26	23	21	29	28	0.69	1.04	43.3	65.0	78.0
11.20	24.00	15.00	4	0.94	1.06	183	0.89	5.0	291.9	437.9	72.0	22	34	25	22	21	29	28	0.68	1.02	40.0	60.0	72.0
11.40	23.00	16.43	4	0.94	1.08	180	0.87	4.8	299.1	448.7	69.0	20	34	25	22	20	28	28	0.67	1.01	38.3	57.5	69.0
11.60	25.00	19.69	4	0.94	1.10	186	0.91	5.0	303.0	454.5	75.0	22	34	25	22	21	29	28	0.69	1.04	41.7	62.5	75.0
11.80	16.00	14.95	2	0.96	1.12	157	0.70	3.5	314.5	471.8	51.8	--	--	--	--	--	--	--	--	--	--	--	--
12.00	9.00	16.98	2	0.88	1.13	127	0.45	2.0	252.5	378.8	37.8	--	--	--	--	--	--	--	--	--	--	--	--
12.20	16.00	59.26	4	0.90	1.15	157	0.70	3.3	323.0	484.5	51.8	6	32	23	19	18	26	27	0.62	0.94	26.7	40.0	48.0
12.40	19.00	28.36	2	0.99	1.17	168	0.78	3.7	330.3	495.4	58.1	--	--	--	--	--	--	--	--	--	--	--	--
12.60	9.00	15.00	2	0.88	1.19	127	0.45	1.9	255.2	382.7	37.8	--	--	--	--	--	--	--	--	--	--	--	--
12.80	9.00	13.43	2	0.88	1.21	127	0.45	1.8	255.9	383.9	37.8	--	--	--	--	--	--	--	--	--	--	--	--
13.00	12.00	16.44	2	0.92	1.23	141	0.57	2.4	305.8	458.8	44.6	--	--	--	--	--	--	--	--	--	--	--	--
13.20	16.00	16.00	2	0.96	1.24	157	0.70	3.0	341.2	511.8	51.8	--	--	--	--	--	--	--	--	--	--	--	--
13.40	14.00	14.00	2	0.94	1.26	150	0.64	2.7	330.0	495.1	48.2	--	--	--	--	--	--	--	--	--	--	--	--
13.60	11.00	13.75	2	0.91	1.28	137	0.54	2.1	297.1	445.6	42.5	--	--	--	--	--	--	--	--	--	--	--	--
13.80	14.00	14.00	2	0.94	1.30	150	0.64	2.6	334.2	501.3	48.2	--	--	--	--	--	--	--	--	--	--	--	--
14.00	15.00	15.00	2	0.95	1.32	154	0.67	2.7	345.3	517.9	49.5	--	--	--	--	--	--	--	--	--	--	--	--
14.20	18.00	15.00	2	0.98	1.34	164	0.75	3.0	367.4	551.1	56.2	--	--	--	--	--	--	--	--	--	--	--	--
14.40	16.00	16.00	2	0.96	1.36	157	0.70	2.7	358.0	537.0	51.8	--	--	--	--	--	--	--	--	--	--	--	--
14.60	16.00	17.20	2	0.96	1.38	157	0.70	2.7	360.3	540.5	51.8	--	--	--	--	--	--	--	--	--	--	--	--
14.80	15.00	17.24	2	0.95	1.40	154	0.67	2.5	353.7	530.5	49.5	--	--	--	--	--	--	--	--	--	--	--	--
15.00	17.00	--	3	0.84	1.41	161	--	--	--	--	--	3	32	22	19	18	25	27	0.67	1.02	28.3	42.5	51.0

FON053

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Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
PARAMETRI GEOTECNICI

CPT	2
riferimento	110-2023

Committente:	**Green-go**	U.M.: **kg/cm²**	Data esec.: 01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Pagina: 1	
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Elaborato:	Falda: -0.50 m da p.c.

							NATURA COESIVA					NATURA GRANULARE											
Prof.	qc	qc/fs	zone	γ'	σ'vo	Vs	Cu	OCR	Eu50	Eu25	Mo	Dr	Sc	Ca	Ko	DB	DM	Me	FLs	FLI	E'50	E'25	Mo
m	U.M.			t/m³	U.M.	m/s	U.M.	%	U.M.	U.M.	U.M.	%	(°)	(°)	(°)	(°)	(°)	(°)			U.M.	U.M.	U.M.
0.20	1.00	2.13	1	1.46	0.03	55	0.05	12.3	2.0	3.0	1.5	--	--	--	--	--	--	--	--	--	--	--	--
0.40	2.00	3.33	1	1.46	0.06	72	0.10	12.3	4.0	6.0	3.0	--	--	--	--	--	--	--	--	--	--	--	--
0.60	5.00	3.57	1	0.46	0.07	101	0.25	32.2	10.0	15.0	7.5	--	--	--	--	--	--	--	--	--	--	--	--
0.80	7.00	5.51	1	0.46	0.08	115	0.35	41.8	14.0	21.0	10.5	--	--	--	--	--	--	--	--	--	--	--	--
1.00	11.00	9.73	2	0.91	0.10	137	0.54	54.7	91.2	136.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
1.20	9.00	7.96	2	0.88	0.11	127	0.45	35.5	76.5	114.8	37.8	--	--	--	--	--	--	--	--	--	--	--	--
1.40	12.00	9.45	2	0.92	0.13	141	0.57	39.6	97.1	145.7	44.6	--	--	--	--	--	--	--	--	--	--	--	--
1.60	12.00	10.00	2	0.92	0.15	141	0.57	33.6	97.1	145.7	44.6	--	--	--	--	--	--	--	--	--	--	--	--
1.80	18.00	12.86	2	0.98	0.17	164	0.75	40.4	127.5	191.3	56.2	--	--	--	--	--	--	--	--	--	--	--	--
2.00	11.00	18.33	2	0.91	0.19	137	0.54	23.4	91.2	136.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
2.20	12.00	16.44	2	0.92	0.21	141	0.57	22.5	97.1	145.7	44.6	--	--	--	--	--	--	--	--	--	--	--	--
2.40	8.00	11.94	2	0.86	0.22	121	0.40	13.0	68.0	102.0	35.2	--	--	--	--	--	--	--	--	--	--	--	--
2.60	8.00	15.09	2	0.86	0.24	121	0.40	11.9	68.0	102.0	35.2	--	--	--	--	--	--	--	--	--	--	--	--
2.80	9.00	15.00	2	0.88	0.26	127	0.45	12.6	76.5	114.8	37.8	--	--	--	--	--	--	--	--	--	--	--	--
3.00	7.00	17.50	2	0.84	0.27	115	0.35	8.5	65.1	97.7	32.2	--	--	--	--	--	--	--	--	--	--	--	--
3.20	8.00	11.94	2	0.86	0.29	121	0.40	9.3	69.6	104.4	35.2	--	--	--	--	--	--	--	--	--	--	--	--
3.40	9.00	7.09	2	0.88	0.31	127	0.45	10.0	76.5	114.8	37.8	--	--	--	--	--	--	--	--	--	--	--	--
3.60	20.00	60.61	⚠ 4	0.93	0.33	171	0.80	19.2	136.0	204.0	60.0	44	37	30	27	25	34	27	0.76	1.14	33.3	50.0	60.0
3.80	12.00	16.44	2	0.92	0.35	141	0.57	11.8	97.1	145.7	44.6	--	--	--	--	--	--	--	--	--	--	--	--
4.00	7.00	13.21	1	0.46	0.36	115	0.35	6.2	19.1	28.7	10.5	--	--	--	--	--	--	--	--	--	--	--	--
4.20	11.00	13.75	2	0.91	0.37	137	0.54	9.9	91.4	137.1	42.5	--	--	--	--	--	--	--	--	--	--	--	--
4.40	14.00	23.33	2	0.94	0.39	150	0.64	11.5	108.2	162.3	48.2	--	--	--	--	--	--	--	--	--	--	--	--
4.60	21.00	26.25	⚠ 4	0.93	0.41	174	0.82	15.0	140.0	210.0	63.0	40	36	29	26	25	33	27	0.72	1.08	35.0	52.5	63.0
4.80	25.00	31.25	⚠ 3	0.86	0.43	186	--	--	--	--	--	45	37	30	27	25	34	28	0.75	1.15	41.7	62.5	75.0
5.00	20.00	22.99	⚠ 4	0.93	0.45	171	0.80	13.0	136.0	204.0	60.0	36	36	29	26	24	32	27	0.69	1.04	33.3	50.0	60.0
5.20	17.00	15.89	2	0.97	0.47	161	0.72	10.9	123.0	184.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
5.40	13.00	14.94	2	0.93	0.48	145	0.60	8.3	115.5	173.2	46.5	--	--	--	--	--	--	--	--	--	--	--	--
5.60	13.00	13.98	2	0.93	0.50	145	0.60	7.9	121.2	181.8	46.5	--	--	--	--	--	--	--	--	--	--	--	--
5.80	12.00	16.44	2	0.92	0.52	141	0.57	7.0	130.6	195.9	44.6	--	--	--	--	--	--	--	--	--	--	--	--
6.00	15.00	25.00	2	0.95	0.54	154	0.67	8.2	129.2	193.8	49.5	--	--	--	--	--	--	--	--	--	--	--	--
6.20	14.00	19.18	2	0.94	0.56	150	0.64	7.4	137.7	206.6	48.2	--	--	--	--	--	--	--	--	--	--	--	--
6.40	21.00	24.14	⚠ 4	0.93	0.58	174	0.82	9.8	140.6	210.9	63.0	32	35	28	24	23	31	27	0.66	1.00	35.0	52.5	63.0
6.60	26.00	15.57	⚠ 4	0.95	0.60	189	0.93	10.9	157.9	236.8	78.0	38	36	29	25	24	32	28	0.71	1.08	43.3	65.0	78.0
6.80	20.00	15.75	⚠ 4	0.93	0.62	171	0.80	8.7	145.8	218.7	60.0	29	35	27	24	22	31	27	0.65	0.98	33.3	50.0	60.0
7.00	14.00	13.08	2	0.94	0.63	150	0.64	6.3	165.2	247.8	48.2	--	--	--	--	--	--	--	--	--	--	--	--
7.20	20.00	20.00	⚠ 4	0.93	0.65	171	0.80	8.1	156.3	234.4	60.0	27	34	27	24	22	30	27	0.64	0.97	33.3	50.0	60.0
7.40	24.00	13.87	⚠ 4	0.94	0.67	183	0.89	8.9	159.1	238.7	72.0	33	35	28	24	23	31	28	0.68	1.02	40.0	60.0	72.0
7.60	23.00	16.43	⚠ 4	0.94	0.69	180	0.87	8.4	164.2	246.3	69.0	31	35	27	24	23	31	28	0.66	1.00	38.3	57.5	69.0
7.80	30.00	15.54	⚠ 4	0.96	0.71	199	1.00	9.6	171.4	257.1	90.0	39	36	28	25	24	32	29	0.73	1.10	50.0	75.0	90.0
8.00	27.00	12.68	⚠ 4	0.95	0.73	192	0.95	8.7	172.6	258.9	81.0	35	35	28	25	23	31	28	0.70	1.05	45.0	67.5	81.0
8.20	19.00	17.76	2	0.99	0.75	168	0.78	6.6	192.2	288.3	58.1	--	--	--	--	--	--	--	--	--	--	--	--
8.40	18.00	18.00	2	0.98	0.77	164	0.75	6.1	202.2	303.4	56.2	--	--	--	--	--	--	--	--	--	--	--	--
8.60	12.00	16.44	2	0.92	0.79	141	0.57	4.2	219.6	329.4	44.6	--	--	--	--	--	--	--	--	--	--	--	--
8.80	20.00	18.69	⚠ 4	0.93	0.80	171	0.80	6.2	210.5	315.7	60.0	22	34	26	23	21	29	27	0.62	0.94	33.3	50.0	60.0
9.00	16.00	12.60	2	0.96	0.82	157	0.70	5.1	226.8	340.3	51.8	--	--	--	--	--	--	--	--	--	--	--	--
9.20	17.00	13.39	2	0.97	0.84	161	0.72	5.2	231.4	347.1	54.1	--	--	--	--	--	--	--	--	--	--	--	--
9.40	19.00	12.93	2	0.99	0.86	168	0.78	5.5	234.0	351.0	58.1	--	--	--	--	--	--	--	--	--	--	--	--
9.60	20.00	15.75	⚠ 4	0.93	0.88	171	0.80	5.6	238.3	357.5	60.0	20	34	25	22	21	29	27	0.62	0.94	33.3	50.0	60.0
9.80	17.00	17.00	2	0.97	0.90	161	0.72	4.8	250.2	375.2	54.1	--	--	--	--	--	--	--	--	--	--	--	--
10.00	16.00	14.16	2	0.96	0.92	157	0.70	4.4	256.9	385.3	51.8	--	--	--	--	--	--	--	--	--	--	--	--
10.20	20.00	13.61	⚠ 4	0.93	0.94	171	0.80	5.1	257.9	386.9	60.0	18	33	25	22	20	28	27	0.63	0.94	33.3	50.0	60.0
10.40	19.00	13.57	2	0.99	0.96	168	0.78	4.8	265.8	398.8	58.1	--	--	--	--	--	--	--	--	--	--	--	--
10.60	22.00	18.33	⚠ 4	0.93	0.98	177	0.85	5.2	267.5	401.3	66.0	21	34	25	22	21	29	28	0.65	0.97	36.7	55.0	66.0
10.80	20.00	15.04	⚠ 4	0.93	1.00	171	0.80	4.8	276.4	414.6	60.0	17	33	25	21	20	28	27	0.63	0.95	33.3	50.0	60.0
11.00	11.00	11.83	2	0.91	1.01	137	0.54	2.8	271.7	407.5	42.5	--	--	--	--	--	--	--	--	--	--	--	--
11.20	20.00	14.29	⚠ 4	0.93	1.03	171	0.80	4.6	287.7	431.6	60.0	16	33	25	21	20	28	27	0.64	0.96	33.3	50.0	60.0
11.40	21.00	13.13	⚠ 4	0.93	1.05	174	0.82	4.6	292.6	438.9	63.0	17	33	25	21	20	28	27	0.65	0.97	35.0	52.5	63.0
11.60	24.00	13.87	⚠ 4	0.94	1.07	183	0.89	5.0	295.4	443.2	72.0	21	34	25	22	21	29	28	0.67	1.01	40.0	60.0	72.0
11.80	22.00	16.54	⚠ 4	0.93	1.09	177	0.85	4.6	303.3	454.9	66.0	18	33	25	21	20	28	28	0.66	0.99	36.7	55.0	66.0
12.00	21.00	17.50	⚠ 4	0.93	1.11	174	0.82	4.3	309.2	463.8	63.0	16	33	24	21	20	28	27	0.65	0.98	35.0	52.5	63.0
12.20	20.00	17.70	⚠ 4	0.93	1.13	171	0.80	4.1	314.2	471.4	60.0	14	33	24	21	20	27	27	0.65	0.97	33.3	50.0	60.0
12.40	11.00	13.75	2	0.91	1.14	137	0.54	2.4	286.6	429.9	42.5	--	--	--	--	--	--	--	--	--	--	--	--
12.60	8.00	7.08	2	0.86	1.16	121	0.40	1.7	230.7	346.0	35.2	--	--	--	--	--	--	--	--	--	--	--	--
12.80	9.00	15.00	2	0.88	1.18	127	0.45	1.9	254.7	382.1	37.8	--	--	--	--	--	--	--	--	--	--	--	--
13.00	12.00	17.91	2	0.92	1.20	141	0.57	2.5	303.2	454.8	44.6	--	--	--	--	--	--	--	--	--	--	--	--
13.20	16.00	21.92	2	0.96	1.22	157	0.70	3.1	336.2	504.3	51.8	--	--	--	--	--	--	--	--	--	--	--	--
13.40	15.00	17.24	2	0.95	1.24	154	0.67	2.9	333.9	500.9	49.5	--	--	--	--	--	--	--	--	--	--	--	--
13.60	30.00	37.50	⚠ 3	0.88	1.25	199	--	--	--	--	--	25	34	26	22	21	29	29	0.74	1.11	50.0	75.0	90.0
13.80	19.00	12.93	2	0.99	1.27	168	0.78	3.4	357.5	536.2	58.1	--	--	--	--	--	--	--	--	--	--	--	--
14.00	10.00	18.87	2	0.90	1.29	132	0.50	1.9	282.1	423.2	40.0	--	--	--	--	--	--	--	--	--	--	--	--
14.20	8.00	11.94	2	0.86	1.31	121	0.40	1.4	234.5	351.7	35.2	--	--	--	--	--	--	--	--	--	--	--	--
14.40	11.00	12.64	2	0.91	1.33	137	0.54	2.0	299.7	449.6	42.5	--	--	--	--	--	--	--	--	--	--	--	--
14.60	14.00	17.50	2	0.94	1.34	150	0.64	2.5	338.8	508.2	48.2	--	--	--	--	--	--	--	--	--	--	--	--
14.80	15.00	16.13	2	0.95	1.36	154	0.67	2.6	350.4	525.5	49.5	--	--	--	--	--	--	--	--	--	--	--	--
15.00	12.00	--	⚠ 3	0.83	1.38	141	--	--	--	--	--	--	31	21	17	16	25	26	0.62	0.96	20.0	30.0	36.0

FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
PARAMETRI GEOTECNICI

CPT	3
riferimento	110-2023

Committente:	**Green-go**	U.M.: **kg/cm²**	Data esec.: 01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Pagina: 1	
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Elaborato:	Falda: Non rilevata

							NATURA COESIVA					NATURA GRANULARE											
Prof.	qc	qc/fs	zone	γ'	σ'vo	Vs	Cu	OCR	Eu50	Eu25	Mo	Dr	Sc	Ca	Ko	DB	DM	Me	FLs	FLl	E'50	E'25	Mo
m	U.M.			t/m³	U.M.	m/s	U.M.	%	U.M.	U.M.	U.M.	%	(°)	(°)	(°)	(°)	(°)	(°)			U.M.	U.M.	U.M.
0.20	6.00	12.77	1	1.46	0.03	109	0.30	99.9	12.0	18.0	9.0	--	--	--	--	--	--	--	--	--	--	--	--
0.40	10.00	16.67	2	1.90	0.07	132	0.50	77.2	85.0	127.5	40.0	--	--	--	--	--	--	--	--	--	--	--	--
0.60	11.00	23.40	2	1.91	0.11	137	0.54	48.0	91.2	136.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
0.80	13.00	19.40	2	1.93	0.14	145	0.60	37.7	102.8	154.2	46.5	--	--	--	--	--	--	--	--	--	--	--	--
1.00	14.00	13.08	2	1.94	0.18	150	0.64	29.9	108.2	162.3	48.2	--	--	--	--	--	--	--	--	--	--	--	--
1.20	16.00	16.00	2	1.96	0.22	157	0.70	26.2	118.3	177.4	51.8	--	--	--	--	--	--	--	--	--	--	--	--
1.40	17.00	15.04	2	1.97	0.26	161	0.72	22.4	123.0	184.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
1.60	14.00	15.05	2	1.94	0.30	150	0.64	16.1	108.2	162.3	48.2	--	--	--	--	--	--	--	--	--	--	--	--
1.80	14.00	17.50	2	1.94	0.34	150	0.64	13.8	108.2	162.3	48.2	--	--	--	--	--	--	--	--	--	--	--	--
2.00	13.00	17.81	2	1.93	0.38	145	0.60	11.3	102.8	154.2	46.5	--	--	--	--	--	--	--	--	--	--	--	--
2.20	12.00	17.91	2	1.92	0.42	141	0.57	9.3	99.3	149.0	44.6	--	--	--	--	--	--	--	--	--	--	--	--
2.40	10.00	18.87	2	1.90	0.45	132	0.50	7.1	113.4	170.1	40.0	--	--	--	--	--	--	--	--	--	--	--	--
2.60	9.00	19.15	2	1.88	0.49	127	0.45	5.6	132.5	198.8	37.8	--	--	--	--	--	--	--	--	--	--	--	--
2.80	12.00	22.64	2	1.92	0.53	141	0.57	6.9	133.7	200.6	44.6	--	--	--	--	--	--	--	--	--	--	--	--
3.00	12.00	22.64	2	1.92	0.57	141	0.57	6.3	147.9	221.9	44.6	--	--	--	--	--	--	--	--	--	--	--	--
3.20	11.00	23.40	2	1.91	0.61	137	0.54	5.4	165.2	247.7	42.5	--	--	--	--	--	--	--	--	--	--	--	--
3.40	12.00	25.53	2	1.92	0.65	141	0.57	5.4	175.5	263.3	44.6	--	--	--	--	--	--	--	--	--	--	--	--
3.60	12.00	25.53	2	1.92	0.68	141	0.57	5.0	188.5	282.7	44.6	--	--	--	--	--	--	--	--	--	--	--	--
3.80	13.00	24.53	2	1.93	0.72	145	0.60	5.0	199.1	298.6	46.5	--	--	--	--	--	--	--	--	--	--	--	--
4.00	13.00	32.50	4	1.88	0.76	145	0.60	4.7	211.1	316.7	46.5	9	32	24	21	19	27	26	--	--	21.7	32.5	39.0
4.20	12.00	36.36	4	1.88	0.80	141	0.57	4.1	222.6	333.9	44.6	5	32	23	20	19	26	26	--	--	20.0	30.0	36.0
4.40	13.00	39.39	4	1.88	0.83	145	0.60	4.2	233.1	349.7	46.5	6	32	23	20	19	27	26	--	--	21.7	32.5	39.0
4.60	16.00	34.04	4	1.90	0.87	157	0.70	4.7	242.5	363.7	51.8	12	33	24	21	20	28	27	--	--	26.7	40.0	48.0
4.80	14.00	23.33	2	1.94	0.91	150	0.64	4.0	254.2	381.3	48.2	--	--	--	--	--	--	--	--	--	--	--	--
5.00	15.00	37.50	4	1.89	0.95	154	0.67	4.0	264.9	397.3	49.5	8	32	23	20	19	27	27	--	--	25.0	37.5	45.0
5.20	12.00	25.53	2	1.92	0.99	141	0.57	3.2	274.0	411.1	44.6	--	--	--	--	--	--	--	--	--	--	--	--
5.40	11.00	40.74	4	1.87	1.03	137	0.54	2.8	273.2	409.8	42.5	--	31	22	18	17	25	26	--	--	18.3	27.5	33.0
5.60	13.00	21.67	2	1.93	1.06	145	0.60	3.1	293.5	440.2	46.5	--	--	--	--	--	--	--	--	--	--	--	--
5.80	13.00	8.84	2	1.93	1.10	145	0.60	3.0	300.1	450.1	46.5	--	--	--	--	--	--	--	--	--	--	--	--
6.00	21.00	24.14	4	1.93	1.14	174	0.82	4.2	318.7	478.0	63.0	15	33	24	21	20	28	27	--	--	35.0	52.5	63.0
6.20	23.00	38.33	3	1.86	1.18	180	--	--	--	--	--	17	33	25	21	20	28	28	--	--	38.3	57.5	69.0
6.40	46.00	97.87	3	1.91	1.22	234	--	--	--	--	--	41	36	28	25	23	32	31	--	--	76.7	115.0	138.0
6.60	27.00	13.04	4	1.95	1.26	192	0.95	4.4	350.4	525.6	81.0	21	34	25	22	21	28	28	--	--	45.0	67.5	81.0
6.80	25.00	19.69	4	1.94	1.29	186	0.91	4.0	361.1	541.7	75.0	18	33	24	21	20	28	28	--	--	41.7	62.5	75.0
7.00	33.00	22.45	4	1.97	1.33	207	1.10	4.9	368.8	553.2	99.0	27	34	26	22	21	29	29	--	--	55.0	82.5	99.0
7.20	35.00	20.23	4	1.98	1.37	211	1.17	5.1	377.6	566.4	105.0	28	35	26	23	21	29	29	--	--	58.3	87.5	105.0
7.40	35.00	21.88	4	1.98	1.41	211	1.17	4.9	390.6	585.9	105.0	27	35	26	22	21	29	29	--	--	58.3	87.5	105.0
7.60	37.00	21.39	4	1.99	1.45	216	1.23	5.1	399.5	599.2	111.0	29	35	26	23	21	29	30	--	--	61.7	92.5	111.0
7.80	39.00	19.50	4	2.00	1.49	220	1.30	5.3	408.1	612.1	117.0	30	35	26	23	21	29	30	--	--	65.0	97.5	117.0
8.00	41.00	16.60	4	2.00	1.53	224	1.37	5.4	416.4	624.6	123.0	31	35	26	23	22	30	30	--	--	68.3	102.5	123.0
8.20	36.00	18.00	4	1.99	1.57	214	1.20	4.5	438.6	657.9	108.0	26	34	25	22	21	29	30	--	--	60.0	90.0	108.0
8.40	29.00	21.80	4	1.96	1.61	197	0.98	3.4	452.8	679.2	87.0	18	33	24	21	20	27	29	--	--	48.3	72.5	87.0
8.60	22.00	19.47	4	1.93	1.65	177	0.85	2.7	435.3	652.9	66.0	8	32	23	19	18	26	28	--	--	36.7	55.0	66.0
8.80	22.00	20.56	4	1.93	1.69	177	0.85	2.6	440.0	660.0	66.0	7	32	23	19	18	26	28	--	--	36.7	55.0	66.0
9.00	20.00	25.00	4	1.93	1.73	171	0.80	2.4	429.3	644.0	60.0	3	32	22	19	18	25	27	--	--	33.3	50.0	60.0
9.20	26.00	20.47	4	1.95	1.77	189	0.93	2.8	471.7	707.6	78.0	12	33	23	20	19	26	28	--	--	43.3	65.0	78.0
9.40	24.00	22.43	4	1.94	1.81	183	0.89	2.6	465.7	698.6	72.0	9	32	23	19	18	26	28	--	--	40.0	60.0	72.0
9.60	26.00	16.99	4	1.95	1.84	189	0.93	2.7	481.7	722.6	78.0	11	33	23	20	18	26	28	--	--	43.3	65.0	78.0
9.80	30.00	16.67	4	1.96	1.88	199	1.00	2.8	505.4	758.0	90.0	15	33	24	20	19	27	29	--	--	50.0	75.0	90.0
10.00	26.00	15.57	4	1.95	1.92	189	0.93	2.5	490.4	735.6	78.0	10	32	23	19	18	26	28	--	--	43.3	65.0	78.0
10.20	27.00	17.65	4	1.95	1.96	192	0.95	2.5	500.3	750.5	81.0	11	33	23	19	18	26	28	--	--	45.0	67.5	81.0
10.40	33.00	19.76	4	1.97	2.00	207	1.10	3.0	545.1	817.6	99.0	17	33	24	20	19	27	29	--	--	55.0	82.5	99.0
10.60	31.00	14.98	4	1.97	2.04	202	1.03	2.7	534.6	801.9	93.0	14	33	23	20	19	26	29	--	--	51.7	77.5	93.0
10.80	30.00	16.04	4	1.96	2.08	199	1.00	2.5	529.0	793.5	90.0	13	33	23	20	19	26	29	--	--	50.0	75.0	90.0
11.00	30.00	16.67	4	1.96	2.12	199	1.00	2.5	532.9	799.3	90.0	12	33	23	20	19	26	29	--	--	50.0	75.0	90.0
11.20	34.00	17.62	4	1.98	2.16	209	1.13	2.8	576.1	864.1	102.0	16	33	23	20	19	27	29	--	--	56.7	85.0	102.0
11.40	33.00	17.10	4	1.97	2.20	207	1.10	2.6	572.2	858.3	99.0	15	33	23	20	19	26	29	--	--	55.0	82.5	99.0
11.60	31.00	16.58	4	1.97	2.24	202	1.03	2.4	555.0	832.5	93.0	12	33	23	19	18	26	29	--	--	51.7	77.5	93.0
11.80	32.00	20.00	4	1.97	2.28	204	1.07	2.4	569.9	854.9	96.0	13	33	23	20	18	26	29	--	--	53.3	80.0	96.0
12.00	30.00	20.41	4	1.96	2.32	199	1.00	2.2	548.9	823.4	90.0	10	32	23	19	18	26	29	--	--	50.0	75.0	90.0
12.20	24.00	24.00	4	1.94	2.35	183	0.89	1.9	504.3	756.4	72.0	2	31	21	18	17	25	28	--	--	40.0	60.0	72.0
12.40	16.00	4.80	2	1.96	2.39	157	0.70	1.3	410.0	615.0	51.8	--	--	--	--	--	--	--	--	--	--	--	--
12.60	24.00	60.00	3	1.86	2.43	183	--	--	--	--	--	1	31	21	18	17	25	28	--	--	40.0	60.0	72.0
12.80	15.00	37.50	4	1.89	2.47	154	0.67	1.2	395.6	593.4	49.5	--	31	19	15	14	25	27	--	--	25.0	37.5	45.0
13.00	6.00	22.22	2	1.82	2.50	109	0.30	0.4	180.0	270.0	28.8	--	--	--	--	--	--	--	--	--	--	--	--
13.20	5.00	9.43	1	1.46	2.53	101	0.25	0.3	32.5	48.8	7.5	--	--	--	--	--	--	--	--	--	--	--	--
13.40	19.00	47.50	4	1.92	2.57	168	0.78	1.4	455.3	683.0	58.1	--	31	20	16	15	25	27	--	--	31.7	47.5	57.0
13.60	16.00	23.88	2	1.96	2.61	157	0.70	1.2	413.3	619.9	51.8	--	--	--	--	--	--	--	--	--	--	--	--
13.80	13.00	21.67	2	1.93	2.65	145	0.60	1.0	362.8	544.2	46.5	--	--	--	--	--	--	--	--	--	--	--	--
14.00	12.00	17.91	2	1.92	2.69	141	0.57	0.9	342.9	514.3	44.6	--	--	--	--	--	--	--	--	--	--	--	--
14.20	14.00	19.18	2	1.94	2.73	150	0.64	1.0	381.5	572.3	48.2	--	--	--	--	--	--	--	--	--	--	--	--
14.40	12.00	16.44	2	1.92	2.77	141	0.57	0.9	342.9	514.3	44.6	--	--	--	--	--	--	--	--	--	--	--	--
14.60	9.00	22.50	2	1.88	2.80	127	0.45	0.6	270.0	405.0	37.8	--	--	--	--	--	--	--	--	--	--	--	--
14.80	14.00	29.79	2	1.94	2.84	150	0.64	1.0	381.8	572.7	48.2	--	--	--	--	--	--	--	--	--	--	--	--
15.00	17.00	--	3	1.84	2.88	161	--	--	--	--	--	--	31	19	15	14	25	27	--	--	28.3	42.5	51.0

FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
PARAMETRI GEOTECNICI

CPT	4
riferimento	110-2023

Committente:	**Green-go**	U.M.: **kg/cm²**	Data esec.: 01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Pagina: 1	
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Elaborato:	Falda: -2.40 m da p.c.

							NATURA COESIVA					NATURA GRANULARE											
Prof.	qc	qc/fs	zone	γ'	σ'vo	Vs	Cu	OCR	Eu50	Eu25	Mo	Dr	Sc	Ca	Ko	DB	DM	Me	FLs	FLI	E'50	E'25	Mo
m	U.M.			t/m³	U.M.	m/s	U.M.	%	U.M.	U.M.	U.M.	%	(°)	(°)	(°)	(°)	(°)	(°)			U.M.	U.M.	U.M.
0.20	5.00	9.43	1	1.46	0.03	101	0.25	91.9	10.0	15.0	7.5	--	--	--	--	--	--	--	--	--	--	--	--
0.40	7.00	13.21	1	1.46	0.06	115	0.35	58.9	14.0	21.0	10.5	--	--	--	--	--	--	--	--	--	--	--	--
0.60	6.00	5.00	1	1.46	0.09	109	0.30	29.2	12.0	18.0	9.0	--	--	--	--	--	--	--	--	--	--	--	--
0.80	14.00	11.67	2	1.94	0.13	150	0.64	47.3	108.2	162.3	48.2	--	--	--	--	--	--	--	--	--	--	--	--
1.00	11.00	9.17	2	1.91	0.16	137	0.54	27.5	91.2	136.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
1.20	10.00	9.35	2	1.90	0.20	132	0.50	19.4	85.0	127.5	40.0	--	--	--	--	--	--	--	--	--	--	--	--
1.40	13.00	13.98	2	1.93	0.24	145	0.60	19.8	102.8	154.2	46.5	--	--	--	--	--	--	--	--	--	--	--	--
1.60	18.00	16.82	2	1.98	0.28	164	0.75	21.4	127.5	191.3	56.2	--	--	--	--	--	--	--	--	--	--	--	--
1.80	14.00	20.90	2	1.94	0.32	150	0.64	14.8	108.2	162.3	48.2	--	--	--	--	--	--	--	--	--	--	--	--
2.00	9.00	27.27	2	1.88	0.36	127	0.45	8.4	84.9	127.4	37.8	--	--	--	--	--	--	--	--	--	--	--	--
2.20	7.00	25.93	2	1.84	0.39	115	0.35	5.4	107.1	160.7	32.2	--	--	--	--	--	--	--	--	--	--	--	--
2.40	8.00	17.02	2	0.86	0.41	121	0.40	6.1	108.5	162.7	35.2	--	--	--	--	--	--	--	--	--	--	--	--
2.60	4.00	12.12	1	0.46	0.42	93	0.20	2.5	22.3	33.5	6.0	--	--	--	--	--	--	--	--	--	--	--	--
2.80	11.00	27.50	2	0.91	0.44	137	0.54	8.1	105.1	157.6	42.5	--	--	--	--	--	--	--	--	--	--	--	--
3.00	11.00	23.40	2	0.91	0.46	137	0.54	7.7	111.0	166.5	42.5	--	--	--	--	--	--	--	--	--	--	--	--
3.20	14.00	23.33	2	0.94	0.48	150	0.64	9.0	112.8	169.2	48.2	--	--	--	--	--	--	--	--	--	--	--	--
3.40	12.00	22.64	2	0.92	0.49	141	0.57	7.5	120.8	181.2	44.6	--	--	--	--	--	--	--	--	--	--	--	--
3.60	14.00	19.18	2	0.94	0.51	150	0.64	8.2	122.3	183.5	48.2	--	--	--	--	--	--	--	--	--	--	--	--
3.80	11.00	16.42	2	0.91	0.53	137	0.54	6.4	137.9	206.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
4.00	14.00	17.50	2	0.94	0.55	150	0.64	7.5	134.4	201.6	48.2	--	--	--	--	--	--	--	--	--	--	--	--
4.20	12.00	17.91	2	0.92	0.57	141	0.57	6.3	147.9	221.8	44.6	--	--	--	--	--	--	--	--	--	--	--	--
4.40	14.00	23.33	2	0.94	0.59	150	0.64	6.9	147.7	221.6	48.2	--	--	--	--	--	--	--	--	--	--	--	--
4.60	14.00	20.90	2	0.94	0.61	150	0.64	6.7	154.7	232.0	48.2	--	--	--	--	--	--	--	--	--	--	--	--
4.80	13.00	27.66	2	0.93	0.62	145	0.60	6.0	165.0	247.5	46.5	--	--	--	--	--	--	--	--	--	--	--	--
5.00	11.00	23.40	2	0.91	0.64	137	0.54	5.0	177.3	265.9	42.5	--	--	--	--	--	--	--	--	--	--	--	--
5.20	10.00	25.00	2	0.90	0.66	132	0.50	4.4	184.4	276.5	40.0	--	--	--	--	--	--	--	--	--	--	--	--
5.40	13.00	19.40	2	0.93	0.68	145	0.60	5.4	184.6	276.9	46.5	--	--	--	--	--	--	--	--	--	--	--	--
5.60	10.00	16.67	2	0.90	0.70	132	0.50	4.1	194.7	292.0	40.0	--	--	--	--	--	--	--	--	--	--	--	--
5.80	9.00	22.50	2	0.88	0.71	127	0.45	3.5	201.6	302.4	37.8	--	--	--	--	--	--	--	--	--	--	--	--
6.00	11.00	20.75	2	0.91	0.73	137	0.54	4.3	204.7	307.1	42.5	--	--	--	--	--	--	--	--	--	--	--	--
6.20	11.00	12.64	2	0.91	0.75	137	0.54	4.1	209.7	314.6	42.5	--	--	--	--	--	--	--	--	--	--	--	--
6.40	21.00	12.57	4	0.93	0.77	174	0.82	6.8	194.9	292.3	63.0	25	34	26	23	22	30	27	0.84	1.26	35.0	52.5	63.0
6.60	36.00	18.00	4	0.99	0.79	214	1.20	10.6	204.0	306.0	108.0	43	36	29	26	24	33	30	0.99	1.51	60.0	90.0	108.0
6.80	30.00	16.04	4	0.96	0.81	199	1.00	8.2	193.1	289.7	90.0	36	36	28	25	23	31	29	0.92	1.39	50.0	75.0	90.0
7.00	25.00	16.34	4	0.94	0.83	186	0.91	7.1	207.0	310.5	75.0	29	35	27	24	22	30	28	0.86	1.29	41.7	62.5	75.0
7.20	22.00	20.56	4	0.93	0.85	177	0.85	6.3	220.8	331.2	66.0	24	34	26	23	21	29	28	0.81	1.23	36.7	55.0	66.0
7.40	27.00	18.37	4	0.95	0.87	192	0.95	7.0	216.8	325.2	81.0	31	35	27	24	22	30	28	0.86	1.30	45.0	67.5	81.0
7.60	24.00	16.33	4	0.94	0.88	183	0.89	6.3	230.1	345.1	72.0	26	34	26	23	22	30	28	0.82	1.24	40.0	60.0	72.0
7.80	28.00	16.77	4	0.96	0.90	194	0.97	6.8	228.8	343.1	84.0	31	35	27	24	22	30	28	0.85	1.29	46.7	70.0	84.0
8.00	25.00	18.80	4	0.94	0.92	186	0.91	6.2	241.9	362.9	75.0	26	34	26	23	22	30	28	0.82	1.23	41.7	62.5	75.0
8.20	28.00	19.05	4	0.96	0.94	194	0.97	6.5	242.8	364.3	84.0	30	35	27	23	22	30	28	0.84	1.27	46.7	70.0	84.0
8.40	20.00	20.00	4	0.93	0.96	171	0.80	5.0	264.9	397.3	60.0	18	33	25	22	20	28	27	0.76	1.14	33.3	50.0	60.0
8.60	18.00	19.35	2	0.98	0.98	164	0.75	4.5	273.1	409.7	56.2	--	--	--	--	--	--	--	--	--	--	--	--
8.80	14.00	23.33	2	0.94	1.00	150	0.64	3.6	281.7	422.6	48.2	--	--	--	--	--	--	--	--	--	--	--	--
9.00	19.00	15.83	2	0.99	1.02	168	0.78	4.5	284.0	426.0	58.1	--	--	--	--	--	--	--	--	--	--	--	--
9.20	15.00	20.55	2	0.95	1.04	154	0.67	3.6	292.8	439.1	49.5	--	--	--	--	--	--	--	--	--	--	--	--
9.40	18.00	15.93	2	0.98	1.06	164	0.75	4.1	294.9	442.4	56.2	--	--	--	--	--	--	--	--	--	--	--	--
9.60	18.00	15.00	2	0.98	1.08	164	0.75	4.0	300.2	450.2	56.2	--	--	--	--	--	--	--	--	--	--	--	--
9.80	16.00	20.00	2	0.96	1.10	157	0.70	3.6	309.1	463.7	51.8	--	--	--	--	--	--	--	--	--	--	--	--
10.00	21.00	15.00	4	0.93	1.11	174	0.82	4.3	311.1	466.6	63.0	16	33	24	21	20	28	27	0.74	1.12	35.0	52.5	63.0
10.20	21.00	15.79	4	0.93	1.13	174	0.82	4.2	316.3	474.5	63.0	15	33	24	21	20	28	27	0.74	1.12	35.0	52.5	63.0
10.40	20.00	20.00	4	0.93	1.15	171	0.80	4.0	321.3	482.0	60.0	13	33	24	21	19	27	27	0.73	1.11	33.3	50.0	60.0
10.60	15.00	17.24	2	0.95	1.17	154	0.67	3.1	323.0	484.5	49.5	--	--	--	--	--	--	--	--	--	--	--	--
10.80	13.00	24.53	2	0.93	1.19	145	0.60	2.7	312.2	468.3	46.5	--	--	--	--	--	--	--	--	--	--	--	--
11.00	11.00	20.75	2	0.91	1.21	137	0.54	2.3	291.9	437.9	42.5	--	--	--	--	--	--	--	--	--	--	--	--
11.20	13.00	17.81	2	0.93	1.23	145	0.60	2.6	316.5	474.8	46.5	--	--	--	--	--	--	--	--	--	--	--	--
11.40	11.00	16.42	2	0.91	1.24	137	0.54	2.2	294.6	441.9	42.5	--	--	--	--	--	--	--	--	--	--	--	--
11.60	13.00	16.25	2	0.93	1.26	145	0.60	2.5	320.4	480.6	46.5	--	--	--	--	--	--	--	--	--	--	--	--
11.80	18.00	18.00	2	0.98	1.28	164	0.75	3.2	356.8	535.2	56.2	--	--	--	--	--	--	--	--	--	--	--	--
12.00	25.00	19.69	4	0.94	1.30	186	0.91	4.0	362.8	544.2	75.0	18	33	24	21	20	28	28	0.78	1.17	41.7	62.5	75.0
12.20	26.00	17.69	4	0.95	1.32	189	0.93	4.0	368.2	552.4	78.0	19	34	25	21	20	28	28	0.79	1.19	43.3	65.0	78.0
12.40	22.00	19.47	4	0.93	1.34	177	0.85	3.5	377.6	566.5	66.0	13	33	24	20	19	27	28	0.76	1.14	36.7	55.0	66.0
12.60	19.00	19.00	2	0.99	1.36	168	0.78	3.1	375.2	562.9	58.1	--	--	--	--	--	--	--	--	--	--	--	--
12.80	16.00	20.00	2	0.96	1.38	157	0.70	2.7	360.4	540.6	51.8	--	--	--	--	--	--	--	--	--	--	--	--
13.00	15.00	18.75	2	0.95	1.40	154	0.67	2.5	353.7	530.6	49.5	--	--	--	--	--	--	--	--	--	--	--	--
13.20	14.00	19.18	2	0.94	1.42	150	0.64	2.3	345.0	517.4	48.2	--	--	--	--	--	--	--	--	--	--	--	--
13.40	15.00	15.00	2	0.95	1.43	154	0.67	2.4	357.3	535.9	49.5	--	--	--	--	--	--	--	--	--	--	--	--
13.60	15.00	18.75	2	0.95	1.45	154	0.67	2.4	358.9	538.4	49.5	--	--	--	--	--	--	--	--	--	--	--	--
13.80	15.00	25.00	2	0.95	1.47	154	0.67	2.3	360.5	540.8	49.5	--	--	--	--	--	--	--	--	--	--	--	--
14.00	12.00	20.00	2	0.92	1.49	141	0.57	1.9	323.1	484.7	44.6	--	--	--	--	--	--	--	--	--	--	--	--
14.20	16.00	20.00	2	0.96	1.51	157	0.70	2.4	374.0	561.0	51.8	--	--	--	--	--	--	--	--	--	--	--	--
14.40	21.00	19.63	4	0.93	1.53	174	0.82	2.9	412.9	619.3	63.0	8	32	23	19	18	26	27	0.77	1.16	35.0	52.5	63.0
14.60	15.00	16.13	2	0.95	1.55	154	0.67	2.2	366.2	549.3	49.5	--	--	--	--	--	--	--	--	--	--	--	--
14.80	19.00	20.43	2	0.99	1.57	168	0.78	2.6	405.4	608.2	58.1	--	--	--	--	--	--	--	--	--	--	--	--
15.00	17.00	--	3	0.84	1.58	161	--	--	--	--	--	--	31	22	18	17	25	27	0.74	1.13	28.3	42.5	51.0

FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
PARAMETRI GEOTECNICI

CPT	5
riferimento	110-2023

Committente:	**Green-go**	U.M.: **kg/cm²**	Data esec.: 01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Pagina: 1	
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Elaborato:	Falda: -2.20 m da p.c.

							NATURA COESIVA					NATURA GRANULARE											
Prof.	qc	qc/fs	zone	γ'	σ'vo	Vs	Cu	OCR	Eu50	Eu25	Mo	Dr	Sc	Ca	Ko	DB	DM	Me	FLs	FLI	E'50	E'25	Mo
m	U.M.			t/m³	U.M.	m/s	U.M.	%	U.M.	U.M.	U.M.	%	(°)	(°)	(°)	(°)	(°)	(°)			U.M.	U.M.	U.M.
0.20	7.00	9.59	1	1.46	0.03	115	0.35	99.9	14.0	21.0	10.5	--	--	--	--	--	--	--	--	--	--	--	--
0.40	5.00	15.15	2	1.80	0.07	101	0.25	33.7	42.5	63.8	25.0	--	--	--	--	--	--	--	--	--	--	--	--
0.60	12.00	15.00	2	1.92	0.10	141	0.57	53.1	97.1	145.7	44.6	--	--	--	--	--	--	--	--	--	--	--	--
0.80	10.00	10.75	2	1.90	0.14	132	0.50	30.4	85.0	127.5	40.0	--	--	--	--	--	--	--	--	--	--	--	--
1.00	9.00	10.34	2	1.88	0.18	127	0.45	19.8	76.5	114.8	37.8	--	--	--	--	--	--	--	--	--	--	--	--
1.20	11.00	11.00	2	1.91	0.22	137	0.54	19.4	91.2	136.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
1.40	31.00	22.14	4	1.97	0.26	202	1.03	35.8	175.7	263.5	93.0	65	39	34	31	29	38	29	--	--	51.7	77.5	93.0
1.60	41.00	13.67	4	2.00	0.30	224	1.37	42.4	232.3	348.5	123.0	71	40	34	31	29	39	30	--	--	68.3	102.5	123.0
1.80	32.00	10.67	4	1.97	0.34	204	1.07	26.6	181.3	272.0	96.0	59	38	32	29	28	37	29	--	--	53.3	80.0	96.0
2.00	33.00	11.79	4	1.97	0.38	207	1.10	24.1	187.0	280.5	99.0	58	38	32	29	27	36	29	--	--	55.0	82.5	99.0
2.20	19.00	11.38	2	0.99	0.40	168	0.78	14.6	131.8	197.8	58.1	--	--	--	--	--	--	--	--	--	--	--	--
2.40	17.00	14.17	2	0.97	0.41	161	0.72	12.6	123.0	184.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
2.60	19.00	12.93	2	0.99	0.43	168	0.78	12.9	131.8	197.8	58.1	--	--	--	--	--	--	--	--	--	--	--	--
2.80	24.00	16.33	4	0.94	0.45	183	0.89	14.6	151.1	226.7	72.0	42	36	29	26	25	33	28	1.29	1.95	40.0	60.0	72.0
3.00	22.00	20.56	⚠ 4	0.93	0.47	177	0.85	13.0	143.8	215.8	66.0	38	36	29	26	24	33	28	1.20	1.81	36.7	55.0	66.0
3.20	18.00	19.35	2	0.98	0.49	164	0.75	10.6	127.5	191.3	56.2	--	--	--	--	--	--	--	--	--	--	--	--
3.40	14.00	20.90	2	0.94	0.51	150	0.64	8.3	121.7	182.5	48.2	--	--	--	--	--	--	--	--	--	--	--	--
3.60	11.00	18.33	2	0.91	0.53	137	0.54	6.4	137.0	205.6	42.5	--	--	--	--	--	--	--	--	--	--	--	--
3.80	5.00	12.50	1	0.46	0.54	101	0.25	2.4	28.3	42.4	7.5	--	--	--	--	--	--	--	--	--	--	--	--
4.00	6.00	22.22	2	0.82	0.55	109	0.30	2.9	150.0	225.0	28.8	--	--	--	--	--	--	--	--	--	--	--	--
4.20	9.00	19.15	2	0.88	0.57	127	0.45	4.7	159.1	238.7	37.8	--	--	--	--	--	--	--	--	--	--	--	--
4.40	11.00	20.75	2	0.91	0.59	137	0.54	5.6	159.4	239.1	42.5	--	--	--	--	--	--	--	--	--	--	--	--
4.60	9.00	19.15	2	0.88	0.61	127	0.45	4.3	169.7	254.6	37.8	--	--	--	--	--	--	--	--	--	--	--	--
4.80	15.00	28.30	2	0.95	0.63	154	0.67	6.8	159.1	238.6	49.5	--	--	--	--	--	--	--	--	--	--	--	--
5.00	16.00	12.03	2	0.96	0.65	157	0.70	6.9	163.0	244.5	51.8	--	--	--	--	--	--	--	--	--	--	--	--
5.20	24.00	45.28	⚠ 3	0.86	0.66	183	--	--	--	--	--	33	35	28	24	23	31	28	0.93	1.41	40.0	60.0	72.0
5.40	18.00	24.66	2	0.98	0.68	164	0.75	7.1	170.8	256.1	56.2	--	--	--	--	--	--	--	--	--	--	--	--
5.60	31.00	38.75	⚠ 3	0.88	0.70	202	--	--	--	--	--	40	36	29	26	24	32	29	0.99	1.50	51.7	77.5	93.0
5.80	36.00	25.71	⚠ 4	0.99	0.72	214	1.20	11.9	204.0	306.0	108.0	45	37	29	26	25	33	30	1.02	1.57	60.0	90.0	108.0
6.00	18.00	20.69	2	0.98	0.74	164	0.75	6.4	191.7	287.6	56.2	--	--	--	--	--	--	--	--	--	--	--	--
6.20	18.00	26.87	2	0.98	0.76	164	0.75	6.2	199.0	298.5	56.2	--	--	--	--	--	--	--	--	--	--	--	--
6.40	16.00	18.39	2	0.96	0.78	157	0.70	5.5	211.3	316.9	51.8	--	--	--	--	--	--	--	--	--	--	--	--
6.60	19.00	14.96	2	0.99	0.80	168	0.78	6.1	210.6	315.9	58.1	--	--	--	--	--	--	--	--	--	--	--	--
6.80	22.00	13.75	⚠ 4	0.93	0.82	177	0.85	6.6	209.8	314.7	66.0	25	34	26	23	22	30	28	0.82	1.23	36.7	55.0	66.0
7.00	21.00	12.14	⚠ 4	0.93	0.84	174	0.82	6.2	219.2	328.8	63.0	23	34	26	23	21	29	27	0.80	1.21	35.0	52.5	63.0
7.20	21.00	11.67	⚠ 4	0.93	0.85	174	0.82	6.0	226.0	339.0	63.0	22	34	26	22	21	29	27	0.79	1.19	35.0	52.5	63.0
7.40	23.00	12.30	⚠ 4	0.94	0.87	180	0.87	6.2	228.2	342.2	69.0	25	34	26	23	21	30	28	0.81	1.22	38.3	57.5	69.0
7.60	23.00	17.29	⚠ 4	0.94	0.89	180	0.87	6.1	235.1	352.6	69.0	24	34	26	23	21	29	28	0.80	1.21	38.3	57.5	69.0
7.80	23.00	13.29	⚠ 4	0.94	0.91	180	0.87	5.9	241.9	362.8	69.0	24	34	26	23	21	29	28	0.79	1.20	38.3	57.5	69.0
8.00	16.00	8.89	2	0.96	0.93	157	0.70	4.4	259.5	389.2	51.8	--	--	--	--	--	--	--	--	--	--	--	--
8.20	25.00	14.97	⚠ 4	0.94	0.95	186	0.91	6.0	251.5	377.3	75.0	26	34	26	23	21	30	28	0.80	1.21	41.7	62.5	75.0
8.40	30.00	13.64	⚠ 4	0.96	0.97	199	1.00	6.5	248.8	373.1	90.0	31	35	27	24	22	30	29	0.84	1.27	50.0	75.0	90.0
8.60	24.00	11.27	⚠ 4	0.94	0.99	183	0.89	5.5	267.1	400.6	72.0	23	34	26	22	21	29	28	0.78	1.18	40.0	60.0	72.0
8.80	34.00	13.77	⚠ 4	0.98	1.01	209	1.13	7.3	248.7	373.1	102.0	35	35	27	24	23	31	29	0.87	1.31	56.7	85.0	102.0
9.00	36.00	14.57	⚠ 4	0.99	1.03	214	1.20	7.6	249.5	374.3	108.0	36	36	27	24	23	31	30	0.88	1.33	60.0	90.0	108.0
9.20	35.00	15.91	⚠ 4	0.98	1.05	211	1.17	7.2	259.5	389.3	105.0	35	35	27	24	23	31	29	0.87	1.31	58.3	87.5	105.0
9.40	33.00	14.54	⚠ 4	0.97	1.06	207	1.10	6.5	273.8	410.7	99.0	32	35	27	24	22	30	29	0.85	1.28	55.0	82.5	99.0
9.60	33.00	14.16	⚠ 4	0.97	1.08	207	1.10	6.4	281.0	421.6	99.0	32	35	27	24	22	30	29	0.84	1.28	55.0	82.5	99.0
9.80	30.00	15.54	⚠ 4	0.96	1.10	199	1.00	5.6	298.3	447.5	90.0	28	35	26	23	22	30	29	0.82	1.23	50.0	75.0	90.0
10.00	19.00	11.38	2	0.99	1.12	168	0.78	4.0	314.2	471.2	58.1	--	--	--	--	--	--	--	--	--	--	--	--
10.20	22.00	12.72	⚠ 4	0.93	1.14	177	0.85	4.3	318.9	478.3	66.0	17	33	24	21	20	28	28	0.75	1.12	36.7	55.0	66.0
10.40	20.00	11.11	⚠ 4	0.93	1.16	171	0.80	3.9	324.7	487.1	60.0	13	33	24	21	19	27	27	0.73	1.10	33.3	50.0	60.0
10.60	22.00	11.00	⚠ 4	0.93	1.18	177	0.85	4.1	329.2	493.8	66.0	16	33	24	21	20	28	28	0.75	1.12	36.7	55.0	66.0
10.80	24.00	12.83	⚠ 4	0.94	1.20	183	0.89	4.3	334.5	501.8	72.0	19	33	25	21	20	28	28	0.76	1.15	40.0	60.0	72.0
11.00	22.00	11.76	⚠ 4	0.93	1.22	177	0.85	4.0	339.5	509.3	66.0	15	33	24	21	20	27	28	0.75	1.12	36.7	55.0	66.0
11.20	25.00	12.95	⚠ 4	0.94	1.24	186	0.91	4.3	345.0	517.6	75.0	19	34	25	21	20	28	28	0.77	1.16	41.7	62.5	75.0
11.40	31.00	12.55	⚠ 4	0.97	1.25	202	1.03	4.9	347.0	520.5	93.0	26	34	26	22	21	29	29	0.82	1.24	51.7	77.5	93.0
11.60	37.00	14.23	⚠ 4	0.99	1.27	216	1.23	6.0	336.9	505.3	111.0	32	35	27	23	22	30	30	0.87	1.32	61.7	92.5	111.0
11.80	38.00	--	⚠ 3	0.90	1.29	218	--	--	--	--	--	32	35	27	23	22	30	30	0.88	1.33	63.3	95.0	114.0

FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
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PROVA PENETROMETRICA STATICA MECCANICA
PARAMETRI GEOTECNICI

CPT	6
riferimento	110-2023

Committente:	**Green-go**	U.M.: **kg/cm²**	Data esec.: 01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Pagina: 1	
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Elaborato:	Falda: Non rilevata

							NATURA COESIVA					NATURA GRANULARE											
Prof.	qc	qc/fs	zone	γ'	σ'vo	Vs	Cu	OCR	Eu50	Eu25	Mo	Dr	Sc	Ca	Ko	DB	DM	Me	FLs	FLl	E'50	E'25	Mo
m	U.M.			t/m³	U.M.	m/s	U.M.	%	U.M.	U.M.	U.M.	%	(°)	(°)	(°)	(°)	(°)	(°)			U.M.	U.M.	U.M.
0.20	4.00	12.12	1	1.46	0.03	93	0.20	69.6	8.0	12.0	6.0	--	--	--	--	--	--	--	--	--	--	--	--
0.40	4.00	10.00	1	1.46	0.06	93	0.20	29.2	8.0	12.0	6.0	--	--	--	--	--	--	--	--	--	--	--	--
0.60	5.00	9.43	1	1.46	0.09	101	0.25	23.3	10.0	15.0	7.5	--	--	--	--	--	--	--	--	--	--	--	--
0.80	13.00	21.67	2	1.93	0.13	145	0.60	44.5	102.8	154.2	46.5	--	--	--	--	--	--	--	--	--	--	--	--
1.00	14.00	5.67	2	1.94	0.17	150	0.64	33.9	108.2	162.3	48.2	--	--	--	--	--	--	--	--	--	--	--	--
1.20	13.00	6.95	2	1.93	0.20	145	0.60	24.5	102.8	154.2	46.5	--	--	--	--	--	--	--	--	--	--	--	--
1.40	14.00	11.67	2	1.94	0.24	150	0.64	21.0	108.2	162.3	48.2	--	--	--	--	--	--	--	--	--	--	--	--
1.60	18.00	15.00	2	1.98	0.28	164	0.75	21.3	127.5	191.3	56.2	--	--	--	--	--	--	--	--	--	--	--	--
1.80	19.00	17.76	2	1.99	0.32	168	0.78	18.9	131.8	197.8	58.1	--	--	--	--	--	--	--	--	--	--	--	--
2.00	16.00	20.00	2	1.96	0.36	157	0.70	14.3	118.3	177.4	51.8	--	--	--	--	--	--	--	--	--	--	--	--
2.20	17.00	18.28	2	1.97	0.40	161	0.72	13.2	123.0	184.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
2.40	12.00	16.44	2	1.92	0.44	141	0.57	8.7	103.9	155.9	44.6	--	--	--	--	--	--	--	--	--	--	--	--
2.60	10.00	21.28	2	1.90	0.48	132	0.50	6.7	121.8	182.7	40.0	--	--	--	--	--	--	--	--	--	--	--	--
2.80	11.00	20.75	2	1.91	0.52	137	0.54	6.6	132.0	197.9	42.5	--	--	--	--	--	--	--	--	--	--	--	--
3.00	10.00	25.00	2	1.90	0.55	132	0.50	5.5	149.6	224.4	40.0	--	--	--	--	--	--	--	--	--	--	--	--
3.20	9.00	19.15	2	1.88	0.59	127	0.45	4.5	164.8	247.2	37.8	--	--	--	--	--	--	--	--	--	--	--	--
3.40	11.00	23.40	2	1.91	0.63	137	0.54	5.1	172.7	259.1	42.5	--	--	--	--	--	--	--	--	--	--	--	--
3.60	11.00	18.33	2	1.91	0.67	137	0.54	4.8	185.1	277.7	42.5	--	--	--	--	--	--	--	--	--	--	--	--
3.80	12.00	20.00	2	1.92	0.71	141	0.57	4.8	195.6	293.4	44.6	--	--	--	--	--	--	--	--	--	--	--	--
4.00	11.00	16.42	2	1.91	0.74	137	0.54	4.2	207.7	311.5	42.5	--	--	--	--	--	--	--	--	--	--	--	--
4.20	11.00	23.40	2	1.91	0.78	137	0.54	3.9	219.0	328.6	42.5	--	--	--	--	--	--	--	--	--	--	--	--
4.40	13.00	21.67	2	1.93	0.82	145	0.60	4.3	229.1	343.7	46.5	--	--	--	--	--	--	--	--	--	--	--	--
4.60	14.00	20.90	2	1.94	0.86	150	0.64	4.3	240.0	359.9	48.2	--	--	--	--	--	--	--	--	--	--	--	--
4.80	11.00	18.33	2	1.91	0.90	137	0.54	3.3	251.1	376.7	42.5	--	--	--	--	--	--	--	--	--	--	--	--
5.00	17.00	21.25	2	1.97	0.94	161	0.72	4.5	261.1	391.7	54.1	--	--	--	--	--	--	--	--	--	--	--	--
5.20	18.00	38.30	4	1.91	0.98	164	0.75	4.5	271.8	407.8	56.2	14	33	24	21	20	28	27	--	--	30.0	45.0	54.0
5.40	10.00	21.28	2	1.90	1.01	132	0.50	2.6	261.7	392.5	40.0	--	--	--	--	--	--	--	--	--	--	--	--
5.60	9.00	27.27	2	1.88	1.05	127	0.45	2.2	247.6	371.4	37.8	--	--	--	--	--	--	--	--	--	--	--	--
5.80	12.00	17.91	2	1.92	1.09	141	0.57	2.8	290.6	435.9	44.6	--	--	--	--	--	--	--	--	--	--	--	--
6.00	9.00	19.15	2	1.88	1.13	127	0.45	2.0	252.2	378.2	37.8	--	--	--	--	--	--	--	--	--	--	--	--
6.20	11.00	20.75	2	1.91	1.16	137	0.54	2.4	288.5	432.7	42.5	--	--	--	--	--	--	--	--	--	--	--	--
6.40	11.00	33.33	4	1.87	1.20	137	0.54	2.3	291.6	437.4	42.5	--	31	21	17	16	25	26	--	--	18.3	27.5	33.0
6.60	11.00	18.33	2	1.91	1.24	137	0.54	2.2	294.4	441.6	42.5	--	--	--	--	--	--	--	--	--	--	--	--
6.80	13.00	21.67	2	1.93	1.28	145	0.60	2.5	322.0	483.0	46.5	--	--	--	--	--	--	--	--	--	--	--	--
7.00	15.00	18.75	2	1.95	1.32	154	0.67	2.7	345.1	517.7	49.5	--	--	--	--	--	--	--	--	--	--	--	--
7.20	15.00	28.30	2	1.95	1.36	154	0.67	2.6	349.6	524.4	49.5	--	--	--	--	--	--	--	--	--	--	--	--
7.40	16.00	30.19	4	1.90	1.40	157	0.70	2.6	362.5	543.7	51.8	1	31	22	18	18	25	27	--	--	26.7	40.0	48.0
7.60	15.00	28.30	2	1.95	1.43	154	0.67	2.4	357.3	535.9	49.5	--	--	--	--	--	--	--	--	--	--	--	--
7.80	14.00	17.50	2	1.94	1.47	150	0.64	2.2	349.3	523.9	48.2	--	--	--	--	--	--	--	--	--	--	--	--
8.00	12.00	17.91	2	1.92	1.51	141	0.57	1.9	324.1	486.1	44.6	--	--	--	--	--	--	--	--	--	--	--	--
8.20	16.00	18.39	2	1.96	1.55	157	0.70	2.3	377.4	566.0	51.8	--	--	--	--	--	--	--	--	--	--	--	--
8.40	23.00	17.29	4	1.94	1.59	180	0.87	2.9	431.8	647.6	69.0	10	32	23	20	19	26	28	--	--	38.3	57.5	69.0
8.60	20.00	17.70	4	1.93	1.63	171	0.80	2.6	419.5	629.2	60.0	5	32	22	19	18	25	27	--	--	33.3	50.0	60.0
8.80	22.00	19.47	4	1.93	1.67	177	0.85	2.7	437.3	655.9	66.0	7	32	23	19	18	26	28	--	--	36.7	55.0	66.0
9.00	20.00	16.67	4	1.93	1.70	171	0.80	2.4	427.2	640.9	60.0	4	32	22	19	18	25	27	--	--	33.3	50.0	60.0
9.20	25.00	15.63	4	1.94	1.74	186	0.91	2.8	463.8	695.7	75.0	11	33	23	20	19	26	28	--	--	41.7	62.5	75.0
9.40	26.00	19.55	4	1.95	1.78	189	0.93	2.8	474.0	710.9	78.0	12	33	23	20	19	26	28	--	--	43.3	65.0	78.0
9.60	20.00	18.69	4	1.93	1.82	171	0.80	2.2	436.9	655.3	60.0	2	31	22	18	17	25	27	--	--	33.3	50.0	60.0
9.80	18.00	24.66	2	1.98	1.86	164	0.75	2.0	419.3	629.0	56.2	--	--	--	--	--	--	--	--	--	--	--	--
10.00	15.00	20.55	2	1.95	1.90	154	0.67	1.7	383.3	575.0	49.5	--	--	--	--	--	--	--	--	--	--	--	--
10.20	21.00	15.79	4	1.93	1.94	174	0.82	2.2	454.2	681.3	63.0	2	32	22	18	17	25	27	--	--	35.0	52.5	63.0
10.40	23.00	15.65	4	1.94	1.98	180	0.87	2.2	474.1	711.1	69.0	5	32	22	19	18	25	28	--	--	38.3	57.5	69.0
10.60	23.00	14.38	4	1.94	2.02	180	0.87	2.2	476.8	715.3	69.0	4	32	22	18	17	25	28	--	--	38.3	57.5	69.0
10.80	27.00	18.37	4	1.95	2.05	192	0.95	2.4	509.2	763.8	81.0	9	32	23	19	18	26	28	--	--	45.0	67.5	81.0
11.00	34.00	15.45	4	1.98	2.09	209	1.13	2.9	566.8	850.2	102.0	17	33	24	20	19	27	29	--	--	56.7	85.0	102.0
11.20	37.00	16.30	4	1.99	2.13	216	1.23	3.2	591.9	887.8	111.0	19	34	24	21	19	27	30	--	--	61.7	92.5	111.0
11.40	36.00	17.39	4	1.99	2.17	214	1.20	3.0	593.2	889.8	108.0	18	33	24	20	19	27	30	--	--	60.0	90.0	108.0
11.60	37.00	15.88	4	1.99	2.21	216	1.23	3.0	606.3	909.4	111.0	18	33	24	20	19	27	30	--	--	61.7	92.5	111.0
11.80	35.00	18.13	4	1.98	2.25	211	1.17	2.8	597.3	895.9	105.0	16	33	23	20	19	27	29	--	--	58.3	87.5	105.0
12.00	36.00	--	3	1.89	2.29	214	--	--	--	--	--	17	33	23	20	19	27	30	--	--	60.0	90.0	108.0

FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
PARAMETRI GEOTECNICI

CPT	7
riferimento	110-2023

Committente:	**Green-go**	U.M.: **kg/cm²**	Data esec.: 01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Pagina: 1	
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Elaborato:	Falda: Non rilevata

							NATURA COESIVA					NATURA GRANULARE											
Prof.	qc	qc/fs	zone	γ'	σ'vo	Vs	Cu	OCR	Eu50	Eu25	Mo	Dr	Sc	Ca	Ko	DB	DM	Me	FLs	FLl	E'50	E'25	Mo
m	U.M.			t/m³	U.M.	m/s	U.M.	%	U.M.	U.M.	U.M.	%	(°)	(°)	(°)	(°)	(°)	(°)			U.M.	U.M.	U.M.
0.20	4.00	14.81	1	1.46	0.03	93	0.20	69.6	8.0	12.0	6.0	--	--	--	--	--	--	--	--	--	--	--	--
0.40	4.00	7.55	1	1.46	0.06	93	0.20	29.2	8.0	12.0	6.0	--	--	--	--	--	--	--	--	--	--	--	--
0.60	9.00	9.00	2	1.88	0.10	127	0.45	43.3	76.5	114.8	37.8	--	--	--	--	--	--	--	--	--	--	--	--
0.80	9.00	9.68	2	1.88	0.13	127	0.45	28.6	76.5	114.8	37.8	--	--	--	--	--	--	--	--	--	--	--	--
1.00	17.00	21.25	2	1.97	0.17	161	0.72	37.5	123.0	184.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
1.20	16.00	16.00	2	1.96	0.21	157	0.70	27.7	118.3	177.4	51.8	--	--	--	--	--	--	--	--	--	--	--	--
1.40	16.00	12.60	2	1.96	0.25	157	0.70	22.4	118.3	177.4	51.8	--	--	--	--	--	--	--	--	--	--	--	--
1.60	24.00	12.44	4	1.94	0.29	183	0.89	25.4	151.1	226.7	72.0	53	38	32	29	27	36	28	--	--	40.0	60.0	72.0
1.80	20.00	11.11	4	1.93	0.33	171	0.80	19.1	136.0	204.0	60.0	44	37	30	27	25	34	27	--	--	33.3	50.0	60.0
2.00	19.00	12.42	2	1.99	0.37	168	0.78	15.9	131.8	197.8	58.1	--	--	--	--	--	--	--	--	--	--	--	--
2.20	17.00	11.11	2	1.97	0.41	161	0.72	12.8	123.0	184.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
2.40	15.00	10.71	2	1.95	0.45	154	0.67	10.4	113.3	170.0	49.5	--	--	--	--	--	--	--	--	--	--	--	--
2.60	15.00	10.71	2	1.95	0.49	154	0.67	9.3	116.0	173.9	49.5	--	--	--	--	--	--	--	--	--	--	--	--
2.80	17.00	12.78	2	1.97	0.53	161	0.72	9.4	125.5	188.3	54.1	--	--	--	--	--	--	--	--	--	--	--	--
3.00	22.00	13.75	4	1.93	0.56	177	0.85	10.4	143.8	215.8	66.0	34	35	28	25	23	32	28	--	--	36.7	55.0	66.0
3.20	19.00	14.96	2	1.99	0.60	168	0.78	8.6	143.2	214.7	58.1	--	--	--	--	--	--	--	--	--	--	--	--
3.40	17.00	15.04	2	1.97	0.64	161	0.72	7.3	159.2	238.8	54.1	--	--	--	--	--	--	--	--	--	--	--	--
3.60	11.00	12.64	2	1.91	0.68	137	0.54	4.7	189.6	284.4	42.5	--	--	--	--	--	--	--	--	--	--	--	--
3.80	15.00	15.00	2	1.95	0.72	154	0.67	5.7	193.5	290.2	49.5	--	--	--	--	--	--	--	--	--	--	--	--
4.00	19.00	15.83	2	1.99	0.76	168	0.78	6.4	196.6	294.9	58.1	--	--	--	--	--	--	--	--	--	--	--	--
4.20	22.00	17.32	4	1.93	0.80	177	0.85	6.7	203.2	304.8	66.0	25	34	26	23	22	30	28	--	--	36.7	55.0	66.0
4.40	21.00	15.79	4	1.93	0.84	174	0.82	6.1	220.0	330.0	63.0	23	34	26	23	21	29	27	--	--	35.0	52.5	63.0
4.60	15.00	14.02	2	1.95	0.88	154	0.67	4.5	244.6	366.8	49.5	--	--	--	--	--	--	--	--	--	--	--	--
4.80	18.00	15.00	2	1.98	0.92	164	0.75	4.9	253.6	380.4	56.2	--	--	--	--	--	--	--	--	--	--	--	--
5.00	25.00	15.63	4	1.94	0.96	186	0.91	5.9	254.0	381.0	75.0	25	34	26	23	21	29	28	--	--	41.7	62.5	75.0
5.20	22.00	15.71	4	1.93	0.99	177	0.85	5.1	273.1	409.6	66.0	20	34	25	22	21	29	28	--	--	36.7	55.0	66.0
5.40	27.00	16.88	4	1.95	1.03	192	0.95	5.6	278.2	417.3	81.0	26	34	26	23	21	29	28	--	--	45.0	67.5	81.0
5.60	23.00	15.03	4	1.94	1.07	180	0.87	4.8	297.1	445.6	69.0	20	34	25	22	20	28	28	--	--	38.3	57.5	69.0
5.80	18.00	14.17	2	1.98	1.11	164	0.75	3.8	312.4	468.6	56.2	--	--	--	--	--	--	--	--	--	--	--	--
6.00	17.00	12.78	2	1.97	1.15	161	0.72	3.5	324.5	486.7	54.1	--	--	--	--	--	--	--	--	--	--	--	--
6.20	15.00	13.27	2	1.95	1.19	154	0.67	3.0	326.5	489.7	49.5	--	--	--	--	--	--	--	--	--	--	--	--
6.40	22.00	13.17	4	1.93	1.23	177	0.85	3.9	343.7	515.6	66.0	15	33	24	21	20	27	28	--	--	36.7	55.0	66.0
6.60	23.00	14.38	4	1.94	1.27	180	0.87	3.9	355.1	532.6	69.0	16	33	24	21	20	27	28	--	--	38.3	57.5	69.0
6.80	30.00	14.49	4	1.96	1.31	199	1.00	4.5	364.2	546.4	90.0	24	34	25	22	21	29	29	--	--	50.0	75.0	90.0
7.00	30.00	14.08	4	1.96	1.35	199	1.00	4.3	375.7	563.5	90.0	23	34	25	22	21	29	29	--	--	50.0	75.0	90.0
7.20	27.00	13.04	4	1.95	1.38	192	0.95	3.9	388.1	582.2	81.0	19	34	25	21	20	28	28	--	--	45.0	67.5	81.0
7.40	25.00	12.08	4	1.94	1.42	186	0.91	3.6	401.7	602.6	75.0	16	33	24	21	20	27	28	--	--	41.7	62.5	75.0
7.60	28.00	13.53	4	1.96	1.46	194	0.97	3.7	412.4	618.6	84.0	19	34	24	21	20	28	28	--	--	46.7	70.0	84.0
7.80	33.00	15.94	4	1.97	1.50	207	1.10	4.3	419.4	629.2	99.0	24	34	25	22	21	29	29	--	--	55.0	82.5	99.0
8.00	32.00	12.65	4	1.97	1.54	204	1.07	4.0	430.8	646.2	96.0	22	34	25	22	20	28	29	--	--	53.3	80.0	96.0
8.20	26.00	15.57	4	1.95	1.58	189	0.93	3.2	440.3	660.5	78.0	15	33	24	20	19	27	28	--	--	43.3	65.0	78.0
8.40	32.00	15.02	4	1.97	1.62	204	1.07	3.7	456.8	685.2	96.0	21	34	25	21	20	28	29	--	--	53.3	80.0	96.0
8.60	35.00	18.13	4	1.98	1.66	211	1.17	4.0	462.9	694.4	105.0	24	34	25	22	20	28	29	--	--	58.3	87.5	105.0
8.80	36.00	16.90	4	1.99	1.70	214	1.20	4.1	474.1	711.1	108.0	24	34	25	22	20	28	30	--	--	60.0	90.0	108.0
9.00	41.00	17.60	4	2.00	1.74	224	1.37	4.6	483.9	725.8	123.0	28	35	25	22	21	29	30	--	--	68.3	102.5	123.0
9.20	32.00	15.02	4	1.97	1.78	204	1.07	3.3	498.0	747.0	96.0	19	34	24	21	20	27	29	--	--	53.3	80.0	96.0
9.40	17.00	14.17	2	1.97	1.82	161	0.72	2.0	405.7	608.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
9.60	18.00	16.82	2	1.98	1.86	164	0.75	2.0	419.1	628.7	56.2	--	--	--	--	--	--	--	--	--	--	--	--
9.80	18.00	15.00	2	1.98	1.90	164	0.75	2.0	421.2	631.9	56.2	--	--	--	--	--	--	--	--	--	--	--	--
10.00	27.00	19.29	4	1.95	1.94	192	0.95	2.6	497.6	746.4	81.0	11	33	23	20	18	26	28	--	--	45.0	67.5	81.0
10.20	26.00	19.55	4	1.95	1.97	189	0.93	2.4	495.5	743.3	78.0	9	32	23	19	18	26	28	--	--	43.3	65.0	78.0
10.40	23.00	15.65	4	1.94	2.01	180	0.87	2.2	476.7	715.0	69.0	4	32	22	18	17	25	28	--	--	38.3	57.5	69.0
10.60	32.00	15.02	4	1.97	2.05	204	1.07	2.8	545.1	817.7	96.0	15	33	23	20	19	27	29	--	--	53.3	80.0	96.0
10.80	27.00	13.04	4	1.95	2.09	192	0.95	2.3	512.3	768.5	81.0	9	32	22	19	18	26	28	--	--	45.0	67.5	81.0
11.00	25.00	22.12	4	1.94	2.13	186	0.91	2.2	500.8	751.1	75.0	6	32	22	19	18	25	28	--	--	41.7	62.5	75.0
11.20	29.00	15.03	4	1.96	2.17	197	0.98	2.3	531.6	797.3	87.0	11	33	23	19	18	26	29	--	--	48.3	72.5	87.0
11.40	36.00	15.00	4	1.99	2.21	214	1.20	2.9	598.9	898.4	108.0	18	33	24	20	19	27	30	--	--	60.0	90.0	108.0
11.60	39.00	15.42	4	2.00	2.25	220	1.30	3.2	623.9	935.8	117.0	20	34	24	21	19	27	30	--	--	65.0	97.5	117.0
11.80	35.00	13.11	4	1.98	2.29	211	1.17	2.7	601.8	902.8	105.0	16	33	23	20	19	26	29	--	--	58.3	87.5	105.0
12.00	35.00	15.91	4	1.98	2.33	211	1.17	2.6	606.6	909.9	105.0	15	33	23	20	19	26	29	--	--	58.3	87.5	105.0
12.20	32.00	14.10	4	1.97	2.37	204	1.07	2.3	577.9	866.8	96.0	12	33	23	19	18	26	29	--	--	53.3	80.0	96.0
12.40	32.00	11.99	4	1.97	2.41	204	1.07	2.3	581.0	871.4	96.0	11	33	23	19	18	26	29	--	--	53.3	80.0	96.0
12.60	25.00	14.45	4	1.94	2.45	186	0.91	1.8	517.4	776.0	75.0	3	32	21	18	17	25	28	--	--	41.7	62.5	75.0
12.80	21.00	14.29	4	1.93	2.48	174	0.82	1.6	477.7	716.6	63.0	--	31	20	17	16	25	27	--	--	35.0	52.5	63.0
13.00	19.00	15.83	2	1.99	2.52	168	0.78	1.4	454.3	681.5	58.1	--	--	--	--	--	--	--	--	--	--	--	--
13.20	14.00	12.39	2	1.94	2.56	150	0.64	1.1	380.0	570.1	48.2	--	--	--	--	--	--	--	--	--	--	--	--
13.40	13.00	12.15	2	1.93	2.60	145	0.60	1.0	362.6	543.9	46.5	--	--	--	--	--	--	--	--	--	--	--	--
13.60	15.00	20.55	2	1.95	2.64	154	0.67	1.1	397.7	596.5	49.5	--	--	--	--	--	--	--	--	--	--	--	--
13.80	17.00	19.54	2	1.97	2.68	161	0.72	1.2	429.3	644.0	54.1	--	--	--	--	--	--	--	--	--	--	--	--
14.00	16.00	18.39	2	1.96	2.72	157	0.70	1.1	414.6	621.9	51.8	--	--	--	--	--	--	--	--	--	--	--	--
14.20	18.00	13.53	2	1.98	2.76	164	0.75	1.2	444.8	667.2	56.2	--	--	--	--	--	--	--	--	--	--	--	--
14.40	21.00	13.73	4	1.93	2.80	174	0.82	1.4	484.8	727.1	63.0	--	31	20	16	15	25	27	--	--	35.0	52.5	63.0
14.60	24.00	13.87	4	1.94	2.84	183	0.89	1.5	519.5	779.3	72.0	--	31	20	17	16	25	28	--	--	40.0	60.0	72.0
14.80	20.00	13.07	4	1.93	2.88	171	0.80	1.3	473.5	710.2	60.0	--	31	19	16	15	25	27	--	--	33.3	50.0	60.0
15.00	21.00	--	3	1.85	2.91	174	--	--	--	--	--	--	31	20	16	15	25	27	--	--	35.0	52.5	63.0

FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
PARAMETRI GEOTECNICI

CPT	8
riferimento	110-2023

Committente:	**Green-go**	U.M.: **kg/cm²**	Data esec.: 01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Pagina: 1	
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Elaborato:	Falda: Non rilevata

							NATURA COESIVA					NATURA GRANULARE											
Prof.	qc	qc/fs	zone	γ'	σ'vo	Vs	Cu	OCR	Eu50	Eu25	Mo	Dr	Sc	Ca	Ko	DB	DM	Me	FLs	FLl	E'50	E'25	Mo
m	U.M.			t/m³	U.M.	m/s	U.M.	%	U.M.	U.M.	U.M.	%	(°)	(°)	(°)	(°)	(°)	(°)			U.M.	U.M.	U.M.
0.20	4.00	7.55	1	1.46	0.03	93	0.20	69.6	8.0	12.0	6.0	--	--	--	--	--	--	--	--	--	--	--	--
0.40	5.00	4.67	1	1.46	0.06	101	0.25	38.7	10.0	15.0	7.5	--	--	--	--	--	--	--	--	--	--	--	--
0.60	11.00	9.73	2	1.91	0.10	137	0.54	53.5	91.2	136.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
0.80	16.00	11.43	2	1.96	0.14	157	0.70	48.4	118.3	177.4	51.8	--	--	--	--	--	--	--	--	--	--	--	--
1.00	20.00	10.36	4	1.93	0.17	171	0.80	42.2	136.0	204.0	60.0	59	38	33	30	28	38	27	--	--	33.3	50.0	60.0
1.20	18.00	9.33	2	1.98	0.21	164	0.75	30.1	127.5	191.3	56.2	--	--	--	--	--	--	--	--	--	--	--	--
1.40	16.00	10.46	2	1.96	0.25	157	0.70	22.2	118.3	177.4	51.8	--	--	--	--	--	--	--	--	--	--	--	--
1.60	17.00	9.44	2	1.97	0.29	161	0.72	19.5	123.0	184.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
1.80	23.00	12.78	4	1.94	0.33	180	0.87	20.9	147.5	221.3	69.0	48	37	31	28	26	35	28	--	--	38.3	57.5	69.0
2.00	20.00	11.11	4	1.93	0.37	171	0.80	16.5	136.0	204.0	60.0	41	36	30	27	25	34	27	--	--	33.3	50.0	60.0
2.20	17.00	15.04	2	1.97	0.41	161	0.72	12.8	123.0	184.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
2.40	14.00	15.05	2	1.94	0.45	150	0.64	9.7	108.7	163.1	48.2	--	--	--	--	--	--	--	--	--	--	--	--
2.60	16.00	14.16	2	1.96	0.49	157	0.70	9.8	118.7	178.0	51.8	--	--	--	--	--	--	--	--	--	--	--	--
2.80	14.00	42.42	4	1.89	0.52	150	0.64	8.0	126.0	189.1	48.2	20	34	26	23	22	30	26	--	--	23.3	35.0	42.0
3.00	8.00	11.94	2	1.86	0.56	121	0.40	4.1	156.9	235.3	35.2	--	--	--	--	--	--	--	--	--	--	--	--
3.20	7.00	17.50	2	1.84	0.60	115	0.35	3.2	166.6	249.9	32.2	--	--	--	--	--	--	--	--	--	--	--	--
3.40	13.00	48.15	4	1.88	0.64	145	0.60	5.9	169.4	254.1	46.5	13	33	25	21	20	28	26	--	--	21.7	32.5	39.0
3.60	14.00	19.18	2	1.94	0.68	150	0.64	5.8	180.2	270.3	48.2	--	--	--	--	--	--	--	--	--	--	--	--
3.80	10.00	16.67	2	1.90	0.71	132	0.50	4.0	199.0	298.5	40.0	--	--	--	--	--	--	--	--	--	--	--	--
4.00	10.00	16.67	2	1.90	0.75	132	0.50	3.8	211.7	317.5	40.0	--	--	--	--	--	--	--	--	--	--	--	--
4.20	11.00	11.83	2	1.91	0.79	137	0.54	3.9	221.7	332.5	42.5	--	--	--	--	--	--	--	--	--	--	--	--
4.40	15.00	16.13	2	1.95	0.83	154	0.67	4.8	229.9	344.9	49.5	--	--	--	--	--	--	--	--	--	--	--	--
4.60	19.00	16.81	2	1.99	0.87	168	0.78	5.5	235.7	353.6	58.1	--	--	--	--	--	--	--	--	--	--	--	--
4.80	23.00	23.00	4	1.94	0.91	180	0.87	5.9	240.7	361.1	69.0	24	34	26	23	21	29	28	--	--	38.3	57.5	69.0
5.00	24.00	20.00	4	1.94	0.95	183	0.89	5.8	252.7	379.0	72.0	24	34	26	23	21	29	28	--	--	40.0	60.0	72.0
5.20	21.00	24.14	4	1.93	0.98	174	0.82	5.0	271.5	407.2	63.0	19	33	25	22	20	28	27	--	--	35.0	52.5	63.0
5.40	20.00	17.70	4	1.93	1.02	171	0.80	4.6	284.8	427.2	60.0	16	33	25	21	20	28	27	--	--	33.3	50.0	60.0
5.60	23.00	18.11	4	1.94	1.06	180	0.87	4.9	293.9	440.9	69.0	20	34	25	22	21	28	28	--	--	38.3	57.5	69.0
5.80	23.00	15.03	4	1.94	1.10	180	0.87	4.7	306.1	459.1	69.0	19	34	25	22	20	28	28	--	--	38.3	57.5	69.0
6.00	16.00	14.16	2	1.96	1.14	157	0.70	3.4	320.2	480.3	51.8	--	--	--	--	--	--	--	--	--	--	--	--
6.20	17.00	17.00	2	1.97	1.18	161	0.72	3.4	331.5	497.3	54.1	--	--	--	--	--	--	--	--	--	--	--	--
6.40	16.00	34.04	4	1.90	1.22	157	0.70	3.1	336.3	504.5	51.8	4	32	23	19	18	26	27	--	--	26.7	40.0	48.0
6.60	13.00	19.40	2	1.93	1.26	145	0.60	2.5	319.7	479.5	46.5	--	--	--	--	--	--	--	--	--	--	--	--
6.80	19.00	21.84	2	1.99	1.30	168	0.78	3.3	362.6	543.9	58.1	--	--	--	--	--	--	--	--	--	--	--	--
7.00	22.00	15.71	4	1.93	1.33	177	0.85	3.6	376.5	564.7	66.0	13	33	24	20	19	27	28	--	--	36.7	55.0	66.0
7.20	21.00	15.79	4	1.93	1.37	174	0.82	3.3	384.4	576.6	63.0	11	33	23	20	19	26	27	--	--	35.0	52.5	63.0
7.40	23.00	16.43	4	1.94	1.41	180	0.87	3.4	397.0	595.5	69.0	13	33	24	20	19	27	28	--	--	38.3	57.5	69.0
7.60	27.00	18.37	4	1.95	1.45	192	0.95	3.7	409.3	614.0	81.0	18	33	24	21	20	28	28	--	--	45.0	67.5	81.0
7.80	28.00	14.51	4	1.96	1.49	194	0.97	3.7	420.5	630.7	84.0	19	33	24	21	20	28	28	--	--	46.7	70.0	84.0
8.00	28.00	19.05	4	1.96	1.53	194	0.97	3.5	431.2	646.9	84.0	18	33	24	21	20	27	28	--	--	46.7	70.0	84.0
8.20	26.00	21.67	4	1.95	1.57	189	0.93	3.3	437.7	656.5	78.0	15	33	24	20	19	27	28	--	--	43.3	65.0	78.0
8.40	24.00	22.43	4	1.94	1.61	183	0.89	3.0	438.7	658.1	72.0	11	33	23	20	19	26	28	--	--	40.0	60.0	72.0
8.60	21.00	19.63	4	1.93	1.64	174	0.82	2.6	428.3	642.5	63.0	6	32	22	19	18	25	27	--	--	35.0	52.5	63.0
8.80	25.00	19.69	4	1.94	1.68	186	0.91	2.9	455.2	682.8	75.0	12	33	23	20	19	26	28	--	--	41.7	62.5	75.0
9.00	14.00	11.67	2	1.94	1.72	150	0.64	1.8	362.6	543.8	48.2	--	--	--	--	--	--	--	--	--	--	--	--
9.20	16.00	10.88	2	1.96	1.76	157	0.70	2.0	390.8	586.3	51.8	--	--	--	--	--	--	--	--	--	--	--	--
9.40	17.00	18.28	2	1.97	1.80	161	0.72	2.0	404.8	607.2	54.1	--	--	--	--	--	--	--	--	--	--	--	--
9.60	23.00	19.17	4	1.94	1.84	180	0.87	2.5	462.6	693.9	69.0	7	32	22	19	18	25	28	--	--	38.3	57.5	69.0
9.80	25.00	17.01	4	1.94	1.88	186	0.91	2.5	479.7	719.6	75.0	9	32	23	19	18	26	28	--	--	41.7	62.5	75.0
10.00	17.00	15.04	2	1.97	1.92	161	0.72	1.9	410.5	615.7	54.1	--	--	--	--	--	--	--	--	--	--	--	--
10.20	13.00	16.25	2	1.93	1.96	145	0.60	1.4	354.0	531.0	46.5	--	--	--	--	--	--	--	--	--	--	--	--
10.40	13.00	21.67	2	1.93	2.00	145	0.60	1.4	354.8	532.2	46.5	--	--	--	--	--	--	--	--	--	--	--	--
10.60	14.00	17.50	2	1.94	2.03	150	0.64	1.5	372.0	558.0	48.2	--	--	--	--	--	--	--	--	--	--	--	--
10.80	16.00	18.39	2	1.96	2.07	157	0.70	1.6	402.8	604.2	51.8	--	--	--	--	--	--	--	--	--	--	--	--
11.00	16.00	17.20	2	1.96	2.11	157	0.70	1.6	403.9	605.9	51.8	--	--	--	--	--	--	--	--	--	--	--	--
11.20	17.00	18.28	2	1.97	2.15	161	0.72	1.6	418.8	628.2	54.1	--	--	--	--	--	--	--	--	--	--	--	--
11.40	20.00	20.00	4	1.93	2.19	171	0.80	1.8	456.8	685.2	60.0	--	31	21	17	16	25	27	--	--	33.3	50.0	60.0
11.60	27.00	16.17	4	1.95	2.23	192	0.95	2.2	522.4	783.7	81.0	7	32	22	19	18	25	28	--	--	45.0	67.5	81.0
11.80	26.00	15.57	4	1.95	2.27	189	0.93	2.1	517.2	775.8	78.0	6	32	22	18	18	25	28	--	--	43.3	65.0	78.0
12.00	31.00	21.09	4	1.97	2.31	202	1.03	2.3	560.9	841.3	93.0	11	33	23	19	18	26	29	--	--	51.7	77.5	93.0
12.20	27.00	17.65	4	1.95	2.35	192	0.95	2.0	529.5	794.2	81.0	6	32	22	19	18	25	28	--	--	45.0	67.5	81.0
12.40	28.00	18.30	4	1.96	2.39	194	0.97	2.0	539.3	809.0	84.0	7	32	22	19	18	25	28	--	--	46.7	70.0	84.0
12.60	25.00	15.63	4	1.94	2.42	186	0.91	1.8	516.4	774.7	75.0	3	32	21	18	17	25	28	--	--	41.7	62.5	75.0
12.80	19.00	14.29	2	1.99	2.46	168	0.78	1.5	453.0	679.5	58.1	--	--	--	--	--	--	--	--	--	--	--	--
13.00	17.00	15.89	2	1.97	2.50	161	0.72	1.3	426.6	639.9	54.1	--	--	--	--	--	--	--	--	--	--	--	--
13.20	15.00	14.02	2	1.95	2.54	154	0.67	1.2	396.6	594.8	49.5	--	--	--	--	--	--	--	--	--	--	--	--
13.40	14.00	16.09	2	1.94	2.58	150	0.64	1.1	380.2	570.3	48.2	--	--	--	--	--	--	--	--	--	--	--	--
13.60	17.00	21.25	2	1.97	2.62	161	0.72	1.3	428.5	642.7	54.1	--	--	--	--	--	--	--	--	--	--	--	--
13.80	19.00	21.84	2	1.99	2.66	168	0.78	1.3	457.0	685.4	58.1	--	--	--	--	--	--	--	--	--	--	--	--
14.00	14.00	17.50	2	1.94	2.70	150	0.64	1.0	381.3	571.9	48.2	--	--	--	--	--	--	--	--	--	--	--	--
14.20	15.00	28.30	2	1.95	2.74	154	0.67	1.1	398.6	598.0	49.5	--	--	--	--	--	--	--	--	--	--	--	--
14.40	13.00	27.66	2	1.93	2.78	145	0.60	0.9	362.8	544.2	46.5	--	--	--	--	--	--	--	--	--	--	--	--
14.60	17.00	25.37	2	1.97	2.82	161	0.72	1.1	431.0	646.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
14.80	21.00	31.34	3	1.85	2.85	174	--	--	--	--	--	--	31	20	16	15	25	27	--	--	35.0	52.5	63.0
15.00	20.00	--	3	1.85	2.89	171	--	--	--	--	--	--	31	19	16	15	25	27	--	--	33.3	50.0	60.0

FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
PARAMETRI GEOTECNICI

CPT	9
riferimento	110-2023

Committente:	**Green-go**	U.M.: **kg/cm²**	Data esec.: 01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Pagina: 1	
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Elaborato:	Falda: -1.80 m da p.c.

							NATURA COESIVA					NATURA GRANULARE											
Prof.	qc	qc/fs	zone	γ'	σ'vo	Vs	Cu	OCR	Eu50	Eu25	Mo	Dr	Sc	Ca	Ko	DB	DM	Me	FLs	FLI	E'50	E'25	Mo
m	U.M.			t/m³	U.M.	m/s	U.M.	%	U.M.	U.M.	U.M.	%	(°)	(°)	(°)	(°)	(°)	(°)			U.M.	U.M.	U.M.
0.20	4.00	30.77	4	1.80	0.04	93	0.20	53.7	34.0	51.0	20.0	43	36	33	30	28	38	25	--	--	6.7	10.0	12.0
0.40	5.00	12.50	1	1.46	0.07	101	0.25	33.8	10.0	15.0	7.5	--	--	--	--	--	--	--	--	--	--	--	--
0.60	6.00	5.61	1	1.46	0.09	109	0.30	26.7	12.0	18.0	9.0	--	--	--	--	--	--	--	--	--	--	--	--
0.80	13.00	14.94	2	1.93	0.13	145	0.60	41.7	102.8	154.2	46.5	--	--	--	--	--	--	--	--	--	--	--	--
1.00	72.00	20.00	4	2.03	0.17	277	2.40	99.9	408.0	612.0	216.0	100	43	40	37	35	43	32	--	--	120.0	180.0	216.0
1.20	61.00	15.76	4	2.02	0.21	260	2.03	99.9	345.7	518.5	183.0	93	42	38	35	33	42	32	--	--	101.7	152.5	183.0
1.40	43.00	13.74	4	2.00	0.25	228	1.43	54.7	243.7	365.5	129.0	76	40	35	32	30	39	30	--	--	71.7	107.5	129.0
1.60	29.00	13.62	4	1.96	0.29	197	0.98	28.5	167.1	250.7	87.0	59	38	33	30	28	37	29	--	--	48.3	72.5	87.0
1.80	23.00	12.30	4	0.94	0.31	180	0.87	22.6	147.5	221.3	69.0	50	37	31	28	26	35	28	--	--	38.3	57.5	69.0
2.00	19.00	11.38	2	0.99	0.33	168	0.78	18.2	131.8	197.8	58.1	--	--	--	--	--	--	--	--	--	--	--	--
2.20	17.00	10.63	2	0.97	0.35	161	0.72	15.5	123.0	184.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
2.40	19.00	9.84	2	0.99	0.37	168	0.78	15.8	131.8	197.8	58.1	--	--	--	--	--	--	--	--	--	--	--	--
2.60	42.00	37.17	3	0.90	0.39	226	--	--	--	--	--	65	39	33	30	28	37	30	1.75	>2.00	70.0	105.0	126.0
2.80	59.00	26.82	4	1.02	0.41	257	1.97	44.7	334.3	501.5	177.0	76	40	34	32	30	39	32	>2.00	>2.00	98.3	147.5	177.0
3.00	18.00	19.35	2	0.98	0.43	164	0.75	12.6	127.5	191.3	56.2	--	--	--	--	--	--	--	--	--	--	--	--
3.20	52.00	86.67	3	0.92	0.45	245	--	--	--	--	--	69	40	33	31	29	38	31	1.79	>2.00	86.7	130.0	156.0
3.40	35.00	35.00	3	0.89	0.46	211	--	--	--	--	--	55	38	31	28	26	35	29	1.26	1.93	58.3	87.5	105.0
3.60	51.00	47.66	3	0.92	0.48	243	--	--	--	--	--	67	39	33	30	28	37	31	1.62	>2.00	85.0	127.5	153.0
3.80	32.00	47.76	3	0.88	0.50	204	--	--	--	--	--	50	37	30	27	26	34	29	1.12	1.74	53.3	80.0	96.0
4.00	36.00	90.00	3	0.89	0.52	214	--	--	--	--	--	53	38	31	28	26	35	30	1.16	1.79	60.0	90.0	108.0
4.20	19.00	47.50	4	0.92	0.54	168	0.78	9.9	131.9	197.9	58.1	30	35	27	24	23	31	27	0.90	1.36	31.7	47.5	57.0
4.40	14.00	42.42	4	0.89	0.55	150	0.64	7.5	136.1	204.1	48.2	19	34	26	23	21	29	26	0.81	1.22	23.3	35.0	42.0
4.60	16.00	80.00	4	0.90	0.57	157	0.70	8.0	137.5	206.2	51.8	23	34	26	23	22	30	27	0.82	1.24	26.7	40.0	48.0
4.80	7.00	5.26	1	0.46	0.58	115	0.35	3.3	32.0	47.9	10.5	--	--	--	--	--	--	--	--	--	--	--	--
5.00	31.00	51.67	3	0.88	0.60	202	--	--	--	--	--	44	37	29	26	25	33	29	0.98	1.51	51.7	77.5	93.0
5.20	30.00	75.00	3	0.88	0.62	199	--	--	--	--	--	42	36	29	26	24	33	29	0.96	1.46	50.0	75.0	90.0
5.40	29.00	39.73	3	0.87	0.63	197	--	--	--	--	--	41	36	29	26	24	33	29	0.94	1.42	48.3	72.5	87.0
5.60	41.00	87.23	3	0.90	0.65	224	--	--	--	--	--	52	37	30	27	26	34	30	1.05	1.62	68.3	102.5	123.0
5.80	24.00	35.82	3	0.86	0.67	183	--	--	--	--	--	33	35	28	24	23	31	28	0.85	1.28	40.0	60.0	72.0
6.00	12.00	25.53	2	0.92	0.69	141	0.57	5.0	190.0	285.0	44.6	--	--	--	--	--	--	--	--	--	--	--	--
6.20	10.00	30.30	4	0.86	0.71	132	0.50	4.1	196.9	295.3	40.0	1	31	23	20	19	26	26	0.67	1.02	16.7	25.0	30.0
6.40	14.00	70.00	4	0.89	0.72	150	0.64	5.4	197.1	295.7	48.2	12	33	24	21	20	28	26	0.71	1.07	23.3	35.0	42.0
6.60	11.00	20.75	2	0.91	0.74	137	0.54	4.2	207.0	310.5	42.5	--	--	--	--	--	--	--	--	--	--	--	--
6.80	21.00	28.77	4	0.93	0.76	174	0.82	6.9	191.2	286.8	63.0	25	34	26	23	22	30	27	0.77	1.16	35.0	52.5	63.0
7.00	7.00	17.50	2	0.84	0.78	115	0.35	2.3	189.6	284.4	32.2	--	--	--	--	--	--	--	--	--	--	--	--
7.20	5.00	12.50	1	0.46	0.79	101	0.25	1.5	31.6	47.3	7.5	--	--	--	--	--	--	--	--	--	--	--	--
7.40	5.00	12.50	1	0.46	0.80	101	0.25	1.5	31.6	47.4	7.5	--	--	--	--	--	--	--	--	--	--	--	--
7.60	6.00	18.18	2	0.82	0.81	109	0.30	1.8	170.9	256.3	28.8	--	--	--	--	--	--	--	--	--	--	--	--
7.80	11.00	15.07	2	0.91	0.83	137	0.54	3.6	234.2	351.3	42.5	--	--	--	--	--	--	--	--	--	--	--	--
8.00	20.00	14.29	4	0.93	0.85	171	0.80	5.8	226.3	339.5	60.0	21	34	25	22	21	29	27	0.72	1.09	33.3	50.0	60.0
8.20	40.00	43.01	3	0.90	0.87	222	--	--	--	--	--	44	37	29	26	24	33	30	0.89	1.38	66.7	100.0	120.0
8.40	113.00	80.71	3	1.02	0.89	329	--	--	--	--	--	79	41	34	31	29	38	34	>2.00	>2.00	188.3	282.5	339.0
8.60	17.00	18.28	2	0.97	0.91	161	0.72	4.7	251.7	377.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
8.80	18.00	30.00	4	0.91	0.92	164	0.75	4.8	256.2	384.3	56.2	15	33	25	21	20	28	27	0.69	1.03	30.0	45.0	54.0
9.00	17.00	18.28	2	0.97	0.94	161	0.72	4.5	263.1	394.7	54.1	--	--	--	--	--	--	--	--	--	--	--	--
9.20	21.00	19.63	4	0.93	0.96	174	0.82	5.2	264.1	396.2	63.0	19	34	25	22	21	28	27	0.71	1.06	35.0	52.5	63.0
9.40	24.00	21.24	4	0.94	0.98	183	0.89	5.6	265.3	397.9	72.0	23	34	26	22	21	29	28	0.73	1.10	40.0	60.0	72.0
9.60	26.00	12.56	4	0.95	1.00	189	0.93	5.7	268.3	402.4	78.0	26	34	26	23	21	29	28	0.75	1.13	43.3	65.0	78.0
9.80	21.00	14.29	4	0.93	1.02	174	0.82	4.8	282.5	423.8	63.0	18	33	25	22	20	28	27	0.71	1.06	35.0	52.5	63.0
10.00	30.00	19.61	4	0.96	1.04	199	1.00	6.0	274.8	412.1	90.0	30	35	26	23	22	30	29	0.78	1.18	50.0	75.0	90.0
10.20	20.00	15.75	4	0.93	1.06	171	0.80	4.4	294.8	442.2	60.0	15	33	24	21	20	28	27	0.70	1.05	33.3	50.0	60.0
10.40	20.00	20.00	4	0.93	1.07	171	0.80	4.3	300.1	450.2	60.0	15	33	24	21	20	28	27	0.70	1.05	33.3	50.0	60.0
10.60	32.00	15.46	4	0.97	1.09	204	1.07	6.1	288.4	432.6	96.0	31	35	27	23	22	30	29	0.80	1.21	53.3	80.0	96.0
10.80	34.00	14.17	4	0.98	1.11	209	1.13	6.4	288.4	432.6	102.0	32	35	27	24	22	30	29	0.82	1.24	56.7	85.0	102.0
11.00	31.00	13.30	4	0.97	1.13	202	1.03	5.6	305.8	458.7	93.0	29	35	26	23	22	30	29	0.79	1.20	51.7	77.5	93.0
11.20	29.00	18.13	4	0.96	1.15	197	0.98	5.1	316.5	474.8	87.0	26	34	26	23	21	29	29	0.78	1.17	48.3	72.5	87.0
11.40	38.00	19.00	4	0.99	1.17	218	1.27	6.9	295.4	443.1	114.0	35	35	27	24	22	31	30	0.85	1.29	63.3	95.0	114.0
11.60	24.00	15.69	4	0.94	1.19	183	0.89	4.4	332.5	498.8	72.0	19	33	25	21	20	28	28	0.74	1.11	40.0	60.0	72.0
11.80	26.00	21.67	4	0.95	1.21	189	0.93	4.5	337.4	506.1	78.0	21	34	25	22	21	28	28	0.75	1.14	43.3	65.0	78.0
12.00	24.00	18.05	4	0.94	1.23	183	0.89	4.2	343.2	514.7	72.0	18	33	25	21	20	28	28	0.74	1.11	40.0	60.0	72.0
12.20	28.00	18.30	4	0.96	1.25	194	0.97	4.6	347.8	521.6	84.0	23	34	25	22	21	29	28	0.77	1.17	46.7	70.0	84.0
12.40	36.00	20.00	4	0.99	1.27	214	1.20	5.9	337.8	506.7	108.0	31	35	26	23	22	30	30	0.84	1.27	60.0	90.0	108.0
12.60	38.00	19.00	4	0.99	1.29	218	1.27	6.2	338.0	507.0	114.0	33	35	27	23	22	30	30	0.86	1.30	63.3	95.0	114.0
12.80	36.00	15.86	4	0.99	1.31	214	1.20	5.6	352.0	527.9	108.0	30	35	26	23	22	30	30	0.84	1.27	60.0	90.0	108.0
13.00	32.00	12.31	4	0.97	1.33	204	1.07	4.8	368.2	552.2	96.0	26	34	26	22	21	29	29	0.81	1.22	53.3	80.0	96.0
13.20	34.00	11.33	4	0.98	1.35	209	1.13	5.1	370.7	556.1	102.0	28	35	26	23	21	29	29	0.83	1.25	56.7	85.0	102.0
13.40	31.00	12.92	4	0.97	1.37	202	1.03	4.4	381.0	571.5	93.0	24	34	25	22	21	29	29	0.81	1.22	51.7	77.5	93.0
13.60	33.00	17.10	4	0.97	1.38	207	1.10	4.7	385.0	577.4	99.0	26	34	26	22	21	29	29	0.83	1.25	55.0	82.5	99.0
13.80	31.00	18.56	4	0.97	1.40	202	1.03	4.3	392.2	588.2	93.0	23	34	25	22	21	29	29	0.81	1.22	51.7	77.5	93.0
14.00	27.00	15.61	4	0.95	1.42	192	0.95	3.8	401.0	601.5	81.0	18	33	24	21	20	28	28	0.78	1.18	45.0	67.5	81.0
14.20	24.00	13.33	4	0.94	1.44	183	0.89	3.4	405.8	608.7	72.0	14	33	24	20	19	27	28	0.76	1.15	40.0	60.0	72.0
14.40	31.00	20.26	4	0.97	1.46	202	1.03	4.1	407.8	611.7	93.0	22	34	25	22	20	28	29	0.82	1.23	51.7	77.5	93.0
14.60	26.00	16.25	4	0.95	1.48	189	0.93	3.5	417.4	626.1	78.0	16	33	24	21	20	27	28	0.78	1.18	43.3	65.0	78.0
14.80	30.00	18.75	4	0.96	1.50	199	1.00	3.8	422.4	633.6	90.0	21	34	25	21	20	28	29	0.82	1.23	50.0	75.0	90.0
15.00	25.00	--	3	0.86	1.52	186	--	--	--	--	--	14	33	24	20	19	27	28	0.78	1.18	41.7	62.5	75.0

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
PARAMETRI GEOTECNICI

CPT	10
riferimento	110-2023

Committente:	**Green-go**	U.M.: **kg/cm²**	Data esec.: 01/02/2024
Cantiere:	**Ralizzazione di un Campo Agrivoltaico**	Pagina: 1	
Località:	**Via Puglia, Loc. Biancolina (San Giovanni in Persiceto (BO)**	Elaborato:	Falda: Non rilevata

							NATURA COESIVA					NATURA GRANULARE											
Prof.	qc	qc/fs	zone	γ'	σ'vo	Vs	Cu	OCR	Eu50	Eu25	Mo	Dr	Sc	Ca	Ko	DB	DM	Me	FLs	FLl	E'50	E'25	Mo
m	U.M.			t/m³	U.M.	m/s	U.M.	%	U.M.	U.M.	U.M.	%	(°)	(°)	(°)	(°)	(°)	(°)			U.M.	U.M.	U.M.
0.20	4.00	14.81	1	1.46	0.03	93	0.20	69.6	8.0	12.0	6.0	--	--	--	--	--	--	--	--	--	--	--	--
0.40	5.00	18.52	2	1.80	0.07	101	0.25	33.7	42.5	63.8	25.0	--	--	--	--	--	--	--	--	--	--	--	--
0.60	7.00	6.19	1	1.46	0.09	115	0.35	32.3	14.0	21.0	10.5	--	--	--	--	--	--	--	--	--	--	--	--
0.80	14.00	11.67	2	1.94	0.13	150	0.64	44.3	108.2	162.3	48.2	--	--	--	--	--	--	--	--	--	--	--	--
1.00	17.00	32.08	4	1.91	0.17	161	0.72	38.0	123.0	184.5	54.1	54	38	33	30	28	37	27	--	--	28.3	42.5	51.0
1.20	8.00	10.00	2	1.86	0.21	121	0.40	14.2	68.0	102.0	35.2	--	--	--	--	--	--	--	--	--	--	--	--
1.40	13.00	9.29	2	1.93	0.25	145	0.60	19.2	102.8	154.2	46.5	--	--	--	--	--	--	--	--	--	--	--	--
1.60	24.00	18.05	4	1.94	0.29	183	0.89	25.9	151.1	226.7	72.0	53	38	32	29	27	36	28	--	--	40.0	60.0	72.0
1.80	20.00	13.61	4	1.93	0.32	171	0.80	19.4	136.0	204.0	60.0	44	37	30	27	26	34	27	--	--	33.3	50.0	60.0
2.00	15.00	14.02	2	1.95	0.36	154	0.67	13.4	113.3	170.0	49.5	--	--	--	--	--	--	--	--	--	--	--	--
2.20	12.00	22.64	2	1.92	0.40	141	0.57	9.8	97.6	146.4	44.6	--	--	--	--	--	--	--	--	--	--	--	--
2.40	13.00	24.53	2	1.93	0.44	145	0.60	9.3	105.1	157.7	46.5	--	--	--	--	--	--	--	--	--	--	--	--
2.60	12.00	22.64	2	1.92	0.48	141	0.57	7.8	115.6	173.4	44.6	--	--	--	--	--	--	--	--	--	--	--	--
2.80	14.00	29.79	2	1.94	0.52	150	0.64	8.1	123.8	185.7	48.2	--	--	--	--	--	--	--	--	--	--	--	--
3.00	11.00	33.33	4	1.87	0.56	137	0.54	6.0	146.7	220.1	42.5	10	33	25	21	20	28	26	--	--	18.3	27.5	33.0
3.20	8.00	24.24	2	1.86	0.59	121	0.40	3.8	166.5	249.8	35.2	--	--	--	--	--	--	--	--	--	--	--	--
3.40	7.00	25.93	2	1.84	0.63	115	0.35	3.0	172.2	258.3	32.2	--	--	--	--	--	--	--	--	--	--	--	--
3.60	11.00	33.33	4	1.87	0.67	137	0.54	4.8	184.9	277.4	42.5	6	32	24	20	19	27	26	--	--	18.3	27.5	33.0
3.80	9.00	33.33	4	1.85	0.70	127	0.45	3.6	198.6	297.9	37.8	--	31	22	19	18	25	26	--	--	15.0	22.5	27.0
4.00	8.00	40.00	4	1.84	0.74	121	0.40	2.9	200.2	300.3	35.2	--	31	22	18	17	25	26	--	--	13.3	20.0	24.0
4.20	11.00	16.42	2	1.91	0.78	137	0.54	3.9	217.8	326.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
4.40	12.00	30.00	4	1.88	0.82	141	0.57	4.0	227.6	341.4	44.6	4	32	23	20	19	26	26	--	--	20.0	30.0	36.0
4.60	10.00	25.00	2	1.90	0.85	132	0.50	3.2	237.7	356.6	40.0	--	--	--	--	--	--	--	--	--	--	--	--
4.80	12.00	25.53	2	1.92	0.89	141	0.57	3.6	251.9	377.9	44.6	--	--	--	--	--	--	--	--	--	--	--	--
5.00	12.00	22.64	2	1.92	0.93	141	0.57	3.4	261.8	392.7	44.6	--	--	--	--	--	--	--	--	--	--	--	--
5.20	10.00	37.04	4	1.86	0.97	132	0.50	2.7	256.3	384.4	40.0	--	31	21	18	17	25	26	--	--	16.7	25.0	30.0
5.40	16.00	40.00	4	1.90	1.01	157	0.70	4.0	281.3	421.9	51.8	9	32	24	20	19	27	27	--	--	26.7	40.0	48.0
5.60	17.00	11.56	2	1.97	1.05	161	0.72	4.0	292.2	438.3	54.1	--	--	--	--	--	--	--	--	--	--	--	--
5.80	19.00	20.43	2	1.99	1.09	168	0.78	4.1	303.0	454.5	58.1	--	--	--	--	--	--	--	--	--	--	--	--
6.00	15.00	31.91	4	1.89	1.12	154	0.67	3.3	313.8	470.6	49.5	4	32	23	19	18	26	27	--	--	25.0	37.5	45.0
6.20	20.00	29.85	4	1.93	1.16	171	0.80	3.9	325.1	487.7	60.0	13	33	24	21	19	27	27	--	--	33.3	50.0	60.0
6.40	21.00	28.77	4	1.93	1.20	174	0.82	3.9	336.3	504.4	63.0	14	33	24	21	20	27	27	--	--	35.0	52.5	63.0
6.60	29.00	25.66	4	1.96	1.24	197	0.98	4.7	344.6	516.8	87.0	24	34	25	22	21	29	29	--	--	48.3	72.5	87.0
6.80	26.00	23.01	4	1.95	1.28	189	0.93	4.2	357.0	535.5	78.0	20	34	25	21	20	28	28	--	--	43.3	65.0	78.0
7.00	29.00	25.66	4	1.96	1.32	197	0.98	4.4	367.9	551.8	87.0	23	34	25	22	21	29	29	--	--	48.3	72.5	87.0
7.20	26.00	21.67	4	1.95	1.36	189	0.93	3.9	380.3	570.4	78.0	18	33	24	21	20	28	28	--	--	43.3	65.0	78.0
7.40	21.00	18.58	4	1.93	1.39	174	0.82	3.2	389.2	583.8	63.0	10	32	23	20	19	26	27	--	--	35.0	52.5	63.0
7.60	20.00	20.00	4	1.93	1.43	171	0.80	3.0	392.8	589.2	60.0	8	32	23	20	18	26	27	--	--	33.3	50.0	60.0
7.80	24.00	32.88	3	1.86	1.47	183	--	--	--	--	--	14	33	24	20	19	27	28	--	--	40.0	60.0	72.0
8.00	18.00	18.00	2	1.98	1.51	164	0.75	2.6	391.5	587.2	56.2	--	--	--	--	--	--	--	--	--	--	--	--
8.20	27.00	19.29	4	1.95	1.55	192	0.95	3.4	435.5	653.2	81.0	16	33	24	21	20	27	28	--	--	45.0	67.5	81.0
8.40	29.00	20.71	4	1.96	1.59	197	0.98	3.4	447.3	670.9	87.0	18	33	24	21	20	27	29	--	--	48.3	72.5	87.0
8.60	30.00	20.41	4	1.96	1.63	199	1.00	3.4	457.8	686.7	90.0	19	33	24	21	20	28	29	--	--	50.0	75.0	90.0
8.80	29.00	18.95	4	1.96	1.67	197	0.98	3.2	464.9	697.4	87.0	17	33	24	21	19	27	29	--	--	48.3	72.5	87.0
9.00	24.00	17.14	4	1.94	1.71	183	0.89	2.8	453.6	680.4	72.0	10	32	23	20	18	26	28	--	--	40.0	60.0	72.0
9.20	24.00	18.90	4	1.94	1.74	183	0.89	2.7	458.6	687.9	72.0	9	32	23	19	18	26	28	--	--	40.0	60.0	72.0
9.40	23.00	18.11	4	1.94	1.78	180	0.87	2.6	456.9	685.4	69.0	7	32	22	19	18	26	28	--	--	38.3	57.5	69.0
9.60	21.00	18.58	4	1.93	1.82	174	0.82	2.3	445.6	668.4	63.0	4	32	22	19	18	25	27	--	--	35.0	52.5	63.0
9.80	24.00	17.14	4	1.94	1.86	183	0.89	2.5	471.5	707.2	72.0	8	32	22	19	18	26	28	--	--	40.0	60.0	72.0
10.00	24.00	16.33	4	1.94	1.90	183	0.89	2.4	475.2	712.8	72.0	7	32	22	19	18	25	28	--	--	40.0	60.0	72.0
10.20	29.00	18.13	4	1.96	1.94	197	0.98	2.7	508.3	762.5	87.0	13	33	23	20	19	26	29	--	--	48.3	72.5	87.0
10.40	35.00	16.43	4	1.98	1.98	211	1.17	3.2	551.8	827.6	105.0	19	34	24	21	20	27	29	--	--	58.3	87.5	105.0
10.60	39.00	18.84	4	2.00	2.02	220	1.30	3.6	569.8	854.6	117.0	22	34	24	21	20	28	30	--	--	65.0	97.5	117.0
10.80	35.00	87.50	3	1.89	2.06	211	--	--	--	--	--	18	33	24	21	19	27	29	--	--	58.3	87.5	105.0
11.00	17.00	15.89	2	1.97	2.10	161	0.72	1.7	417.1	625.6	54.1	--	--	--	--	--	--	--	--	--	--	--	--
11.20	23.00	19.17	4	1.94	2.13	180	0.87	2.0	484.2	726.3	69.0	3	32	22	18	17	25	28	--	--	38.3	57.5	69.0
11.40	42.00	17.50	4	2.00	2.17	226	1.40	3.6	613.8	920.6	126.0	23	34	24	21	20	28	30	--	--	70.0	105.0	126.0
11.60	41.00	15.36	4	2.00	2.21	224	1.37	3.4	623.1	934.7	123.0	22	34	24	21	20	28	30	--	--	68.3	102.5	123.0
11.80	35.00	18.72	4	1.98	2.25	211	1.17	2.8	597.3	895.9	105.0	16	33	23	20	19	27	29	--	--	58.3	87.5	105.0
12.00	35.00	20.96	4	1.98	2.29	211	1.17	2.7	602.3	903.5	105.0	16	33	23	20	19	26	29	--	--	58.3	87.5	105.0
12.20	33.00	17.65	4	1.97	2.33	207	1.10	2.5	586.4	879.6	99.0	13	33	23	20	19	26	29	--	--	55.0	82.5	99.0
12.40	33.00	15.49	4	1.97	2.37	207	1.10	2.4	590.0	885.0	99.0	13	33	23	19	18	26	29	--	--	55.0	82.5	99.0
12.60	32.00	15.02	4	1.97	2.41	204	1.07	2.3	581.3	871.9	96.0	11	33	23	19	18	26	29	--	--	53.3	80.0	96.0
12.80	35.00	23.81	4	1.98	2.45	211	1.17	2.5	619.7	929.6	105.0	14	33	23	20	19	26	29	--	--	58.3	87.5	105.0
13.00	39.00	17.18	4	2.00	2.49	220	1.30	2.8	662.9	994.3	117.0	17	33	23	20	19	27	30	--	--	65.0	97.5	117.0
13.20	37.00	19.17	4	1.99	2.53	216	1.23	2.6	649.0	973.5	111.0	15	33	23	20	19	26	30	--	--	61.7	92.5	111.0
13.40	35.00	18.13	4	1.98	2.57	211	1.17	2.3	630.4	945.7	105.0	13	33	23	19	18	26	29	--	--	58.3	87.5	105.0
13.60	28.00	14.97	4	1.96	2.61	194	0.97	1.8	549.9	824.9	84.0	5	32	22	18	17	25	28	--	--	46.7	70.0	84.0
13.80	25.00	15.63	4	1.94	2.65	186	0.91	1.6	524.6	786.9	75.0	1	31	21	17	17	25	28	--	--	41.7	62.5	75.0
14.00	20.00	12.50	4	1.93	2.69	171	0.80	1.4	470.3	705.5	60.0	--	31	20	16	15	25	27	--	--	33.3	50.0	60.0
14.20	27.00	16.88	4	1.95	2.73	192	0.95	1.7	545.6	818.4	81.0	3	32	21	18	17	25	28	--	--	45.0	67.5	81.0
14.40	35.00	19.44	4	1.98	2.77	211	1.17	2.1	644.7	967.0	105.0	11	33	22	19	18	25	29	--	--	58.3	87.5	105.0
14.60	25.00	15.63	4	1.94	2.80	186	0.91	1.5	529.0	793.5	75.0	--	31	21	17	16	25	28	--	--	41.7	62.5	75.0
14.80	27.00	14.44	4	1.95	2.84	192	0.95	1.6	549.1	823.7	81.0	1	31	21	18	17	25	28	--	--	45.0	67.5	81.0
15.00	31.00	--	3	1.88	2.88	202	--	--	--	--	--	6	32	22	18	17	25	29	--	--	51.7	77.5	93.0

FON053

Software by dott. Geol. Diego Merlin 0425-840820

ALLEGATO II

- PROVE PENETROMETRICHE STATICHE ELETTRICHE
CON PIEZOCONO-

DIAGRAMMI DI RESISTENZA
--
VALUTAZIONI LITOLOGICHE
--
PARAMETRI GEOTECNICI

Dott. geol. Maurizio Zamboni
Corso Esperanto, 3/h
40065 Pianoro (BO)
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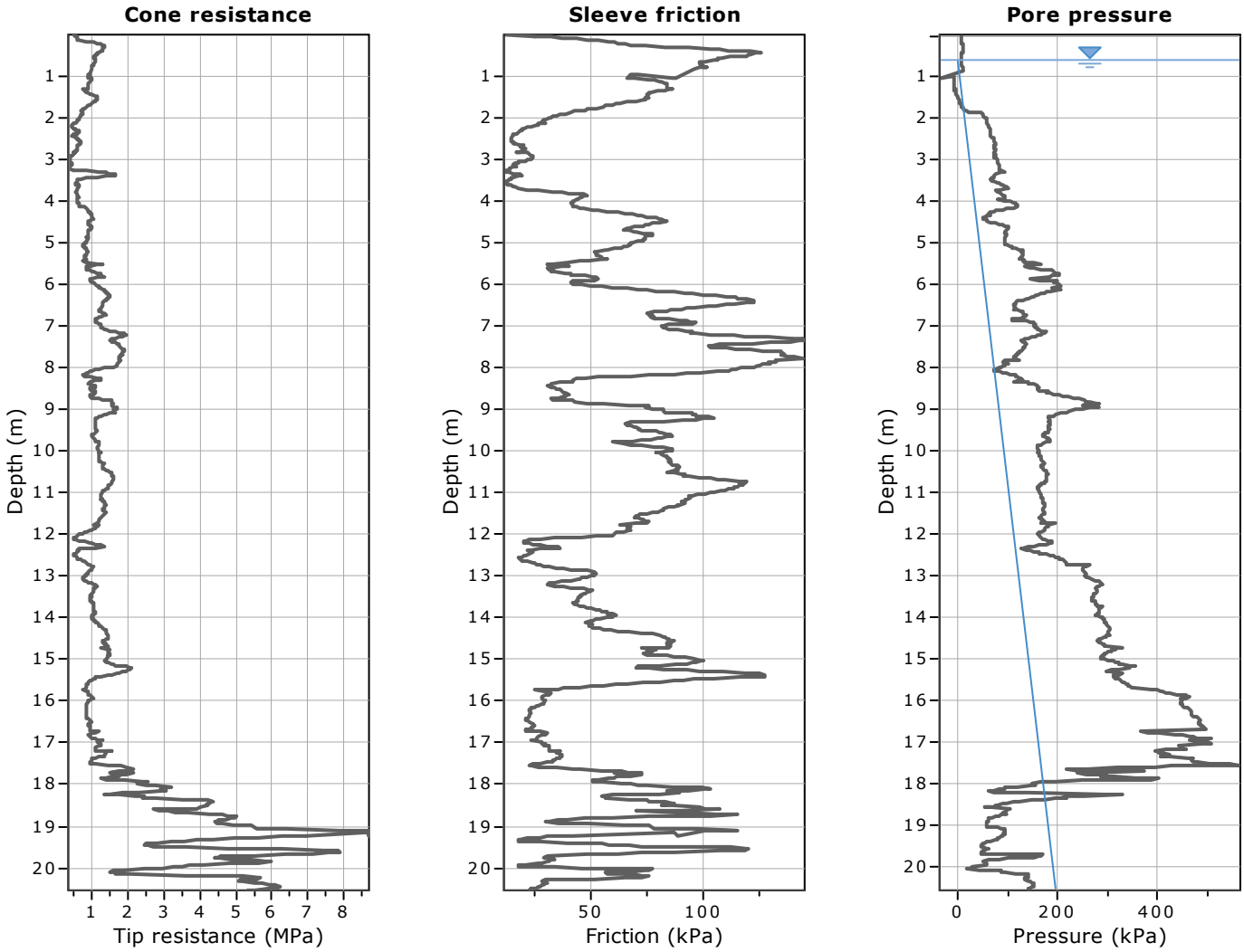
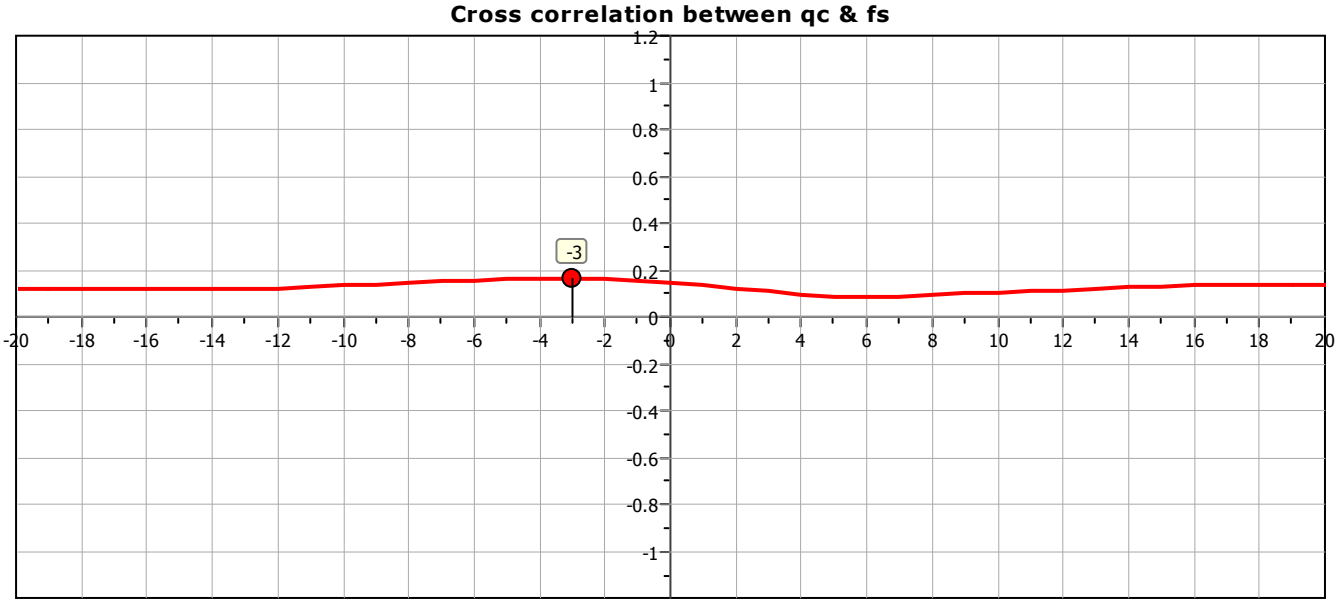
CPT: CPTu-01
Total depth: 20.54 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:



The plot below presents the cross correlation coeficient between the raw qc and fs values (as measured on the field). X axes presents the lag distance (one lag is the distance between two sucessive CPT measurements).



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Project:
Location:

CPT: CPTu-01
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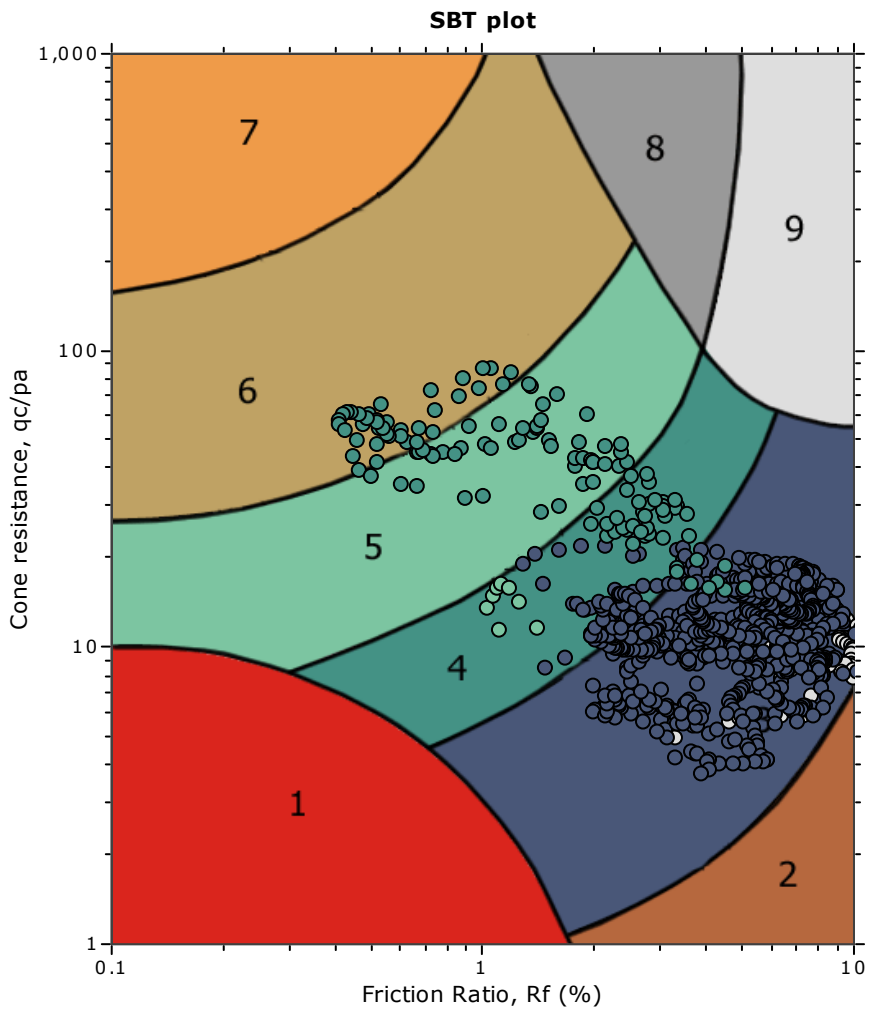
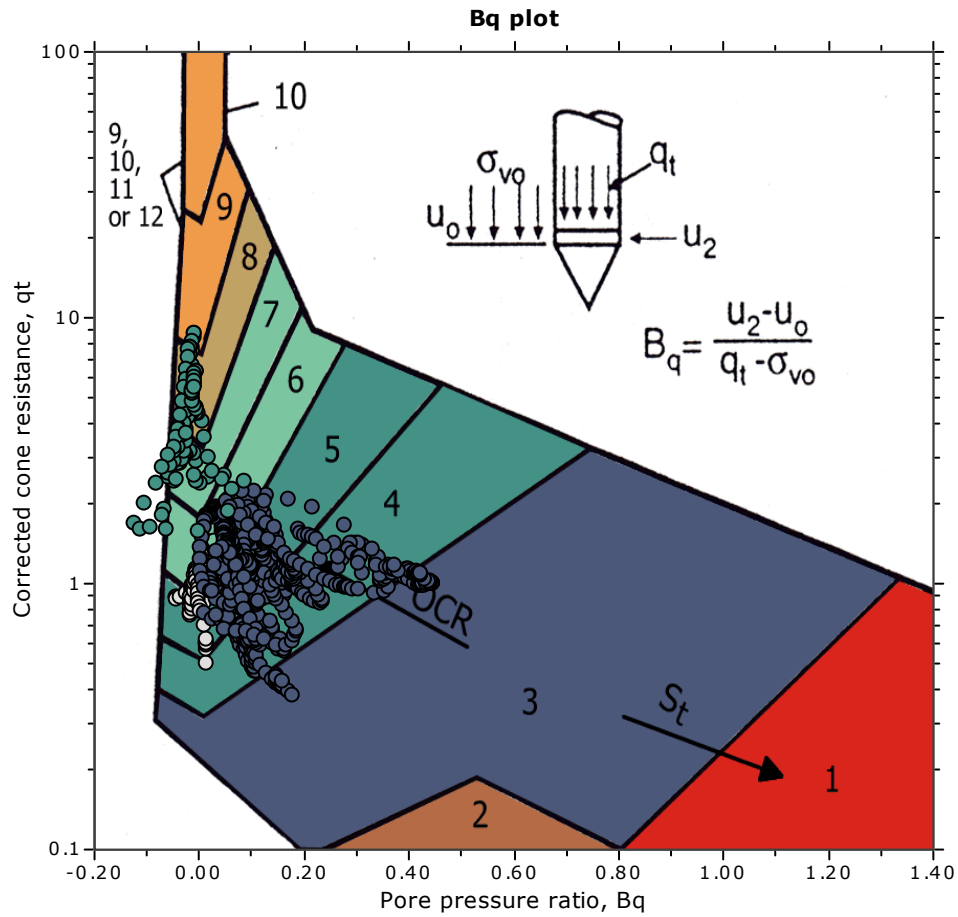
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

SBT - Bq plots





SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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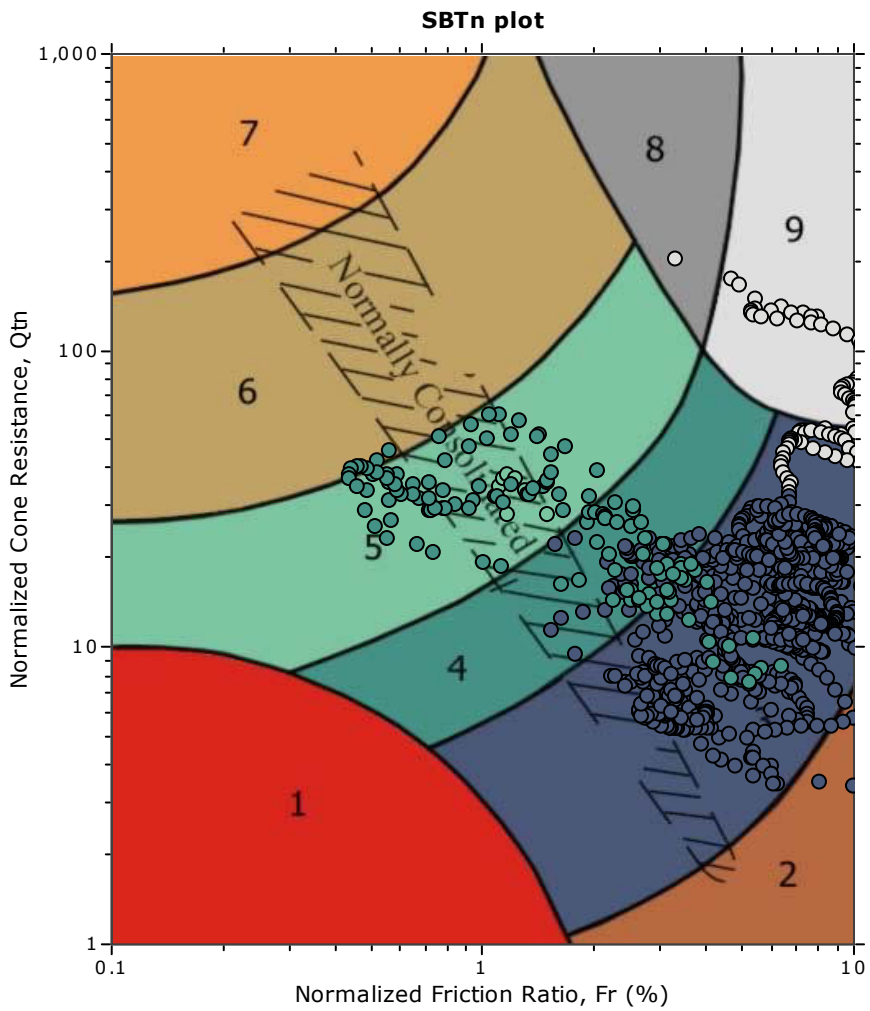
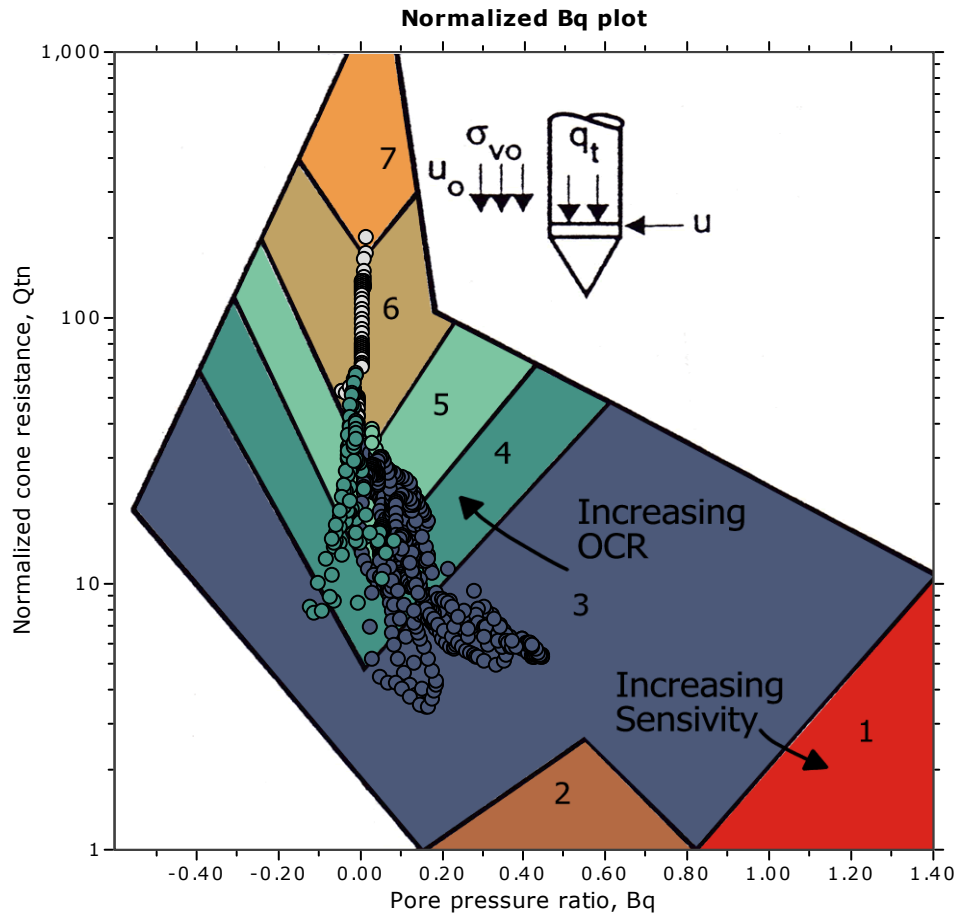
Project:
Location:

CPT: CPTu-01
Total depth: 20.54 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

SBT - Bq plots (normalized)





SBTn legend

- 1. Sensitive fine grained
- 2. Organic material
- 3. Clay to silty clay
- 4. Clayey silt to silty clay
- 5. Silty sand to sandy silt
- 6. Clean sand to silty sand
- 7. Gravely sand to sand
- 8. Very stiff sand to clayey sand
- 9. Very stiff fine grained

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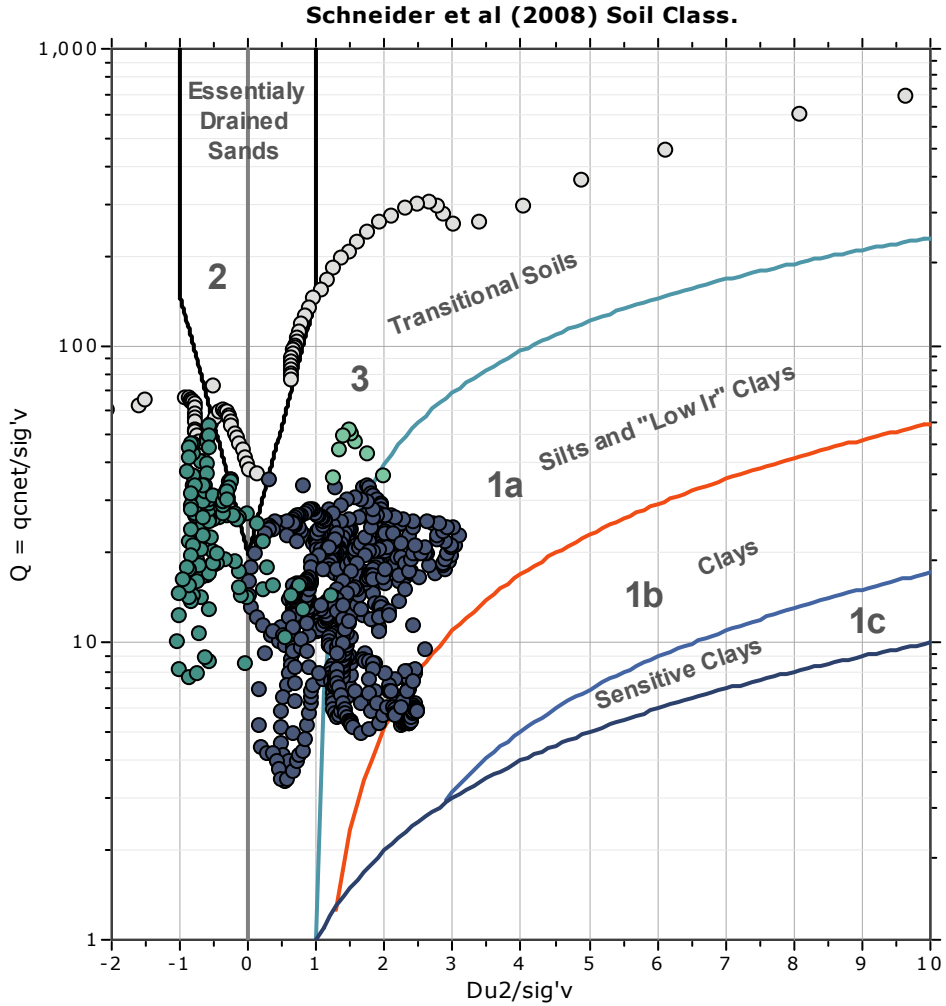
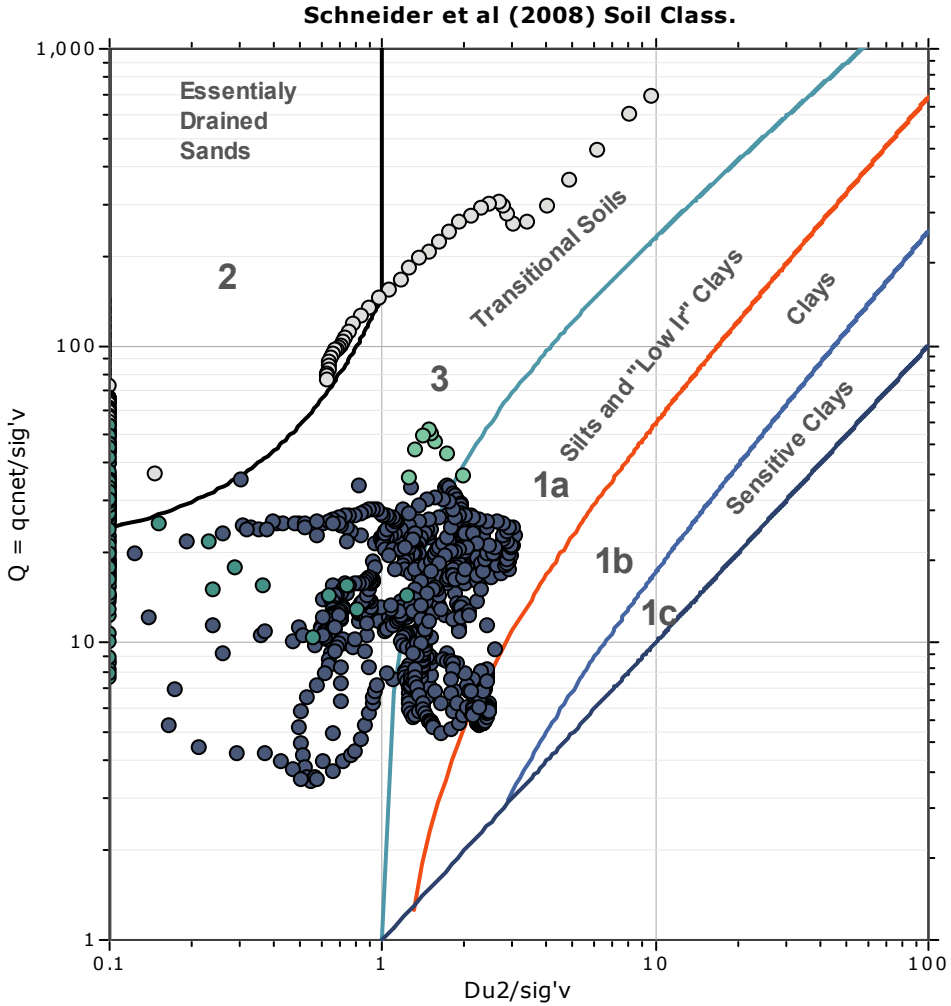
Project:
Location:

CPT: CPTu-01
Total depth: 20.54 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Bq plots (Schneider)





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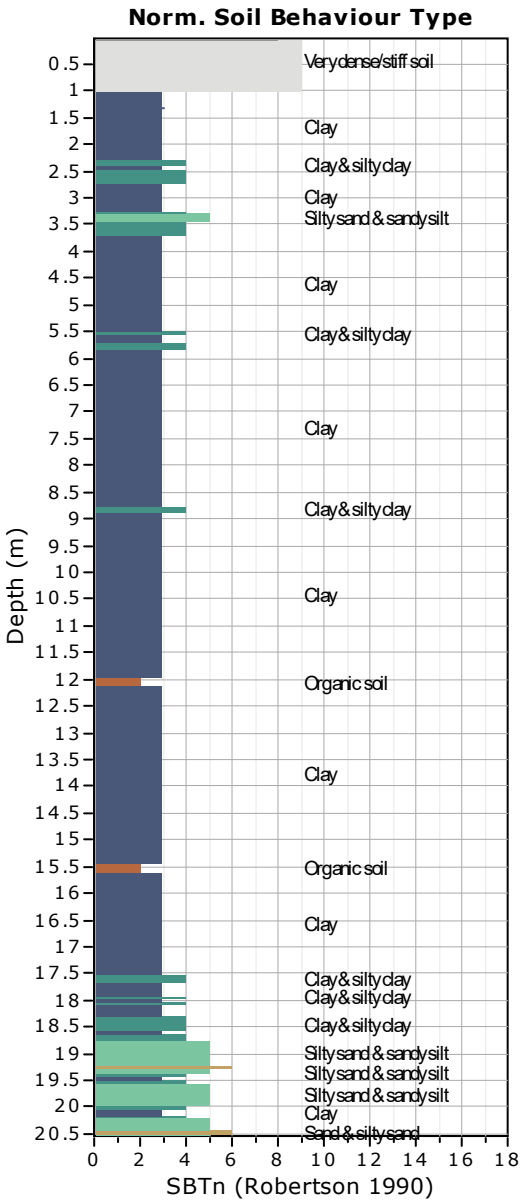
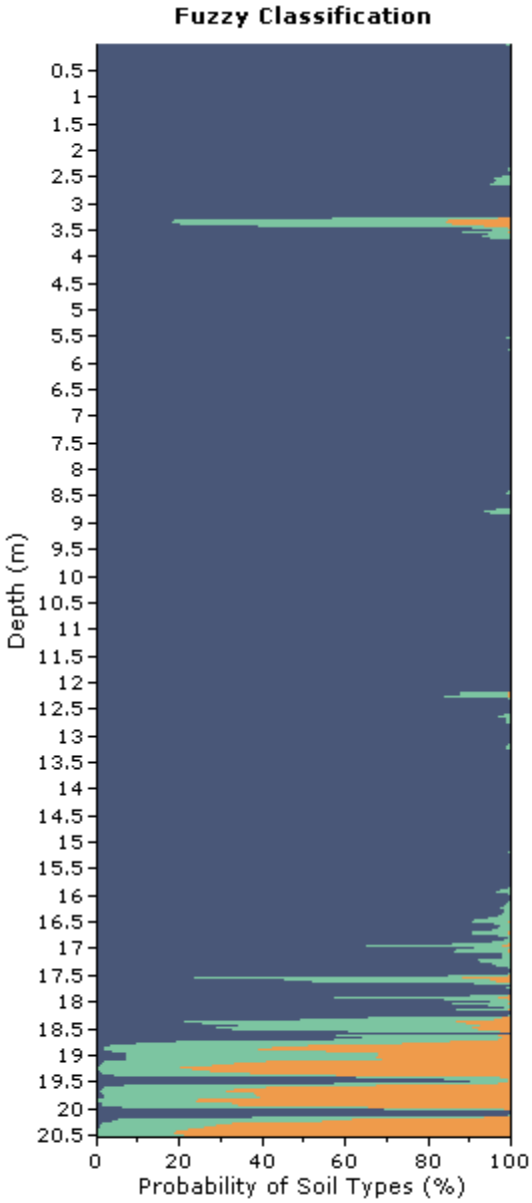
CPT: CPTu-01
Total depth: 20.54 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:





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Project:
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CPT: CPTu-01
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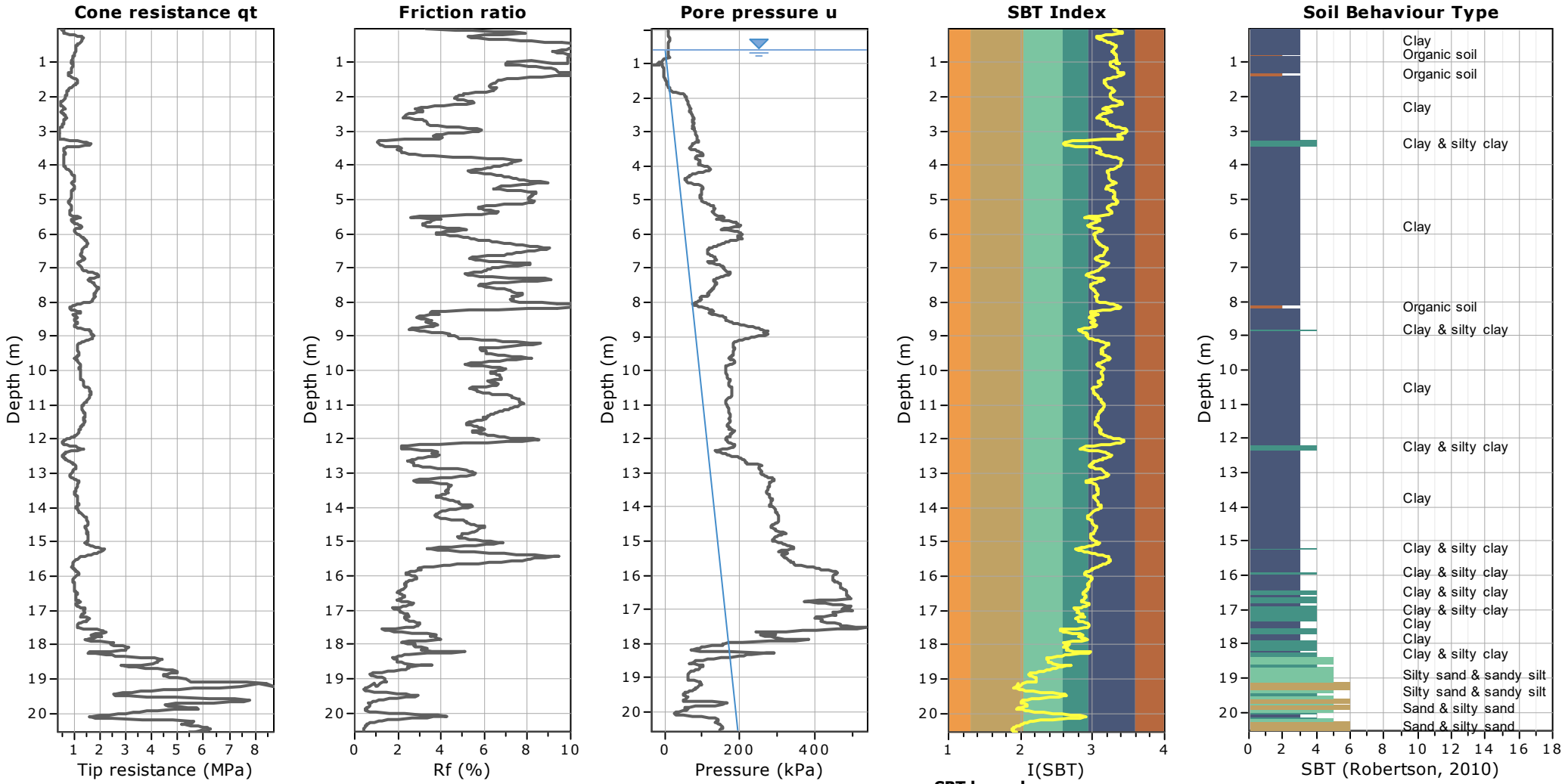
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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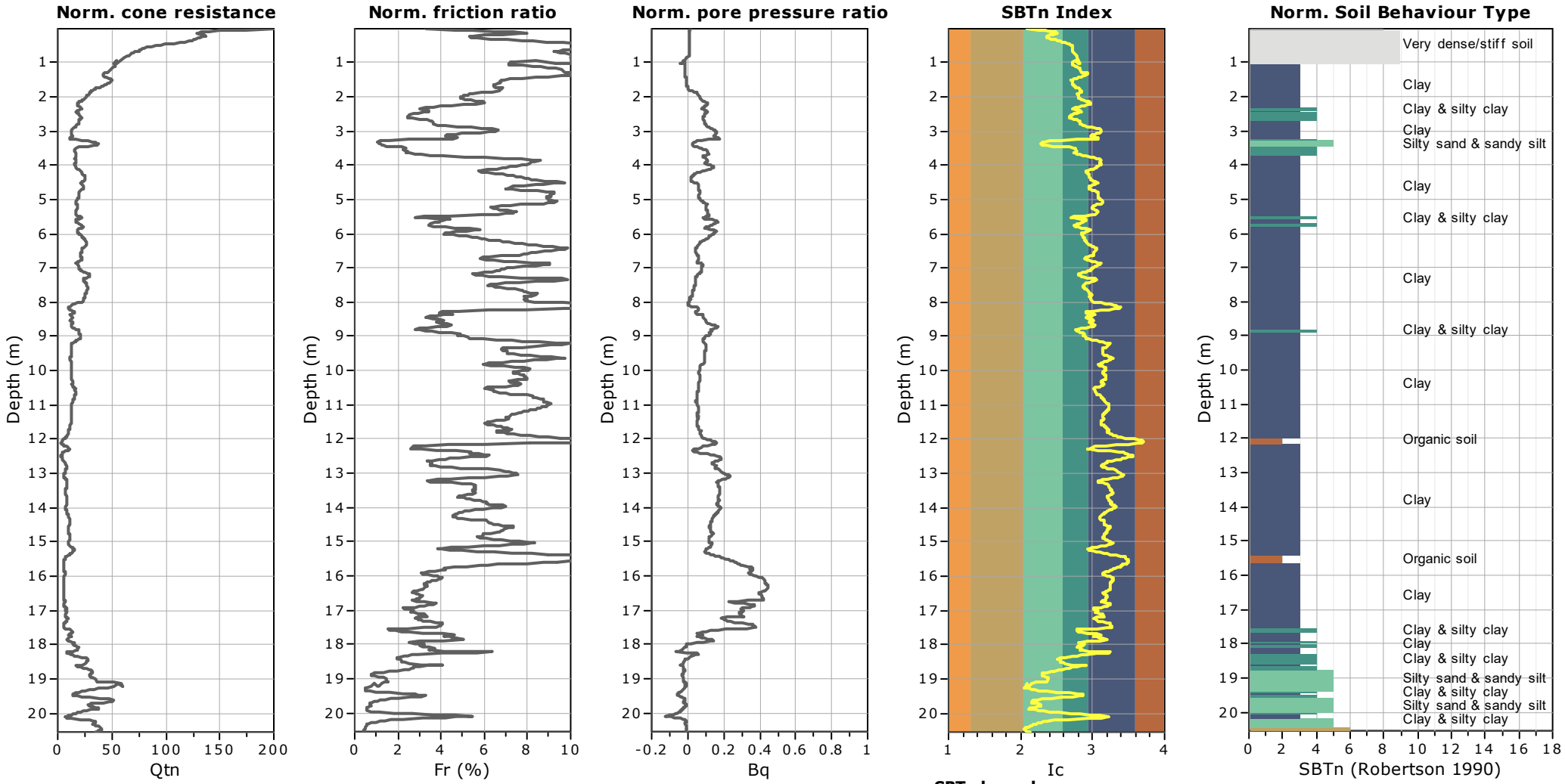
Project:
Location:

CPT: CPTu-01
Total depth: 20.54 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



SBTn legend

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5. Silty sand to sandy silt
6. Clean sand to silty sand
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9. Very stiff fine grained

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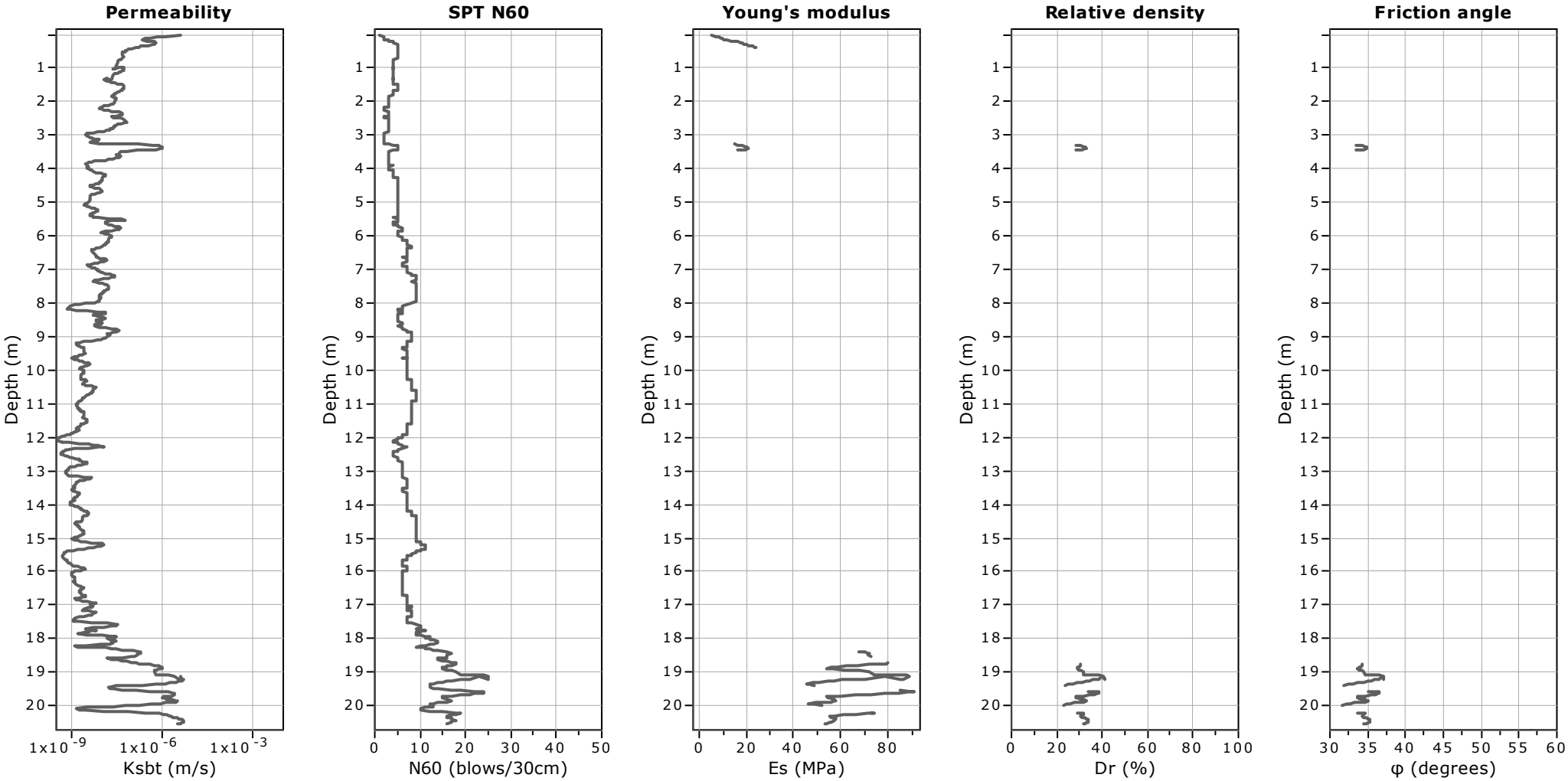
CPT: CPTu-01
Total depth: 20.54 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:



Calculation parameters

Permeability: Based on SBT_n
SPT N_{60}: Based on I_c and q_t
Young's modulus: Based on variable alpha using I_c (Robertson, 2009)
Relative desnisty constant, C_{Dr}: 350.0
Phi: Based on Kulhawy & Mayne (1990)
User defined estimation data

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Project:
Location:

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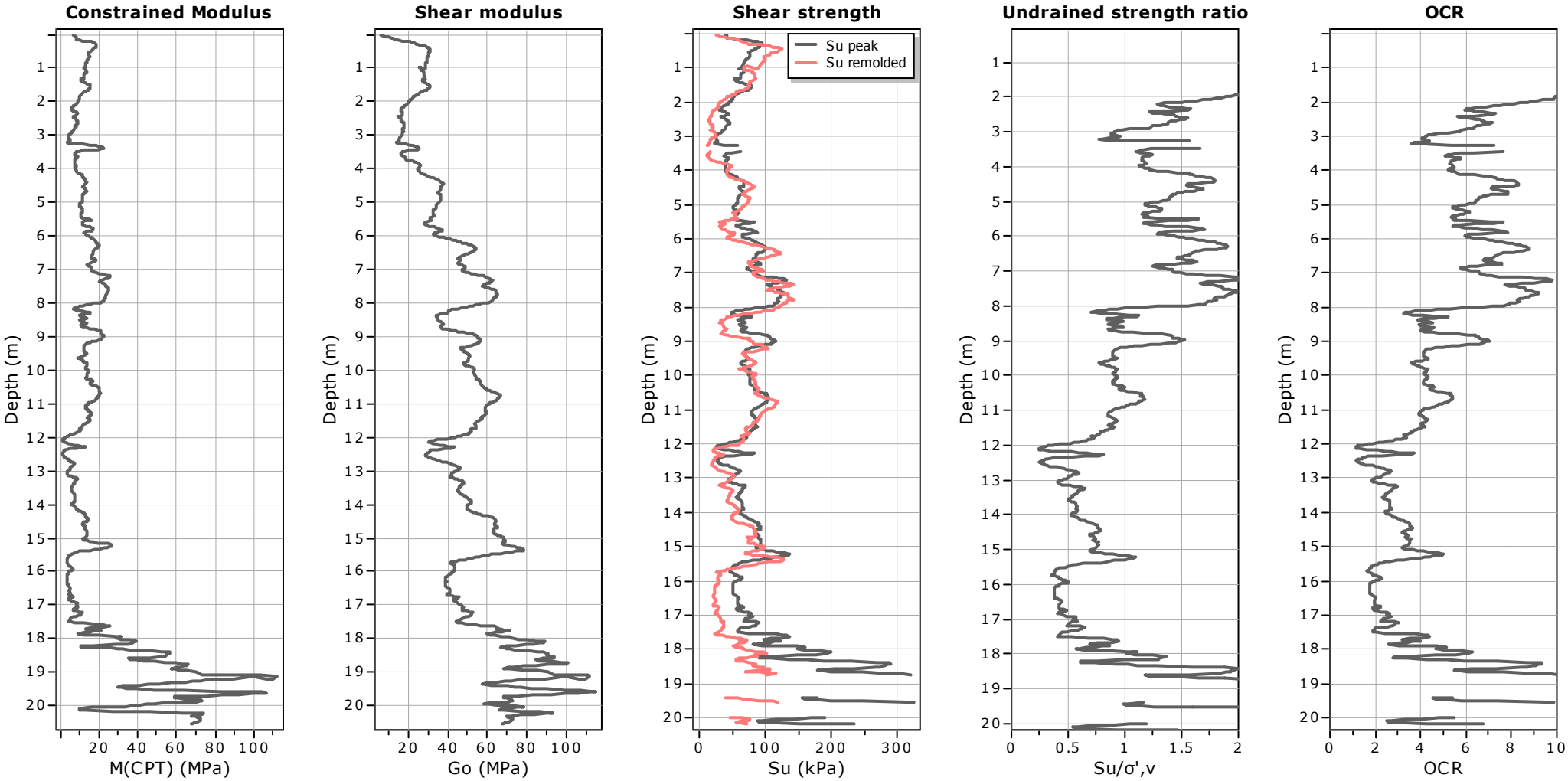
Total depth: 20.54 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Constrained modulus: Based on variable *alpha* using I_c and Q_{tn} (Robertson, 2009)
Go: Based on variable *alpha* using I_c (Robertson, 2009)
Undrained shear strength cone factor for clays, N_{kt}: 14

OCR factor for clays, N_{kt}: 0.33
User defined estimation data

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Project:
Location:

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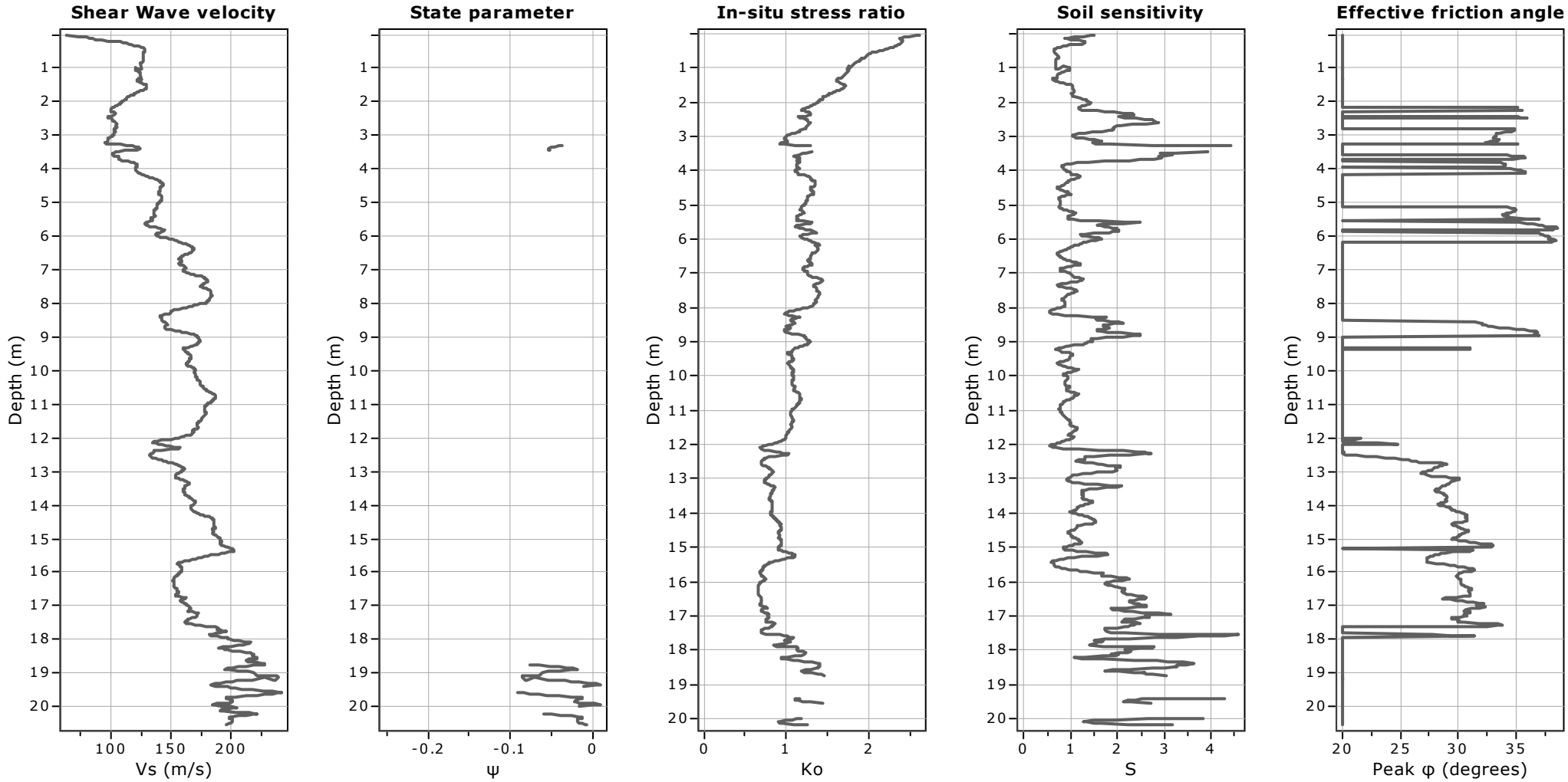
Total depth: 20.54 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Soil Sensitivity factor, N_S: 7.00

User defined estimation data

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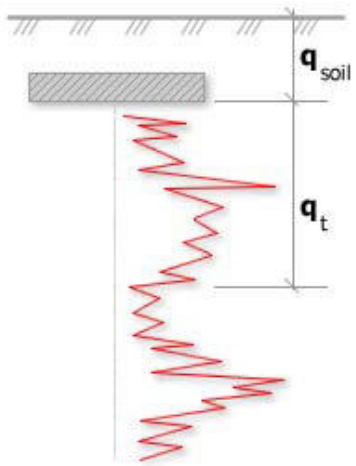
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

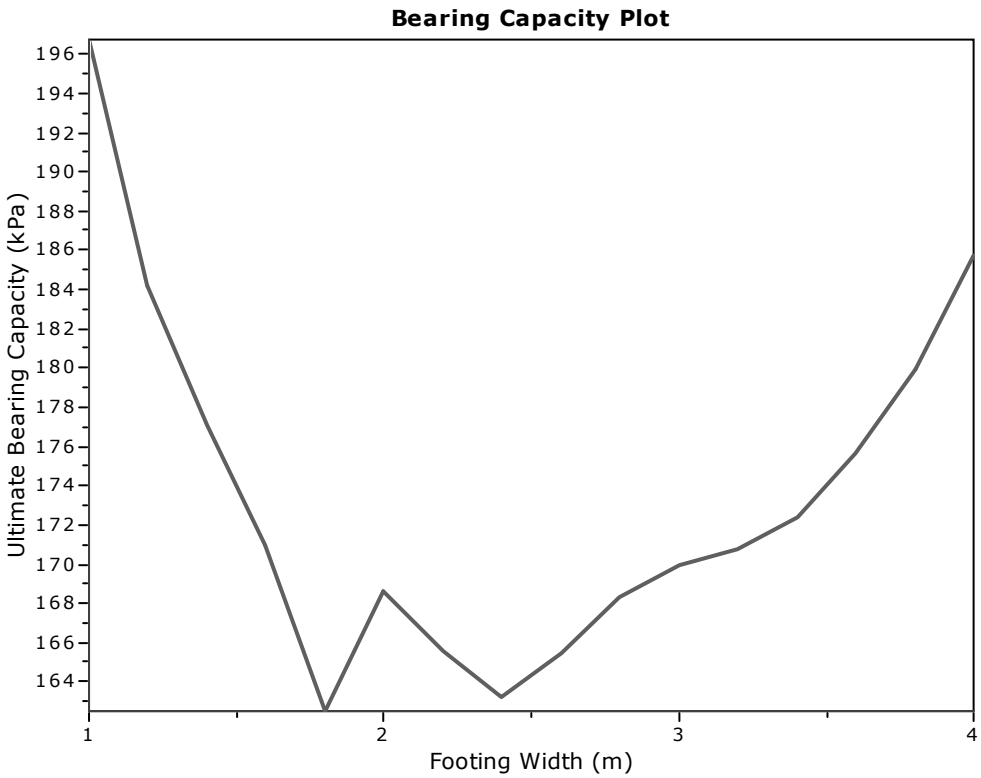
Project:
Location:



Bearing Capacity calculation is perfromed based on the formula:

$$Q_{ult} = R_k \times q_t + q_{soil}$$

where:
R_k: Bearing capacity factor
q_t: Average corrected cone resistance over calculation depth
q_{soil}: Pressure applied by soil above footing



:: Tabular results ::

No	B (m)	Start Depth (m)	End Depth (m)	Ave. q_t (MPa)	R_k	Soil Press. (kPa)	Ult. bearing cap. (kPa)
1	1.00	0.50	2.00	0.94	0.20	9.50	196.74
2	1.20	0.50	2.30	0.87	0.20	9.50	184.24
3	1.40	0.50	2.60	0.84	0.20	9.50	177.08
4	1.60	0.50	2.90	0.81	0.20	9.50	171.01
5	1.80	0.50	3.20	0.77	0.20	9.50	162.52
6	2.00	0.50	3.50	0.80	0.20	9.50	168.60
7	2.20	0.50	3.80	0.78	0.20	9.50	165.59
8	2.40	0.50	4.10	0.77	0.20	9.50	163.21
9	2.60	0.50	4.40	0.78	0.20	9.50	165.49
10	2.80	0.50	4.70	0.79	0.20	9.50	168.27
11	3.00	0.50	5.00	0.80	0.20	9.50	169.92
12	3.20	0.50	5.30	0.81	0.20	9.50	170.73
13	3.40	0.50	5.60	0.81	0.20	9.50	172.43
14	3.60	0.50	5.90	0.83	0.20	9.50	175.69
15	3.80	0.50	6.20	0.85	0.20	9.50	179.98
16	4.00	0.50	6.50	0.88	0.20	9.50	185.78

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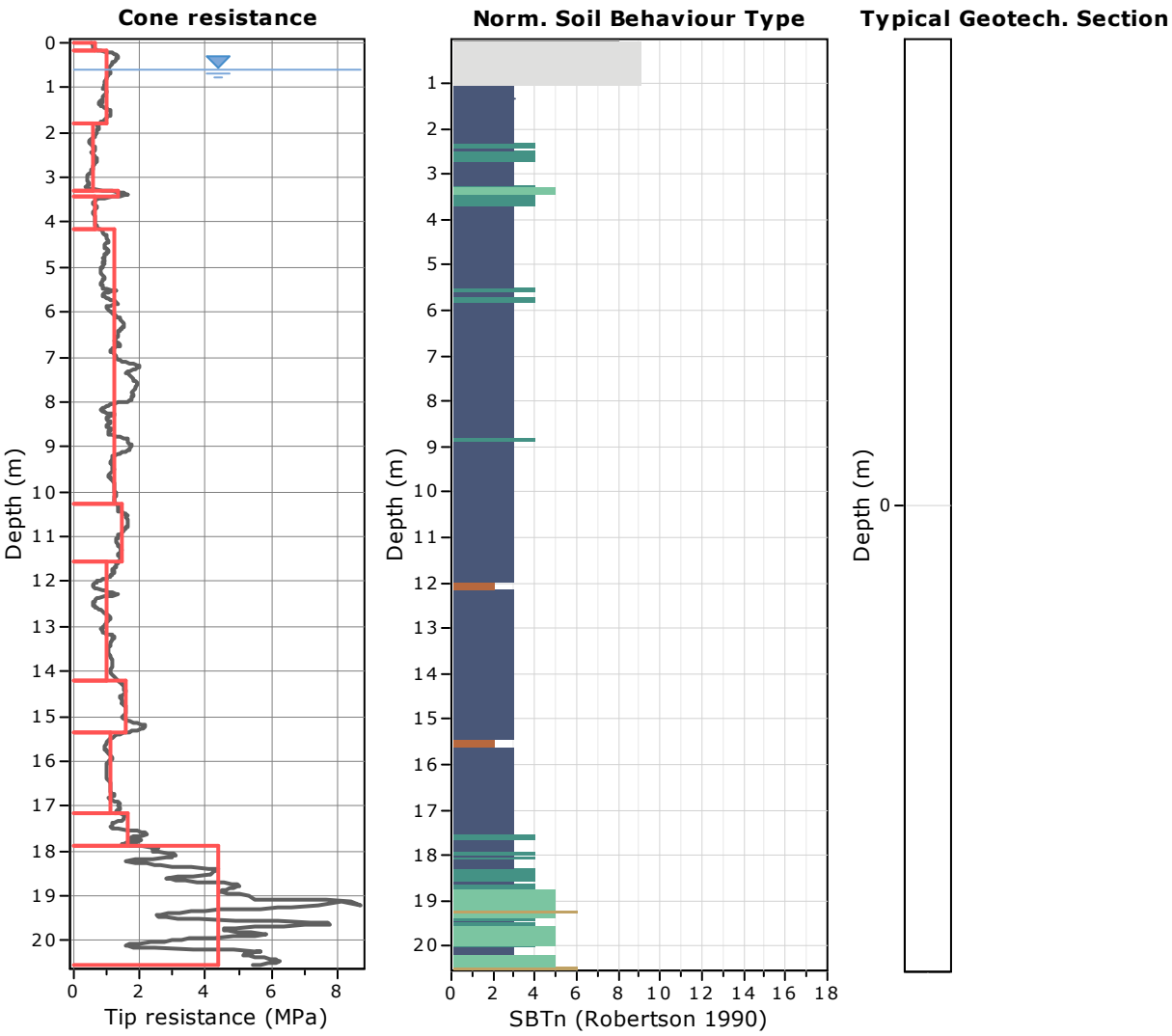
Total depth: 20.54 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Tabular results

.:: Layer No: 1 ::.

Code: R **Start depth:** 0.00 (m), **End depth:** 0.18 (m)

Description: Very dense/stiff soil

Basic results	Estimation results	
Total cone resistance: 0.62 ±0.10 MPa	Permeability: 9.03E-07 ±1.17E-06 m/s	Constrained Mod.: 8.61 ±1.46 MPa
Sleeve friction: 37.80 ±14.77 kPa	N60: 2.11 ±0.60 blows	Go: 11.59 ±3.25 MPa
SBT_n: 9	Es: 9.77 ±2.20 MPa	Su: 45.35 ±6.49 kPa
SBTn description: Very dense/stiff soil	Dr (%): 0.00 ±0.00	Su ratio: 10.29 ±1.21
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 47.53 ±5.60
	Unit weight: 16.92 ±0.51 kN/m³	

.:: Layer No: 2 ::.

Code: A **Start depth:** 0.18 (m), **End depth:** 1.80 (m)

Description: Very dense/stiff soil

Basic results	**Estimation results**	
Total cone resistance: 1.02 ±0.15 MPa	Permeability: 8.86E-08 ±1.40E-07 m/s	Constrained Mod.: 13.99 ±2.17 MPa
Sleeve friction: 84.10 ±18.67 kPa	N60: 4.38 ±0.51 blows	Go: 28.00 ±2.66 MPa
SBT_n: 9	Es: 19.44 ±3.34 MPa	Su: 71.37 ±11.08 kPa
SBTn description: Very dense/stiff soil	Dr (%): 0.00 ±0.00	Su ratio: 4.87 ±2.19
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 22.49 ±10.13
	Unit weight: 18.06 ±0.28 kN/m³	

.:: Layer No: 3 ::.

Code: E **Start depth:** 1.80 (m), **End depth:** 3.28 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 0.58 ±0.12 MPa	Permeability: 2.44E-08 ±2.20E-08 m/s	Constrained Mod.: 7.33 ±1.85 MPa
Sleeve friction: 23.25 ±8.79 kPa	N60: 2.69 ±0.52 blows	Go: 17.75 ±2.24 MPa
SBT_n: 3	Es: 14.74 ±14.74 MPa	Su: 37.96 ±8.55 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.41 ±0.39
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 6.51 ±1.80
	Unit weight: 16.32 ±0.42 kN/m³	

.:: Layer No: 4 ::.

Code: A2 **Start depth:** 3.28 (m), **End depth:** 3.44 (m)

Description: Silty sand & sandy silt

Basic results	**Estimation results**	
Total cone resistance: 1.37 ±0.26 MPa	Permeability: 6.57E-07 ±2.96E-07 m/s	Constrained Mod.: 18.38 ±3.64 MPa
Sleeve friction: 16.12 ±2.77 kPa	N60: 4.56 ±0.73 blows	Go: 23.32 ±2.52 MPa
SBT_n: 5	Es: 19.09 ±1.50 MPa	Su: 0.00 ±0.00 kPa
SBTn description: Silty sand & sandy silt	Dr (%): 30.89 ±1.80	Su ratio: 0.00 ±0.00
	ö (degrees): 34.34 ±0.57 °	O.C.R.: 0.00 ±0.00
	Unit weight: 16.29 ±0.25 kN/m³	

.:: Layer No: 5 ::.

Code: E2 **Start depth:** 3.44 (m), **End depth:** 4.16 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 0.67 ±0.11 MPa	Permeability: 2.75E-08 ±5.42E-08 m/s	Constrained Mod.: 8.47 ±1.52 MPa
Sleeve friction: 30.69 ±14.24 kPa	N60: 3.27 ±0.45 blows	Go: 22.23 ±3.86 MPa
SBT_n: 3	Es: 16.18 ±16.18 MPa	Su: 42.22 ±4.87 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.21 ±0.11
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 5.57 ±0.50
	Unit weight: 16.63 ±0.60 kN/m³	

.:: Layer No: 6 ::.

Code: A3 **Start depth:** 4.16 (m), **End depth:** 10.28 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.25 ±0.31 MPa	Permeability: 9.06E-09 ±8.13E-09 m/s	Constrained Mod.: 15.32 ±4.43 MPa
Sleeve friction: 77.73 ±28.49 kPa	N60: 6.48 ±1.40 blows	Go: 45.49 ±10.17 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 80.25 ±21.08 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.36 ±0.36
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 6.27 ±1.67
	Unit weight: 17.99 ±0.51 kN/m³	

.:: Layer No: 7 ::.

Code: D **Start depth:** 10.28 (m), **End depth:** 11.56 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.45 ±0.11 MPa	Permeability: 2.80E-09 ±1.18E-09 m/s	Constrained Mod.: 16.55 ±2.44 MPa
Sleeve friction: 94.32 ±12.73 kPa	N60: 8.23 ±0.46 blows	Go: 59.82 ±3.41 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 89.51 ±8.28 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.98 ±0.11
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 4.52 ±0.51
	Unit weight: 18.35 ±0.17 kN/m³	

.:: Layer No: 8 ::.

Code: A4 **Start depth:** 11.56 (m), **End depth:** 14.22 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.02 ±0.21 MPa	Permeability: 1.63E-09 ±1.59E-09 m/s	Constrained Mod.: 6.32 ±2.96 MPa
Sleeve friction: 45.19 ±15.44 kPa	N60: 6.21 ±0.98 blows	Go: 44.04 ±7.31 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 56.85 ±14.90 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.53 ±0.14
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.45 ±0.65
	Unit weight: 17.30 ±0.49 kN/m³	

.:: Layer No: 9 ::.

Code: D2 **Start depth:** 14.22 (m), **End depth:** 15.38 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.61 ±0.21 MPa	Permeability: 2.86E-09 ±2.44E-09 m/s	Constrained Mod.: 15.00 ±4.36 MPa
Sleeve friction: 83.67 ±16.21 kPa	N60: 9.22 ±0.79 blows	Go: 65.44 ±5.78 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 96.15 ±14.53 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.79 ±0.11
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 3.64 ±0.49
	Unit weight: 18.24 ±0.23 kN/m³	

.:: Layer No: 10 ::.

Code: A5 **Start depth:** 15.38 (m), **End depth:** 17.18 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.12 ±0.14 MPa	Permeability: 1.78E-09 ±1.27E-09 m/s	Constrained Mod.: 5.32 ±1.80 MPa
Sleeve friction: 37.03 ±25.22 kPa	N60: 6.68 ±0.84 blows	Go: 45.46 ±8.24 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 59.47 ±9.76 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.45 ±0.07
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.06 ±0.32
	Unit weight: 17.03 ±0.54 kN/m³	

.:: Layer No: 11 ::.

Code: B **Start depth:** 17.18 (m), **End depth:** 17.90 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.61 ±0.34 MPa	Permeability: 7.20E-09 ±8.67E-09 m/s	Constrained Mod.: 12.71 ±6.33 MPa
Sleeve friction: 43.98 ±15.27 kPa	N60: 8.57 ±1.21 blows	Go: 55.70 ±8.34 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 93.20 ±24.14 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.65 ±0.17
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 3.02 ±0.77
	Unit weight: 17.45 ±0.43 kN/m³	

.:: Layer No: 12 ::.

Code: F **Start depth:** 17.90 (m), **End depth:** 20.54 (m)

Description: Clay & silty clay

Basic results	**Estimation results**	
Total cone resistance: 4.38 ±1.70 MPa	Permeability: 1.03E-06 ±1.39E-06 m/s	Constrained Mod.: 55.01 ±23.32 MPa
Sleeve friction: 62.54 ±28.32 kPa	N60: 15.62 ±3.58 blows	Go: 80.51 ±13.54 MPa
SBT_n: 4	Es: 74.30 ±5.29 MPa	Su: 191.37 ±63.63 kPa
SBTn description: Clay & silty clay	Dr (%): 0.00 ±0.00	Su ratio: 1.28 ±0.45
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 5.91 ±2.08
	Unit weight: 18.15 ±0.57 kN/m³	

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Project:
Location:

CPT: CPTu-01
Total depth: 20.54 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Summary table of mean values

From depth To depth (m)	Thickness (m)	Permeability (m/s)	SPT_{N60} (blows/30cm)	E_s (MPa)	D_r	Friction angle	Constrained modulus, M (MPa)	Shear modulus, G_O (MPa)	Undrained strength, S_U (kPa)	Undrained strength ratio	OCR	Unit weight (kN/m³)
0.00	0.18	9.03E-07	2.1	9.8	0.0	0.0	8.6	11.6	45.4	10.3	47.5	16.9
0.18		(±1.17E-06)	(±0.6)	(±2.2)	(±0.0)	(±0.0)	(±1.5)	(±3.2)	(±6.5)	(±1.2)	(±5.6)	(±0.5)
0.18	1.62	8.86E-08	4.4	19.4	0.0	0.0	14.0	28.0	71.4	4.9	22.5	18.1
1.80		(±1.40E-07)	(±0.5)	(±3.3)	(±0.0)	(±0.0)	(±2.2)	(±2.7)	(±11.1)	(±2.2)	(±10.1)	(±0.3)
1.80	1.48	2.44E-08	2.7	14.7	0.0	0.0	7.3	17.8	38.0	1.4	6.5	16.3
3.28		(±2.20E-08)	(±0.5)	(±14.7)	(±0.0)	(±0.0)	(±1.8)	(±2.2)	(±8.6)	(±0.4)	(±1.8)	(±0.4)
3.28	0.16	6.57E-07	4.6	19.1	30.9	34.3	18.4	23.3	0.0	0.0	0.0	16.3
3.44		(±2.96E-07)	(±0.7)	(±1.5)	(±1.8)	(±0.6)	(±3.6)	(±2.5)	(±0.0)	(±0.0)	(±0.0)	(±0.2)
3.44	0.72	2.75E-08	3.3	16.2	0.0	0.0	8.5	22.2	42.2	1.2	5.6	16.6
4.16		(±5.42E-08)	(±0.5)	(±16.2)	(±0.0)	(±0.0)	(±1.5)	(±3.9)	(±4.9)	(±0.1)	(±0.5)	(±0.6)
4.16	6.12	9.06E-09	6.5	0.0	0.0	0.0	15.3	45.5	80.2	1.4	6.3	18.0
10.28		(±8.13E-09)	(±1.4)	(±0.0)	(±0.0)	(±0.0)	(±4.4)	(±10.2)	(±21.1)	(±0.4)	(±1.7)	(±0.5)
10.28	1.28	2.80E-09	8.2	0.0	0.0	0.0	16.6	59.8	89.5	1.0	4.5	18.3
11.56		(±1.18E-09)	(±0.5)	(±0.0)	(±0.0)	(±0.0)	(±2.4)	(±3.4)	(±8.3)	(±0.1)	(±0.5)	(±0.2)
11.56	2.66	1.63E-09	6.2	0.0	0.0	0.0	6.3	44.0	56.9	0.5	2.5	17.3
14.22		(±1.59E-09)	(±1.0)	(±0.0)	(±0.0)	(±0.0)	(±3.0)	(±7.3)	(±14.9)	(±0.1)	(±0.7)	(±0.5)
14.22	1.16	2.86E-09	9.2	0.0	0.0	0.0	15.0	65.4	96.2	0.8	3.6	18.2
15.38		(±2.44E-09)	(±0.8)	(±0.0)	(±0.0)	(±0.0)	(±4.4)	(±5.8)	(±14.5)	(±0.1)	(±0.5)	(±0.2)
15.38	1.80	1.78E-09	6.7	0.0	0.0	0.0	5.3	45.5	59.5	0.4	2.1	17.0
17.18		(±1.27E-09)	(±0.8)	(±0.0)	(±0.0)	(±0.0)	(±1.8)	(±8.2)	(±9.8)	(±0.1)	(±0.3)	(±0.5)
17.18	0.72	7.20E-09	8.6	0.0	0.0	0.0	12.7	55.7	93.2	0.7	3.0	17.5
17.90		(±8.67E-09)	(±1.2)	(±0.0)	(±0.0)	(±0.0)	(±6.3)	(±8.3)	(±24.1)	(±0.2)	(±0.8)	(±0.4)

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CPT: CPTu-01
Total depth: 20.54 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:

Summary table of mean values

From depth To depth (m)	Thickness (m)	Permeability (m/s)	SPT_{N60} (blows/30cm)	E_s (MPa)	D_r	Friction angle	Constrained modulus, M (MPa)	Shear modulus, G_O (MPa)	Undrained strength, S_U (kPa)	Undrained strength ratio	OCR	Unit weight (kN/m³)
17.90	2.64	1.03E-06	15.6	74.3	0.0	0.0	55.0	80.5	191.4	1.3	5.9	18.2
20.54		(±1.39E-06)	(±3.6)	(±5.3)	(±0.0)	(±0.0)	(±23.3)	(±13.5)	(±63.6)	(±0.5)	(±2.1)	(±0.6)

Depth values presented in this table are measured from free ground surface

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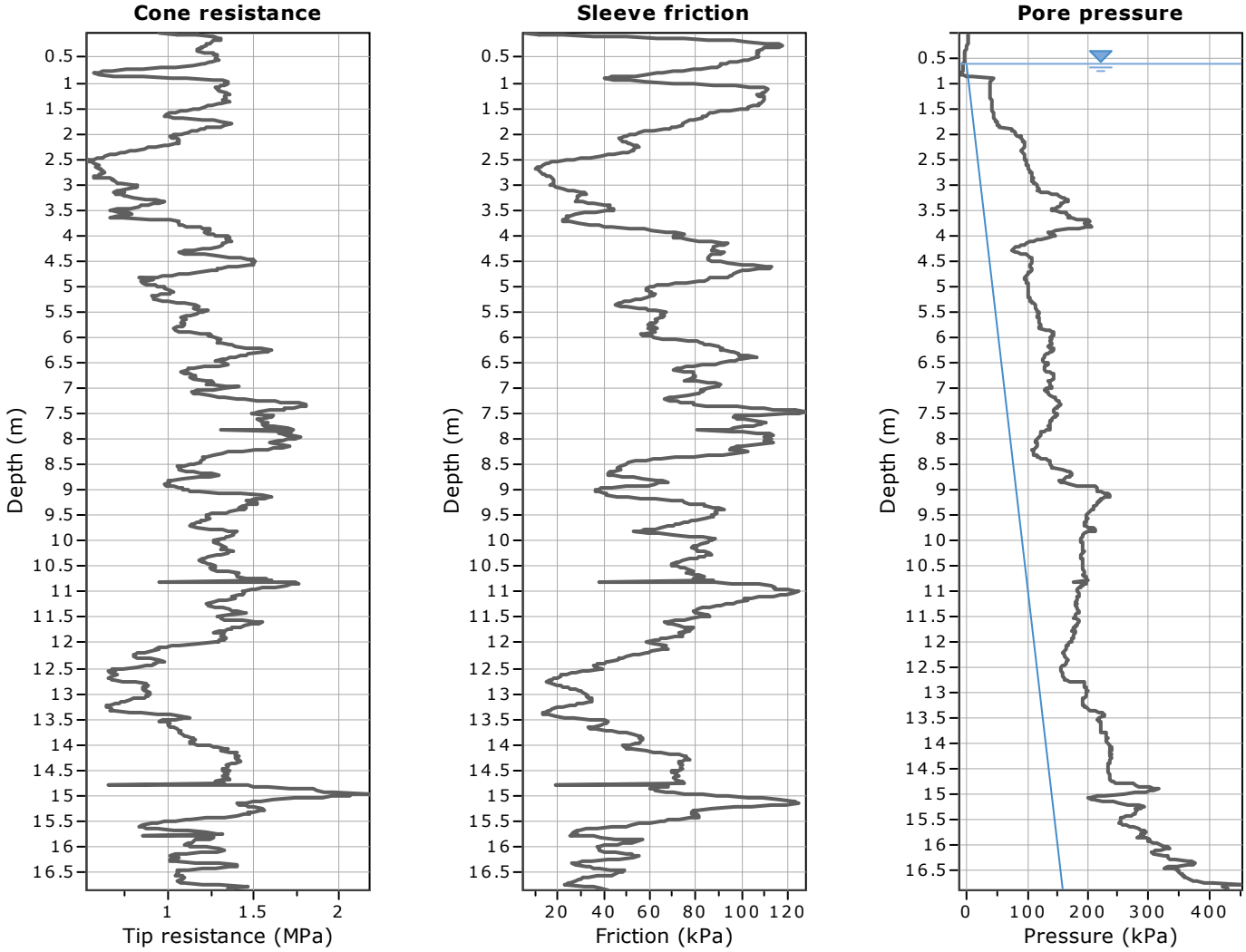
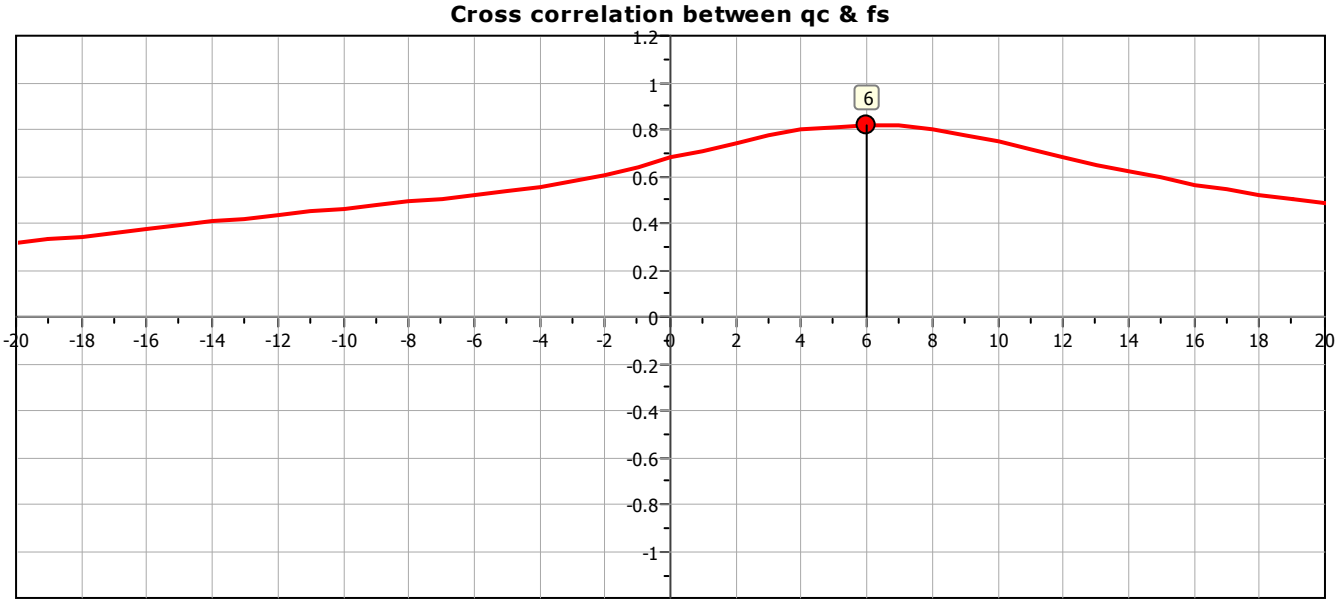
CPT: CPTu-02
Total depth: 16.86 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:



The plot below presents the cross correlation coeficient between the raw qc and fs values (as measured on the field). X axes presents the lag distance (one lag is the distance between two sucessive CPT measurements).



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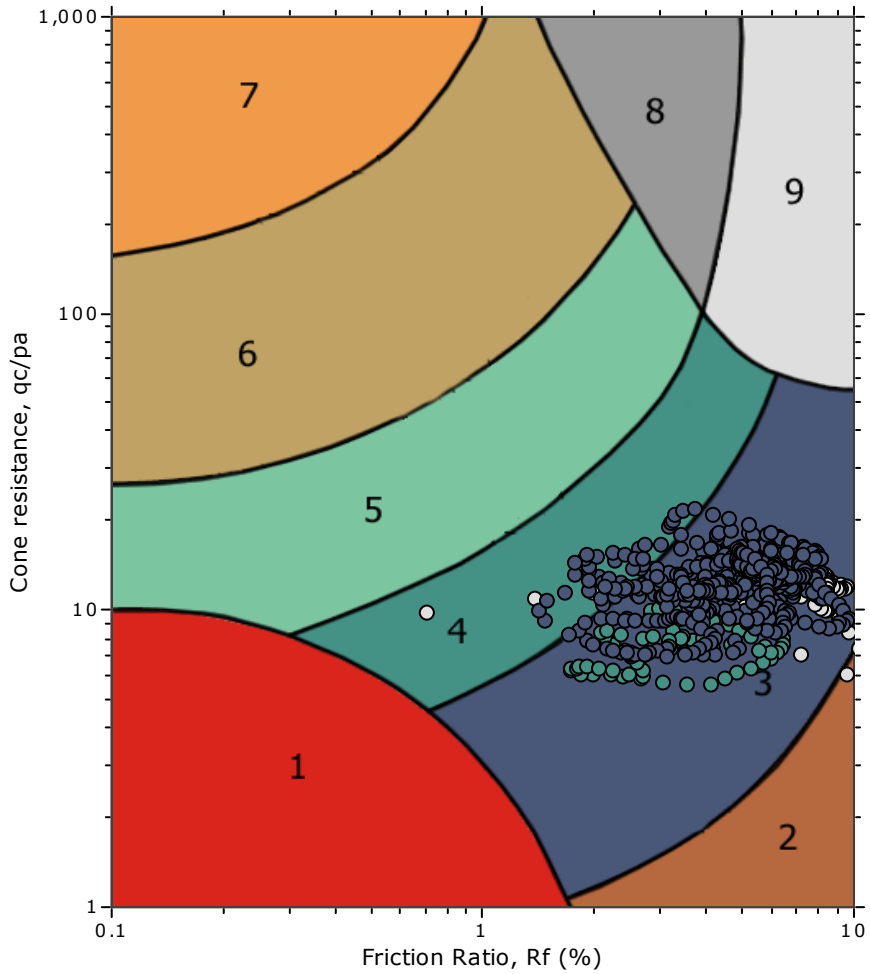
Project:
Location:

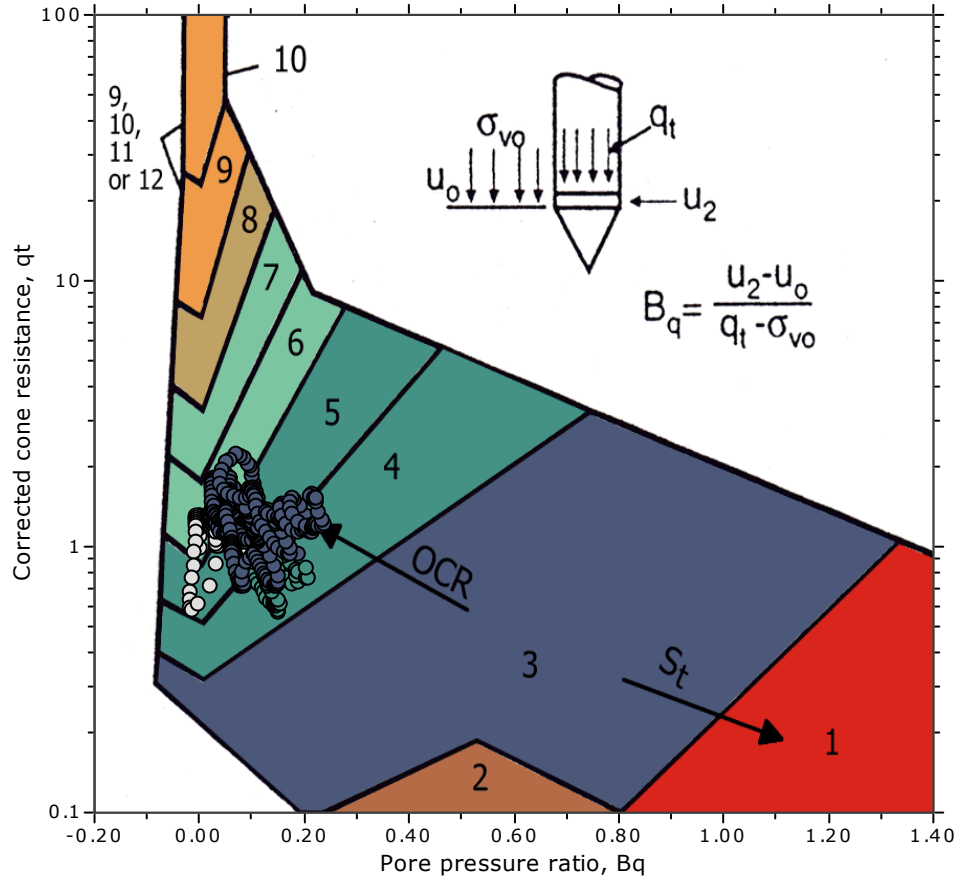
CPT: CPTu-02
Total depth: 16.86 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

SBT - Bq plots

SBT plot



Bq plot



SBT legend

- 1. Sensitive fine grained
- 2. Organic material
- 3. Clay to silty clay
- 4. Clayey silt to silty clay
- 5. Silty sand to sandy silt
- 6. Clean sand to silty sand
- 7. Gravely sand to sand
- 8. Very stiff sand to clayey sand
- 9. Very stiff fine grained

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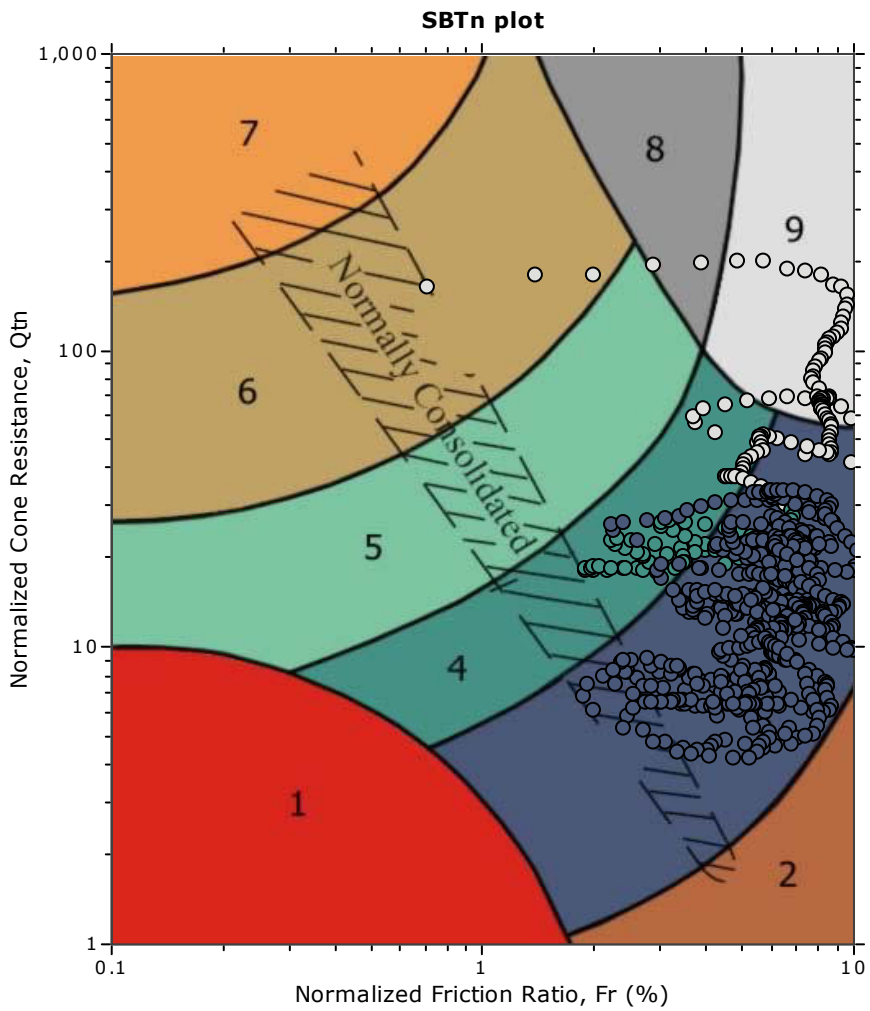
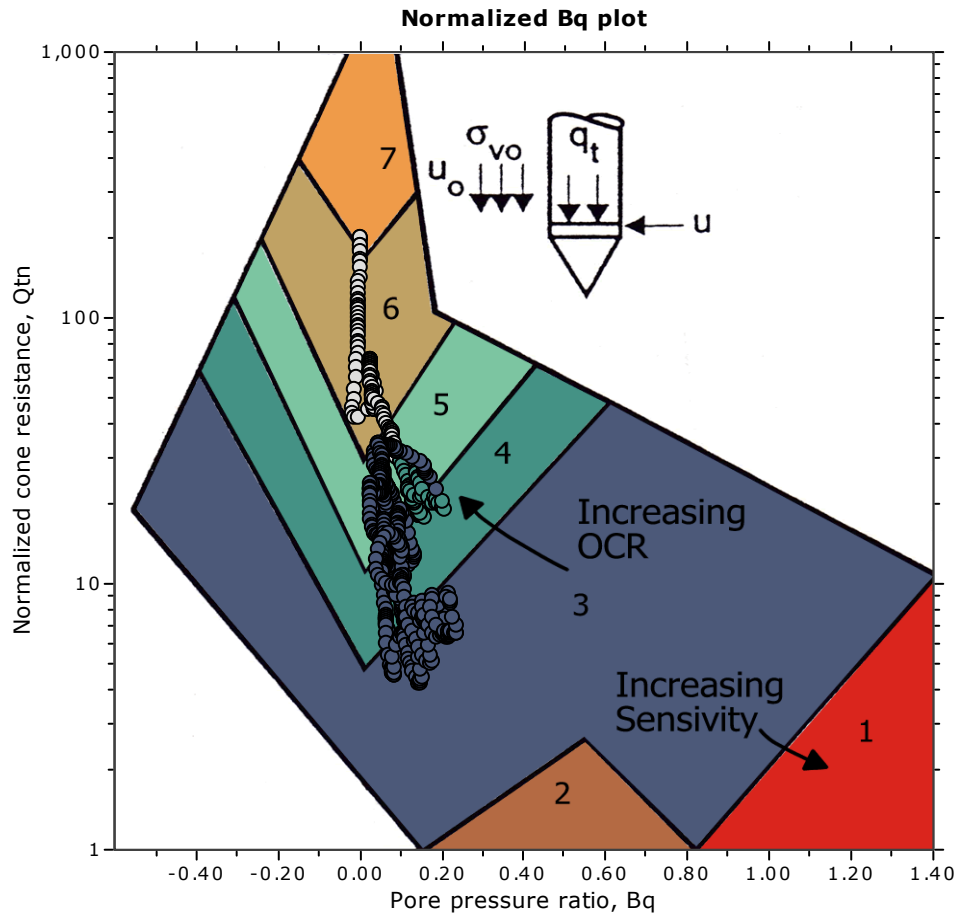
Project:
Location:

CPT: CPTu-02
Total depth: 16.86 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

SBT - Bq plots (normalized)





SBTn legend

- 1. Sensitive fine grained
- 2. Organic material
- 3. Clay to silty clay
- 4. Clayey silt to silty clay
- 5. Silty sand to sandy silt
- 6. Clean sand to silty sand
- 7. Gravely sand to sand
- 8. Very stiff sand to clayey sand
- 9. Very stiff fine grained

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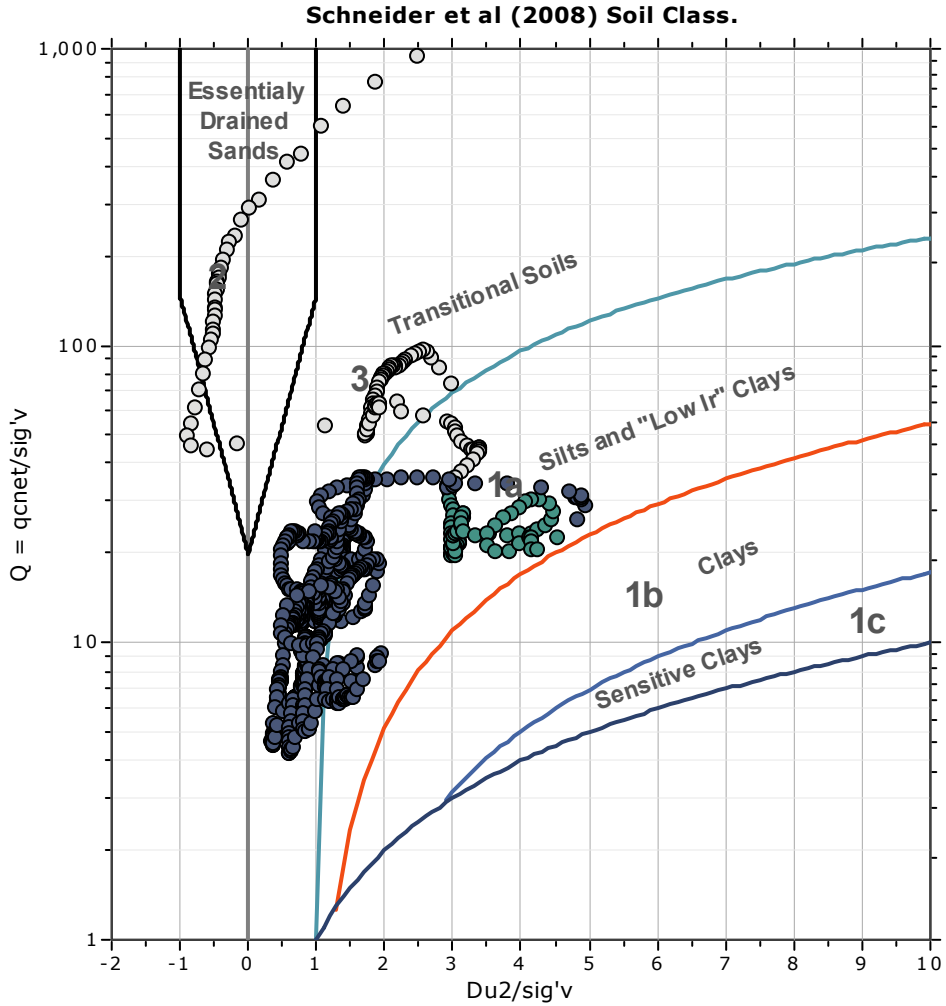
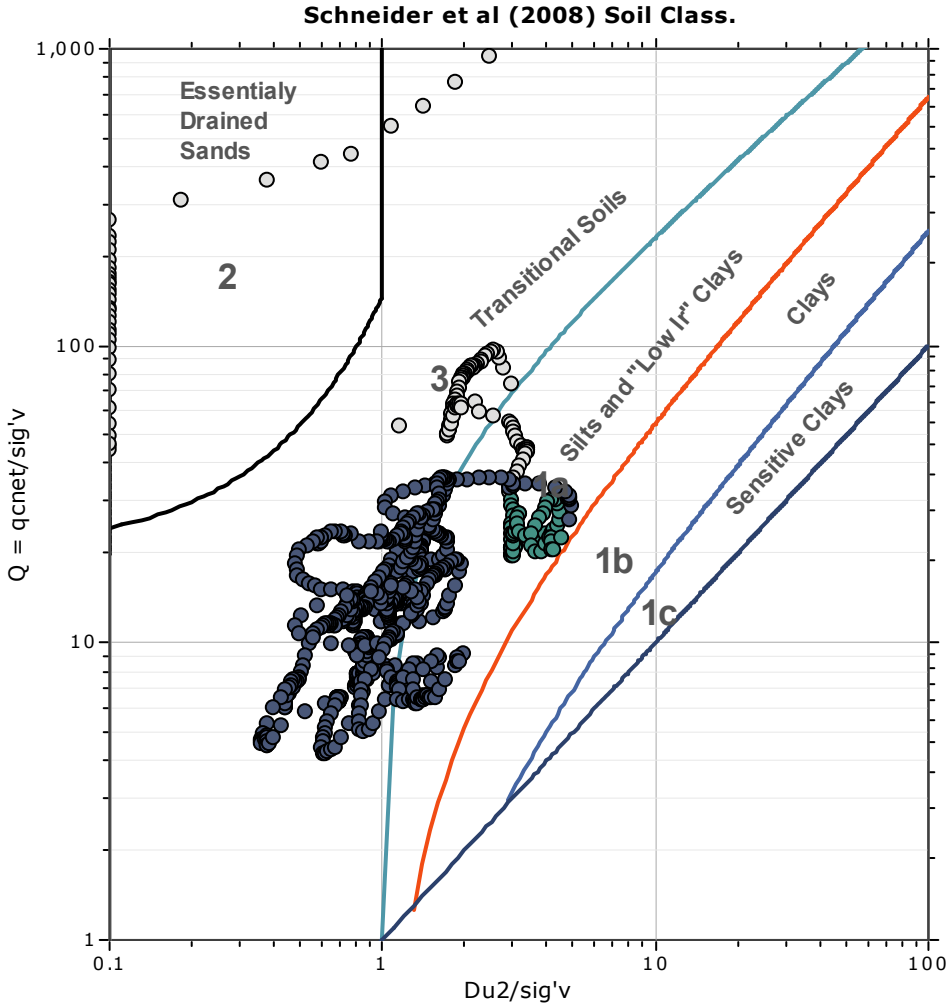
Project:
Location:

CPT: CPTu-02
Total depth: 16.86 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Bq plots (Schneider)





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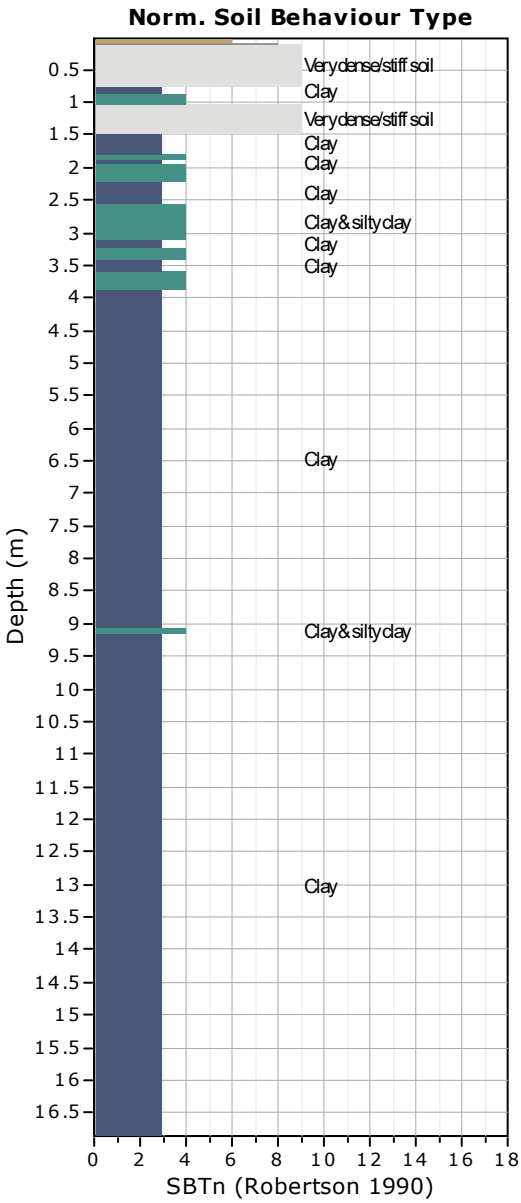
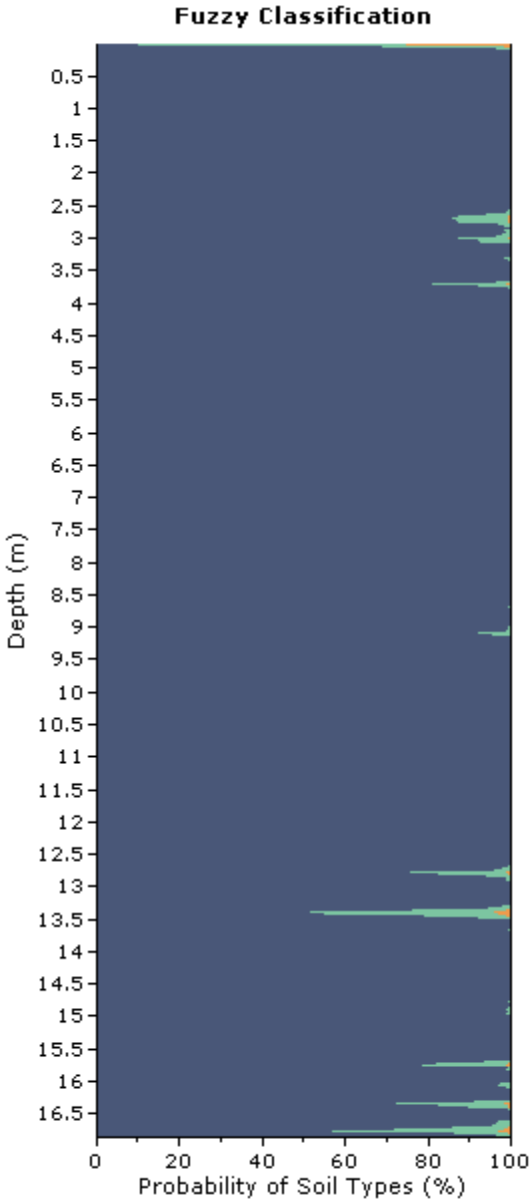
CPT: CPTu-02
Total depth: 16.86 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:





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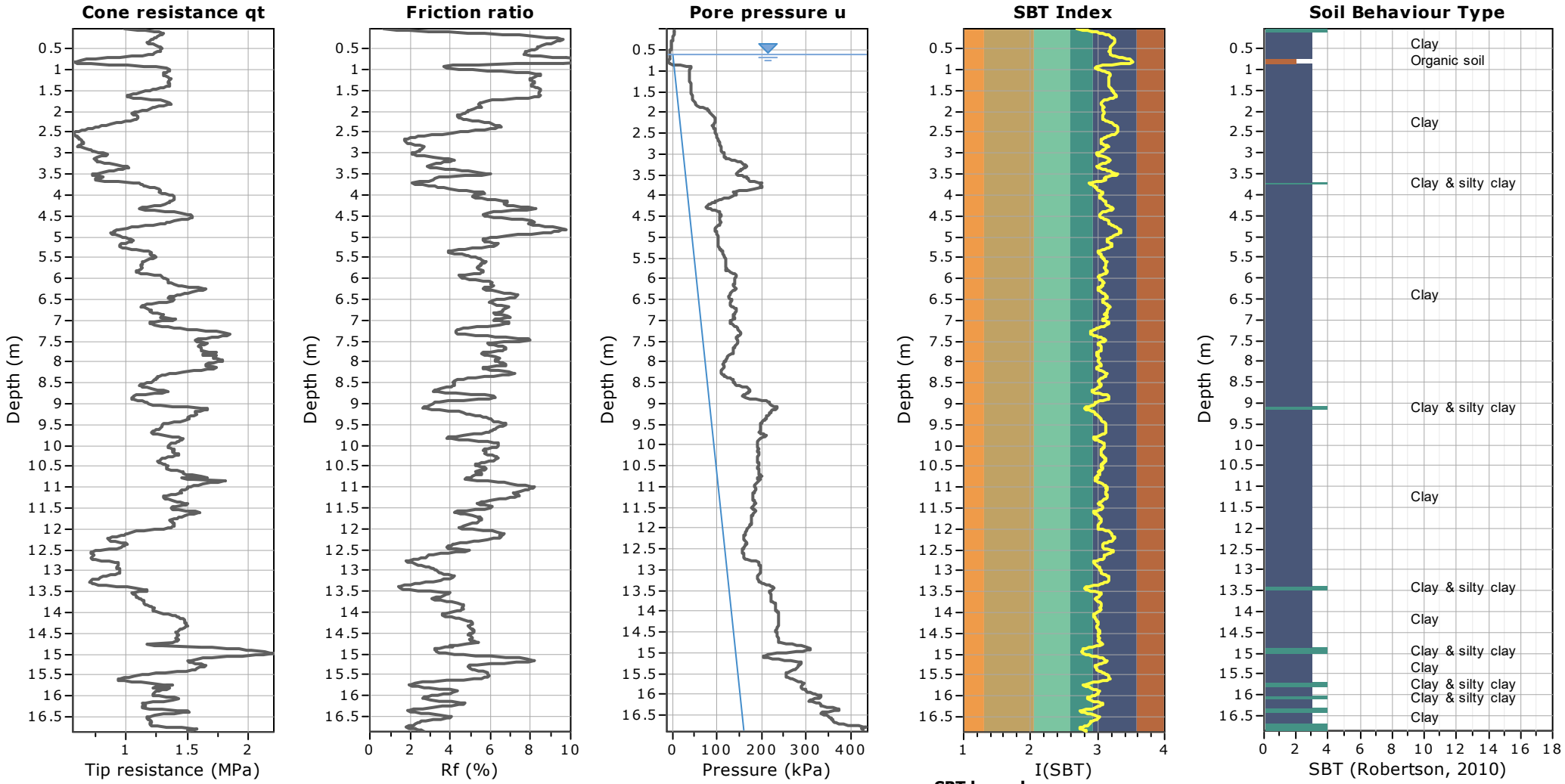
Project:
Location:

CPT: CPTu-02
Total depth: 16.86 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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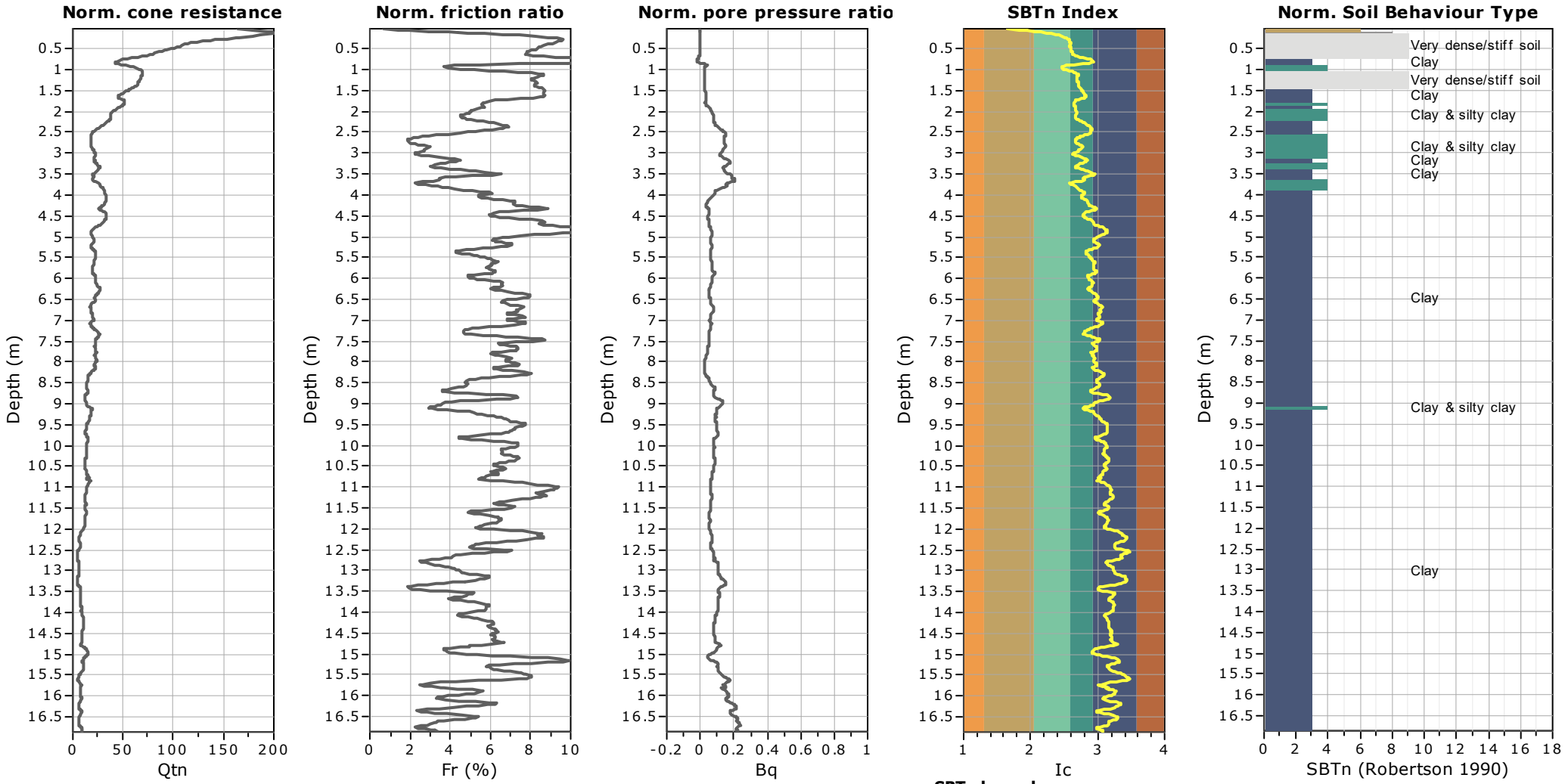
Project:
Location:

CPT: CPTu-02
Total depth: 16.86 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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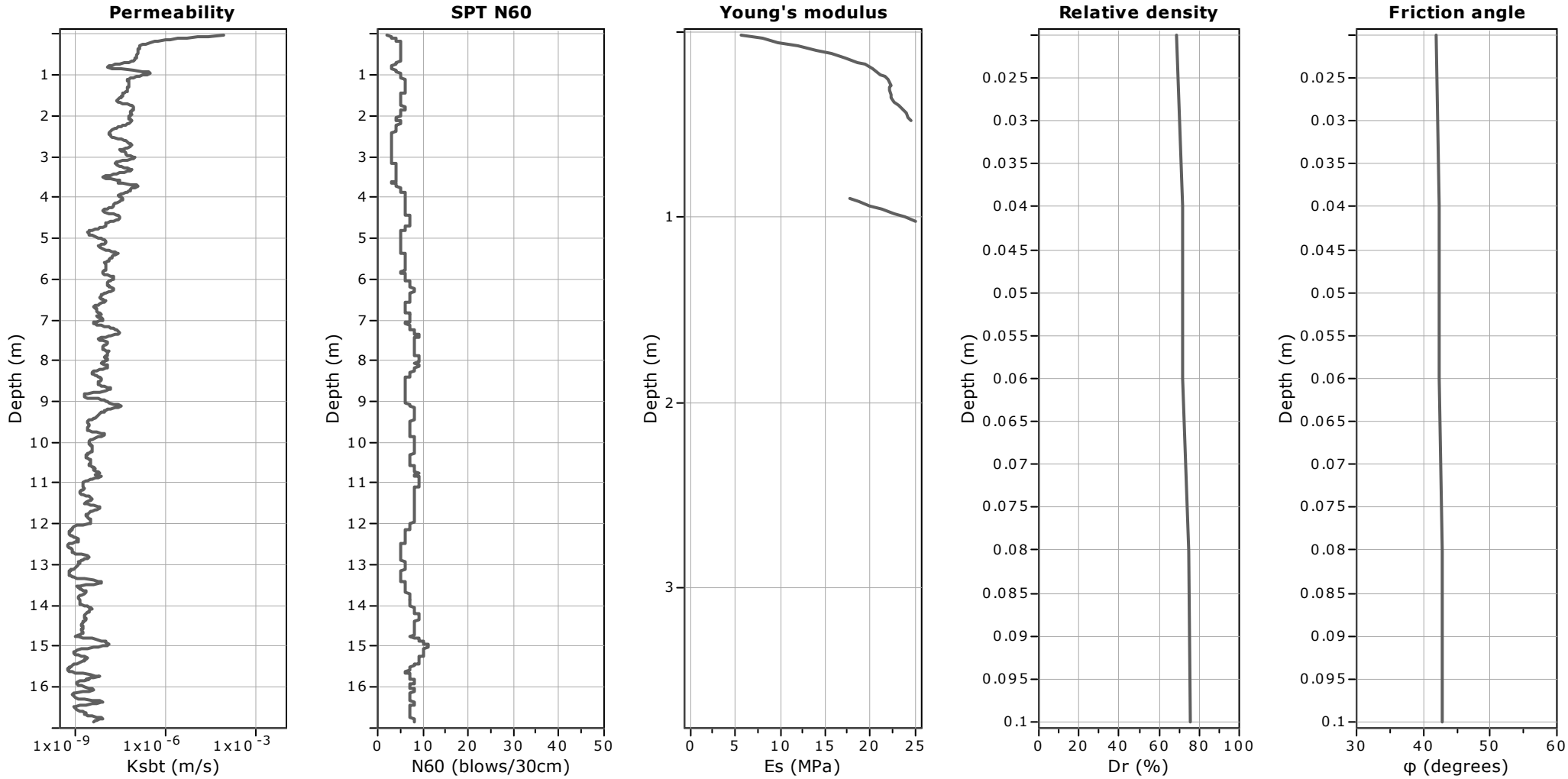
Project:
Location:

CPT: CPTu-02
Total depth: 16.86 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Permeability: Based on SBT_n
SPT N_{60}: Based on I_c and q_t
Young's modulus: Based on variable alpha using I_c (Robertson, 2009)
Relative desnisty constant, C_{Dr}: 350.0
Phi: Based on Kulhawy & Mayne (1990)
User defined estimation data

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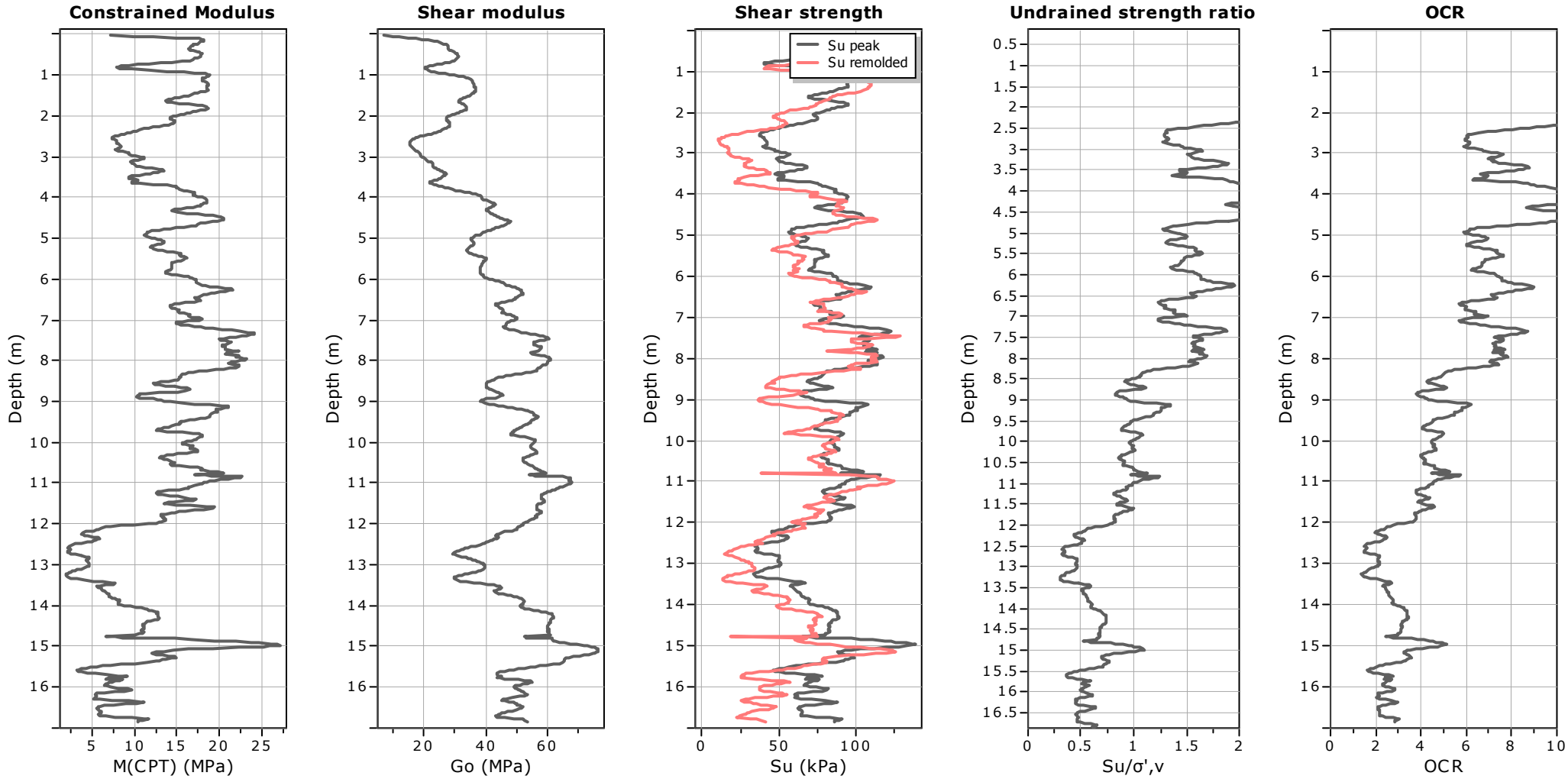
Project:
Location:

CPT: CPTu-02
Total depth: 16.86 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Constrained modulus: Based on variable *alpha* using I_c and Q_{tn} (Robertson, 2009)
Go: Based on variable *alpha* using I_c (Robertson, 2009)
Undrained shear strength cone factor for clays, N_{kt}: 14

OCR factor for clays, N_{kt}: 0.33
User defined estimation data

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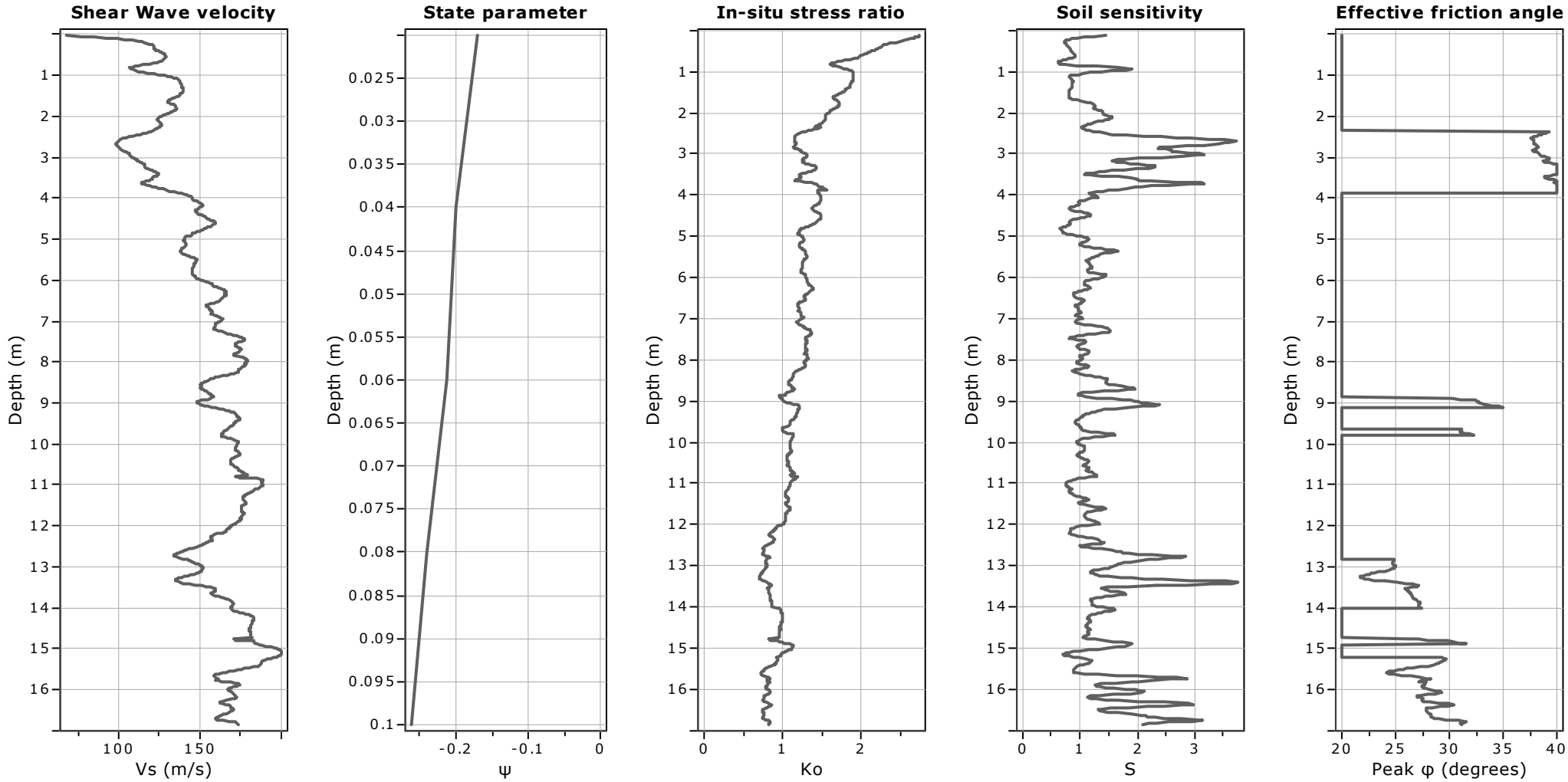
Project:
Location:

CPT: CPTu-02
Total depth: 16.86 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Soil Sensitivity factor, N_S: 7.00

User defined estimation data

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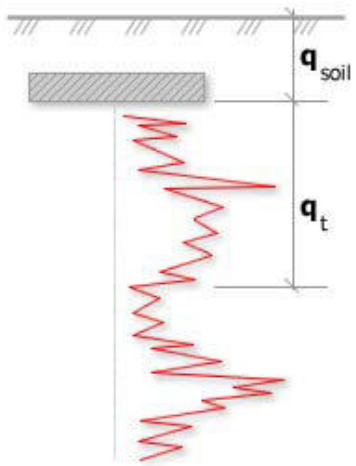
CPT: CPTu-02
Total depth: 16.86 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

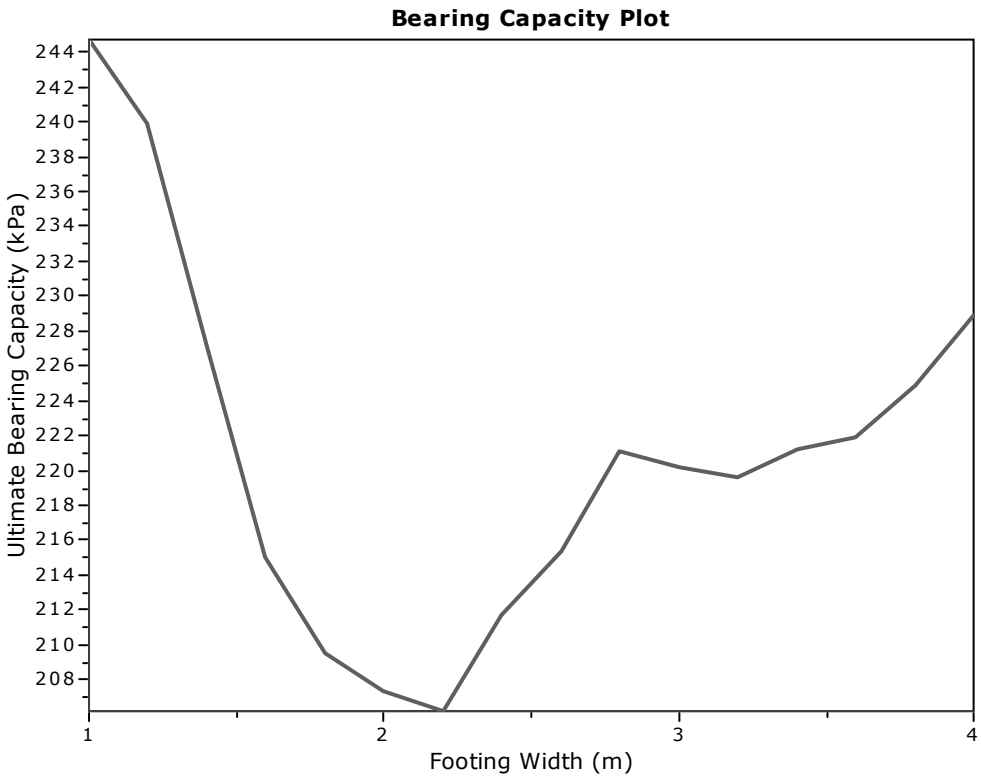
Project:
Location:



Bearing Capacity calculation is perfromed based on the formula:

$$Q_{ult} = R_k \times q_t + q_{soil}$$

where:
R_k: Bearing capacity factor
q_t: Average corrected cone resistance over calculation depth
q_{soil}: Pressure applied by soil above footing



:: Tabular results ::

No	B (m)	Start Depth (m)	End Depth (m)	Ave. q_t (MPa)	R_k	Soil Press. (kPa)	Ult. bearing cap. (kPa)
1	1.00	0.50	2.00	1.18	0.20	9.50	244.71
2	1.20	0.50	2.30	1.15	0.20	9.50	239.91
3	1.40	0.50	2.60	1.09	0.20	9.50	227.10
4	1.60	0.50	2.90	1.03	0.20	9.50	215.06
5	1.80	0.50	3.20	1.00	0.20	9.50	209.51
6	2.00	0.50	3.50	0.99	0.20	9.50	207.34
7	2.20	0.50	3.80	0.98	0.20	9.50	206.19
8	2.40	0.50	4.10	1.01	0.20	9.50	211.65
9	2.60	0.50	4.40	1.03	0.20	9.50	215.40
10	2.80	0.50	4.70	1.06	0.20	9.50	221.06
11	3.00	0.50	5.00	1.05	0.20	9.50	220.21
12	3.20	0.50	5.30	1.05	0.20	9.50	219.59
13	3.40	0.50	5.60	1.06	0.20	9.50	221.17
14	3.60	0.50	5.90	1.06	0.20	9.50	221.84
15	3.80	0.50	6.20	1.08	0.20	9.50	224.89
16	4.00	0.50	6.50	1.10	0.20	9.50	228.94

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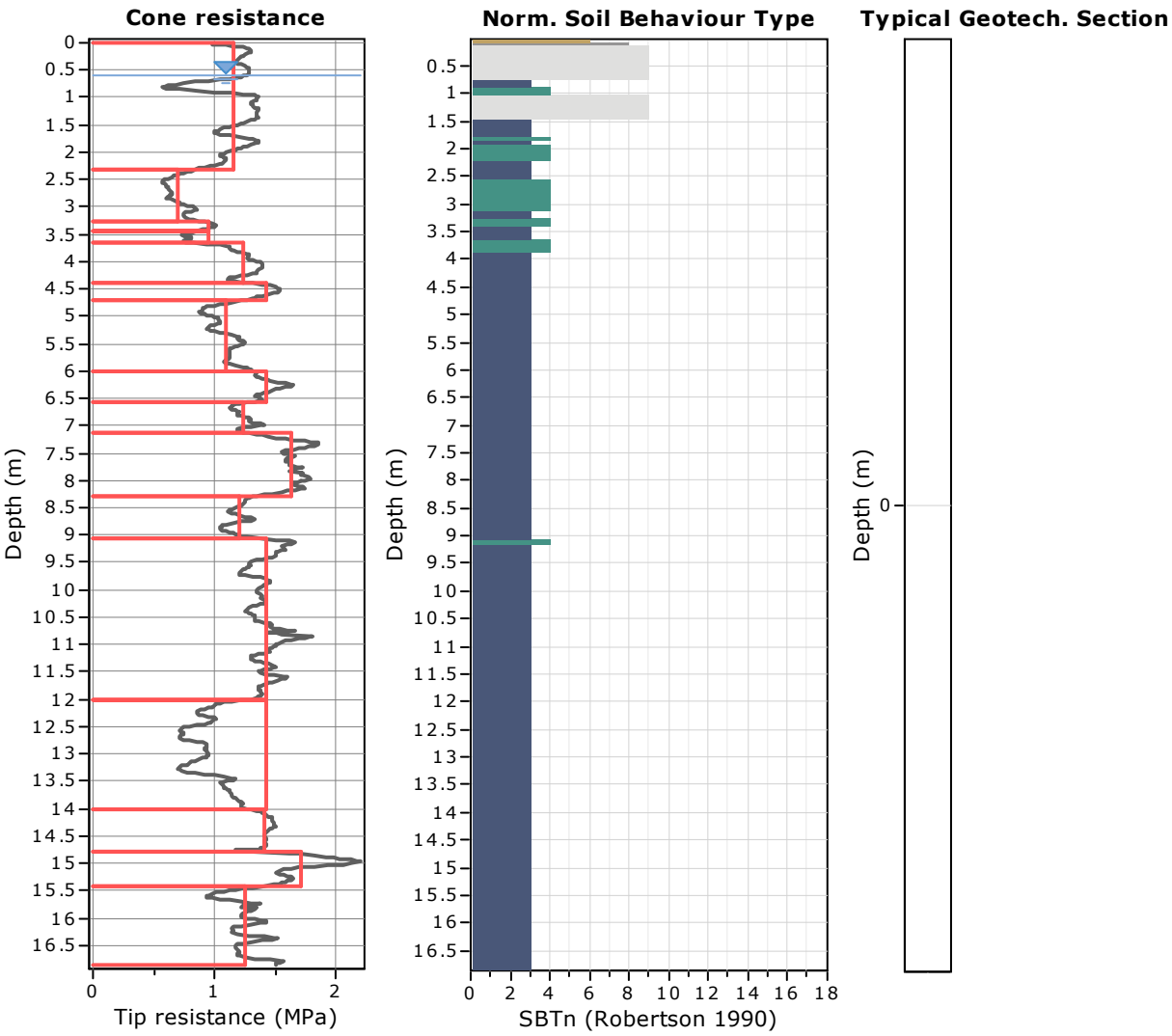
Total depth: 16.86 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Tabular results

.:: Layer No: 1 ::.

Code: A **Start depth:** 0.00 (m), **End depth:** 2.32 (m)

Description: Very dense/stiff soil

Basic results	Estimation results	
Total cone resistance: 1.16 ±0.19 MPa	Permeability: 1.22E-06 ±8.40E-06 m/s	Constrained Mod.: 15.83 ±2.82 MPa
Sleeve friction: 81.18 ±26.05 kPa	N60: 4.83 ±0.86 blows	Go: 29.33 ±5.69 MPa
SBT_n: 9	Es: 21.50 ±2.42 MPa	Su: 81.58 ±13.62 kPa
SBTn description: Very dense/stiff soil	Dr (%): 0.00 ±0.00	Su ratio: 5.02 ±2.77
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 23.21 ±12.78
	Unit weight: 18.02 ±0.52 kN/m³	

.:: Layer No: 2 ::.

Code: E **Start depth:** 2.32 (m), **End depth:** 3.26 (m)

Description: Clay & silty clay

Basic results	**Estimation results**	
Total cone resistance: 0.70 ±0.09 MPa	Permeability: 3.96E-08 ±2.22E-08 m/s	Constrained Mod.: 9.12 ±1.22 MPa
Sleeve friction: 23.84 ±11.76 kPa	N60: 3.19 ±0.39 blows	Go: 19.70 ±3.24 MPa
SBT_n: 4	Es: 0.00 ±0.00 MPa	Su: 46.53 ±6.20 kPa
SBTn description: Clay & silty clay	Dr (%): 0.00 ±0.00	Su ratio: 1.51 ±0.21
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 6.95 ±0.98
	Unit weight: 16.38 ±0.55 kN/m³	

.:: Layer No: 3 ::.

Code: A1 **Start depth:** 3.26 (m), **End depth:** 3.44 (m)

Description: Clay & silty clay

Basic results	**Estimation results**	
Total cone resistance: 0.95 ±0.06 MPa	Permeability: 4.59E-08 ±1.88E-08 m/s	Constrained Mod.: 12.42 ±0.80 MPa
Sleeve friction: 33.64 ±6.00 kPa	N60: 4.00 ±0.00 blows	Go: 25.63 ±1.34 MPa
SBT_n: 4	Es: 0.00 ±0.00 MPa	Su: 63.35 ±4.09 kPa
SBTn description: Clay & silty clay	Dr (%): 0.00 ±0.00	Su ratio: 1.80 ±0.08
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 8.31 ±0.37
	Unit weight: 17.00 ±0.19 kN/m³	

.:: Layer No: 4 ::.

Code: E2 **Start depth:** 3.44 (m), **End depth:** 3.66 (m)

Description: Clay & silty clay

Basic results	**Estimation results**	
Total cone resistance: 0.95 ±0.06 MPa	Permeability: 4.59E-08 ±1.88E-08 m/s	Constrained Mod.: 12.42 ±0.80 MPa
Sleeve friction: 33.64 ±6.00 kPa	N60: 4.00 ±0.00 blows	Go: 25.63 ±1.34 MPa
SBT_n: 4	Es: 0.00 ±0.00 MPa	Su: 63.35 ±4.09 kPa
SBTn description: Clay & silty clay	Dr (%): 0.00 ±0.00	Su ratio: 1.80 ±0.08
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 8.31 ±0.37
	Unit weight: 17.00 ±0.19 kN/m³	

.:: Layer No: 5 ::.

Code: A3 **Start depth:** 3.66 (m), **End depth:** 4.40 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.24 ±0.13 MPa	Permeability: 3.81E-08 ±2.99E-08 m/s	Constrained Mod.: 16.33 ±1.83 MPa
Sleeve friction: 66.99 ±24.83 kPa	N60: 5.58 ±0.72 blows	Go: 36.45 ±6.48 MPa
SBT_n: 3	Es: 19.75 ±19.75 MPa	Su: 83.31 ±9.34 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 2.11 ±0.23
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 9.76 ±1.05
	Unit weight: 17.80 ±0.58 kN/m³	

.:: Layer No: 6 ::.

Code: D **Start depth:** 4.40 (m), **End depth:** 4.70 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.43 ±0.09 MPa	Permeability: 1.98E-08 ±7.93E-09 m/s	Constrained Mod.: 18.96 ±1.33 MPa
Sleeve friction: 96.93 ±10.73 kPa	N60: 6.81 ±0.40 blows	Go: 45.49 ±1.86 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 96.74 ±6.81 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 2.27 ±0.14
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 10.48 ±0.65
	Unit weight: 18.38 ±0.12 kN/m³	

.:: Layer No: 7 ::.

Code: A4 **Start depth:** 4.70 (m), **End depth:** 6.00 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.09 ±0.12 MPa	Permeability: 1.03E-08 ±5.31E-09 m/s	Constrained Mod.: 13.96 ±1.58 MPa
Sleeve friction: 65.26 ±13.49 kPa	N60: 5.55 ±0.50 blows	Go: 38.02 ±2.51 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 71.20 ±8.08 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.48 ±0.14
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 6.85 ±0.64
	Unit weight: 17.81 ±0.21 kN/m³	

.:: Layer No: 8 ::.

Code: D2 **Start depth:** 6.00 (m), **End depth:** 6.56 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.43 ±0.10 MPa	Permeability: 1.18E-08 ±3.86E-09 m/s	Constrained Mod.: 18.49 ±1.46 MPa
Sleeve friction: 89.01 ±11.18 kPa	N60: 7.10 ±0.56 blows	Go: 48.47 ±3.08 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 94.34 ±7.43 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.70 ±0.13
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 7.84 ±0.60
	Unit weight: 18.28 ±0.17 kN/m³	

.:: Layer No: 9 ::.

Code: A5 **Start depth:** 6.56 (m), **End depth:** 7.14 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.24 ±0.08 MPa	Permeability: 5.80E-09 ±1.31E-09 m/s	Constrained Mod.: 15.68 ±1.04 MPa
Sleeve friction: 80.78 ±5.43 kPa	N60: 6.47 ±0.51 blows	Go: 46.46 ±1.93 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 80.00 ±5.33 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.33 ±0.08
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 6.16 ±0.38
	Unit weight: 18.12 ±0.09 kN/m³	

.:: Layer No: 10 ::.

Code: B **Start depth:** 7.14 (m), **End depth:** 8.28 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.64 ±0.12 MPa	Permeability: 1.13E-08 ±5.80E-09 m/s	Constrained Mod.: 21.06 ±1.73 MPa
Sleeve friction: 99.32 ±15.37 kPa	N60: 8.16 ±0.62 blows	Go: 56.14 ±4.15 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 107.45 ±8.81 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.59 ±0.14
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 7.36 ±0.64
	Unit weight: 18.45 ±0.20 kN/m³	

.:: Layer No: 11 ::.

Code: A6 **Start depth:** 8.28 (m), **End depth:** 9.06 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.20 ±0.09 MPa	Permeability: 6.84E-09 ±3.90E-09 m/s	Constrained Mod.: 13.99 ±2.03 MPa
Sleeve friction: 54.11 ±15.03 kPa	N60: 6.20 ±0.41 blows	Go: 43.14 ±3.86 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 74.56 ±6.69 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.99 ±0.10
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 4.58 ±0.46
	Unit weight: 17.61 ±0.29 kN/m³	

.:: Layer No: 12 ::.

Code: D3 **Start depth:** 9.06 (m), **End depth:** 12.00 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.42 ±0.12 MPa	Permeability: 4.54E-09 ±4.87E-09 m/s	Constrained Mod.: 16.30 ±2.47 MPa
Sleeve friction: 80.50 ±16.29 kPa	N60: 7.82 ±0.58 blows	Go: 55.88 ±4.94 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 88.25 ±8.50 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.98 ±0.13
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 4.53 ±0.61
	Unit weight: 18.15 ±0.23 kN/m³	

.:: Layer No: 13 ::.

Code: A7 **Start depth:** 12.00 (m), **End depth:** 14.00 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.42 ±0.12 MPa	Permeability: 4.54E-09 ±4.87E-09 m/s	Constrained Mod.: 16.30 ±2.47 MPa
Sleeve friction: 80.50 ±16.29 kPa	N60: 7.82 ±0.58 blows	Go: 55.88 ±4.94 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 88.25 ±8.50 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.98 ±0.13
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 4.53 ±0.61
	Unit weight: 18.15 ±0.23 kN/m³	

.:: Layer No: 14 ::.

Code: D4 **Start depth:** 14.00 (m), **End depth:** 14.78 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.42 ±0.07 MPa	Permeability: 1.98E-09 ±5.52E-10 m/s	Constrained Mod.: 11.21 ±1.37 MPa
Sleeve friction: 67.32 ±11.73 kPa	N60: 8.10 ±0.55 blows	Go: 58.64 ±3.50 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 82.81 ±5.12 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.69 ±0.05
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 3.18 ±0.21
	Unit weight: 17.96 ±0.18 kN/m³	

.:: Layer No: 15 ::.

Code: B2 **Start depth:** 14.78 (m), **End depth:** 15.42 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.71 ±0.25 MPa	Permeability: 3.94E-09 ±3.74E-09 m/s	Constrained Mod.: 16.63 ±5.69 MPa
Sleeve friction: 86.81 ±23.91 kPa	N60: 9.64 ±0.90 blows	Go: 68.18 ±6.35 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 102.72 ±18.20 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.81 ±0.15
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 3.76 ±0.69
	Unit weight: 18.30 ±0.29 kN/m³	

.:: Layer No: 16 ::.

Code: A8 **Start depth:** 15.42 (m), **End depth:** 16.86 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.25 ±0.15 MPa	Permeability: 2.38E-09 ±1.94E-09 m/s	Constrained Mod.: 7.02 ±2.03 MPa
Sleeve friction: 41.79 ±13.24 kPa	N60: 7.31 ±0.57 blows	Go: 49.80 ±4.37 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 68.71 ±10.30 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.51 ±0.07
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.36 ±0.34
	Unit weight: 17.31 ±0.33 kN/m³	

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Project:
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CPT: CPTu-02
Total depth: 16.86 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Summary table of mean values

From depth To depth (m)	Thickness (m)	Permeability (m/s)	SPT_{N60} (blows/30cm)	E_s (MPa)	D_r	Friction angle	Constrained modulus, M (MPa)	Shear modulus, G_O (MPa)	Undrained strength, S_U (kPa)	Undrained strength ratio	OCR	Unit weight (kN/m³)
0.00	2.32	1.22E-06	4.8	21.5	0.0	0.0	15.8	29.3	81.6	5.0	23.2	18.0
2.32		(±8.40E-06)	(±0.9)	(±2.4)	(±0.0)	(±0.0)	(±2.8)	(±5.7)	(±13.6)	(±2.8)	(±12.8)	(±0.5)
2.32	0.94	3.96E-08	3.2	0.0	0.0	0.0	9.1	19.7	46.5	1.5	7.0	16.4
3.26		(±2.22E-08)	(±0.4)	(±0.0)	(±0.0)	(±0.0)	(±1.2)	(±3.2)	(±6.2)	(±0.2)	(±1.0)	(±0.5)
3.26	0.18	4.59E-08	4.0	0.0	0.0	0.0	12.4	25.6	63.3	1.8	8.3	17.0
3.44		(±1.88E-08)	(±0.0)	(±0.0)	(±0.0)	(±0.0)	(±0.8)	(±1.3)	(±4.1)	(±0.1)	(±0.4)	(±0.2)
3.44	0.22	4.59E-08	4.0	0.0	0.0	0.0	12.4	25.6	63.3	1.8	8.3	17.0
3.66		(±1.88E-08)	(±0.0)	(±0.0)	(±0.0)	(±0.0)	(±0.8)	(±1.3)	(±4.1)	(±0.1)	(±0.4)	(±0.2)
3.66	0.74	3.81E-08	5.6	19.7	0.0	0.0	16.3	36.4	83.3	2.1	9.8	17.8
4.40		(±2.99E-08)	(±0.7)	(±19.7)	(±0.0)	(±0.0)	(±1.8)	(±6.5)	(±9.3)	(±0.2)	(±1.1)	(±0.6)
4.40	0.30	1.98E-08	6.8	0.0	0.0	0.0	19.0	45.5	96.7	2.3	10.5	18.4
4.70		(±7.93E-09)	(±0.4)	(±0.0)	(±0.0)	(±0.0)	(±1.3)	(±1.9)	(±6.8)	(±0.1)	(±0.6)	(±0.1)
4.70	1.30	1.03E-08	5.5	0.0	0.0	0.0	14.0	38.0	71.2	1.5	6.9	17.8
6.00		(±5.31E-09)	(±0.5)	(±0.0)	(±0.0)	(±0.0)	(±1.6)	(±2.5)	(±8.1)	(±0.1)	(±0.6)	(±0.2)
6.00	0.56	1.18E-08	7.1	0.0	0.0	0.0	18.5	48.5	94.3	1.7	7.8	18.3
6.56		(±3.86E-09)	(±0.6)	(±0.0)	(±0.0)	(±0.0)	(±1.5)	(±3.1)	(±7.4)	(±0.1)	(±0.6)	(±0.2)
6.56	0.58	5.80E-09	6.5	0.0	0.0	0.0	15.7	46.5	80.0	1.3	6.2	18.1
7.14		(±1.31E-09)	(±0.5)	(±0.0)	(±0.0)	(±0.0)	(±1.0)	(±1.9)	(±5.3)	(±0.1)	(±0.4)	(±0.1)
7.14	1.14	1.13E-08	8.2	0.0	0.0	0.0	21.1	56.1	107.5	1.6	7.4	18.5
8.28		(±5.80E-09)	(±0.6)	(±0.0)	(±0.0)	(±0.0)	(±1.7)	(±4.2)	(±8.8)	(±0.1)	(±0.6)	(±0.2)
8.28	0.78	6.84E-09	6.2	0.0	0.0	0.0	14.0	43.1	74.6	1.0	4.6	17.6
9.06		(±3.90E-09)	(±0.4)	(±0.0)	(±0.0)	(±0.0)	(±2.0)	(±3.9)	(±6.7)	(±0.1)	(±0.5)	(±0.3)

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Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Summary table of mean values

From depth To depth (m)	Thickness (m)	Permeability (m/s)	SPT_{N60} (blows/30cm)	E_s (MPa)	D_r	Friction angle	Constrained modulus, M (MPa)	Shear modulus, G_O (MPa)	Undrained strength, S_U (kPa)	Undrained strength ratio	OCR	Unit weight (kN/m³)
9.06	2.94	4.54E-09	7.8	0.0	0.0	0.0	16.3	55.9	88.3	1.0	4.5	18.1
12.00		(±4.87E-09)	(±0.6)	(±0.0)	(±0.0)	(±0.0)	(±2.5)	(±4.9)	(±8.5)	(±0.1)	(±0.6)	(±0.2)
12.00	2.00	4.54E-09	7.8	0.0	0.0	0.0	16.3	55.9	88.3	1.0	4.5	18.1
14.00		(±4.87E-09)	(±0.6)	(±0.0)	(±0.0)	(±0.0)	(±2.5)	(±4.9)	(±8.5)	(±0.1)	(±0.6)	(±0.2)
14.00	0.78	1.98E-09	8.1	0.0	0.0	0.0	11.2	58.6	82.8	0.7	3.2	18.0
14.78		(±5.52E-10)	(±0.5)	(±0.0)	(±0.0)	(±0.0)	(±1.4)	(±3.5)	(±5.1)	(±0.0)	(±0.2)	(±0.2)
14.78	0.64	3.94E-09	9.6	0.0	0.0	0.0	16.6	68.2	102.7	0.8	3.8	18.3
15.42		(±3.74E-09)	(±0.9)	(±0.0)	(±0.0)	(±0.0)	(±5.7)	(±6.4)	(±18.2)	(±0.1)	(±0.7)	(±0.3)
15.42	1.44	2.38E-09	7.3	0.0	0.0	0.0	7.0	49.8	68.7	0.5	2.4	17.3
16.86		(±1.94E-09)	(±0.6)	(±0.0)	(±0.0)	(±0.0)	(±2.0)	(±4.4)	(±10.3)	(±0.1)	(±0.3)	(±0.3)

Depth values presented in this table are measured from free ground surface

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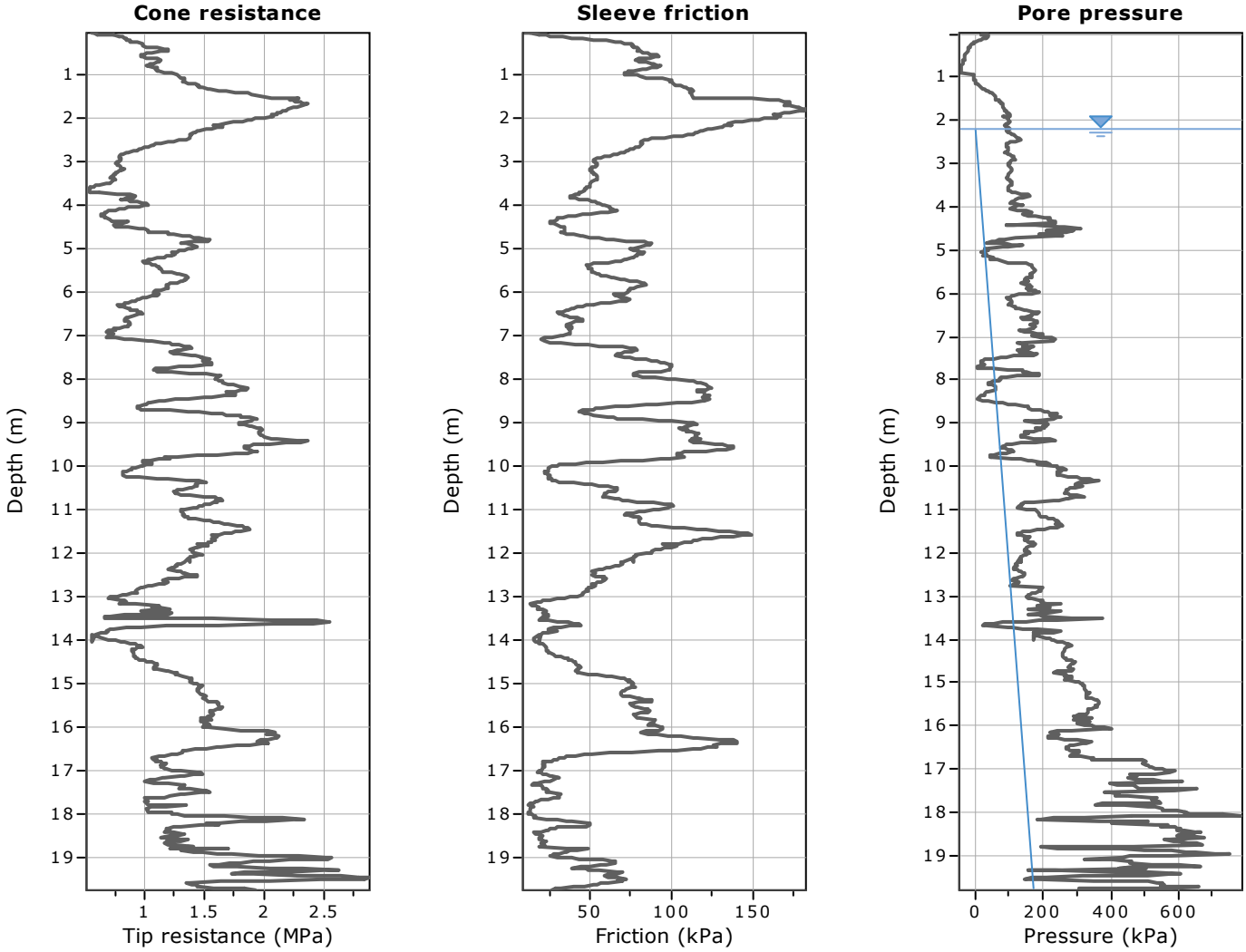
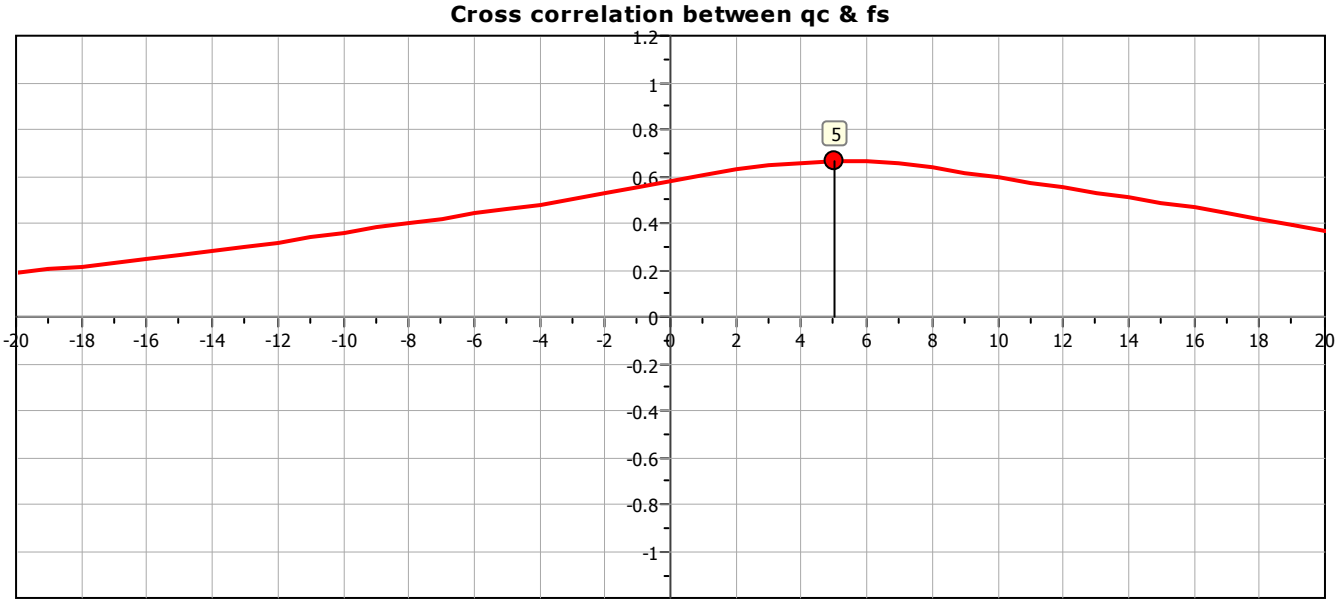
CPT: CPTu-03
Total depth: 19.76 m, Date: 11/02/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:



The plot below presents the cross correlation coeficient between the raw qc and fs values (as measured on the field). X axes presents the lag distance (one lag is the distance between two sucessive CPT measurements).



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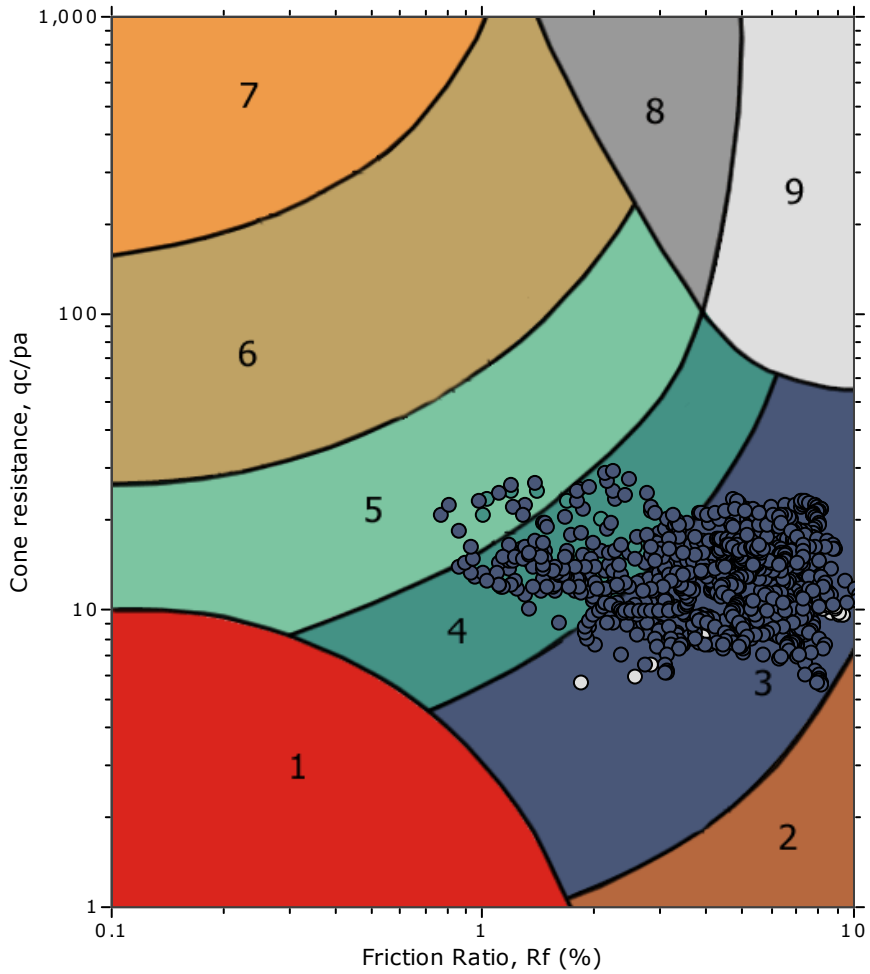
Project:
Location:

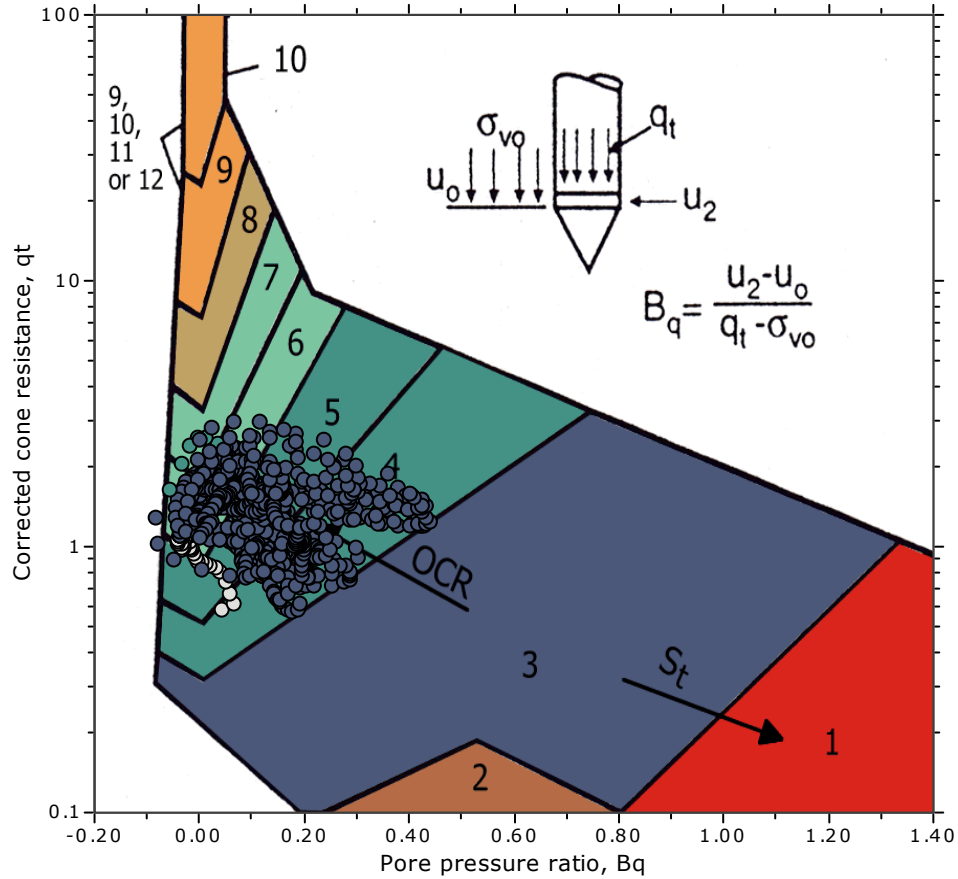
CPT: CPTu-03
Total depth: 19.76 m, Date: 11/02/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

SBT - Bq plots

SBT plot



Bq plot



SBT legend

- 1. Sensitive fine grained
- 2. Organic material
- 3. Clay to silty clay
- 4. Clayey silt to silty clay
- 5. Silty sand to sandy silt
- 6. Clean sand to silty sand
- 7. Gravely sand to sand
- 8. Very stiff sand to clayey sand
- 9. Very stiff fine grained

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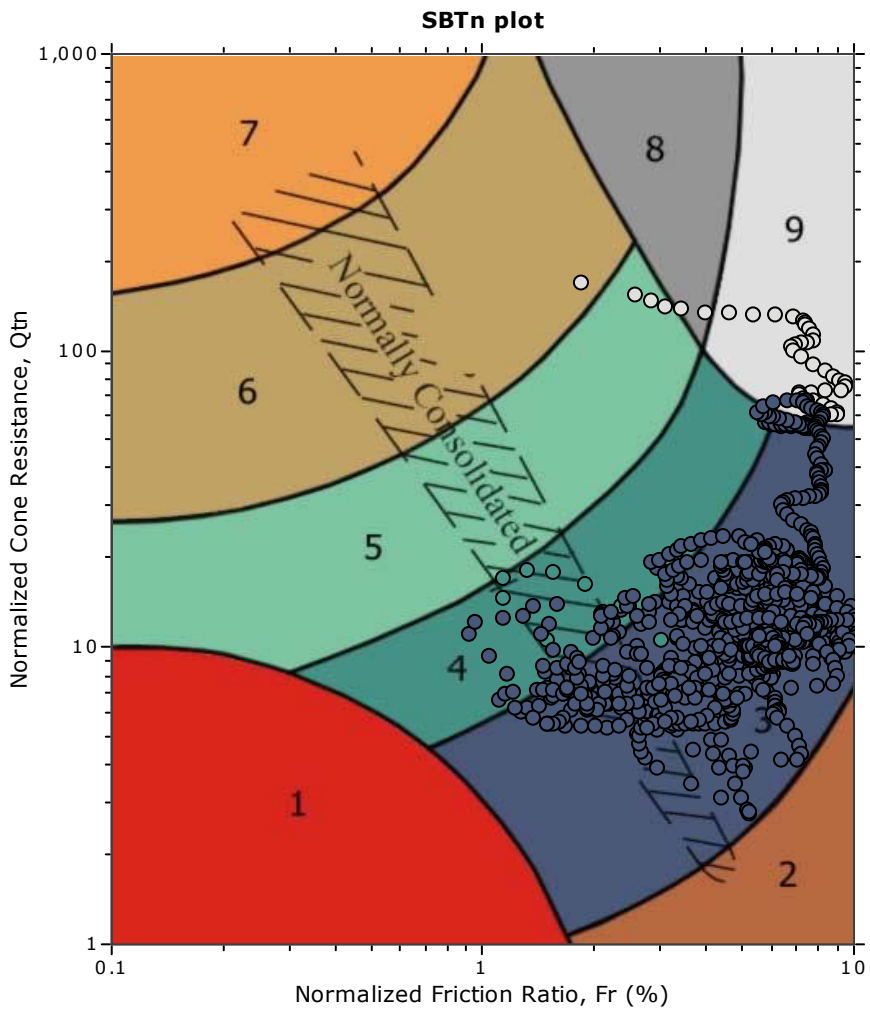
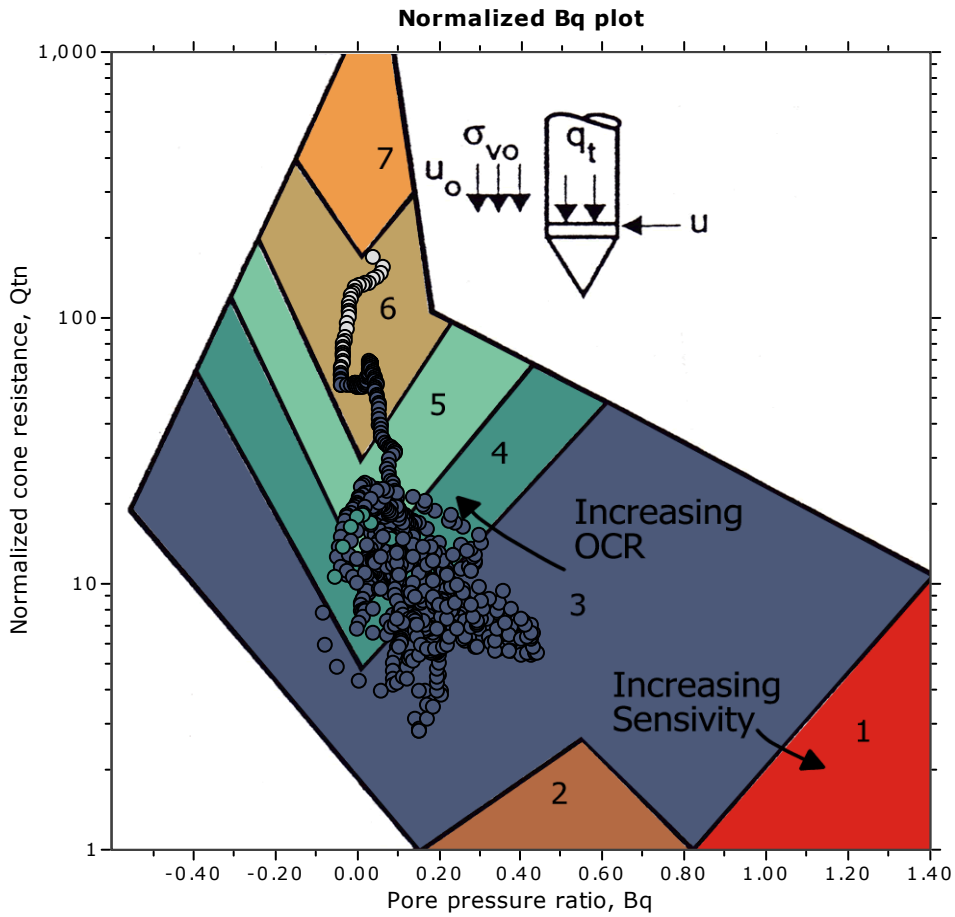
Project:
Location:

CPT: CPTu-03
Total depth: 19.76 m, Date: 11/02/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

SBT - Bq plots (normalized)





SBTn legend

- 1. Sensitive fine grained
- 2. Organic material
- 3. Clay to silty clay
- 4. Clayey silt to silty clay
- 5. Silty sand to sandy silt
- 6. Clean sand to silty sand
- 7. Gravely sand to sand
- 8. Very stiff sand to clayey sand
- 9. Very stiff fine grained

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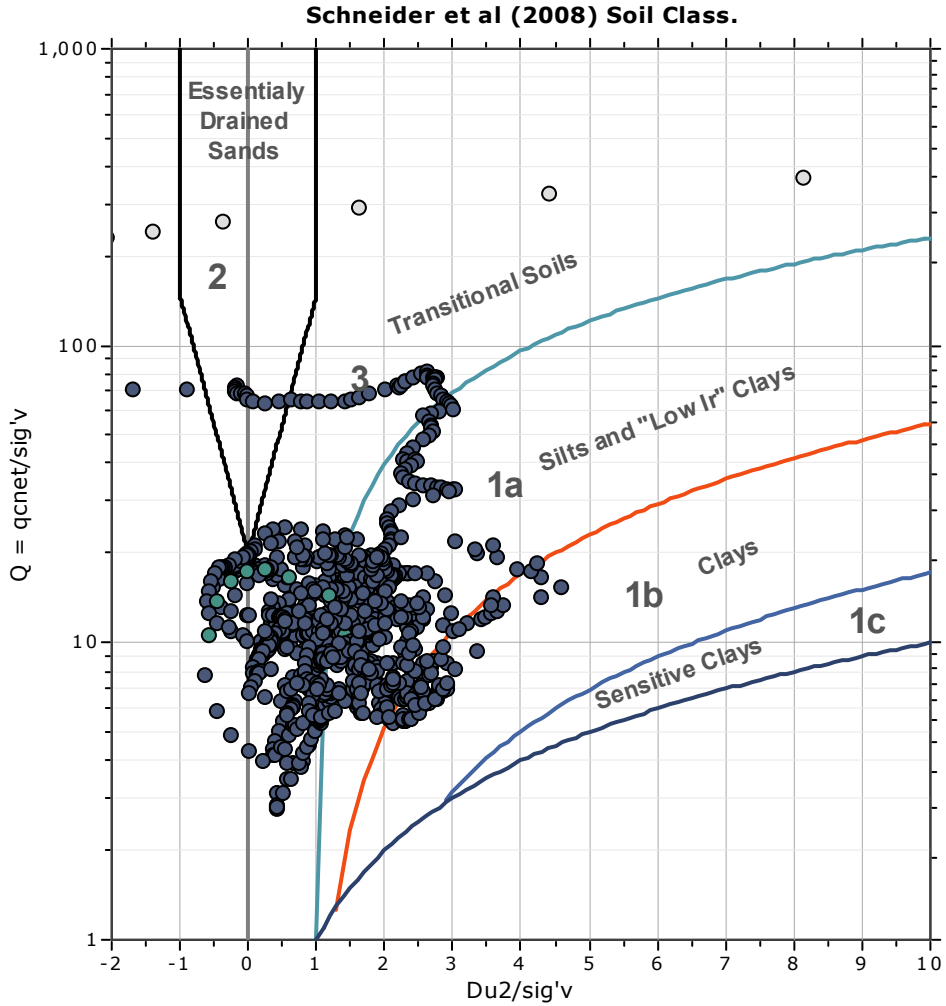
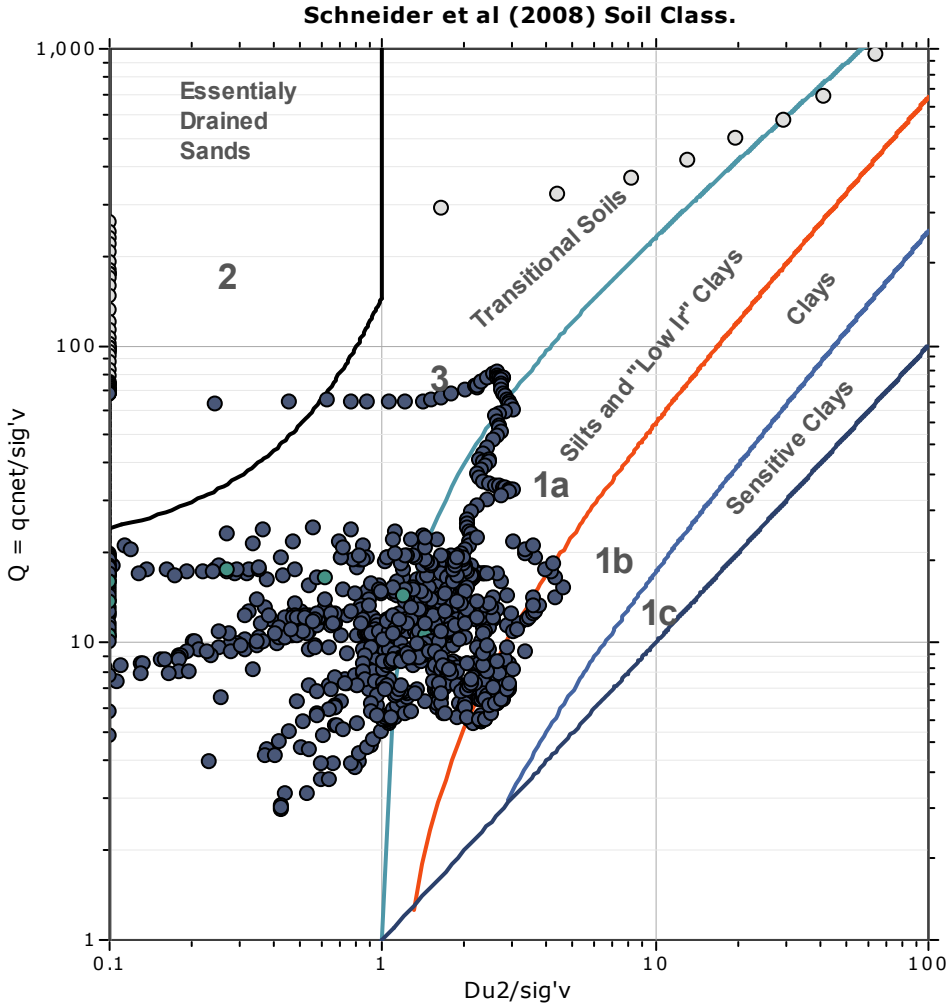
Project:
Location:

CPT: CPTu-03
Total depth: 19.76 m, Date: 11/02/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Bq plots (Schneider)





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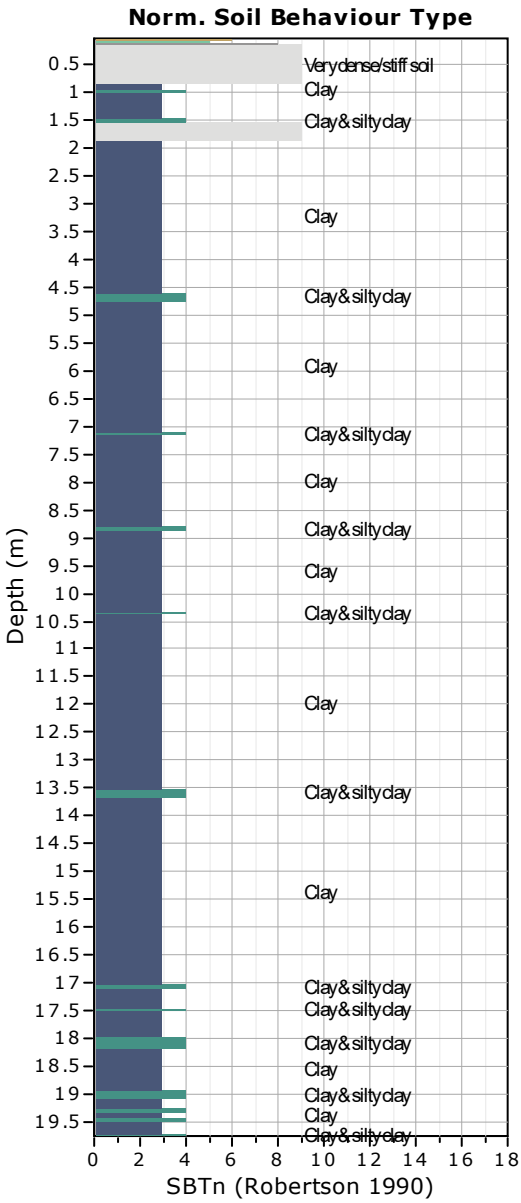
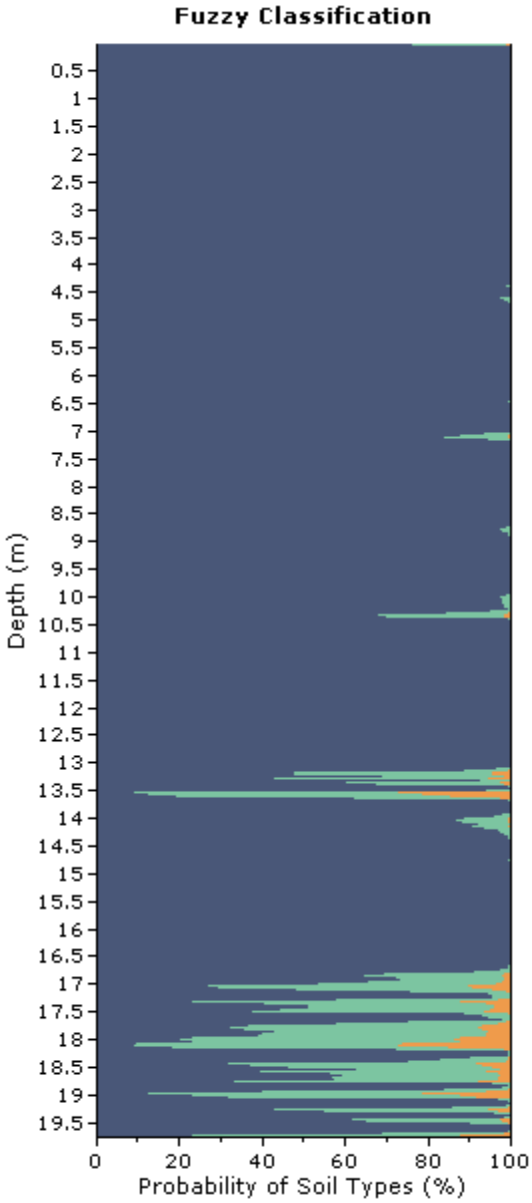
CPT: CPTu-03
Total depth: 19.76 m, Date: 11/02/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:





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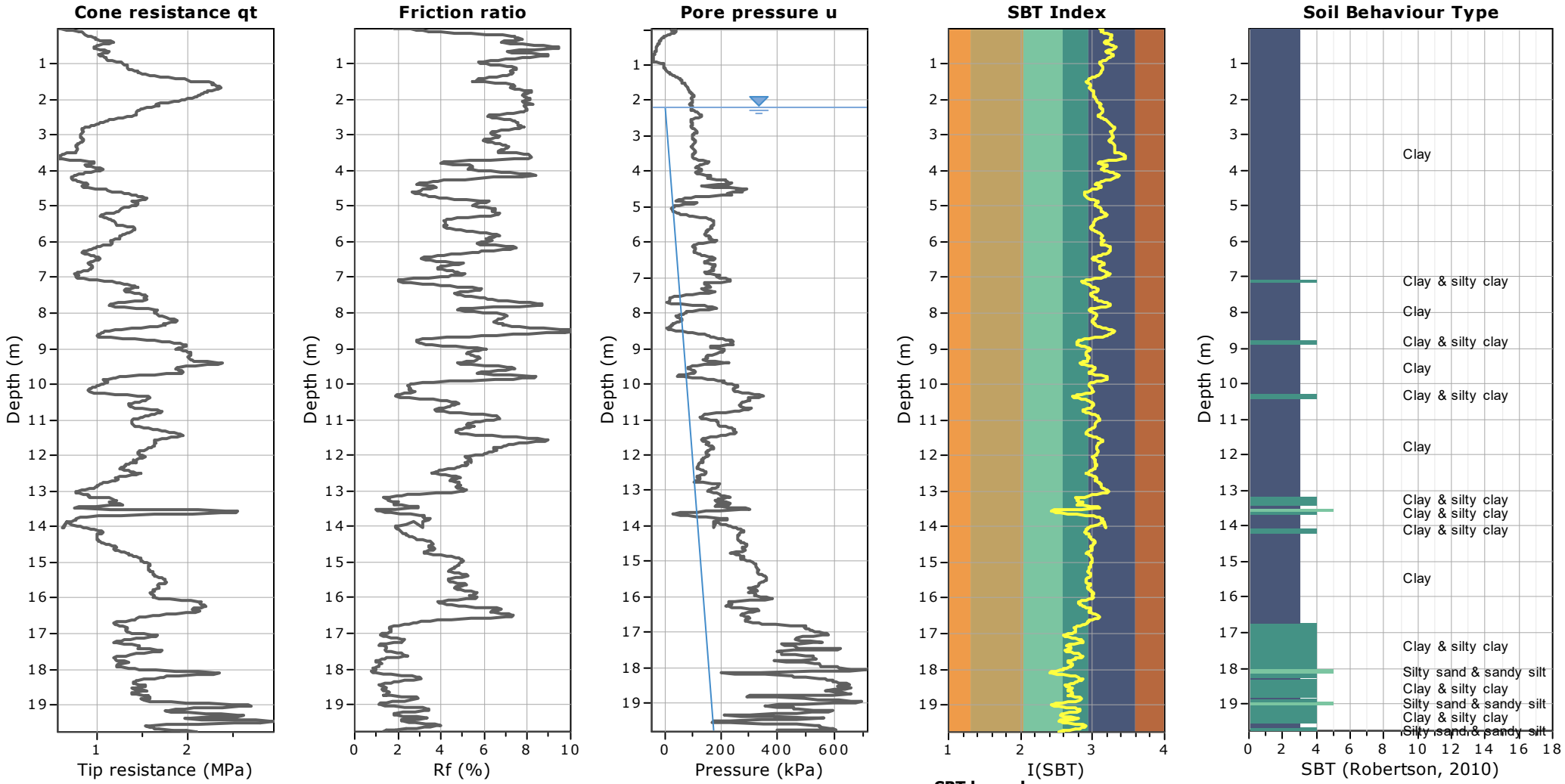
Project:
Location:

CPT: CPTu-03
Total depth: 19.76 m, Date: 11/02/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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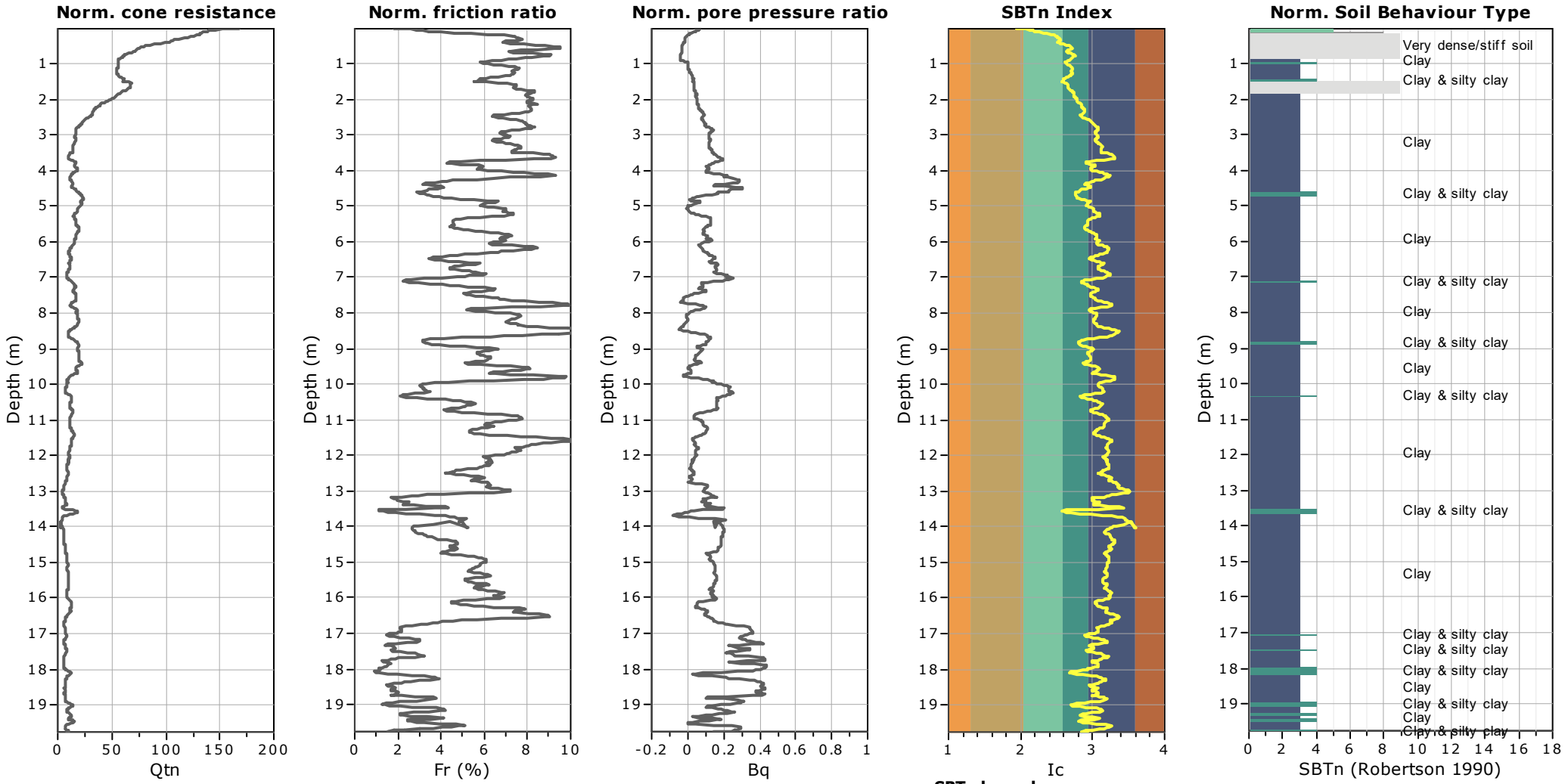
Project:
Location:

CPT: CPTu-03
Total depth: 19.76 m, Date: 11/02/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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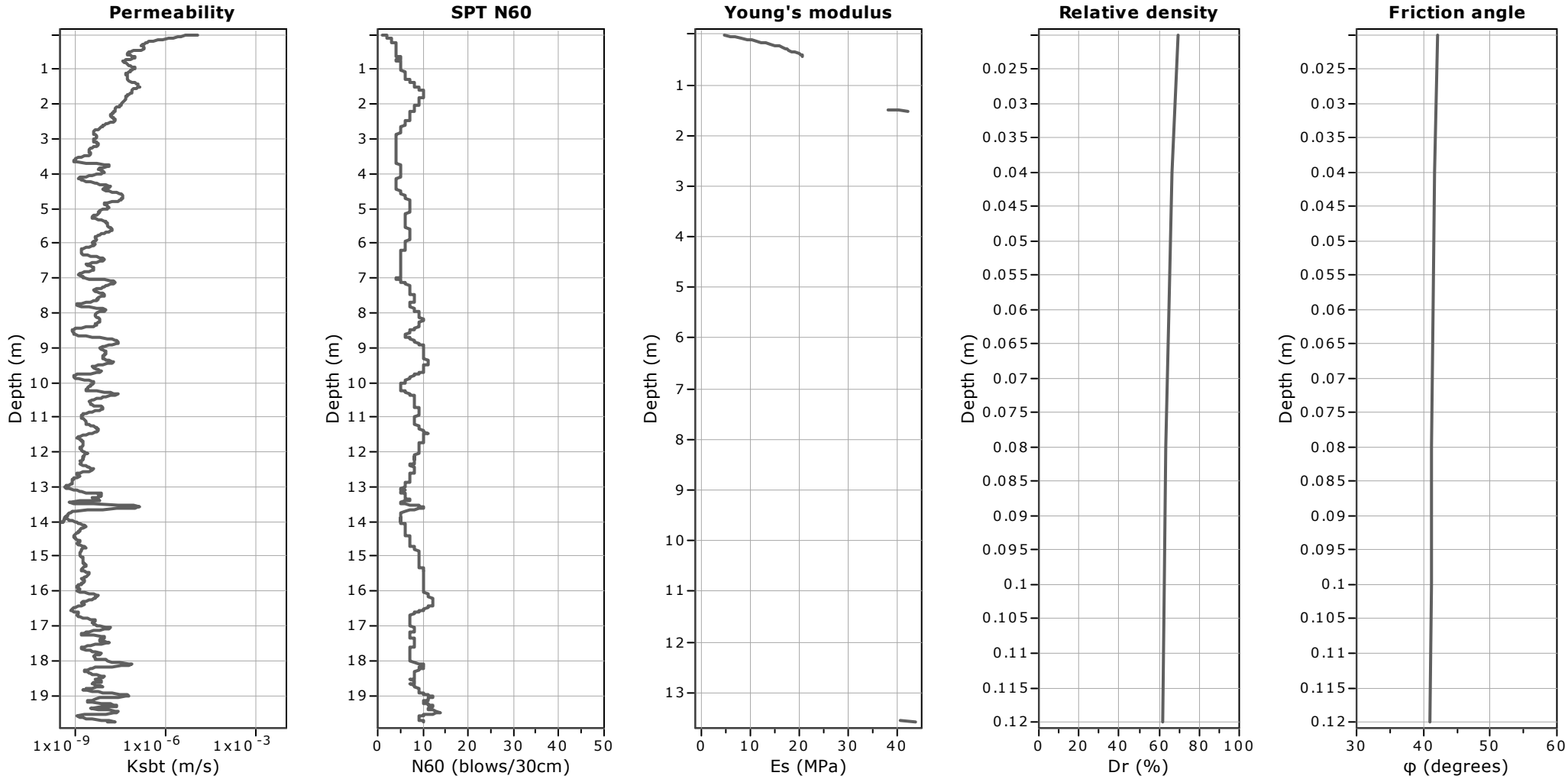
Project:
Location:

CPT: CPTu-03
Total depth: 19.76 m, Date: 11/02/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Permeability: Based on SBT_n
SPT N_{60}: Based on I_c and q_t
Young's modulus: Based on variable alpha using I_c (Robertson, 2009)
Relative desnisty constant, C_{Dr}: 350.0
Phi: Based on Kulhawy & Mayne (1990)
User defined estimation data

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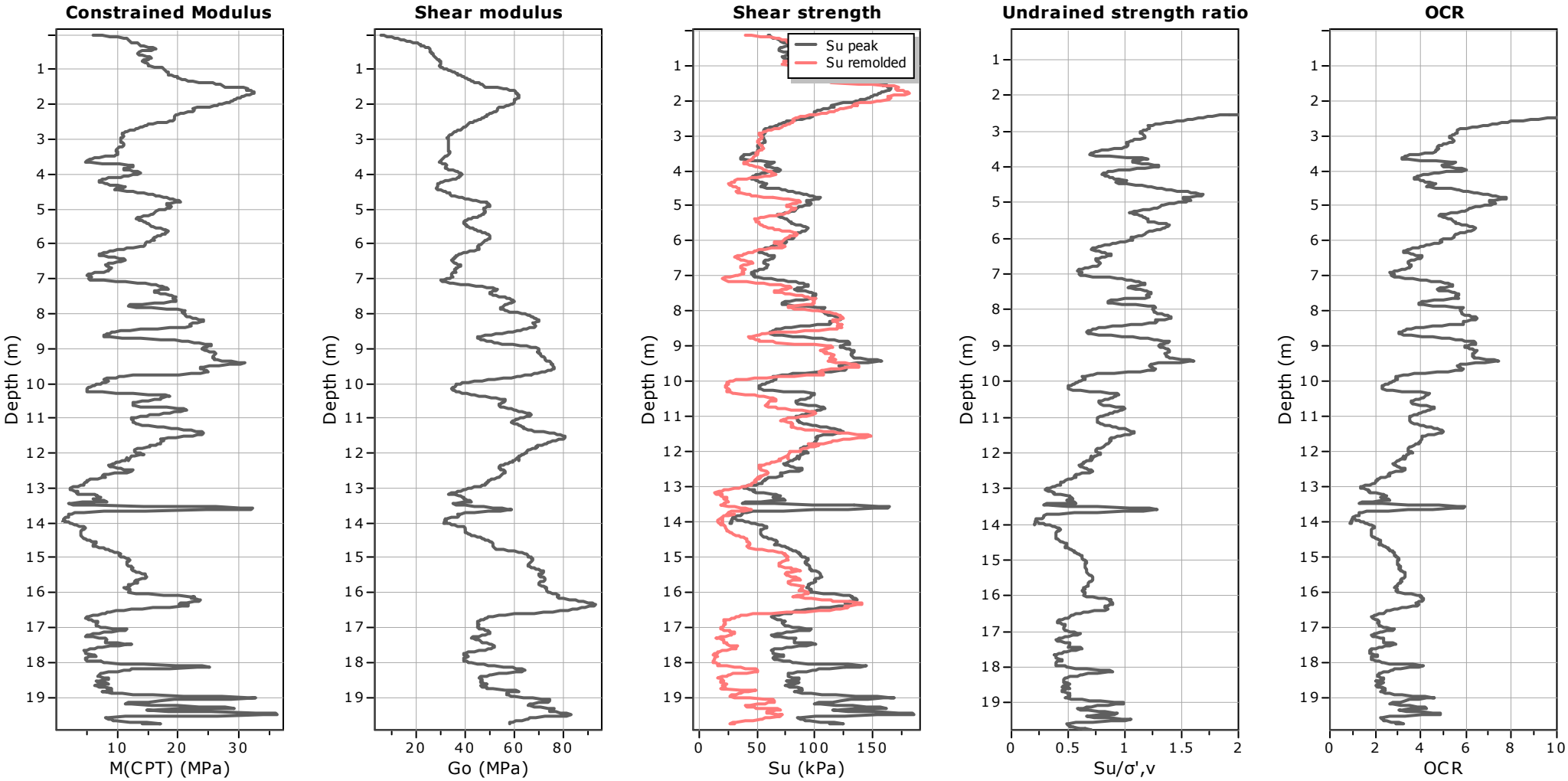
Project:
Location:

CPT: CPTu-03
Total depth: 19.76 m, Date: 11/02/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Constrained modulus: Based on variable *alpha* using I_c and Q_{tn} (Robertson, 2009)
Go: Based on variable *alpha* using I_c (Robertson, 2009)
Undrained shear strength cone factor for clays, N_{kt}: 14

OCR factor for clays, N_{kt}: 0.33
User defined estimation data

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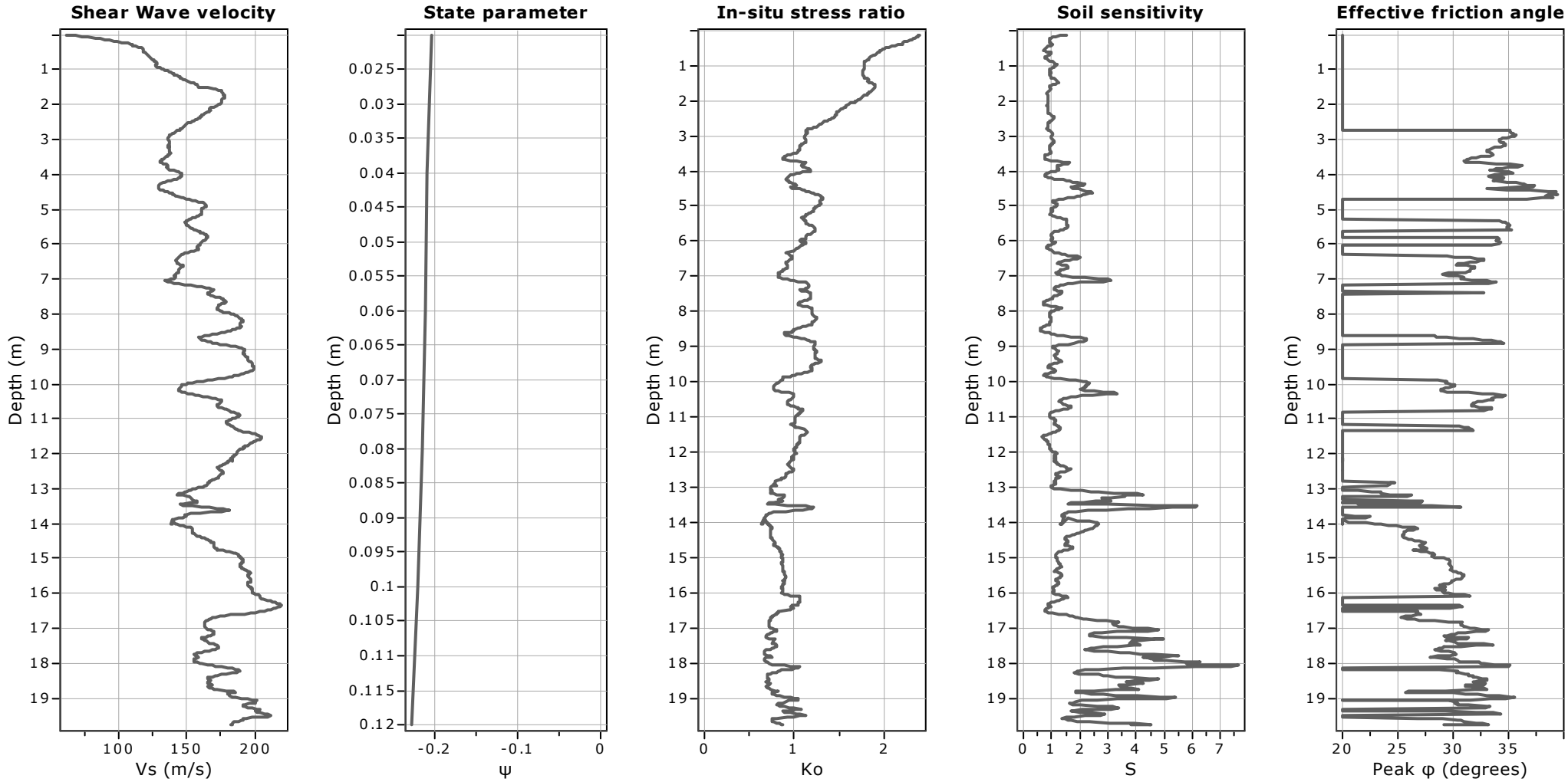
Project:
Location:

CPT: CPTu-03
Total depth: 19.76 m, Date: 11/02/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Soil Sensitivity factor, N_S: 7.00

User defined estimation data

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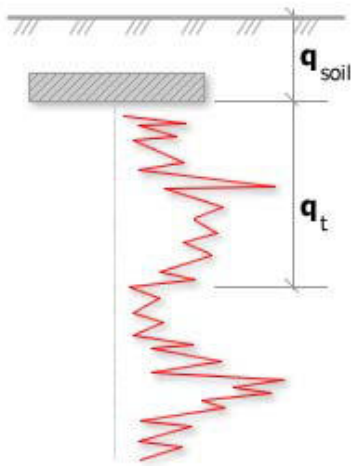
CPT: CPTu-03
Total depth: 19.76 m, Date: 11/02/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

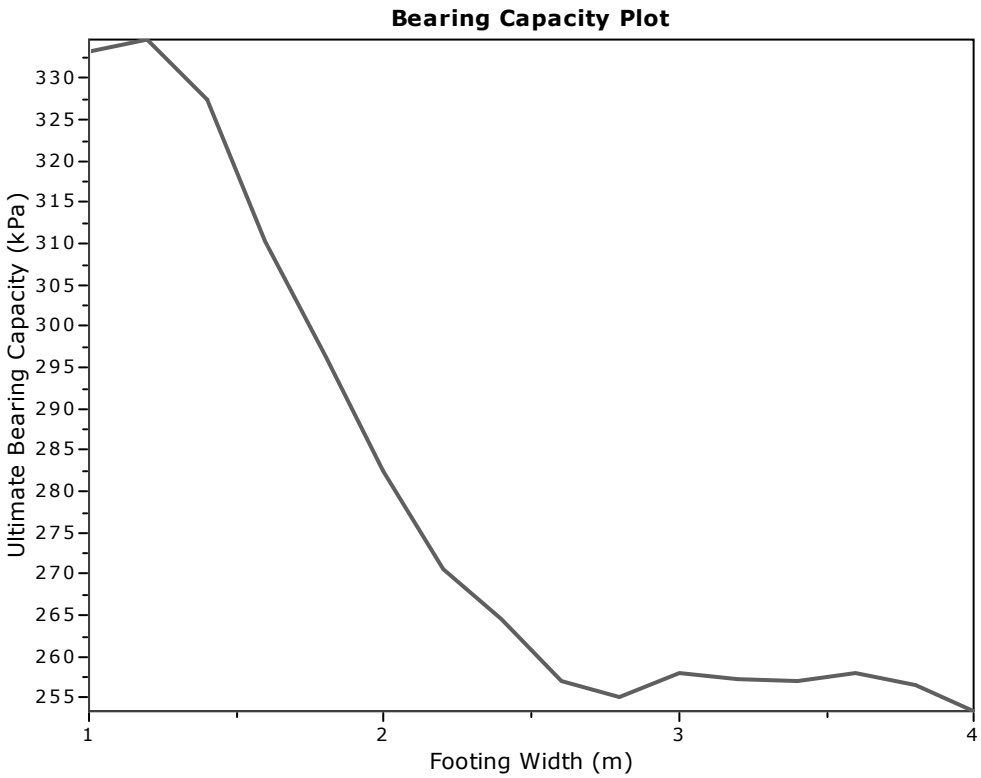
Project:
Location:



Bearing Capacity calculation is perfromed based on the formula:

$$Q_{ult} = R_k \times q_t + q_{soil}$$

where:
R_k: Bearing capacity factor
q_t: Average corrected cone resistance over calculation depth
q_{soil}: Pressure applied by soil above footing



:: Tabular results ::

No	B (m)	Start Depth (m)	End Depth (m)	Ave. q_t (MPa)	R_k	Soil Press. (kPa)	Ult. bearing cap. (kPa)
1	1.00	0.50	2.00	1.62	0.20	9.50	333.12
2	1.20	0.50	2.30	1.63	0.20	9.50	334.63
3	1.40	0.50	2.60	1.59	0.20	9.50	327.46
4	1.60	0.50	2.90	1.50	0.20	9.50	310.29
5	1.80	0.50	3.20	1.43	0.20	9.50	296.35
6	2.00	0.50	3.50	1.36	0.20	9.50	282.41
7	2.20	0.50	3.80	1.31	0.20	9.50	270.64
8	2.40	0.50	4.10	1.27	0.20	9.50	264.50
9	2.60	0.50	4.40	1.24	0.20	9.50	256.92
10	2.80	0.50	4.70	1.23	0.20	9.50	254.98
11	3.00	0.50	5.00	1.24	0.20	9.50	258.10
12	3.20	0.50	5.30	1.24	0.20	9.50	257.32
13	3.40	0.50	5.60	1.24	0.20	9.50	257.02
14	3.60	0.50	5.90	1.24	0.20	9.50	258.02
15	3.80	0.50	6.20	1.23	0.20	9.50	256.46
16	4.00	0.50	6.50	1.22	0.20	9.50	253.39

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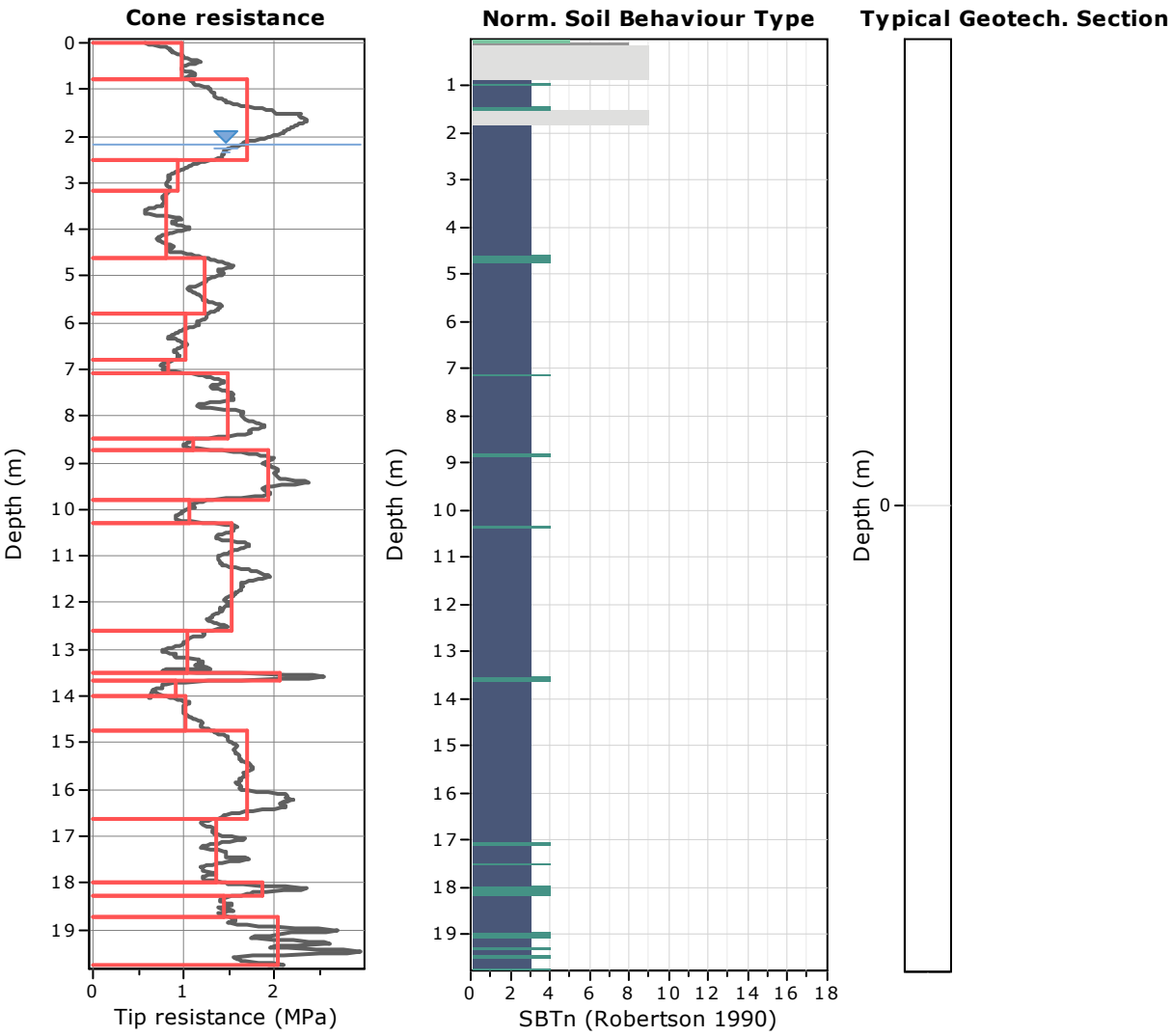
Project:
Location:

CPT: CPTu-03
Total depth: 19.76 m, Date: 11/02/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Tabular results

.:: Layer No: 1 ::.

Code: R **Start depth:** 0.00 (m), **End depth:** 0.80 (m)

Description: Very dense/stiff soil

Basic results	Estimation results	
Total cone resistance: 0.97 ±0.15 MPa	Permeability: 7.39E-07 ±1.94E-06 m/s	Constrained Mod.: 13.42 ±2.26 MPa
Sleeve friction: 69.81 ±24.24 kPa	N60: 3.73 ±0.96 blows	Go: 22.42 ±6.83 MPa
SBT_n: 9	Es: 16.92 ±3.00 MPa	Su: 72.25 ±6.31 kPa
SBTn description: Very dense/stiff soil	Dr (%): 0.00 ±0.00	Su ratio: 6.60 ±1.74
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 30.50 ±8.04
	Unit weight: 17.74 ±0.68 kN/m³	

.:: Layer No: 2 ::.

Code: B **Start depth:** 0.80 (m), **End depth:** 2.50 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.70 ±0.40 MPa	Permeability: 5.20E-08 ±2.86E-08 m/s	Constrained Mod.: 23.43 ±5.50 MPa
Sleeve friction: 123.66 ±33.50 kPa	N60: 7.43 ±1.61 blows	Go: 47.87 ±10.43 MPa
SBT_n: 3	Es: 39.94 ±1.75 MPa	Su: 119.53 ±28.08 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 3.72 ±0.80
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 17.17 ±3.72
	Unit weight: 18.68 ±0.40 kN/m³	

.:: Layer No: 3 ::.

Code: A **Start depth:** 2.50 (m), **End depth:** 3.18 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 0.94 ±0.15 MPa	Permeability: 6.46E-09 ±3.58E-09 m/s	Constrained Mod.: 12.42 ±2.16 MPa
Sleeve friction: 64.78 ±12.31 kPa	N60: 4.71 ±0.79 blows	Go: 36.32 ±3.45 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 63.36 ±11.02 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.39 ±0.28
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 6.41 ±1.29
	Unit weight: 17.74 ±0.27 kN/m³	

.:: Layer No: 4 ::.

Code: E **Start depth:** 3.18 (m), **End depth:** 4.60 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 0.80 ±0.12 MPa	Permeability: 4.20E-09 ±3.02E-09 m/s	Constrained Mod.: 9.59 ±2.42 MPa
Sleeve friction: 49.17 ±8.98 kPa	N60: 4.34 ±0.48 blows	Go: 33.18 ±2.78 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 52.09 ±8.82 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.99 ±0.16
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 4.56 ±0.76
	Unit weight: 17.36 ±0.24 kN/m³	

.:: Layer No: 5 ::.

Code: D **Start depth:** 4.60 (m), **End depth:** 5.80 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.24 ±0.19 MPa	Permeability: 1.34E-08 ±9.08E-09 m/s	Constrained Mod.: 16.00 ±2.68 MPa
Sleeve friction: 59.25 ±19.09 kPa	N60: 6.15 ±0.95 blows	Go: 42.19 ±6.62 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 81.83 ±13.24 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.29 ±0.20
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 5.97 ±0.92
	Unit weight: 17.69 ±0.46 kN/m³	

.:: Layer No: 6 ::.

Code: A2 **Start depth:** 5.80 (m), **End depth:** 6.80 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.01 ±0.13 MPa	Permeability: 3.80E-09 ±1.85E-09 m/s	Constrained Mod.: 11.00 ±3.06 MPa
Sleeve friction: 54.33 ±17.68 kPa	N60: 5.55 ±0.73 blows	Go: 41.01 ±5.33 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 64.41 ±9.78 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.89 ±0.16
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 4.12 ±0.75
	Unit weight: 17.53 ±0.41 kN/m³	

.:: Layer No: 7 ::.

Code: E2 **Start depth:** 6.80 (m), **End depth:** 7.08 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 0.82 ±0.07 MPa	Permeability: 3.31E-09 ±3.52E-09 m/s	Constrained Mod.: 6.32 ±1.30 MPa
Sleeve friction: 33.00 ±7.20 kPa	N60: 4.80 ±0.41 blows	Go: 33.65 ±2.01 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 49.73 ±4.93 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.64 ±0.06
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.97 ±0.29
	Unit weight: 16.90 ±0.25 kN/m³	

.:: Layer No: 8 ::.

Code: D2 **Start depth:** 7.08 (m), **End depth:** 8.46 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.49 ±0.22 MPa	Permeability: 6.38E-09 ±4.27E-09 m/s	Constrained Mod.: 18.67 ±3.47 MPa
Sleeve friction: 90.03 ±28.14 kPa	N60: 7.87 ±1.19 blows	Go: 57.32 ±9.61 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 96.66 ±15.32 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.15 ±0.16
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 5.30 ±0.72
	Unit weight: 18.23 ±0.53 kN/m³	

.:: Layer No: 9 ::.

Code: A3 **Start depth:** 8.46 (m), **End depth:** 8.72 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.10 ±0.10 MPa	Permeability: 1.61E-09 ±1.60E-09 m/s	Constrained Mod.: 9.86 ±2.09 MPa
Sleeve friction: 82.28 ±28.99 kPa	N60: 6.71 ±0.73 blows	Go: 52.76 ±7.05 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 67.36 ±6.85 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.74 ±0.08
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 3.42 ±0.35
	Unit weight: 18.03 ±0.42 kN/m³	

.:: Layer No: 10 ::.

Code: B2 **Start depth:** 8.72 (m), **End depth:** 9.78 (m)

Description: Clay

Basic results	Estimation results	
Total cone resistance: 1.92 ±0.22 MPa	Permeability: 1.02E-08 ±6.37E-09 m/s	Constrained Mod.: 24.38 ±3.48 MPa
Sleeve friction: 102.61 ±26.48 kPa	N60: 9.63 ±1.03 blows	Go: 67.65 ±8.60 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 125.09 ±15.79 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.29 ±0.16
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 5.98 ±0.75
	Unit weight: 18.51 ±0.40 kN/m³	

.:: Layer No: 11 ::.

Code: A4 **Start depth:** 9.78 (m), **End depth:** 10.30 (m)

Description: Clay

Basic results	Estimation results	
Total cone resistance: 1.06 ±0.13 MPa	Permeability: 3.20E-09 ±2.74E-09 m/s	Constrained Mod.: 7.61 ±2.28 MPa
Sleeve friction: 42.96 ±29.18 kPa	N60: 5.96 ±1.02 blows	Go: 42.94 ±9.64 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 62.69 ±9.04 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.61 ±0.09
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.80 ±0.42
	Unit weight: 17.14 ±0.67 kN/m³	

.:: Layer No: 12 ::.

Code: D3 **Start depth:** 10.30 (m), **End depth:** 12.60 (m)

Description: Clay

Basic results	Estimation results	
Total cone resistance: 1.52 ±0.16 MPa	Permeability: 3.62E-09 ±3.82E-09 m/s	Constrained Mod.: 15.23 ±3.97 MPa
Sleeve friction: 80.84 ±26.49 kPa	N60: 8.57 ±0.88 blows	Go: 62.29 ±8.47 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 93.67 ±11.81 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.82 ±0.12
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 3.79 ±0.55
	Unit weight: 18.14 ±0.41 kN/m³	

.:: Layer No: 13 ::.

Code: A5 **Start depth:** 12.60 (m), **End depth:** 13.50 (m)

Description: Clay

Basic results	Estimation results	
Total cone resistance: 1.03 ±0.16 MPa	Permeability: 2.19E-09 ±2.16E-09 m/s	Constrained Mod.: 5.19 ±1.98 MPa
Sleeve friction: 34.98 ±15.21 kPa	N60: 6.15 ±0.79 blows	Go: 43.61 ±6.56 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 56.99 ±11.45 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.45 ±0.09
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.06 ±0.42
	Unit weight: 16.97 ±0.54 kN/m³	

.:: Layer No: 14 ::.

Code: C **Start depth:** 13.50 (m), **End depth:** 13.66 (m)

Description: Clay & silty clay

Basic results	**Estimation results**	
Total cone resistance: 2.05 ±0.48 MPa	Permeability: 5.98E-08 ±4.83E-08 m/s	Constrained Mod.: 23.41 ±9.34 MPa
Sleeve friction: 31.33 ±10.20 kPa	N60: 8.67 ±1.41 blows	Go: 51.85 ±6.75 MPa
SBT_n: 4	Es: 42.32 ±2.25 MPa	Su: 128.78 ±34.57 kPa
SBTn description: Clay & silty clay	Dr (%): 0.00 ±0.00	Su ratio: 1.00 ±0.28
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 4.60 ±1.27
	Unit weight: 17.15 ±0.41 kN/m³	

.:: Layer No: 15 ::.

Code: E3 **Start depth:** 13.66 (m), **End depth:** 14.00 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 0.91 ±0.29 MPa	Permeability: 1.44E-09 ±2.18E-09 m/s	Constrained Mod.: 3.97 ±4.02 MPa
Sleeve friction: 28.62 ±7.37 kPa	N60: 5.64 ±1.03 blows	Go: 40.28 ±6.51 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 47.71 ±21.07 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.36 ±0.16
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 1.66 ±0.74
	Unit weight: 16.77 ±0.35 kN/m³	

.:: Layer No: 16 ::.

Code: A7 **Start depth:** 14.00 (m), **End depth:** 14.74 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.01 ±0.19 MPa	Permeability: 1.20E-09 ±4.75E-10 m/s	Constrained Mod.: 4.37 ±1.82 MPa
Sleeve friction: 29.51 ±10.16 kPa	N60: 6.20 ±0.84 blows	Go: 42.45 ±7.05 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 53.79 ±12.96 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.39 ±0.09
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 1.82 ±0.42
	Unit weight: 16.81 ±0.47 kN/m³	

.:: Layer No: 17 ::.

Code: D4 **Start depth:** 14.74 (m), **End depth:** 16.62 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.69 ±0.23 MPa	Permeability: 1.94E-09 ±9.93E-10 m/s	Constrained Mod.: 13.83 ±4.31 MPa
Sleeve friction: 86.21 ±21.42 kPa	N60: 9.94 ±1.08 blows	Go: 72.44 ±8.76 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 100.96 ±16.10 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.68 ±0.10
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 3.16 ±0.45
	Unit weight: 18.28 ±0.31 kN/m³	

.:: Layer No: 18 ::.

Code: A8 **Start depth:** 16.62 (m), **End depth:** 18.00 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.36 ±0.15 MPa	Permeability: 5.07E-09 ±3.41E-09 m/s	Constrained Mod.: 7.00 ±2.02 MPa
Sleeve friction: 22.96 ±7.94 kPa	N60: 7.34 ±0.48 blows	Go: 46.16 ±4.32 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 74.92 ±10.39 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.47 ±0.07
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.16 ±0.30
	Unit weight: 16.65 ±0.38 kN/m³	

.:: Layer No: 19 ::.

Code: B3 **Start depth:** 18.00 (m), **End depth:** 18.28 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.85 ±0.30 MPa	Permeability: 2.16E-08 ±2.25E-08 m/s	Constrained Mod.: 14.78 ±6.00 MPa
Sleeve friction: 31.21 ±15.53 kPa	N60: 9.00 ±1.07 blows	Go: 55.29 ±8.16 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 109.41 ±21.72 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.66 ±0.14
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 3.07 ±0.63
	Unit weight: 17.03 ±0.61 kN/m³	

.:: Layer No: 20 ::.

Code: C2 **Start depth:** 18.28 (m), **End depth:** 18.72 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.45 ±0.05 MPa	Permeability: 4.84E-09 ±1.96E-09 m/s	Constrained Mod.: 7.46 ±0.73 MPa
Sleeve friction: 23.69 ±7.50 kPa	N60: 7.96 ±0.37 blows	Go: 48.65 ±3.65 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 79.98 ±3.86 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.47 ±0.02
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.19 ±0.11
	Unit weight: 16.73 ±0.29 kN/m³	

.:: Layer No: 21 ::.

Code: B4 **Start depth:** 18.72 (m), **End depth:** 19.76 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 2.04 ±0.43 MPa	Permeability: 1.14E-08 ±1.25E-08 m/s	Constrained Mod.: 17.60 ±8.77 MPa
Sleeve friction: 48.48 ±15.26 kPa	N60: 10.42 ±1.45 blows	Go: 66.87 ±8.78 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 121.42 ±30.73 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.70 ±0.18
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 3.23 ±0.81
	Unit weight: 17.66 ±0.42 kN/m³	

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Project:
Location:

CPT: CPTu-03
Total depth: 19.76 m, Date: 11/02/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Summary table of mean values

From depth To depth (m)	Thickness (m)	Permeability (m/s)	SPT_{N60} (blows/30cm)	E_s (MPa)	D_r	Friction angle	Constrained modulus, M (MPa)	Shear modulus, G_O (MPa)	Undrained strength, S_U (kPa)	Undrained strength ratio	OCR	Unit weight (kN/m³)
0.00	0.80	7.39E-07	3.7	16.9	0.0	0.0	13.4	22.4	72.2	6.6	30.5	17.7
0.80		(±1.94E-06)	(±1.0)	(±3.0)	(±0.0)	(±0.0)	(±2.3)	(±6.8)	(±6.3)	(±1.7)	(±8.0)	(±0.7)
0.80	1.70	5.20E-08	7.4	39.9	0.0	0.0	23.4	47.9	119.5	3.7	17.2	18.7
2.50		(±2.86E-08)	(±1.6)	(±1.8)	(±0.0)	(±0.0)	(±5.5)	(±10.4)	(±28.1)	(±0.8)	(±3.7)	(±0.4)
2.50	0.68	6.46E-09	4.7	0.0	0.0	0.0	12.4	36.3	63.4	1.4	6.4	17.7
3.18		(±3.58E-09)	(±0.8)	(±0.0)	(±0.0)	(±0.0)	(±2.2)	(±3.4)	(±11.0)	(±0.3)	(±1.3)	(±0.3)
3.18	1.42	4.20E-09	4.3	0.0	0.0	0.0	9.6	33.2	52.1	1.0	4.6	17.4
4.60		(±3.02E-09)	(±0.5)	(±0.0)	(±0.0)	(±0.0)	(±2.4)	(±2.8)	(±8.8)	(±0.2)	(±0.8)	(±0.2)
4.60	1.20	1.34E-08	6.1	0.0	0.0	0.0	16.0	42.2	81.8	1.3	6.0	17.7
5.80		(±9.08E-09)	(±0.9)	(±0.0)	(±0.0)	(±0.0)	(±2.7)	(±6.6)	(±13.2)	(±0.2)	(±0.9)	(±0.5)
5.80	1.00	3.80E-09	5.5	0.0	0.0	0.0	11.0	41.0	64.4	0.9	4.1	17.5
6.80		(±1.85E-09)	(±0.7)	(±0.0)	(±0.0)	(±0.0)	(±3.1)	(±5.3)	(±9.8)	(±0.2)	(±0.7)	(±0.4)
6.80	0.28	3.31E-09	4.8	0.0	0.0	0.0	6.3	33.7	49.7	0.6	3.0	16.9
7.08		(±3.52E-09)	(±0.4)	(±0.0)	(±0.0)	(±0.0)	(±1.3)	(±2.0)	(±4.9)	(±0.1)	(±0.3)	(±0.3)
7.08	1.38	6.38E-09	7.9	0.0	0.0	0.0	18.7	57.3	96.7	1.1	5.3	18.2
8.46		(±4.27E-09)	(±1.2)	(±0.0)	(±0.0)	(±0.0)	(±3.5)	(±9.6)	(±15.3)	(±0.2)	(±0.7)	(±0.5)
8.46	0.26	1.61E-09	6.7	0.0	0.0	0.0	9.9	52.8	67.4	0.7	3.4	18.0
8.72		(±1.60E-09)	(±0.7)	(±0.0)	(±0.0)	(±0.0)	(±2.1)	(±7.0)	(±6.8)	(±0.1)	(±0.4)	(±0.4)
8.72	1.06	1.02E-08	9.6	0.0	0.0	0.0	24.4	67.6	125.1	1.3	6.0	18.5
9.78		(±6.37E-09)	(±1.0)	(±0.0)	(±0.0)	(±0.0)	(±3.5)	(±8.6)	(±15.8)	(±0.2)	(±0.7)	(±0.4)
9.78	0.52	3.20E-09	6.0	0.0	0.0	0.0	7.6	42.9	62.7	0.6	2.8	17.1
10.30		(±2.74E-09)	(±1.0)	(±0.0)	(±0.0)	(±0.0)	(±2.3)	(±9.6)	(±9.0)	(±0.1)	(±0.4)	(±0.7)

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Project:
Location:

CPT: CPTu-03
Total depth: 19.76 m, Date: 11/02/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Summary table of mean values

From depth To depth (m)	Thickness (m)	Permeability (m/s)	SPT_{N60} (blows/30cm)	E_s (MPa)	D_r	Friction angle	Constrained modulus, M (MPa)	Shear modulus, G_O (MPa)	Undrained strength, S_U (kPa)	Undrained strength ratio	OCR	Unit weight (kN/m³)
10.30	2.30	3.62E-09	8.6	0.0	0.0	0.0	15.2	62.3	93.7	0.8	3.8	18.1
12.60		(±3.82E-09)	(±0.9)	(±0.0)	(±0.0)	(±0.0)	(±4.0)	(±8.5)	(±11.8)	(±0.1)	(±0.6)	(±0.4)
12.60	0.90	2.19E-09	6.2	0.0	0.0	0.0	5.2	43.6	57.0	0.4	2.1	17.0
13.50		(±2.16E-09)	(±0.8)	(±0.0)	(±0.0)	(±0.0)	(±2.0)	(±6.6)	(±11.5)	(±0.1)	(±0.4)	(±0.5)
13.50	0.16	5.98E-08	8.7	42.3	0.0	0.0	23.4	51.8	128.8	1.0	4.6	17.2
13.66		(±4.83E-08)	(±1.4)	(±2.3)	(±0.0)	(±0.0)	(±9.3)	(±6.8)	(±34.6)	(±0.3)	(±1.3)	(±0.4)
13.66	0.34	1.44E-09	5.6	0.0	0.0	0.0	4.0	40.3	47.7	0.4	1.7	16.8
14.00		(±2.18E-09)	(±1.0)	(±0.0)	(±0.0)	(±0.0)	(±4.0)	(±6.5)	(±21.1)	(±0.2)	(±0.7)	(±0.4)
14.00	0.74	1.20E-09	6.2	0.0	0.0	0.0	4.4	42.5	53.8	0.4	1.8	16.8
14.74		(±4.75E-10)	(±0.8)	(±0.0)	(±0.0)	(±0.0)	(±1.8)	(±7.0)	(±13.0)	(±0.1)	(±0.4)	(±0.5)
14.74	1.88	1.94E-09	9.9	0.0	0.0	0.0	13.8	72.4	101.0	0.7	3.2	18.3
16.62		(±9.93E-10)	(±1.1)	(±0.0)	(±0.0)	(±0.0)	(±4.3)	(±8.8)	(±16.1)	(±0.1)	(±0.4)	(±0.3)
16.62	1.38	5.07E-09	7.3	0.0	0.0	0.0	7.0	46.2	74.9	0.5	2.2	16.6
18.00		(±3.41E-09)	(±0.5)	(±0.0)	(±0.0)	(±0.0)	(±2.0)	(±4.3)	(±10.4)	(±0.1)	(±0.3)	(±0.4)
18.00	0.28	2.16E-08	9.0	0.0	0.0	0.0	14.8	55.3	109.4	0.7	3.1	17.0
18.28		(±2.25E-08)	(±1.1)	(±0.0)	(±0.0)	(±0.0)	(±6.0)	(±8.2)	(±21.7)	(±0.1)	(±0.6)	(±0.6)
18.28	0.44	4.84E-09	8.0	0.0	0.0	0.0	7.5	48.6	80.0	0.5	2.2	16.7
18.72		(±1.96E-09)	(±0.4)	(±0.0)	(±0.0)	(±0.0)	(±0.7)	(±3.7)	(±3.9)	(±0.0)	(±0.1)	(±0.3)
18.72	1.04	1.14E-08	10.4	0.0	0.0	0.0	17.6	66.9	121.4	0.7	3.2	17.7
19.76		(±1.25E-08)	(±1.4)	(±0.0)	(±0.0)	(±0.0)	(±8.8)	(±8.8)	(±30.7)	(±0.2)	(±0.8)	(±0.4)

Depth values presented in this table are measured from free ground surface

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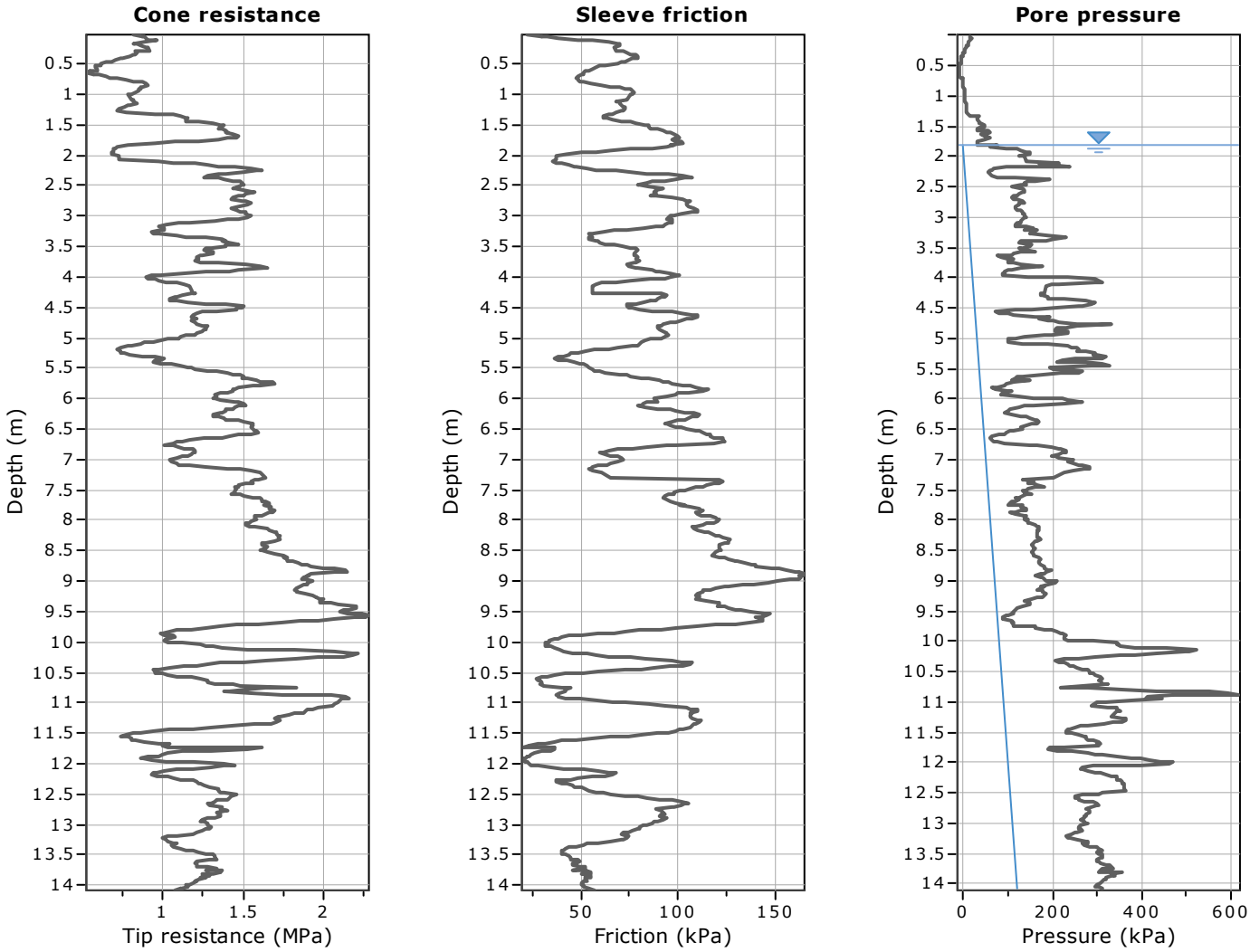
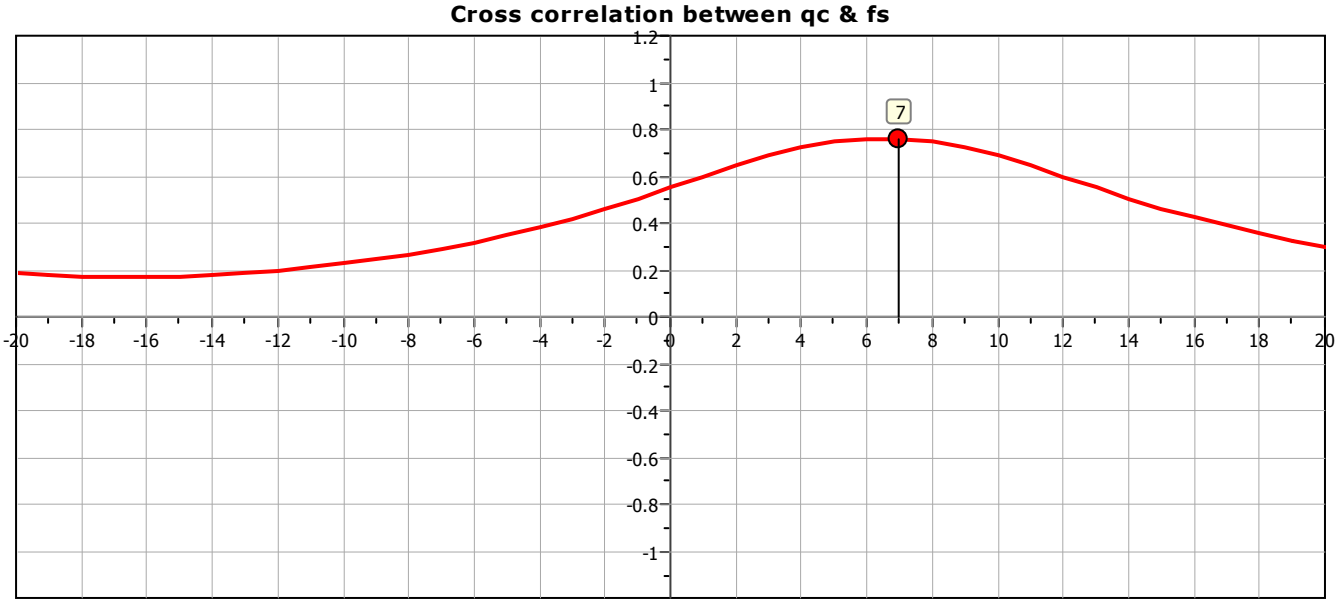
CPT: CPTu-04
Total depth: 14.08 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:



The plot below presents the cross correlation coeficient between the raw qc and fs values (as measured on the field). X axes presents the lag distance (one lag is the distance between two sucessive CPT measurements).



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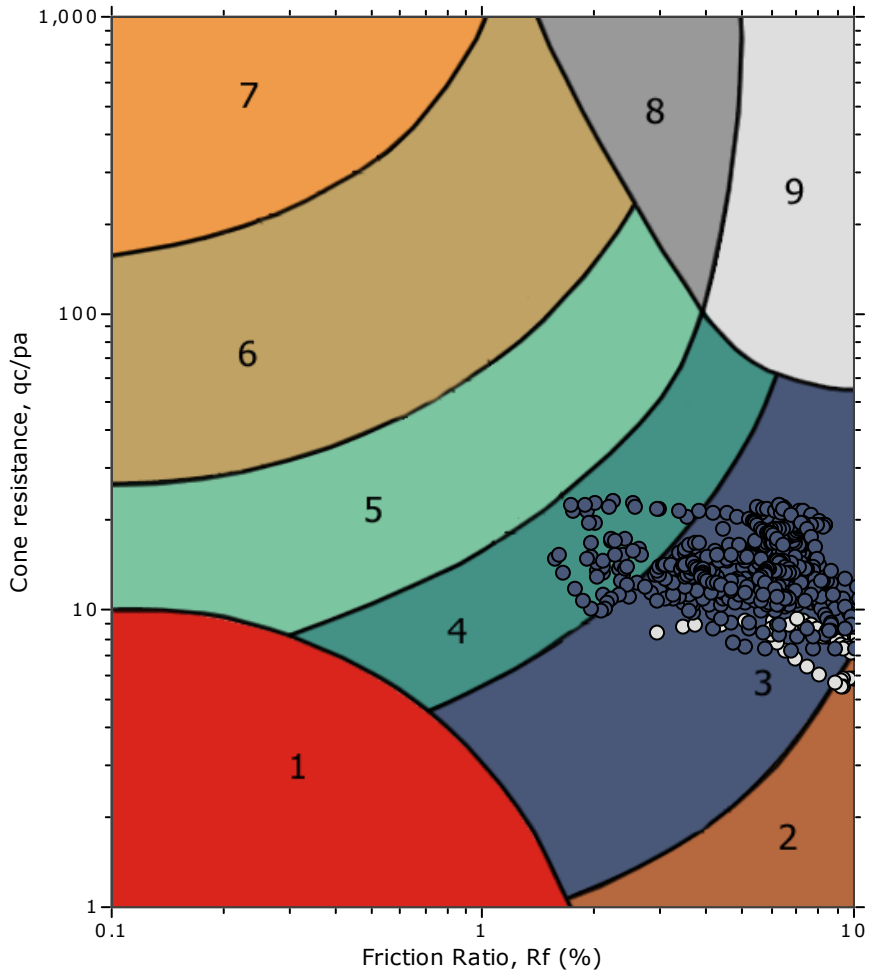
Project:
Location:

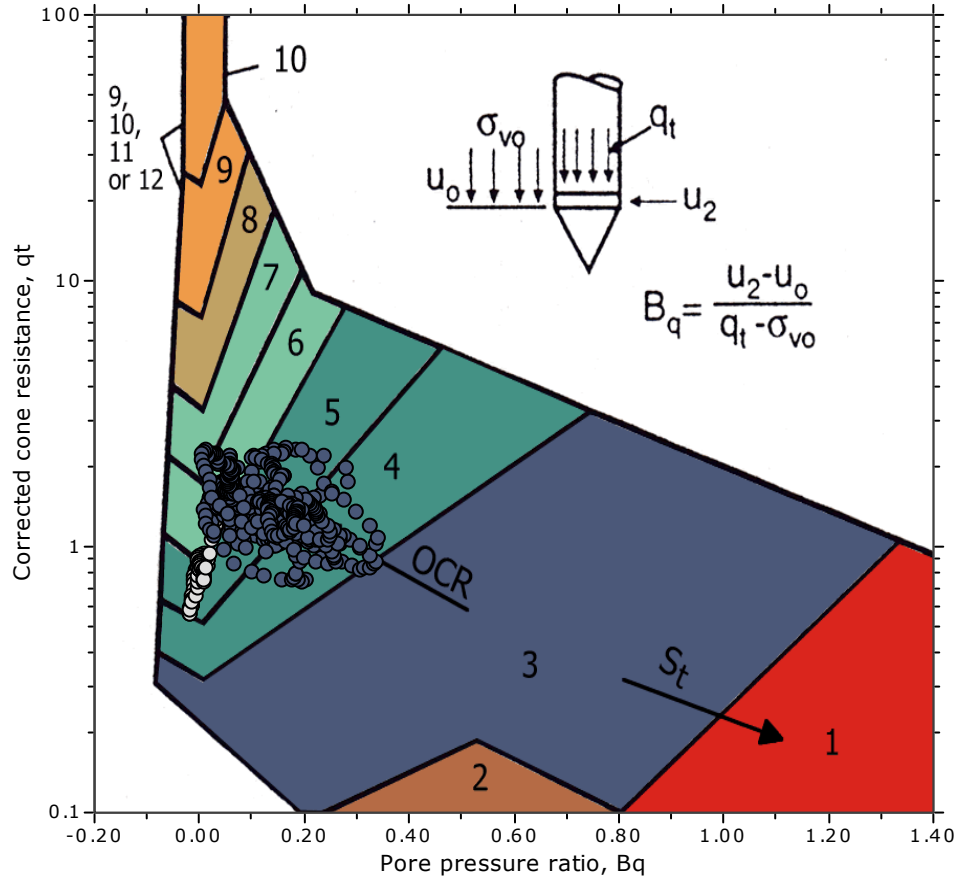
CPT: CPTu-04
Total depth: 14.08 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

SBT - Bq plots

SBT plot



Bq plot



SBT legend

- 1. Sensitive fine grained
- 2. Organic material
- 3. Clay to silty clay
- 4. Clayey silt to silty clay
- 5. Silty sand to sandy silt
- 6. Clean sand to silty sand
- 7. Gravely sand to sand
- 8. Very stiff sand to clayey sand
- 9. Very stiff fine grained

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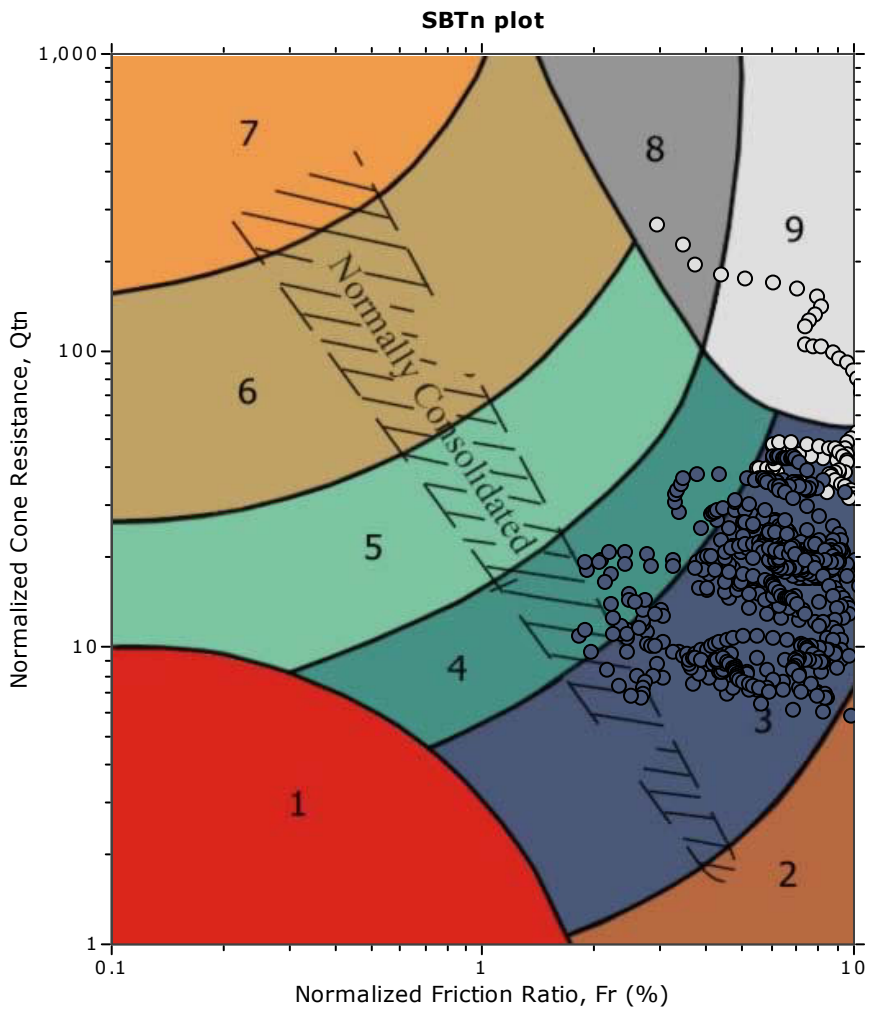
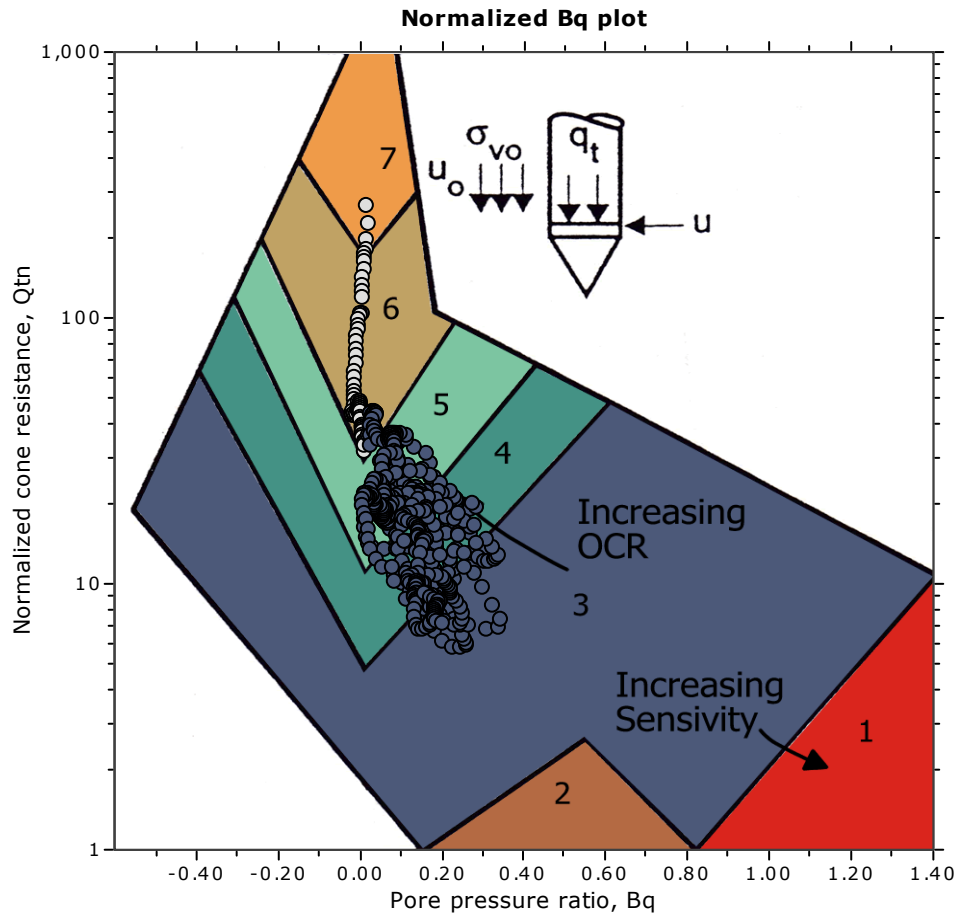
Project:
Location:

CPT: CPTu-04
Total depth: 14.08 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

SBT - Bq plots (normalized)





SBTn legend

- 1. Sensitive fine grained
- 2. Organic material
- 3. Clay to silty clay
- 4. Clayey silt to silty clay
- 5. Silty sand to sandy silt
- 6. Clean sand to silty sand
- 7. Gravely sand to sand
- 8. Very stiff sand to clayey sand
- 9. Very stiff fine grained

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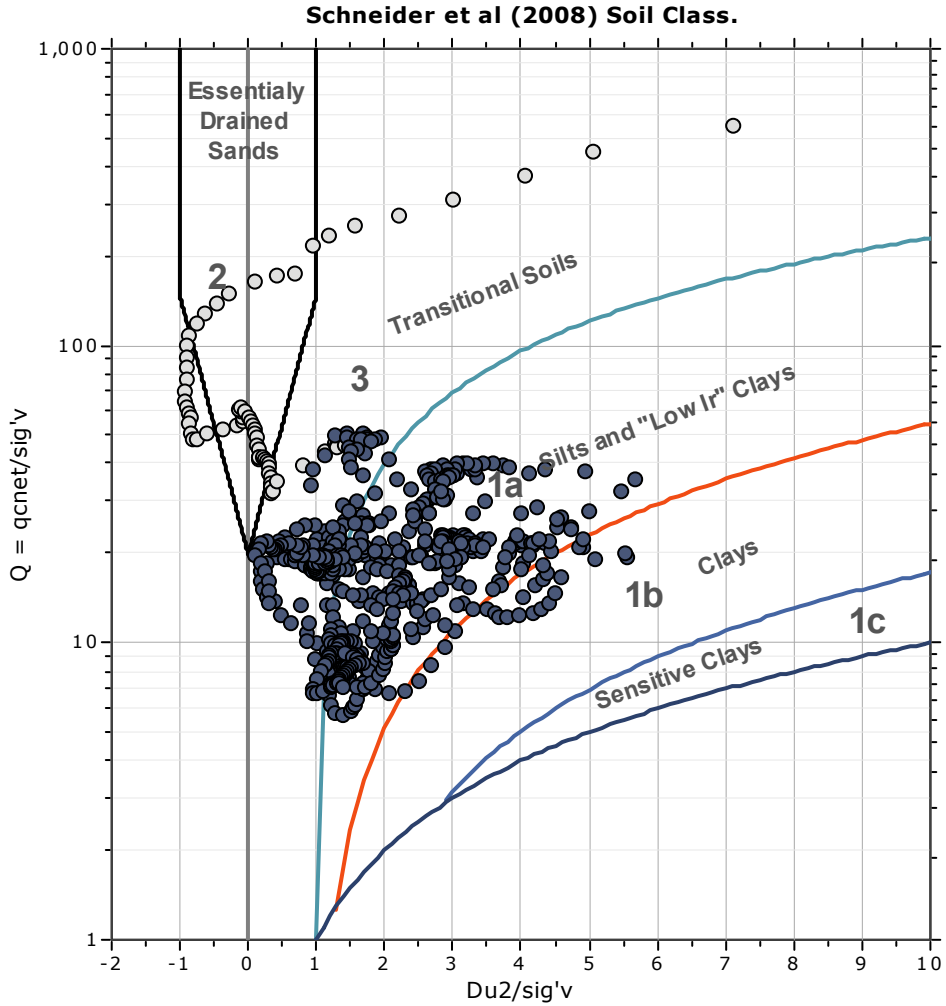
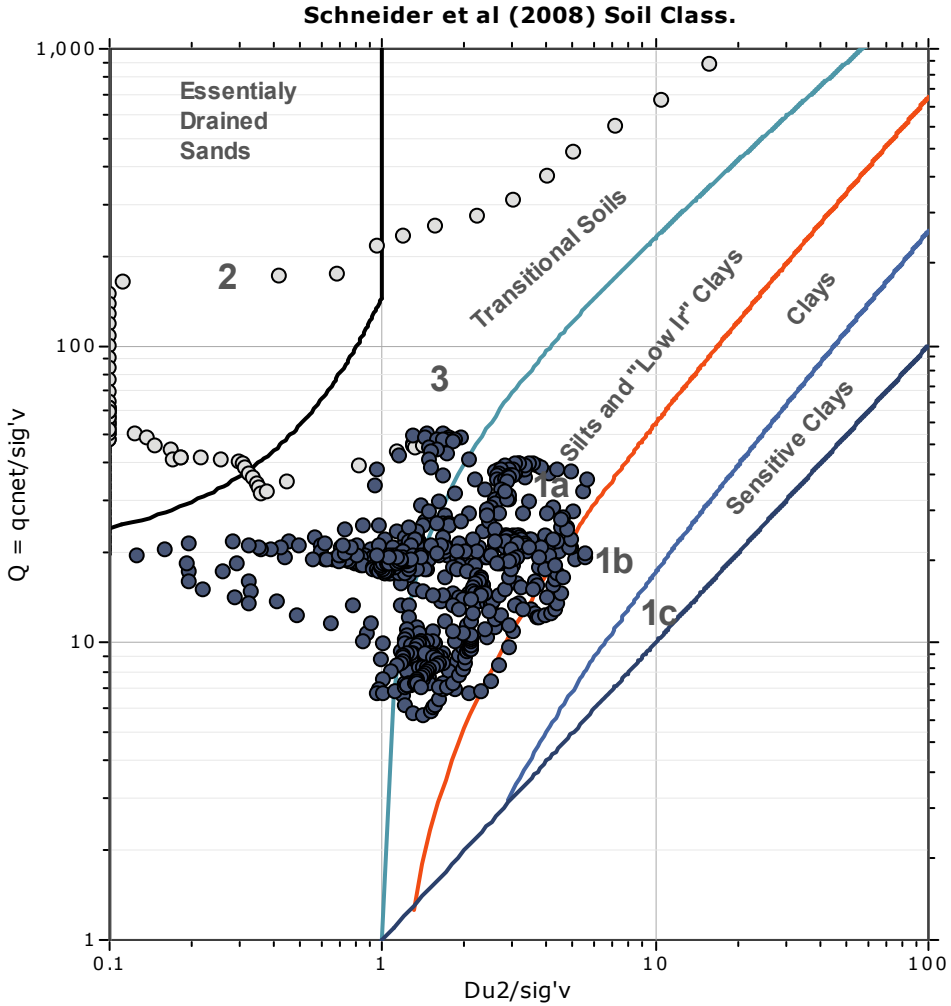
Project:
Location:

CPT: CPTu-04
Total depth: 14.08 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Bq plots (Schneider)





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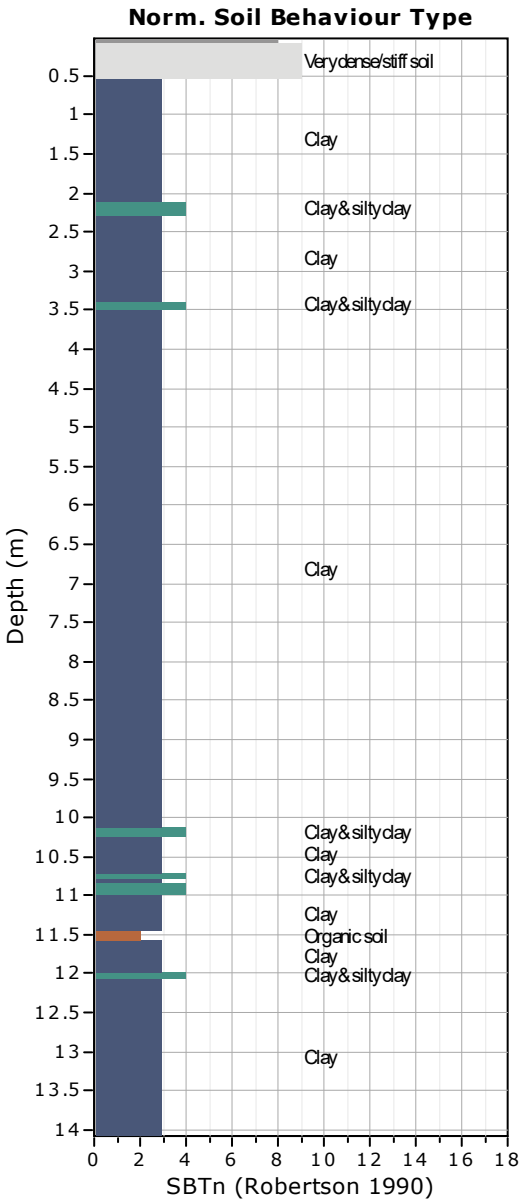
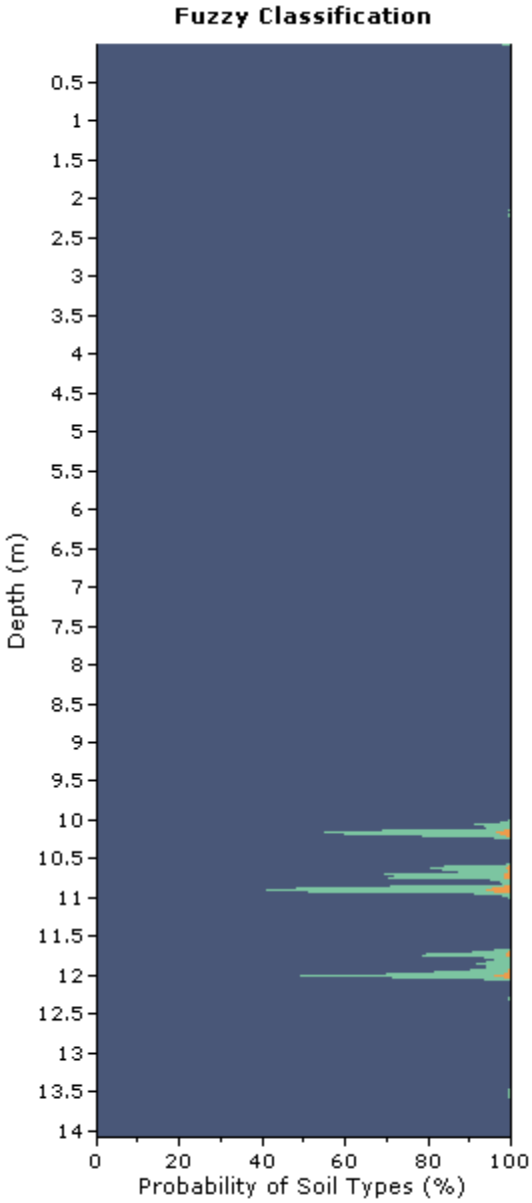
CPT: CPTu-04
Total depth: 14.08 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:





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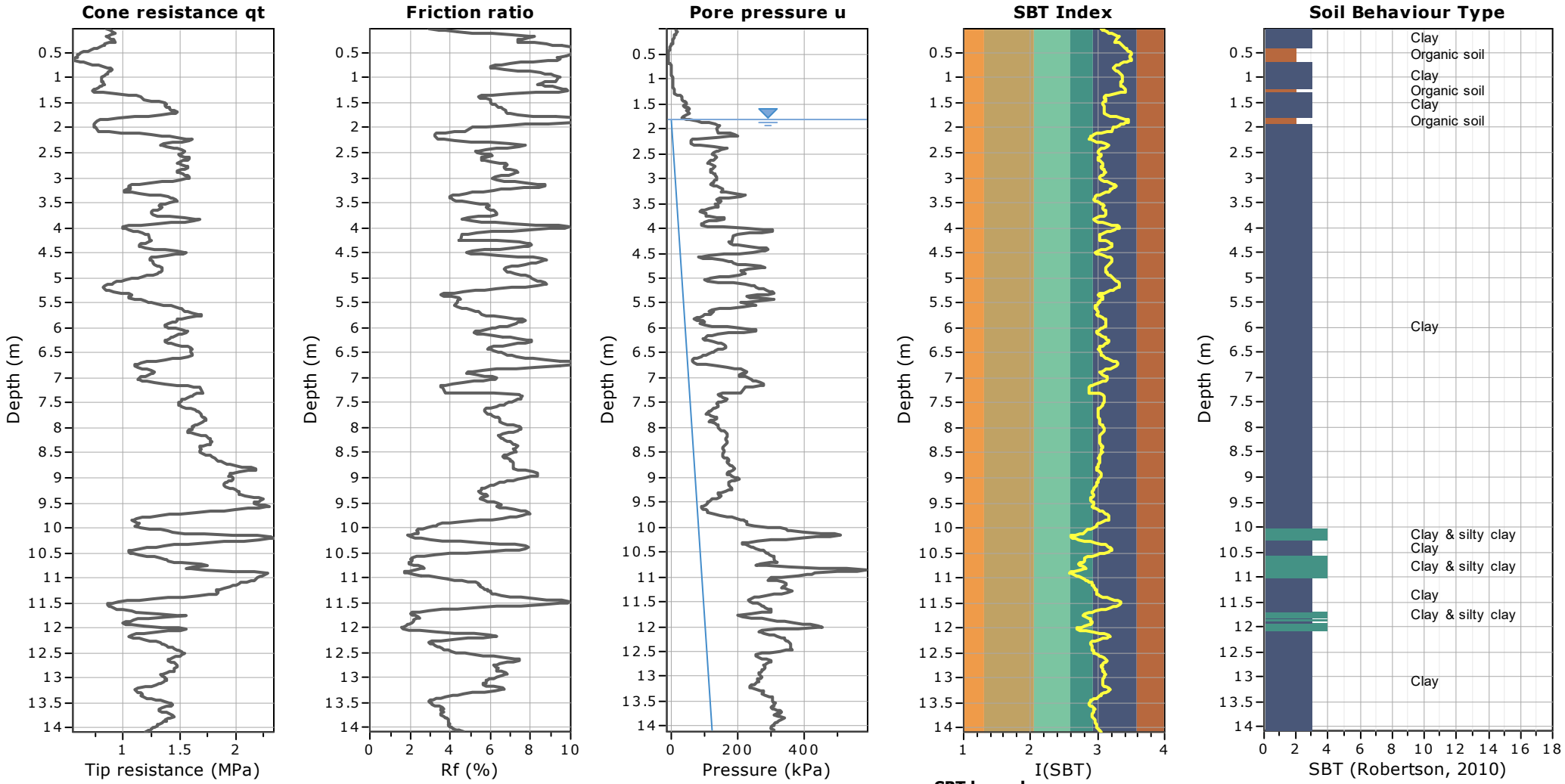
Project:
Location:

CPT: CPTu-04
Total depth: 14.08 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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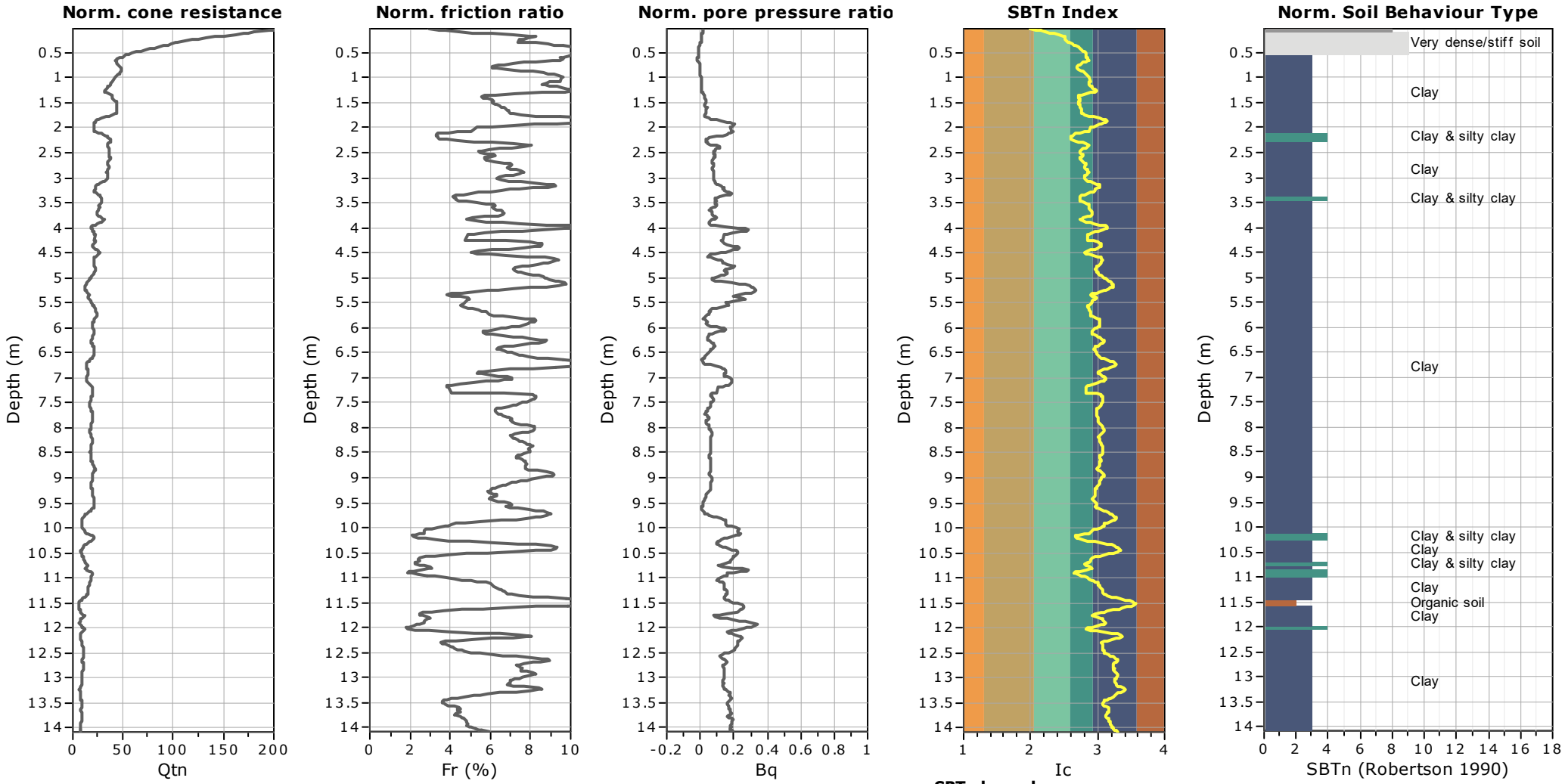
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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CPT: CPTu-04
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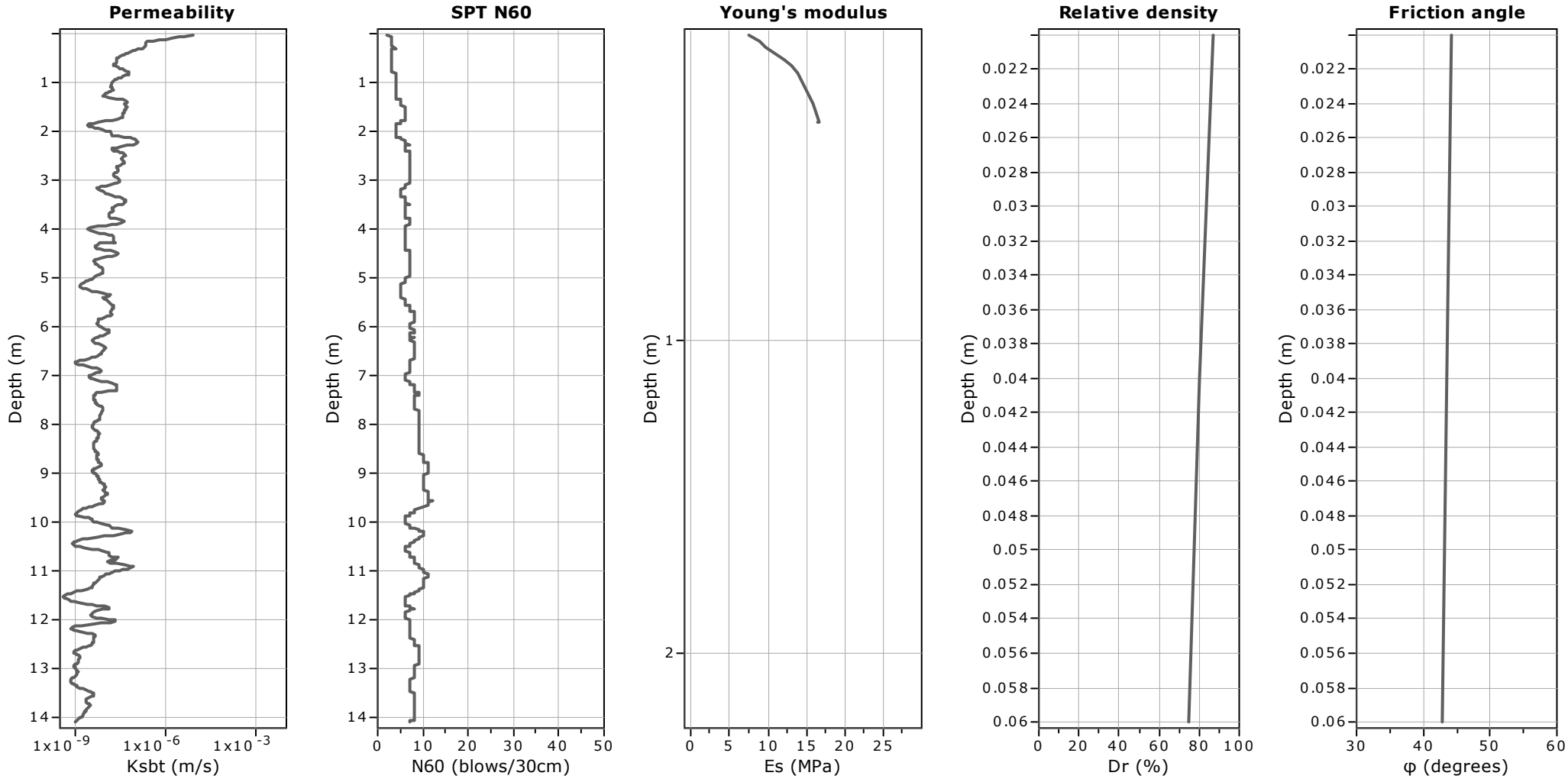
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Permeability: Based on SBT_n
SPT N_{60}: Based on I_c and q_t
Young's modulus: Based on variable alpha using I_c (Robertson, 2009)
Relative desnisty constant, C_{Dr}: 350.0
Phi: Based on Kulhawy & Mayne (1990)
User defined estimation data

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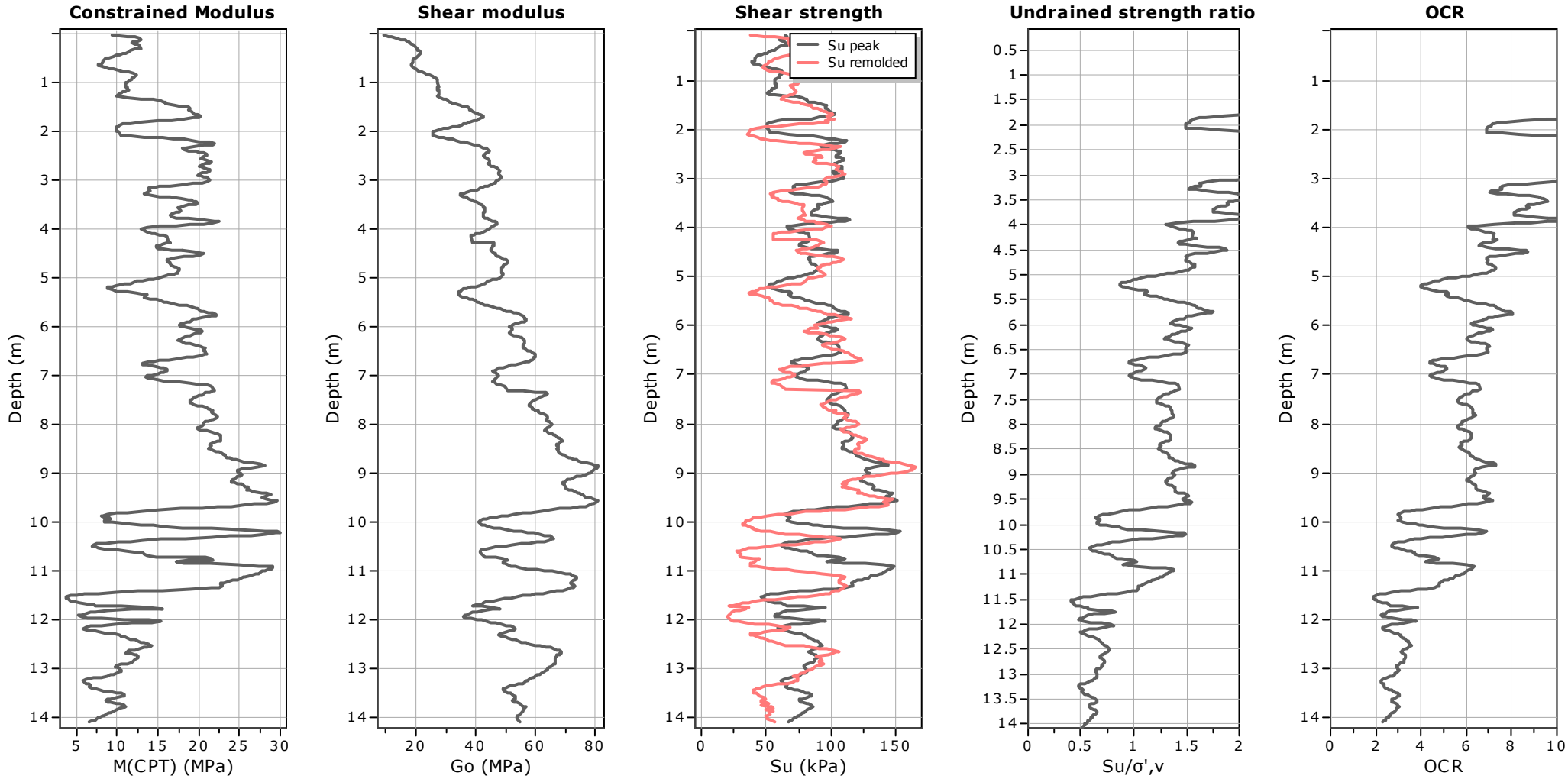
Total depth: 14.08 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Constrained modulus: Based on variable *alpha* using I_c and Q_{tn} (Robertson, 2009)
Go: Based on variable *alpha* using I_c (Robertson, 2009)
Undrained shear strength cone factor for clays, N_{kt}: 14

OCR factor for clays, N_{kt}: 0.33
User defined estimation data

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Location:

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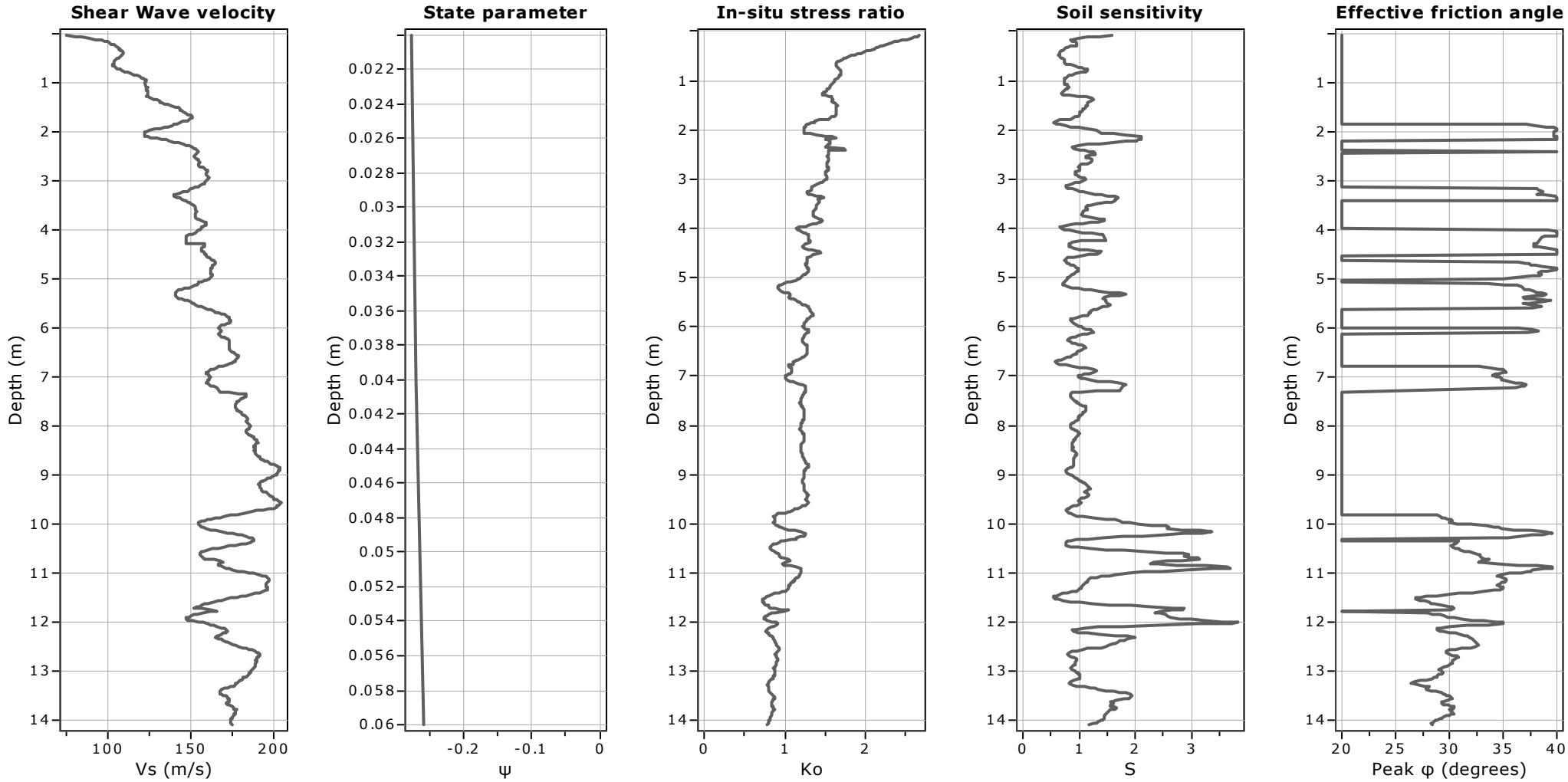
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Soil Sensitivity factor, N_S: 7.00

User defined estimation data

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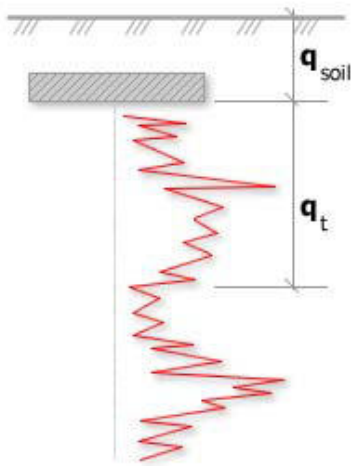
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

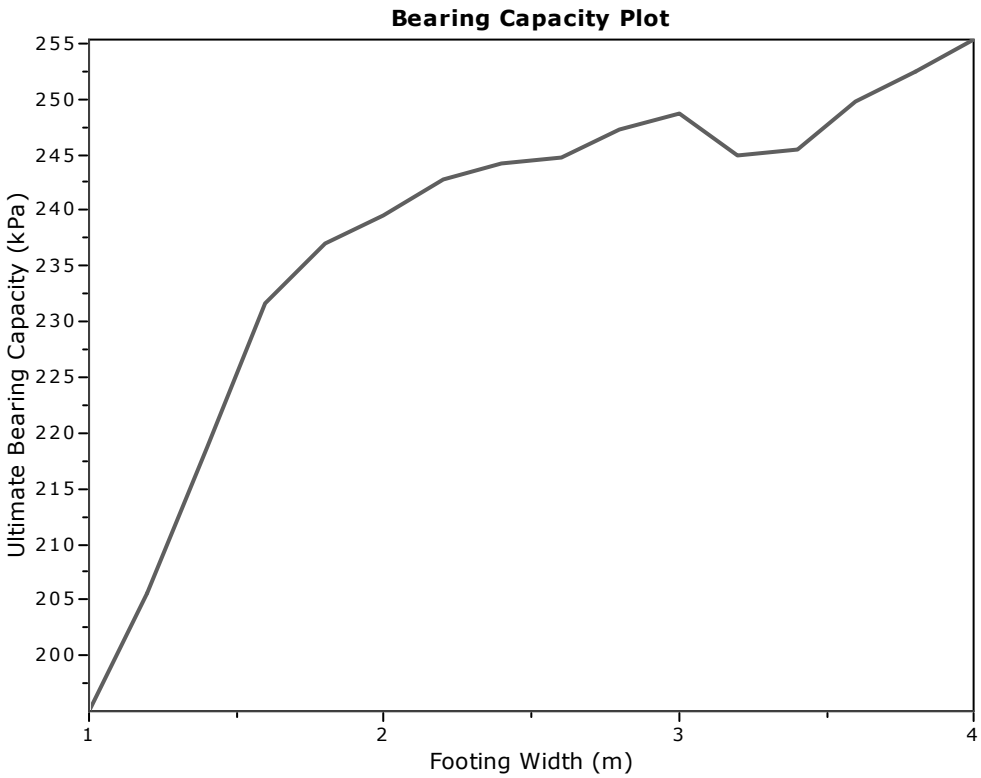
Project:
Location:



Bearing Capacity calculation is perfromed based on the formula:

$$Q_{ult} = R_k \times q_t + q_{soil}$$

where:
R_k: Bearing capacity factor
q_t: Average corrected cone resistance over calculation depth
q_{soil}: Pressure applied by soil above footing



:: Tabular results ::

No	B (m)	Start Depth (m)	End Depth (m)	Ave. q_t (MPa)	R_k	Soil Press. (kPa)	Ult. bearing cap. (kPa)
1	1.00	0.50	2.00	0.93	0.20	9.50	195.03
2	1.20	0.50	2.30	0.98	0.20	9.50	205.60
3	1.40	0.50	2.60	1.05	0.20	9.50	218.69
4	1.60	0.50	2.90	1.11	0.20	9.50	231.65
5	1.80	0.50	3.20	1.14	0.20	9.50	237.03
6	2.00	0.50	3.50	1.15	0.20	9.50	239.59
7	2.20	0.50	3.80	1.17	0.20	9.50	242.72
8	2.40	0.50	4.10	1.17	0.20	9.50	244.22
9	2.60	0.50	4.40	1.18	0.20	9.50	244.69
10	2.80	0.50	4.70	1.19	0.20	9.50	247.26
11	3.00	0.50	5.00	1.20	0.20	9.50	248.64
12	3.20	0.50	5.30	1.18	0.20	9.50	244.99
13	3.40	0.50	5.60	1.18	0.20	9.50	245.47
14	3.60	0.50	5.90	1.20	0.20	9.50	249.74
15	3.80	0.50	6.20	1.21	0.20	9.50	252.48
16	4.00	0.50	6.50	1.23	0.20	9.50	255.33

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Project:
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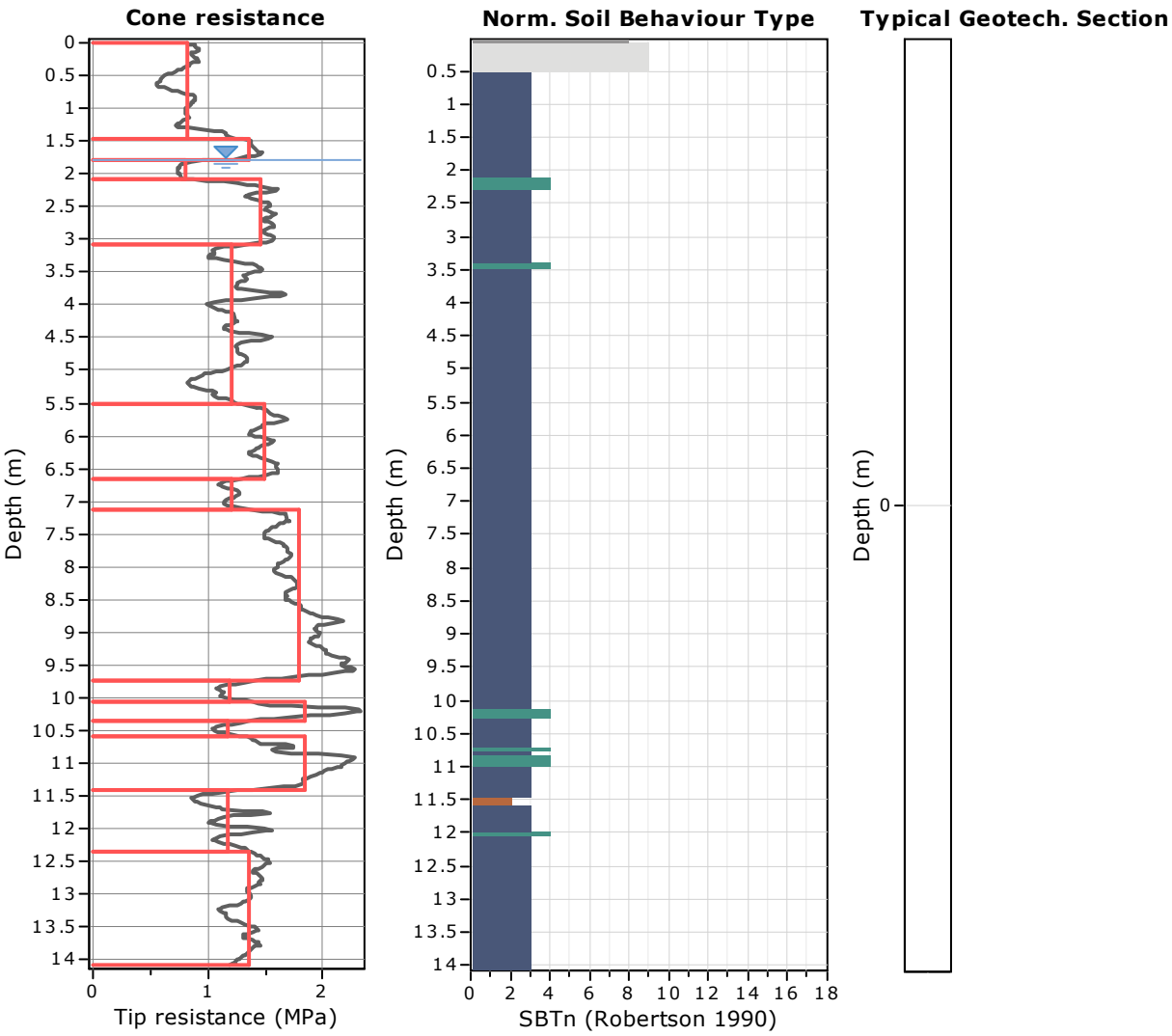
CPT: CPTu-04
Total depth: 14.08 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Tabular results

.:: Layer No: 1 ::.

Code: A **Start depth:** 0.00 (m), **End depth:** 1.46 (m)

Description: Very dense/stiff soil

Basic results	Estimation results	
Total cone resistance: 0.82 ±0.15 MPa	Permeability: 2.98E-07 ±1.11E-06 m/s	Constrained Mod.: 11.30 ±2.07 MPa
Sleeve friction: 64.31 ±12.23 kPa	N60: 3.56 ±0.69 blows	Go: 23.19 ±5.41 MPa
SBT_n: 9	Es: 14.53 ±1.80 MPa	Su: 57.76 ±10.73 kPa
SBTn description: Very dense/stiff soil	Dr (%): 0.00 ±0.00	Su ratio: 4.55 ±2.78
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 21.03 ±12.84
	Unit weight: 17.67 ±0.27 kN/m³	

.:: Layer No: 2 ::.

Code: D **Start depth:** 1.46 (m), **End depth:** 1.78 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.36 ±0.10 MPa	Permeability: 3.72E-08 ±1.10E-08 m/s	Constrained Mod.: 18.66 ±1.34 MPa
Sleeve friction: 91.77 ±8.38 kPa	N60: 5.88 ±0.33 blows	Go: 39.78 ±2.24 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 95.20 ±6.85 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 2.99 ±0.22
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 13.82 ±1.00
	Unit weight: 18.30 ±0.11 kN/m³	

.:: Layer No: 3 ::.

Code: E **Start depth:** 1.78 (m), **End depth:** 2.08 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 0.81 ±0.10 MPa	Permeability: 8.65E-09 ±6.45E-09 m/s	Constrained Mod.: 10.86 ±1.42 MPa
Sleeve friction: 67.97 ±26.72 kPa	N60: 4.20 ±0.41 blows	Go: 31.38 ±5.03 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 55.41 ±7.24 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.66 ±0.25
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 7.67 ±1.16
	Unit weight: 17.67 ±0.49 kN/m³	

.:: Layer No: 4 ::.

Code: D1 **Start depth:** 2.08 (m), **End depth:** 3.08 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.47 ±0.15 MPa	Permeability: 3.90E-08 ±2.70E-08 m/s	Constrained Mod.: 19.92 ±2.00 MPa
Sleeve friction: 86.45 ±22.00 kPa	N60: 6.55 ±0.78 blows	Go: 43.16 ±5.74 MPa
SBT_n: 3	Es: 29.09 ±29.09 MPa	Su: 101.61 ±10.18 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 2.47 ±0.21
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 11.40 ±0.95
	Unit weight: 18.21 ±0.40 kN/m³	

.:: Layer No: 5 ::.

Code: A2 **Start depth:** 3.08 (m), **End depth:** 5.50 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.22 ±0.19 MPa	Permeability: 1.24E-08 ±1.05E-08 m/s	Constrained Mod.: 15.86 ±2.84 MPa
Sleeve friction: 76.71 ±18.05 kPa	N60: 6.09 ±0.70 blows	Go: 43.21 ±4.52 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 81.28 ±13.65 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.55 ±0.33
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 7.17 ±1.53
	Unit weight: 18.02 ±0.31 kN/m³	

.:: Layer No: 6 ::.

Code: D2 **Start depth:** 5.50 (m), **End depth:** 6.66 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.49 ±0.10 MPa	Permeability: 9.02E-09 ±4.54E-09 m/s	Constrained Mod.: 19.38 ±1.45 MPa
Sleeve friction: 95.14 ±16.67 kPa	N60: 7.54 ±0.60 blows	Go: 54.19 ±4.49 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 98.89 ±7.41 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.47 ±0.12
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 6.78 ±0.57
	Unit weight: 18.36 ±0.23 kN/m³	

.:: Layer No: 7 ::.

Code: A3 **Start depth:** 6.66 (m), **End depth:** 7.12 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.20 ±0.07 MPa	Permeability: 3.86E-09 ±2.44E-09 m/s	Constrained Mod.: 14.91 ±1.17 MPa
Sleeve friction: 81.10 ±23.91 kPa	N60: 6.71 ±0.46 blows	Go: 49.89 ±4.54 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 76.91 ±5.00 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.03 ±0.07
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 4.78 ±0.30
	Unit weight: 18.07 ±0.29 kN/m³	

.:: Layer No: 8 ::.

Code: B **Start depth:** 7.12 (m), **End depth:** 9.74 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.80 ±0.22 MPa	Permeability: 6.51E-09 ±3.72E-09 m/s	Constrained Mod.: 23.07 ±2.92 MPa
Sleeve friction: 119.05 ±22.63 kPa	N60: 9.42 ±1.08 blows	Go: 68.14 ±7.98 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 117.83 ±14.68 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.34 ±0.11
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 6.19 ±0.49
	Unit weight: 18.69 ±0.27 kN/m³	

.:: Layer No: 9 ::.

Code: A4 **Start depth:** 9.74 (m), **End depth:** 10.06 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.19 ±0.11 MPa	Permeability: 3.69E-09 ±3.51E-09 m/s	Constrained Mod.: 10.26 ±2.32 MPa
Sleeve friction: 56.07 ±26.19 kPa	N60: 6.65 ±0.79 blows	Go: 48.63 ±7.82 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 72.20 ±7.87 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.72 ±0.08
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 3.31 ±0.36
	Unit weight: 17.58 ±0.51 kN/m³	

.:: Layer No: 10 ::.

Code: B2 **Start depth:** 10.06 (m), **End depth:** 10.36 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.84 ±0.36 MPa	Permeability: 2.73E-08 ±2.49E-08 m/s	Constrained Mod.: 22.45 ±5.99 MPa
Sleeve friction: 63.38 ±27.72 kPa	N60: 8.88 ±1.15 blows	Go: 57.05 ±8.33 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 118.42 ±25.61 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.15 ±0.25
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 5.31 ±1.16
	Unit weight: 17.89 ±0.49 kN/m³	

.:: Layer No: 11 ::.

Code: A5 **Start depth:** 10.36 (m), **End depth:** 10.60 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.18 ±0.11 MPa	Permeability: 2.95E-09 ±3.44E-09 m/s	Constrained Mod.: 9.33 ±2.12 MPa
Sleeve friction: 63.49 ±29.07 kPa	N60: 6.85 ±0.80 blows	Go: 51.27 ±8.46 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 70.38 ±7.91 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.67 ±0.08
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 3.09 ±0.35
	Unit weight: 17.71 ±0.56 kN/m³	

.:: Layer No: 12 ::.

Code: B3 **Start depth:** 10.60 (m), **End depth:** 11.40 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.84 ±0.29 MPa	Permeability: 1.76E-08 ±1.89E-08 m/s	Constrained Mod.: 22.22 ±5.12 MPa
Sleeve friction: 72.28 ±34.19 kPa	N60: 9.17 ±1.28 blows	Go: 61.02 ±11.96 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 117.32 ±20.36 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.07 ±0.19
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 4.96 ±0.86
	Unit weight: 17.99 ±0.64 kN/m³	

.:: Layer No: 13 ::.

Code: A6 **Start depth:** 11.40 (m), **End depth:** 12.36 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.17 ±0.19 MPa	Permeability: 4.27E-09 ±4.87E-09 m/s	Constrained Mod.: 8.13 ±3.22 MPa
Sleeve friction: 47.19 ±25.21 kPa	N60: 6.73 ±0.67 blows	Go: 47.70 ±7.46 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 68.23 ±13.68 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.59 ±0.11
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.71 ±0.53
	Unit weight: 17.33 ±0.56 kN/m³	

.:: Layer No: 14 ::.

Code: D3 **Start depth:** 12.36 (m), **End depth:** 14.08 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.35 ±0.11 MPa	Permeability: 1.85E-09 ±1.02E-09 m/s	Constrained Mod.: 9.94 ±2.16 MPa
Sleeve friction: 66.21 ±19.75 kPa	N60: 8.05 ±0.65 blows	Go: 58.56 ±5.95 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 79.66 ±8.12 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.63 ±0.08
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.91 ±0.36
	Unit weight: 17.88 ±0.35 kN/m³	

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Project:
Location:

CPT: CPTu-04
Total depth: 14.08 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Summary table of mean values

From depth To depth (m)	Thickness (m)	Permeability (m/s)	SPT_{N60} (blows/30cm)	E_s (MPa)	D_r	Friction angle	Constrained modulus, M (MPa)	Shear modulus, G_O (MPa)	Undrained strength, S_U (kPa)	Undrained strength ratio	OCR	Unit weight (kN/m³)
0.00	1.46	2.98E-07	3.6	14.5	0.0	0.0	11.3	23.2	57.8	4.6	21.0	17.7
1.46		(±1.11E-06)	(±0.7)	(±1.8)	(±0.0)	(±0.0)	(±2.1)	(±5.4)	(±10.7)	(±2.8)	(±12.8)	(±0.3)
1.46	0.32	3.72E-08	5.9	0.0	0.0	0.0	18.7	39.8	95.2	3.0	13.8	18.3
1.78		(±1.10E-08)	(±0.3)	(±0.0)	(±0.0)	(±0.0)	(±1.3)	(±2.2)	(±6.9)	(±0.2)	(±1.0)	(±0.1)
1.78	0.30	8.65E-09	4.2	0.0	0.0	0.0	10.9	31.4	55.4	1.7	7.7	17.7
2.08		(±6.45E-09)	(±0.4)	(±0.0)	(±0.0)	(±0.0)	(±1.4)	(±5.0)	(±7.2)	(±0.3)	(±1.2)	(±0.5)
2.08	1.00	3.90E-08	6.5	29.1	0.0	0.0	19.9	43.2	101.6	2.5	11.4	18.2
3.08		(±2.70E-08)	(±0.8)	(±29.1)	(±0.0)	(±0.0)	(±2.0)	(±5.7)	(±10.2)	(±0.2)	(±1.0)	(±0.4)
3.08	2.42	1.24E-08	6.1	0.0	0.0	0.0	15.9	43.2	81.3	1.6	7.2	18.0
5.50		(±1.05E-08)	(±0.7)	(±0.0)	(±0.0)	(±0.0)	(±2.8)	(±4.5)	(±13.7)	(±0.3)	(±1.5)	(±0.3)
5.50	1.16	9.02E-09	7.5	0.0	0.0	0.0	19.4	54.2	98.9	1.5	6.8	18.4
6.66		(±4.54E-09)	(±0.6)	(±0.0)	(±0.0)	(±0.0)	(±1.5)	(±4.5)	(±7.4)	(±0.1)	(±0.6)	(±0.2)
6.66	0.46	3.86E-09	6.7	0.0	0.0	0.0	14.9	49.9	76.9	1.0	4.8	18.1
7.12		(±2.44E-09)	(±0.5)	(±0.0)	(±0.0)	(±0.0)	(±1.2)	(±4.5)	(±5.0)	(±0.1)	(±0.3)	(±0.3)
7.12	2.62	6.51E-09	9.4	0.0	0.0	0.0	23.1	68.1	117.8	1.3	6.2	18.7
9.74		(±3.72E-09)	(±1.1)	(±0.0)	(±0.0)	(±0.0)	(±2.9)	(±8.0)	(±14.7)	(±0.1)	(±0.5)	(±0.3)
9.74	0.32	3.69E-09	6.6	0.0	0.0	0.0	10.3	48.6	72.2	0.7	3.3	17.6
10.06		(±3.51E-09)	(±0.8)	(±0.0)	(±0.0)	(±0.0)	(±2.3)	(±7.8)	(±7.9)	(±0.1)	(±0.4)	(±0.5)
10.06	0.30	2.73E-08	8.9	0.0	0.0	0.0	22.4	57.1	118.4	1.2	5.3	17.9
10.36		(±2.49E-08)	(±1.1)	(±0.0)	(±0.0)	(±0.0)	(±6.0)	(±8.3)	(±25.6)	(±0.3)	(±1.2)	(±0.5)
10.36	0.24	2.95E-09	6.8	0.0	0.0	0.0	9.3	51.3	70.4	0.7	3.1	17.7
10.60		(±3.44E-09)	(±0.8)	(±0.0)	(±0.0)	(±0.0)	(±2.1)	(±8.5)	(±7.9)	(±0.1)	(±0.3)	(±0.6)

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CPT: CPTu-04
Total depth: 14.08 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:

Summary table of mean values

From depth To depth (m)	Thickness (m)	Permeability (m/s)	SPT_{N60} (blows/30cm)	E_s (MPa)	D_r	Friction angle	Constrained modulus, M (MPa)	Shear modulus, G_O (MPa)	Undrained strength, S_U (kPa)	Undrained strength ratio	OCR	Unit weight (kN/m³)
10.60	0.80	1.76E-08	9.2	0.0	0.0	0.0	22.2	61.0	117.3	1.1	5.0	18.0
11.40		(±1.89E-08)	(±1.3)	(±0.0)	(±0.0)	(±0.0)	(±5.1)	(±12.0)	(±20.4)	(±0.2)	(±0.9)	(±0.6)
11.40	0.96	4.27E-09	6.7	0.0	0.0	0.0	8.1	47.7	68.2	0.6	2.7	17.3
12.36		(±4.87E-09)	(±0.7)	(±0.0)	(±0.0)	(±0.0)	(±3.2)	(±7.5)	(±13.7)	(±0.1)	(±0.5)	(±0.6)
12.36	1.72	1.85E-09	8.0	0.0	0.0	0.0	9.9	58.6	79.7	0.6	2.9	17.9
14.08		(±1.02E-09)	(±0.6)	(±0.0)	(±0.0)	(±0.0)	(±2.2)	(±5.9)	(±8.1)	(±0.1)	(±0.4)	(±0.3)

Depth values presented in this table are measured from free ground surface

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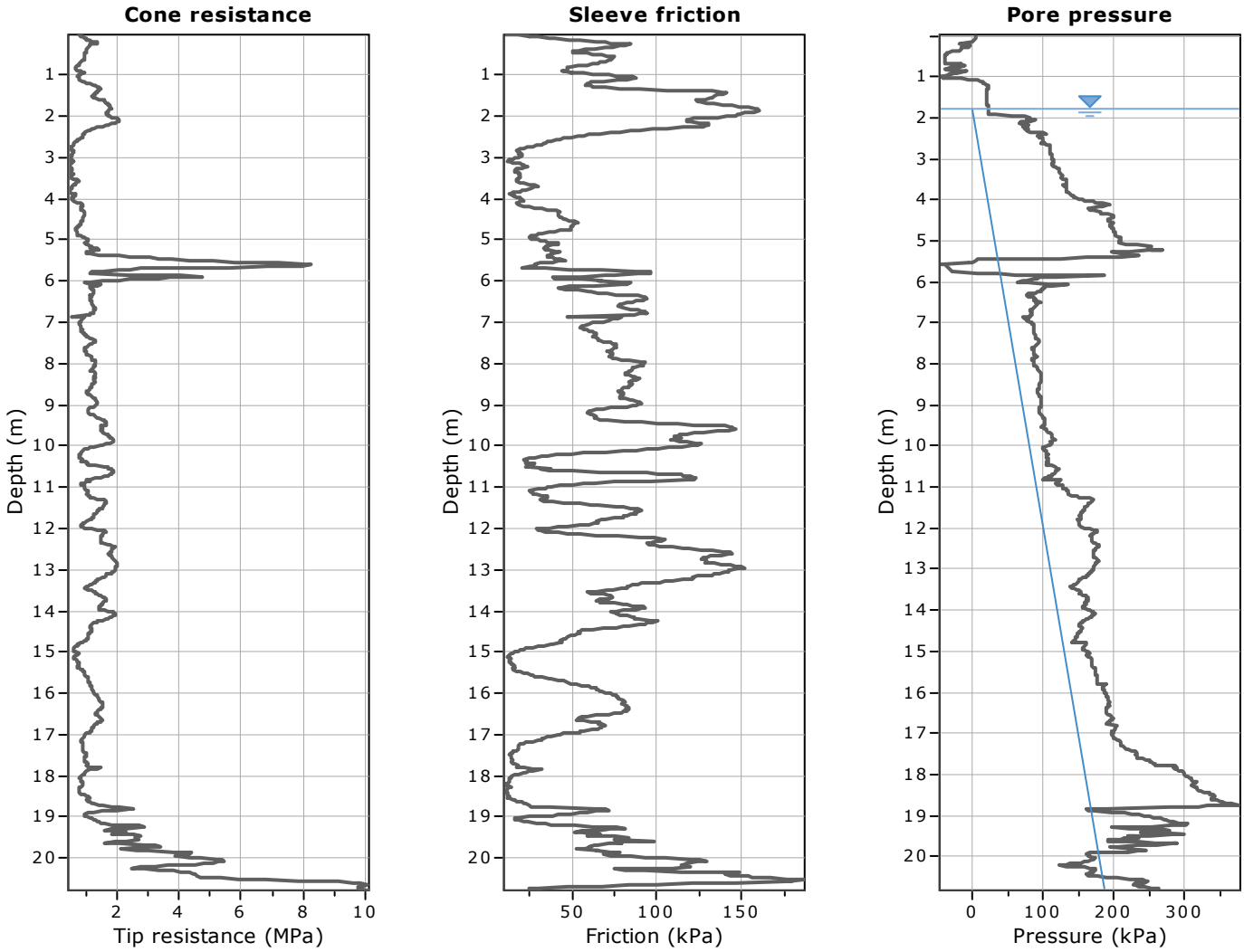
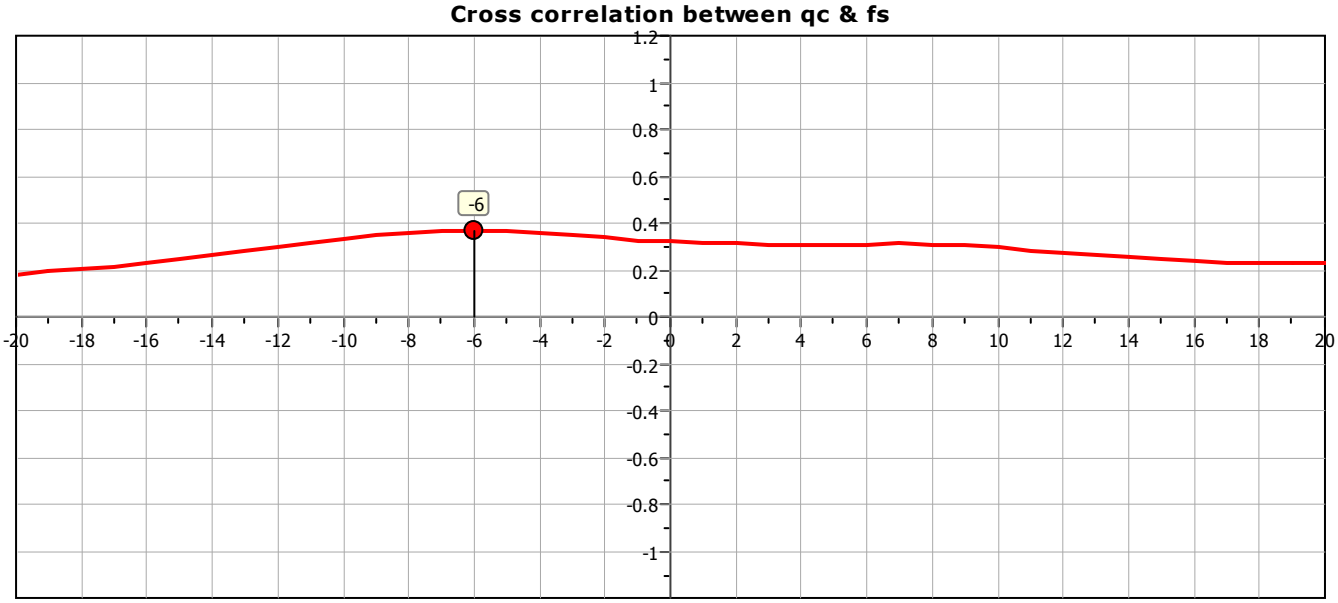
CPT: CPTu-05
Total depth: 20.78 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:



The plot below presents the cross correlation coeficient between the raw qc and fs values (as measured on the field). X axes presents the lag distance (one lag is the distance between two sucessive CPT measurements).



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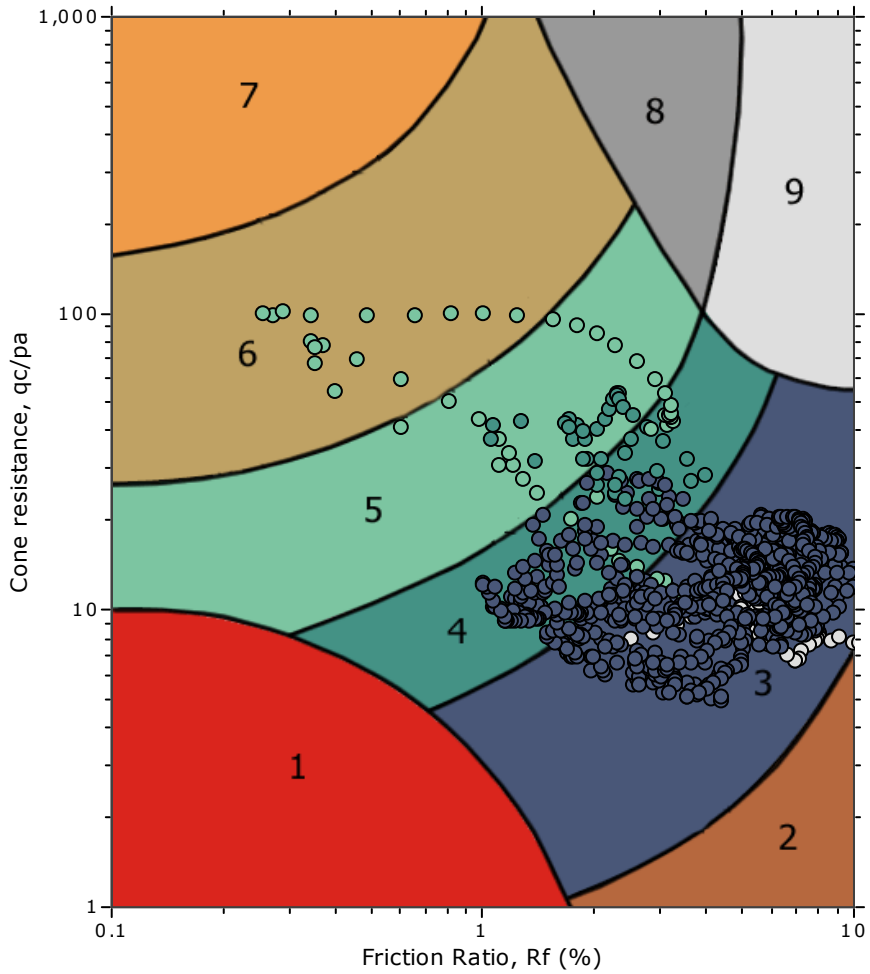
Project:
Location:

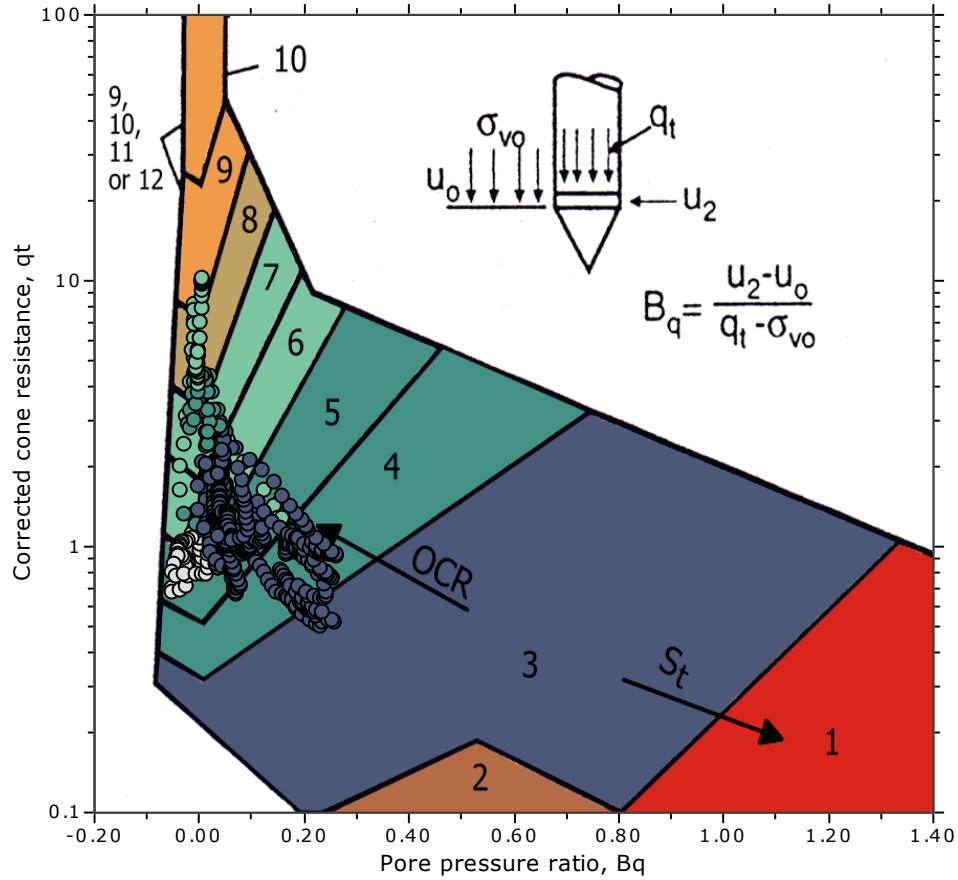
CPT: CPTu-05
Total depth: 20.78 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

SBT - Bq plots

SBT plot



Bq plot



SBT legend

- 1. Sensitive fine grained
- 2. Organic material
- 3. Clay to silty clay
- 4. Clayey silt to silty clay
- 5. Silty sand to sandy silt
- 6. Clean sand to silty sand
- 7. Gravely sand to sand
- 8. Very stiff sand to clayey sand
- 9. Very stiff fine grained

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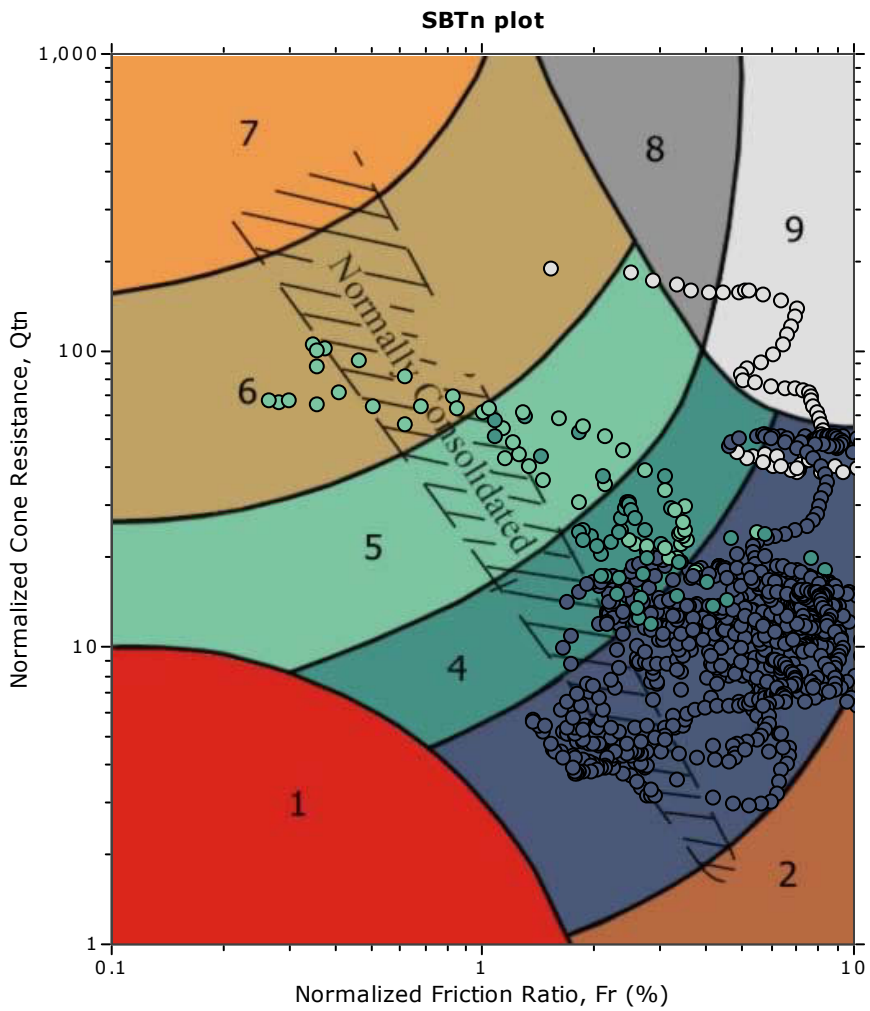
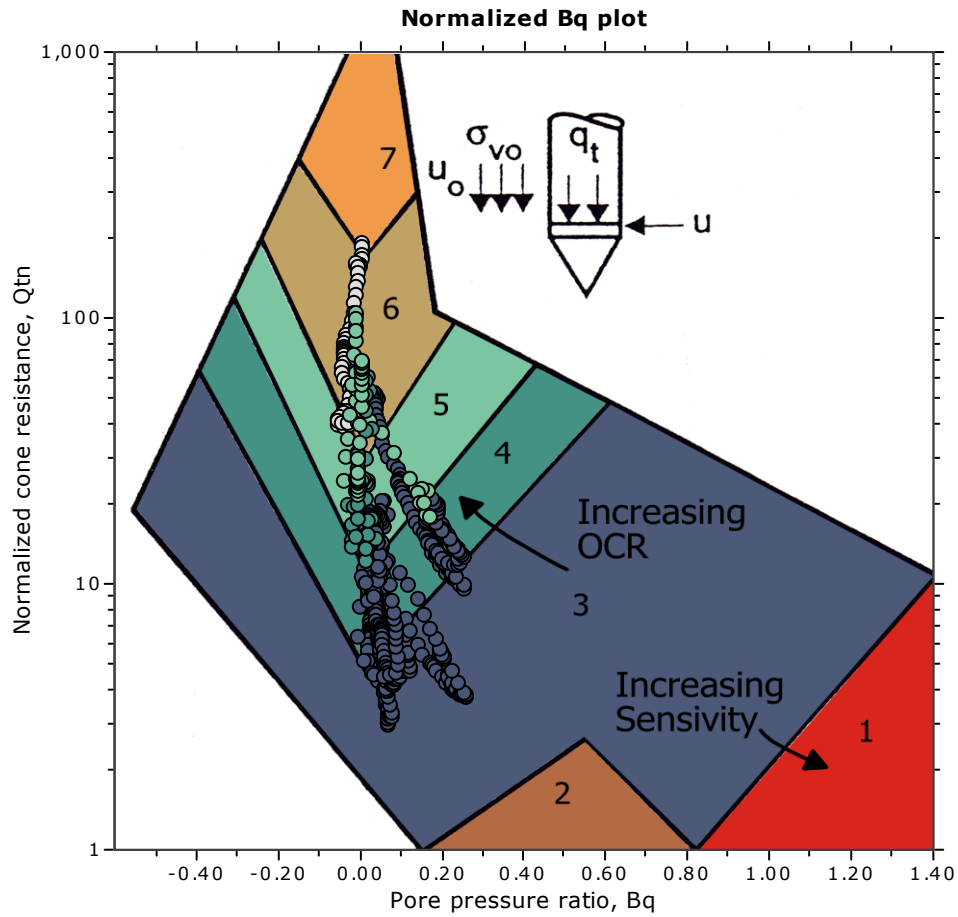
Project:
Location:

CPT: CPTu-05
Total depth: 20.78 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

SBT - Bq plots (normalized)





SBTn legend

- 1. Sensitive fine grained
- 2. Organic material
- 3. Clay to silty clay
- 4. Clayey silt to silty clay
- 5. Silty sand to sandy silt
- 6. Clean sand to silty sand
- 7. Gravely sand to sand
- 8. Very stiff sand to clayey sand
- 9. Very stiff fine grained

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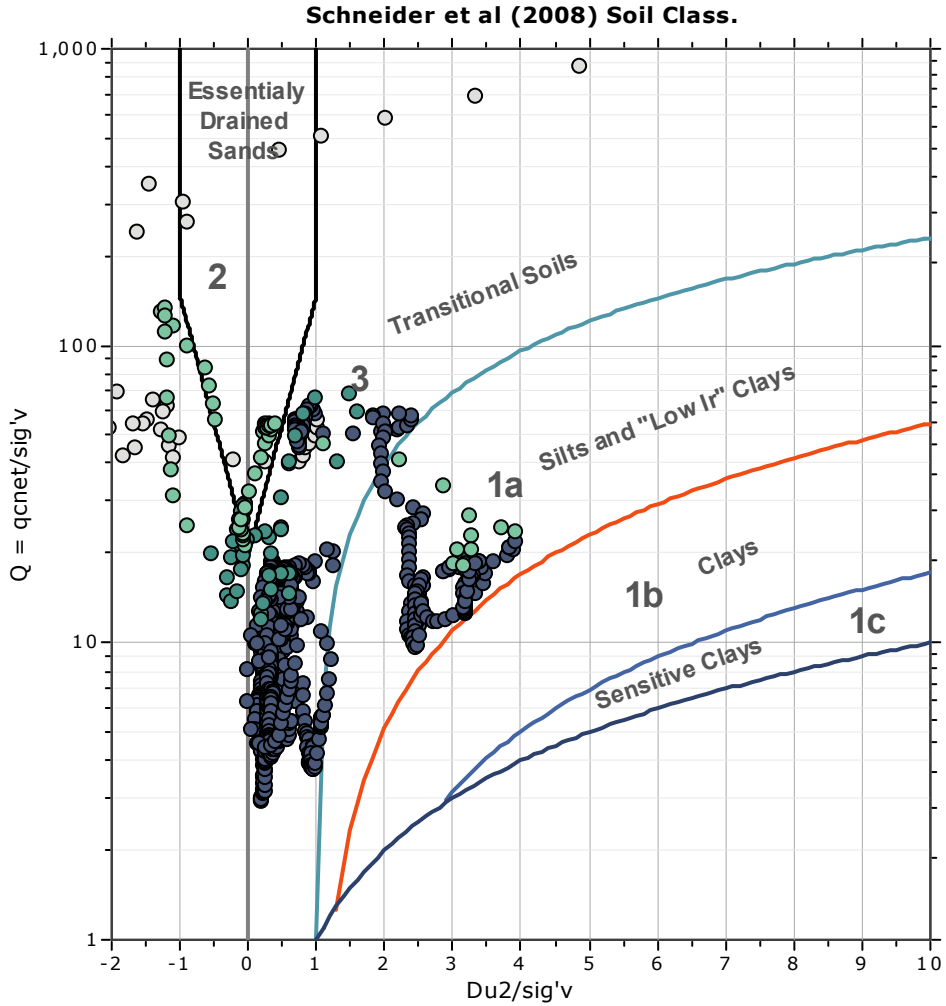
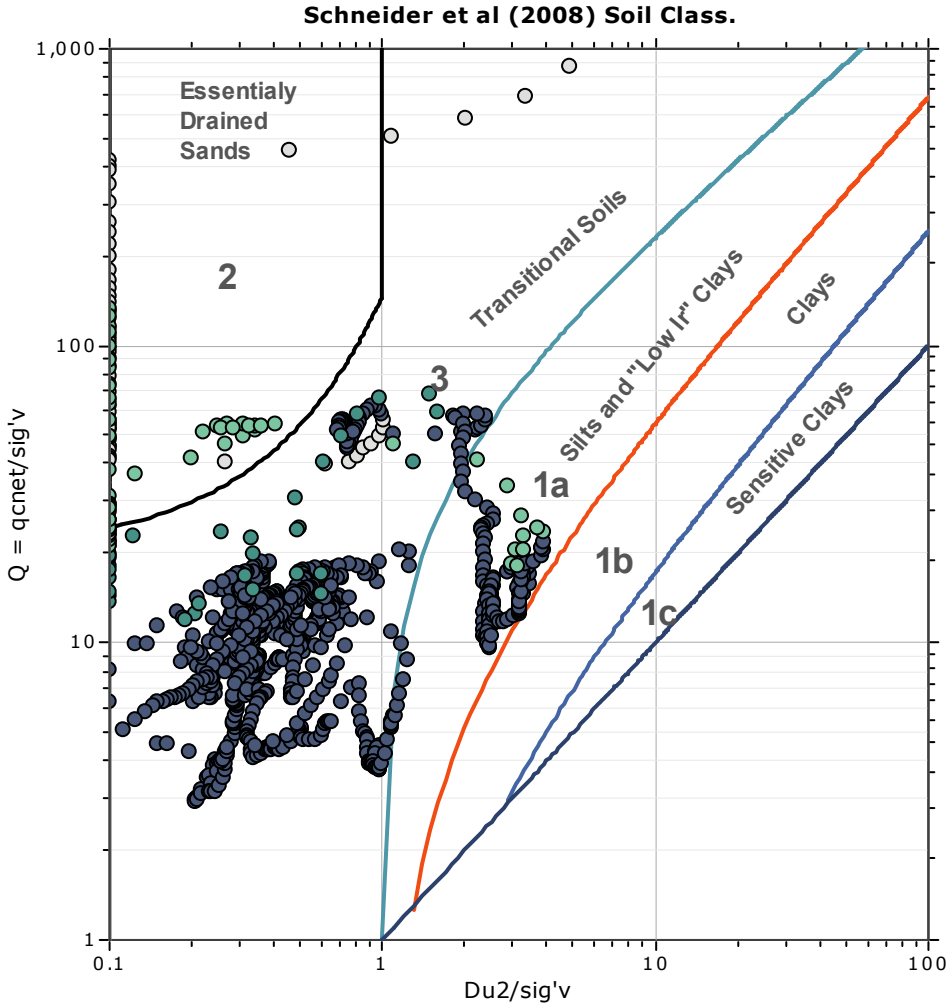
Project:
Location:

CPT: CPTu-05
Total depth: 20.78 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Bq plots (Schneider)





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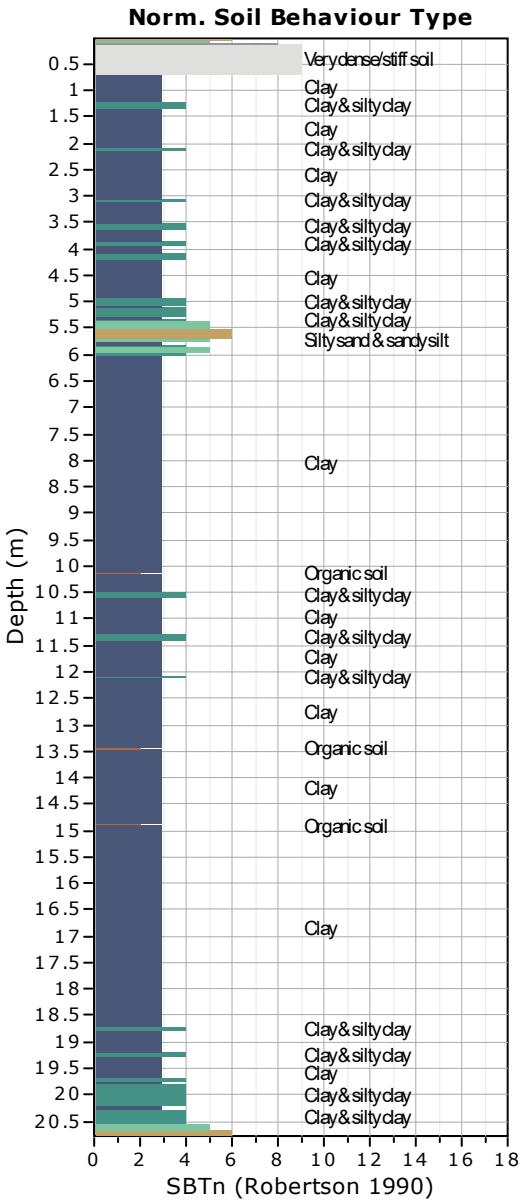
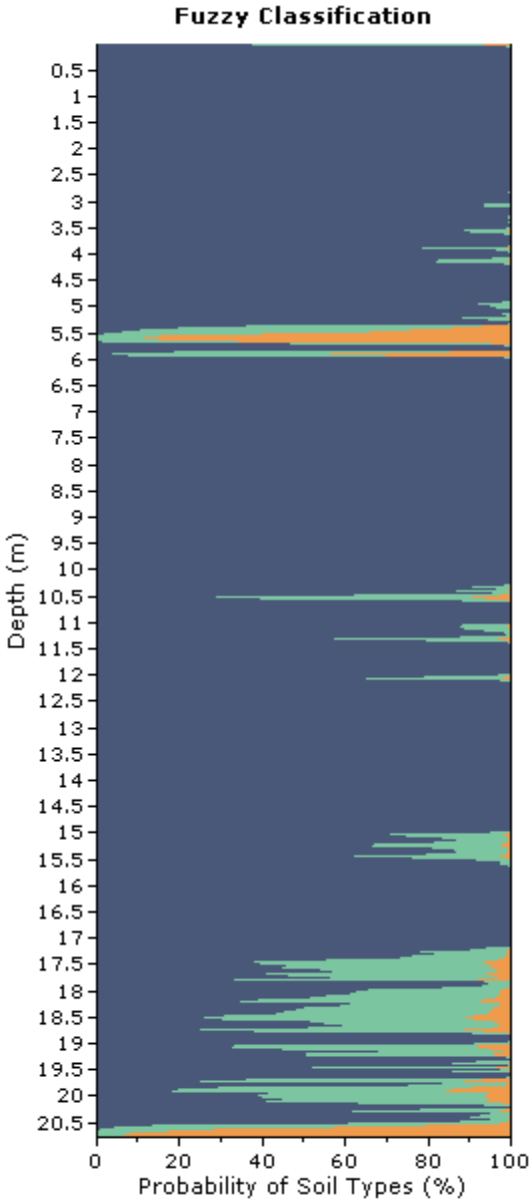
CPT: CPTu-05
Total depth: 20.78 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:





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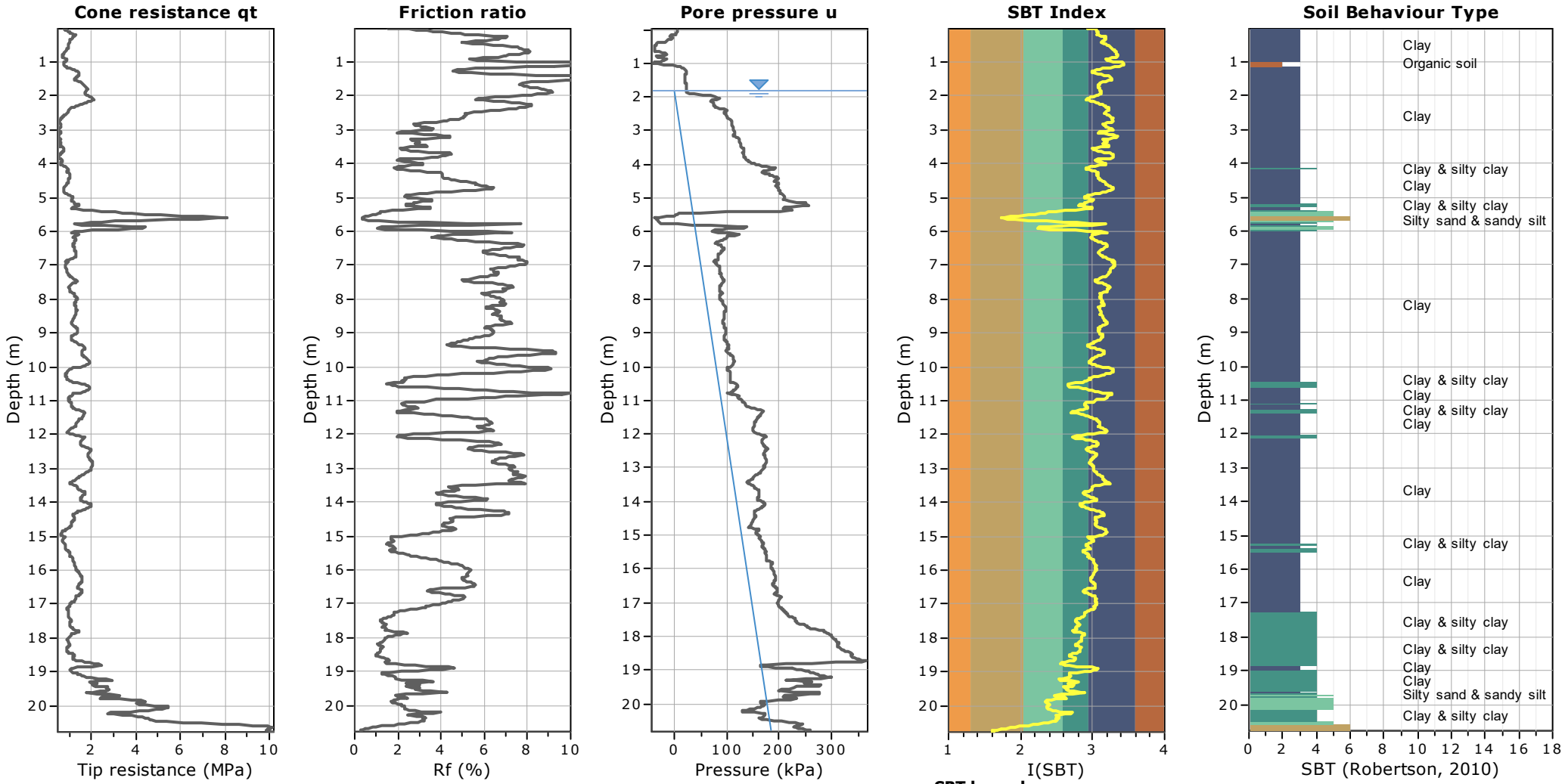
Project:
Location:

CPT: CPTu-05
Total depth: 20.78 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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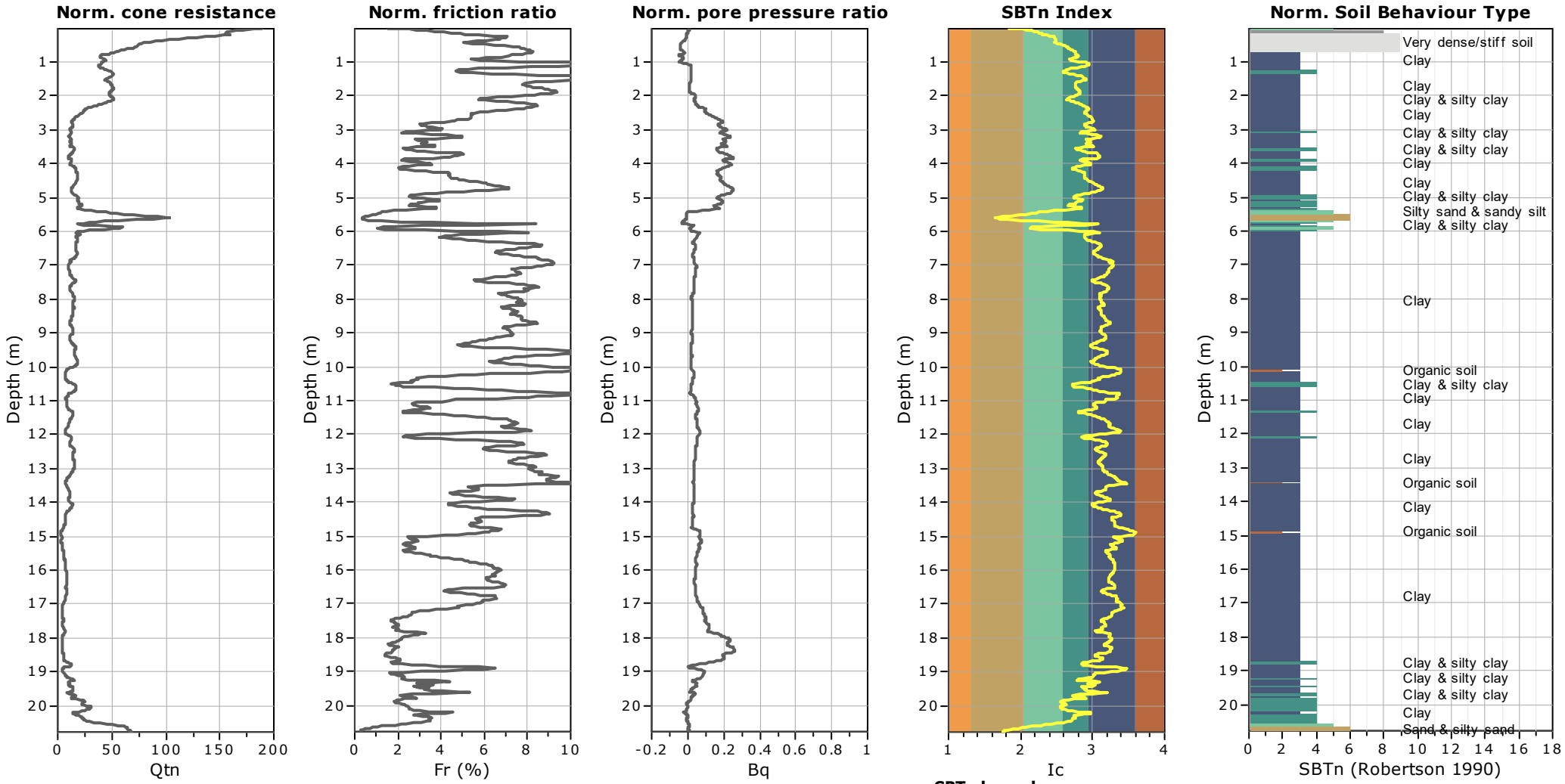
Project:
Location:

CPT: CPTu-05
Total depth: 20.78 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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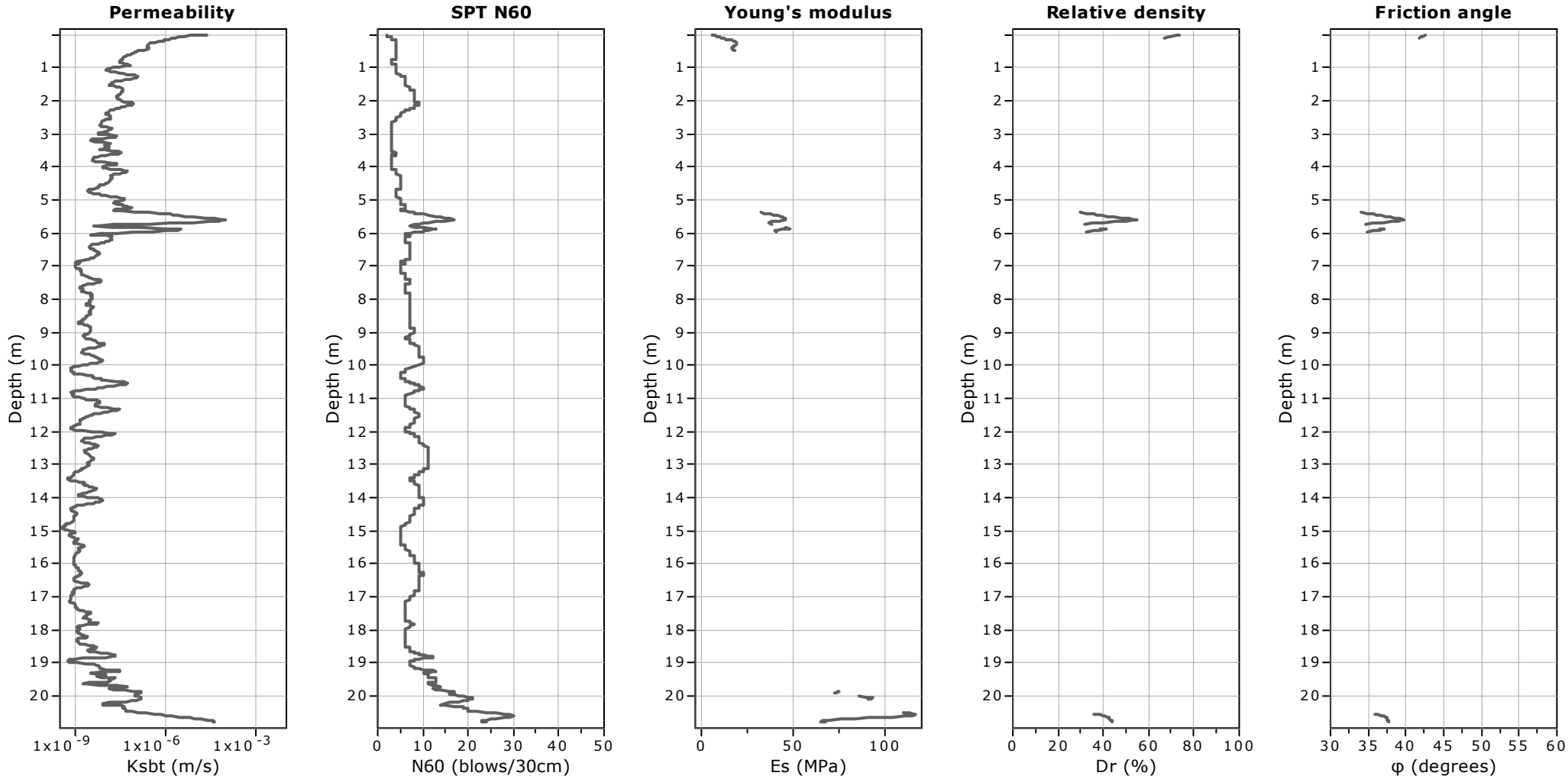
Project:
Location:

CPT: CPTu-05
Total depth: 20.78 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Permeability: Based on SBT_n
SPT N_{60}: Based on I_c and q_t
Young's modulus: Based on variable alpha using I_c (Robertson, 2009)
Relative desnisty constant, C_{Dr}: 350.0
Phi: Based on Kulhawy & Mayne (1990)
User defined estimation data

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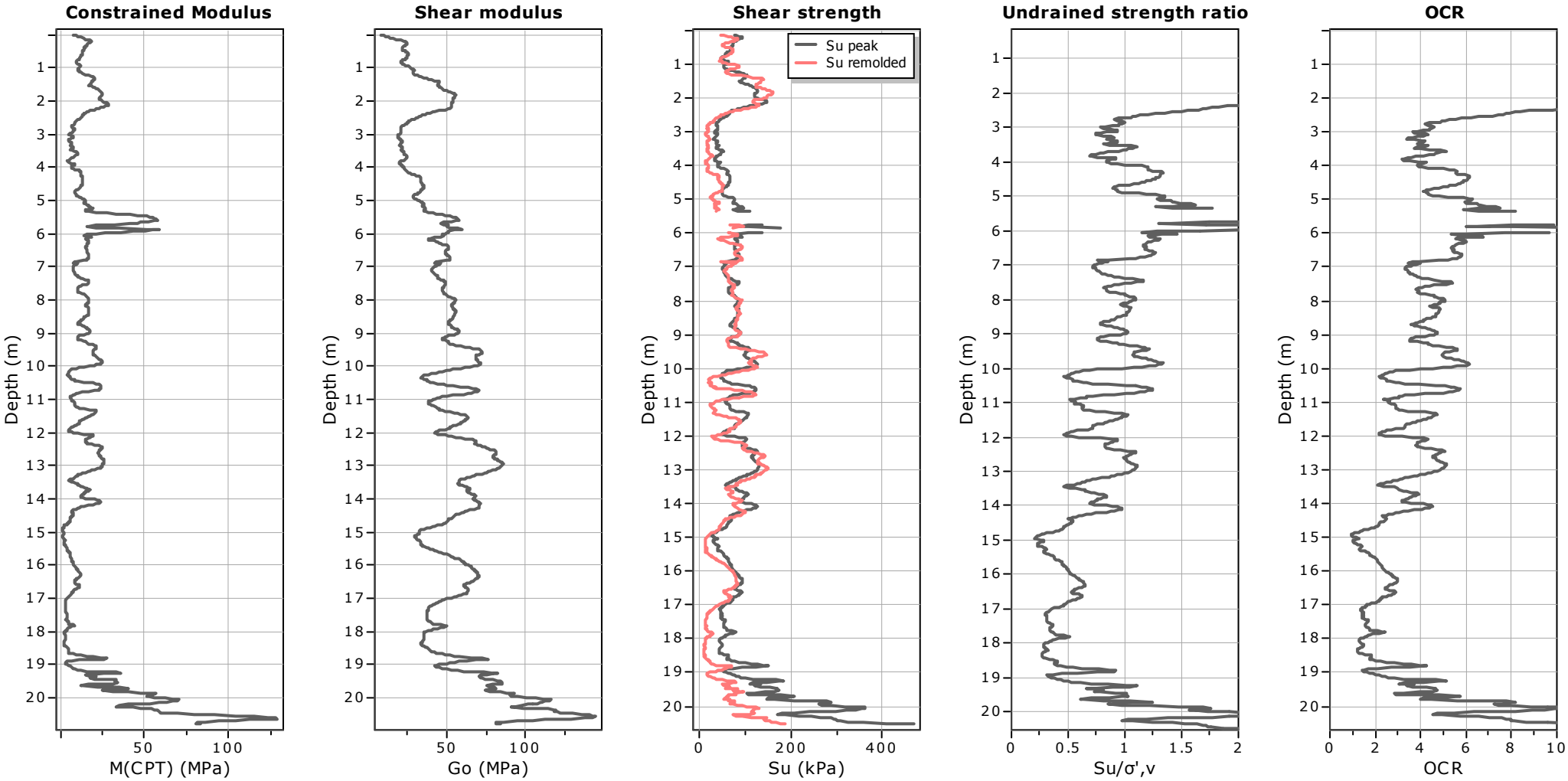
Project:
Location:

CPT: CPTu-05
Total depth: 20.78 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Constrained modulus: Based on variable *alpha* using I_c and Q_{tn} (Robertson, 2009)
Go: Based on variable *alpha* using I_c (Robertson, 2009)
Undrained shear strength cone factor for clays, N_{kt}: 14

OCR factor for clays, N_{kt}: 0.33
User defined estimation data

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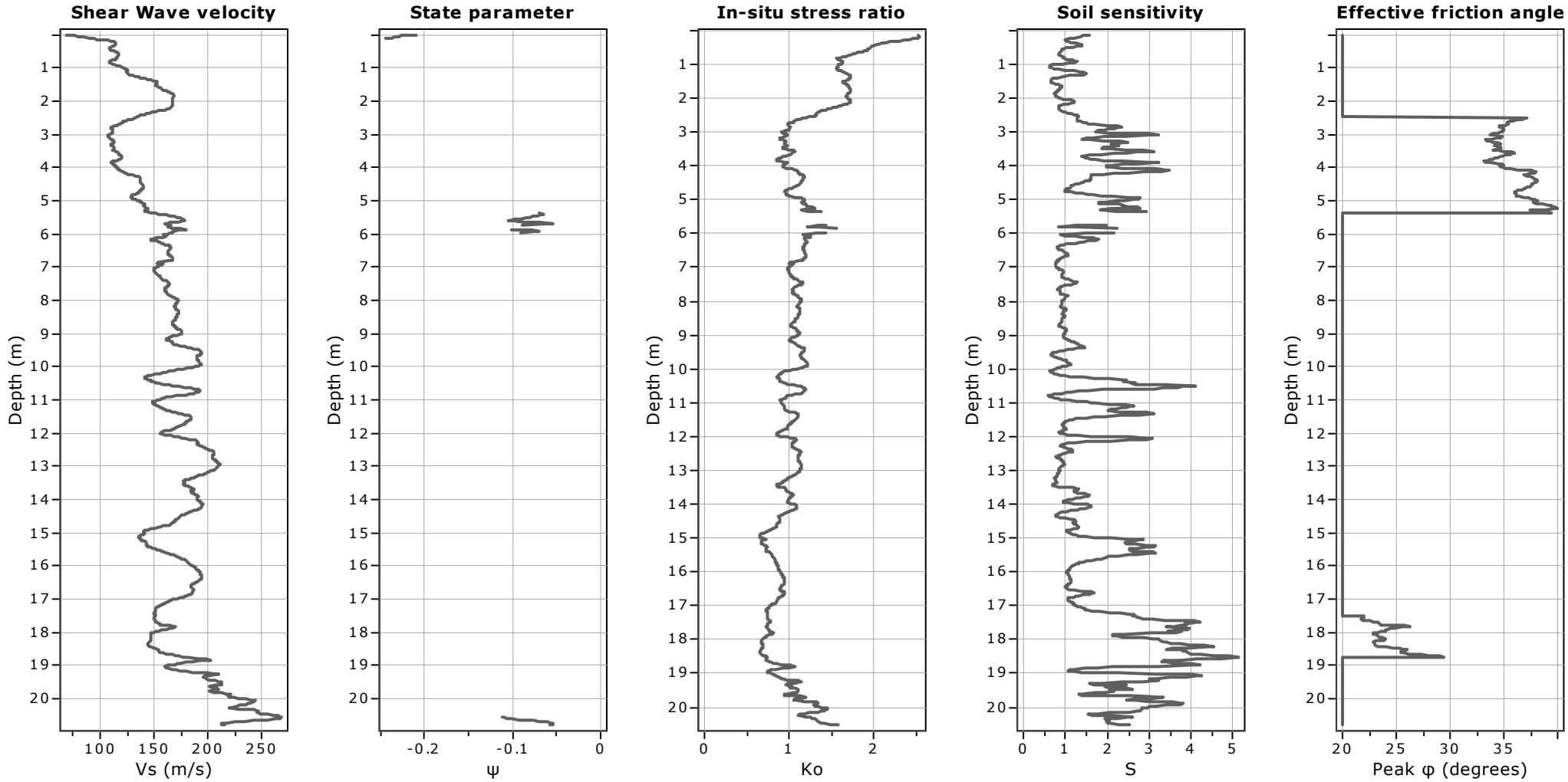
Project:
Location:

CPT: CPTu-05
Total depth: 20.78 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Soil Sensitivity factor, N_S: 7.00

User defined estimation data

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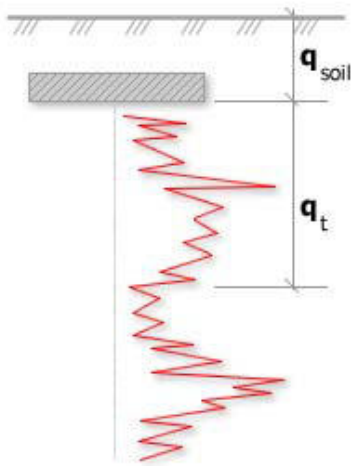
CPT: CPTu-05
Total depth: 20.78 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

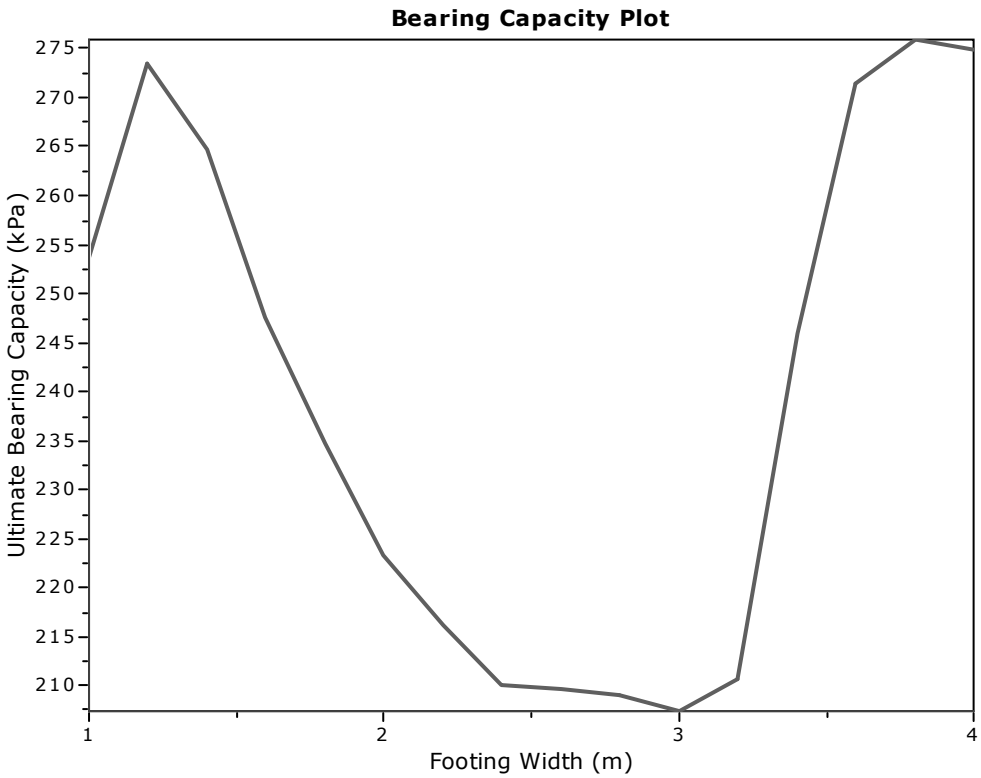
Project:
Location:



Bearing Capacity calculation is perfromed based on the formula:

$$Q_{ult} = R_k \times q_t + q_{soil}$$

where:
R_k: Bearing capacity factor
q_t: Average corrected cone resistance over calculation depth
q_{soil}: Pressure applied by soil above footing



:: Tabular results ::

No	B (m)	Start Depth (m)	End Depth (m)	Ave. q_t (MPa)	R_k	Soil Press. (kPa)	Ult. bearing cap. (kPa)
1	1.00	0.50	2.00	1.22	0.20	9.50	253.59
2	1.20	0.50	2.30	1.32	0.20	9.50	273.51
3	1.40	0.50	2.60	1.28	0.20	9.50	264.60
4	1.60	0.50	2.90	1.19	0.20	9.50	247.55
5	1.80	0.50	3.20	1.13	0.20	9.50	234.69
6	2.00	0.50	3.50	1.07	0.20	9.50	223.31
7	2.20	0.50	3.80	1.03	0.20	9.50	216.24
8	2.40	0.50	4.10	1.00	0.20	9.50	210.05
9	2.60	0.50	4.40	1.00	0.20	9.50	209.68
10	2.80	0.50	4.70	1.00	0.20	9.50	208.96
11	3.00	0.50	5.00	0.99	0.20	9.50	207.40
12	3.20	0.50	5.30	1.01	0.20	9.50	210.62
13	3.40	0.50	5.60	1.18	0.20	9.50	245.88
14	3.60	0.50	5.90	1.31	0.20	9.50	271.50
15	3.80	0.50	6.20	1.33	0.20	9.50	275.90
16	4.00	0.50	6.50	1.33	0.20	9.50	274.96

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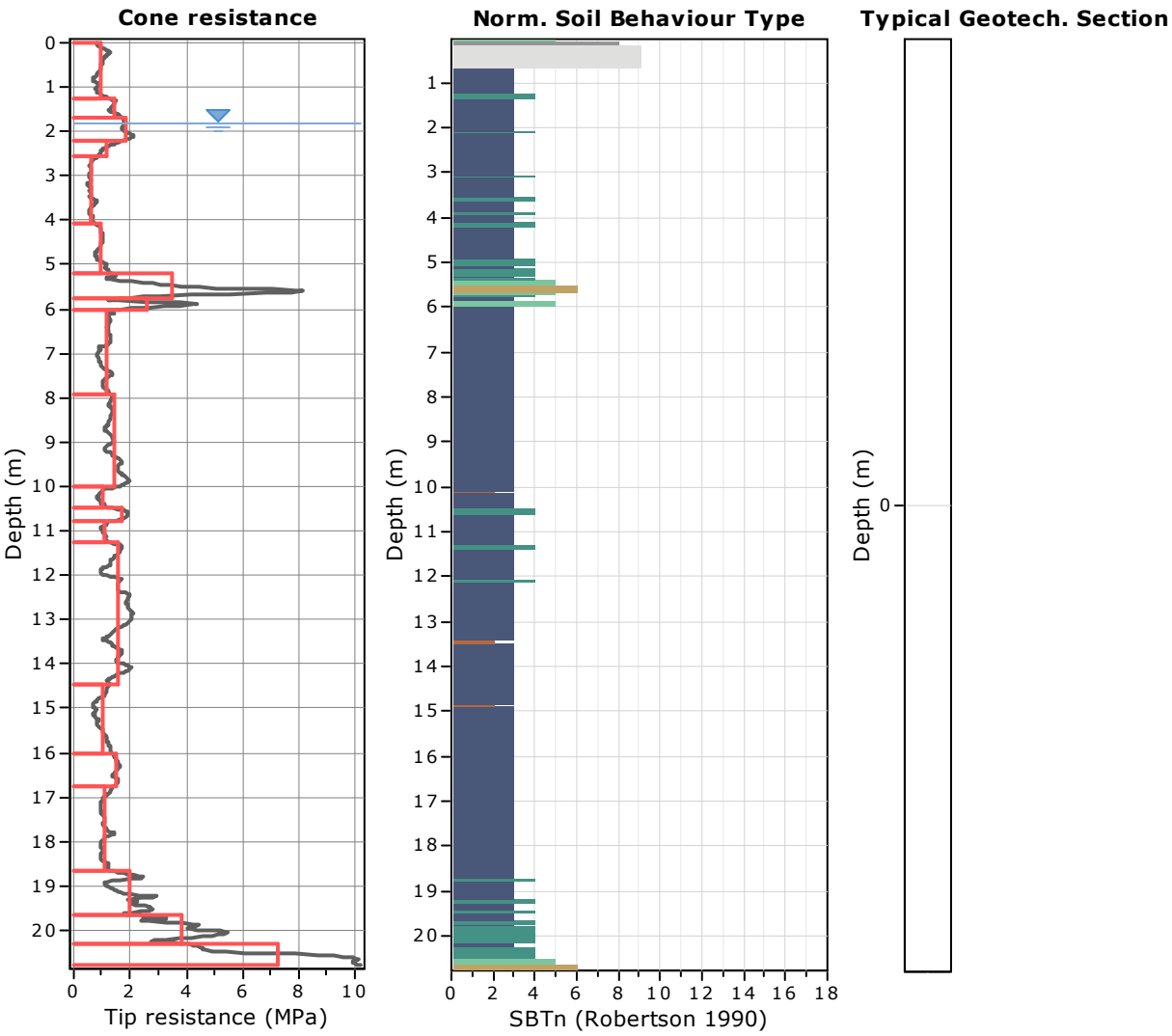
Project:
Location:

CPT: CPTu-05
Total depth: 20.78 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Tabular results

.:: Layer No: 1 ::.

Code: A **Start depth:** 0.00 (m), **End depth:** 1.24 (m)

Description: Very dense/stiff soil

Basic results	**Estimation results**	
Total cone resistance: 0.95 ±0.16 MPa	Permeability: 7.72E-07 ±2.93E-06 m/s	Constrained Mod.: 12.97 ±2.45 MPa
Sleeve friction: 60.90 ±16.47 kPa	N60: 3.77 ±0.61 blows	Go: 22.92 ±4.76 MPa
SBT_n: 9	Es: 17.54 ±1.44 MPa	Su: 67.07 ±12.18 kPa
SBTn description: Very dense/stiff soil	Dr (%): 0.00 ±0.00	Su ratio: 5.07 ±2.73
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 23.43 ±12.62
	Unit weight: 17.63 ±0.42 kN/m³	

.:: Layer No: 2 ::.

Code: D **Start depth:** 1.24 (m), **End depth:** 1.70 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.43 ±0.14 MPa	Permeability: 4.28E-08 ±3.30E-08 m/s	Constrained Mod.: 19.66 ±1.93 MPa
Sleeve friction: 114.75 ±28.06 kPa	N60: 6.25 ±0.68 blows	Go: 42.53 ±5.44 MPa
SBT_n: 3	Es: 26.53 ±26.53 MPa	Su: 100.30 ±9.84 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 3.44 ±0.18
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 15.91 ±0.81
	Unit weight: 18.54 ±0.34 kN/m³	

.:: Layer No: 3 ::.

Code: B **Start depth:** 1.70 (m), **End depth:** 2.20 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.85 ±0.13 MPa	Permeability: 4.08E-08 ±1.91E-08 m/s	Constrained Mod.: 25.45 ±1.78 MPa
Sleeve friction: 140.94 ±15.10 kPa	N60: 8.19 ±0.40 blows	Go: 53.58 ±1.23 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 129.85 ±9.09 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 3.53 ±0.13
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 16.33 ±0.61
	Unit weight: 18.91 ±0.10 kN/m³	

.:: Layer No: 4 ::.

Code: A2 **Start depth:** 2.20 (m), **End depth:** 2.56 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.17 ±0.29 MPa	Permeability: 1.55E-08 ±6.10E-09 m/s	Constrained Mod.: 15.83 ±4.13 MPa
Sleeve friction: 82.96 ±31.72 kPa	N60: 5.58 ±1.30 blows	Go: 39.14 ±8.03 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 80.76 ±21.05 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 2.10 ±0.56
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 9.69 ±2.59
	Unit weight: 18.04 ±0.54 kN/m³	

.:: Layer No: 5 ::.

Code: E **Start depth:** 2.56 (m), **End depth:** 4.08 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 0.63 ±0.08 MPa	Permeability: 1.10E-08 ±6.55E-09 m/s	Constrained Mod.: 7.21 ±1.58 MPa
Sleeve friction: 20.74 ±6.31 kPa	N60: 3.12 ±0.32 blows	Go: 21.51 ±2.07 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 40.66 ±5.48 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.92 ±0.14
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 4.25 ±0.63
	Unit weight: 16.25 ±0.31 kN/m³	

.:: Layer No: 6 ::.

Code: A3 **Start depth:** 4.08 (m), **End depth:** 5.20 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 0.98 ±0.14 MPa	Permeability: 1.90E-08 ±1.40E-08 m/s	Constrained Mod.: 12.44 ±2.18 MPa
Sleeve friction: 37.09 ±10.43 kPa	N60: 4.70 ±0.60 blows	Go: 31.56 ±3.36 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 64.11 ±10.18 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.19 ±0.16
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 5.49 ±0.73
	Unit weight: 17.08 ±0.36 kN/m³	

.:: Layer No: 7 ::.

Code: F **Start depth:** 5.20 (m), **End depth:** 5.76 (m)

Description: Silty sand & sandy silt

Basic results	**Estimation results**	
Total cone resistance: 3.50 ±2.30 MPa	Permeability: 1.44E-05 ±2.68E-05 m/s	Constrained Mod.: 36.59 ±16.22 MPa
Sleeve friction: 38.08 ±13.03 kPa	N60: 10.10 ±3.98 blows	Go: 46.06 ±8.15 MPa
SBT_n: 5	Es: 40.36 ±4.44 MPa	Su: 0.00 ±0.00 kPa
SBTn description: Silty sand & sandy silt	Dr (%): 42.07 ±8.27	Su ratio: 0.00 ±0.00
	ö (degrees): 37.14 ±1.90 °	O.C.R.: 0.00 ±0.00
	Unit weight: 17.53 ±0.30 kN/m³	

.:: Layer No: 8 ::.

Code: C **Start depth:** 5.76 (m), **End depth:** 6.00 (m)

Description: Clay & silty clay

Basic results	**Estimation results**	
Total cone resistance: 2.62 ±1.15 MPa	Permeability: 8.22E-07 ±1.13E-06 m/s	Constrained Mod.: 34.92 ±15.63 MPa
Sleeve friction: 67.49 ±20.69 kPa	N60: 9.46 ±2.11 blows	Go: 52.72 ±3.82 MPa
SBT_n: 4	Es: 45.52 ±45.52 MPa	Su: 115.08 ±33.58 kPa
SBTn description: Clay & silty clay	Dr (%): 0.00 ±0.00	Su ratio: 1.80 ±0.47
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 8.33 ±2.15
	Unit weight: 18.12 ±0.21 kN/m³	

.:: Layer No: 9 ::.

Code: A4 **Start depth:** 6.00 (m), **End depth:** 7.92 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.14 ±0.17 MPa	Permeability: 4.41E-09 ±4.13E-09 m/s	Constrained Mod.: 13.39 ±3.46 MPa
Sleeve friction: 72.10 ±12.48 kPa	N60: 6.30 ±0.72 blows	Go: 46.48 ±3.75 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 72.82 ±12.25 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.03 ±0.21
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 4.78 ±0.98
	Unit weight: 17.94 ±0.22 kN/m³	

.:: Layer No: 10 ::.

Code: D2 **Start depth:** 7.92 (m), **End depth:** 10.00 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.41 ±0.23 MPa	Permeability: 3.32E-09 ±1.67E-09 m/s	Constrained Mod.: 16.89 ±3.85 MPa
Sleeve friction: 92.24 ±22.23 kPa	N60: 7.75 ±1.12 blows	Go: 58.07 ±7.81 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 89.49 ±15.76 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.02 ±0.14
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 4.71 ±0.65
	Unit weight: 18.29 ±0.31 kN/m³	

.:: Layer No: 11 ::.

Code: A5 **Start depth:** 10.00 (m), **End depth:** 10.46 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.01 ±0.17 MPa	Permeability: 2.51E-09 ±2.48E-09 m/s	Constrained Mod.: 7.26 ±3.36 MPa
Sleeve friction: 53.83 ±34.43 kPa	N60: 6.04 ±1.12 blows	Go: 44.50 ±10.95 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 59.04 ±12.29 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.60 ±0.13
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.78 ±0.60
	Unit weight: 17.35 ±0.76 kN/m³	

.:: Layer No: 12 ::.

Code: D3 **Start depth:** 10.46 (m), **End depth:** 10.78 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.71 ±0.23 MPa	Permeability: 2.03E-08 ±1.87E-08 m/s	Constrained Mod.: 20.65 ±4.46 MPa
Sleeve friction: 70.01 ±40.42 kPa	N60: 8.41 ±1.33 blows	Go: 56.80 ±12.48 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 108.70 ±16.65 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.08 ±0.16
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 4.97 ±0.76
	Unit weight: 17.87 ±0.75 kN/m³	

.:: Layer No: 13 ::.

Code: A6 **Start depth:** 10.78 (m), **End depth:** 11.26 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.11 ±0.10 MPa	Permeability: 3.11E-09 ±2.27E-09 m/s	Constrained Mod.: 8.13 ±1.83 MPa
Sleeve friction: 51.55 ±32.85 kPa	N60: 6.40 ±0.71 blows	Go: 46.28 ±9.51 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 65.39 ±7.20 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.63 ±0.07
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.90 ±0.32
	Unit weight: 17.38 ±0.64 kN/m³	

.:: Layer No: 14 ::.

Code: D4 **Start depth:** 11.26 (m), **End depth:** 14.46 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.58 ±0.30 MPa	Permeability: 3.65E-09 ±4.54E-09 m/s	Constrained Mod.: 15.89 ±6.28 MPa
Sleeve friction: 89.43 ±31.40 kPa	N60: 8.99 ±1.40 blows	Go: 65.92 ±11.22 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 96.78 ±21.31 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.81 ±0.18
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 3.76 ±0.85
	Unit weight: 18.25 ±0.49 kN/m³	

.:: Layer No: 15 ::.

Code: A7 **Start depth:** 14.46 (m), **End depth:** 16.00 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.00 ±0.21 MPa	Permeability: 9.16E-10 ±3.23E-10 m/s	Constrained Mod.: 4.14 ±2.16 MPa
Sleeve friction: 34.67 ±18.75 kPa	N60: 6.32 ±1.21 blows	Go: 43.95 ±10.69 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 52.09 ±14.95 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.38 ±0.11
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 1.74 ±0.49
	Unit weight: 16.87 ±0.76 kN/m³	

.:: Layer No: 16 ::.

Code: D5 **Start depth:** 16.00 (m), **End depth:** 16.76 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.50 ±0.08 MPa	Permeability: 1.34E-09 ±5.23E-10 m/s	Constrained Mod.: 10.01 ±1.27 MPa
Sleeve friction: 73.04 ±9.60 kPa	N60: 9.10 ±0.31 blows	Go: 66.20 ±2.99 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 86.47 ±5.55 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.59 ±0.04
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.72 ±0.18
	Unit weight: 18.07 ±0.16 kN/m³	

.:: Layer No: 17 ::.

Code: A8 **Start depth:** 16.76 (m), **End depth:** 18.66 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.09 ±0.13 MPa	Permeability: 1.78E-09 ±1.18E-09 m/s	Constrained Mod.: 3.95 ±1.48 MPa
Sleeve friction: 23.12 ±16.07 kPa	N60: 6.55 ±0.81 blows	Go: 41.68 ±8.12 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 55.31 ±9.68 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.35 ±0.06
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 1.63 ±0.30
	Unit weight: 16.43 ±0.65 kN/m³	

.:: Layer No: 18 ::.

Code: B2 **Start depth:** 18.66 (m), **End depth:** 19.66 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.95 ±0.56 MPa	Permeability: 8.70E-09 ±7.22E-09 m/s	Constrained Mod.: 17.29 ±10.38 MPa
Sleeve friction: 51.43 ±22.76 kPa	N60: 10.10 ±2.12 blows	Go: 65.41 ±14.05 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 115.56 ±39.45 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.69 ±0.23
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 3.20 ±1.07
	Unit weight: 17.63 ±0.67 kN/m³	

.:: Layer No: 19 ::.

Code: C2 **Start depth:** 19.66 (m), **End depth:** 20.30 (m)

Description: Clay & silty clay

Basic results	**Estimation results**	
Total cone resistance: 3.84 ±0.95 MPa	Permeability: 7.12E-08 ±5.20E-08 m/s	Constrained Mod.: 48.37 ±13.94 MPa
Sleeve friction: 89.69 ±24.86 kPa	N60: 16.30 ±2.79 blows	Go: 95.49 ±13.08 MPa
SBT_n: 4	Es: 83.69 ±9.24 MPa	Su: 249.01 ±67.51 kPa
SBTn description: Clay & silty clay	Dr (%): 0.00 ±0.00	Su ratio: 1.47 ±0.42
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 6.81 ±1.95
	Unit weight: 18.63 ±0.38 kN/m³	

.:: Layer No: 20 ::.

Code: F2 **Start depth:** 20.30 (m), **End depth:** 20.78 (m)

Description: Silty sand & sandy silt

Basic results	**Estimation results**	
Total cone resistance: 7.22 ±2.54 MPa	Permeability: 5.87E-06 ±1.13E-05 m/s	Constrained Mod.: 85.15 ±27.24 MPa
Sleeve friction: 122.90 ±52.12 kPa	N60: 23.75 ±4.17 blows	Go: 118.65 ±19.43 MPa
SBT_n: 5	Es: 92.21 ±20.12 MPa	Su: 0.00 ±0.00 kPa
SBTn description: Silty sand & sandy silt	Dr (%): 41.52 ±2.39	Su ratio: 0.00 ±0.00
	ö (degrees): 37.17 ±0.57 °	O.C.R.: 0.00 ±0.00
	Unit weight: 19.10 ±0.64 kN/m³	

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Project:
Location:

CPT: CPTu-05
Total depth: 20.78 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Summary table of mean values

From depth To depth (m)	Thickness (m)	Permeability (m/s)	SPT_{N60} (blows/30cm)	E_s (MPa)	D_r	Friction angle	Constrained modulus, M (MPa)	Shear modulus, G_O (MPa)	Undrained strength, S_U (kPa)	Undrained strength ratio	OCR	Unit weight (kN/m³)
0.00	1.24	7.72E-07	3.8	17.5	0.0	0.0	13.0	22.9	67.1	5.1	23.4	17.6
1.24		(±2.93E-06)	(±0.6)	(±1.4)	(±0.0)	(±0.0)	(±2.4)	(±4.8)	(±12.2)	(±2.7)	(±12.6)	(±0.4)
1.24	0.46	4.28E-08	6.3	26.5	0.0	0.0	19.7	42.5	100.3	3.4	15.9	18.5
1.70		(±3.30E-08)	(±0.7)	(±26.5)	(±0.0)	(±0.0)	(±1.9)	(±5.4)	(±9.8)	(±0.2)	(±0.8)	(±0.3)
1.70	0.50	4.08E-08	8.2	0.0	0.0	0.0	25.5	53.6	129.8	3.5	16.3	18.9
2.20		(±1.91E-08)	(±0.4)	(±0.0)	(±0.0)	(±0.0)	(±1.8)	(±1.2)	(±9.1)	(±0.1)	(±0.6)	(±0.1)
2.20	0.36	1.55E-08	5.6	0.0	0.0	0.0	15.8	39.1	80.8	2.1	9.7	18.0
2.56		(±6.10E-09)	(±1.3)	(±0.0)	(±0.0)	(±0.0)	(±4.1)	(±8.0)	(±21.1)	(±0.6)	(±2.6)	(±0.5)
2.56	1.52	1.10E-08	3.1	0.0	0.0	0.0	7.2	21.5	40.7	0.9	4.3	16.3
4.08		(±6.55E-09)	(±0.3)	(±0.0)	(±0.0)	(±0.0)	(±1.6)	(±2.1)	(±5.5)	(±0.1)	(±0.6)	(±0.3)
4.08	1.12	1.90E-08	4.7	0.0	0.0	0.0	12.4	31.6	64.1	1.2	5.5	17.1
5.20		(±1.40E-08)	(±0.6)	(±0.0)	(±0.0)	(±0.0)	(±2.2)	(±3.4)	(±10.2)	(±0.2)	(±0.7)	(±0.4)
5.20	0.56	1.44E-05	10.1	40.4	42.1	37.1	36.6	46.1	0.0	0.0	0.0	17.5
5.76		(±2.68E-05)	(±4.0)	(±4.4)	(±8.3)	(±1.9)	(±16.2)	(±8.2)	(±0.0)	(±0.0)	(±0.0)	(±0.3)
5.76	0.24	8.22E-07	9.5	45.5	0.0	0.0	34.9	52.7	115.1	1.8	8.3	18.1
6.00		(±1.13E-06)	(±2.1)	(±45.5)	(±0.0)	(±0.0)	(±15.6)	(±3.8)	(±33.6)	(±0.5)	(±2.2)	(±0.2)
6.00	1.92	4.41E-09	6.3	0.0	0.0	0.0	13.4	46.5	72.8	1.0	4.8	17.9
7.92		(±4.13E-09)	(±0.7)	(±0.0)	(±0.0)	(±0.0)	(±3.5)	(±3.8)	(±12.2)	(±0.2)	(±1.0)	(±0.2)
7.92	2.08	3.32E-09	7.8	0.0	0.0	0.0	16.9	58.1	89.5	1.0	4.7	18.3
10.00		(±1.67E-09)	(±1.1)	(±0.0)	(±0.0)	(±0.0)	(±3.9)	(±7.8)	(±15.8)	(±0.1)	(±0.7)	(±0.3)
10.00	0.46	2.51E-09	6.0	0.0	0.0	0.0	7.3	44.5	59.0	0.6	2.8	17.3
10.46		(±2.48E-09)	(±1.1)	(±0.0)	(±0.0)	(±0.0)	(±3.4)	(±11.0)	(±12.3)	(±0.1)	(±0.6)	(±0.8)

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Project:
Location:

CPT: CPTu-05
Total depth: 20.78 m, Date: 23/01/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Summary table of mean values

From depth To depth (m)	Thickness (m)	Permeability (m/s)	SPT_{N60} (blows/30cm)	E_s (MPa)	D_r	Friction angle	Constrained modulus, M (MPa)	Shear modulus, G_O (MPa)	Undrained strength, S_U (kPa)	Undrained strength ratio	OCR	Unit weight (kN/m³)
10.46	0.32	2.03E-08	8.4	0.0	0.0	0.0	20.6	56.8	108.7	1.1	5.0	17.9
10.78		(±1.87E-08)	(±1.3)	(±0.0)	(±0.0)	(±0.0)	(±4.5)	(±12.5)	(±16.7)	(±0.2)	(±0.8)	(±0.8)
10.78	0.48	3.11E-09	6.4	0.0	0.0	0.0	8.1	46.3	65.4	0.6	2.9	17.4
11.26		(±2.27E-09)	(±0.7)	(±0.0)	(±0.0)	(±0.0)	(±1.8)	(±9.5)	(±7.2)	(±0.1)	(±0.3)	(±0.6)
11.26	3.20	3.65E-09	9.0	0.0	0.0	0.0	15.9	65.9	96.8	0.8	3.8	18.2
14.46		(±4.54E-09)	(±1.4)	(±0.0)	(±0.0)	(±0.0)	(±6.3)	(±11.2)	(±21.3)	(±0.2)	(±0.9)	(±0.5)
14.46	1.54	9.16E-10	6.3	0.0	0.0	0.0	4.1	43.9	52.1	0.4	1.7	16.9
16.00		(±3.23E-10)	(±1.2)	(±0.0)	(±0.0)	(±0.0)	(±2.2)	(±10.7)	(±14.9)	(±0.1)	(±0.5)	(±0.8)
16.00	0.76	1.34E-09	9.1	0.0	0.0	0.0	10.0	66.2	86.5	0.6	2.7	18.1
16.76		(±5.23E-10)	(±0.3)	(±0.0)	(±0.0)	(±0.0)	(±1.3)	(±3.0)	(±5.5)	(±0.0)	(±0.2)	(±0.2)
16.76	1.90	1.78E-09	6.6	0.0	0.0	0.0	4.0	41.7	55.3	0.4	1.6	16.4
18.66		(±1.18E-09)	(±0.8)	(±0.0)	(±0.0)	(±0.0)	(±1.5)	(±8.1)	(±9.7)	(±0.1)	(±0.3)	(±0.6)
18.66	1.00	8.70E-09	10.1	0.0	0.0	0.0	17.3	65.4	115.6	0.7	3.2	17.6
19.66		(±7.22E-09)	(±2.1)	(±0.0)	(±0.0)	(±0.0)	(±10.4)	(±14.0)	(±39.5)	(±0.2)	(±1.1)	(±0.7)
19.66	0.64	7.12E-08	16.3	83.7	0.0	0.0	48.4	95.5	249.0	1.5	6.8	18.6
20.30		(±5.20E-08)	(±2.8)	(±9.2)	(±0.0)	(±0.0)	(±13.9)	(±13.1)	(±67.5)	(±0.4)	(±1.9)	(±0.4)
20.30	0.48	5.87E-06	23.8	92.2	41.5	37.2	85.1	118.6	0.0	0.0	0.0	19.1
20.78		(±1.13E-05)	(±4.2)	(±20.1)	(±2.4)	(±0.6)	(±27.2)	(±19.4)	(±0.0)	(±0.0)	(±0.0)	(±0.6)

Depth values presented in this table are measured from free ground surface

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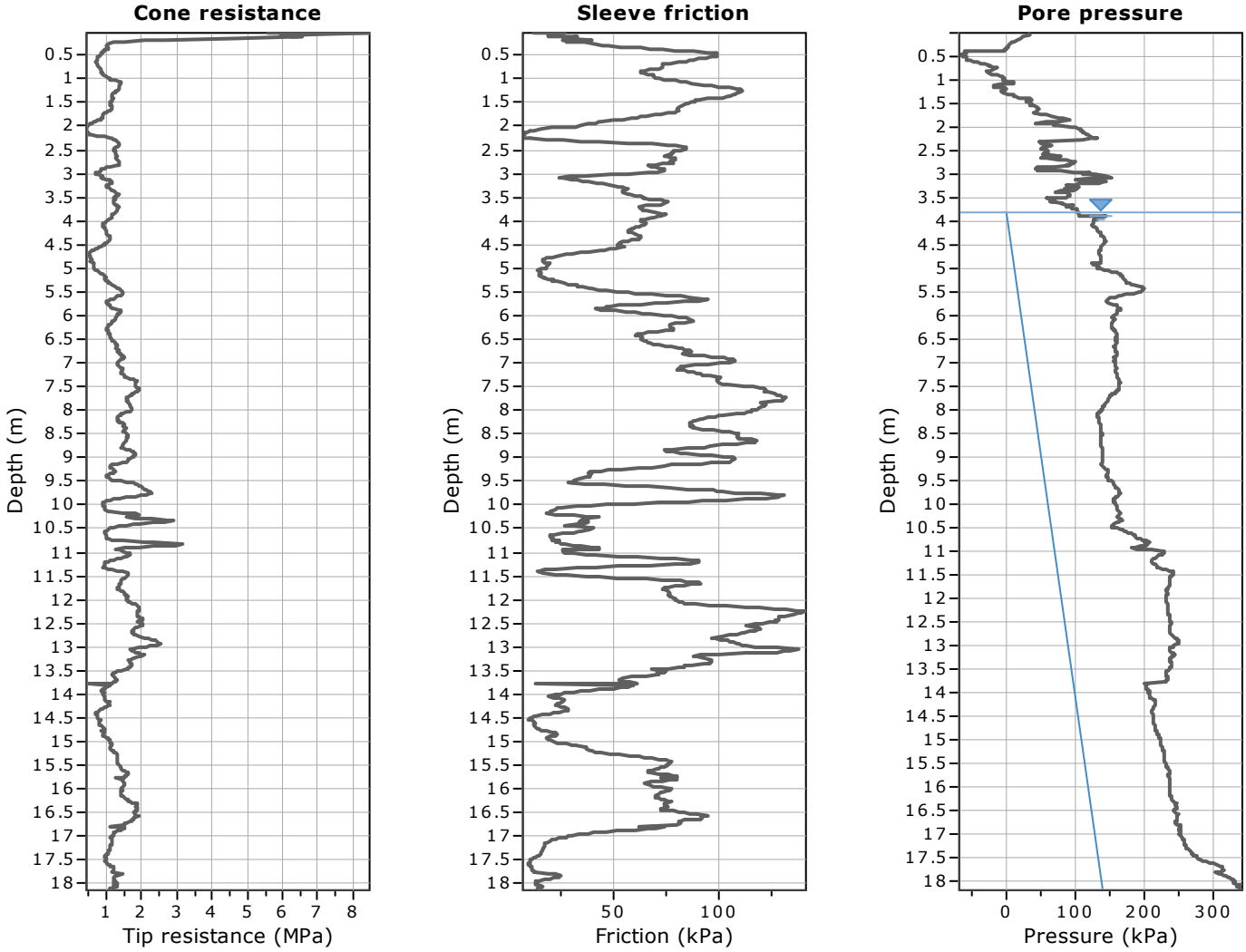
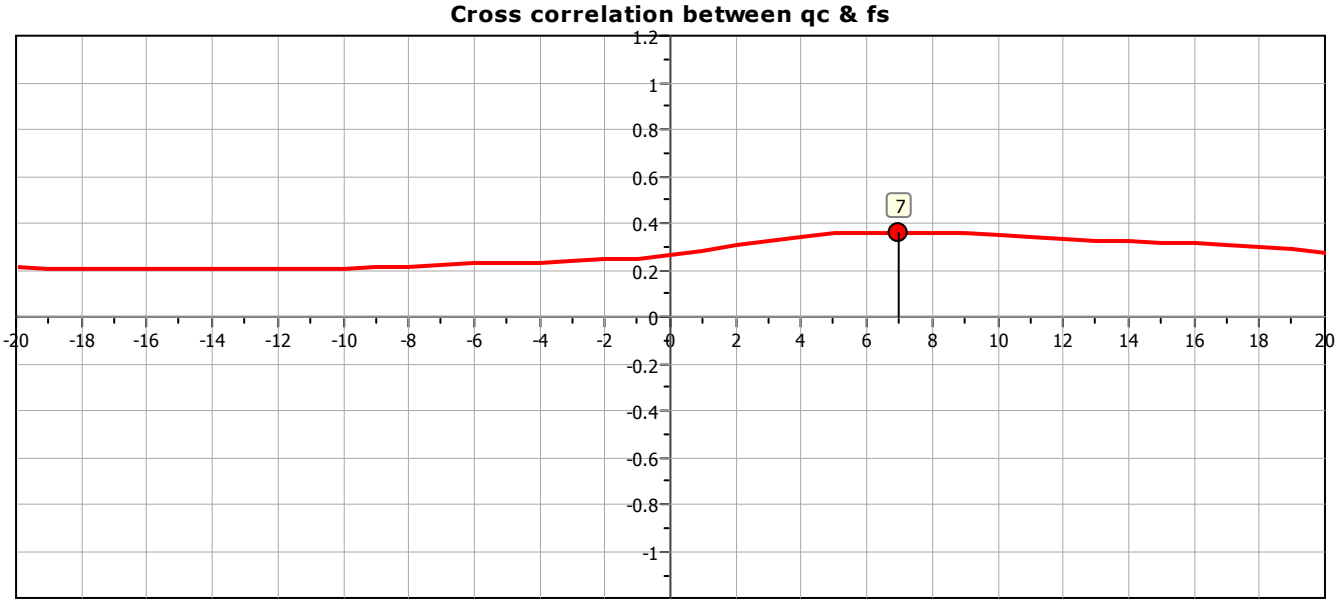
CPT: CPT-06
Total depth: 18.14 m, Date: 11/02/2024
Surface Elevation: 1.20 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:



The plot below presents the cross correlation coeficient between the raw qc and fs values (as measured on the field). X axes presents the lag distance (one lag is the distance between two sucessive CPT measurements).



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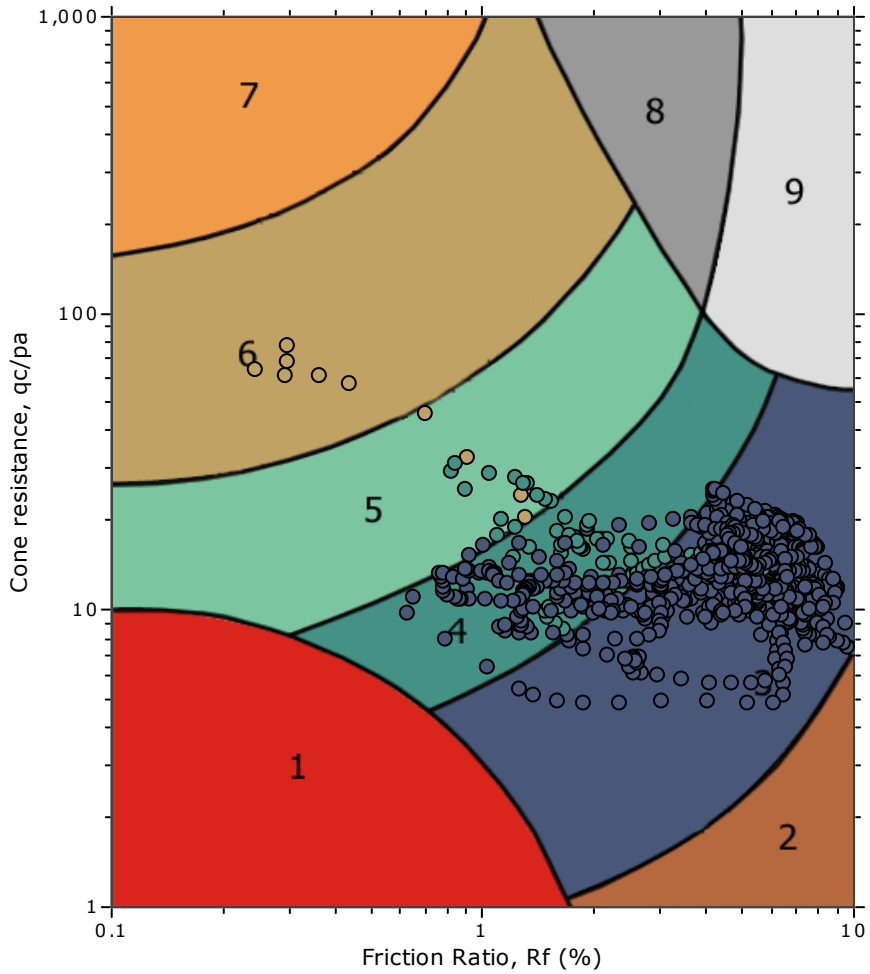
Project:
Location:

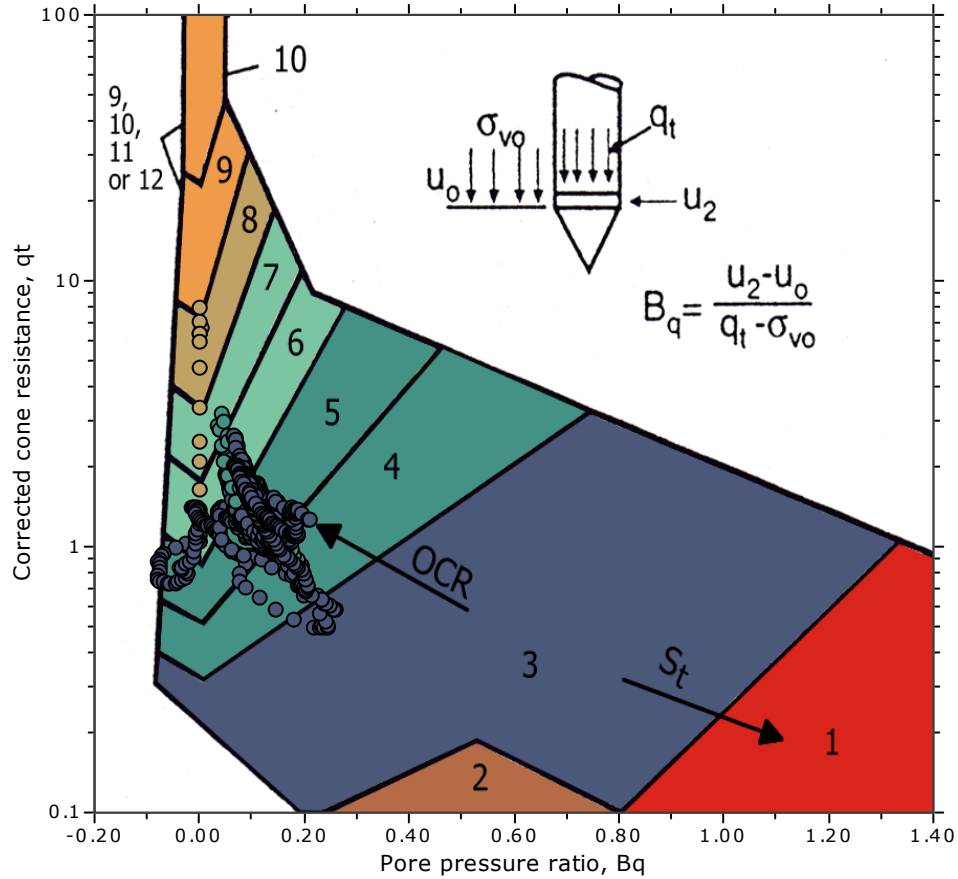
CPT: CPT-06
Total depth: 18.14 m, Date: 11/02/2024
Surface Elevation: 1.20 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

SBT - Bq plots

SBT plot



Bq plot



SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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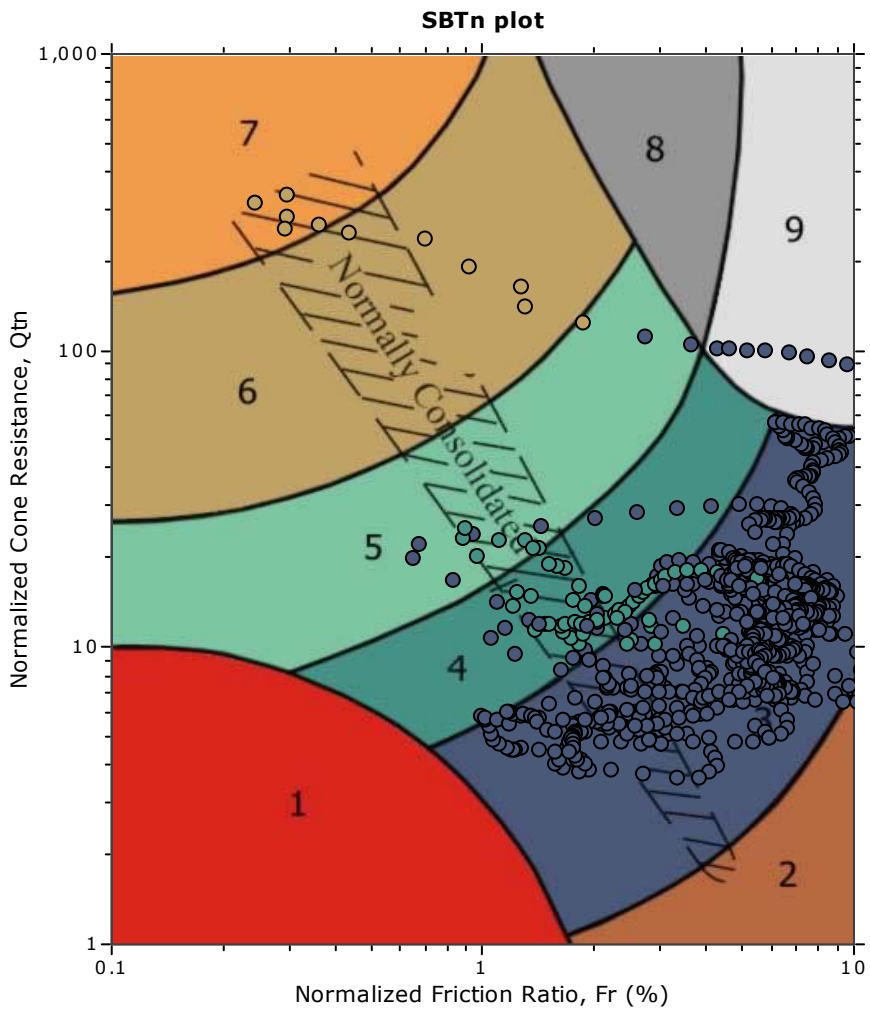
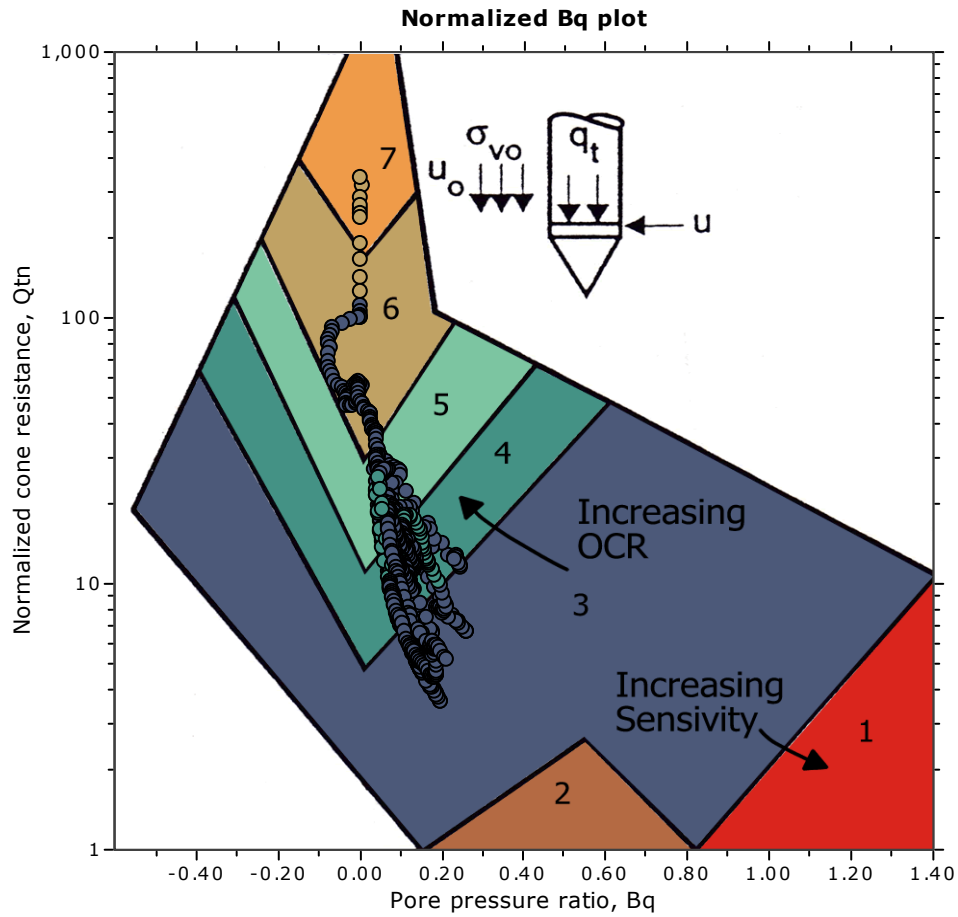
Project:
Location:

CPT: CPT-06
Total depth: 18.14 m, Date: 11/02/2024
Surface Elevation: 1.20 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

SBT - Bq plots (normalized)





SBTn legend

- 1. Sensitive fine grained
- 2. Organic material
- 3. Clay to silty clay
- 4. Clayey silt to silty clay
- 5. Silty sand to sandy silt
- 6. Clean sand to silty sand
- 7. Gravely sand to sand
- 8. Very stiff sand to clayey sand
- 9. Very stiff fine grained

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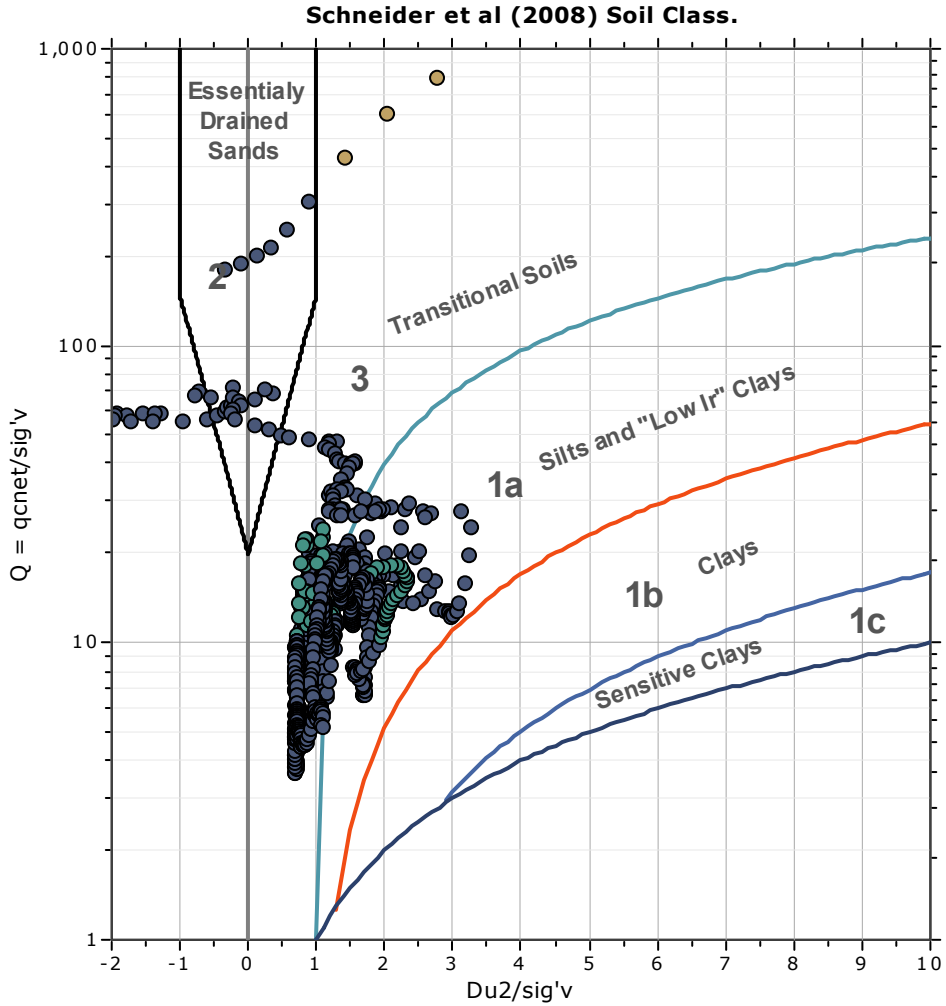
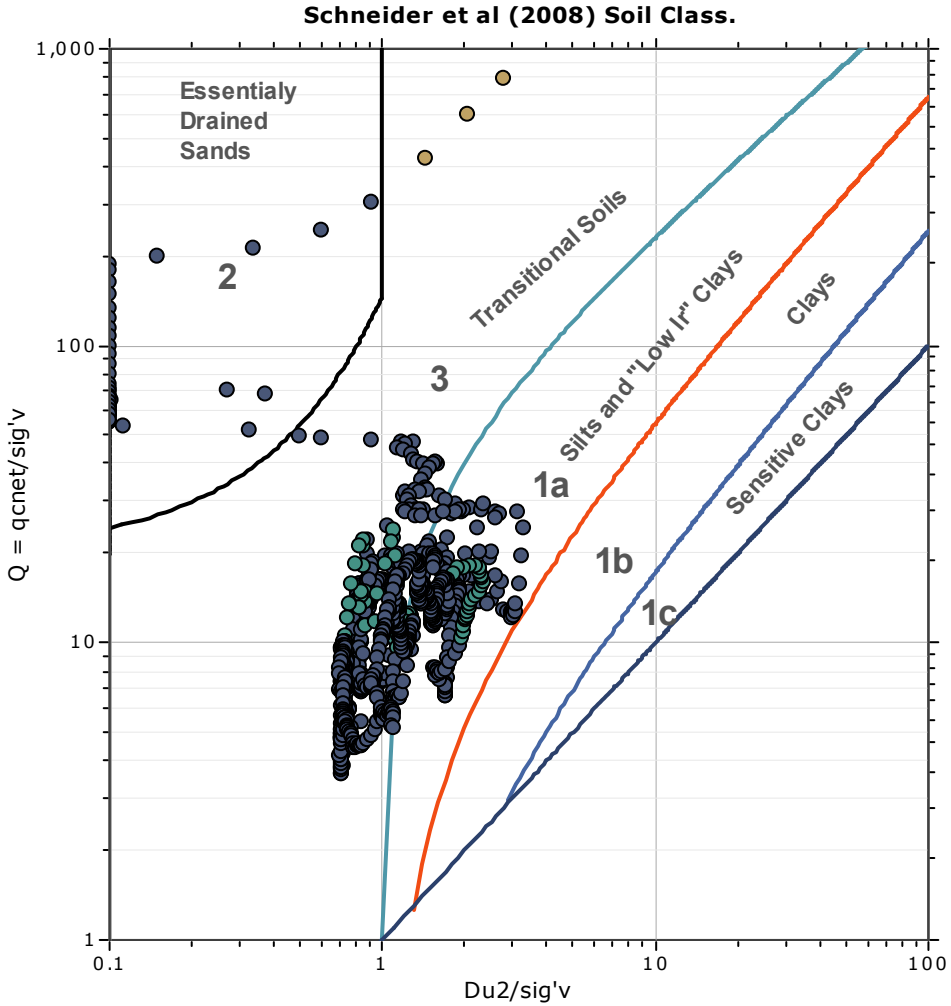
Project:
Location:

CPT: CPT-06
Total depth: 18.14 m, Date: 11/02/2024
Surface Elevation: 1.20 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Bq plots (Schneider)





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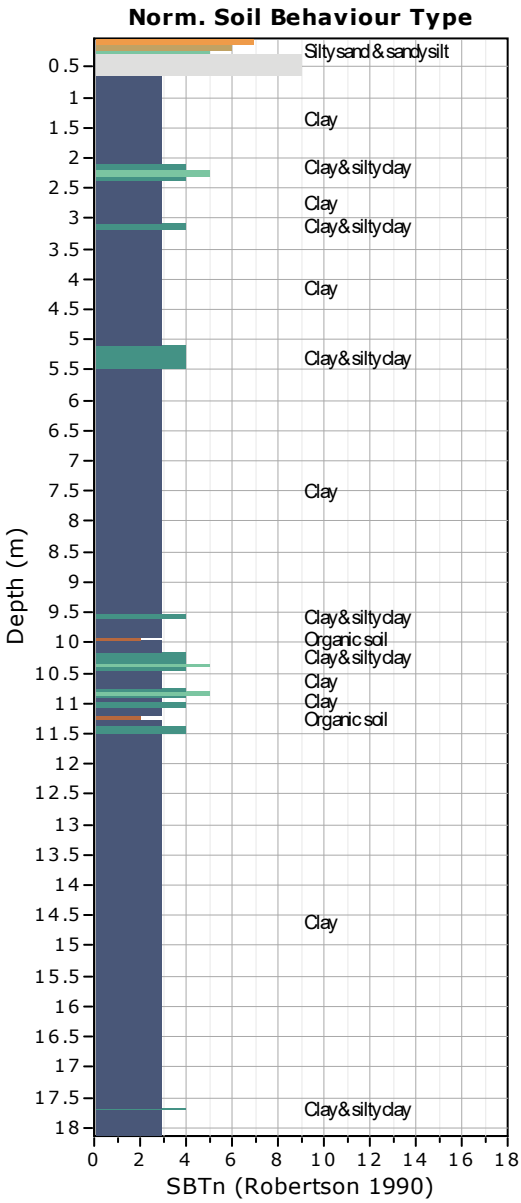
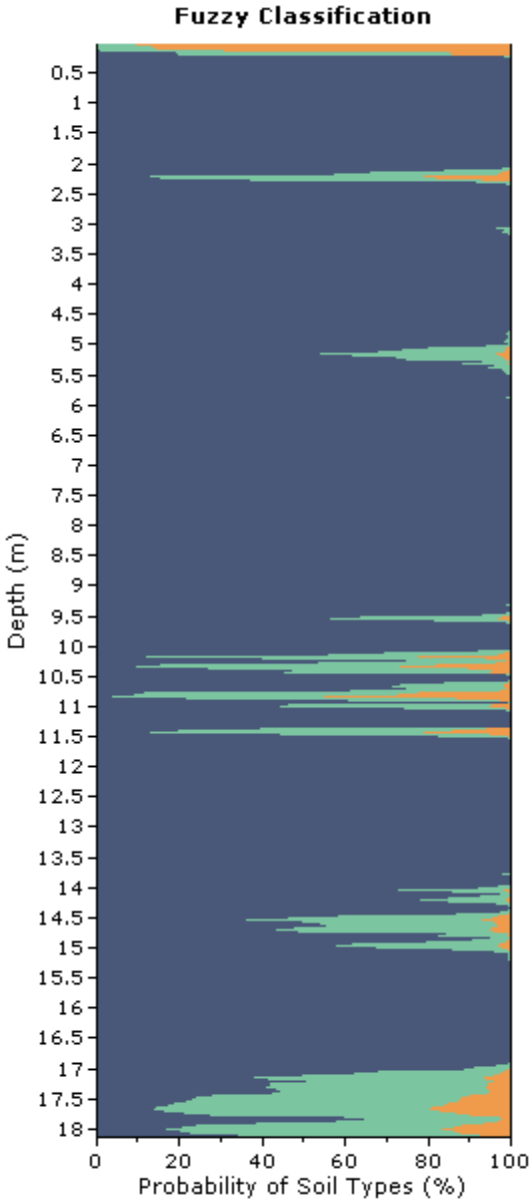
CPT: CPT-06
Total depth: 18.14 m, Date: 11/02/2024
Surface Elevation: 1.20 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:





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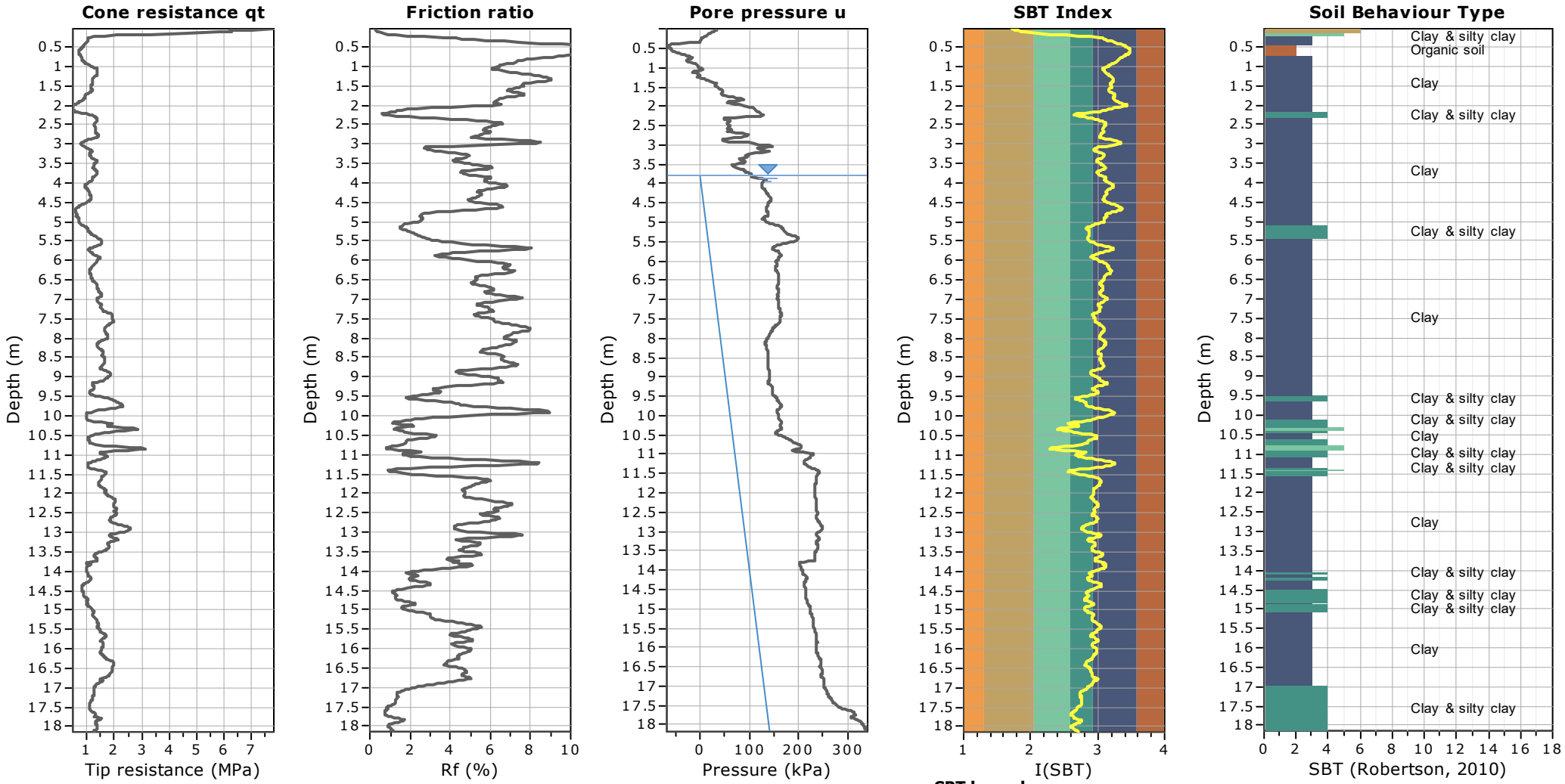
Project:
Location:

CPT: CPT-06
Total depth: 18.14 m, Date: 11/02/2024
Surface Elevation: 1.20 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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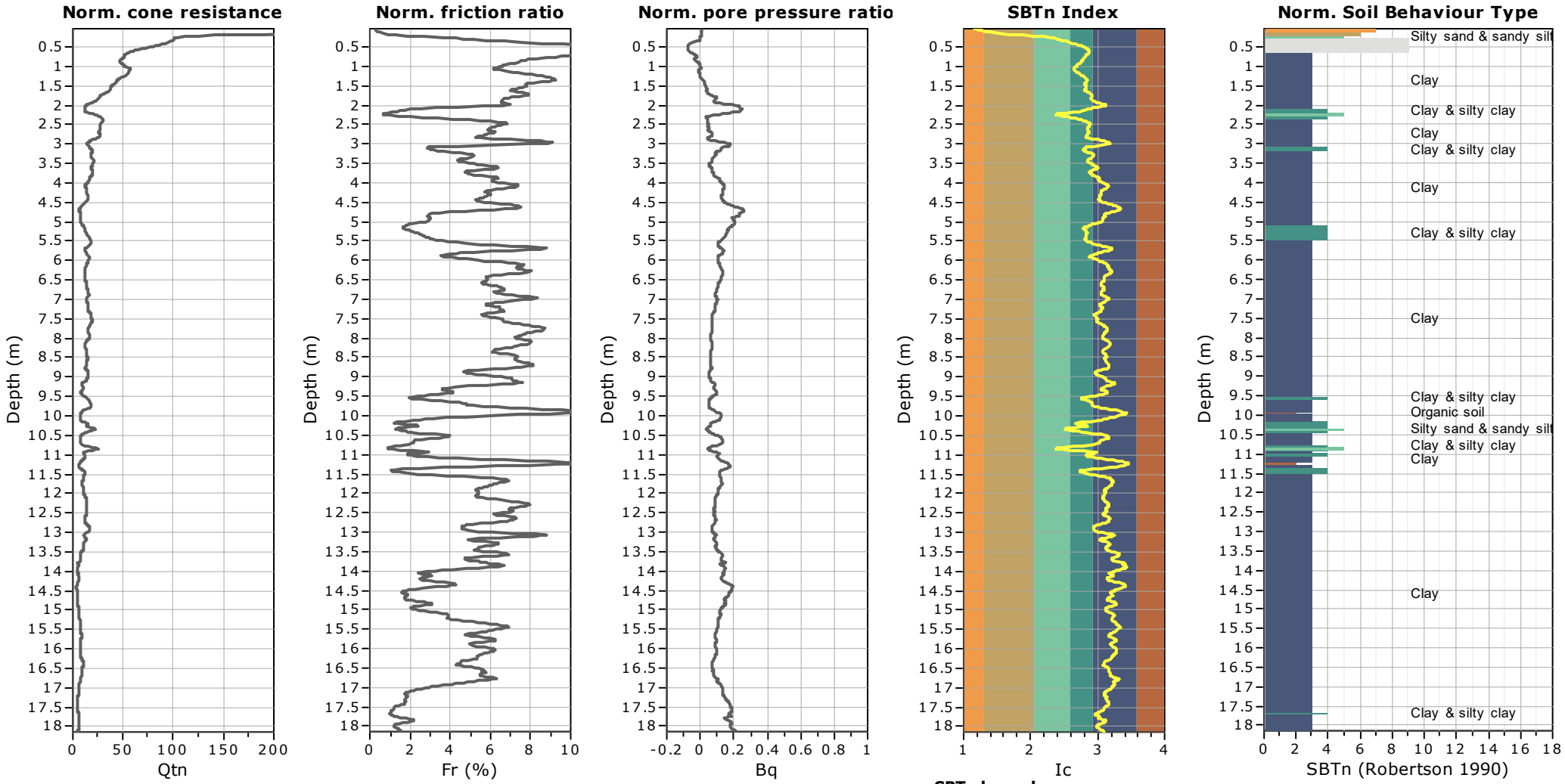
Project:
Location:

CPT: CPT-06
Total depth: 18.14 m, Date: 11/02/2024
Surface Elevation: 1.20 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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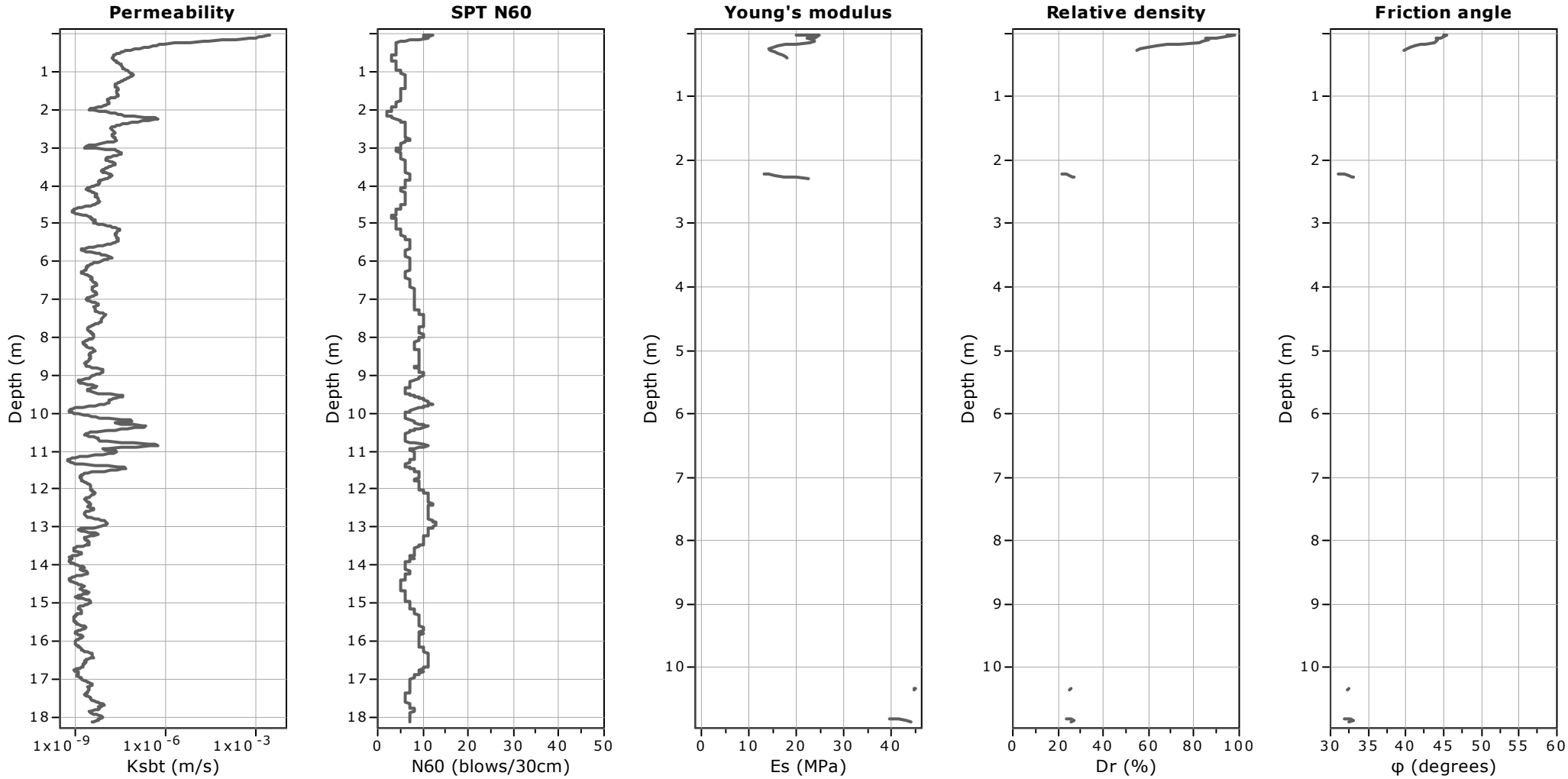
Project:
Location:

CPT: CPT-06
Total depth: 18.14 m, Date: 11/02/2024
Surface Elevation: 1.20 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Permeability: Based on SBT_n
SPT N_{60}: Based on I_c and q_t
Young's modulus: Based on variable alpha using I_c (Robertson, 2009)
Relative desnisty constant, C_{Dr}: 350.0
Phi: Based on Kulhawy & Mayne (1990)
User defined estimation data

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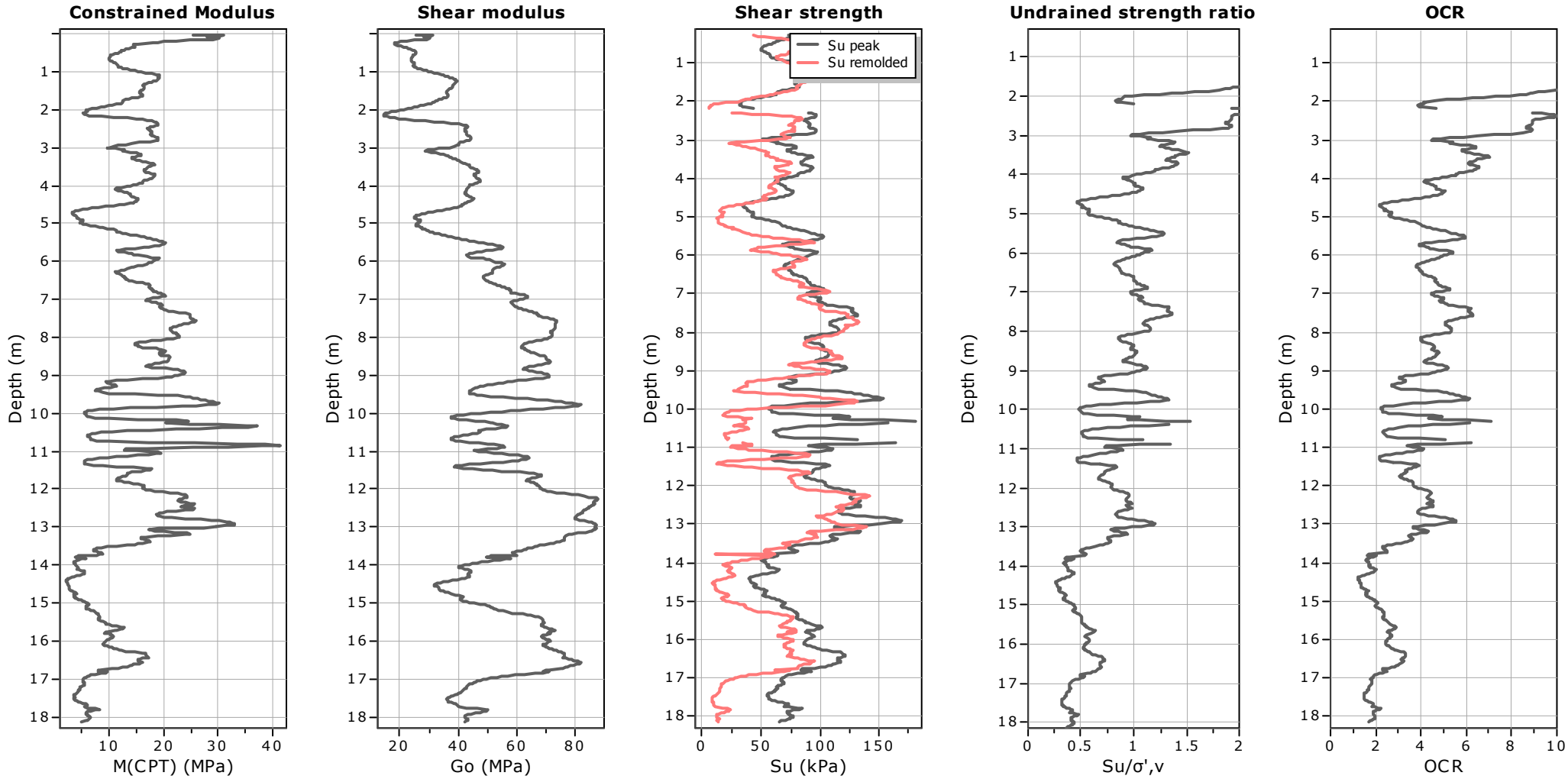
Project:
Location:

CPT: CPT-06
Total depth: 18.14 m, Date: 11/02/2024
Surface Elevation: 1.20 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Constrained modulus: Based on variable *alpha* using I_c and Q_{tn} (Robertson, 2009)
Go: Based on variable *alpha* using I_c (Robertson, 2009)
Undrained shear strength cone factor for clays, N_{kt}: 14

OCR factor for clays, N_{kt}: 0.33
User defined estimation data

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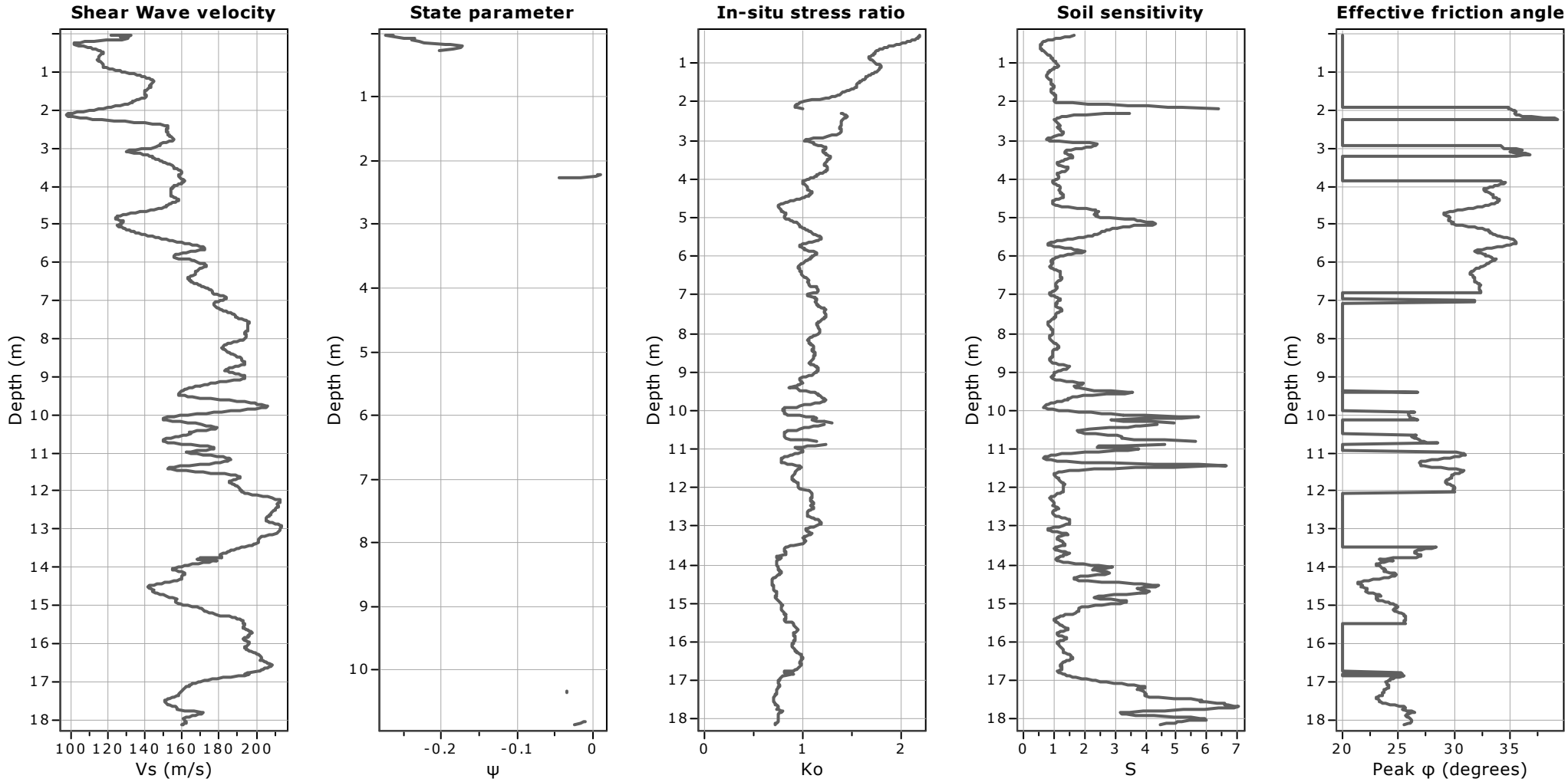
CPT: CPT-06
Total depth: 18.14 m, Date: 11/02/2024
Surface Elevation: 1.20 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:



Calculation parameters

Soil Sensitivity factor, N_S: 7.00

User defined estimation data

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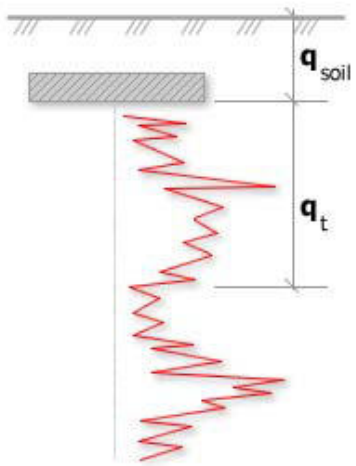
CPT: CPT-06
Total depth: 18.14 m, Date: 11/02/2024
Surface Elevation: 1.20 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

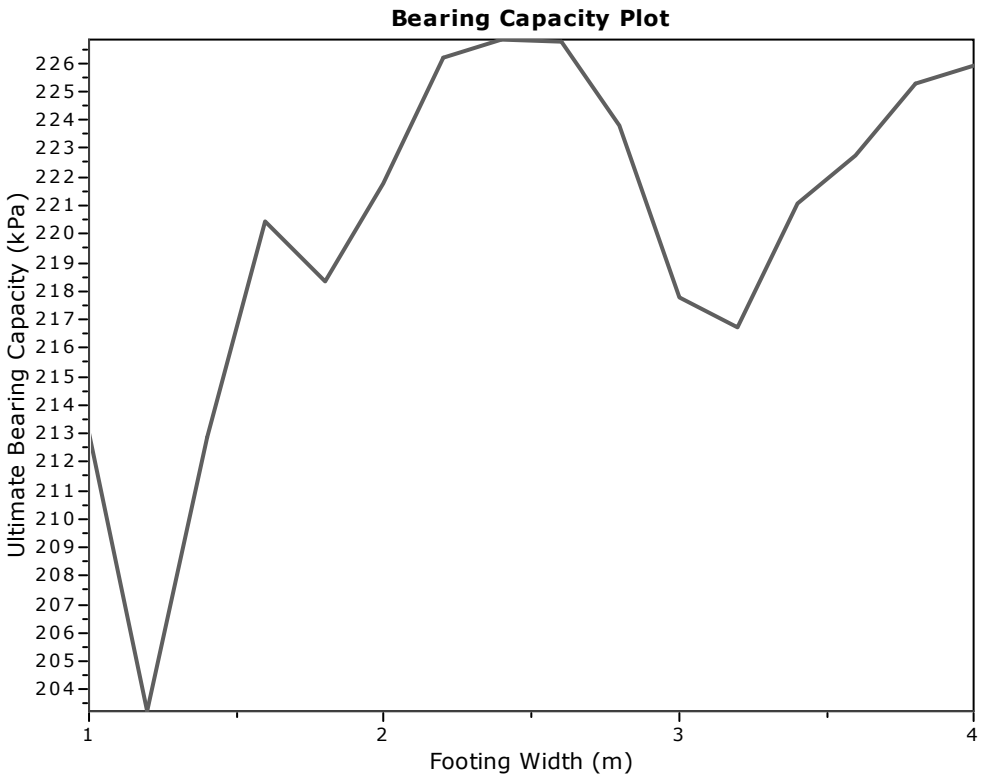
Project:
Location:



Bearing Capacity calculation is perfromed based on the formula:

$$Q_{ult} = R_k \times q_t + q_{soil}$$

where:
R_k: Bearing capacity factor
q_t: Average corrected cone resistance over calculation depth
q_{soil}: Pressure applied by soil above footing



:: Tabular results ::

No	B (m)	Start Depth (m)	End Depth (m)	Ave. q_t (MPa)	R_k	Soil Press. (kPa)	Ult. bearing cap. (kPa)
1	1.00	0.50	2.00	1.02	0.20	9.50	213.00
2	1.20	0.50	2.30	0.97	0.20	9.50	203.26
3	1.40	0.50	2.60	1.02	0.20	9.50	212.85
4	1.60	0.50	2.90	1.05	0.20	9.50	220.44
5	1.80	0.50	3.20	1.04	0.20	9.50	218.37
6	2.00	0.50	3.50	1.06	0.20	9.50	221.77
7	2.20	0.50	3.80	1.08	0.20	9.50	226.20
8	2.40	0.50	4.10	1.09	0.20	9.50	226.82
9	2.60	0.50	4.40	1.09	0.20	9.50	226.76
10	2.80	0.50	4.70	1.07	0.20	9.50	223.83
11	3.00	0.50	5.00	1.04	0.20	9.50	217.77
12	3.20	0.50	5.30	1.04	0.20	9.50	216.69
13	3.40	0.50	5.60	1.06	0.20	9.50	221.05
14	3.60	0.50	5.90	1.07	0.20	9.50	222.72
15	3.80	0.50	6.20	1.08	0.20	9.50	225.27
16	4.00	0.50	6.50	1.08	0.20	9.50	225.94

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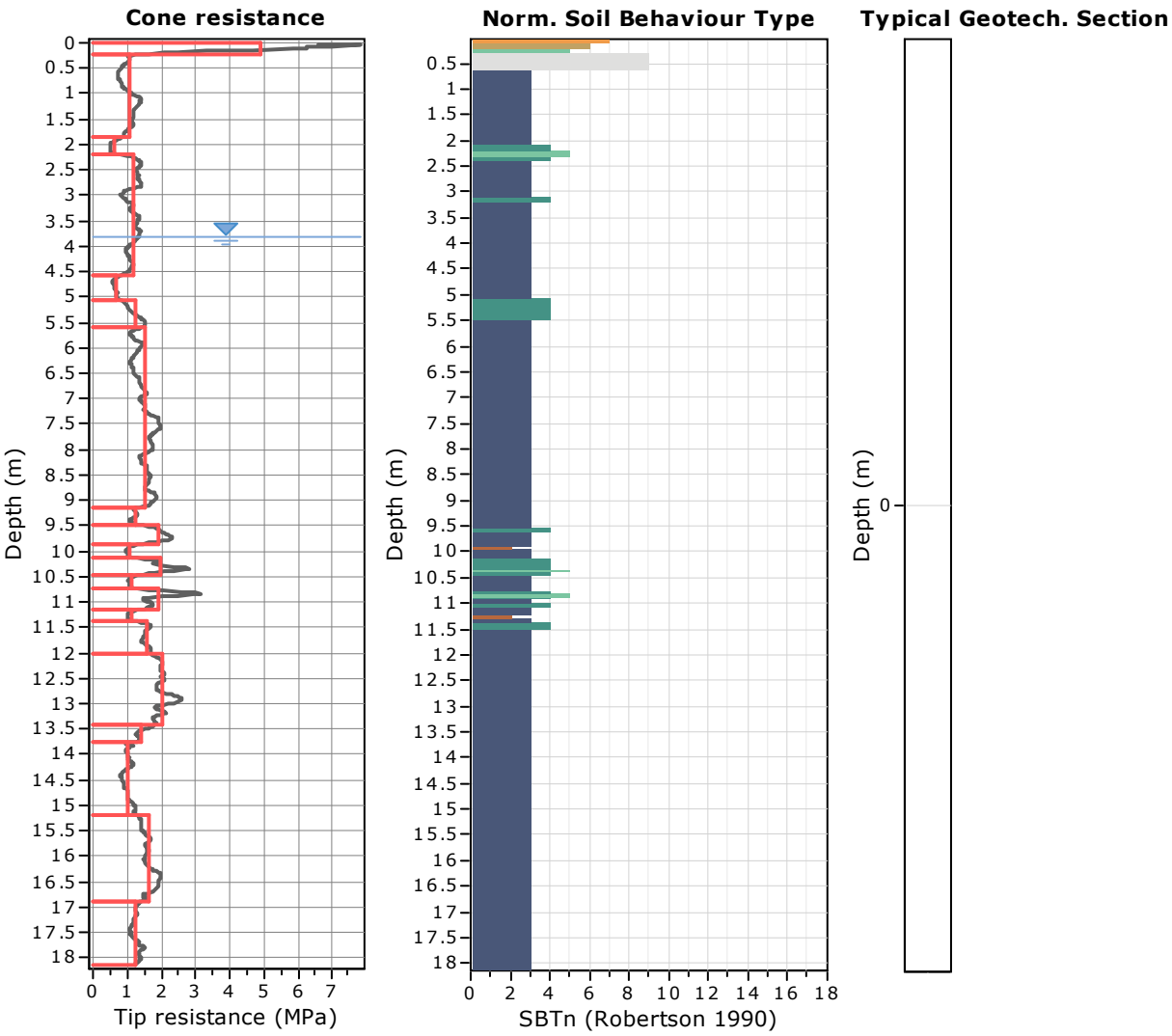
Project:
Location:

CPT: CPT-06
Total depth: 18.14 m, Date: 11/02/2024
Surface Elevation: 1.20 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Tabular results

.:: Layer No: 1 ::.

Code: R **Start depth:** 0.00 (m), **End depth:** 0.22 (m)

Description: Sand & silty sand

Basic results	**Estimation results**	
Total cone resistance: 4.90 ±2.18 MPa	Permeability: 9.11E-04 ±1.02E-03 m/s	Constrained Mod.: 26.31 ±4.27 MPa
Sleeve friction: 24.60 ±7.72 kPa	N60: 8.73 ±2.76 blows	Go: 26.31 ±4.27 MPa
SBT_n: 6	Es: 20.99 ±3.41 MPa	Su: 0.00 ±0.00 kPa
SBTn description: Sand & silty sand	Dr (%): 80.52 ±12.59	Su ratio: 0.00 ±0.00
	ö (degrees): 43.40 ±1.56 °	O.C.R.: 0.00 ±0.00
	Unit weight: 17.24 ±0.20 kN/m³	

.:: Layer No: 2 ::.

Code: A **Start depth:** 0.22 (m), **End depth:** 1.86 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.05 ±0.21 MPa	Permeability: 1.61E-07 ±6.93E-07 m/s	Constrained Mod.: 14.37 ±2.85 MPa
Sleeve friction: 80.77 ±18.43 kPa	N60: 4.64 ±0.94 blows	Go: 30.28 ±6.51 MPa
SBT_n: 3	Es: 16.60 ±1.41 MPa	Su: 72.74 ±14.39 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 3.79 ±1.38
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 17.51 ±6.40
	Unit weight: 18.02 ±0.31 kN/m³	

.:: Layer No: 3 ::.

Code: E **Start depth:** 1.86 (m), **End depth:** 2.21 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 0.60 ±0.12 MPa	Permeability: 2.71E-08 ±4.61E-08 m/s	Constrained Mod.: 7.47 ±2.12 MPa
Sleeve friction: 24.98 ±16.98 kPa	N60: 2.89 ±0.76 blows	Go: 20.43 ±5.21 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 39.42 ±8.43 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.08 ±0.29
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 4.98 ±1.33
	Unit weight: 16.18 ±0.95 kN/m³	

.:: Layer No: 4 ::.

Code: A2 **Start depth:** 2.21 (m), **End depth:** 4.56 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.17 ±0.17 MPa	Permeability: 2.99E-08 ±7.93E-08 m/s	Constrained Mod.: 15.44 ±2.60 MPa
Sleeve friction: 59.96 ±17.16 kPa	N60: 5.69 ±0.80 blows	Go: 40.81 ±6.11 MPa
SBT_n: 3	Es: 22.79 ±22.79 MPa	Su: 79.72 ±12.09 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.38 ±0.38
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 6.37 ±1.74
	Unit weight: 17.67 ±0.56 kN/m³	

.:: Layer No: 5 ::.

Code: E2 **Start depth:** 4.56 (m), **End depth:** 5.08 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 0.68 ±0.08 MPa	Permeability: 3.52E-09 ±3.24E-09 m/s	Constrained Mod.: 4.75 ±1.26 MPa
Sleeve friction: 25.06 ±12.85 kPa	N60: 3.96 ±0.52 blows	Go: 28.81 ±4.47 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 42.27 ±5.51 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.56 ±0.07
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.61 ±0.34
	Unit weight: 16.42 ±0.52 kN/m³	

.:: Layer No: 6 ::.

Code: A3 **Start depth:** 5.08 (m), **End depth:** 5.58 (m)

Description: Clay & silty clay

Basic results	**Estimation results**	
Total cone resistance: 1.22 ±0.23 MPa	Permeability: 2.14E-08 ±5.01E-09 m/s	Constrained Mod.: 14.89 ±4.24 MPa
Sleeve friction: 32.50 ±18.03 kPa	N60: 5.65 ±1.09 blows	Go: 37.26 ±8.45 MPa
SBT_n: 4	Es: 0.00 ±0.00 MPa	Su: 80.67 ±16.34 kPa
SBTn description: Clay & silty clay	Dr (%): 0.00 ±0.00	Su ratio: 1.02 ±0.19
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 4.72 ±0.90
	Unit weight: 16.90 ±0.69 kN/m³	

.:: Layer No: 7 ::.

Code: D **Start depth:** 5.58 (m), **End depth:** 9.13 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.50 ±0.23 MPa	Permeability: 4.25E-09 ±2.50E-09 m/s	Constrained Mod.: 18.68 ±3.72 MPa
Sleeve friction: 92.59 ±20.76 kPa	N60: 8.16 ±1.23 blows	Go: 61.45 ±8.50 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 98.23 ±15.84 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.03 ±0.13
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 4.77 ±0.61
	Unit weight: 18.32 ±0.32 kN/m³	

.:: Layer No: 8 ::.

Code: A4 **Start depth:** 9.13 (m), **End depth:** 9.48 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.21 ±0.08 MPa	Permeability: 3.23E-09 ±1.94E-09 m/s	Constrained Mod.: 9.90 ±1.57 MPa
Sleeve friction: 50.61 ±19.21 kPa	N60: 6.74 ±0.65 blows	Go: 49.81 ±6.30 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 74.85 ±5.85 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.67 ±0.05
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 3.10 ±0.25
	Unit weight: 17.51 ±0.41 kN/m³	

.:: Layer No: 9 ::.

Code: B1 **Start depth:** 9.48 (m), **End depth:** 9.86 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.94 ±0.31 MPa	Permeability: 1.43E-08 ±1.01E-08 m/s	Constrained Mod.: 24.00 ±5.56 MPa
Sleeve friction: 82.81 ±39.05 kPa	N60: 9.60 ±1.54 blows	Go: 66.31 ±13.44 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 126.29 ±21.77 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.10 ±0.19
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 5.10 ±0.86
	Unit weight: 18.16 ±0.68 kN/m³	

.:: Layer No: 10 ::.

Code: A5 **Start depth:** 9.86 (m), **End depth:** 10.14 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.09 ±0.14 MPa	Permeability: 2.60E-09 ±3.43E-09 m/s	Constrained Mod.: 7.24 ±2.49 MPa
Sleeve friction: 58.22 ±37.43 kPa	N60: 6.67 ±0.98 blows	Go: 50.43 ±12.27 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 65.04 ±10.21 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.55 ±0.09
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.56 ±0.41
	Unit weight: 17.46 ±0.81 kN/m³	

.:: Layer No: 11 ::.

Code: B2 **Start depth:** 10.14 (m), **End depth:** 10.46 (m)

Description: Clay & silty clay

Basic results	**Estimation results**	
Total cone resistance: 1.99 ±0.46 MPa	Permeability: 6.93E-08 ±6.42E-08 m/s	Constrained Mod.: 24.13 ±7.83 MPa
Sleeve friction: 30.85 ±7.39 kPa	N60: 8.47 ±1.37 blows	Go: 49.89 ±5.58 MPa
SBT_n: 4	Es: 45.12 ±45.12 MPa	Su: 121.45 ±26.83 kPa
SBTn description: Clay & silty clay	Dr (%): 0.00 ±0.00	Su ratio: 1.03 ±0.23
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 4.74 ±1.07
	Unit weight: 17.16 ±0.34 kN/m³	

.:: Layer No: 12 ::.

Code: A6 **Start depth:** 10.46 (m), **End depth:** 10.74 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.15 ±0.12 MPa	Permeability: 4.86E-09 ±2.84E-09 m/s	Constrained Mod.: 7.66 ±2.08 MPa
Sleeve friction: 27.42 ±7.95 kPa	N60: 6.20 ±0.41 blows	Go: 41.90 ±3.89 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 68.46 ±8.58 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.56 ±0.07
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.60 ±0.33
	Unit weight: 16.81 ±0.33 kN/m³	

.:: Layer No: 13 ::.

Code: B3 **Start depth:** 10.74 (m), **End depth:** 11.14 (m)

Description: Clay & silty clay

Basic results	**Estimation results**	
Total cone resistance: 1.91 ±0.56 MPa	Permeability: 9.05E-08 ±1.50E-07 m/s	Constrained Mod.: 21.52 ±9.68 MPa
Sleeve friction: 37.09 ±16.75 kPa	N60: 8.33 ±1.35 blows	Go: 52.25 ±5.98 MPa
SBT_n: 4	Es: 0.00 ±0.00 MPa	Su: 106.27 ±20.10 kPa
SBTn description: Clay & silty clay	Dr (%): 0.00 ±0.00	Su ratio: 0.86 ±0.17
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 3.97 ±0.79
	Unit weight: 17.30 ±0.41 kN/m³	

.:: Layer No: 14 ::.

Code: A8 **Start depth:** 11.14 (m), **End depth:** 11.38 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.13 ±0.12 MPa	Permeability: 1.97E-09 ±3.06E-09 m/s	Constrained Mod.: 6.99 ±1.97 MPa
Sleeve friction: 64.39 ±27.98 kPa	N60: 7.00 ±0.82 blows	Go: 54.90 ±9.31 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 66.62 ±8.89 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.53 ±0.07
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.43 ±0.33
	Unit weight: 17.68 ±0.65 kN/m³	

.:: Layer No: 15 ::.

Code: D2 **Start depth:** 11.38 (m), **End depth:** 12.00 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.55 ±0.11 MPa	Permeability: 8.20E-09 ±1.23E-08 m/s	Constrained Mod.: 14.07 ±2.23 MPa
Sleeve friction: 64.07 ±25.36 kPa	N60: 8.44 ±0.88 blows	Go: 60.46 ±9.96 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 96.22 ±7.81 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.74 ±0.06
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 3.43 ±0.28
	Unit weight: 17.80 ±0.68 kN/m³	

.:: Layer No: 16 ::.

Code: B4 **Start depth:** 12.00 (m), **End depth:** 13.40 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 2.01 ±0.22 MPa	Permeability: 3.72E-09 ±2.41E-09 m/s	Constrained Mod.: 22.62 ±4.53 MPa
Sleeve friction: 111.78 ±17.38 kPa	N60: 11.03 ±0.84 blows	Go: 81.60 ±5.20 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 127.17 ±15.37 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.92 ±0.11
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 4.24 ±0.51
	Unit weight: 18.66 ±0.19 kN/m³	

.:: Layer No: 17 ::.

Code: D3 **Start depth:** 13.40 (m), **End depth:** 13.76 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.43 ±0.21 MPa	Permeability: 1.52E-09 ±7.38E-10 m/s	Constrained Mod.: 9.92 ±3.61 MPa
Sleeve friction: 67.70 ±10.51 kPa	N60: 8.53 ±0.90 blows	Go: 63.73 ±5.78 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 84.75 ±14.92 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.58 ±0.11
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.68 ±0.49
	Unit weight: 17.94 ±0.25 kN/m³	

.:: Layer No: 18 ::.

Code: A9 **Start depth:** 13.76 (m), **End depth:** 15.20 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.03 ±0.13 MPa	Permeability: 1.48E-09 ±7.03E-10 m/s	Constrained Mod.: 4.01 ±1.24 MPa
Sleeve friction: 24.89 ±12.49 kPa	N60: 6.19 ±0.79 blows	Go: 42.56 ±6.48 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 55.23 ±8.88 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.36 ±0.06
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 1.67 ±0.26
	Unit weight: 16.58 ±0.55 kN/m³	

.:: Layer No: 19 ::.

Code: D4 **Start depth:** 15.20 (m), **End depth:** 16.90 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.62 ±0.19 MPa	Permeability: 1.57E-09 ±7.20E-10 m/s	Constrained Mod.: 10.97 ±2.96 MPa
Sleeve friction: 72.39 ±10.69 kPa	N60: 9.57 ±0.93 blows	Go: 70.81 ±5.71 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 95.23 ±13.26 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.58 ±0.07
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.67 ±0.34
	Unit weight: 18.08 ±0.22 kN/m³	

.:: Layer No: 20 ::.

Code: A10 **Start depth:** 16.90 (m), **End depth:** 18.14 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.26 ±0.10 MPa	Permeability: 3.88E-09 ±1.99E-09 m/s	Constrained Mod.: 5.21 ±1.08 MPa
Sleeve friction: 17.09 ±7.81 kPa	N60: 6.95 ±0.61 blows	Go: 43.36 ±5.15 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 67.94 ±7.30 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.39 ±0.04
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 1.79 ±0.18
	Unit weight: 16.25 ±0.46 kN/m³	

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Project:
Location:

CPT: CPT-06
Total depth: 18.14 m, Date: 11/02/2024
Surface Elevation: 1.20 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Summary table of mean values

From depth To depth (m)	Thickness (m)	Permeability (m/s)	SPT_{N60} (blows/30cm)	E_s (MPa)	D_r	Friction angle	Constrained modulus, M (MPa)	Shear modulus, G_O (MPa)	Undrained strength, S_U (kPa)	Undrained strength ratio	OCR	Unit weight (kN/m³)
0.00	0.22	9.11E-04	8.7	21.0	80.5	43.4	26.3	26.3	0.0	0.0	0.0	17.2
0.22		(±1.02E-03)	(±2.8)	(±3.4)	(±12.6)	(±1.6)	(±4.3)	(±4.3)	(±0.0)	(±0.0)	(±0.0)	(±0.2)
0.22	1.64	1.61E-07	4.6	16.6	0.0	0.0	14.4	30.3	72.7	3.8	17.5	18.0
1.86		(±6.93E-07)	(±0.9)	(±1.4)	(±0.0)	(±0.0)	(±2.8)	(±6.5)	(±14.4)	(±1.4)	(±6.4)	(±0.3)
1.86	0.35	2.71E-08	2.9	0.0	0.0	0.0	7.5	20.4	39.4	1.1	5.0	16.2
2.21		(±4.61E-08)	(±0.8)	(±0.0)	(±0.0)	(±0.0)	(±2.1)	(±5.2)	(±8.4)	(±0.3)	(±1.3)	(±1.0)
2.21	2.35	2.99E-08	5.7	22.8	0.0	0.0	15.4	40.8	79.7	1.4	6.4	17.7
4.56		(±7.93E-08)	(±0.8)	(±22.8)	(±0.0)	(±0.0)	(±2.6)	(±6.1)	(±12.1)	(±0.4)	(±1.7)	(±0.6)
4.56	0.52	3.52E-09	4.0	0.0	0.0	0.0	4.7	28.8	42.3	0.6	2.6	16.4
5.08		(±3.24E-09)	(±0.5)	(±0.0)	(±0.0)	(±0.0)	(±1.3)	(±4.5)	(±5.5)	(±0.1)	(±0.3)	(±0.5)
5.08	0.50	2.14E-08	5.7	0.0	0.0	0.0	14.9	37.3	80.7	1.0	4.7	16.9
5.58		(±5.01E-09)	(±1.1)	(±0.0)	(±0.0)	(±0.0)	(±4.2)	(±8.5)	(±16.3)	(±0.2)	(±0.9)	(±0.7)
5.58	3.55	4.25E-09	8.2	0.0	0.0	0.0	18.7	61.4	98.2	1.0	4.8	18.3
9.13		(±2.50E-09)	(±1.2)	(±0.0)	(±0.0)	(±0.0)	(±3.7)	(±8.5)	(±15.8)	(±0.1)	(±0.6)	(±0.3)
9.13	0.35	3.23E-09	6.7	0.0	0.0	0.0	9.9	49.8	74.8	0.7	3.1	17.5
9.48		(±1.94E-09)	(±0.7)	(±0.0)	(±0.0)	(±0.0)	(±1.6)	(±6.3)	(±5.9)	(±0.1)	(±0.3)	(±0.4)
9.48	0.38	1.43E-08	9.6	0.0	0.0	0.0	24.0	66.3	126.3	1.1	5.1	18.2
9.86		(±1.01E-08)	(±1.5)	(±0.0)	(±0.0)	(±0.0)	(±5.6)	(±13.4)	(±21.8)	(±0.2)	(±0.9)	(±0.7)
9.86	0.28	2.60E-09	6.7	0.0	0.0	0.0	7.2	50.4	65.0	0.6	2.6	17.5
10.14		(±3.43E-09)	(±1.0)	(±0.0)	(±0.0)	(±0.0)	(±2.5)	(±12.3)	(±10.2)	(±0.1)	(±0.4)	(±0.8)
10.14	0.32	6.93E-08	8.5	45.1	0.0	0.0	24.1	49.9	121.5	1.0	4.7	17.2
10.46		(±6.42E-08)	(±1.4)	(±45.1)	(±0.0)	(±0.0)	(±7.8)	(±5.6)	(±26.8)	(±0.2)	(±1.1)	(±0.3)

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Project:
Location:

CPT: CPT-06
Total depth: 18.14 m, Date: 11/02/2024
Surface Elevation: 1.20 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Summary table of mean values

From depth To depth (m)	Thickness (m)	Permeability (m/s)	SPT_{N60} (blows/30cm)	E_s (MPa)	D_r	Friction angle	Constrained modulus, M (MPa)	Shear modulus, G_O (MPa)	Undrained strength, S_U (kPa)	Undrained strength ratio	OCR	Unit weight (kN/m³)
10.46	0.28	4.86E-09	6.2	0.0	0.0	0.0	7.7	41.9	68.5	0.6	2.6	16.8
10.74		(±2.84E-09)	(±0.4)	(±0.0)	(±0.0)	(±0.0)	(±2.1)	(±3.9)	(±8.6)	(±0.1)	(±0.3)	(±0.3)
10.74	0.40	9.05E-08	8.3	0.0	0.0	0.0	21.5	52.3	106.3	0.9	4.0	17.3
11.14		(±1.50E-07)	(±1.4)	(±0.0)	(±0.0)	(±0.0)	(±9.7)	(±6.0)	(±20.1)	(±0.2)	(±0.8)	(±0.4)
11.14	0.24	1.97E-09	7.0	0.0	0.0	0.0	7.0	54.9	66.6	0.5	2.4	17.7
11.38		(±3.06E-09)	(±0.8)	(±0.0)	(±0.0)	(±0.0)	(±2.0)	(±9.3)	(±8.9)	(±0.1)	(±0.3)	(±0.6)
11.38	0.62	8.20E-09	8.4	0.0	0.0	0.0	14.1	60.5	96.2	0.7	3.4	17.8
12.00		(±1.23E-08)	(±0.9)	(±0.0)	(±0.0)	(±0.0)	(±2.2)	(±10.0)	(±7.8)	(±0.1)	(±0.3)	(±0.7)
12.00	1.40	3.72E-09	11.0	0.0	0.0	0.0	22.6	81.6	127.2	0.9	4.2	18.7
13.40		(±2.41E-09)	(±0.8)	(±0.0)	(±0.0)	(±0.0)	(±4.5)	(±5.2)	(±15.4)	(±0.1)	(±0.5)	(±0.2)
13.40	0.36	1.52E-09	8.5	0.0	0.0	0.0	9.9	63.7	84.7	0.6	2.7	17.9
13.76		(±7.38E-10)	(±0.9)	(±0.0)	(±0.0)	(±0.0)	(±3.6)	(±5.8)	(±14.9)	(±0.1)	(±0.5)	(±0.3)
13.76	1.44	1.48E-09	6.2	0.0	0.0	0.0	4.0	42.6	55.2	0.4	1.7	16.6
15.20		(±7.03E-10)	(±0.8)	(±0.0)	(±0.0)	(±0.0)	(±1.2)	(±6.5)	(±8.9)	(±0.1)	(±0.3)	(±0.5)
15.20	1.70	1.57E-09	9.6	0.0	0.0	0.0	11.0	70.8	95.2	0.6	2.7	18.1
16.90		(±7.20E-10)	(±0.9)	(±0.0)	(±0.0)	(±0.0)	(±3.0)	(±5.7)	(±13.3)	(±0.1)	(±0.3)	(±0.2)
16.90	1.24	3.88E-09	7.0	0.0	0.0	0.0	5.2	43.4	67.9	0.4	1.8	16.2
18.14		(±1.99E-09)	(±0.6)	(±0.0)	(±0.0)	(±0.0)	(±1.1)	(±5.2)	(±7.3)	(±0.0)	(±0.2)	(±0.5)

Depth values presented in this table are measured from free ground surface

Presented below is a list of formulas used for the estimation of various soil properties. The formulas are presented in SI unit system and assume that all components are expressed in the same units.

:: Unit Weight, g (kN/m³) ::

$$g = g_w \cdot \left(0.27 \cdot \log(R_f) + 0.36 \cdot \log(\frac{q_t}{p_a}) + 1.236\right)$$

where g_w = water unit weight

:: Permeability, k (m/s) ::

$I_c < 3.27$ and $I_c > 1.00$ then $k = 10^{0.952-3.04 \cdot I_c}$

$I_c \leq 4.00$ and $I_c > 3.27$ then $k = 10^{-4.52-1.37 \cdot I_c}$

:: N_{SPT} (blows per 30 cm) ::

$$N_{60} = \left(\frac{q_c}{P_a}\right) \cdot \frac{1}{10^{1.1268-0.2817 \cdot I_c}}$$

$$N_{1(60)} = Q_{tn} \cdot \frac{1}{10^{1.1268-0.2817 \cdot I_c}}$$

:: Young's Modulus, Es (MPa) ::

$$(q_t - \sigma_v) \cdot 0.015 \cdot 10^{0.55 \cdot I_c + 1.68}$$

(applicable only to $I_c < I_{c\_cutoff}$)

:: Relative Density, Dr (%) ::

$$100 \cdot \sqrt{\frac{Q_{tn}}{k_{DR}}}$$

(applicable only to SBT_n: 5, 6, 7 and 8 or $I_c < I_{c\_cutoff}$)

:: State Parameter, ψ ::

$$\psi = 0.56 - 0.33 \cdot \log(Q_{tn,cs})$$

:: Peak drained friction angle, φ (°) ::

$$\varphi = 17.60 + 11 \cdot \log(Q_{tn})$$

(applicable only to SBT_n: 5, 6, 7 and 8)

:: 1-D constrained modulus, M (MPa) ::

If $I_c > 2.20$

$\alpha = 14$ for $Q_{tn} > 14$

$\alpha = Q_{tn}$ for $Q_{tn} \leq 14$

$M_{CPT} = \alpha \cdot (q_t - \sigma_v)$

If $I_c \leq 2.20$

$M_{CPT} = (q_t - \sigma_v) \cdot 0.0188 \cdot 10^{0.55 \cdot I_c + 1.68}$

:: Small strain shear Modulus, Go (MPa) ::

$$G_0 = (q_t - \sigma_v) \cdot 0.0188 \cdot 10^{0.55 \cdot I_c + 1.68}$$

:: Shear Wave Velocity, Vs (m/s) ::

$$V_s = \left(\frac{G_0}{\rho}\right)^{0.50}$$

:: Undrained peak shear strength, Su (kPa) ::

$N_{kt} = 10.50 + 7 \cdot \log(F_r)$ or user defined

$$S_u = \frac{(q_t - \sigma_v)}{N_{kt}}$$

(applicable only to SBT_n: 1, 2, 3, 4 and 9 or $I_c > I_{c\_cutoff}$)

:: Remolded undrained shear strength, Su(rem) (kPa) ::

$S_{u(rem)} = f_s$ (applicable only to SBT_n: 1, 2, 3, 4 and 9 or $I_c > I_{c\_cutoff}$)

:: Overconsolidation Ratio, OCR ::

$$k_{OCR} = \left[\frac{Q_{tn}^{0.20}}{0.25 \cdot (10.50 \cdot +7 \cdot \log(F_r))}\right]^{1.25}$$ or user defined

$OCR = k_{OCR} \cdot Q_{tn}$

(applicable only to SBT_n: 1, 2, 3, 4 and 9 or $I_c > I_{c\_cutoff}$)

:: In situ Stress Ratio, Ko ::

$$K_O = (1 - \sin\varphi') \cdot OCR^{\sin\varphi'}$$

(applicable only to SBT_n: 1, 2, 3, 4 and 9 or $I_c > I_{c\_cutoff}$)

:: Soil Sensitivity, S_t ::

$$S_t = \frac{N_S}{F_r}$$

(applicable only to SBT_n: 1, 2, 3, 4 and 9 or $I_c > I_{c\_cutoff}$)

:: Effective Stress Friction Angle, φ' (°) ::

$$\varphi' = 29.5° \cdot B_q^{0.121} \cdot (0.256 + 0.336 \cdot B_q + \log Q_t)$$

(applicable for $0.10 < B_q < 1.00$)

References

• Robertson, P.K., Cabal K.L., Guide to Cone Penetration Testing for Geotechnical Engineering, Gregg Drilling & Testing, Inc., 5th Edition, November 2012

• Robertson, P.K., Interpretation of Cone Penetration Tests - a unified approach., Can. Geotech. J. 46(11): 1337–1355 (2009)

ALLEGATO III

- PROVE DI LABORATORIO -

TAGLIO DIRETTO CD

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laboratorio geoTecnico GeoTest
terre - rocce - aggregati - prove cidiche e dinamiche - prove geotecniche in sito - geochimica ambientale - prospezioni geofisiche - misura del Radon
Via Lucca 55 A-B - MELFI (PZ) - tel/fax 0972347447
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s.a.s. di Carbone Andrea & C.

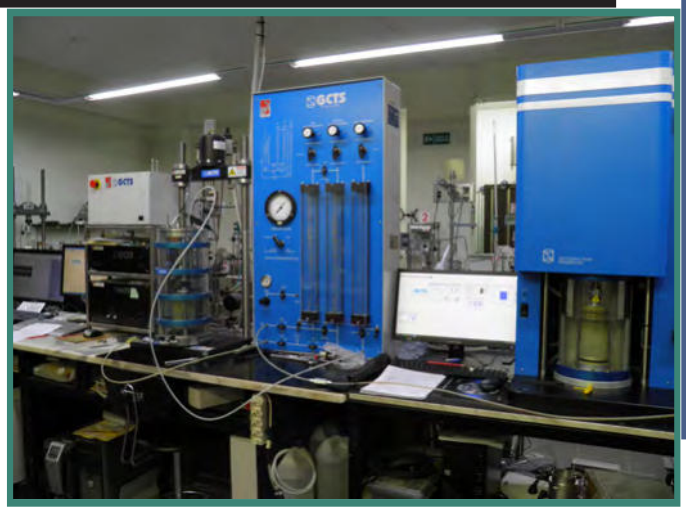
LABORATORIO UFFICIALE
Art. 59 D.P.R. 380/2001
Circolare 7618/STC
Settori "A" e "B"
Consiglio Superiore dei Lavori Pubblici

Certitalia Sistema di Gestione certificato UNI EN ISO 9001:2015
Geotest S.a.s. - Melfi (PZ) - Italy has been resulted in compliance with the standard UNI EN ISO 9001:2015 for the following field of activities: Provision of geotechnical tests

Committente: ***Geologo Zamboni Maurizio - Via dei Giardini, 11 - Monzuno (BO)***

Riferimento: ***Via Puglia - Loc. Biancolina - San Giovanni in Persiceto (BO)***

Verbale n.: ***027/06.02.2024*** - Certificati n.: ***00581 - 00583*** - *Emissione:* ***28/02/2024***



Il Direttore del laboratorio
dott. Carbone Raffaele

LABORATORIO GEOTECHNICO GEOTEST s.a.s. di Carbone Andrea & C. TERRE - ROCCE - AGGREGATI MELFI (PZ)
Autorizzazione del Ministero Infrastrutture
Decreto n. 0000155 del 2023

DEFINIZIONI ADOTTATE PER LA DESCRIZIONE DEI CAMPIONI

CONSERVAZIONE ED APERTURA DEI CAMPIONI

Dopo il controllo dei dati identificativi, i campioni ricevuti sono stati ricoverati in camera climatica in cui temperatura e umidità relativa vengono mantenute costanti rispettivamente a 20°C e oltre 85 %.
Per ogni campione aperto sono stati rilevati i dati identificativi (sondaggio e numero d'ordine progressivo). Il modulo di prova è stato quindi compilato con data di consegna, data di apertura e con ogni altra informazione disponibile riguardo le modalità di campionamento. Per tutti i campioni in fustella esaminati è stata adottata l'estrusione orizzontale: con un estrusore pneumatico, provvisto di variatore di pressione e di teste intercambiabili in funzione del diametro interno del carotiere, il campione è stato estratto in una singola corsa e depositato su un banco posto allo stesso livello del bordo della fustella; dopo una cauta scorticazione del terreno per liberarlo dal velo costituito dal fango di perforazione è stata ottenuta una ripresa fotografica.

DESCRIZIONE GEOTECNICA DEI TERRENI

La descrizione del campione, riportata sul "*Modulo Riassuntivo*", raccoglie tutte le indicazioni desunte dall'osservazione delle caratteristiche del campione immediatamente dopo la sua estrusione e scorticazione. Sono state in primo luogo descritte le caratteristiche generali del campione, evidenziando ad esempio la eventuale presenza di discontinuità, fratture o rammollimenti di alcune parti del campione stesso. Il campione è stato quindi descritto evidenziando le parti aventi caratteristiche omogenee, nel seguito chiamate "***settori***". Ogni singolo settore è stato analizzato a partire dalla testa del campione, secondo il seguente ordine: delimitazione del settore, natura del materiale, colore, struttura (se riconoscibile), consistenza (se misurabile) e nell'eventualità, presenza di materiale organico vegetale, reattività con acido cloridrico, strutture subordinate, discontinuità, torba e/o fossili. Per i campioni rimaneggiati la descrizione è stata di norma adeguata alle caratteristiche del campione e limitata alle informazioni relative a natura del terreno, colore, reattività con acido cloridrico ed eventuali presenze di strutture subordinate e/o torba o fossili.
I **limiti spaziali** del settore sono stati espressi in metri, attribuendo alla testa del campione la profondità reale di campionamento.
La **natura del terreno** è stata descritta con riferimento alle dimensioni dei grani ed alle percentuali dei diversi tipi di materiali presenti, così come determinati visivamente dall'Operatore e successivamente tramite verifica con le analisi granulometriche secondo lo schema e le definizioni delle Raccomandazioni AGI (AGI, 1977). Al materiale è stato attribuito il nome della percentuale più rilevante seguita da specificazioni per indicare le frazioni minoritarie. **Per la ghiaia è stato descritto l'assortimento, il grado di arrotondamento, la forma e la dimensione maggiore (Lmax) espressa in millimetri; mentre per la sabbia è stato descritto l'assortimento e, per la frazione avente grani ben osservabili ad occhio nudo, è stato anche riportato il grado di arrotondamento**.
Per descrivere l'**assortimento** sono stati utilizzati i termini fine (f), media (m), grossolana (g), medio fine (m/f), medio grossolana (m/g) ed eterogenea.
Per il **grado di arrotondamento** sono stati usati i termini arrotondata, subarrotondata, subangolare, angolare con riferimento alle fig. 1 (Rittenhouse, 1943) per la sabbia e alla fig. 1 per la ghiaia e i ciottoli (Pettijohn, 1949).
Per la **forma** sono stati usati i termini discoidale, sferoidale, lamellare, allungata con riferimento allo schema di fig. 1 (Gnaccolini, 1978), in cui la dimensione dell'elemento di dimensione maggiore (Lmax) è espressa in centimetri.
Il **colore fondamentale** o i colori fondamentali (se più di uno, ma distribuiti senza una struttura particolare)

sono stati descritti con l'ausilio della Tavola dei colori Munsell (Munsell, 1975) fornendo il nome e la sigla.

La **struttura** del settore, cioè l'organizzazione macroscopica delle particelle costituenti il materiale, è stata individuata, quando evidente, con riferimento ai seguenti tipi:

Struttura omogenea: consiste in materiale con organizzazione indifferenziata delle particelle.

Struttura a livelli: consiste nella presenza di livelli (spessore di materiale maggiore di 6 mm) che si alternano nel settore. I livelli possono essere descritti come da schema di fig. 1.

Struttura laminata: consiste nella presenza di laminazioni e livelli (rispettivamente con spessore di materiale inferiore o superiore a 6 mm) che si alternano nel settore. Queste possono essere descritte come da schema di fig. 1 con il termine "*in alternanza*".

Struttura caotica: è individuata da segni evidenti di rimescolamento legato a fenomeni naturali.

Struttura scagliosa: è individuata dall'attitudine del materiale a sfaldarsi secondo "scaglie".

L'assenza di indicazioni segnala una struttura omogenea del materiale.

La **consistenza** è stata descritta per i soli terreni fini sulla base dei risultati del Penetrometro Tascabile condotti sulle teste del campione o sui fianchi previamente scorticati.

Il **materiale organico** è stato descritto mediante i termini resti vegetali e torba cioè materiale vegetale in variabile stato di decomposizione. Di quest'ultimo sono stati indicati: tessitura: fibrosa o amorfa a seconda che sia stato riconosciuto o meno il tessuto vegetale originario; consistenza: compatta o spugnosa a seconda che possa essere stata o meno manipolata; colore: ricavato dal confronto con le tavole "*Munsell Soil Color Chart*".

Per qualificare un terreno contenente percentuali variabili di torba è stato utilizzato il termine "*torboso*". Si è, infine, fatto uso del termine "*frustolo*" per indicare l'eventuale struttura irregolare della torba.

I **fossili** sono stati descritti con riferimento al colore ed alla loro integrità o fratturazione.

La **reazione all'acido cloridrico** è stata descritta con i termini "*debolmente reagente con HCl*", "*reagente con HCl*", "*fortemente reagente con HCl*". Le classi corrispondono rispettivamente ad una debole reazione, ad una reazione evidente e ad una reazione molto intensa. L'assenza di indicazioni segnala la mancata reazione del materiale con HCl.

Le **strutture subordinate** sono state classificate come livelli, laminazioni, lenti, noduli, granuli, identificabili all'interno del settore per diversa granulometria, reazione con HCl o colore. I termini "*livelli*" e "*laminazioni*" sono stati utilizzati per indicare rispettivamente spessori di materiale superiori e inferiori a 6 mm relativi all'intera sezione del campione. La geometria della loro disposizione è stata descritta con riferimento allo schema di fig. 1. Il termine "*lenti*" è stato utilizzato per descrivere materiali con geometria lentiforme; il termine "*noduli*" per materiali subsferoidali di diametro superiore a 2 mm; il termine "*granuli*" per materiali subsferoidali di diametro inferiore a 2 mm. La descrizione dei materiali subordinati, quando significativa, è stata eseguita con le stesse modalità previste per il settore.

Le **discontinuità** sono state segnalate con il termine "*frattura*", con indicazione dell'eventuale assenza di scabrezza.

Di ogni materiale subordinato è stato indicato l'intervallo di profondità all'interno del quale è stato osservato. Nel caso fosse presente in tutto lo strato considerato, è stato utilizzato il termine "*sparso*". Del materiale subordinato è stata indicata anche la frequenza con gli aggettivi "*raro*", "*qualche" e "frequente*". Di ogni campione è stata ottenuta documentazione fotografica per meglio evidenziare i tipi di materiali esaminati e le eventuali anomalie strutturali. Le fotografie sono completate con i dati identificativi, una scala cromatica e un riferimento dimensionale.

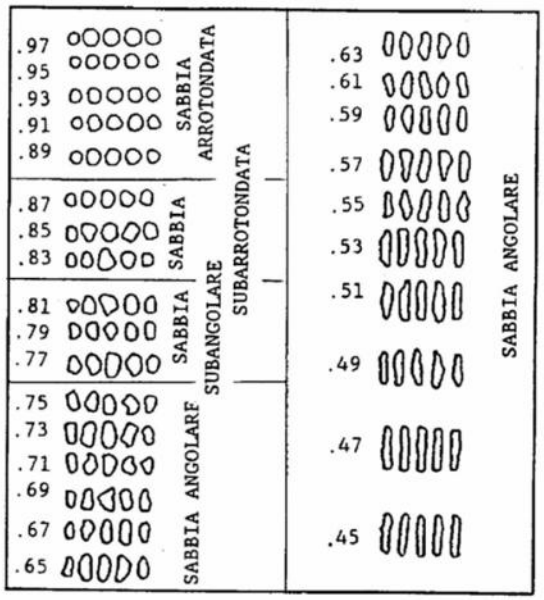


Fig. 1/1 - Classificazione delle sabbie in relazione al grado di arrotondamento (Rittenhouse, 1943)

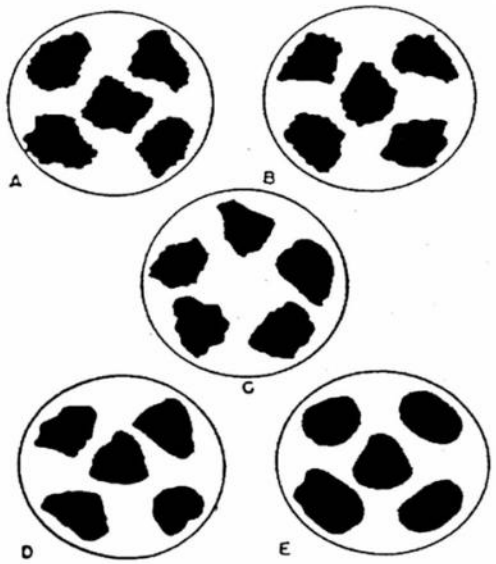


Fig. 1/2 - Classificazione della ghiaia e dei ciottoli in relazione al grado di arrotondomento:
A = Angolare B = Subangolare,
C = Subarrotondata D E = Arrotondata

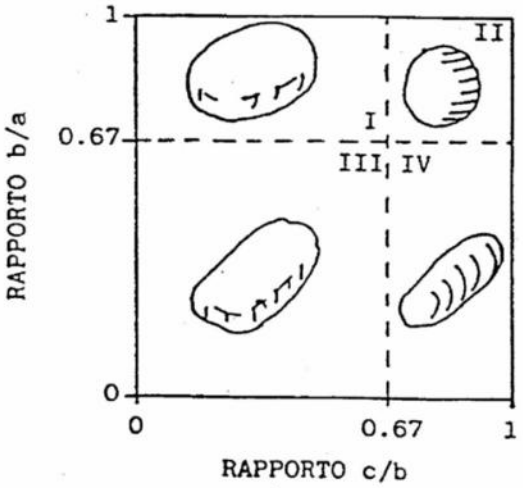


Fig. 1/3 - Classificazione della ghiaia e dei ciottoli in funzione della forma (Gnaccolini, 1978): a, b, c d sono le dimensioni caratteristiche dei grani.
I = discoidali II = sferoidali
III = lamellari IV = allungati

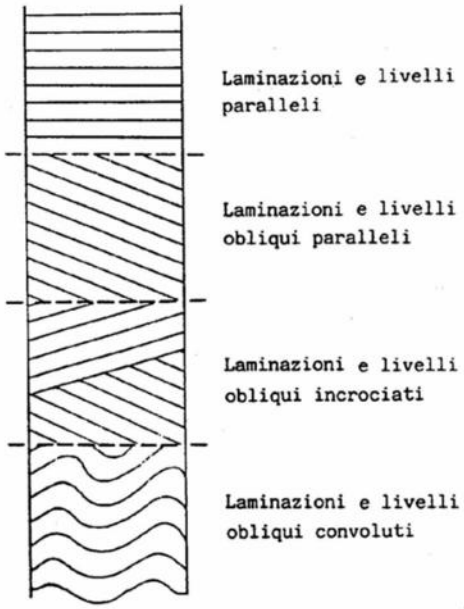


Fig. 1/4 – Schema per la descrizione dei livelli e delle laminazioni.

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COMMITTENTE:	**Geologo Zamboni Maurizio - Via dei Giardini, 11 - Monzuno (BO)**
RIFERIMENTO:	**Via Puglia - Loc. Biancolina - San Giovanni in Persiceto (BO)**
SONDAGGIO:	**CPT9** ***CAMPIONE:*** **C1** ***PROFONDITA': m*** **0,40 - 0,65**

MODULO RIASSUNTIVO

TAGLIO DIRETTO

Coesione:	***8,6***	***kPa***
Angolo di attrito interno:	***18,7***	***°***

FOTOGRAFIA

Posizione delle prove TD	*cm*	*Rp kPa*	*VT kPa*	*cm*	*DESCRIZIONE DEL CAMPIONE*
	0				**Argilla limosa con tracce di sabbia (f) [ESAME VISIVO], di colore beige grigiastro, estremamante compatto e a struttura omogena. Reagente all'HCl.**
	5	400			**Qualità del campione: Q5**
	10	410			
	15	410.			
	20				
	25			25	

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IL DIRETTORE DEL LABORATORIO
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RIFERIMENTO: Via Puglia - Loc. Biancolina - San Giovanni in Persiceto (BO)
SONDAGGIO: CPT9 **CAMPIONE:** C1 **PROFONDITA': m** 0,40 - 0,65

PROVA DI TAGLIO DIRETTO

Modalità di prova: Norma ASTM D3080-04

Provino n°:	1	2	3
Condizione del provino:	Indisturbato	Indisturbato	Indisturbato
Tempo di consolidazione (ore):	24	24	24
Pressione verticale (kPa):	100,0	200,0	300,0
Umidità iniziale e umidità finale (%):	25,9 26,3	26,0 25,0	25,8 24,2
Peso di volume (kN/m³):	19,0	19,0	19,0
Tipo di prova: Consolidata - lenta	Velocità di deformazione: 0,004 mm / min		

DIAGRAMMA
Tensione
Deformazione orizzontale

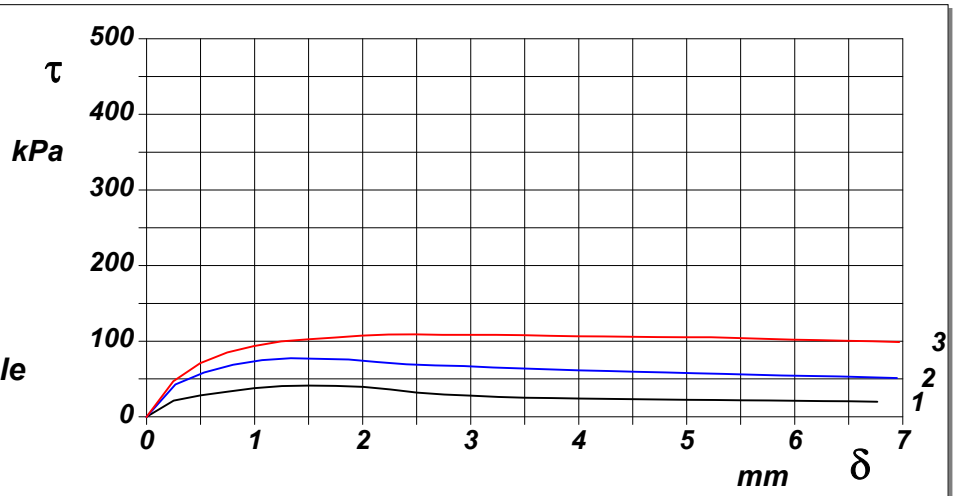
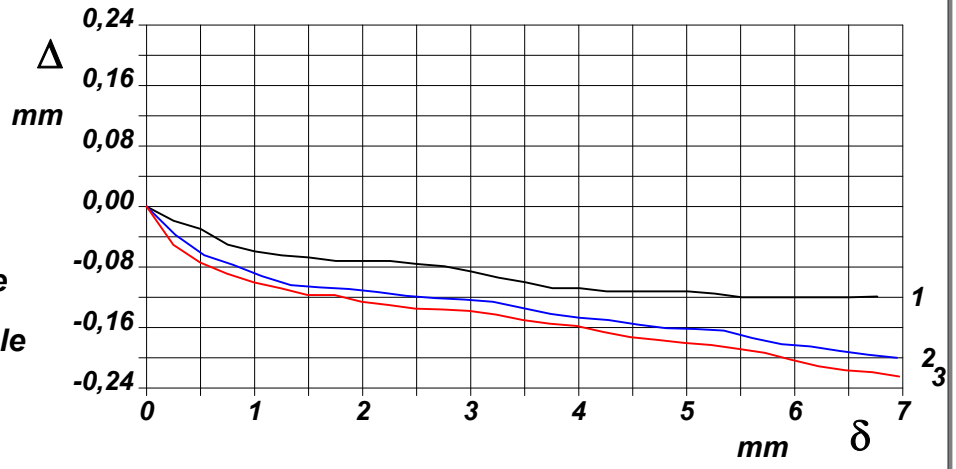


DIAGRAMMA
Deformazione verticale
Deformazione orizzontale



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RIFERIMENTO: Via Puglia - Loc. Biancolina - San Giovanni in Persiceto (BO)

SONDAGGIO: CPT9 **CAMPIONE:** C1 **PROFONDITA': m** 0,40 - 0,65

PROVA DI TAGLIO DIRETTO

Modalità di prova: Norma ASTM D3080-04

Provino 1			Provino 2			Provino 3		
Spostam. mm	Tensione kPa	Deform. vert. mm	Spostam. mm	Tensione kPa	Deform. vert. mm	Spostam. mm	Tensione kPa	Deform. vert. mm
0,251	21,3	-0,02	0,267	42,9	-0,04	0,249	46,9	-0,05
0,501	28,5	-0,03	0,534	58,5	-0,06	0,498	70,9	-0,07
0,752	33,4	-0,05	0,802	68,8	-0,08	0,746	85,0	-0,09
1,002	38,0	-0,06	1,069	74,9	-0,09	0,995	93,6	-0,10
1,253	40,7	-0,06	1,336	77,5	-0,10	1,244	99,7	-0,11
1,503	41,2	-0,07	1,603	76,8	-0,11	1,493	102,5	-0,12
1,754	40,8	-0,07	1,870	75,9	-0,11	1,742	104,7	-0,12
2,004	39,7	-0,07	2,138	72,3	-0,11	1,991	107,3	-0,13
2,255	36,1	-0,07	2,405	69,5	-0,12	2,239	108,9	-0,13
2,505	31,9	-0,08	2,672	67,8	-0,12	2,488	108,9	-0,14
2,756	29,4	-0,08	2,939	67,0	-0,12	2,737	108,4	-0,14
3,006	27,8	-0,09	3,206	65,2	-0,13	2,986	108,2	-0,14
3,257	26,2	-0,09	3,474	64,0	-0,13	3,235	108,2	-0,14
3,507	25,3	-0,10	3,741	62,7	-0,14	3,484	107,9	-0,15
3,758	24,6	-0,11	4,008	61,5	-0,15	3,732	107,1	-0,16
4,008	24,2	-0,11	4,275	60,4	-0,15	3,981	106,5	-0,16
4,259	23,7	-0,11	4,542	59,4	-0,16	4,230	106,4	-0,17
4,509	23,3	-0,11	4,810	58,7	-0,16	4,479	105,9	-0,17
4,760	22,9	-0,11	5,077	57,4	-0,16	4,728	105,4	-0,18
5,010	22,5	-0,11	5,344	56,8	-0,16	4,977	105,3	-0,18
5,261	22,2	-0,12	5,611	55,7	-0,17	5,225	105,1	-0,18
5,511	21,8	-0,12	5,878	54,6	-0,18	5,474	104,1	-0,19
5,762	21,6	-0,12	6,146	54,0	-0,19	5,723	103,2	-0,19
6,012	21,2	-0,12	6,413	53,2	-0,19	5,972	102,2	-0,20
6,263	20,7	-0,12	6,680	52,3	-0,20	6,221	101,5	-0,21
6,513	20,4	-0,12	6,947	51,3	-0,20	6,470	100,5	-0,22
6,764	20,0	-0,12				6,718	99,9	-0,22
						6,967	98,8	-0,22

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SONDAGGIO: CPT9 **CAMPIONE:** C1 **PROFONDITA': m** 0,40 - 0,65

PROVA DI TAGLIO DIRETTO - FASE DI CONSOLIDAZIONE

Modalità di prova: Norma ASTM D3080-04

Diagramma TEMPO - CEDIMENTO

PROVINO 1	
Pressione (kPa)	100
Altezza iniziale (cm)	2,000
Altezza finale (cm)	1,974
Sezione (cm²):	36,00
T_{100} (min)	7,8
Df (mm)	1
Vs (mm/min)	0,013

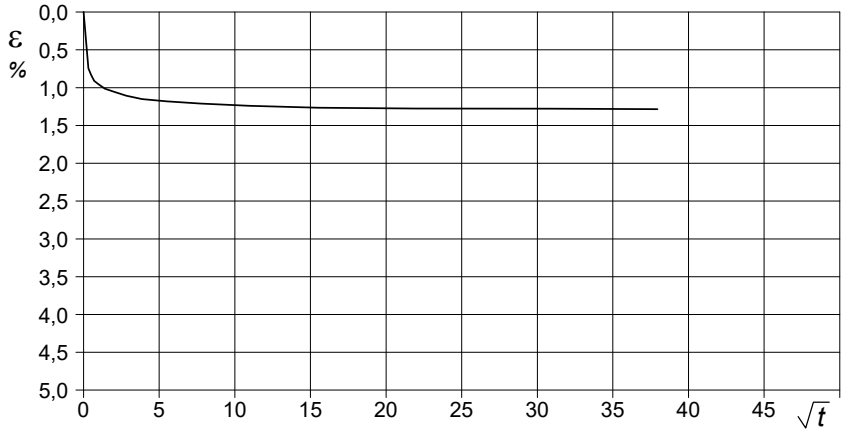


Diagramma TEMPO - CEDIMENTO

PROVINO 2	
Pressione (kPa)	200
Altezza iniziale (cm)	2,000
Altezza finale (cm)	1,925
Sezione (cm²):	36,00
T_{100} (min)	6,1
Df (mm)	1
Vs (mm/min)	0,017

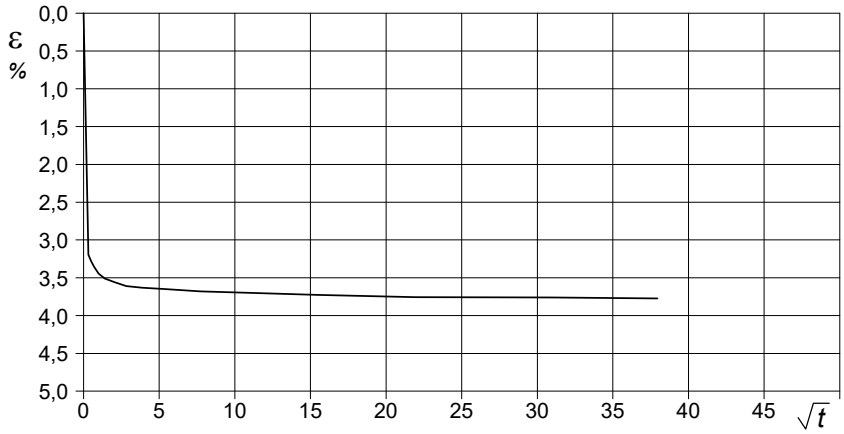
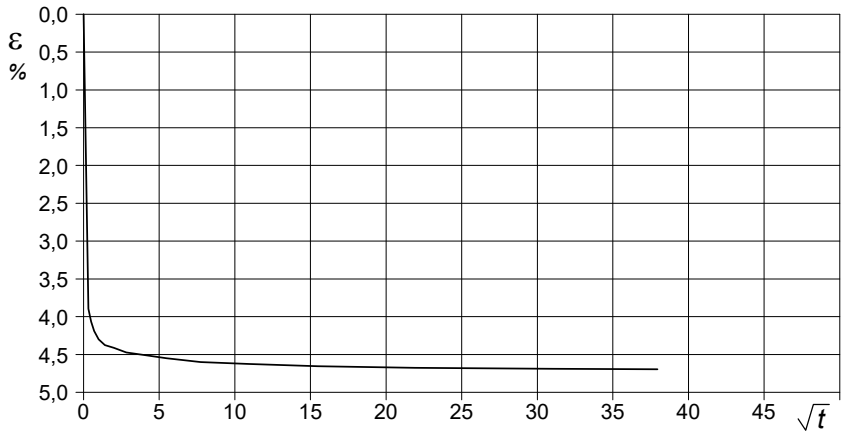


Diagramma TEMPO - CEDIMENTO

PROVINO 3	
Pressione (kPa)	300
Altezza iniziale (cm)	2,000
Altezza finale (cm)	1,906
Sezione (cm²):	36,00
T_{100} (min)	5,6
Df (mm)	2
Vs (mm/min)	0,036



Vs = Velocità stimata di prova Df = Deformazione a rottura stimata $tf = 10 \times T_{100}$ Vs = Df / tf

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SGEO - Laboratorio 7.0 - 2022

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PROVA DI TAGLIO DIRETTO - FASE DI CONSOLIDAZIONE

Modalità di prova: Norma ASTM D3080-04

Provino 1			Provino 2			Provino 3		
Tempo minuti	Cedim. mm/100	Cedim. %	Tempo minuti	Cedim. mm/100	Cedim. %	Tempo minuti	Cedim. mm/100	Cedim. %
0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
0,10	14,90	0,75	0,10	63,90	3,20	0,10	77,90	3,90
0,25	16,62	0,83	0,25	65,60	3,28	0,25	81,30	4,07
0,50	18,21	0,91	0,50	67,10	3,36	0,50	83,80	4,19
1,00	19,12	0,96	1,00	68,90	3,45	1,00	86,00	4,30
2,00	20,24	1,01	2,00	70,20	3,51	2,00	87,50	4,38
4,00	21,07	1,05	4,00	71,10	3,56	4,00	88,20	4,41
8,00	22,14	1,11	8,00	72,20	3,61	8,00	89,44	4,47
15,00	23,00	1,15	15,00	72,60	3,63	15,00	90,04	4,50
30,00	23,60	1,18	30,00	73,00	3,65	30,00	91,00	4,55
60,00	24,20	1,21	60,00	73,60	3,68	60,00	92,00	4,60
120,00	24,80	1,24	120,00	74,00	3,70	120,00	92,50	4,63
240,00	25,30	1,27	240,00	74,50	3,73	240,00	93,10	4,66
480,00	25,50	1,28	480,00	75,10	3,76	480,00	93,50	4,68
960,00	25,56	1,28	960,00	75,23	3,76	960,00	93,78	4,69
1440,00	25,68	1,28	1440,00	75,46	3,77	1440,00	93,90	4,70

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RIFERIMENTO: **Via Puglia - Loc. Biancolina - San Giovanni in Persiceto (BO)**		
SONDAGGIO: **CPT9**	***CAMPIONE:*** **C2**	***PROFONDITA': m*** **1,00 - 1,55**

MODULO RIASSUNTIVO

TAGLIO DIRETTO

Coesione:	***20,0***	***kPa***
Angolo di attrito interno:	***16,1***	***°***

FOTOGRAFIA

Posizione delle prove TD	*cm*	*Rp kPa*	*VT kPa*	*cm*	*DESCRIZIONE DEL CAMPIONE*
	0	120			**Argilla sabbiosa (f) limosa [ESAME VISIVO], di colore marrone-verdastro, consistente e a struttura omogena. Reagente all'HCl.**
	10				
	20	120			**Qualità del campione: Q5**
	30				
	40				
	50	130		55	

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CERTIFICATO DI PROVA N°: 00582	Pagina 1/4	DATA DI EMISSIONE: 28/02/24	Inizio analisi: 12/02/24
VERBALE DI ACCETTAZIONE N°: 027 del 09/02/24		Apertura campione: 12/02/24	Fine analisi: 19/02/24

COMMITTENTE: Geologo Zamboni Maurizio - Via dei Giardini, 11 - Monzuno (BO)
RIFERIMENTO: Via Puglia - Loc. Biancolina - San Giovanni in Persiceto (BO)
SONDAGGIO: CPT9 **CAMPIONE:** C2 **PROFONDITA': m** 1,00 - 1,55

PROVA DI TAGLIO DIRETTO

Modalità di prova: Norma ASTM D3080-04

Provino n°:	1	2	3
Condizione del provino:	Indisturbato	Indisturbato	Indisturbato
Tempo di consolidazione (ore):	24	24	24
Pressione verticale (kPa):	100,0	200,0	300,0
Umidità iniziale e umidità finale (%):	26,5 27,4	26,4 26,0	26,3 24,1
Peso di volume (kN/m³):	18,5	18,5	18,4

Tipo di prova: Consolidata - lenta — Velocità di deformazione: 0,004 mm / min

DIAGRAMMA
Tensione
Deformazione orizzontale

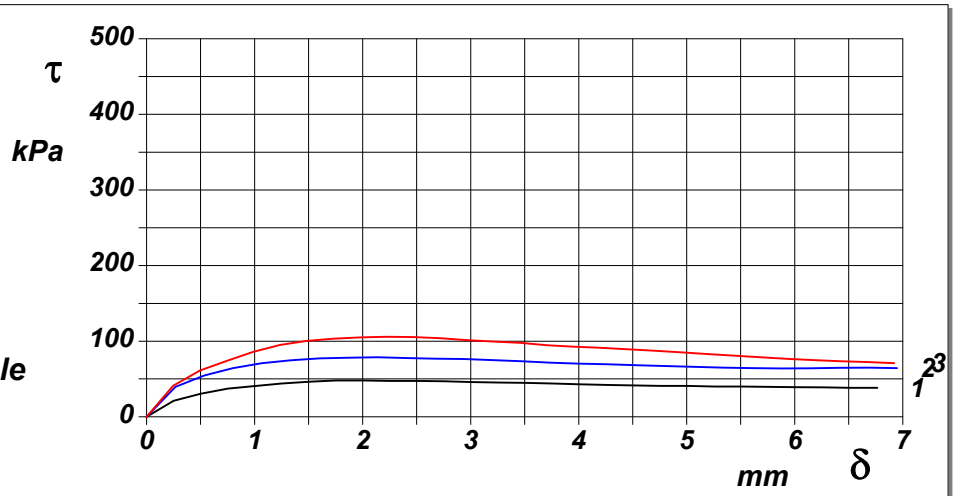
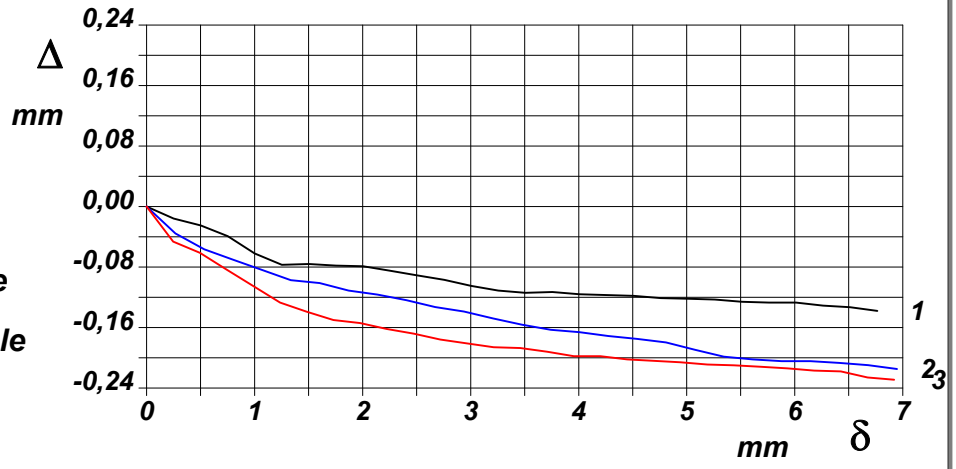


DIAGRAMMA
Deformazione verticale
Deformazione orizzontale



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Art. 59 DPR 380/2001- Circolare 7618/STC - Consiglio Superiore dei Lavori Pubblici
Certificazione ufficiale - Decreto 0000195.20-04-2023
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CERTIFICATO DI PROVA N°: 00582	Pagina 2/4	DATA DI EMISSIONE: 28/02/24	Inizio analisi: 12/02/24
VERBALE DI ACCETTAZIONE N°: 027 del 09/02/24		Apertura campione: 12/02/24	Fine analisi: 19/02/24

COMMITTENTE: Geologo Zamboni Maurizio - Via dei Giardini, 11 - Monzuno (BO)

RIFERIMENTO: Via Puglia - Loc. Biancolina - San Giovanni in Persiceto (BO)

SONDAGGIO: CPT9 **CAMPIONE:** C2 **PROFONDITA': m** 1,00 - 1,55

PROVA DI TAGLIO DIRETTO

Modalità di prova: Norma ASTM D3080-04

Provino 1			Provino 2			Provino 3		
Spostam. mm	Tensione kPa	Deform. vert. mm	Spostam. mm	Tensione kPa	Deform. vert. mm	Spostam. mm	Tensione kPa	Deform. vert. mm
0,251	21,1	-0,02	0,267	39,4	-0,04	0,247	41,1	-0,05
0,501	30,6	-0,03	0,534	54,7	-0,06	0,494	61,1	-0,06
0,752	37,2	-0,04	0,802	64,4	-0,07	0,741	73,9	-0,08
1,002	40,6	-0,06	1,069	70,8	-0,08	0,989	85,8	-0,11
1,253	44,2	-0,08	1,336	74,7	-0,10	1,236	95,0	-0,13
1,503	46,4	-0,08	1,603	77,2	-0,10	1,483	100,3	-0,14
1,754	48,1	-0,08	1,870	78,1	-0,11	1,730	103,3	-0,15
2,004	48,1	-0,08	2,138	78,6	-0,12	1,977	105,0	-0,15
2,255	47,5	-0,09	2,405	77,8	-0,12	2,224	105,8	-0,16
2,505	47,5	-0,09	2,672	76,9	-0,13	2,472	105,6	-0,17
2,756	46,9	-0,10	2,939	76,4	-0,14	2,719	103,9	-0,18
3,006	46,1	-0,11	3,206	75,0	-0,15	2,966	101,4	-0,18
3,257	45,3	-0,11	3,474	73,3	-0,16	3,213	99,4	-0,19
3,507	45,0	-0,11	3,741	71,7	-0,16	3,460	97,8	-0,19
3,758	44,2	-0,11	4,008	70,3	-0,17	3,707	94,7	-0,19
4,008	43,1	-0,12	4,275	69,4	-0,17	3,955	92,8	-0,20
4,259	42,2	-0,12	4,542	68,3	-0,18	4,202	91,1	-0,20
4,509	41,4	-0,12	4,810	67,2	-0,18	4,449	89,4	-0,20
4,760	40,8	-0,12	5,077	66,1	-0,19	4,696	87,5	-0,20
5,010	40,8	-0,12	5,344	65,0	-0,20	4,943	85,3	-0,21
5,261	40,0	-0,12	5,611	64,4	-0,20	5,190	83,1	-0,21
5,511	40,0	-0,13	5,878	63,9	-0,20	5,438	80,8	-0,21
5,762	39,7	-0,13	6,146	64,2	-0,20	5,685	78,9	-0,21
6,012	39,2	-0,13	6,413	64,7	-0,21	5,932	76,7	-0,21
6,263	38,9	-0,13	6,680	65,0	-0,21	6,179	75,0	-0,22
6,513	38,3	-0,13	6,947	64,4	-0,21	6,426	73,6	-0,22
6,764	38,3	-0,14				6,673	72,5	-0,23
						6,920	70,8	-0,23

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CERTIFICATO DI PROVA N°: 00582	Pagina 3/4	DATA DI EMISSIONE: 28/02/24	Inizio analisi: 12/02/24
VERBALE DI ACCETTAZIONE N°: 027 del 09/02/24		Apertura campione: 12/02/24	Fine analisi: 19/02/24

COMMITTENTE: Geologo Zamboni Maurizio - Via dei Giardini, 11 - Monzuno (BO)
RIFERIMENTO: Via Puglia - Loc. Biancolina - San Giovanni in Persiceto (BO)
SONDAGGIO: CPT9 **CAMPIONE:** C2 **PROFONDITA': m** 1,00 - 1,55

PROVA DI TAGLIO DIRETTO - FASE DI CONSOLIDAZIONE

Modalità di prova: Norma ASTM D3080-04

Diagramma TEMPO - CEDIMENTO

PROVINO 1	
Pressione (kPa)	100
Altezza iniziale (cm)	2,000
Altezza finale (cm)	1,939
Sezione (cm²):	36,00
T_{100} (min)	9,1
Df (mm)	2
Vs (mm/min)	0,022

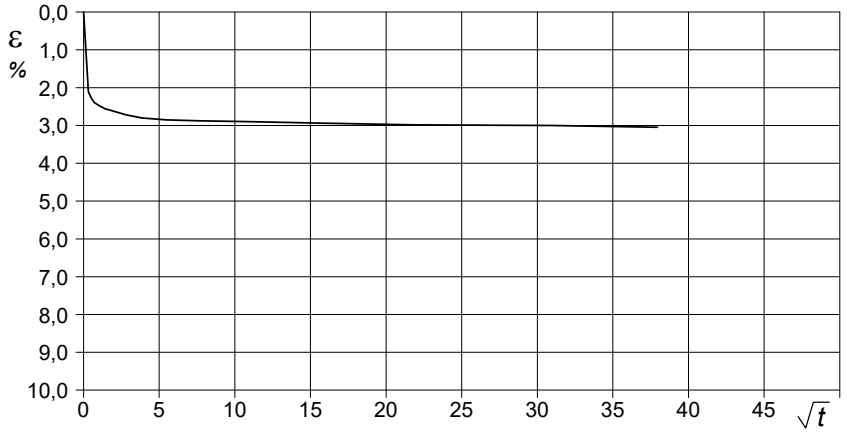


Diagramma TEMPO - CEDIMENTO

PROVINO 2	
Pressione (kPa)	200
Altezza iniziale (cm)	2,000
Altezza finale (cm)	1,898
Sezione (cm²):	36,00
T_{100} (min)	8,3
Df (mm)	2
Vs (mm/min)	0,024

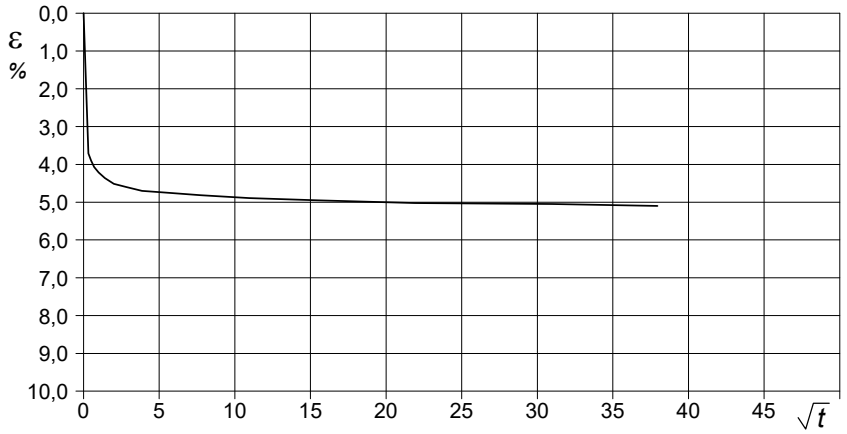
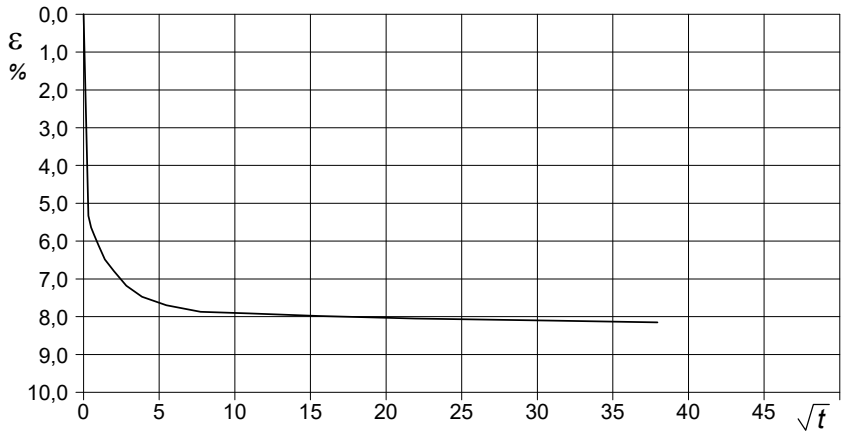


Diagramma TEMPO - CEDIMENTO

PROVINO 3	
Pressione (kPa)	300
Altezza iniziale (cm)	2,000
Altezza finale (cm)	1,837
Sezione (cm²):	36,00
T_{100} (min)	10,3
Df (mm)	2
Vs (mm/min)	0,019



Vs = Velocità stimata di prova Df = Deformazione a rottura stimata $tf = 10 \times T_{100}$ Vs = Df / tf

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SGEO - Laboratorio 7.0 - 2022

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CERTIFICATO DI PROVA N°: 00582	Pagina 4/4	DATA DI EMISSIONE: 28/02/24	Inizio analisi: 12/02/24
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COMMITTENTE: Geologo Zamboni Maurizio - Via dei Giardini, 11 - Monzuno (BO)
RIFERIMENTO: Via Puglia - Loc. Biancolina - San Giovanni in Persiceto (BO)
SONDAGGIO: CPT9 **CAMPIONE:** C2 **PROFONDITA': m** 1,00 - 1,55

PROVA DI TAGLIO DIRETTO - FASE DI CONSOLIDAZIONE

Modalità di prova: Norma ASTM D3080-04

Provino 1			Provino 2			Provino 3		
Tempo minuti	Cedim. mm/100	Cedim. %	Tempo minuti	Cedim. mm/100	Cedim. %	Tempo minuti	Cedim. mm/100	Cedim. %
0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
0,10	42,10	2,11	0,10	74,20	3,71	0,10	106,60	5,33
0,25	45,40	2,27	0,25	78,00	3,90	0,25	112,80	5,64
0,50	47,88	2,39	0,50	81,36	4,07	0,50	116,80	5,84
1,00	49,32	2,47	1,00	84,30	4,22	1,00	122,40	6,12
2,00	51,08	2,55	2,00	87,20	4,36	2,00	129,70	6,49
4,00	52,48	2,62	4,00	90,30	4,52	4,00	135,80	6,79
8,00	54,40	2,72	8,00	92,00	4,60	8,00	143,60	7,18
15,00	56,00	2,80	15,00	94,00	4,70	15,00	149,50	7,48
30,00	57,00	2,85	30,00	95,00	4,75	30,00	153,90	7,70
60,00	57,60	2,88	60,00	96,30	4,82	60,00	157,40	7,87
120,00	58,00	2,90	120,00	97,80	4,89	120,00	158,30	7,92
240,00	58,70	2,94	240,00	99,00	4,95	240,00	159,60	7,98
480,00	59,70	2,99	480,00	100,40	5,02	480,00	161,00	8,05
960,00	60,00	3,00	960,00	101,00	5,05	960,00	162,00	8,10
1440,00	61,00	3,05	1440,00	102,00	5,10	1440,00	163,00	8,15

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COMMITTENTE:	Geologo Zamboni Maurizio - Via dei Giardini, 11 - Monzuno (BO)
RIFERIMENTO:	Via Puglia - Loc. Biancolina - San Giovanni in Persiceto (BO)
SONDAGGIO: CPT4	*CAMPIONE:* C3 — *PROFONDITA': m* 1,30 - 1,60

MODULO RIASSUNTIVO

CARATTERISTICHE FISICHE

Umidità naturale	*29,3*	*%*
Peso di volume	*20,1*	*kN/m³*
Peso di volume secco	*15,5*	*kN/m³*
Peso di volume saturo	*0,0*	*kN/m³*

TAGLIO DIRETTO

Coesione:	*6,6*	*kPa*
Angolo di attrito interno:	*18,4*	*°*

FOTOGRAFIA

Posizione delle prove TD	cm	Rp kPa	VT kPa	cm	DESCRIZIONE DEL CAMPIONE
	0				Argilla limosa [ESAME VISIVO], di colore marrone, consistente e a struttura omogena. Reagente all'HCl.
	5	230			
	10				Qualità del campione: Q5
	15	230			
	20				
	25	220			
	30			30	

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CERTIFICATO DI PROVA N°: 00583	Pagina 1/4	DATA DI EMISSIONE: 28/02/24	Inizio analisi: 10/02/24
VERBALE DI ACCETTAZIONE N°: 027 del 09/02/24		Apertura campione: 09/02/24	Fine analisi: 17/02/24

COMMITTENTE: Geologo Zamboni Maurizio - Via dei Giardini, 11 - Monzuno (BO)
RIFERIMENTO: Via Puglia - Loc. Biancolina - San Giovanni in Persiceto (BO)
SONDAGGIO: CPT4 **CAMPIONE:** C3 **PROFONDITA': m** 1,30 - 1,60

PROVA DI TAGLIO DIRETTO

Modalità di prova: Norma ASTM D3080-04

Provino n°:	1	2	3
Condizione del provino:	Indisturbato	Indisturbato	Indisturbato
Tempo di consolidazione (ore):	24	24	24
Pressione verticale (kPa):	100,0	200,0	300,0
Umidità iniziale e umidità finale (%):	29,4 23,1	29,5 23,5	29,1 22,0
Peso di volume (kN/m³):	20,1	20,1	20,1
Tipo di prova: Consolidata - lenta	Velocità di deformazione: 0,004 mm / min		

DIAGRAMMA
Tensione
Deformazione orizzontale

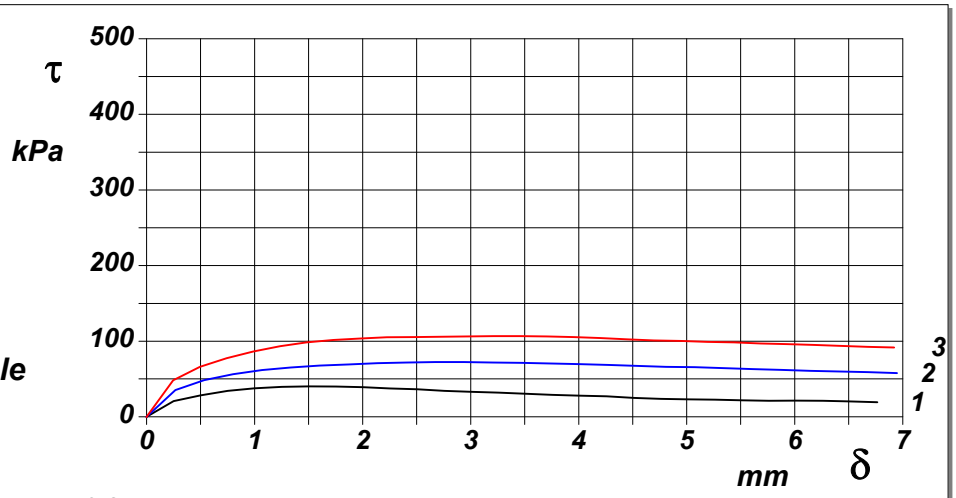
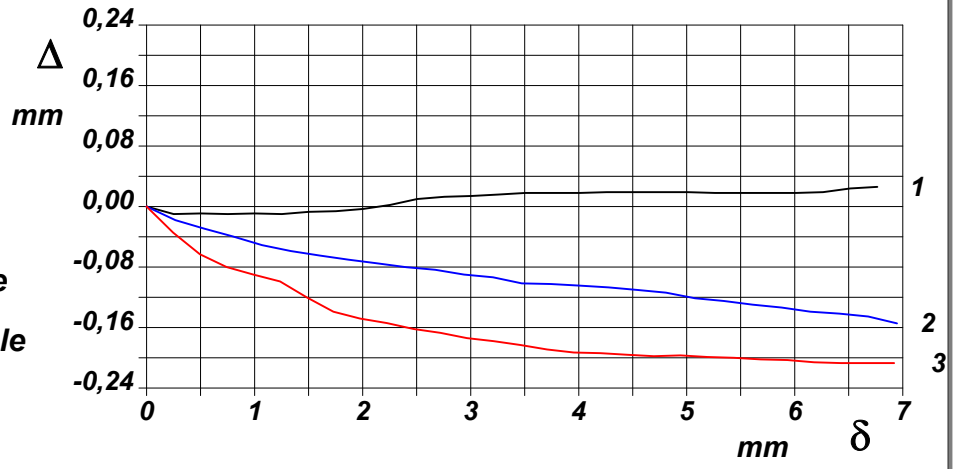


DIAGRAMMA
Deformazione verticale
Deformazione orizzontale



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CERTIFICATO DI PROVA N°: 00583	Pagina 2/4	DATA DI EMISSIONE: 28/02/24	Inizio analisi: 10/02/24
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COMMITTENTE: Geologo Zamboni Maurizio - Via dei Giardini, 11 - Monzuno (BO)
RIFERIMENTO: Via Puglia - Loc. Biancolina - San Giovanni in Persiceto (BO)
SONDAGGIO: CPT4 **CAMPIONE:** C3 **PROFONDITA': m** 1,30 - 1,60

PROVA DI TAGLIO DIRETTO

Modalità di prova: Norma ASTM D3080-04

Provino 1			Provino 2			Provino 3		
Spostam. mm	Tensione kPa	Deform. vert. mm	Spostam. mm	Tensione kPa	Deform. vert. mm	Spostam. mm	Tensione kPa	Deform. vert. mm
0,251	20,8	-0,01	0,267	35,4	-0,02	0,247	48,3	-0,03
0,501	28,3	-0,01	0,534	48,5	-0,03	0,494	66,1	-0,06
0,752	34,2	-0,01	0,802	56,3	-0,04	0,741	77,5	-0,08
1,002	37,8	-0,01	1,069	61,8	-0,05	0,989	86,4	-0,09
1,253	39,7	-0,01	1,336	65,3	-0,06	1,236	93,3	-0,10
1,503	40,3	-0,01	1,603	67,8	-0,06	1,483	98,3	-0,12
1,754	40,0	-0,01	1,870	69,3	-0,07	1,730	101,7	-0,14
2,004	39,2	0,00	2,138	70,9	-0,08	1,977	103,6	-0,15
2,255	37,5	0,00	2,405	71,8	-0,08	2,224	105,3	-0,15
2,505	36,4	0,01	2,672	72,4	-0,08	2,472	105,6	-0,16
2,756	34,4	0,01	2,939	72,4	-0,09	2,719	105,8	-0,17
3,006	33,1	0,01	3,206	71,8	-0,09	2,966	106,4	-0,17
3,257	31,9	0,02	3,474	71,2	-0,10	3,213	106,7	-0,18
3,507	30,6	0,02	3,741	70,5	-0,10	3,460	106,7	-0,18
3,758	29,2	0,02	4,008	69,6	-0,10	3,707	106,4	-0,19
4,008	28,1	0,02	4,275	68,7	-0,11	3,955	105,6	-0,19
4,259	27,2	0,02	4,542	67,4	-0,11	4,202	104,2	-0,19
4,509	25,0	0,02	4,810	66,2	-0,11	4,449	102,5	-0,20
4,760	23,6	0,02	5,077	65,6	-0,12	4,696	101,1	-0,20
5,010	23,1	0,02	5,344	64,3	-0,12	4,943	100,3	-0,20
5,261	22,5	0,02	5,611	63,1	-0,13	5,190	99,2	-0,20
5,511	21,9	0,02	5,878	62,2	-0,13	5,438	98,3	-0,20
5,762	21,1	0,02	6,146	60,9	-0,14	5,685	96,9	-0,20
6,012	21,4	0,02	6,413	60,0	-0,14	5,932	96,1	-0,20
6,263	21,1	0,02	6,680	59,1	-0,15	6,179	95,0	-0,21
6,513	20,3	0,02	6,947	57,8	-0,15	6,426	93,9	-0,21
6,764	19,2	0,03				6,673	92,5	-0,21
						6,920	91,7	-0,21

090-24

LO SPERIMENTATORE
dott. Geol. GRAZIANO Giuseppe Mario

IL DIRETTORE DEL LABORATORIO
dott. Geol. CARBONE Raffaele

laboratorio geoTecnico GeoTest s.a.s. di Carbone Andrea & C.
Via Lucca 55 A-B - 85025 MELFI (PZ)
tel/fax 0972347447 - laboratorio@geotest.it
http://www.geotest.it - P.IVA 01073440768

AZIENDA CON SISTEMA DI GESTIONE QUALITA' UNI EN ISO 9001:2015 CERTIFICATO DA CERTITALIA

Art. 59 DPR 380/2001- Circolare 7618/STC - Consiglio Superiore dei Lavori Pubblici
Certificazione ufficiale - Decreto 0000195.20-04-2023
SETTORE «A» Prove di laboratorio sulle TERRE • Prove Cicliche e Dinamiche (RC - TTC - TXC) • Prove di Carico su Piastra • Densità in sito
SETTORE «B» Prove di laboratorio su ROCCE e AGGREGATI

CERTIFICATO DI PROVA N°: 00583	Pagina 3/4	DATA DI EMISSIONE: 28/02/24	Inizio analisi: 10/02/24
VERBALE DI ACCETTAZIONE N°: 027 del 09/02/24		Apertura campione: 09/02/24	Fine analisi: 17/02/24

COMMITTENTE: Geologo Zamboni Maurizio - Via dei Giardini, 11 - Monzuno (BO)
RIFERIMENTO: Via Puglia - Loc. Biancolina - San Giovanni in Persiceto (BO)
SONDAGGIO: CPT4 **CAMPIONE:** C3 **PROFONDITA': m** 1,30 - 1,60

PROVA DI TAGLIO DIRETTO - FASE DI CONSOLIDAZIONE

Modalità di prova: Norma ASTM D3080-04

Diagramma TEMPO - CEDIMENTO

PROVINO 1	
Pressione (kPa)	100
Altezza iniziale (cm)	2,000
Altezza finale (cm)	1,972
Sezione (cm²):	36,00
T_{100} (min)	8,1
Df (mm)	2
Vs (mm/min)	0,025

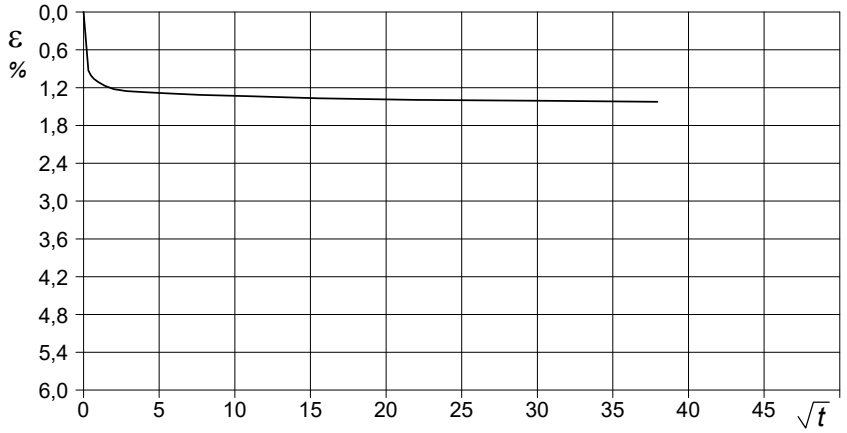


Diagramma TEMPO - CEDIMENTO

PROVINO 2	
Pressione (kPa)	200
Altezza iniziale (cm)	2,000
Altezza finale (cm)	1,934
Sezione (cm²):	36,00
T_{100} (min)	31,2
Df (mm)	3
Vs (mm/min)	0,010

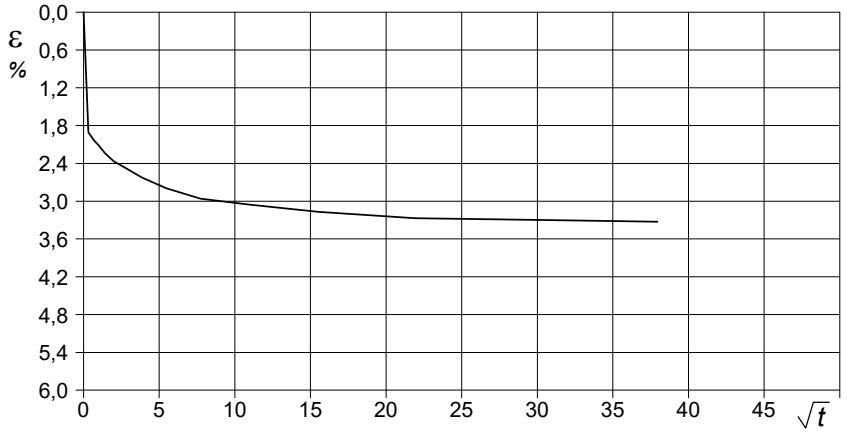
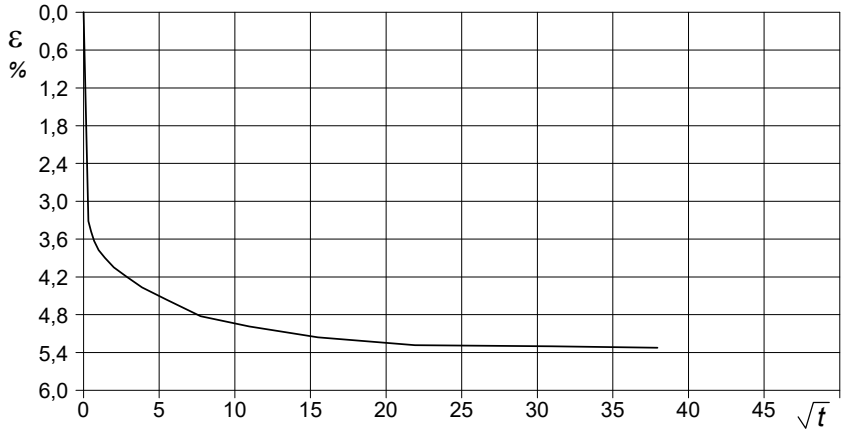


Diagramma TEMPO - CEDIMENTO

PROVINO 3	
Pressione (kPa)	300
Altezza iniziale (cm)	2,000
Altezza finale (cm)	1,894
Sezione (cm²):	36,00
T_{100} (min)	20,6
Df (mm)	3
Vs (mm/min)	0,015



Vs = Velocità stimata di prova Df = Deformazione a rottura stimata $tf = 10 \times T_{100}$ Vs = Df / tf

090-24

SGEO - Laboratorio 7.0 - 2022

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COMMITTENTE: Geologo Zamboni Maurizio - Via dei Giardini, 11 - Monzuno (BO)
RIFERIMENTO: Via Puglia - Loc. Biancolina - San Giovanni in Persiceto (BO)
SONDAGGIO: CPT4 **CAMPIONE:** C3 **PROFONDITA': m** 1,30 - 1,60

PROVA DI TAGLIO DIRETTO - FASE DI CONSOLIDAZIONE

Modalità di prova: Norma ASTM D3080-04

Provino 1			Provino 2			Provino 3		
Tempo minuti	Cedim. mm/100	Cedim. %	Tempo minuti	Cedim. mm/100	Cedim. %	Tempo minuti	Cedim. mm/100	Cedim. %
0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
0,10	18,60	0,93	0,10	38,10	1,91	0,10	66,30	3,32
0,25	20,20	1,01	0,25	39,40	1,97	0,25	69,63	3,48
0,50	21,30	1,07	0,50	40,80	2,04	0,50	72,61	3,63
1,00	22,30	1,12	1,00	42,30	2,12	1,00	75,50	3,78
2,00	23,43	1,17	2,00	44,70	2,24	2,00	77,97	3,90
4,00	24,46	1,22	4,00	47,40	2,37	4,00	81,00	4,05
8,00	25,10	1,25	8,00	49,60	2,48	8,00	83,90	4,20
15,00	25,40	1,27	15,00	52,50	2,63	15,00	87,30	4,37
30,00	25,80	1,29	30,00	55,90	2,80	30,00	91,20	4,56
60,00	26,30	1,32	60,00	59,20	2,96	60,00	96,50	4,83
120,00	26,70	1,34	120,00	61,10	3,06	120,00	99,70	4,99
240,00	27,40	1,37	240,00	63,40	3,17	240,00	103,20	5,16
480,00	27,90	1,40	480,00	65,40	3,27	480,00	105,70	5,29
960,00	28,20	1,41	960,00	66,00	3,30	960,00	106,00	5,30
1440,00	28,50	1,43	1440,00	66,50	3,33	1440,00	106,50	5,33

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LO SPERIMENTATORE
dott. Geol. GRAZIANO Giuseppe Mario

IL DIRETTORE DEL LABORATORIO
dott. Geol. CARBONE Raffaele

ALLEGATO IV

- SISMICA -

REPORT TOMOGRAFIA SISMICA
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PARAMETRI SISMICI
--

TROMINO
www.moho.world

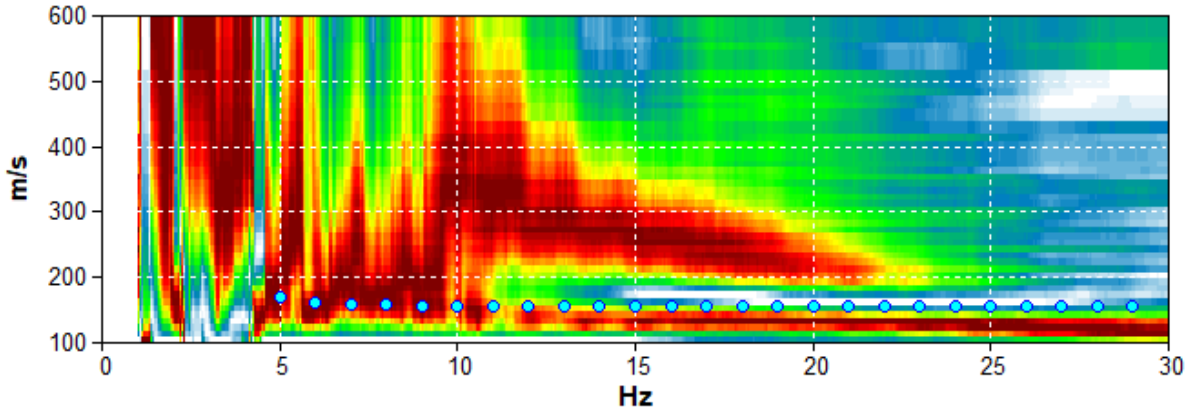
BIANCOLINA, BIANCOLINA

Inizio registrazione: 25/01/2024 15:28:39 Fine registrazione: 25/01/2024 15:32:52
Durata registrazione: 0h04'12".
Freq. campionamento: 256 Hz

Nomi canali: TR1+ TR1- ; TR2+ TR2- ; TR3+ TR3- ; TR4+ TR4- ; TR5+ TR5- ; TR6+ TR6- ; TR7+ TR7- ; TR8+ TR8-

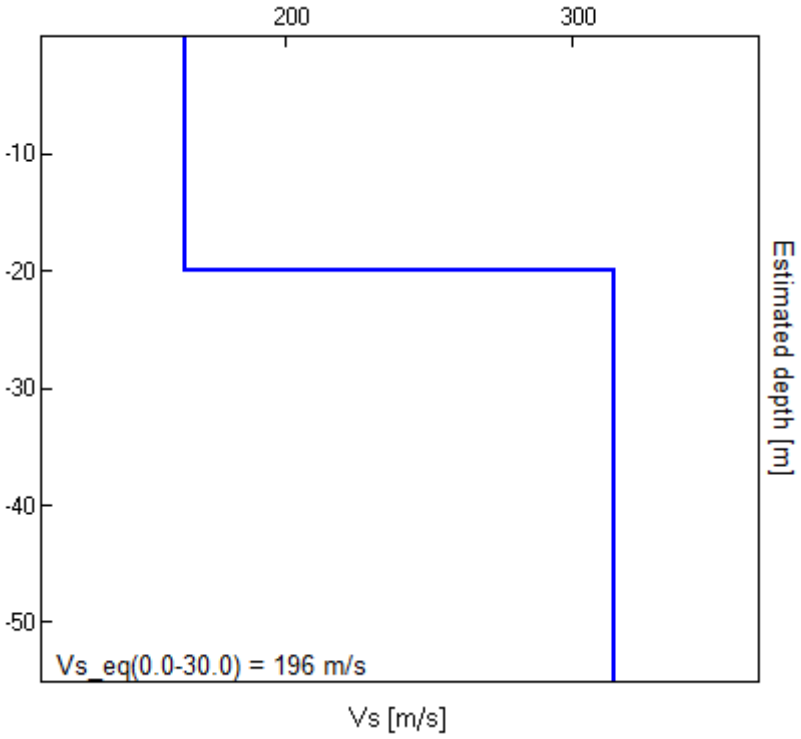
Array geometry (x): 0.0 3.0 6.0 9.0 12.0 15.0 18.0 21.0 m.

MODELLED RAYLEIGH WAVE PHASE VELOCITY DISPERSION CURVE



Depth at the bottom of the layer [m]	Thickness [m]	Vs [m/s]	Poisson ratio
20.00	20.00	165	0.42
inf.	inf.	315	0.42

Vs_eq(0.0-30.0) = 196 m/s


200
300
-10
-20
-30
-40
-50
Estimated depth [m]
Vs_eq(0.0-30.0) = 196 m/s
Vs [m/s]

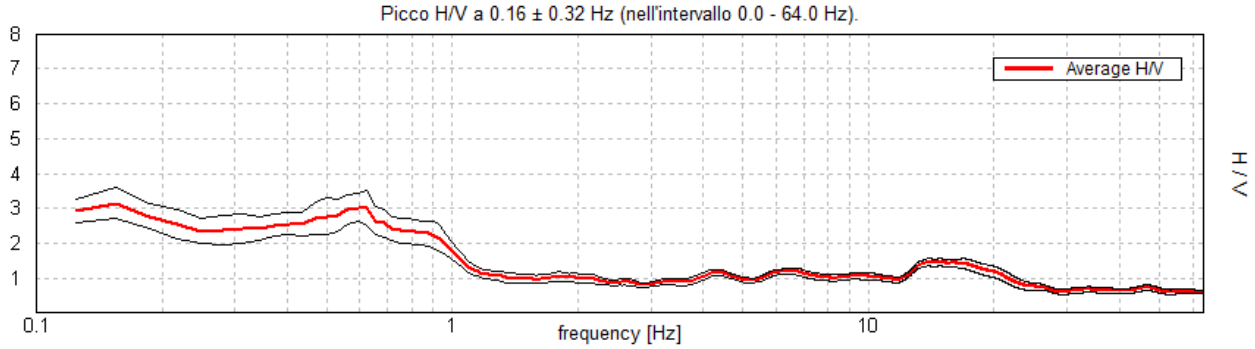
TROMINO
www.moho.world

BIANCOLINA, SGP 1

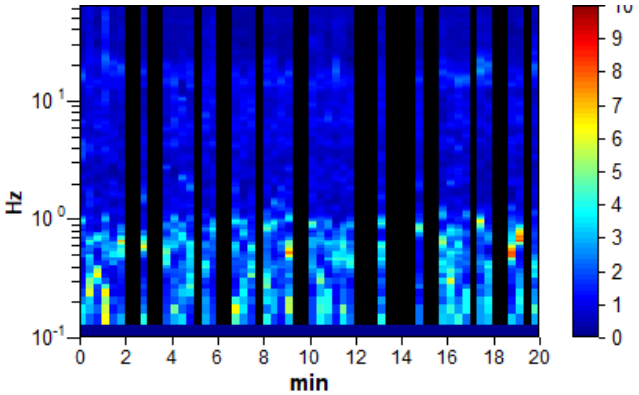
Strumento: TZB-0127/01-20
Formato dati: 32 bit
Fondo scala [mV]: 179
Inizio registrazione: 24/01/2024 14:50:42 Fine registrazione: 24/01/2024 15:10:42
Nomi canali: NORTH SOUTH; EAST WEST ; UP DOWN
Dato GPS non disponibile

Durata registrazione: 0h20'00". Analizzato 62% tracciato (selezione manuale)
Freq. campionamento: 128 Hz
Lunghezza finestre: 20 s
Tipo di lisciamento: Triangular window
Lisciamento: 10%

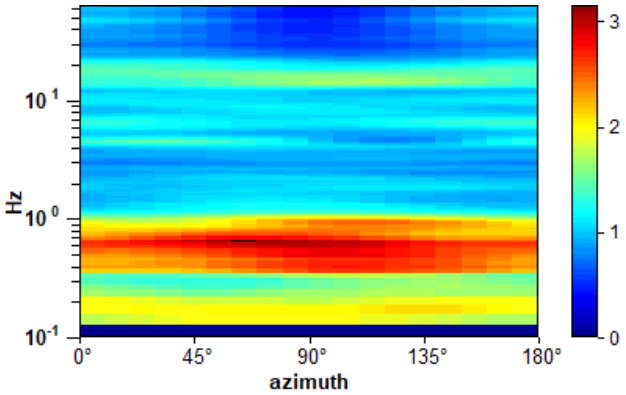
RAPPORTO SPETTRALE ORIZZONTALE SU VERTICALE



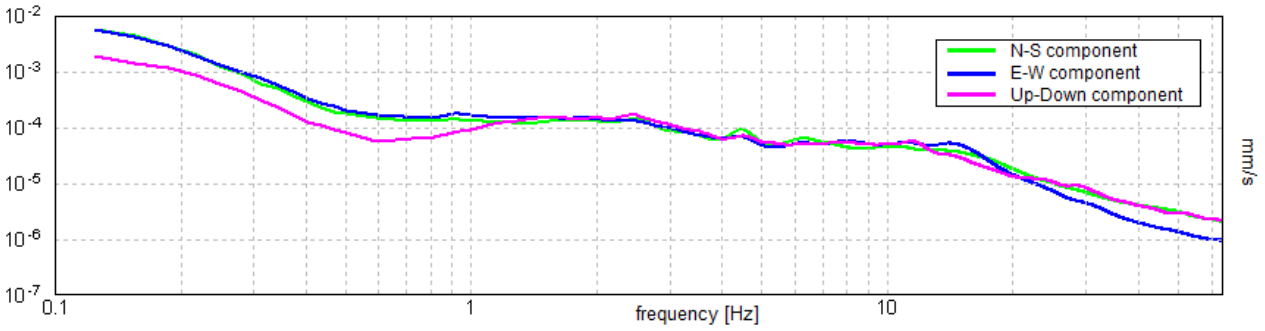
SERIE TEMPORALE H/V



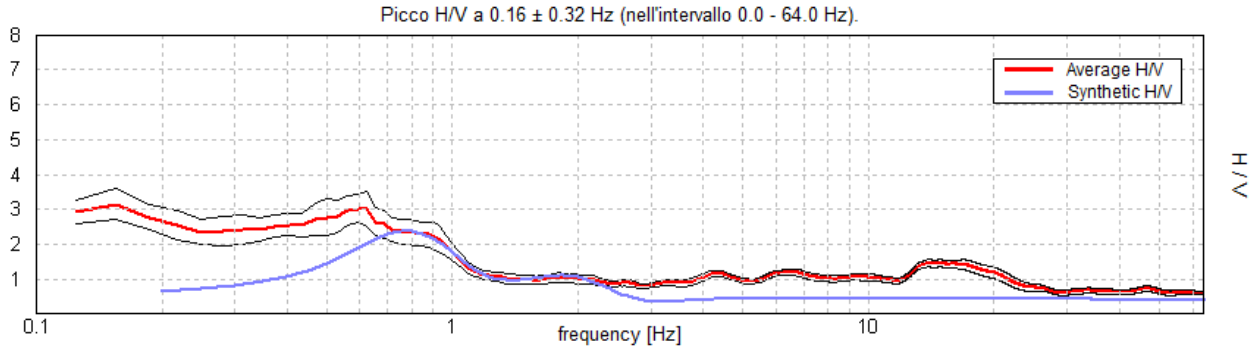
DIREZIONALITA' H/V



SPETTRI DELLE SINGOLE COMPONENTI

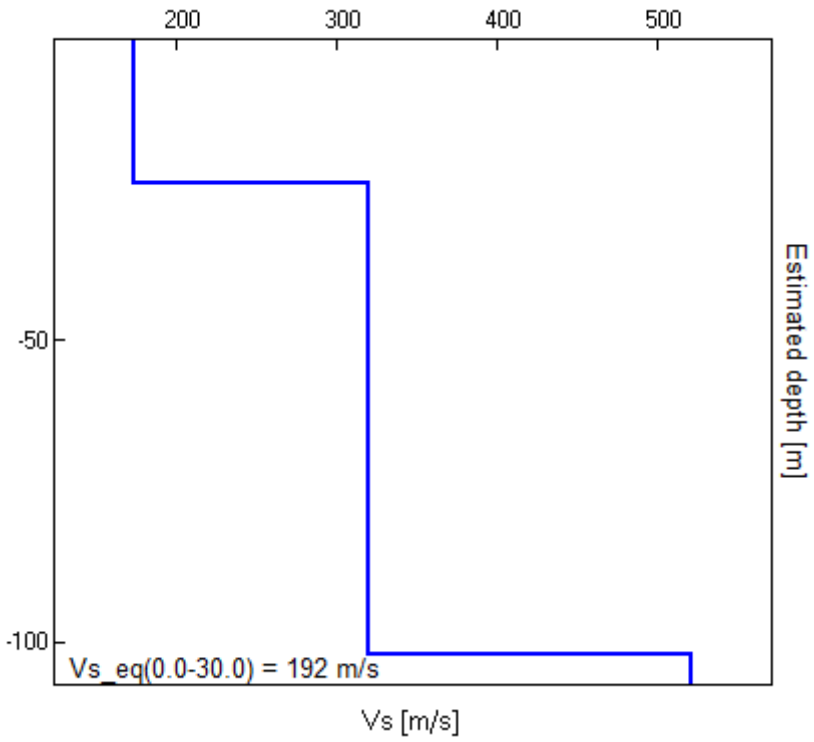


H/V SPERIMENTALE vs. H/V SINTETICO



Profondità alla base dello strato [m]	Spessore [m]	Vs [m/s]	Rapporto di Poisson
24.00	24.00	175	0.42
102.00	78.00	320	0.42
inf.	inf.	520	0.42

Vs_eq(0.0-30.0) = 192 m/s



[Secondo le linee guida SESAME, 2005. **Si raccomanda di leggere attentamente il manuale di** *Grilla* **prima di interpretare la tabella seguente**].

Picco H/V a 0.16 ± 0.32 Hz (nell'intervallo 0.0 - 64.0 Hz).

Criteri per una curva H/V affidabile [Tutti 3 dovrebbero risultare soddisfatti]			
$f_0 > 10 / L_w$	0.16 > 0.50		**NO**
$n_c(f_0) > 200$	115.6 > 200		**NO**
$\sigma_A(f) < 2$ per $0.5f_0 < f < 2f_0$ se $f_0 > 0.5$Hz **$\sigma_A(f) < 3$ per $0.5f_0 < f < 2f_0$ se $f_0 < 0.5$Hz**	Superato 0 volte su 9	**OK**	
Criteri per un picco H/V chiaro [Almeno 5 su 6 dovrebbero essere soddisfatti]			
Esiste f^- in $[f_0/4, f_0]$ | $A_{H/V}(f^-) < A_0 / 2$	0.094 Hz	**OK**	
Esiste f^+ in $[f_0, 4f_0]$ | $A_{H/V}(f^+) < A_0 / 2$			**NO**
$A_0 > 2$	3.14 > 2	**OK**	
$f_{picco}[A_{H/V}(f) \pm \sigma_A(f)] = f_0 \pm 5\%$	|2.06725| < 0.05		**NO**
$\sigma_f < \varepsilon(f_0)$	0.32301 < 0.03906		**NO**
$\sigma_A(f_0) < \theta(f_0)$	0.4436 < 3.0	**OK**	

L_w	lunghezza della finestra
n_w	numero di finestre usate nell'analisi
$n_c = L_w n_w f_0$	numero di cicli significativi
f	frequenza attuale
f_0	frequenza del picco H/V
σ_f	deviazione standard della frequenza del picco H/V
$\varepsilon(f_0)$	valore di soglia per la condizione di stabilità $\sigma_f < \varepsilon(f_0)$
A_0	ampiezza della curva H/V alla frequenza f_0
$A_{H/V}(f)$	ampiezza della curva H/V alla frequenza f
f^-	frequenza tra $f_0/4$ e f_0 alla quale $A_{H/V}(f^-) < A_0/2$
f^+	frequenza tra f_0 e $4f_0$ alla quale $A_{H/V}(f^+) < A_0/2$
$\sigma_A(f)$	deviazione standard di $A_{H/V}(f)$, $\sigma_A(f)$ è il fattore per il quale la curva $A_{H/V}(f)$ media deve essere moltiplicata o divisa
$\sigma_{logH/V}(f)$	deviazione standard della funzione log $A_{H/V}(f)$
$\theta(f_0)$	valore di soglia per la condizione di stabilità $\sigma_A(f) < \theta(f_0)$

Valori di soglia per σ_f e $\sigma_A(f_0)$					
Intervallo di freq. [Hz]	< 0.2	0.2 – 0.5	0.5 – 1.0	1.0 – 2.0	> 2.0
$\varepsilon(f_0)$ [Hz]	0.25 f_0	0.2 f_0	0.15 f_0	0.10 f_0	0.05 f_0
$\theta(f_0)$ per $\sigma_A(f_0)$	3.0	2.5	2.0	1.78	1.58
log $\theta(f_0)$ per $\sigma_{logH/V}(f_0)$	0.48	0.40	0.30	0.25	0.20

Parametri sismici

determinati con **GeoStru PS**

Le coordinate geografiche espresse in questo file sono in ED50

Tipo di elaborazione:Stabilità dei pendii

Sito in esame.

latitudine: 44,651083 [°]

longitudine: 11,227753 [°]

Classe d'uso: II. Costruzioni il cui uso preveda normali affollamenti, senza contenuti pericolosi per l'ambiente e senza funzioni pubbliche e sociali essenziali. Industrie con attività non pericolose per l'ambiente. Ponti, opere infrastrutturali, reti viarie non ricadenti in Classe d'uso III o in Classe d'uso IV, reti ferroviarie la cui interruzione non provochi situazioni di emergenza. Dighe il cui collasso non provochi conseguenze rilevanti.

Vita nominale: 50 [anni]

Tipo di interpolazione: Media ponderata

Siti di riferimento.

	ID	Latitudine [°]	Longitudine [°]	Distanza [m]
Sito 1	16062	44,662290	11,171630	4610,7
Sito 2	16063	44,663640	11,241840	1786,4
Sito 3	16285	44,613660	11,243670	4347,7
Sito 4	16284	44,612310	11,173560	6080,9

Parametri sismici

Categoria sottosuolo: C

Categoria topografica: T1

Periodo di riferimento: 50 anni

Coefficiente cu: 1

	Prob. superamento [%]	Tr [anni]	ag [g]	Fo [-]	Tc* [s]
Operatività (SLO)	81	30	0,048	2,477	0,256
Danno (SLD)	63	50	0,059	2,515	0,271
Salvaguardia della vita (SLV)	10	475	0,160	2,563	0,276
Prevenzione dal collasso (SLC)	5	975	0,212	2,517	0,282

Coefficienti Sismici Stabilità dei pendii

	Ss [-]	Cc [-]	St [-]	Kh [-]	Kv [-]	Amax [m/s²]	Beta [-]
SLO	1,500	1,650	1,000	0,014	0,007	0,699	0,200
SLD	1,500	1,620	1,000	0,018	0,009	0,862	0,200
SLV	1,450	1,610	1,000	0,056	0,028	2,280	0,240
SLC	1,380	1,590	1,000	0,082	0,041	2,870	0,280

Geostru

ALLEGATO V

- REPORT VERIFICA LIQUEFAZIONE -

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Vertical settlements data report 616
Strength loss data report 626

Dott. geol. Maurizio Zamboni
Corso Esperanto, 3/h
40065 Pianoro (BO)
geologozamboni@gmail.com

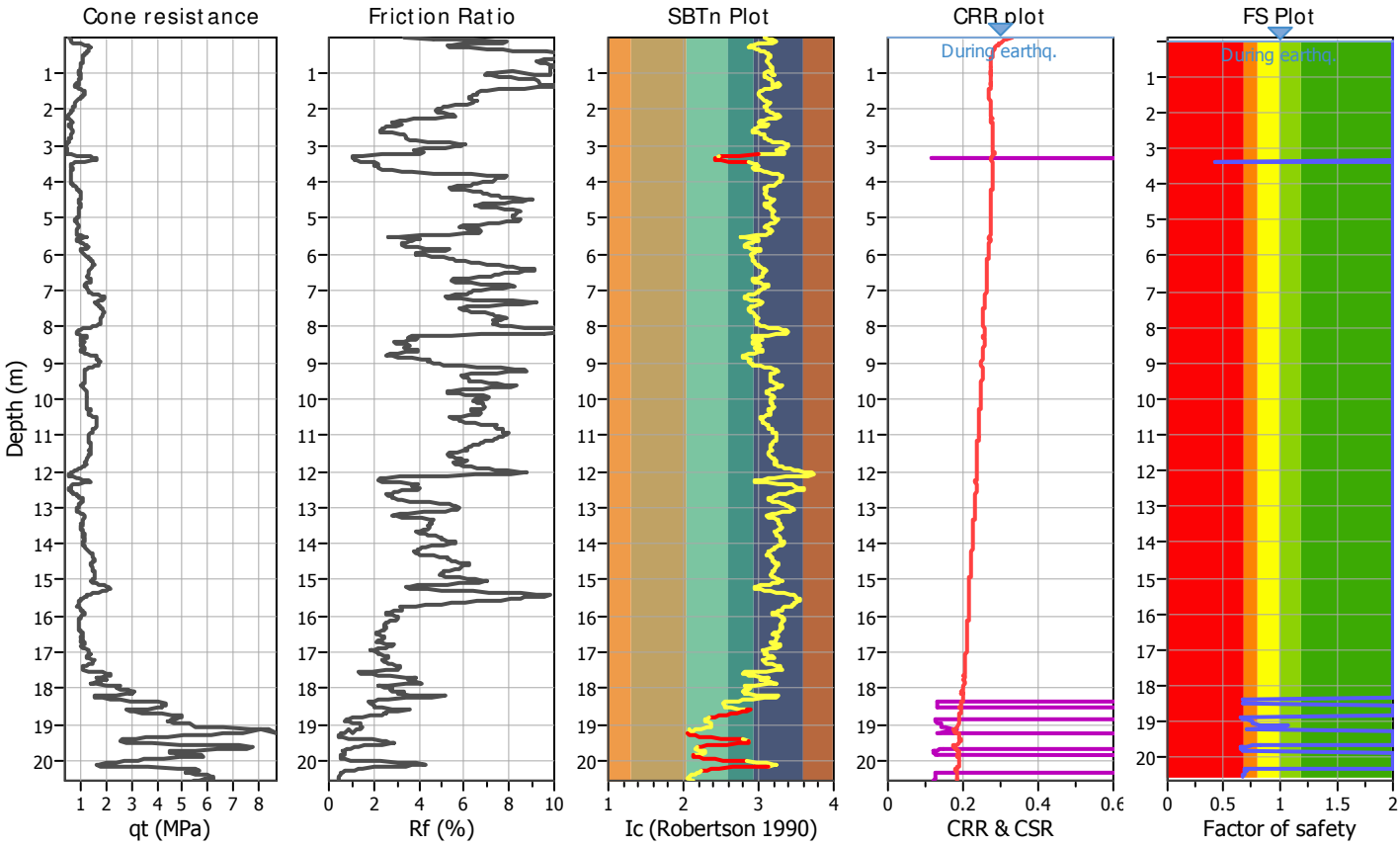
LIQUEFACTION ANALYSIS REPORT

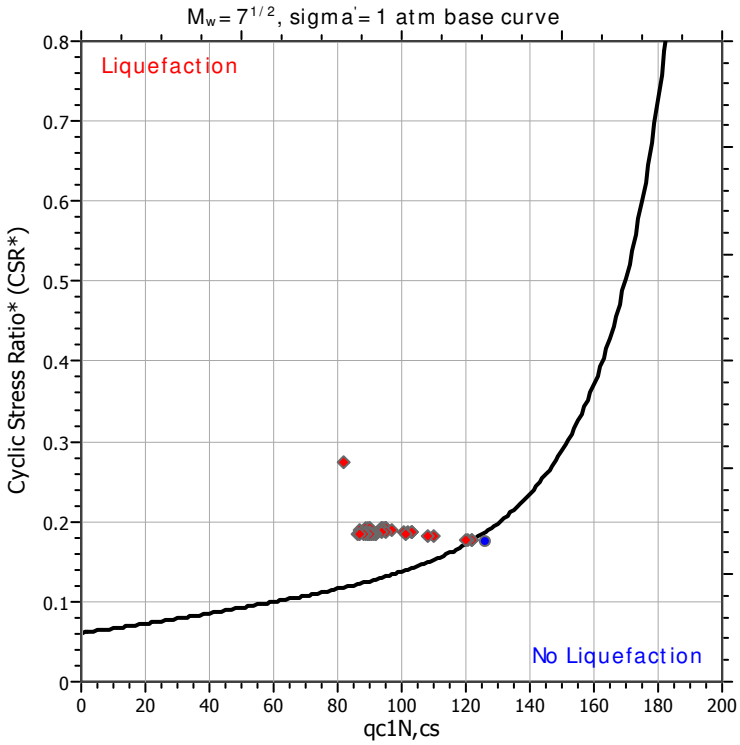
Project title : Location :

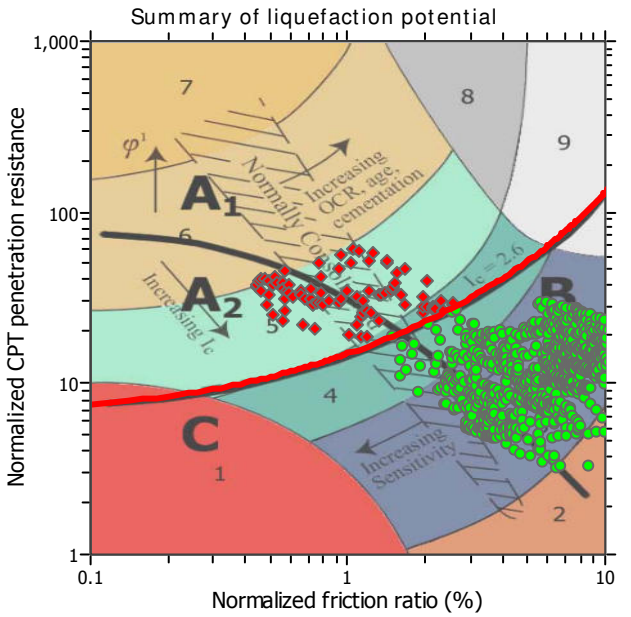
CPT file : CPTu-01_Biancolina

Input parameters and analysis data

Analysis method:	B&I (2014)	G.W.T. (in-situ):	0.60 m	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	0.00 m	Fill height:	N/A	Limit depth applied:	No
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	N/A
Earthquake magnitude M_w:	6.14	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.23	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		

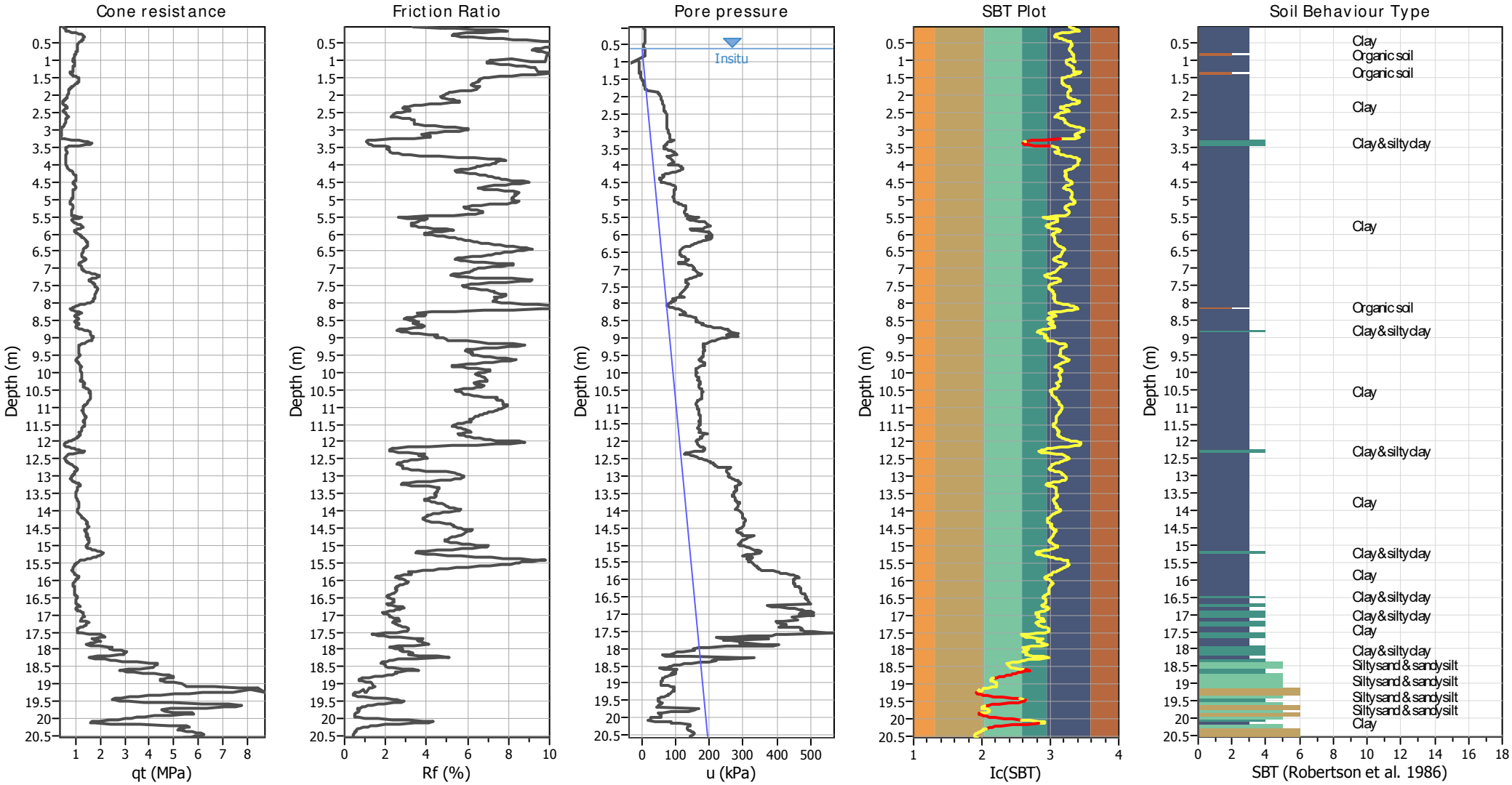






Zone A_1: Cyclic liquefaction likely depending on size and duration of cyclic loading
Zone A_2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



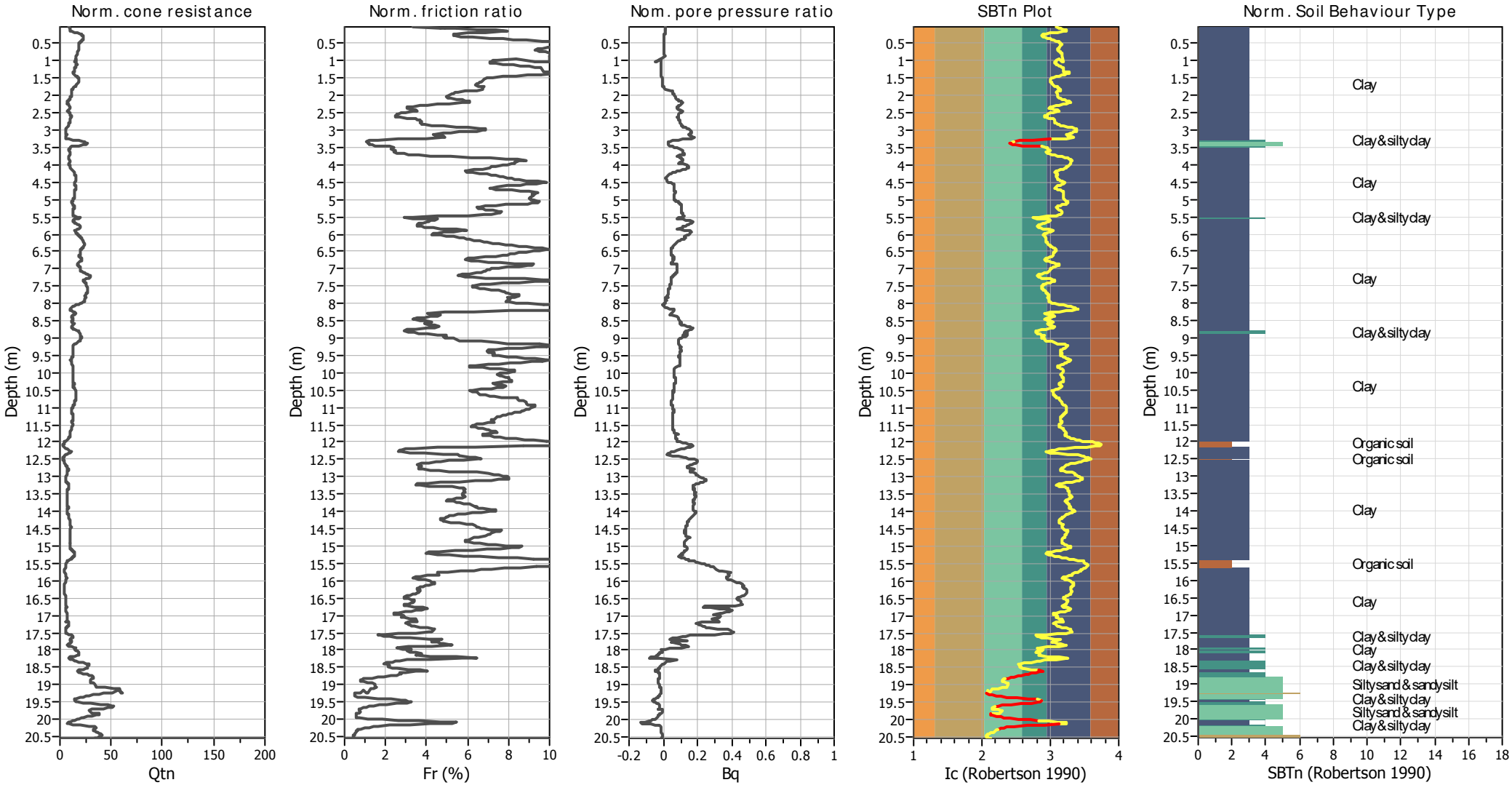
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	0.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.23	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	0.60 m	Fill height:	N/A	Limit depth:	N/A

SBT legend

1. Sensitive fine grained	4. Clayey silt to silty	7. Gravely sand to sand
2. Organic material	5. Silty sand to sandy silt	8. Very stiff sand to
3. Clay to silty clay	6. Clean sand to silty sand	9. Very stiff fine grained

CPT basic interpretation plots (normalized)



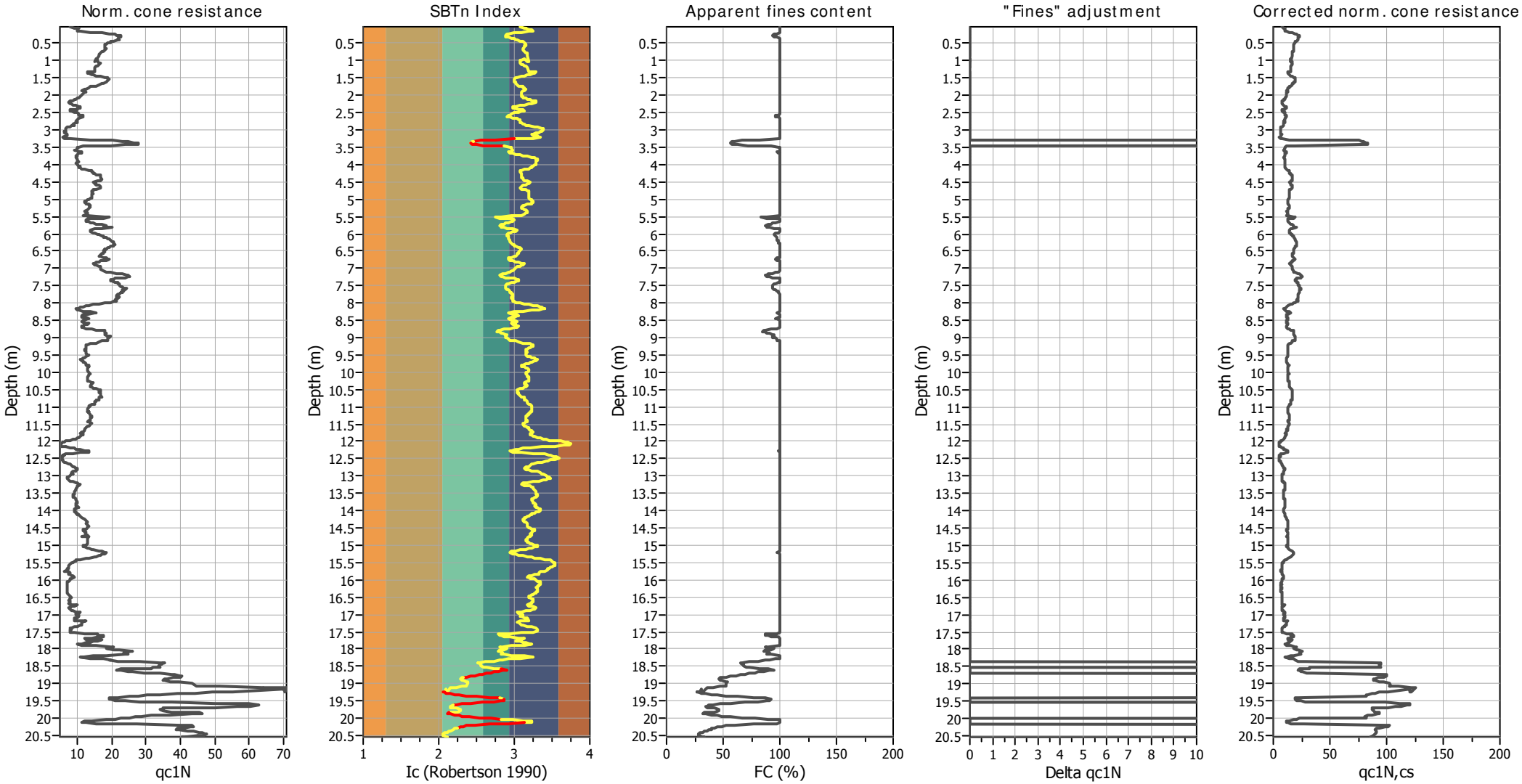
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	0.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.23	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	0.60 m	Fill height:	N/A	Limit depth:	N/A

SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

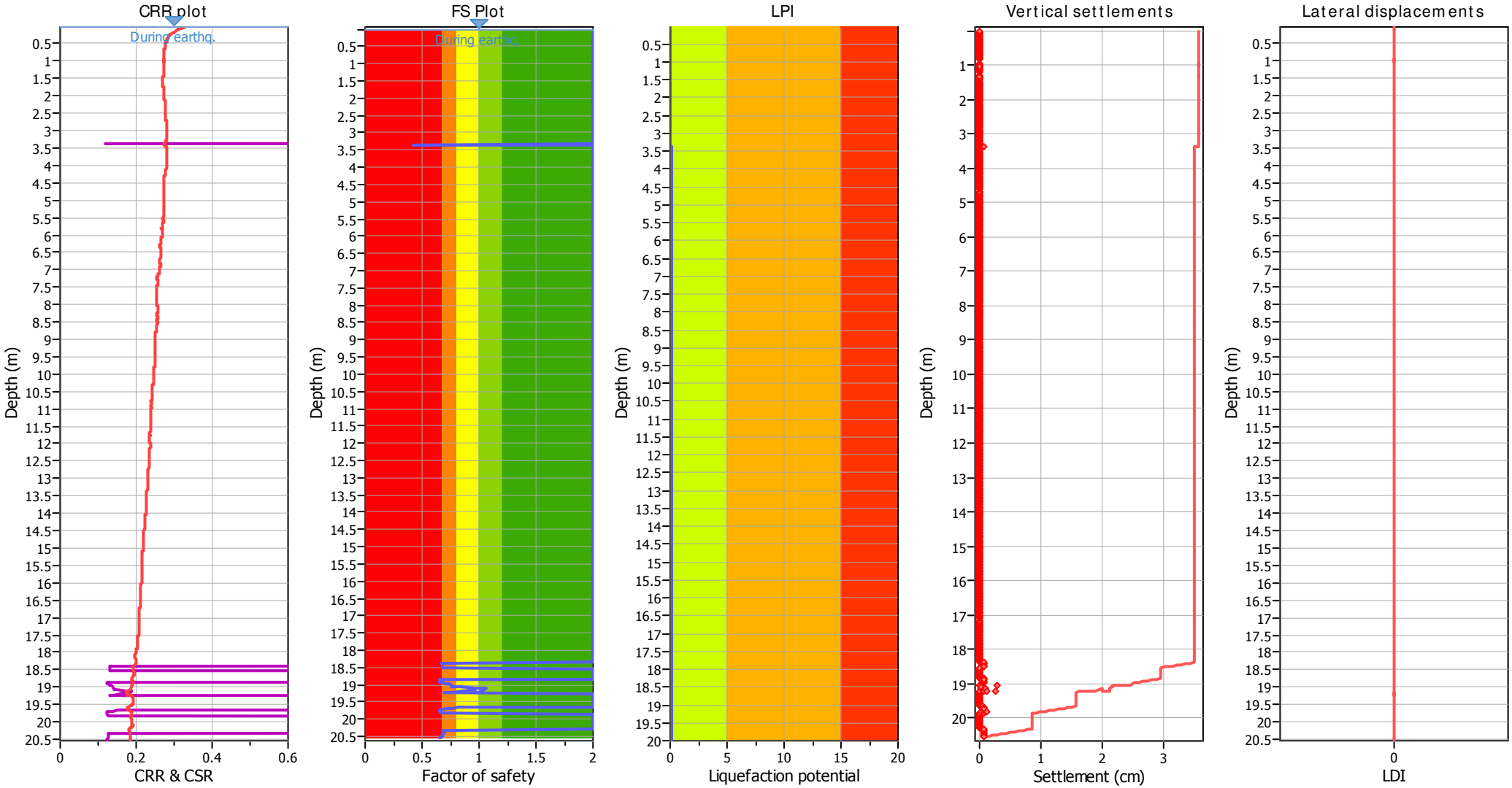
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	0.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.23	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	0.60 m	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	0.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.23	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	0.60 m	Fill height:	N/A	Limit depth:	N/A

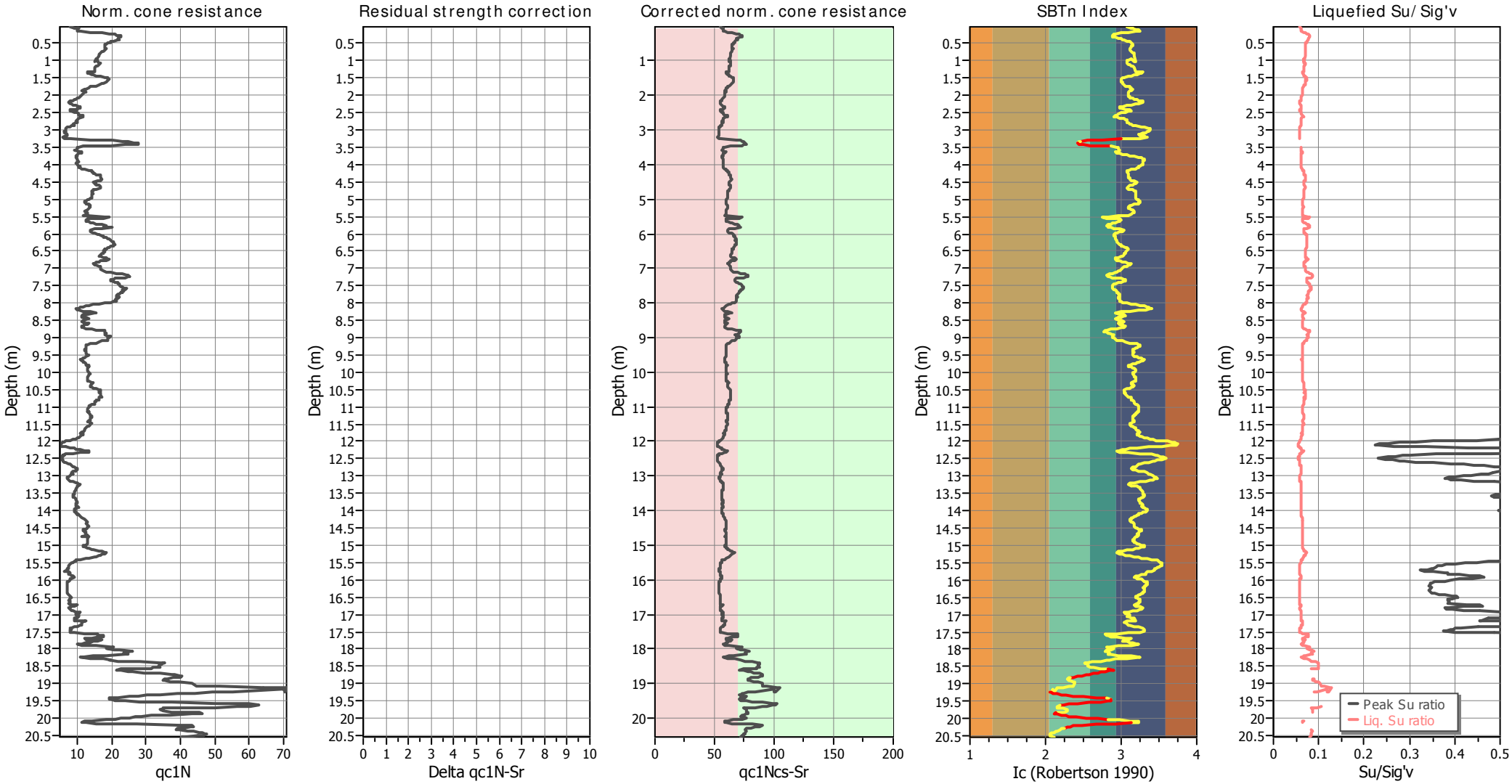
F.S. color scheme

- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

LPI color scheme

- Very high risk
- High risk
- Low risk

Check for strength loss plots (Idriss & Boulanger (2008))



Input parameters and analysis data

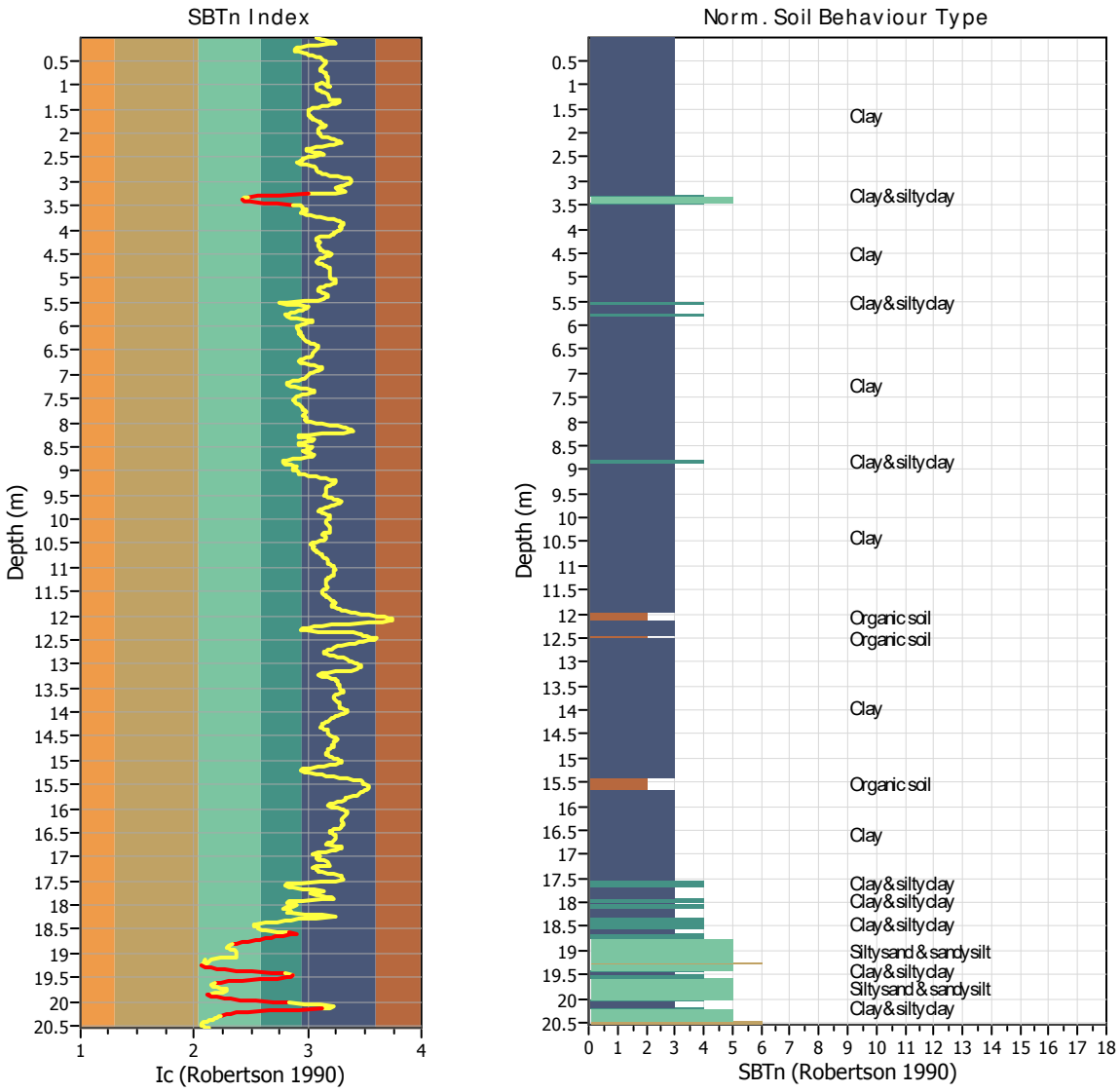
Analysis method:	B&I (2014)	Depth to GWT (erthq.):	0.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.23	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	0.60 m	Fill height:	N/A	Limit depth:	N/A

TRANSITION LAYER DETECTION ALGORITHM REPORT
Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vise-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between $1.80 < I_c < 3.0$) and a rate of change of I_c. Transitions typically occur when the rate of change of I_c is fast (i.e. delta I_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties		General statistics	
I_c minimum check value:	1.70	Total points in CPT file:	1025
I_c maximum check value:	3.00	Total points excluded:	61
I_c change ratio value:	0.0100	Exclusion percentage:	5.95%
Minimum number of points in layer:	4	Number of layers detected:	7

Transition layer No	Number of points	Depth	SBT_n number	SBT_n description
Transition layer 1	4	Start depth: 3.28 (m)	4	Clay & silty clay
		End depth: 3.34 (m)	5	Silty sand & sandy silt
Transition layer 2	7	Start depth: 3.38 (m)	5	Silty sand & sandy silt
		End depth: 3.50 (m)	3	Clay
Transition layer 3	13	Start depth: 18.60 (m)	3	Clay
		End depth: 18.84 (m)	5	Silty sand & sandy silt
Transition layer 4	10	Start depth: 19.26 (m)	6	Sand & silty sand
		End depth: 19.44 (m)	3	Clay
Transition layer 5	9	Start depth: 19.48 (m)	3	Clay
		End depth: 19.64 (m)	5	Silty sand & sandy silt
Transition layer 6	10	Start depth: 19.86 (m)	5	Silty sand & sandy silt
		End depth: 20.04 (m)	3	Clay
Transition layer 7	8	Start depth: 20.16 (m)	3	Clay
		End depth: 20.30 (m)	5	Silty sand & sandy silt

Start depth: Depth where the transition layer begins
End depth: Depth where the transition layer ends

:: Field input data ::

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
1	0.02	0.47	12.12	7.57	64.20	15.94
2	0.05	0.54	25.22	7.82	67.33	16.53
3	0.06	0.61	28.32	7.94	67.38	16.64
4	0.08	0.60	32.62	8.06	68.85	16.81
5	0.10	0.59	37.65	8.18	72.47	16.98
6	0.12	0.59	44.13	8.06	75.61	17.13
7	0.14	0.59	48.64	7.94	76.40	17.27
8	0.16	0.65	53.49	7.94	72.46	17.42
9	0.18	0.83	57.97	8.62	65.28	17.58
10	0.20	1.03	60.70	9.66	58.54	17.71
11	0.22	1.15	62.30	10.09	54.00	17.80
12	0.24	1.26	65.13	10.34	52.02	17.87
13	0.26	1.27	67.53	10.34	50.94	17.94
14	0.28	1.34	71.80	10.22	50.76	18.00
15	0.30	1.36	74.23	10.03	51.42	18.09
16	0.32	1.34	82.79	9.85	53.49	18.19
17	0.34	1.30	93.24	9.60	56.10	18.31
18	0.36	1.31	102.69	9.35	58.03	18.40
19	0.38	1.31	107.15	9.17	59.41	18.47
20	0.40	1.29	111.28	8.98	61.45	18.52
21	0.42	1.23	120.35	8.62	64.05	18.57
22	0.44	1.19	125.35	8.37	66.35	18.59
23	0.46	1.16	123.42	7.94	67.15	18.59
24	0.48	1.16	120.28	7.57	67.75	18.56
25	0.50	1.12	120.05	7.38	68.37	18.54
26	0.52	1.10	119.09	7.32	69.59	18.52
27	0.54	1.06	117.20	7.26	69.90	18.49
28	0.56	1.06	111.97	7.32	69.59	18.44
29	0.58	1.07	107.99	7.45	68.66	18.41
30	0.60	1.08	106.48	7.57	68.10	18.39
31	0.62	1.07	106.25	7.75	67.77	18.38
32	0.64	1.08	104.52	7.94	66.98	18.36
33	0.66	1.10	100.83	8.12	66.40	18.33
34	0.68	1.08	98.58	8.31	66.14	18.31
35	0.70	1.06	98.45	8.49	66.68	18.29
36	0.72	1.05	98.03	8.74	67.54	18.29
37	0.74	1.02	99.28	9.05	68.55	18.28
38	0.76	1.00	99.47	9.23	69.45	18.28
39	0.78	1.00	100.04	9.54	70.20	18.29
40	0.80	0.98	101.10	9.85	70.39	18.28
41	0.82	0.98	98.24	10.09	70.55	18.26
42	0.84	0.98	95.90	10.46	70.99	18.20
43	1.04	0.90	88.02	-33.11	71.84	18.14
44	1.04	0.90	88.02	-33.11	72.72	18.09
45	1.04	0.89	86.61	-32.98	72.85	18.08
46	1.04	0.89	86.61	-32.98	72.97	18.07
47	1.04	0.89	86.61	-32.98	70.90	18.01
48	0.96	0.92	70.93	-9.85	67.79	17.92

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
49	0.98	0.95	67.47	-9.11	64.76	17.83
50	1.00	0.95	67.21	-7.94	63.79	17.81
51	1.02	0.96	67.50	-7.82	63.71	17.81
52	1.04	0.95	66.63	-7.57	63.38	17.81
53	1.06	0.97	66.44	-7.38	63.21	17.82
54	1.08	0.99	69.48	-7.14	63.72	17.88
55	1.10	0.98	75.82	-6.83	64.63	17.94
56	1.12	0.98	78.13	-6.65	66.18	17.99
57	1.14	0.95	80.27	-6.46	67.56	18.01
58	1.16	0.93	81.10	-6.28	69.26	18.02
59	1.18	0.91	82.70	-6.15	70.61	18.03
60	1.20	0.89	83.59	-5.91	71.56	18.03
61	1.32	0.89	83.94	-5.91	72.12	18.04
62	1.32	0.89	83.94	-5.91	72.41	18.04
63	1.32	0.88	83.88	-5.85	72.62	18.03
64	1.32	0.88	83.88	-5.85	74.66	18.03
65	1.30	0.79	85.59	-4.80	77.13	18.02
66	1.32	0.77	86.48	-4.55	79.77	18.01
67	1.34	0.76	84.78	-4.25	79.98	17.99
68	1.36	0.77	82.70	-3.88	78.97	17.96
69	1.38	0.78	79.81	-3.26	76.48	17.94
70	1.40	0.84	76.53	-2.77	73.69	17.92
71	1.42	0.87	75.76	-2.28	70.61	17.92
72	1.44	0.93	75.92	-1.66	67.82	17.94
73	1.46	0.99	75.14	-0.92	64.51	17.96
74	1.49	1.07	74.79	0.00	61.45	17.98
75	1.50	1.13	74.97	1.11	59.71	18.00
76	1.53	1.13	76.09	2.65	58.76	18.01
77	1.54	1.15	74.65	3.45	58.76	18.01
78	1.56	1.13	74.71	3.88	58.59	18.00
79	1.58	1.13	74.12	4.37	58.98	17.98
80	1.60	1.11	73.22	4.86	58.98	17.96
81	1.62	1.10	70.08	5.11	59.31	17.91
82	1.64	1.05	66.58	5.66	59.57	17.84
83	1.66	1.02	63.41	6.52	60.36	17.77
84	1.68	0.98	61.29	7.63	60.88	17.72
85	1.70	0.96	59.49	8.55	61.65	17.66
86	1.72	0.92	56.80	9.78	62.97	17.61
87	1.74	0.86	56.19	10.89	64.66	17.57
88	1.76	0.83	55.67	11.45	66.26	17.53
89	1.78	0.80	52.88	11.75	66.71	17.47
90	1.80	0.79	49.99	13.85	67.32	17.41
91	1.82	0.76	48.93	18.89	68.13	17.36
92	1.84	0.73	48.19	22.03	69.45	17.29
93	1.86	0.68	42.93	47.08	68.73	17.22
94	1.88	0.73	41.68	49.11	66.72	17.14
95	1.91	0.75	38.70	49.54	64.91	17.09
96	1.92	0.72	37.29	51.75	64.65	17.04

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
97	1.94	0.70	36.46	51.75	65.20	16.99
98	1.96	0.69	34.76	53.42	65.41	16.94
99	1.98	0.68	33.35	55.63	65.37	16.88
100	2.00	0.67	32.33	56.62	65.68	16.84
101	2.02	0.65	31.91	57.72	65.67	16.80
102	2.04	0.65	30.46	57.85	66.15	16.77
103	2.06	0.63	29.92	57.72	67.13	16.73
104	2.08	0.59	29.63	58.15	68.78	16.69
105	2.10	0.58	29.02	58.58	71.27	16.67
106	2.13	0.54	29.95	59.57	73.60	16.65
107	2.14	0.51	29.53	60.55	75.79	16.61
108	2.16	0.50	27.41	60.43	77.71	16.55
109	2.18	0.46	26.80	60.62	79.74	16.49
110	2.20	0.44	26.16	61.29	80.76	16.43
111	2.22	0.45	24.24	62.58	79.35	16.36
112	2.24	0.46	22.28	63.75	75.92	16.28
113	2.26	0.48	20.74	64.62	71.90	16.23
114	2.28	0.52	20.04	65.42	67.94	16.21
115	2.30	0.56	19.84	65.91	63.92	16.21
116	2.32	0.61	19.49	66.65	60.36	16.22
117	2.34	0.65	18.94	67.08	57.77	16.20
118	2.37	0.65	18.07	65.97	57.69	16.17
119	2.38	0.60	17.91	65.42	58.93	16.13
120	2.42	0.58	17.82	65.42	62.96	16.05
121	2.42	0.47	16.24	66.28	65.96	15.97
122	2.44	0.46	15.60	68.00	68.09	15.89
123	2.46	0.49	15.50	70.09	65.76	15.88
124	2.48	0.53	15.15	71.69	61.84	15.90
125	2.50	0.59	15.21	72.74	58.62	15.91
126	2.52	0.61	15.02	72.80	56.32	15.92
127	2.54	0.63	14.89	73.29	55.75	15.93
128	2.56	0.62	15.37	74.15	55.26	15.95
129	2.58	0.64	15.53	75.38	54.17	15.98
130	2.60	0.69	15.49	75.51	53.35	16.02
131	2.62	0.68	16.64	75.75	52.66	16.04
132	2.64	0.68	16.03	73.78	54.90	16.11
133	2.66	0.63	18.92	73.23	57.65	16.19
134	2.68	0.61	20.77	73.48	60.97	16.25
135	2.70	0.59	20.13	72.68	62.20	16.25
136	2.72	0.59	19.36	73.48	63.32	16.25
137	2.74	0.57	21.09	75.51	63.52	16.26
138	2.76	0.59	20.60	75.88	63.47	16.28
139	2.78	0.60	20.41	74.40	63.33	16.26
140	2.80	0.57	19.90	73.17	64.66	16.20
141	2.82	0.52	18.74	73.42	66.18	16.13
142	2.84	0.51	17.43	73.66	67.42	16.16
143	2.86	0.55	21.91	75.82	69.43	16.24
144	2.89	0.50	23.29	75.08	72.58	16.34

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
145	2.90	0.47	23.32	73.72	77.84	16.34
146	2.92	0.42	24.06	73.72	82.28	16.34
147	2.94	0.40	24.64	76.00	86.08	16.33
148	2.96	0.40	24.54	77.72	88.07	16.33
149	2.99	0.38	24.86	79.14	88.40	16.32
150	3.00	0.39	23.96	80.25	88.23	16.28
151	3.03	0.39	22.39	80.43	87.39	16.22
152	3.05	0.38	21.30	80.68	85.89	16.12
153	3.06	0.39	18.38	80.68	85.06	16.03
154	3.08	0.37	18.06	80.98	82.88	15.95
155	3.10	0.39	16.97	81.78	80.57	15.91
156	3.12	0.42	16.36	82.71	77.30	15.88
157	3.14	0.43	16.07	83.26	76.13	15.89
158	3.16	0.41	16.81	82.58	77.37	15.90
159	3.18	0.40	17.22	82.65	81.25	15.88
160	3.20	0.34	16.16	82.71	83.89	15.79
161	3.22	0.34	14.18	83.14	84.16	15.70
162	3.24	0.37	14.05	84.43	76.40	15.69
163	3.26	0.48	14.08	87.26	59.03	15.76
164	3.28	0.82	12.22	94.65	42.64	15.85
165	3.30	1.19	11.86	88.18	33.07	15.98
166	3.32	1.38	14.49	77.23	29.27	16.16
167	3.34	1.46	16.22	74.40	28.08	16.34
168	3.36	1.58	17.63	73.97	27.34	16.46
169	3.38	1.65	18.72	73.23	27.00	16.54
170	3.40	1.64	19.58	71.75	28.00	16.54
171	3.42	1.42	18.17	68.92	30.48	16.45
172	3.44	1.17	16.18	67.02	35.56	16.27
173	3.46	0.86	15.25	65.23	42.36	16.11
174	3.48	0.71	15.18	64.92	50.14	15.98
175	3.50	0.61	14.35	67.14	54.89	15.89
176	3.52	0.59	13.52	72.55	55.96	15.78
177	3.54	0.60	11.98	80.49	55.72	15.70
178	3.56	0.58	12.07	83.02	55.88	15.67
179	3.58	0.56	12.42	87.57	57.80	15.71
180	3.60	0.56	13.83	92.31	57.27	15.78
181	3.62	0.64	14.12	96.06	55.67	15.87
182	3.64	0.66	14.76	99.69	53.91	15.94
183	3.66	0.67	15.68	101.78	55.01	16.01
184	3.68	0.63	16.77	102.83	57.63	16.07
185	3.70	0.60	18.18	97.48	60.23	16.11
186	3.72	0.59	18.18	83.08	63.31	16.21
187	3.74	0.58	22.02	76.25	66.13	16.37
188	3.76	0.59	27.08	78.09	71.05	16.60
189	3.78	0.56	33.46	82.52	74.77	16.79
190	3.80	0.57	37.08	86.71	77.88	16.94
191	3.82	0.58	40.73	87.51	79.85	17.08
192	3.84	0.58	47.34	92.00	81.30	17.19

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
193	3.86	0.59	48.69	93.11	82.04	17.25
194	3.88	0.60	48.05	93.48	81.74	17.25
195	3.90	0.59	47.18	94.46	80.40	17.24
196	3.92	0.62	46.38	93.29	80.06	17.22
197	3.94	0.60	45.48	86.83	80.19	17.20
198	3.96	0.58	44.97	80.43	80.74	17.17
199	3.98	0.59	43.68	92.92	80.52	17.14
200	4.00	0.59	42.82	106.95	79.81	17.12
201	4.02	0.58	42.53	111.38	78.56	17.11
202	4.04	0.61	41.95	117.91	76.74	17.11
203	4.06	0.64	41.47	118.09	75.32	17.12
204	4.08	0.63	42.30	120.74	74.86	17.13
205	4.10	0.63	42.30	119.75	74.36	17.14
206	4.12	0.66	41.91	119.32	71.97	17.15
207	4.14	0.72	41.94	114.34	68.64	17.19
208	4.16	0.79	43.64	109.23	65.51	17.25
209	4.18	0.84	45.37	99.63	63.90	17.31
210	4.20	0.85	47.16	90.15	63.45	17.38
211	4.22	0.87	50.78	78.03	64.21	17.45
212	4.24	0.87	53.86	71.75	65.04	17.53
213	4.26	0.89	57.60	66.46	65.65	17.62
214	4.28	0.92	61.93	63.26	65.61	17.70
215	4.30	0.95	65.32	64.80	65.18	17.78
216	4.32	0.99	68.46	64.43	64.73	17.84
217	4.34	1.01	70.77	59.69	64.79	17.89
218	4.36	1.00	72.75	54.65	65.15	17.93
219	4.38	1.01	75.25	52.18	65.73	17.96
220	4.40	1.01	76.78	51.69	66.03	17.99
221	4.42	1.02	78.99	57.17	66.30	18.02
222	4.44	1.02	80.56	58.52	66.98	18.04
223	4.46	0.99	81.81	57.60	68.54	18.05
224	4.48	0.95	82.99	58.46	71.25	18.05
225	4.50	0.88	83.82	64.92	73.32	18.03
226	4.52	0.88	80.97	78.03	73.30	18.00
227	4.54	0.91	77.09	83.94	72.20	17.96
228	4.56	0.90	76.03	90.95	70.52	17.94
229	4.58	0.93	74.49	94.95	69.09	17.93
230	4.60	0.97	73.17	100.18	66.52	17.91
231	4.62	1.01	69.10	100.37	64.52	17.88
232	4.68	1.01	67.24	99.26	63.35	17.85
233	4.68	1.01	67.24	99.26	63.15	17.83
234	4.68	1.00	66.41	99.02	63.87	17.81
235	4.70	0.95	65.06	96.49	65.34	17.80
236	4.72	0.92	67.01	95.75	67.50	17.80
237	4.74	0.89	69.09	95.51	69.03	17.82
238	4.76	0.90	70.31	95.69	70.55	17.85
239	4.78	0.87	73.70	97.05	71.83	17.89
240	4.80	0.87	77.26	97.42	73.09	17.93

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
241	4.82	0.87	77.48	97.85	72.93	17.93
242	4.84	0.89	74.25	94.15	72.66	17.92
243	4.86	0.87	74.41	94.34	72.44	17.90
244	4.89	0.87	74.35	92.92	72.72	17.90
245	4.90	0.88	74.31	93.72	72.66	17.90
246	4.93	0.88	74.09	94.52	72.09	17.90
247	4.94	0.89	73.38	95.14	72.13	17.89
248	4.96	0.87	73.19	95.45	72.30	17.87
249	4.98	0.85	71.43	95.20	73.08	17.84
250	5.01	0.83	69.02	94.95	73.68	17.80
251	5.02	0.81	67.58	94.40	74.78	17.77
252	5.04	0.78	67.36	97.29	76.10	17.75
253	5.06	0.76	67.84	104.43	76.97	17.73
254	5.08	0.76	65.88	107.88	76.85	17.72
255	5.10	0.77	64.60	110.40	76.01	17.69
256	5.12	0.78	63.57	115.32	74.97	17.68
257	5.14	0.79	62.83	123.45	73.11	17.67
258	5.16	0.83	60.65	129.05	70.54	17.64
259	5.18	0.86	57.61	131.20	68.39	17.61
260	5.20	0.86	56.52	130.58	66.31	17.57
261	5.22	0.89	53.00	128.98	65.22	17.53
262	5.24	0.88	51.87	131.63	64.74	17.51
263	5.26	0.86	52.93	132.18	65.31	17.50
264	5.28	0.86	52.96	130.40	66.35	17.50
265	5.30	0.84	52.90	129.23	67.34	17.50
266	5.32	0.81	53.22	127.45	69.21	17.50
267	5.34	0.78	54.98	126.22	70.65	17.51
268	5.36	0.78	54.85	125.35	71.27	17.52
269	5.38	0.80	55.27	128.00	70.73	17.54
270	5.40	0.82	57.67	131.88	69.94	17.56
271	5.42	0.83	55.91	132.86	68.58	17.52
272	5.44	0.83	49.21	132.25	68.10	17.42
273	5.46	0.77	45.65	134.95	65.14	17.30
274	5.48	0.86	40.11	153.97	56.30	17.20
275	5.51	1.18	32.42	168.25	47.26	17.11
276	5.52	1.28	30.98	154.95	43.28	17.09
277	5.54	1.17	35.59	139.02	46.84	17.16
278	5.56	0.96	40.43	135.02	53.17	17.18
279	5.58	0.85	37.74	144.12	57.74	17.10
280	5.60	0.84	32.58	153.72	58.40	16.98
281	5.62	0.83	31.08	168.49	57.73	16.92
282	5.64	0.82	32.10	187.26	56.99	16.93
283	5.66	0.88	33.13	188.55	55.63	16.97
284	5.68	0.92	32.90	191.69	53.37	17.00
285	5.70	0.98	32.91	194.09	51.31	17.03
286	5.72	1.04	34.64	195.14	49.50	17.13
287	5.74	1.14	39.16	202.40	47.66	17.25
288	5.76	1.24	41.21	203.82	46.37	17.33

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
289	5.78	1.25	41.53	187.38	47.10	17.41
290	5.80	1.18	47.58	185.42	47.12	17.51
291	5.82	1.36	51.38	180.86	49.29	17.59
292	5.84	1.17	52.44	144.68	51.75	17.62
293	5.86	1.02	53.24	145.85	57.35	17.59
294	5.88	0.94	53.69	161.91	60.78	17.55
295	5.90	0.93	52.18	191.38	60.83	17.49
296	5.92	0.95	45.65	199.57	59.14	17.40
297	5.94	0.95	42.09	193.23	56.72	17.32
298	5.96	0.99	41.74	197.17	54.90	17.29
299	5.98	1.03	41.70	203.75	52.99	17.32
300	6.00	1.09	42.44	200.80	52.01	17.37
301	6.02	1.11	46.16	206.34	51.85	17.45
302	6.04	1.14	50.26	206.22	52.32	17.56
303	6.06	1.18	55.03	189.48	52.82	17.67
304	6.08	1.20	59.61	190.52	53.39	17.79
305	6.10	1.23	66.05	206.09	53.79	17.89
306	6.12	1.29	71.08	205.42	53.88	17.99
307	6.14	1.32	75.09	204.74	53.69	18.08
308	6.16	1.36	79.28	187.32	53.64	18.13
309	6.18	1.38	81.05	179.75	54.14	18.19
310	6.20	1.37	87.04	175.14	54.57	18.26
311	6.22	1.42	92.10	167.45	54.93	18.32
312	6.24	1.44	94.69	161.54	54.98	18.38
313	6.26	1.47	99.98	156.12	55.39	18.44
314	6.28	1.47	105.10	151.32	56.06	18.50
315	6.30	1.49	110.48	148.25	57.07	18.55
316	6.32	1.46	114.29	142.83	57.90	18.58
317	6.34	1.46	114.93	137.11	59.11	18.60
318	6.36	1.42	118.68	129.23	60.37	18.62
319	6.38	1.39	121.88	123.57	61.87	18.63
320	6.40	1.36	121.72	119.94	63.34	18.64
321	6.42	1.31	122.61	116.25	64.55	18.63
322	6.44	1.29	122.16	116.37	65.01	18.62
323	6.46	1.31	119.37	114.77	64.84	18.59
324	6.48	1.28	113.79	111.75	64.23	18.55
325	6.50	1.28	110.39	112.12	63.58	18.50
326	6.52	1.29	105.52	113.11	62.89	18.45
327	6.54	1.28	102.15	115.20	62.00	18.40
328	6.56	1.27	96.09	115.02	61.78	18.34
329	6.58	1.23	92.34	114.03	61.56	18.29
330	6.60	1.22	90.45	115.63	61.51	18.24
331	6.62	1.21	85.42	118.46	61.25	18.20
332	6.64	1.20	84.07	125.85	60.12	18.15
333	6.66	1.23	78.21	131.45	58.22	18.11
334	6.68	1.29	75.00	131.69	55.70	18.08
335	6.70	1.35	75.26	131.57	54.01	18.08
336	6.72	1.37	75.99	133.54	52.92	18.11

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
337	6.74	1.42	77.78	139.08	52.94	18.11
338	6.76	1.36	75.89	133.66	54.41	18.11
339	6.78	1.25	77.91	129.42	56.64	18.08
340	6.80	1.21	76.57	126.22	59.47	18.07
341	6.82	1.15	78.36	108.49	62.04	18.09
342	6.84	1.10	84.58	109.35	65.10	18.13
343	6.86	1.07	89.39	129.17	67.15	18.19
344	6.88	1.08	92.40	139.26	67.58	18.23
345	6.90	1.12	94.54	146.28	66.77	18.28
346	6.92	1.16	96.98	152.37	65.31	18.30
347	6.94	1.20	95.41	153.29	63.48	18.30
348	6.96	1.24	91.56	157.54	61.52	18.26
349	6.98	1.25	84.93	156.68	60.03	18.21
350	7.00	1.24	82.40	153.29	59.14	18.16
351	7.02	1.25	81.47	154.77	58.67	18.15
352	7.04	1.27	82.01	159.20	57.96	18.16
353	7.06	1.31	83.20	158.58	57.21	18.19
354	7.08	1.34	84.64	163.88	56.37	18.23
355	7.10	1.40	88.87	166.09	55.07	18.29
356	7.12	1.51	92.42	173.11	53.09	18.36
357	7.14	1.64	95.02	176.74	50.58	18.41
358	7.16	1.76	94.57	176.31	48.22	18.46
359	7.18	1.88	96.74	171.88	46.87	18.51
360	7.20	1.92	102.99	166.28	46.58	18.57
361	7.22	1.94	108.21	160.12	47.35	18.63
362	7.24	1.91	113.34	154.71	48.62	18.68
363	7.26	1.86	118.18	149.54	50.90	18.74
364	7.28	1.76	128.52	141.91	54.25	18.80
365	7.30	1.63	139.19	135.51	58.04	18.85
366	7.32	1.57	143.48	130.77	61.23	18.87
367	7.34	1.51	144.67	128.98	62.56	18.87
368	7.36	1.52	142.26	128.80	62.55	18.86
369	7.38	1.55	138.32	131.14	60.64	18.82
370	7.40	1.63	129.57	134.65	57.99	18.78
371	7.42	1.70	121.27	139.69	55.36	18.72
372	7.44	1.71	114.09	137.42	53.24	18.65
373	7.46	1.75	106.84	136.12	52.02	18.59
374	7.48	1.74	104.18	135.32	51.05	18.56
375	7.50	1.76	102.64	133.29	50.65	18.55
376	7.52	1.78	103.25	131.69	50.54	18.58
377	7.54	1.82	110.65	131.57	50.69	18.62
378	7.56	1.84	114.49	129.97	50.76	18.69
379	7.58	1.92	120.71	128.86	51.11	18.75
380	7.60	1.89	126.09	126.52	52.15	18.81
381	7.62	1.85	134.51	124.98	53.24	18.85
382	7.64	1.86	134.51	123.75	54.16	18.87
383	7.66	1.83	134.74	120.98	54.61	18.87
384	7.68	1.80	135.73	118.77	54.96	18.86

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
385	7.70	1.83	134.38	117.72	55.08	18.87
386	7.72	1.82	135.05	115.14	55.33	18.87
387	7.74	1.79	136.62	113.35	56.20	18.88
388	7.76	1.76	140.08	112.49	57.49	18.89
389	7.78	1.73	143.48	111.14	57.72	18.88
390	7.81	1.73	131.63	124.92	57.07	18.86
391	7.82	1.80	131.82	106.77	56.04	18.83
392	7.84	1.79	132.43	95.08	55.98	18.83
393	7.86	1.76	131.53	90.89	56.53	18.81
394	7.88	1.73	128.39	89.78	57.20	18.80
395	7.90	1.70	129.10	100.25	57.29	18.78
396	7.92	1.72	126.40	96.06	57.15	18.77
397	7.94	1.72	124.58	95.08	57.10	18.75
398	7.96	1.68	124.09	89.42	58.02	18.73
399	7.99	1.60	122.04	85.54	60.29	18.70
400	8.00	1.47	120.88	81.72	63.55	18.65
401	8.02	1.33	117.00	75.94	67.83	18.58
402	8.04	1.19	113.99	72.37	72.71	18.52
403	8.06	1.08	112.90	73.23	77.61	18.46
404	8.08	1.00	111.26	77.17	81.63	18.41
405	8.10	0.95	106.51	81.78	84.38	18.33
406	8.12	0.89	98.50	90.83	86.13	18.24
407	8.14	0.85	92.86	98.46	88.35	18.14
408	8.16	0.78	86.80	107.08	89.36	18.03
409	8.18	0.76	76.10	115.94	87.83	17.90
410	8.20	0.81	68.25	117.91	82.87	17.78
411	8.22	0.86	61.20	121.60	75.65	17.68
412	8.24	0.96	53.67	124.62	67.03	17.59
413	8.26	1.12	48.12	128.31	58.64	17.51
414	8.28	1.26	44.25	129.54	53.66	17.44
415	8.30	1.24	42.36	123.26	53.53	17.39
416	8.32	1.08	42.27	112.62	57.32	17.34
417	8.34	0.96	42.52	120.18	61.03	17.25
418	8.36	0.94	36.73	140.37	62.25	17.14
419	8.38	0.91	32.56	141.78	60.95	17.03
420	8.40	0.93	32.88	154.15	58.52	17.00
421	8.42	1.04	32.72	161.11	55.38	17.01
422	8.44	1.10	31.38	161.66	53.21	17.02
423	8.46	1.09	32.44	160.12	53.77	17.03
424	8.48	1.02	34.08	163.75	56.23	17.05
425	8.50	0.97	34.21	160.06	58.72	17.06
426	8.52	0.95	34.79	161.29	60.76	17.07
427	8.54	0.92	36.29	164.68	60.55	17.11
428	8.56	1.01	37.07	175.82	58.65	17.15
429	8.58	1.10	37.13	183.20	56.21	17.20
430	8.60	1.11	38.29	178.71	55.58	17.23
431	8.62	1.08	39.06	183.94	57.21	17.25
432	8.64	1.02	40.89	194.65	59.59	17.26

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
433	8.66	0.97	40.15	204.06	61.72	17.24
434	8.68	0.94	39.10	211.26	62.32	17.21
435	8.70	0.96	38.33	220.80	61.37	17.17
436	8.72	0.98	35.83	233.60	58.58	17.13
437	8.74	1.06	33.75	244.49	54.36	17.09
438	8.76	1.19	32.79	253.66	50.17	17.10
439	8.78	1.30	33.40	253.66	46.55	17.24
440	8.80	1.54	41.89	258.03	44.86	17.38
441	8.82	1.54	43.17	263.94	44.74	17.53
442	8.85	1.54	48.46	279.08	46.10	17.63
443	8.86	1.53	53.84	284.98	47.07	17.73
444	8.88	1.58	55.70	259.20	48.77	17.86
445	8.90	1.55	66.69	251.75	50.79	17.99
446	8.92	1.53	76.05	280.62	52.26	18.11
447	8.94	1.61	76.17	283.82	51.55	18.16
448	8.96	1.71	74.09	265.29	50.58	18.17
449	8.98	1.68	77.10	252.12	50.53	18.20
450	9.00	1.68	81.04	236.06	51.90	18.23
451	9.02	1.62	82.13	226.40	52.82	18.25
452	9.05	1.62	82.10	224.18	53.44	18.26
453	9.07	1.64	83.44	218.28	54.08	18.28
454	9.08	1.60	86.58	214.09	56.23	18.33
455	9.10	1.49	95.45	209.23	59.39	18.36
456	9.12	1.40	94.78	198.09	63.03	18.38
457	9.15	1.33	96.76	192.43	66.04	18.36
458	9.16	1.26	97.05	184.68	69.58	18.37
459	9.18	1.18	102.37	181.85	73.20	18.38
460	9.20	1.13	104.67	182.03	75.95	18.37
461	9.22	1.10	99.96	183.14	77.14	18.34
462	9.24	1.09	96.56	183.94	76.51	18.29
463	9.26	1.11	91.31	184.06	75.50	18.21
464	9.29	1.08	82.49	181.91	73.96	18.12
465	9.31	1.08	76.27	182.52	72.29	18.01
466	9.32	1.08	68.04	184.55	70.72	17.92
467	9.34	1.07	65.57	186.28	69.67	17.86
468	9.36	1.08	65.85	185.91	69.49	17.85
469	9.38	1.08	66.46	183.94	69.37	17.86
470	9.40	1.10	67.61	183.02	69.66	17.88
471	9.42	1.08	69.09	181.97	69.84	17.91
472	9.44	1.10	70.50	182.03	70.27	17.93
473	9.46	1.10	71.71	183.51	70.01	17.95
474	9.48	1.12	71.26	183.88	69.55	17.96
475	9.50	1.15	72.58	183.26	69.19	17.99
476	9.52	1.16	76.68	181.85	69.93	18.04
477	9.54	1.12	79.11	180.25	71.65	18.07
478	9.56	1.09	80.97	178.34	73.66	18.08
479	9.58	1.08	81.61	176.31	75.78	18.10
480	9.60	1.03	83.98	173.42	78.16	18.11

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
481	9.62	0.99	85.68	171.14	80.63	18.11
482	9.64	0.97	86.09	170.58	81.53	18.11
483	9.66	0.99	84.11	174.22	79.99	18.10
484	9.68	1.05	81.54	178.09	77.92	18.08
485	9.70	1.05	80.00	183.02	75.58	18.06
486	9.72	1.09	77.02	185.48	73.76	18.02
487	9.74	1.11	72.51	185.60	71.66	17.97
488	9.76	1.11	68.53	186.58	70.10	17.91
489	9.78	1.12	66.36	187.32	67.23	17.86
490	9.80	1.22	60.07	178.89	65.79	17.84
491	9.82	1.19	64.50	170.28	65.31	17.85
492	9.85	1.17	67.83	167.20	66.72	17.91
493	9.86	1.20	69.75	162.77	67.68	17.95
494	9.88	1.19	72.76	161.11	68.84	18.01
495	9.90	1.17	78.40	161.11	70.74	18.07
496	9.92	1.16	82.25	160.49	72.29	18.12
497	9.94	1.16	85.22	160.43	73.09	18.16
498	9.96	1.17	86.02	161.72	72.94	18.18
499	9.98	1.19	85.93	162.34	72.35	18.18
500	10.00	1.20	84.65	162.71	71.29	18.16
501	10.02	1.21	81.06	161.78	70.08	18.14
502	10.04	1.24	79.45	161.85	69.70	18.12
503	10.06	1.21	80.32	161.91	69.75	18.12
504	10.08	1.21	81.15	162.40	70.33	18.13
505	10.10	1.22	81.66	162.22	70.72	18.14
506	10.12	1.20	83.07	162.95	71.49	18.15
507	10.14	1.18	84.00	166.95	72.07	18.16
508	10.16	1.19	83.84	167.26	72.20	18.16
509	10.18	1.21	84.51	167.32	72.26	18.17
510	10.20	1.19	85.21	166.65	72.43	18.17
511	10.22	1.19	84.47	166.95	72.84	18.17
512	10.24	1.18	84.73	169.42	72.87	18.17
513	10.26	1.19	85.47	171.02	72.03	18.18
514	10.28	1.25	84.63	173.48	70.26	18.20
515	10.30	1.31	85.37	175.32	68.09	18.21
516	10.32	1.36	85.33	174.28	67.41	18.23
517	10.34	1.32	86.49	171.38	67.93	18.24
518	10.36	1.30	88.89	169.11	69.40	18.25
519	10.38	1.28	89.75	168.98	70.29	18.26
520	10.40	1.28	89.78	170.03	70.44	18.26
521	10.42	1.29	88.69	169.97	69.74	18.26
522	10.44	1.33	88.15	171.02	68.38	18.26
523	10.46	1.38	88.63	174.15	66.48	18.27
524	10.48	1.44	87.03	176.98	63.97	18.27
525	10.50	1.51	83.76	178.58	61.69	18.26
526	10.52	1.56	83.79	179.02	60.49	18.27
527	10.54	1.56	87.41	179.32	60.80	18.31
528	10.56	1.54	90.48	180.68	61.78	18.34

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
529	10.58	1.52	91.48	179.14	62.05	18.35
530	10.60	1.57	90.96	178.58	61.77	18.37
531	10.62	1.59	93.37	178.15	61.81	18.40
532	10.64	1.58	98.40	178.65	62.46	18.45
533	10.66	1.59	103.20	179.51	63.26	18.50
534	10.68	1.60	105.93	179.38	63.75	18.54
535	10.70	1.61	109.32	178.71	64.96	18.58
536	10.72	1.56	115.60	176.80	66.43	18.62
537	10.74	1.55	119.06	176.37	67.68	18.65
538	10.77	1.55	118.39	175.75	67.76	18.65
539	10.78	1.56	115.49	171.38	67.86	18.64
540	10.80	1.53	117.32	167.69	68.49	18.63
541	10.82	1.49	117.42	166.15	69.74	18.63
542	10.84	1.46	115.94	164.74	70.77	18.61
543	10.86	1.44	115.01	163.45	71.09	18.59
544	10.88	1.45	113.25	161.54	71.31	18.58
545	10.91	1.43	113.22	160.92	71.79	18.56
546	10.92	1.38	110.81	161.48	72.82	18.54
547	10.95	1.35	109.69	162.40	74.40	18.51
548	10.96	1.29	107.99	162.58	75.04	18.48
549	10.98	1.31	104.66	163.75	75.47	18.45
550	11.00	1.29	102.76	163.69	75.33	18.42
551	11.02	1.27	100.62	164.18	75.78	18.39
552	11.04	1.25	98.37	166.65	76.04	18.37
553	11.06	1.25	97.51	167.69	75.76	18.35
554	11.09	1.26	94.78	167.88	75.52	18.33
555	11.10	1.24	93.63	168.37	75.39	18.31
556	11.13	1.24	93.88	169.05	75.08	18.30
557	11.15	1.27	92.60	170.03	74.60	18.30
558	11.16	1.27	91.86	169.85	73.86	18.29
559	11.18	1.28	91.96	170.15	73.44	18.29
560	11.20	1.30	91.60	170.77	72.44	18.29
561	11.22	1.34	90.45	170.40	71.73	18.30
562	11.24	1.34	91.73	171.14	71.11	18.30
563	11.26	1.35	91.60	172.74	70.30	18.30
564	11.28	1.40	89.55	173.48	69.54	18.30
565	11.30	1.38	88.97	173.48	69.34	18.29
566	11.32	1.36	89.16	173.66	69.57	18.27
567	11.34	1.37	86.95	174.52	69.56	18.25
568	11.36	1.36	84.77	173.97	69.35	18.22
569	11.38	1.33	82.34	172.12	69.87	18.19
570	11.40	1.30	82.21	170.71	70.81	18.17
571	11.42	1.28	82.02	170.46	71.27	18.17
572	11.44	1.30	81.70	171.45	70.05	18.16
573	11.46	1.38	79.49	173.66	68.45	18.15
574	11.48	1.37	77.37	173.72	67.28	18.12
575	11.50	1.35	75.32	173.85	67.07	18.08
576	11.52	1.34	71.79	172.43	67.23	18.04

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
577	11.54	1.32	70.99	170.40	67.46	18.01
578	11.56	1.30	70.39	168.98	68.26	17.99
579	11.58	1.28	70.03	166.89	69.33	17.98
580	11.60	1.24	69.68	165.54	70.56	17.98
581	11.62	1.23	71.41	165.29	71.71	17.98
582	11.64	1.22	72.28	168.00	72.56	18.00
583	11.66	1.21	73.21	172.25	72.99	18.01
584	11.68	1.22	74.29	172.00	73.75	18.03
585	11.70	1.19	75.87	173.05	74.70	18.03
586	11.72	1.16	75.19	170.03	75.64	18.00
587	11.74	1.14	70.16	168.25	76.38	17.92
588	11.76	1.07	62.90	196.55	75.02	17.87
589	11.78	1.18	65.65	182.15	74.31	17.86
590	11.80	1.17	67.32	181.11	73.97	17.89
591	11.82	1.12	66.94	180.12	75.82	17.89
592	11.84	1.09	67.93	178.09	77.36	17.87
593	11.86	1.08	66.42	175.63	79.28	17.87
594	11.88	1.03	67.39	173.48	81.42	17.85
595	11.90	0.98	67.96	175.75	84.29	17.84
596	11.92	0.95	67.45	174.15	87.61	17.80
597	11.94	0.87	64.34	168.92	91.29	17.74
598	11.96	0.81	61.81	164.49	96.17	17.67
599	11.98	0.75	60.49	160.98	100.00	17.62
600	12.00	0.67	60.43	162.03	100.00	17.57
601	12.02	0.62	59.76	163.08	100.00	17.49
602	12.04	0.58	52.42	163.94	100.00	17.36
603	12.06	0.53	45.98	165.42	100.00	17.19
604	12.08	0.51	40.53	166.65	100.00	17.01
605	12.10	0.50	34.60	168.55	100.00	16.82
606	12.12	0.50	28.26	170.03	100.00	16.62
607	12.14	0.53	23.39	174.65	100.00	16.46
608	12.16	0.65	21.28	182.09	86.96	16.40
609	12.18	0.79	21.02	187.57	73.88	16.42
610	12.20	0.93	20.57	187.82	67.14	16.50
611	12.22	0.97	23.17	183.45	62.63	16.60
612	12.24	1.09	24.87	186.89	59.21	16.75
613	12.27	1.25	27.50	179.88	55.68	16.90
614	12.28	1.36	31.09	164.43	54.63	17.07
615	12.30	1.35	35.70	153.97	57.82	17.16
616	12.32	1.12	36.57	140.31	65.40	17.15
617	12.34	0.87	34.87	131.32	77.42	16.98
618	12.36	0.66	28.02	127.63	89.22	16.74
619	12.38	0.60	23.56	138.77	95.05	16.51
620	12.40	0.62	22.09	146.83	96.69	16.43
621	12.42	0.59	23.82	153.05	97.03	16.44
622	12.44	0.60	24.27	163.94	100.00	16.44
623	12.46	0.55	23.19	163.75	100.00	16.41
624	12.48	0.51	22.87	167.57	100.00	16.35

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
625	12.50	0.51	21.68	176.68	100.00	16.31
626	12.52	0.54	20.82	187.26	100.00	16.27
627	12.54	0.58	19.83	192.62	97.69	16.23
628	12.56	0.58	18.64	198.09	93.97	16.20
629	12.58	0.60	18.87	202.03	91.58	16.20
630	12.60	0.63	19.16	204.62	86.94	16.23
631	12.62	0.70	19.22	210.83	81.49	16.28
632	12.64	0.76	19.51	213.97	77.43	16.37
633	12.66	0.80	22.36	215.02	75.29	16.48
634	12.68	0.84	24.45	216.92	74.63	16.60
635	12.70	0.86	25.54	217.17	73.38	16.68
636	12.72	0.90	26.66	219.38	71.80	16.74
637	12.74	0.94	27.52	223.63	69.97	16.81
638	12.76	0.98	29.53	264.86	68.31	16.90
639	12.78	1.04	31.87	257.54	68.50	17.01
640	12.80	1.02	35.33	253.60	69.86	17.11
641	12.82	1.00	38.05	251.51	72.75	17.20
642	12.84	0.98	41.10	250.09	75.39	17.28
643	12.86	0.96	44.27	250.89	78.69	17.36
644	12.88	0.93	48.43	251.26	82.51	17.43
645	12.90	0.88	51.64	256.00	85.64	17.49
646	12.94	0.89	52.60	259.94	87.01	17.51
647	12.94	0.90	51.86	258.34	87.39	17.51
648	12.96	0.86	51.38	257.78	88.71	17.49
649	12.99	0.83	51.60	256.74	90.95	17.46
650	13.00	0.81	50.00	256.25	92.61	17.43
651	13.03	0.79	48.53	257.29	94.36	17.38
652	13.04	0.75	46.60	259.32	95.36	17.33
653	13.06	0.75	45.35	261.78	96.24	17.30
654	13.08	0.74	44.74	268.68	94.33	17.26
655	13.10	0.78	41.41	270.34	92.35	17.23
656	13.13	0.79	41.41	275.94	87.84	17.18
657	13.14	0.85	37.44	283.14	83.05	17.13
658	13.16	0.91	34.55	286.77	76.35	17.06
659	13.18	1.00	31.92	289.05	71.15	17.01
660	13.20	1.05	31.06	290.34	66.73	17.00
661	13.22	1.12	31.41	291.63	65.11	17.04
662	13.24	1.13	34.58	289.17	65.47	17.13
663	13.26	1.11	38.36	284.86	67.76	17.24
664	13.28	1.09	41.79	280.37	71.09	17.35
665	13.30	1.05	46.82	278.09	74.07	17.44
666	13.32	1.05	49.80	278.46	76.12	17.51
667	13.34	1.05	50.73	279.94	77.05	17.54
668	13.36	1.04	51.15	279.08	77.34	17.54
669	13.38	1.03	49.83	280.12	77.40	17.52
670	13.40	1.04	48.52	279.02	77.77	17.49
671	13.42	1.00	48.17	277.35	78.47	17.46
672	13.44	0.98	46.79	275.08	79.53	17.43

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
673	13.46	0.97	45.86	274.71	79.83	17.41
674	13.48	0.97	46.11	273.97	79.50	17.40
675	13.50	0.99	45.47	273.72	79.38	17.39
676	13.52	0.97	44.64	272.68	79.77	17.37
677	13.54	0.95	44.35	270.83	80.92	17.36
678	13.56	0.93	44.54	269.85	81.82	17.34
679	13.58	0.93	43.84	269.48	81.68	17.34
680	13.60	0.95	44.03	270.83	80.69	17.34
681	13.62	0.98	44.29	276.00	78.58	17.35
682	13.64	1.02	42.97	278.22	76.56	17.34
683	13.66	1.04	42.14	278.46	75.03	17.34
684	13.68	1.05	42.84	278.40	74.70	17.35
685	13.70	1.05	43.80	277.42	75.28	17.38
686	13.72	1.04	45.73	280.92	75.86	17.42
687	13.74	1.06	47.39	281.29	76.30	17.46
688	13.76	1.06	48.69	289.54	76.66	17.50
689	13.79	1.06	50.32	287.69	77.64	17.54
690	13.80	1.05	52.76	285.48	78.86	17.58
691	13.82	1.04	54.17	283.69	79.58	17.62
692	13.85	1.06	55.03	283.08	80.06	17.65
693	13.86	1.06	56.95	283.45	79.73	17.67
694	13.88	1.09	57.56	285.66	79.12	17.69
695	13.90	1.11	57.34	284.25	79.68	17.72
696	13.92	1.05	60.09	281.35	81.00	17.73
697	13.94	1.04	61.18	279.02	83.37	17.75
698	13.96	1.02	60.83	276.92	84.85	17.73
699	13.98	0.98	59.61	281.54	85.62	17.70
700	14.00	0.99	57.33	287.32	84.96	17.66
701	14.02	1.01	54.16	291.02	82.88	17.62
702	14.04	1.04	52.84	292.49	80.66	17.58
703	14.06	1.06	51.34	293.91	78.24	17.57
704	14.08	1.11	50.50	296.68	76.13	17.54
705	14.10	1.12	48.23	296.37	74.74	17.52
706	14.12	1.11	48.10	296.06	73.96	17.51
707	14.14	1.14	48.29	296.74	73.18	17.53
708	14.16	1.18	49.86	297.29	72.24	17.56
709	14.18	1.20	50.85	298.83	71.15	17.58
710	14.20	1.22	49.67	299.38	70.11	17.59
711	14.22	1.25	50.27	301.85	68.55	17.60
712	14.24	1.31	51.04	301.72	67.88	17.65
713	14.26	1.32	54.66	306.95	67.08	17.70
714	14.28	1.37	56.17	304.86	66.98	17.76
715	14.30	1.39	58.86	305.23	66.72	17.82
716	14.32	1.41	62.38	304.62	67.45	17.90
717	14.34	1.41	66.97	302.65	69.07	17.98
718	14.36	1.38	73.05	301.35	70.62	18.06
719	14.38	1.40	76.54	301.17	71.58	18.11
720	14.40	1.42	77.83	303.08	71.46	18.16

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
721	14.42	1.45	80.49	304.12	71.10	18.18
722	14.44	1.47	80.80	301.42	71.08	18.21
723	14.46	1.46	82.50	299.63	71.27	18.22
724	14.48	1.46	83.40	297.17	72.02	18.23
725	14.50	1.43	84.13	293.97	73.16	18.24
726	14.52	1.39	84.81	287.88	74.67	18.24
727	14.54	1.36	85.38	284.86	76.73	18.24
728	14.56	1.31	86.72	281.11	78.10	18.24
729	14.58	1.31	85.79	280.86	78.15	18.23
730	14.60	1.35	83.84	282.52	76.81	18.22
731	14.62	1.38	83.61	285.91	75.82	18.22
732	14.64	1.37	84.32	292.49	75.52	18.23
733	14.66	1.39	85.60	295.32	75.24	18.24
734	14.68	1.41	84.22	294.52	74.62	18.25
735	14.70	1.43	85.27	296.25	73.86	18.25
736	14.72	1.44	84.60	296.80	74.74	18.18
737	14.74	1.27	72.72	330.58	73.36	18.16
738	14.76	1.48	78.81	320.37	72.47	18.13
739	14.78	1.47	78.65	316.68	70.83	18.17
740	14.81	1.44	77.27	310.77	71.02	18.14
741	14.83	1.45	75.29	308.80	70.78	18.12
742	14.84	1.46	74.17	303.63	70.06	18.11
743	14.86	1.47	73.85	299.26	69.90	18.11
744	14.88	1.47	75.16	295.02	70.27	18.14
745	14.90	1.48	79.39	293.42	71.44	18.18
746	14.92	1.46	84.10	292.12	72.63	18.24
747	14.94	1.46	87.01	291.02	74.06	18.29
748	14.96	1.45	91.53	288.43	75.66	18.34
749	14.98	1.42	96.17	286.03	77.77	18.38
750	15.01	1.38	98.96	287.45	80.04	18.41
751	15.02	1.34	99.92	294.34	81.29	18.41
752	15.04	1.35	98.99	302.71	80.95	18.40
753	15.06	1.39	96.30	311.88	78.95	18.39
754	15.08	1.45	95.11	316.49	75.98	18.38
755	15.10	1.53	93.06	323.45	72.60	18.37
756	15.12	1.61	87.61	323.32	68.97	18.32
757	15.14	1.67	80.88	332.68	64.30	18.26
758	15.16	1.84	74.25	345.78	59.75	18.20
759	15.18	1.95	70.75	355.20	55.87	18.17
760	15.20	2.05	70.21	337.54	54.28	18.20
761	15.22	2.08	75.88	338.95	54.44	18.26
762	15.24	2.06	82.48	347.51	56.64	18.36
763	15.26	1.98	92.38	324.80	59.38	18.45
764	15.28	1.93	97.98	310.09	63.04	18.54
765	15.30	1.84	108.40	296.74	66.80	18.62
766	15.32	1.75	118.20	307.45	70.57	18.70
767	15.34	1.71	124.54	326.22	75.07	18.74
768	15.37	1.53	127.27	329.85	78.98	18.74

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
769	15.38	1.46	126.11	322.65	85.17	18.71
770	15.40	1.27	127.17	311.45	90.41	18.67
771	15.42	1.18	123.03	313.48	96.13	18.60
772	15.44	1.12	116.98	314.65	97.76	18.51
773	15.46	1.10	104.41	314.22	98.15	18.41
774	15.48	1.06	96.02	316.98	98.20	18.30
775	15.50	1.01	91.40	324.37	100.00	18.21
776	15.52	0.96	86.72	326.89	100.00	18.13
777	15.54	0.91	80.57	328.00	100.00	18.03
778	15.56	0.90	73.43	330.65	100.00	17.92
779	15.58	0.88	66.60	333.85	100.00	17.80
780	15.60	0.85	61.15	338.03	100.00	17.69
781	15.62	0.86	55.61	340.68	100.00	17.58
782	15.64	0.85	49.91	342.71	97.27	17.46
783	15.66	0.85	45.49	343.57	95.72	17.35
784	15.68	0.83	41.90	346.03	94.32	17.25
785	15.70	0.83	38.41	348.80	93.81	17.15
786	15.72	0.81	35.81	353.11	92.79	16.97
787	15.74	0.75	25.63	388.68	89.56	16.86
788	15.76	0.86	29.54	401.35	85.41	16.82
789	15.78	0.90	31.08	406.40	83.24	16.92
790	15.80	0.89	32.23	410.58	83.00	16.96
791	15.82	0.89	32.30	417.17	83.05	16.97
792	15.84	0.91	31.56	426.09	81.29	16.95
793	15.86	0.94	30.28	441.60	78.31	16.92
794	15.88	0.99	29.03	450.22	75.16	16.90
795	15.90	1.02	28.52	457.91	72.51	16.89
796	15.92	1.06	28.68	463.38	71.22	16.89
797	15.94	1.05	28.36	464.80	71.67	16.89
798	15.96	1.00	28.68	457.17	74.24	16.89
799	15.98	0.94	29.77	449.23	77.77	16.90
800	16.00	0.91	30.29	450.89	80.48	16.90
801	16.03	0.89	29.81	450.34	82.01	16.89
802	16.04	0.88	29.65	448.12	83.10	16.87
803	16.06	0.85	29.20	446.46	84.47	16.85
804	16.08	0.83	28.63	449.23	85.18	16.81
805	16.10	0.83	27.34	450.83	84.89	16.77
806	16.12	0.84	26.42	450.40	84.17	16.72
807	16.14	0.83	25.23	451.69	83.22	16.67
808	16.16	0.83	23.85	452.80	82.78	16.63
809	16.18	0.83	24.05	453.72	81.75	16.61
810	16.20	0.85	23.54	460.92	81.45	16.60
811	16.22	0.84	23.09	465.66	80.77	16.58
812	16.24	0.85	22.80	467.45	80.91	16.57
813	16.26	0.84	22.96	468.55	81.07	16.58
814	16.28	0.84	23.83	469.48	81.75	16.60
815	16.30	0.83	24.08	470.22	82.08	16.60
816	16.32	0.83	23.38	469.17	81.81	16.59

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
817	16.34	0.84	22.93	469.54	81.32	16.58
818	16.36	0.85	23.09	471.57	80.90	16.57
819	16.38	0.85	22.87	472.00	80.35	16.57
820	16.40	0.86	22.65	475.45	79.26	16.54
821	16.42	0.87	21.52	481.11	77.28	16.52
822	16.44	0.91	21.08	482.89	75.38	16.51
823	16.46	0.93	21.62	484.92	73.57	16.53
824	16.48	0.96	21.88	488.55	72.66	16.57
825	16.50	0.97	22.68	489.17	72.68	16.60
826	16.52	0.96	23.35	485.97	73.90	16.64
827	16.54	0.94	24.51	484.12	75.52	16.66
828	16.56	0.92	24.44	485.17	76.83	16.69
829	16.58	0.92	25.18	486.46	77.07	16.69
830	16.60	0.93	24.96	489.78	76.85	16.70
831	16.62	0.93	24.80	493.17	76.29	16.68
832	16.64	0.93	23.90	493.35	76.08	16.66
833	16.66	0.93	23.65	494.03	75.50	16.61
834	16.68	0.92	21.50	496.18	75.01	16.56
835	16.70	0.92	21.27	497.54	74.39	16.52
836	16.72	0.93	21.53	499.63	71.15	16.66
837	16.74	1.20	28.04	370.95	70.44	16.83
838	16.76	1.11	30.77	369.17	71.74	16.97
839	16.78	1.00	31.31	383.38	76.93	16.97
840	16.80	0.95	30.58	404.86	80.36	16.92
841	16.82	0.92	28.62	436.31	80.63	16.86
842	16.84	0.94	26.89	451.57	79.20	16.81
843	16.86	0.96	26.83	467.02	76.73	16.78
844	16.88	1.00	26.12	472.98	73.76	16.79
845	16.91	1.07	26.22	481.97	69.89	16.81
846	16.92	1.16	26.22	498.46	64.76	16.81
847	16.94	1.29	24.04	510.40	61.59	16.79
848	16.96	1.26	23.69	469.17	62.10	16.82
849	16.98	1.16	28.33	467.20	64.86	16.87
850	17.00	1.16	28.56	488.12	66.16	16.94
851	17.02	1.24	28.88	503.82	65.05	16.97
852	17.04	1.26	30.03	510.15	63.88	17.00
853	17.06	1.26	29.42	491.20	65.29	17.03
854	17.08	1.20	31.79	443.82	68.02	17.04
855	17.10	1.11	32.02	448.00	71.22	17.05
856	17.18	1.10	31.82	456.92	72.98	17.04
857	17.18	1.10	31.82	456.92	73.12	17.04
858	17.18	1.10	31.82	456.92	72.98	17.04
859	17.18	1.11	31.79	460.49	67.04	17.14
860	17.20	1.54	36.92	419.26	64.02	17.22
861	17.22	1.40	36.21	396.25	61.29	17.28
862	17.24	1.40	35.22	399.94	63.08	17.25
863	17.26	1.39	36.18	405.42	63.66	17.25
864	17.28	1.35	36.53	413.17	64.33	17.28

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
865	17.30	1.37	37.72	425.05	65.25	17.29
866	17.32	1.33	37.75	426.77	67.05	17.28
867	17.34	1.22	36.46	416.37	70.82	17.24
868	17.36	1.11	36.59	406.65	75.68	17.18
869	17.38	1.02	35.12	424.92	79.56	17.14
870	17.40	0.99	34.54	463.57	80.81	17.10
871	17.42	1.01	33.83	473.23	80.93	17.08
872	17.44	0.99	33.67	471.51	81.17	17.06
873	17.46	0.96	32.81	469.42	81.88	17.01
874	17.48	0.95	30.76	473.35	81.61	16.94
875	17.50	0.95	28.16	481.05	76.46	16.85
876	17.52	1.11	24.57	506.09	65.54	16.80
877	17.54	1.47	23.03	546.58	54.10	16.81
878	17.56	1.81	24.22	564.55	47.19	16.91
879	17.58	1.97	26.72	428.43	45.87	17.12
880	17.60	1.95	35.15	396.43	46.48	17.35
881	17.62	2.14	42.04	385.29	47.68	17.55
882	17.64	2.17	45.46	319.14	49.72	17.73
883	17.66	2.01	55.27	262.09	55.04	17.86
884	17.68	1.73	63.47	219.38	63.00	17.96
885	17.70	1.51	66.38	243.26	68.31	17.95
886	17.72	1.54	60.68	376.62	64.97	18.04
887	17.74	2.13	72.76	268.18	61.38	18.10
888	17.76	1.96	72.41	241.29	60.42	18.19
889	17.78	1.80	72.64	259.02	63.47	18.13
890	17.80	1.73	67.86	296.92	66.15	18.05
891	17.82	1.57	61.32	295.14	69.33	17.94
892	17.84	1.40	60.59	289.05	74.20	17.85
893	17.86	1.26	58.50	312.12	75.77	17.78
894	17.88	1.38	53.09	358.58	67.74	17.76
895	17.90	1.90	50.87	405.78	55.70	17.79
896	17.92	2.41	51.19	389.60	48.22	17.87
897	17.94	2.54	55.42	251.02	46.53	17.99
898	17.96	2.45	64.17	197.17	48.70	18.07
899	17.98	2.28	64.33	167.69	51.49	18.13
900	18.00	2.27	68.20	150.58	51.75	18.17
901	18.02	2.52	71.25	154.22	49.95	18.25
902	18.04	2.73	74.71	156.18	46.52	18.39
903	18.06	3.19	86.24	150.40	45.45	18.55
904	18.08	3.14	98.67	121.35	46.56	18.67
905	18.10	2.88	103.15	103.32	48.70	18.72
906	18.12	2.91	100.91	95.26	48.93	18.69
907	18.14	3.04	93.73	96.06	47.48	18.62
908	18.16	2.97	83.61	85.05	49.52	18.53
909	18.18	2.31	86.01	71.02	56.02	18.45
910	18.20	1.85	89.15	61.66	67.63	18.35
911	18.22	1.47	81.00	70.95	77.16	18.22
912	18.24	1.34	72.48	142.09	75.33	18.06

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
913	18.26	1.74	59.50	295.38	63.91	17.97
914	18.28	2.21	55.27	330.95	53.03	17.94
915	18.30	2.47	55.88	253.97	48.76	17.96
916	18.32	2.40	57.25	223.14	46.05	18.00
917	18.34	2.75	56.77	209.05	41.90	18.12
918	18.36	3.51	66.76	219.45	36.38	18.30
919	18.38	4.20	75.19	197.54	32.85	18.45
920	18.40	4.36	75.93	174.65	31.70	18.56
921	18.42	4.34	82.94	149.23	32.11	18.62
922	18.44	4.29	85.98	124.74	33.07	18.66
923	18.46	4.22	87.01	111.38	33.48	18.65
924	18.48	4.18	81.85	97.97	33.63	18.63
925	18.50	4.18	82.87	89.23	33.60	18.63
926	18.52	4.24	86.58	81.23	34.97	18.70
927	18.54	3.99	98.02	74.52	36.60	18.76
928	18.58	3.93	100.30	73.11	42.15	18.80
929	18.58	2.85	107.22	53.85	47.77	18.78
930	18.60	2.69	106.54	66.03	52.20	18.70
931	18.62	2.86	90.39	104.37	48.81	18.56
932	18.64	3.10	70.24	101.54	44.92	18.50
933	18.66	3.29	88.25	99.51	41.62	18.54
934	18.68	3.68	90.68	98.28	39.57	18.73
935	18.70	4.25	105.64	92.74	36.87	18.88
936	18.72	4.63	115.13	89.17	34.58	18.96
937	18.74	4.78	103.38	99.88	32.33	18.92
938	18.76	4.96	90.95	88.25	29.74	18.78
939	18.78	5.04	75.64	82.46	27.36	18.58
940	18.80	4.96	60.22	75.45	25.32	18.34
941	18.82	4.86	48.24	68.37	23.77	18.08
942	18.84	4.74	40.26	64.80	22.87	17.87
943	18.86	4.54	35.58	62.22	22.41	17.69
944	18.88	4.44	31.93	61.78	22.25	17.57
945	18.90	4.39	30.33	60.55	22.48	17.57
946	18.92	4.45	36.09	60.98	23.49	17.76
947	18.94	4.63	48.49	59.32	24.88	18.07
948	18.96	4.94	64.29	58.22	25.51	18.37
949	18.98	5.40	75.98	58.52	25.41	18.56
950	19.07	5.56	78.00	58.65	25.10	18.64
951	19.07	5.56	78.00	58.65	24.95	18.66
952	19.07	5.59	79.22	58.71	24.51	18.77
953	19.08	6.38	97.12	79.08	22.73	18.98
954	19.10	7.86	114.81	88.31	19.94	19.11
955	19.12	8.69	101.03	94.22	17.54	19.12
956	19.22	8.68	88.31	95.63	16.12	19.03
957	19.22	8.68	88.31	95.63	15.71	18.97
958	19.14	8.66	86.87	95.69	15.51	18.72
959	19.22	6.95	42.20	91.57	15.17	18.34
960	19.24	6.54	32.97	90.40	14.53	17.82

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
961	19.26	6.27	31.17	89.42	14.94	17.62
962	19.28	5.63	27.49	85.60	15.93	17.45
963	19.30	4.98	22.52	82.77	5.00	17.21
964	19.32	4.38	19.06	80.68	5.00	17.00
965	19.34	3.89	18.29	79.45	21.35	16.88
966	19.36	3.55	18.44	79.51	25.13	17.01
967	19.38	3.22	27.96	76.31	30.93	17.30
968	19.40	2.81	40.04	64.80	39.11	17.67
969	19.42	2.50	55.38	56.49	45.95	17.89
970	19.44	2.47	58.62	53.48	49.85	18.06
971	19.46	2.54	66.98	50.46	50.22	18.17
972	19.48	2.69	72.49	48.55	49.37	18.37
973	19.50	3.08	90.43	47.38	47.24	18.62
974	19.52	3.62	111.86	47.75	41.78	18.88
975	19.54	4.75	118.94	51.82	34.22	19.07
976	19.56	6.29	119.81	58.34	27.29	19.18
977	19.58	7.46	118.40	60.25	22.76	19.20
978	19.60	7.82	106.92	58.71	20.02	19.12
979	19.62	7.87	86.93	54.83	18.43	18.94
980	19.64	7.58	72.90	50.46	17.51	18.71
981	19.66	7.11	62.39	48.06	17.43	18.47
982	19.68	6.40	48.99	47.08	17.61	18.14
983	19.70	5.53	31.21	45.35	18.91	17.80
984	19.72	4.54	31.30	170.09	20.20	17.53
985	19.74	4.52	29.48	165.85	22.01	17.49
986	19.76	4.42	30.31	164.12	22.15	17.51
987	19.78	4.53	32.49	154.40	21.98	17.57
988	19.81	4.85	34.09	138.89	20.54	17.63
989	19.82	5.40	32.68	100.55	18.58	17.65
990	19.84	5.83	31.72	85.29	16.93	17.64
991	19.86	5.98	31.34	60.55	16.41	17.59
992	19.88	5.60	28.42	49.42	17.32	17.51
993	19.90	4.83	26.94	51.51	19.12	17.32
994	19.92	4.12	21.18	58.09	21.33	17.10
995	19.94	3.73	18.07	58.15	23.10	16.90
996	19.96	3.50	18.29	58.95	26.84	17.10
997	19.98	3.28	34.25	56.49	32.44	17.46
998	20.00	2.97	46.07	29.17	40.13	17.88
999	20.02	2.74	65.62	28.06	47.90	18.14
1000	20.04	2.45	77.44	25.97	56.60	18.25
1001	20.06	1.89	76.25	21.42	66.13	18.23
1002	20.08	1.61	74.07	19.63	74.84	18.11
1003	20.10	1.52	65.78	42.09	75.77	17.98
1004	20.12	1.64	56.61	87.63	73.06	17.88
1005	20.14	1.67	57.25	87.26	67.44	17.94
1006	20.16	2.04	68.91	93.48	53.47	18.16
1007	20.18	3.60	73.05	114.52	38.84	18.41
1008	20.20	5.16	75.54	141.85	29.45	18.54

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
1009	20.22	5.60	72.53	142.28	25.18	18.55
1010	20.24	5.66	65.41	142.03	23.35	18.42
1011	20.26	5.55	51.60	140.37	21.81	18.17
1012	20.28	5.31	36.41	136.55	20.41	17.86
1013	20.30	5.11	30.10	133.48	19.43	17.59
1014	20.32	5.06	28.31	132.74	19.04	17.49
1015	20.34	5.16	28.60	134.34	18.50	17.51
1016	20.36	5.53	30.81	140.68	17.75	17.55
1017	20.38	5.74	30.42	144.55	16.82	17.58
1018	20.40	5.93	29.17	148.37	15.99	17.56
1019	20.42	6.10	28.53	151.20	5.00	17.53
1020	20.44	6.20	27.57	153.97	5.00	17.51
1021	20.46	6.23	27.25	154.46	5.00	17.48
1022	20.48	6.13	25.97	153.42	5.00	17.42
1023	20.50	5.91	24.14	150.40	5.00	17.34
1024	20.52	5.53	23.18	145.23	5.00	17.29
1025	20.54	5.32	23.47	143.08	5.00	17.26

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (m)
q_c:	Measured cone resistance (MPa)
f_s:	Sleeve friction resistance (kPa)
u:	Pore pressure (kPa)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (kN/m^3)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1	0.02	0.32	0.20	0.12	1.00	0.389	1.43	0.272	1.10	1.00	0.329	No
2	0.05	0.81	0.49	0.32	1.00	0.376	1.43	0.263	1.10	1.00	0.318	No
3	0.06	0.98	0.59	0.39	1.00	0.374	1.43	0.262	1.10	1.00	0.316	No
4	0.08	1.32	0.78	0.53	1.00	0.370	1.43	0.259	1.10	1.00	0.312	No
5	0.10	1.66	0.98	0.68	1.00	0.366	1.43	0.257	1.10	1.00	0.310	No
6	0.12	2.00	1.18	0.82	1.00	0.364	1.43	0.254	1.10	1.00	0.307	No
7	0.14	2.34	1.37	0.97	1.00	0.361	1.43	0.253	1.10	1.00	0.305	No
8	0.16	2.69	1.57	1.12	1.00	0.358	1.43	0.251	1.10	1.00	0.302	No
9	0.18	3.04	1.77	1.28	1.00	0.356	1.43	0.249	1.10	1.00	0.299	No
10	0.20	3.40	1.96	1.44	1.00	0.354	1.43	0.248	1.10	1.00	0.295	No
11	0.22	3.76	2.16	1.60	1.00	0.352	1.43	0.246	1.10	1.00	0.292	No
12	0.24	4.11	2.35	1.76	1.00	0.350	1.43	0.245	1.10	1.00	0.290	No
13	0.26	4.47	2.55	1.92	1.00	0.348	1.43	0.244	1.10	1.00	0.288	No
14	0.28	4.83	2.75	2.08	1.00	0.346	1.43	0.243	1.10	1.00	0.286	No
15	0.30	5.19	2.94	2.25	1.00	0.345	1.43	0.242	1.10	1.00	0.285	No
16	0.32	5.56	3.14	2.42	1.00	0.344	1.43	0.241	1.10	1.00	0.284	No
17	0.34	5.92	3.34	2.59	1.00	0.342	1.43	0.240	1.10	1.00	0.283	No
18	0.36	6.29	3.53	2.76	1.00	0.341	1.43	0.239	1.10	1.00	0.282	No
19	0.38	6.66	3.73	2.93	1.00	0.340	1.43	0.238	1.10	1.00	0.280	No
20	0.40	7.03	3.92	3.11	1.00	0.338	1.43	0.237	1.10	1.00	0.280	No
21	0.42	7.40	4.12	3.28	1.00	0.337	1.43	0.236	1.10	1.00	0.279	No
22	0.44	7.77	4.32	3.46	1.00	0.336	1.43	0.235	1.10	1.00	0.279	No
23	0.46	8.15	4.51	3.63	1.00	0.335	1.43	0.235	1.10	1.00	0.278	No
24	0.48	8.52	4.71	3.81	1.00	0.334	1.43	0.234	1.10	1.00	0.278	No
25	0.50	8.89	4.91	3.98	1.00	0.334	1.43	0.234	1.10	1.00	0.278	No
26	0.52	9.26	5.10	4.16	1.00	0.333	1.43	0.233	1.10	1.00	0.277	No
27	0.54	9.63	5.30	4.33	1.00	0.332	1.43	0.233	1.10	1.00	0.277	No
28	0.56	10.00	5.49	4.50	1.00	0.332	1.43	0.232	1.10	1.00	0.277	No
29	0.58	10.36	5.69	4.67	1.00	0.331	1.43	0.232	1.10	1.00	0.276	No
30	0.60	10.73	5.89	4.85	1.00	0.331	1.43	0.232	1.10	1.00	0.276	No
31	0.62	11.10	6.08	5.02	1.00	0.331	1.43	0.231	1.10	1.00	0.275	No
32	0.64	11.47	6.28	5.19	1.00	0.330	1.43	0.231	1.10	1.00	0.275	No
33	0.66	11.83	6.47	5.36	1.00	0.330	1.43	0.231	1.10	1.00	0.275	No
34	0.68	12.20	6.67	5.53	1.00	0.330	1.43	0.231	1.10	1.00	0.275	No
35	0.70	12.57	6.87	5.70	1.00	0.329	1.43	0.230	1.10	1.00	0.274	No
36	0.72	12.93	7.06	5.87	1.00	0.329	1.43	0.230	1.10	1.00	0.274	No
37	0.74	13.30	7.26	6.04	1.00	0.329	1.43	0.230	1.10	1.00	0.274	No
38	0.76	13.66	7.46	6.21	1.00	0.328	1.43	0.230	1.10	1.00	0.274	No
39	0.78	14.03	7.65	6.38	1.00	0.328	1.43	0.230	1.10	1.00	0.274	No
40	0.80	14.39	7.85	6.55	1.00	0.328	1.43	0.229	1.10	1.00	0.274	No
41	0.82	14.76	8.04	6.72	1.00	0.328	1.43	0.229	1.10	1.00	0.274	No
42	0.84	15.12	8.24	6.88	1.00	0.327	1.43	0.229	1.10	1.00	0.274	No
43	1.04	18.75	10.20	8.55	0.99	0.326	1.43	0.228	1.10	1.00	0.273	No
44	1.04	18.75	10.20	8.55	0.99	0.326	1.43	0.228	1.10	1.00	0.273	No
45	1.04	18.75	10.20	8.55	0.99	0.326	1.43	0.228	1.10	1.00	0.273	No
46	1.04	18.75	10.20	8.55	0.99	0.326	1.43	0.228	1.10	1.00	0.273	No
47	1.04	18.75	10.20	8.55	0.99	0.326	1.43	0.228	1.10	1.00	0.273	No
48	0.96	17.32	9.42	7.90	1.00	0.326	1.43	0.228	1.10	1.00	0.273	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
49	0.98	17.67	9.61	8.06	0.99	0.326	1.43	0.228	1.10	1.00	0.273	No
50	1.00	18.03	9.81	8.22	0.99	0.326	1.43	0.228	1.10	1.00	0.273	No
51	1.02	18.39	10.01	8.38	0.99	0.326	1.43	0.228	1.10	1.00	0.273	No
52	1.04	18.74	10.20	8.54	0.99	0.326	1.43	0.228	1.10	1.00	0.273	No
53	1.06	19.10	10.40	8.70	0.99	0.326	1.43	0.228	1.10	1.00	0.273	No
54	1.08	19.46	10.59	8.86	0.99	0.326	1.43	0.228	1.10	1.00	0.272	No
55	1.10	19.82	10.79	9.02	0.99	0.326	1.43	0.228	1.10	1.00	0.272	No
56	1.12	20.18	10.99	9.19	0.99	0.326	1.43	0.228	1.10	1.00	0.272	No
57	1.14	20.54	11.18	9.35	0.99	0.326	1.43	0.228	1.10	1.00	0.272	No
58	1.16	20.90	11.38	9.52	0.99	0.326	1.43	0.228	1.10	1.00	0.273	No
59	1.18	21.26	11.58	9.68	0.99	0.326	1.43	0.228	1.10	1.00	0.273	No
60	1.20	21.62	11.77	9.85	0.99	0.325	1.43	0.228	1.10	1.00	0.273	No
61	1.32	23.78	12.95	10.83	0.99	0.325	1.43	0.227	1.10	1.00	0.272	No
62	1.32	23.78	12.95	10.83	0.99	0.325	1.43	0.227	1.10	1.00	0.272	No
63	1.32	23.78	12.95	10.83	0.99	0.325	1.43	0.227	1.10	1.00	0.272	No
64	1.32	23.78	12.95	10.83	0.99	0.325	1.43	0.227	1.10	1.00	0.272	No
65	1.30	23.42	12.75	10.67	0.99	0.325	1.43	0.227	1.10	1.00	0.273	No
66	1.32	23.78	12.95	10.83	0.99	0.325	1.43	0.227	1.10	1.00	0.273	No
67	1.34	24.14	13.15	11.00	0.99	0.325	1.43	0.227	1.10	1.00	0.273	No
68	1.36	24.50	13.34	11.16	0.99	0.325	1.43	0.227	1.10	1.00	0.273	No
69	1.38	24.86	13.54	11.32	0.99	0.325	1.43	0.227	1.10	1.00	0.273	No
70	1.40	25.22	13.73	11.48	0.99	0.325	1.43	0.227	1.10	1.00	0.272	No
71	1.42	25.58	13.93	11.65	0.99	0.324	1.43	0.227	1.10	1.00	0.272	No
72	1.44	25.93	14.13	11.81	0.99	0.324	1.43	0.227	1.10	1.00	0.272	No
73	1.46	26.29	14.32	11.97	0.99	0.324	1.43	0.227	1.10	1.00	0.271	No
74	1.49	26.83	14.62	12.22	0.99	0.324	1.43	0.227	1.10	1.00	0.270	No
75	1.50	27.01	14.72	12.30	0.99	0.324	1.43	0.227	1.10	1.00	0.269	No
76	1.53	27.55	15.01	12.54	0.99	0.324	1.43	0.227	1.10	1.00	0.269	No
77	1.54	27.73	15.11	12.63	0.99	0.324	1.43	0.227	1.10	1.00	0.269	No
78	1.56	28.09	15.30	12.79	0.99	0.324	1.43	0.227	1.10	1.00	0.269	No
79	1.58	28.45	15.50	12.95	0.99	0.324	1.43	0.227	1.10	1.00	0.269	No
80	1.60	28.81	15.70	13.12	0.99	0.324	1.43	0.226	1.10	1.00	0.269	No
81	1.62	29.17	15.89	13.28	0.99	0.324	1.43	0.226	1.10	1.00	0.269	No
82	1.64	29.53	16.09	13.44	0.98	0.323	1.43	0.226	1.10	1.00	0.270	No
83	1.66	29.88	16.28	13.60	0.98	0.323	1.43	0.226	1.10	1.00	0.270	No
84	1.68	30.24	16.48	13.76	0.98	0.323	1.43	0.226	1.10	1.00	0.270	No
85	1.70	30.59	16.68	13.91	0.98	0.323	1.43	0.226	1.10	1.00	0.270	No
86	1.72	30.94	16.87	14.07	0.98	0.323	1.43	0.226	1.10	1.00	0.271	No
87	1.74	31.29	17.07	14.22	0.98	0.323	1.43	0.226	1.10	1.00	0.271	No
88	1.76	31.64	17.27	14.38	0.98	0.323	1.43	0.226	1.10	1.00	0.271	No
89	1.78	31.99	17.46	14.53	0.98	0.323	1.43	0.226	1.10	1.00	0.272	No
90	1.80	32.34	17.66	14.68	0.98	0.323	1.43	0.226	1.10	1.00	0.272	No
91	1.82	32.69	17.85	14.84	0.98	0.323	1.43	0.226	1.10	1.00	0.272	No
92	1.84	33.04	18.05	14.98	0.98	0.323	1.43	0.226	1.10	1.00	0.272	No
93	1.86	33.38	18.25	15.13	0.98	0.324	1.43	0.226	1.10	1.00	0.273	No
94	1.88	33.72	18.44	15.28	0.98	0.324	1.43	0.227	1.10	1.00	0.272	No
95	1.91	34.24	18.74	15.50	0.98	0.324	1.43	0.227	1.10	1.00	0.272	No
96	1.92	34.41	18.84	15.57	0.98	0.324	1.43	0.227	1.10	1.00	0.273	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
97	1.94	34.75	19.03	15.71	0.98	0.324	1.43	0.227	1.10	1.00	0.273	No
98	1.96	35.08	19.23	15.86	0.98	0.324	1.43	0.227	1.10	1.00	0.273	No
99	1.98	35.42	19.42	16.00	0.98	0.324	1.43	0.227	1.10	1.00	0.273	No
100	2.00	35.76	19.62	16.14	0.98	0.324	1.43	0.227	1.10	1.00	0.273	No
101	2.02	36.09	19.82	16.28	0.98	0.324	1.43	0.227	1.10	1.00	0.274	No
102	2.04	36.43	20.01	16.42	0.98	0.325	1.43	0.227	1.10	1.00	0.274	No
103	2.06	36.76	20.21	16.56	0.98	0.325	1.43	0.227	1.10	1.00	0.274	No
104	2.08	37.10	20.40	16.69	0.98	0.325	1.43	0.227	1.10	1.00	0.274	No
105	2.10	37.43	20.60	16.83	0.98	0.325	1.43	0.227	1.10	1.00	0.275	No
106	2.13	37.93	20.90	17.04	0.98	0.325	1.43	0.228	1.10	1.00	0.275	No
107	2.14	38.10	20.99	17.10	0.98	0.325	1.43	0.228	1.10	1.00	0.275	No
108	2.16	38.43	21.19	17.24	0.98	0.325	1.43	0.228	1.10	1.00	0.276	No
109	2.18	38.76	21.39	17.37	0.98	0.325	1.43	0.228	1.10	1.00	0.276	No
110	2.20	39.09	21.58	17.51	0.98	0.326	1.43	0.228	1.10	1.00	0.276	No
111	2.22	39.41	21.78	17.64	0.98	0.326	1.43	0.228	1.10	1.00	0.276	No
112	2.24	39.74	21.97	17.77	0.97	0.326	1.43	0.228	1.10	1.00	0.276	No
113	2.26	40.06	22.17	17.89	0.97	0.326	1.43	0.228	1.10	1.00	0.276	No
114	2.28	40.39	22.37	18.02	0.97	0.326	1.43	0.228	1.10	1.00	0.276	No
115	2.30	40.71	22.56	18.15	0.97	0.327	1.43	0.229	1.10	1.00	0.276	No
116	2.32	41.04	22.76	18.28	0.97	0.327	1.43	0.229	1.10	1.00	0.276	No
117	2.34	41.36	22.96	18.41	0.97	0.327	1.43	0.229	1.10	1.00	0.276	No
118	2.37	41.85	23.25	18.60	0.97	0.327	1.43	0.229	1.10	1.00	0.276	No
119	2.38	42.01	23.35	18.66	0.97	0.327	1.43	0.229	1.10	1.00	0.277	No
120	2.42	42.65	23.74	18.91	0.97	0.328	1.43	0.229	1.10	1.00	0.277	No
121	2.42	42.65	23.74	18.91	0.97	0.328	1.43	0.229	1.10	1.00	0.278	No
122	2.44	42.97	23.94	19.03	0.97	0.328	1.43	0.230	1.10	1.00	0.278	No
123	2.46	43.28	24.13	19.15	0.97	0.328	1.43	0.230	1.10	1.00	0.278	No
124	2.48	43.60	24.33	19.27	0.97	0.328	1.43	0.230	1.10	1.00	0.278	No
125	2.50	43.92	24.53	19.40	0.97	0.329	1.43	0.230	1.10	1.00	0.278	No
126	2.52	44.24	24.72	19.52	0.97	0.329	1.43	0.230	1.10	1.00	0.278	No
127	2.54	44.56	24.92	19.64	0.97	0.329	1.43	0.230	1.10	1.00	0.278	No
128	2.56	44.88	25.11	19.76	0.97	0.329	1.43	0.230	1.10	1.00	0.278	No
129	2.58	45.20	25.31	19.89	0.97	0.329	1.43	0.230	1.10	1.00	0.278	No
130	2.60	45.52	25.51	20.01	0.97	0.329	1.43	0.231	1.10	1.00	0.278	No
131	2.62	45.84	25.70	20.14	0.97	0.330	1.43	0.231	1.10	1.00	0.278	No
132	2.64	46.16	25.90	20.26	0.97	0.330	1.43	0.231	1.10	1.00	0.278	No
133	2.66	46.48	26.09	20.39	0.97	0.330	1.43	0.231	1.10	1.00	0.278	No
134	2.68	46.81	26.29	20.52	0.97	0.330	1.43	0.231	1.10	1.00	0.279	No
135	2.70	47.13	26.49	20.65	0.97	0.330	1.43	0.231	1.10	1.00	0.279	No
136	2.72	47.46	26.68	20.78	0.97	0.330	1.43	0.231	1.10	1.00	0.279	No
137	2.74	47.78	26.88	20.90	0.97	0.330	1.43	0.231	1.10	1.00	0.279	No
138	2.76	48.11	27.08	21.03	0.97	0.330	1.43	0.231	1.10	1.00	0.279	No
139	2.78	48.43	27.27	21.16	0.97	0.330	1.43	0.231	1.10	1.00	0.279	No
140	2.80	48.76	27.47	21.29	0.97	0.330	1.43	0.231	1.10	1.00	0.279	No
141	2.82	49.08	27.66	21.42	0.96	0.331	1.43	0.231	1.10	1.00	0.280	No
142	2.84	49.40	27.86	21.54	0.96	0.331	1.43	0.231	1.10	1.00	0.280	No
143	2.86	49.73	28.06	21.67	0.96	0.331	1.43	0.231	1.10	1.00	0.280	No
144	2.89	50.22	28.35	21.87	0.96	0.331	1.43	0.232	1.10	1.00	0.280	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
145	2.90	50.38	28.45	21.93	0.96	0.331	1.43	0.232	1.10	1.00	0.280	No
146	2.92	50.71	28.65	22.06	0.96	0.331	1.43	0.232	1.10	1.00	0.281	No
147	2.94	51.04	28.84	22.20	0.96	0.331	1.43	0.232	1.10	1.00	0.281	No
148	2.96	51.36	29.04	22.33	0.96	0.331	1.43	0.232	1.10	1.00	0.281	No
149	2.99	51.85	29.33	22.52	0.96	0.331	1.43	0.232	1.10	1.00	0.281	No
150	3.00	52.02	29.43	22.59	0.96	0.331	1.43	0.232	1.10	1.00	0.281	No
151	3.03	52.50	29.72	22.78	0.96	0.331	1.43	0.232	1.10	1.00	0.281	No
152	3.05	52.82	29.92	22.90	0.96	0.331	1.43	0.232	1.10	1.00	0.281	No
153	3.06	52.99	30.02	22.97	0.96	0.331	1.43	0.232	1.10	1.00	0.281	No
154	3.08	53.30	30.21	23.09	0.96	0.331	1.43	0.232	1.10	1.00	0.281	No
155	3.10	53.62	30.41	23.21	0.96	0.331	1.43	0.232	1.10	1.00	0.281	No
156	3.12	53.94	30.61	23.33	0.96	0.332	1.43	0.232	1.10	1.00	0.281	No
157	3.14	54.26	30.80	23.45	0.96	0.332	1.43	0.232	1.10	1.00	0.281	No
158	3.16	54.58	31.00	23.58	0.96	0.332	1.43	0.232	1.10	1.00	0.281	No
159	3.18	54.89	31.20	23.70	0.96	0.332	1.43	0.232	1.10	1.00	0.282	No
160	3.20	55.21	31.39	23.82	0.96	0.332	1.43	0.232	1.10	1.00	0.282	No
161	3.22	55.52	31.59	23.94	0.96	0.332	1.43	0.232	1.10	1.00	0.282	No
162	3.24	55.84	31.78	24.05	0.96	0.332	1.43	0.233	1.10	1.00	0.282	No
163	3.26	56.15	31.98	24.17	0.96	0.332	1.43	0.233	1.10	1.00	0.282	No
164	3.28	56.47	32.18	24.29	0.96	0.332	1.43	0.233	1.10	1.00	2.000	Yes
165	3.30	56.79	32.37	24.42	0.96	0.332	1.43	0.233	1.10	1.00	2.000	Yes
166	3.32	57.11	32.57	24.54	0.96	0.332	1.43	0.233	1.10	1.00	2.000	Yes
167	3.34	57.44	32.77	24.67	0.96	0.332	1.43	0.233	1.10	1.00	2.000	Yes
168	3.36	57.77	32.96	24.81	0.95	0.332	1.43	0.233	1.10	1.00	0.275	No
169	3.38	58.10	33.16	24.94	0.95	0.332	1.43	0.233	1.10	1.00	2.000	Yes
170	3.40	58.43	33.35	25.08	0.95	0.332	1.43	0.233	1.10	1.00	2.000	Yes
171	3.42	58.76	33.55	25.21	0.95	0.332	1.43	0.233	1.10	1.00	2.000	Yes
172	3.44	59.08	33.75	25.34	0.95	0.332	1.43	0.233	1.10	1.00	2.000	Yes
173	3.46	59.41	33.94	25.46	0.95	0.332	1.43	0.233	1.10	1.00	2.000	Yes
174	3.48	59.73	34.14	25.59	0.95	0.332	1.43	0.233	1.10	1.00	2.000	Yes
175	3.50	60.04	34.34	25.71	0.95	0.332	1.43	0.233	1.10	1.00	2.000	Yes
176	3.52	60.36	34.53	25.83	0.95	0.333	1.43	0.233	1.10	1.00	0.281	No
177	3.54	60.67	34.73	25.95	0.95	0.333	1.43	0.233	1.10	1.00	0.281	No
178	3.56	60.99	34.92	26.06	0.95	0.333	1.43	0.233	1.10	1.00	0.281	No
179	3.58	61.30	35.12	26.18	0.95	0.333	1.43	0.233	1.10	1.00	0.281	No
180	3.60	61.62	35.32	26.30	0.95	0.333	1.43	0.233	1.10	1.00	0.281	No
181	3.62	61.93	35.51	26.42	0.95	0.333	1.43	0.233	1.10	1.00	0.281	No
182	3.64	62.25	35.71	26.54	0.95	0.333	1.43	0.233	1.10	1.00	0.281	No
183	3.66	62.57	35.90	26.67	0.95	0.333	1.43	0.233	1.10	1.00	0.281	No
184	3.68	62.89	36.10	26.79	0.95	0.333	1.43	0.233	1.10	1.00	0.281	No
185	3.70	63.22	36.30	26.92	0.95	0.333	1.43	0.233	1.10	1.00	0.281	No
186	3.72	63.54	36.49	27.05	0.95	0.333	1.43	0.233	1.10	1.00	0.281	No
187	3.74	63.87	36.69	27.18	0.95	0.333	1.43	0.233	1.10	1.00	0.281	No
188	3.76	64.20	36.89	27.31	0.95	0.333	1.43	0.233	1.10	1.00	0.281	No
189	3.78	64.54	37.08	27.45	0.95	0.333	1.43	0.233	1.10	1.00	0.281	No
190	3.80	64.88	37.28	27.60	0.95	0.333	1.43	0.233	1.10	1.00	0.281	No
191	3.82	65.22	37.47	27.74	0.95	0.332	1.43	0.233	1.10	1.00	0.281	No
192	3.84	65.56	37.67	27.89	0.95	0.332	1.43	0.233	1.10	1.00	0.281	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
193	3.86	65.91	37.87	28.04	0.95	0.332	1.43	0.233	1.10	1.00	0.281	No
194	3.88	66.25	38.06	28.19	0.94	0.332	1.43	0.232	1.10	1.00	0.280	No
195	3.90	66.60	38.26	28.34	0.94	0.332	1.43	0.232	1.10	1.00	0.280	No
196	3.92	66.94	38.46	28.48	0.94	0.332	1.43	0.232	1.10	1.00	0.280	No
197	3.94	67.28	38.65	28.63	0.94	0.332	1.43	0.232	1.10	1.00	0.280	No
198	3.96	67.63	38.85	28.78	0.94	0.331	1.43	0.232	1.10	1.00	0.280	No
199	3.98	67.97	39.04	28.93	0.94	0.331	1.43	0.232	1.10	1.00	0.280	No
200	4.00	68.31	39.24	29.07	0.94	0.331	1.43	0.232	1.10	1.00	0.280	No
201	4.02	68.65	39.44	29.22	0.94	0.331	1.43	0.232	1.10	1.00	0.280	No
202	4.04	69.00	39.63	29.36	0.94	0.331	1.43	0.232	1.10	1.00	0.279	No
203	4.06	69.34	39.83	29.51	0.94	0.331	1.43	0.231	1.10	1.00	0.279	No
204	4.08	69.68	40.02	29.66	0.94	0.331	1.43	0.231	1.10	1.00	0.279	No
205	4.10	70.02	40.22	29.80	0.94	0.330	1.43	0.231	1.10	1.00	0.279	No
206	4.12	70.37	40.42	29.95	0.94	0.330	1.43	0.231	1.10	1.00	0.279	No
207	4.14	70.71	40.61	30.10	0.94	0.330	1.43	0.231	1.10	1.00	0.278	No
208	4.16	71.06	40.81	30.25	0.94	0.330	1.43	0.231	1.10	1.00	0.277	No
209	4.18	71.40	41.01	30.40	0.94	0.330	1.43	0.231	1.10	1.00	0.277	No
210	4.20	71.75	41.20	30.55	0.94	0.330	1.43	0.231	1.10	1.00	0.276	No
211	4.22	72.10	41.40	30.70	0.94	0.329	1.43	0.231	1.10	1.00	0.276	No
212	4.24	72.45	41.59	30.86	0.94	0.329	1.43	0.230	1.10	1.00	0.276	No
213	4.26	72.80	41.79	31.01	0.94	0.329	1.43	0.230	1.10	1.00	0.276	No
214	4.28	73.16	41.99	31.17	0.94	0.329	1.43	0.230	1.10	1.00	0.275	No
215	4.30	73.51	42.18	31.33	0.94	0.329	1.43	0.230	1.10	1.00	0.275	No
216	4.32	73.87	42.38	31.49	0.94	0.328	1.43	0.230	1.10	1.00	0.274	No
217	4.34	74.23	42.58	31.65	0.94	0.328	1.43	0.230	1.10	1.00	0.274	No
218	4.36	74.59	42.77	31.81	0.94	0.328	1.43	0.229	1.10	1.00	0.274	No
219	4.38	74.94	42.97	31.98	0.93	0.328	1.43	0.229	1.10	1.00	0.274	No
220	4.40	75.30	43.16	32.14	0.93	0.327	1.43	0.229	1.10	1.00	0.273	No
221	4.42	75.66	43.36	32.30	0.93	0.327	1.43	0.229	1.10	1.00	0.273	No
222	4.44	76.03	43.56	32.47	0.93	0.327	1.43	0.229	1.10	1.00	0.273	No
223	4.46	76.39	43.75	32.63	0.93	0.327	1.43	0.229	1.10	1.00	0.273	No
224	4.48	76.75	43.95	32.80	0.93	0.326	1.43	0.228	1.10	1.00	0.273	No
225	4.50	77.11	44.15	32.96	0.93	0.326	1.43	0.228	1.10	1.00	0.274	No
226	4.52	77.47	44.34	33.13	0.93	0.326	1.43	0.228	1.10	1.00	0.274	No
227	4.54	77.83	44.54	33.29	0.93	0.326	1.43	0.228	1.10	1.00	0.274	No
228	4.56	78.19	44.73	33.45	0.93	0.325	1.43	0.228	1.10	1.00	0.274	No
229	4.58	78.55	44.93	33.62	0.93	0.325	1.43	0.228	1.10	1.00	0.273	No
230	4.60	78.90	45.13	33.78	0.93	0.325	1.43	0.227	1.10	1.00	0.273	No
231	4.62	79.26	45.32	33.94	0.93	0.325	1.43	0.227	1.10	1.00	0.272	No
232	4.68	80.33	45.91	34.42	0.93	0.324	1.43	0.227	1.09	1.00	0.272	No
233	4.68	80.33	45.91	34.42	0.93	0.324	1.43	0.227	1.09	1.00	0.272	No
234	4.68	80.33	45.91	34.42	0.93	0.324	1.43	0.227	1.09	1.00	0.272	No
235	4.70	80.69	46.11	34.58	0.93	0.324	1.43	0.227	1.09	1.00	0.273	No
236	4.72	81.04	46.30	34.74	0.93	0.324	1.43	0.227	1.09	1.00	0.273	No
237	4.74	81.40	46.50	34.90	0.93	0.323	1.43	0.226	1.09	1.00	0.273	No
238	4.76	81.76	46.70	35.06	0.93	0.323	1.43	0.226	1.09	1.00	0.273	No
239	4.78	82.12	46.89	35.22	0.93	0.323	1.43	0.226	1.09	1.00	0.273	No
240	4.80	82.47	47.09	35.39	0.93	0.323	1.43	0.226	1.09	1.00	0.273	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
241	4.82	82.83	47.28	35.55	0.93	0.323	1.43	0.226	1.09	1.00	0.273	No
242	4.84	83.19	47.48	35.71	0.93	0.322	1.43	0.226	1.09	1.00	0.273	No
243	4.86	83.55	47.68	35.87	0.93	0.322	1.43	0.225	1.09	1.00	0.273	No
244	4.89	84.09	47.97	36.11	0.92	0.322	1.43	0.225	1.09	1.00	0.273	No
245	4.90	84.26	48.07	36.20	0.92	0.322	1.43	0.225	1.09	1.00	0.273	No
246	4.93	84.80	48.36	36.44	0.92	0.321	1.43	0.225	1.09	1.00	0.273	No
247	4.94	84.98	48.46	36.52	0.92	0.321	1.43	0.225	1.09	1.00	0.273	No
248	4.96	85.34	48.66	36.68	0.92	0.321	1.43	0.225	1.09	1.00	0.273	No
249	4.98	85.69	48.85	36.84	0.92	0.321	1.43	0.225	1.09	1.00	0.273	No
250	5.01	86.23	49.15	37.08	0.92	0.321	1.43	0.224	1.09	1.00	0.273	No
251	5.02	86.41	49.25	37.16	0.92	0.320	1.43	0.224	1.08	1.00	0.273	No
252	5.04	86.76	49.44	37.32	0.92	0.320	1.43	0.224	1.08	1.00	0.273	No
253	5.06	87.12	49.64	37.48	0.92	0.320	1.43	0.224	1.08	1.00	0.274	No
254	5.08	87.47	49.83	37.64	0.92	0.320	1.43	0.224	1.08	1.00	0.273	No
255	5.10	87.82	50.03	37.79	0.92	0.320	1.43	0.224	1.08	1.00	0.273	No
256	5.12	88.18	50.23	37.95	0.92	0.319	1.43	0.224	1.08	1.00	0.273	No
257	5.14	88.53	50.42	38.11	0.92	0.319	1.43	0.223	1.08	1.00	0.273	No
258	5.16	88.88	50.62	38.26	0.92	0.319	1.43	0.223	1.08	1.00	0.273	No
259	5.18	89.24	50.82	38.42	0.92	0.319	1.43	0.223	1.08	1.00	0.272	No
260	5.20	89.59	51.01	38.58	0.92	0.319	1.43	0.223	1.08	1.00	0.272	No
261	5.22	89.94	51.21	38.73	0.92	0.319	1.43	0.223	1.08	1.00	0.272	No
262	5.24	90.29	51.40	38.88	0.92	0.318	1.43	0.223	1.08	1.00	0.272	No
263	5.26	90.64	51.60	39.04	0.92	0.318	1.43	0.223	1.08	1.00	0.272	No
264	5.28	90.99	51.80	39.19	0.92	0.318	1.43	0.223	1.08	1.00	0.272	No
265	5.30	91.34	51.99	39.35	0.92	0.318	1.43	0.222	1.08	1.00	0.272	No
266	5.32	91.69	52.19	39.50	0.92	0.318	1.43	0.222	1.08	1.00	0.272	No
267	5.34	92.04	52.39	39.65	0.92	0.318	1.43	0.222	1.08	1.00	0.273	No
268	5.36	92.39	52.58	39.81	0.91	0.317	1.43	0.222	1.08	1.00	0.273	No
269	5.38	92.74	52.78	39.96	0.91	0.317	1.43	0.222	1.08	1.00	0.272	No
270	5.40	93.09	52.97	40.12	0.91	0.317	1.43	0.222	1.08	1.00	0.272	No
271	5.42	93.44	53.17	40.27	0.91	0.317	1.43	0.222	1.08	1.00	0.272	No
272	5.44	93.79	53.37	40.42	0.91	0.317	1.43	0.222	1.08	1.00	0.272	No
273	5.46	94.14	53.56	40.57	0.91	0.316	1.43	0.222	1.08	1.00	0.272	No
274	5.48	94.48	53.76	40.72	0.91	0.316	1.43	0.221	1.08	1.00	0.272	No
275	5.51	94.99	54.05	40.94	0.91	0.316	1.43	0.221	1.08	1.00	0.269	No
276	5.52	95.16	54.15	41.01	0.91	0.316	1.43	0.221	1.08	1.00	0.268	No
277	5.54	95.51	54.35	41.16	0.91	0.316	1.43	0.221	1.08	1.00	0.269	No
278	5.56	95.85	54.54	41.31	0.91	0.316	1.43	0.221	1.08	1.00	0.271	No
279	5.58	96.19	54.74	41.45	0.91	0.316	1.43	0.221	1.08	1.00	0.271	No
280	5.60	96.53	54.94	41.60	0.91	0.316	1.43	0.221	1.08	1.00	0.272	No
281	5.62	96.87	55.13	41.74	0.91	0.315	1.43	0.221	1.07	1.00	0.272	No
282	5.64	97.21	55.33	41.88	0.91	0.315	1.43	0.221	1.07	1.00	0.272	No
283	5.66	97.55	55.52	42.02	0.91	0.315	1.43	0.221	1.07	1.00	0.271	No
284	5.68	97.89	55.72	42.17	0.91	0.315	1.43	0.221	1.07	1.00	0.271	No
285	5.70	98.23	55.92	42.31	0.91	0.315	1.43	0.220	1.07	1.00	0.270	No
286	5.72	98.57	56.11	42.46	0.91	0.315	1.43	0.220	1.08	1.00	0.270	No
287	5.74	98.92	56.31	42.61	0.91	0.315	1.43	0.220	1.08	1.00	0.269	No
288	5.76	99.26	56.51	42.76	0.91	0.314	1.43	0.220	1.08	1.00	0.268	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
289	5.78	99.61	56.70	42.91	0.91	0.314	1.43	0.220	1.08	1.00	0.268	No
290	5.80	99.96	56.90	43.06	0.91	0.314	1.43	0.220	1.08	1.00	0.268	No
291	5.82	100.31	57.09	43.22	0.90	0.314	1.43	0.220	1.08	1.00	0.266	No
292	5.84	100.67	57.29	43.38	0.90	0.314	1.43	0.220	1.07	1.00	0.268	No
293	5.86	101.02	57.49	43.53	0.90	0.314	1.43	0.219	1.07	1.00	0.269	No
294	5.88	101.37	57.68	43.69	0.90	0.313	1.43	0.219	1.07	1.00	0.270	No
295	5.90	101.72	57.88	43.84	0.90	0.313	1.43	0.219	1.07	1.00	0.270	No
296	5.92	102.07	58.08	43.99	0.90	0.313	1.43	0.219	1.07	1.00	0.270	No
297	5.94	102.41	58.27	44.14	0.90	0.313	1.43	0.219	1.07	1.00	0.270	No
298	5.96	102.76	58.47	44.29	0.90	0.313	1.43	0.219	1.07	1.00	0.269	No
299	5.98	103.11	58.66	44.44	0.90	0.313	1.43	0.219	1.07	1.00	0.269	No
300	6.00	103.45	58.86	44.59	0.90	0.312	1.43	0.219	1.07	1.00	0.268	No
301	6.02	103.80	59.06	44.75	0.90	0.312	1.43	0.219	1.07	1.00	0.268	No
302	6.04	104.15	59.25	44.90	0.90	0.312	1.43	0.218	1.07	1.00	0.268	No
303	6.06	104.51	59.45	45.06	0.90	0.312	1.43	0.218	1.07	1.00	0.267	No
304	6.08	104.86	59.64	45.22	0.90	0.312	1.43	0.218	1.07	1.00	0.267	No
305	6.10	105.22	59.84	45.38	0.90	0.311	1.43	0.218	1.07	1.00	0.267	No
306	6.12	105.58	60.04	45.54	0.90	0.311	1.43	0.218	1.07	1.00	0.266	No
307	6.14	105.94	60.23	45.71	0.90	0.311	1.43	0.218	1.07	1.00	0.266	No
308	6.16	106.30	60.43	45.88	0.90	0.311	1.43	0.218	1.07	1.00	0.265	No
309	6.18	106.67	60.63	46.04	0.90	0.311	1.43	0.217	1.07	1.00	0.265	No
310	6.20	107.03	60.82	46.21	0.90	0.310	1.43	0.217	1.07	1.00	0.265	No
311	6.22	107.40	61.02	46.38	0.90	0.310	1.43	0.217	1.07	1.00	0.264	No
312	6.24	107.77	61.21	46.55	0.90	0.310	1.43	0.217	1.07	1.00	0.264	No
313	6.26	108.14	61.41	46.73	0.89	0.310	1.43	0.217	1.07	1.00	0.264	No
314	6.28	108.51	61.61	46.90	0.89	0.309	1.43	0.217	1.07	1.00	0.263	No
315	6.30	108.88	61.80	47.07	0.89	0.309	1.43	0.216	1.07	1.00	0.263	No
316	6.32	109.25	62.00	47.25	0.89	0.309	1.43	0.216	1.07	1.00	0.263	No
317	6.34	109.62	62.20	47.43	0.89	0.309	1.43	0.216	1.07	1.00	0.263	No
318	6.36	109.99	62.39	47.60	0.89	0.308	1.43	0.216	1.07	1.00	0.263	No
319	6.38	110.37	62.59	47.78	0.89	0.308	1.43	0.216	1.07	1.00	0.264	No
320	6.40	110.74	62.78	47.96	0.89	0.308	1.43	0.216	1.07	1.00	0.264	No
321	6.42	111.11	62.98	48.13	0.89	0.308	1.43	0.215	1.07	1.00	0.264	No
322	6.44	111.48	63.18	48.31	0.89	0.307	1.43	0.215	1.07	1.00	0.264	No
323	6.46	111.86	63.37	48.48	0.89	0.307	1.43	0.215	1.07	1.00	0.264	No
324	6.48	112.23	63.57	48.66	0.89	0.307	1.43	0.215	1.07	1.00	0.264	No
325	6.50	112.60	63.77	48.83	0.89	0.307	1.43	0.215	1.06	1.00	0.264	No
326	6.52	112.97	63.96	49.00	0.89	0.306	1.43	0.214	1.06	1.00	0.264	No
327	6.54	113.33	64.16	49.18	0.89	0.306	1.43	0.214	1.06	1.00	0.264	No
328	6.56	113.70	64.35	49.35	0.89	0.306	1.43	0.214	1.06	1.00	0.264	No
329	6.58	114.07	64.55	49.52	0.89	0.306	1.43	0.214	1.06	1.00	0.264	No
330	6.60	114.43	64.75	49.69	0.89	0.306	1.43	0.214	1.06	1.00	0.264	No
331	6.62	114.80	64.94	49.85	0.89	0.305	1.43	0.214	1.06	1.00	0.264	No
332	6.64	115.16	65.14	50.02	0.89	0.305	1.43	0.214	1.06	1.00	0.264	No
333	6.66	115.52	65.33	50.19	0.89	0.305	1.43	0.213	1.06	1.00	0.264	No
334	6.68	115.88	65.53	50.35	0.89	0.305	1.43	0.213	1.06	1.00	0.263	No
335	6.70	116.24	65.73	50.52	0.89	0.305	1.43	0.213	1.06	1.00	0.263	No
336	6.72	116.61	65.92	50.68	0.88	0.304	1.43	0.213	1.06	1.00	0.262	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
337	6.74	116.97	66.12	50.85	0.88	0.304	1.43	0.213	1.06	1.00	0.262	No
338	6.76	117.33	66.32	51.01	0.88	0.304	1.43	0.213	1.06	1.00	0.262	No
339	6.78	117.69	66.51	51.18	0.88	0.304	1.43	0.213	1.06	1.00	0.263	No
340	6.80	118.05	66.71	51.35	0.88	0.303	1.43	0.212	1.06	1.00	0.263	No
341	6.82	118.42	66.90	51.51	0.88	0.303	1.43	0.212	1.06	1.00	0.264	No
342	6.84	118.78	67.10	51.68	0.88	0.303	1.43	0.212	1.06	1.00	0.264	No
343	6.86	119.14	67.30	51.84	0.88	0.303	1.43	0.212	1.06	1.00	0.264	No
344	6.88	119.51	67.49	52.01	0.88	0.303	1.43	0.212	1.06	1.00	0.264	No
345	6.90	119.87	67.69	52.18	0.88	0.302	1.43	0.212	1.06	1.00	0.264	No
346	6.92	120.24	67.89	52.35	0.88	0.302	1.43	0.212	1.06	1.00	0.263	No
347	6.94	120.60	68.08	52.52	0.88	0.302	1.43	0.211	1.06	1.00	0.263	No
348	6.96	120.97	68.28	52.69	0.88	0.302	1.43	0.211	1.06	1.00	0.262	No
349	6.98	121.33	68.47	52.86	0.88	0.302	1.43	0.211	1.06	1.00	0.262	No
350	7.00	121.70	68.67	53.03	0.88	0.301	1.43	0.211	1.06	1.00	0.262	No
351	7.02	122.06	68.87	53.19	0.88	0.301	1.43	0.211	1.06	1.00	0.262	No
352	7.04	122.42	69.06	53.36	0.88	0.301	1.43	0.211	1.06	1.00	0.262	No
353	7.06	122.79	69.26	53.53	0.88	0.301	1.43	0.211	1.06	1.00	0.261	No
354	7.08	123.15	69.45	53.70	0.88	0.301	1.43	0.210	1.06	1.00	0.261	No
355	7.10	123.52	69.65	53.87	0.88	0.300	1.43	0.210	1.06	1.00	0.260	No
356	7.12	123.88	69.85	54.04	0.88	0.300	1.43	0.210	1.06	1.00	0.259	No
357	7.14	124.25	70.04	54.21	0.88	0.300	1.43	0.210	1.06	1.00	0.258	No
358	7.16	124.62	70.24	54.38	0.87	0.300	1.43	0.210	1.06	1.00	0.257	No
359	7.18	124.99	70.44	54.56	0.87	0.299	1.43	0.210	1.06	1.00	0.256	No
360	7.20	125.36	70.63	54.73	0.87	0.299	1.43	0.209	1.06	1.00	0.256	No
361	7.22	125.74	70.83	54.91	0.87	0.299	1.43	0.209	1.06	1.00	0.255	No
362	7.24	126.11	71.02	55.08	0.87	0.299	1.43	0.209	1.06	1.00	0.255	No
363	7.26	126.48	71.22	55.26	0.87	0.299	1.43	0.209	1.06	1.00	0.256	No
364	7.28	126.86	71.42	55.44	0.87	0.298	1.43	0.209	1.06	1.00	0.256	No
365	7.30	127.24	71.61	55.62	0.87	0.298	1.43	0.209	1.06	1.00	0.257	No
366	7.32	127.61	71.81	55.80	0.87	0.298	1.43	0.208	1.05	1.00	0.258	No
367	7.34	127.99	72.01	55.99	0.87	0.298	1.43	0.208	1.05	1.00	0.258	No
368	7.36	128.37	72.20	56.17	0.87	0.297	1.43	0.208	1.05	1.00	0.258	No
369	7.38	128.75	72.40	56.35	0.87	0.297	1.43	0.208	1.05	1.00	0.257	No
370	7.40	129.12	72.59	56.53	0.87	0.297	1.43	0.208	1.05	1.00	0.257	No
371	7.42	129.50	72.79	56.70	0.87	0.297	1.43	0.208	1.05	1.00	0.256	No
372	7.44	129.87	72.99	56.88	0.87	0.296	1.43	0.207	1.05	1.00	0.256	No
373	7.46	130.24	73.18	57.06	0.87	0.296	1.43	0.207	1.05	1.00	0.255	No
374	7.48	130.61	73.38	57.23	0.87	0.296	1.43	0.207	1.05	1.00	0.256	No
375	7.50	130.98	73.58	57.41	0.87	0.296	1.43	0.207	1.05	1.00	0.255	No
376	7.52	131.35	73.77	57.58	0.87	0.295	1.43	0.207	1.05	1.00	0.255	No
377	7.54	131.73	73.97	57.76	0.87	0.295	1.43	0.207	1.05	1.00	0.255	No
378	7.56	132.10	74.16	57.94	0.87	0.295	1.43	0.207	1.05	1.00	0.254	No
379	7.58	132.47	74.36	58.12	0.87	0.295	1.43	0.206	1.05	1.00	0.253	No
380	7.60	132.85	74.56	58.30	0.86	0.295	1.43	0.206	1.05	1.00	0.254	No
381	7.62	133.23	74.75	58.48	0.86	0.294	1.43	0.206	1.05	1.00	0.254	No
382	7.64	133.61	74.95	58.66	0.86	0.294	1.43	0.206	1.05	1.00	0.253	No
383	7.66	133.98	75.14	58.84	0.86	0.294	1.43	0.206	1.05	1.00	0.254	No
384	7.68	134.36	75.34	59.02	0.86	0.294	1.43	0.206	1.05	1.00	0.254	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
385	7.70	134.74	75.54	59.20	0.86	0.293	1.43	0.205	1.05	1.00	0.253	No
386	7.72	135.11	75.73	59.38	0.86	0.293	1.43	0.205	1.05	1.00	0.253	No
387	7.74	135.49	75.93	59.56	0.86	0.293	1.43	0.205	1.05	1.00	0.253	No
388	7.76	135.87	76.13	59.74	0.86	0.293	1.43	0.205	1.05	1.00	0.254	No
389	7.78	136.25	76.32	59.93	0.86	0.292	1.43	0.205	1.05	1.00	0.254	No
390	7.81	136.81	76.62	60.20	0.86	0.292	1.43	0.204	1.05	1.00	0.253	No
391	7.82	137.00	76.71	60.29	0.86	0.292	1.43	0.204	1.05	1.00	0.253	No
392	7.84	137.38	76.91	60.47	0.86	0.292	1.43	0.204	1.05	1.00	0.253	No
393	7.86	137.75	77.11	60.65	0.86	0.292	1.43	0.204	1.05	1.00	0.253	No
394	7.88	138.13	77.30	60.83	0.86	0.291	1.43	0.204	1.05	1.00	0.253	No
395	7.90	138.51	77.50	61.01	0.86	0.291	1.43	0.204	1.05	1.00	0.253	No
396	7.92	138.88	77.70	61.19	0.86	0.291	1.43	0.204	1.05	1.00	0.253	No
397	7.94	139.26	77.89	61.36	0.86	0.291	1.43	0.203	1.05	1.00	0.253	No
398	7.96	139.63	78.09	61.54	0.86	0.290	1.43	0.203	1.05	1.00	0.253	No
399	7.99	140.19	78.38	61.81	0.86	0.290	1.43	0.203	1.04	1.00	0.254	No
400	8.00	140.38	78.48	61.90	0.86	0.290	1.43	0.203	1.04	1.00	0.254	No
401	8.02	140.75	78.68	62.07	0.85	0.290	1.43	0.203	1.04	1.00	0.255	No
402	8.04	141.12	78.87	62.25	0.85	0.290	1.43	0.203	1.04	1.00	0.256	No
403	8.06	141.49	79.07	62.42	0.85	0.289	1.43	0.203	1.04	1.00	0.257	No
404	8.08	141.86	79.26	62.59	0.85	0.289	1.43	0.202	1.04	1.00	0.257	No
405	8.10	142.22	79.46	62.76	0.85	0.289	1.43	0.202	1.04	1.00	0.258	No
406	8.12	142.59	79.66	62.93	0.85	0.289	1.43	0.202	1.04	1.00	0.258	No
407	8.14	142.95	79.85	63.10	0.85	0.289	1.43	0.202	1.04	1.00	0.258	No
408	8.16	143.31	80.05	63.26	0.85	0.288	1.43	0.202	1.04	1.00	0.258	No
409	8.18	143.67	80.25	63.42	0.85	0.288	1.43	0.202	1.04	1.00	0.258	No
410	8.20	144.03	80.44	63.58	0.85	0.288	1.43	0.202	1.04	1.00	0.258	No
411	8.22	144.38	80.64	63.74	0.85	0.288	1.43	0.201	1.04	1.00	0.257	No
412	8.24	144.73	80.83	63.90	0.85	0.288	1.43	0.201	1.04	1.00	0.257	No
413	8.26	145.08	81.03	64.05	0.85	0.288	1.43	0.201	1.04	1.00	0.256	No
414	8.28	145.43	81.23	64.20	0.85	0.287	1.43	0.201	1.04	1.00	0.255	No
415	8.30	145.78	81.42	64.36	0.85	0.287	1.43	0.201	1.04	1.00	0.255	No
416	8.32	146.12	81.62	64.51	0.85	0.287	1.43	0.201	1.04	1.00	0.256	No
417	8.34	146.47	81.82	64.65	0.85	0.287	1.43	0.201	1.04	1.00	0.256	No
418	8.36	146.81	82.01	64.80	0.85	0.287	1.43	0.201	1.04	1.00	0.256	No
419	8.38	147.15	82.21	64.95	0.85	0.287	1.43	0.201	1.04	1.00	0.257	No
420	8.40	147.49	82.40	65.09	0.85	0.287	1.43	0.201	1.04	1.00	0.256	No
421	8.42	147.83	82.60	65.23	0.85	0.286	1.43	0.200	1.04	1.00	0.256	No
422	8.44	148.17	82.80	65.38	0.84	0.286	1.43	0.200	1.04	1.00	0.255	No
423	8.46	148.51	82.99	65.52	0.84	0.286	1.43	0.200	1.04	1.00	0.255	No
424	8.48	148.86	83.19	65.67	0.84	0.286	1.43	0.200	1.04	1.00	0.256	No
425	8.50	149.20	83.39	65.81	0.84	0.286	1.43	0.200	1.04	1.00	0.256	No
426	8.52	149.54	83.58	65.96	0.84	0.286	1.43	0.200	1.04	1.00	0.256	No
427	8.54	149.88	83.78	66.10	0.84	0.286	1.43	0.200	1.04	1.00	0.256	No
428	8.56	150.22	83.97	66.25	0.84	0.285	1.43	0.200	1.04	1.00	0.255	No
429	8.58	150.57	84.17	66.40	0.84	0.285	1.43	0.200	1.04	1.00	0.255	No
430	8.60	150.91	84.37	66.55	0.84	0.285	1.43	0.200	1.04	1.00	0.255	No
431	8.62	151.26	84.56	66.69	0.84	0.285	1.43	0.200	1.04	1.00	0.255	No
432	8.64	151.60	84.76	66.84	0.84	0.285	1.43	0.199	1.03	1.00	0.255	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
433	8.66	151.95	84.95	66.99	0.84	0.285	1.43	0.199	1.03	1.00	0.255	No
434	8.68	152.29	85.15	67.14	0.84	0.285	1.43	0.199	1.03	1.00	0.255	No
435	8.70	152.63	85.35	67.29	0.84	0.284	1.43	0.199	1.03	1.00	0.255	No
436	8.72	152.98	85.54	67.43	0.84	0.284	1.43	0.199	1.03	1.00	0.255	No
437	8.74	153.32	85.74	67.58	0.84	0.284	1.43	0.199	1.03	1.00	0.254	No
438	8.76	153.66	85.94	67.73	0.84	0.284	1.43	0.199	1.03	1.00	0.254	No
439	8.78	154.01	86.13	67.87	0.84	0.284	1.43	0.199	1.03	1.00	0.253	No
440	8.80	154.35	86.33	68.03	0.84	0.284	1.43	0.199	1.04	1.00	0.252	No
441	8.82	154.70	86.52	68.18	0.84	0.284	1.43	0.198	1.03	1.00	0.252	No
442	8.85	155.23	86.82	68.41	0.84	0.283	1.43	0.198	1.03	1.00	0.251	No
443	8.86	155.41	86.92	68.49	0.83	0.283	1.43	0.198	1.03	1.00	0.251	No
444	8.88	155.77	87.11	68.65	0.83	0.283	1.43	0.198	1.03	1.00	0.251	No
445	8.90	156.13	87.31	68.82	0.83	0.283	1.43	0.198	1.03	1.00	0.251	No
446	8.92	156.49	87.51	68.98	0.83	0.283	1.43	0.198	1.03	1.00	0.251	No
447	8.94	156.85	87.70	69.15	0.83	0.283	1.43	0.198	1.03	1.00	0.250	No
448	8.96	157.22	87.90	69.32	0.83	0.282	1.43	0.198	1.03	1.00	0.249	No
449	8.98	157.58	88.09	69.49	0.83	0.282	1.43	0.197	1.03	1.00	0.250	No
450	9.00	157.94	88.29	69.65	0.83	0.282	1.43	0.197	1.03	1.00	0.249	No
451	9.02	158.31	88.49	69.82	0.83	0.282	1.43	0.197	1.03	1.00	0.250	No
452	9.05	158.86	88.78	70.08	0.83	0.281	1.43	0.197	1.03	1.00	0.249	No
453	9.07	159.22	88.98	70.25	0.83	0.281	1.43	0.197	1.03	1.00	0.249	No
454	9.08	159.41	89.07	70.33	0.83	0.281	1.43	0.197	1.03	1.00	0.249	No
455	9.10	159.77	89.27	70.50	0.83	0.281	1.43	0.197	1.03	1.00	0.250	No
456	9.12	160.14	89.47	70.67	0.83	0.281	1.43	0.197	1.03	1.00	0.250	No
457	9.15	160.69	89.76	70.93	0.83	0.280	1.43	0.196	1.03	1.00	0.251	No
458	9.16	160.88	89.86	71.02	0.83	0.280	1.43	0.196	1.03	1.00	0.251	No
459	9.18	161.24	90.06	71.19	0.83	0.280	1.43	0.196	1.03	1.00	0.251	No
460	9.20	161.61	90.25	71.36	0.83	0.280	1.43	0.196	1.03	1.00	0.251	No
461	9.22	161.98	90.45	71.53	0.83	0.280	1.43	0.196	1.03	1.00	0.252	No
462	9.24	162.34	90.64	71.70	0.83	0.280	1.43	0.196	1.03	1.00	0.252	No
463	9.26	162.71	90.84	71.87	0.83	0.279	1.43	0.196	1.03	1.00	0.251	No
464	9.29	163.25	91.13	72.12	0.82	0.279	1.43	0.195	1.03	1.00	0.251	No
465	9.31	163.61	91.33	72.28	0.82	0.279	1.43	0.195	1.03	1.00	0.251	No
466	9.32	163.79	91.43	72.36	0.82	0.279	1.43	0.195	1.03	1.00	0.251	No
467	9.34	164.15	91.63	72.52	0.82	0.279	1.43	0.195	1.03	1.00	0.251	No
468	9.36	164.50	91.82	72.68	0.82	0.279	1.43	0.195	1.03	1.00	0.251	No
469	9.38	164.86	92.02	72.84	0.82	0.278	1.43	0.195	1.03	1.00	0.251	No
470	9.40	165.22	92.21	73.01	0.82	0.278	1.43	0.195	1.03	1.00	0.251	No
471	9.42	165.58	92.41	73.17	0.82	0.278	1.43	0.195	1.03	1.00	0.251	No
472	9.44	165.94	92.61	73.33	0.82	0.278	1.43	0.194	1.03	1.00	0.250	No
473	9.46	166.29	92.80	73.49	0.82	0.278	1.43	0.194	1.03	1.00	0.250	No
474	9.48	166.65	93.00	73.66	0.82	0.277	1.43	0.194	1.03	1.00	0.250	No
475	9.50	167.01	93.19	73.82	0.82	0.277	1.43	0.194	1.03	1.00	0.250	No
476	9.52	167.37	93.39	73.98	0.82	0.277	1.43	0.194	1.03	1.00	0.250	No
477	9.54	167.74	93.59	74.15	0.82	0.277	1.43	0.194	1.03	1.00	0.250	No
478	9.56	168.10	93.78	74.31	0.82	0.277	1.43	0.194	1.03	1.00	0.250	No
479	9.58	168.46	93.98	74.48	0.82	0.277	1.43	0.194	1.03	1.00	0.250	No
480	9.60	168.82	94.18	74.65	0.82	0.276	1.43	0.193	1.03	1.00	0.250	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
481	9.62	169.18	94.37	74.81	0.82	0.276	1.43	0.193	1.03	1.00	0.250	No
482	9.64	169.55	94.57	74.98	0.82	0.276	1.43	0.193	1.02	1.00	0.250	No
483	9.66	169.91	94.76	75.14	0.82	0.276	1.43	0.193	1.02	1.00	0.250	No
484	9.68	170.27	94.96	75.31	0.82	0.276	1.43	0.193	1.02	1.00	0.249	No
485	9.70	170.63	95.16	75.47	0.81	0.275	1.43	0.193	1.02	1.00	0.249	No
486	9.72	170.99	95.35	75.64	0.81	0.275	1.43	0.193	1.02	1.00	0.249	No
487	9.74	171.35	95.55	75.80	0.81	0.275	1.43	0.193	1.02	1.00	0.249	No
488	9.76	171.71	95.75	75.96	0.81	0.275	1.43	0.192	1.02	1.00	0.249	No
489	9.78	172.07	95.94	76.12	0.81	0.275	1.43	0.192	1.02	1.00	0.248	No
490	9.80	172.42	96.14	76.29	0.81	0.275	1.43	0.192	1.02	1.00	0.248	No
491	9.82	172.78	96.33	76.45	0.81	0.274	1.43	0.192	1.02	1.00	0.248	No
492	9.85	173.32	96.63	76.69	0.81	0.274	1.43	0.192	1.02	1.00	0.248	No
493	9.86	173.50	96.73	76.77	0.81	0.274	1.43	0.192	1.02	1.00	0.248	No
494	9.88	173.86	96.92	76.93	0.81	0.274	1.43	0.192	1.02	1.00	0.247	No
495	9.90	174.22	97.12	77.10	0.81	0.274	1.43	0.192	1.02	1.00	0.247	No
496	9.92	174.58	97.32	77.27	0.81	0.274	1.43	0.191	1.02	1.00	0.247	No
497	9.94	174.94	97.51	77.43	0.81	0.273	1.43	0.191	1.02	1.00	0.247	No
498	9.96	175.31	97.71	77.60	0.81	0.273	1.43	0.191	1.02	1.00	0.247	No
499	9.98	175.67	97.90	77.77	0.81	0.273	1.43	0.191	1.02	1.00	0.247	No
500	10.00	176.03	98.10	77.93	0.81	0.273	1.43	0.191	1.02	1.00	0.247	No
501	10.02	176.40	98.30	78.10	0.81	0.273	1.43	0.191	1.02	1.00	0.247	No
502	10.04	176.76	98.49	78.27	0.81	0.272	1.43	0.191	1.02	1.00	0.246	No
503	10.06	177.12	98.69	78.43	0.81	0.272	1.43	0.191	1.02	1.00	0.246	No
504	10.08	177.48	98.88	78.60	0.81	0.272	1.43	0.190	1.02	1.00	0.246	No
505	10.10	177.85	99.08	78.77	0.81	0.272	1.43	0.190	1.02	1.00	0.246	No
506	10.12	178.21	99.28	78.93	0.80	0.272	1.43	0.190	1.02	1.00	0.246	No
507	10.14	178.57	99.47	79.10	0.80	0.272	1.43	0.190	1.02	1.00	0.246	No
508	10.16	178.94	99.67	79.27	0.80	0.271	1.43	0.190	1.02	1.00	0.246	No
509	10.18	179.30	99.87	79.43	0.80	0.271	1.43	0.190	1.02	1.00	0.246	No
510	10.20	179.66	100.06	79.60	0.80	0.271	1.43	0.190	1.02	1.00	0.246	No
511	10.22	180.03	100.26	79.77	0.80	0.271	1.43	0.190	1.02	1.00	0.246	No
512	10.24	180.39	100.45	79.94	0.80	0.271	1.43	0.189	1.02	1.00	0.245	No
513	10.26	180.75	100.65	80.10	0.80	0.270	1.43	0.189	1.02	1.00	0.245	No
514	10.28	181.12	100.85	80.27	0.80	0.270	1.43	0.189	1.02	1.00	0.245	No
515	10.30	181.48	101.04	80.44	0.80	0.270	1.43	0.189	1.02	1.00	0.244	No
516	10.32	181.85	101.24	80.61	0.80	0.270	1.43	0.189	1.02	1.00	0.244	No
517	10.34	182.21	101.44	80.78	0.80	0.270	1.43	0.189	1.02	1.00	0.244	No
518	10.36	182.58	101.63	80.95	0.80	0.269	1.43	0.189	1.02	1.00	0.244	No
519	10.38	182.94	101.83	81.11	0.80	0.269	1.43	0.189	1.02	1.00	0.244	No
520	10.40	183.31	102.02	81.28	0.80	0.269	1.43	0.188	1.02	1.00	0.244	No
521	10.42	183.67	102.22	81.45	0.80	0.269	1.43	0.188	1.02	1.00	0.244	No
522	10.44	184.04	102.42	81.62	0.80	0.269	1.43	0.188	1.02	1.00	0.244	No
523	10.46	184.40	102.61	81.79	0.80	0.269	1.43	0.188	1.02	1.00	0.243	No
524	10.48	184.77	102.81	81.96	0.80	0.268	1.43	0.188	1.02	1.00	0.243	No
525	10.50	185.13	103.01	82.13	0.80	0.268	1.43	0.188	1.02	1.00	0.242	No
526	10.52	185.50	103.20	82.30	0.80	0.268	1.43	0.188	1.02	1.00	0.242	No
527	10.54	185.87	103.40	82.47	0.79	0.268	1.43	0.187	1.02	1.00	0.242	No
528	10.56	186.23	103.59	82.64	0.79	0.268	1.43	0.187	1.02	1.00	0.242	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
529	10.58	186.60	103.79	82.81	0.79	0.267	1.43	0.187	1.02	1.00	0.242	No
530	10.60	186.97	103.99	82.98	0.79	0.267	1.43	0.187	1.02	1.00	0.241	No
531	10.62	187.33	104.18	83.15	0.79	0.267	1.43	0.187	1.02	1.00	0.241	No
532	10.64	187.70	104.38	83.33	0.79	0.267	1.43	0.187	1.02	1.00	0.241	No
533	10.66	188.07	104.57	83.50	0.79	0.267	1.43	0.187	1.02	1.00	0.241	No
534	10.68	188.44	104.77	83.67	0.79	0.267	1.43	0.187	1.02	1.00	0.241	No
535	10.70	188.82	104.97	83.85	0.79	0.266	1.43	0.186	1.02	1.00	0.241	No
536	10.72	189.19	105.16	84.03	0.79	0.266	1.43	0.186	1.02	1.00	0.241	No
537	10.74	189.56	105.36	84.20	0.79	0.266	1.43	0.186	1.02	1.00	0.241	No
538	10.77	190.12	105.65	84.47	0.79	0.266	1.43	0.186	1.02	1.00	0.240	No
539	10.78	190.31	105.75	84.56	0.79	0.266	1.43	0.186	1.02	1.00	0.240	No
540	10.80	190.68	105.95	84.73	0.79	0.265	1.43	0.186	1.02	1.00	0.240	No
541	10.82	191.05	106.14	84.91	0.79	0.265	1.43	0.186	1.02	1.00	0.240	No
542	10.84	191.43	106.34	85.08	0.79	0.265	1.43	0.185	1.02	1.00	0.240	No
543	10.86	191.80	106.54	85.26	0.79	0.265	1.43	0.185	1.01	1.00	0.240	No
544	10.88	192.17	106.73	85.44	0.79	0.265	1.43	0.185	1.01	1.00	0.240	No
545	10.91	192.73	107.03	85.70	0.79	0.264	1.43	0.185	1.01	1.00	0.240	No
546	10.92	192.91	107.13	85.79	0.79	0.264	1.43	0.185	1.01	1.00	0.240	No
547	10.95	193.47	107.42	86.05	0.79	0.264	1.43	0.185	1.01	1.00	0.240	No
548	10.96	193.65	107.52	86.13	0.78	0.264	1.43	0.185	1.01	1.00	0.240	No
549	10.98	194.02	107.71	86.31	0.78	0.264	1.43	0.185	1.01	1.00	0.240	No
550	11.00	194.39	107.91	86.48	0.78	0.263	1.43	0.184	1.01	1.00	0.240	No
551	11.02	194.76	108.11	86.65	0.78	0.263	1.43	0.184	1.01	1.00	0.240	No
552	11.04	195.12	108.30	86.82	0.78	0.263	1.43	0.184	1.01	1.00	0.240	No
553	11.06	195.49	108.50	86.99	0.78	0.263	1.43	0.184	1.01	1.00	0.240	No
554	11.09	196.04	108.79	87.25	0.78	0.263	1.43	0.184	1.01	1.00	0.240	No
555	11.10	196.22	108.89	87.33	0.78	0.263	1.43	0.184	1.01	1.00	0.240	No
556	11.13	196.77	109.19	87.59	0.78	0.262	1.43	0.184	1.01	1.00	0.240	No
557	11.15	197.14	109.38	87.76	0.78	0.262	1.43	0.183	1.01	1.00	0.239	No
558	11.16	197.32	109.48	87.84	0.78	0.262	1.43	0.183	1.01	1.00	0.239	No
559	11.18	197.69	109.68	88.01	0.78	0.262	1.43	0.183	1.01	1.00	0.239	No
560	11.20	198.05	109.87	88.18	0.78	0.262	1.43	0.183	1.01	1.00	0.239	No
561	11.22	198.42	110.07	88.35	0.78	0.261	1.43	0.183	1.01	1.00	0.239	No
562	11.24	198.79	110.26	88.52	0.78	0.261	1.43	0.183	1.01	1.00	0.239	No
563	11.26	199.15	110.46	88.69	0.78	0.261	1.43	0.183	1.01	1.00	0.238	No
564	11.28	199.52	110.66	88.86	0.78	0.261	1.43	0.183	1.01	1.00	0.238	No
565	11.30	199.88	110.85	89.03	0.78	0.261	1.43	0.182	1.01	1.00	0.238	No
566	11.32	200.25	111.05	89.20	0.78	0.261	1.43	0.182	1.01	1.00	0.238	No
567	11.34	200.61	111.25	89.37	0.78	0.260	1.43	0.182	1.01	1.00	0.238	No
568	11.36	200.98	111.44	89.54	0.78	0.260	1.43	0.182	1.01	1.00	0.238	No
569	11.38	201.34	111.64	89.70	0.77	0.260	1.43	0.182	1.01	1.00	0.238	No
570	11.40	201.71	111.83	89.87	0.77	0.260	1.43	0.182	1.01	1.00	0.238	No
571	11.42	202.07	112.03	90.04	0.77	0.260	1.43	0.182	1.01	1.00	0.238	No
572	11.44	202.43	112.23	90.21	0.77	0.259	1.43	0.182	1.01	1.00	0.238	No
573	11.46	202.80	112.42	90.37	0.77	0.259	1.43	0.181	1.01	1.00	0.237	No
574	11.48	203.16	112.62	90.54	0.77	0.259	1.43	0.181	1.01	1.00	0.237	No
575	11.50	203.52	112.82	90.70	0.77	0.259	1.43	0.181	1.01	1.00	0.237	No
576	11.52	203.88	113.01	90.87	0.77	0.259	1.43	0.181	1.01	1.00	0.237	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
577	11.54	204.24	113.21	91.03	0.77	0.259	1.43	0.181	1.01	1.00	0.237	No
578	11.56	204.60	113.40	91.20	0.77	0.258	1.43	0.181	1.01	1.00	0.237	No
579	11.58	204.96	113.60	91.36	0.77	0.258	1.43	0.181	1.01	1.00	0.237	No
580	11.60	205.32	113.80	91.52	0.77	0.258	1.43	0.181	1.01	1.00	0.237	No
581	11.62	205.68	113.99	91.69	0.77	0.258	1.43	0.181	1.01	1.00	0.237	No
582	11.64	206.04	114.19	91.85	0.77	0.258	1.43	0.180	1.01	1.00	0.237	No
583	11.66	206.40	114.38	92.01	0.77	0.258	1.43	0.180	1.01	1.00	0.237	No
584	11.68	206.76	114.58	92.18	0.77	0.257	1.43	0.180	1.01	1.00	0.237	No
585	11.70	207.12	114.78	92.34	0.77	0.257	1.43	0.180	1.01	1.00	0.236	No
586	11.72	207.48	114.97	92.51	0.77	0.257	1.43	0.180	1.01	1.00	0.237	No
587	11.74	207.84	115.17	92.67	0.77	0.257	1.43	0.180	1.01	1.00	0.236	No
588	11.76	208.20	115.37	92.83	0.77	0.257	1.43	0.180	1.01	1.00	0.237	No
589	11.78	208.55	115.56	92.99	0.77	0.257	1.43	0.180	1.01	1.00	0.236	No
590	11.80	208.91	115.76	93.15	0.76	0.256	1.43	0.179	1.01	1.00	0.236	No
591	11.82	209.27	115.95	93.31	0.76	0.256	1.43	0.179	1.01	1.00	0.236	No
592	11.84	209.63	116.15	93.48	0.76	0.256	1.43	0.179	1.01	1.00	0.236	No
593	11.86	209.98	116.35	93.64	0.76	0.256	1.43	0.179	1.01	1.00	0.236	No
594	11.88	210.34	116.54	93.80	0.76	0.256	1.43	0.179	1.01	1.00	0.236	No
595	11.90	210.70	116.74	93.96	0.76	0.256	1.43	0.179	1.01	1.00	0.236	No
596	11.92	211.05	116.94	94.12	0.76	0.255	1.43	0.179	1.01	1.00	0.236	No
597	11.94	211.41	117.13	94.28	0.76	0.255	1.43	0.179	1.01	1.00	0.236	No
598	11.96	211.76	117.33	94.43	0.76	0.255	1.43	0.179	1.01	1.00	0.236	No
599	11.98	212.11	117.52	94.59	0.76	0.255	1.43	0.178	1.01	1.00	0.237	No
600	12.00	212.47	117.72	94.75	0.76	0.255	1.43	0.178	1.01	1.00	0.237	No
601	12.02	212.82	117.92	94.90	0.76	0.255	1.43	0.178	1.01	1.00	0.237	No
602	12.04	213.16	118.11	95.05	0.76	0.255	1.43	0.178	1.01	1.00	0.237	No
603	12.06	213.51	118.31	95.20	0.76	0.254	1.43	0.178	1.00	1.00	0.237	No
604	12.08	213.85	118.50	95.34	0.76	0.254	1.43	0.178	1.00	1.00	0.237	No
605	12.10	214.18	118.70	95.48	0.76	0.254	1.43	0.178	1.00	1.00	0.237	No
606	12.12	214.52	118.90	95.62	0.76	0.254	1.43	0.178	1.00	1.00	0.237	No
607	12.14	214.84	119.09	95.75	0.76	0.254	1.43	0.178	1.00	1.00	0.236	No
608	12.16	215.17	119.29	95.88	0.76	0.254	1.43	0.178	1.00	1.00	0.236	No
609	12.18	215.50	119.49	96.01	0.76	0.254	1.43	0.178	1.00	1.00	0.235	No
610	12.20	215.83	119.68	96.15	0.76	0.253	1.43	0.177	1.00	1.00	0.235	No
611	12.22	216.16	119.88	96.28	0.75	0.253	1.43	0.177	1.00	1.00	0.235	No
612	12.24	216.50	120.07	96.42	0.75	0.253	1.43	0.177	1.00	1.00	0.234	No
613	12.27	217.00	120.37	96.64	0.75	0.253	1.43	0.177	1.00	1.00	0.233	No
614	12.28	217.18	120.47	96.71	0.75	0.253	1.43	0.177	1.00	1.00	0.233	No
615	12.30	217.52	120.66	96.86	0.75	0.253	1.43	0.177	1.00	1.00	0.233	No
616	12.32	217.86	120.86	97.00	0.75	0.253	1.43	0.177	1.00	1.00	0.234	No
617	12.34	218.20	121.06	97.15	0.75	0.253	1.43	0.177	1.00	1.00	0.234	No
618	12.36	218.54	121.25	97.28	0.75	0.252	1.43	0.177	1.00	1.00	0.235	No
619	12.38	218.87	121.45	97.42	0.75	0.252	1.43	0.177	1.00	1.00	0.235	No
620	12.40	219.19	121.64	97.55	0.75	0.252	1.43	0.176	1.00	1.00	0.235	No
621	12.42	219.52	121.84	97.68	0.75	0.252	1.43	0.176	1.00	1.00	0.235	No
622	12.44	219.85	122.04	97.82	0.75	0.252	1.43	0.176	1.00	1.00	0.235	No
623	12.46	220.18	122.23	97.95	0.75	0.252	1.43	0.176	1.00	1.00	0.235	No
624	12.48	220.51	122.43	98.08	0.75	0.252	1.43	0.176	1.00	1.00	0.235	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
625	12.50	220.83	122.63	98.21	0.75	0.252	1.43	0.176	1.00	1.00	0.235	No
626	12.52	221.16	122.82	98.34	0.75	0.251	1.43	0.176	1.00	1.00	0.235	No
627	12.54	221.48	123.02	98.47	0.75	0.251	1.43	0.176	1.00	1.00	0.234	No
628	12.56	221.81	123.21	98.59	0.75	0.251	1.43	0.176	1.00	1.00	0.234	No
629	12.58	222.13	123.41	98.72	0.75	0.251	1.43	0.176	1.00	1.00	0.234	No
630	12.60	222.46	123.61	98.85	0.75	0.251	1.43	0.176	1.00	1.00	0.234	No
631	12.62	222.78	123.80	98.98	0.75	0.251	1.43	0.176	1.00	1.00	0.234	No
632	12.64	223.11	124.00	99.11	0.74	0.251	1.43	0.175	1.00	1.00	0.233	No
633	12.66	223.44	124.19	99.24	0.74	0.251	1.43	0.175	1.00	1.00	0.233	No
634	12.68	223.77	124.39	99.38	0.74	0.250	1.43	0.175	1.00	1.00	0.233	No
635	12.70	224.10	124.59	99.52	0.74	0.250	1.43	0.175	1.00	1.00	0.233	No
636	12.72	224.44	124.78	99.66	0.74	0.250	1.43	0.175	1.00	1.00	0.233	No
637	12.74	224.78	124.98	99.80	0.74	0.250	1.43	0.175	1.00	1.00	0.232	No
638	12.76	225.11	125.18	99.94	0.74	0.250	1.43	0.175	1.00	1.00	0.232	No
639	12.78	225.45	125.37	100.08	0.74	0.250	1.43	0.175	1.00	1.00	0.232	No
640	12.80	225.80	125.57	100.23	0.74	0.250	1.43	0.175	1.00	1.00	0.232	No
641	12.82	226.14	125.76	100.38	0.74	0.249	1.43	0.175	1.00	1.00	0.232	No
642	12.84	226.49	125.96	100.52	0.74	0.249	1.43	0.175	1.00	1.00	0.232	No
643	12.86	226.83	126.16	100.68	0.74	0.249	1.43	0.174	1.00	1.00	0.232	No
644	12.88	227.18	126.35	100.83	0.74	0.249	1.43	0.174	1.00	1.00	0.232	No
645	12.90	227.53	126.55	100.98	0.74	0.249	1.43	0.174	1.00	1.00	0.232	No
646	12.94	228.23	126.94	101.29	0.74	0.249	1.43	0.174	1.00	1.00	0.232	No
647	12.94	228.23	126.94	101.29	0.74	0.249	1.43	0.174	1.00	1.00	0.232	No
648	12.96	228.58	127.14	101.44	0.74	0.248	1.43	0.174	1.00	1.00	0.231	No
649	12.99	229.10	127.43	101.67	0.74	0.248	1.43	0.174	1.00	1.00	0.231	No
650	13.00	229.28	127.53	101.75	0.74	0.248	1.43	0.174	1.00	1.00	0.231	No
651	13.03	229.80	127.82	101.98	0.74	0.248	1.43	0.174	1.00	1.00	0.231	No
652	13.04	229.97	127.92	102.05	0.74	0.248	1.43	0.173	1.00	1.00	0.231	No
653	13.06	230.32	128.12	102.20	0.74	0.248	1.43	0.173	1.00	1.00	0.231	No
654	13.08	230.67	128.31	102.35	0.73	0.248	1.43	0.173	1.00	1.00	0.231	No
655	13.10	231.01	128.51	102.50	0.73	0.247	1.43	0.173	1.00	1.00	0.231	No
656	13.13	231.52	128.81	102.72	0.73	0.247	1.43	0.173	1.00	1.00	0.231	No
657	13.14	231.70	128.90	102.79	0.73	0.247	1.43	0.173	1.00	1.00	0.231	No
658	13.16	232.04	129.10	102.94	0.73	0.247	1.43	0.173	1.00	1.00	0.230	No
659	13.18	232.38	129.30	103.08	0.73	0.247	1.43	0.173	1.00	1.00	0.230	No
660	13.20	232.72	129.49	103.23	0.73	0.247	1.43	0.173	1.00	1.00	0.230	No
661	13.22	233.06	129.69	103.37	0.73	0.247	1.43	0.173	1.00	1.00	0.229	No
662	13.24	233.40	129.88	103.52	0.73	0.246	1.43	0.172	1.00	1.00	0.229	No
663	13.26	233.75	130.08	103.67	0.73	0.246	1.43	0.172	1.00	1.00	0.229	No
664	13.28	234.09	130.28	103.82	0.73	0.246	1.43	0.172	1.00	1.00	0.229	No
665	13.30	234.44	130.47	103.97	0.73	0.246	1.43	0.172	1.00	1.00	0.229	No
666	13.32	234.79	130.67	104.12	0.73	0.246	1.43	0.172	1.00	1.00	0.229	No
667	13.34	235.14	130.87	104.28	0.73	0.246	1.43	0.172	1.00	1.00	0.229	No
668	13.36	235.49	131.06	104.43	0.73	0.245	1.43	0.172	1.00	1.00	0.229	No
669	13.38	235.84	131.26	104.59	0.73	0.245	1.43	0.172	1.00	1.00	0.229	No
670	13.40	236.19	131.45	104.74	0.73	0.245	1.43	0.172	1.00	1.00	0.229	No
671	13.42	236.54	131.65	104.89	0.73	0.245	1.43	0.172	1.00	1.00	0.229	No
672	13.44	236.89	131.85	105.04	0.73	0.245	1.43	0.171	1.00	1.00	0.229	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
673	13.46	237.24	132.04	105.20	0.73	0.245	1.43	0.171	1.00	1.00	0.228	No
674	13.48	237.59	132.24	105.35	0.73	0.245	1.43	0.171	1.00	1.00	0.228	No
675	13.50	237.94	132.44	105.50	0.72	0.244	1.43	0.171	1.00	1.00	0.228	No
676	13.52	238.28	132.63	105.65	0.72	0.244	1.43	0.171	1.00	1.00	0.228	No
677	13.54	238.63	132.83	105.80	0.72	0.244	1.43	0.171	1.00	1.00	0.228	No
678	13.56	238.98	133.02	105.95	0.72	0.244	1.43	0.171	1.00	1.00	0.228	No
679	13.58	239.32	133.22	106.10	0.72	0.244	1.43	0.171	1.00	1.00	0.228	No
680	13.60	239.67	133.42	106.25	0.72	0.244	1.43	0.171	1.00	1.00	0.228	No
681	13.62	240.02	133.61	106.40	0.72	0.244	1.43	0.170	1.00	1.00	0.228	No
682	13.64	240.36	133.81	106.56	0.72	0.243	1.43	0.170	1.00	1.00	0.227	No
683	13.66	240.71	134.00	106.71	0.72	0.243	1.43	0.170	1.00	1.00	0.227	No
684	13.68	241.06	134.20	106.86	0.72	0.243	1.43	0.170	1.00	1.00	0.227	No
685	13.70	241.41	134.40	107.01	0.72	0.243	1.43	0.170	1.00	1.00	0.227	No
686	13.72	241.75	134.59	107.16	0.72	0.243	1.43	0.170	1.00	1.00	0.227	No
687	13.74	242.10	134.79	107.31	0.72	0.243	1.43	0.170	1.00	1.00	0.227	No
688	13.76	242.45	134.99	107.47	0.72	0.242	1.43	0.170	1.00	1.00	0.227	No
689	13.79	242.98	135.28	107.70	0.72	0.242	1.43	0.170	1.00	1.00	0.226	No
690	13.80	243.16	135.38	107.78	0.72	0.242	1.43	0.170	0.99	1.00	0.226	No
691	13.82	243.51	135.57	107.93	0.72	0.242	1.43	0.169	0.99	1.00	0.226	No
692	13.85	244.04	135.87	108.17	0.72	0.242	1.43	0.169	0.99	1.00	0.226	No
693	13.86	244.21	135.97	108.25	0.72	0.242	1.43	0.169	0.99	1.00	0.226	No
694	13.88	244.57	136.16	108.40	0.72	0.242	1.43	0.169	0.99	1.00	0.226	No
695	13.90	244.92	136.36	108.56	0.72	0.241	1.43	0.169	0.99	1.00	0.226	No
696	13.92	245.28	136.56	108.72	0.72	0.241	1.43	0.169	0.99	1.00	0.226	No
697	13.94	245.63	136.75	108.88	0.71	0.241	1.43	0.169	0.99	1.00	0.226	No
698	13.96	245.99	136.95	109.04	0.71	0.241	1.43	0.169	0.99	1.00	0.225	No
699	13.98	246.34	137.14	109.20	0.71	0.241	1.43	0.169	0.99	1.00	0.225	No
700	14.00	246.69	137.34	109.35	0.71	0.241	1.43	0.168	0.99	1.00	0.225	No
701	14.02	247.05	137.54	109.51	0.71	0.240	1.43	0.168	0.99	1.00	0.225	No
702	14.04	247.40	137.73	109.66	0.71	0.240	1.43	0.168	0.99	1.00	0.225	No
703	14.06	247.75	137.93	109.82	0.71	0.240	1.43	0.168	0.99	1.00	0.225	No
704	14.08	248.10	138.12	109.97	0.71	0.240	1.43	0.168	0.99	1.00	0.225	No
705	14.10	248.45	138.32	110.13	0.71	0.240	1.43	0.168	0.99	1.00	0.224	No
706	14.12	248.80	138.52	110.28	0.71	0.240	1.43	0.168	0.99	1.00	0.224	No
707	14.14	249.15	138.71	110.44	0.71	0.240	1.43	0.168	0.99	1.00	0.224	No
708	14.16	249.50	138.91	110.59	0.71	0.239	1.43	0.168	0.99	1.00	0.224	No
709	14.18	249.85	139.11	110.75	0.71	0.239	1.43	0.167	0.99	1.00	0.224	No
710	14.20	250.21	139.30	110.90	0.71	0.239	1.43	0.167	0.99	1.00	0.224	No
711	14.22	250.56	139.50	111.06	0.71	0.239	1.43	0.167	0.99	1.00	0.223	No
712	14.24	250.91	139.69	111.22	0.71	0.239	1.43	0.167	0.99	1.00	0.223	No
713	14.26	251.26	139.89	111.37	0.71	0.239	1.43	0.167	0.99	1.00	0.223	No
714	14.28	251.62	140.09	111.53	0.71	0.238	1.43	0.167	0.99	1.00	0.223	No
715	14.30	251.98	140.28	111.69	0.71	0.238	1.43	0.167	0.99	1.00	0.222	No
716	14.32	252.33	140.48	111.85	0.71	0.238	1.43	0.167	0.99	1.00	0.222	No
717	14.34	252.69	140.68	112.02	0.71	0.238	1.43	0.167	0.99	1.00	0.222	No
718	14.36	253.05	140.87	112.18	0.71	0.238	1.43	0.166	0.99	1.00	0.222	No
719	14.38	253.42	141.07	112.35	0.70	0.238	1.43	0.166	0.99	1.00	0.222	No
720	14.40	253.78	141.26	112.52	0.70	0.238	1.43	0.166	0.99	1.00	0.222	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
721	14.42	254.14	141.46	112.68	0.70	0.237	1.43	0.166	0.99	1.00	0.221	No
722	14.44	254.51	141.66	112.85	0.70	0.237	1.43	0.166	0.99	1.00	0.221	No
723	14.46	254.87	141.85	113.02	0.70	0.237	1.43	0.166	0.99	1.00	0.221	No
724	14.48	255.24	142.05	113.19	0.70	0.237	1.43	0.166	0.99	1.00	0.221	No
725	14.50	255.60	142.25	113.36	0.70	0.237	1.43	0.166	0.99	1.00	0.221	No
726	14.52	255.97	142.44	113.53	0.70	0.237	1.43	0.166	0.99	1.00	0.221	No
727	14.54	256.33	142.64	113.69	0.70	0.236	1.43	0.165	0.99	1.00	0.221	No
728	14.56	256.70	142.83	113.86	0.70	0.236	1.43	0.165	0.99	1.00	0.221	No
729	14.58	257.06	143.03	114.03	0.70	0.236	1.43	0.165	0.99	1.00	0.221	No
730	14.60	257.42	143.23	114.20	0.70	0.236	1.43	0.165	0.99	1.00	0.221	No
731	14.62	257.79	143.42	114.37	0.70	0.236	1.43	0.165	0.99	1.00	0.220	No
732	14.64	258.15	143.62	114.54	0.70	0.236	1.43	0.165	0.99	1.00	0.220	No
733	14.66	258.52	143.81	114.70	0.70	0.235	1.43	0.165	0.99	1.00	0.220	No
734	14.68	258.88	144.01	114.87	0.70	0.235	1.43	0.165	0.99	1.00	0.220	No
735	14.70	259.25	144.21	115.04	0.70	0.235	1.43	0.165	0.99	1.00	0.220	No
736	14.72	259.61	144.40	115.21	0.70	0.235	1.43	0.164	0.99	1.00	0.220	No
737	14.74	259.98	144.60	115.38	0.70	0.235	1.43	0.164	0.99	1.00	0.220	No
738	14.76	260.34	144.80	115.54	0.70	0.235	1.43	0.164	0.99	1.00	0.219	No
739	14.78	260.70	144.99	115.71	0.70	0.234	1.43	0.164	0.99	1.00	0.219	No
740	14.81	261.25	145.29	115.96	0.70	0.234	1.43	0.164	0.99	1.00	0.219	No
741	14.83	261.61	145.48	116.13	0.69	0.234	1.43	0.164	0.99	1.00	0.219	No
742	14.84	261.79	145.58	116.21	0.69	0.234	1.43	0.164	0.99	1.00	0.219	No
743	14.86	262.15	145.78	116.37	0.69	0.234	1.43	0.164	0.99	1.00	0.219	No
744	14.88	262.51	145.97	116.54	0.69	0.234	1.43	0.163	0.99	1.00	0.219	No
745	14.90	262.88	146.17	116.71	0.69	0.233	1.43	0.163	0.99	1.00	0.218	No
746	14.92	263.24	146.37	116.88	0.69	0.233	1.43	0.163	0.99	1.00	0.218	No
747	14.94	263.61	146.56	117.05	0.69	0.233	1.43	0.163	0.99	1.00	0.218	No
748	14.96	263.97	146.76	117.22	0.69	0.233	1.43	0.163	0.99	1.00	0.218	No
749	14.98	264.34	146.95	117.39	0.69	0.233	1.43	0.163	0.99	1.00	0.218	No
750	15.01	264.89	147.25	117.65	0.69	0.233	1.43	0.163	0.99	1.00	0.218	No
751	15.02	265.08	147.35	117.73	0.69	0.232	1.43	0.163	0.99	1.00	0.218	No
752	15.04	265.45	147.54	117.90	0.69	0.232	1.43	0.163	0.99	1.00	0.218	No
753	15.06	265.81	147.74	118.08	0.69	0.232	1.43	0.162	0.99	1.00	0.218	No
754	15.08	266.18	147.93	118.25	0.69	0.232	1.43	0.162	0.99	1.00	0.217	No
755	15.10	266.55	148.13	118.42	0.69	0.232	1.43	0.162	0.99	1.00	0.217	No
756	15.12	266.92	148.33	118.59	0.69	0.232	1.43	0.162	0.99	1.00	0.217	No
757	15.14	267.28	148.52	118.76	0.69	0.231	1.43	0.162	0.99	1.00	0.216	No
758	15.16	267.65	148.72	118.93	0.69	0.231	1.43	0.162	0.99	1.00	0.216	No
759	15.18	268.01	148.92	119.09	0.69	0.231	1.43	0.162	0.99	1.00	0.215	No
760	15.20	268.37	149.11	119.26	0.69	0.231	1.43	0.162	0.99	1.00	0.215	No
761	15.22	268.74	149.31	119.43	0.69	0.231	1.43	0.162	0.99	1.00	0.215	No
762	15.24	269.11	149.50	119.60	0.69	0.231	1.43	0.161	0.99	1.00	0.214	No
763	15.26	269.47	149.70	119.77	0.69	0.230	1.43	0.161	0.99	1.00	0.215	No
764	15.28	269.85	149.90	119.95	0.68	0.230	1.43	0.161	0.99	1.00	0.215	No
765	15.30	270.22	150.09	120.12	0.68	0.230	1.43	0.161	0.99	1.00	0.215	No
766	15.32	270.59	150.29	120.30	0.68	0.230	1.43	0.161	0.99	1.00	0.215	No
767	15.34	270.97	150.49	120.48	0.68	0.230	1.43	0.161	0.99	1.00	0.215	No
768	15.37	271.53	150.78	120.75	0.68	0.230	1.43	0.161	0.99	1.00	0.215	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
769	15.38	271.72	150.88	120.84	0.68	0.229	1.43	0.161	0.99	1.00	0.216	No
770	15.40	272.09	151.07	121.02	0.68	0.229	1.43	0.160	0.99	1.00	0.216	No
771	15.42	272.46	151.27	121.19	0.68	0.229	1.43	0.160	0.99	1.00	0.216	No
772	15.44	272.83	151.47	121.36	0.68	0.229	1.43	0.160	0.99	1.00	0.216	No
773	15.46	273.20	151.66	121.54	0.68	0.229	1.43	0.160	0.99	1.00	0.216	No
774	15.48	273.57	151.86	121.71	0.68	0.229	1.43	0.160	0.99	1.00	0.216	No
775	15.50	273.93	152.06	121.87	0.68	0.228	1.43	0.160	0.99	1.00	0.216	No
776	15.52	274.29	152.25	122.04	0.68	0.228	1.43	0.160	0.99	1.00	0.216	No
777	15.54	274.65	152.45	122.21	0.68	0.228	1.43	0.160	0.98	1.00	0.216	No
778	15.56	275.01	152.64	122.37	0.68	0.228	1.43	0.160	0.98	1.00	0.216	No
779	15.58	275.37	152.84	122.53	0.68	0.228	1.43	0.159	0.98	1.00	0.216	No
780	15.60	275.72	153.04	122.68	0.68	0.228	1.43	0.159	0.98	1.00	0.216	No
781	15.62	276.07	153.23	122.84	0.68	0.228	1.43	0.159	0.98	1.00	0.216	No
782	15.64	276.42	153.43	122.99	0.68	0.227	1.43	0.159	0.98	1.00	0.216	No
783	15.66	276.77	153.62	123.14	0.68	0.227	1.43	0.159	0.98	1.00	0.215	No
784	15.68	277.11	153.82	123.29	0.68	0.227	1.43	0.159	0.98	1.00	0.215	No
785	15.70	277.46	154.02	123.44	0.68	0.227	1.43	0.159	0.98	1.00	0.215	No
786	15.72	277.80	154.21	123.58	0.68	0.227	1.43	0.159	0.98	1.00	0.215	No
787	15.74	278.13	154.41	123.72	0.67	0.227	1.43	0.159	0.98	1.00	0.215	No
788	15.76	278.47	154.61	123.86	0.67	0.227	1.43	0.159	0.98	1.00	0.215	No
789	15.78	278.81	154.80	124.01	0.67	0.226	1.43	0.159	0.98	1.00	0.215	No
790	15.80	279.15	155.00	124.15	0.67	0.226	1.43	0.158	0.98	1.00	0.215	No
791	15.82	279.49	155.19	124.29	0.67	0.226	1.43	0.158	0.98	1.00	0.214	No
792	15.84	279.83	155.39	124.44	0.67	0.226	1.43	0.158	0.98	1.00	0.214	No
793	15.86	280.16	155.59	124.58	0.67	0.226	1.43	0.158	0.98	1.00	0.214	No
794	15.88	280.50	155.78	124.72	0.67	0.226	1.43	0.158	0.98	1.00	0.214	No
795	15.90	280.84	155.98	124.86	0.67	0.226	1.43	0.158	0.98	1.00	0.214	No
796	15.92	281.18	156.18	125.00	0.67	0.226	1.43	0.158	0.98	1.00	0.214	No
797	15.94	281.52	156.37	125.14	0.67	0.225	1.43	0.158	0.98	1.00	0.214	No
798	15.96	281.85	156.57	125.29	0.67	0.225	1.43	0.158	0.98	1.00	0.214	No
799	15.98	282.19	156.76	125.43	0.67	0.225	1.43	0.158	0.98	1.00	0.214	No
800	16.00	282.53	156.96	125.57	0.67	0.225	1.43	0.158	0.98	1.00	0.214	No
801	16.03	283.04	157.25	125.78	0.67	0.225	1.43	0.157	0.98	1.00	0.213	No
802	16.04	283.20	157.35	125.85	0.67	0.225	1.43	0.157	0.98	1.00	0.213	No
803	16.06	283.54	157.55	125.99	0.67	0.225	1.43	0.157	0.98	1.00	0.213	No
804	16.08	283.88	157.74	126.13	0.67	0.225	1.43	0.157	0.98	1.00	0.213	No
805	16.10	284.21	157.94	126.27	0.67	0.224	1.43	0.157	0.98	1.00	0.213	No
806	16.12	284.55	158.14	126.41	0.67	0.224	1.43	0.157	0.98	1.00	0.213	No
807	16.14	284.88	158.33	126.55	0.67	0.224	1.43	0.157	0.98	1.00	0.213	No
808	16.16	285.21	158.53	126.68	0.67	0.224	1.43	0.157	0.98	1.00	0.213	No
809	16.18	285.55	158.73	126.82	0.67	0.224	1.43	0.157	0.98	1.00	0.213	No
810	16.20	285.88	158.92	126.96	0.66	0.224	1.43	0.157	0.98	1.00	0.213	No
811	16.22	286.21	159.12	127.09	0.66	0.224	1.43	0.157	0.98	1.00	0.213	No
812	16.24	286.54	159.31	127.23	0.66	0.224	1.43	0.156	0.98	1.00	0.212	No
813	16.26	286.87	159.51	127.36	0.66	0.223	1.43	0.156	0.98	1.00	0.212	No
814	16.28	287.20	159.71	127.50	0.66	0.223	1.43	0.156	0.98	1.00	0.212	No
815	16.30	287.54	159.90	127.63	0.66	0.223	1.43	0.156	0.98	1.00	0.212	No
816	16.32	287.87	160.10	127.77	0.66	0.223	1.43	0.156	0.98	1.00	0.212	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
817	16.34	288.20	160.30	127.90	0.66	0.223	1.43	0.156	0.98	1.00	0.212	No
818	16.36	288.53	160.49	128.04	0.66	0.223	1.43	0.156	0.98	1.00	0.212	No
819	16.38	288.86	160.69	128.17	0.66	0.223	1.43	0.156	0.98	1.00	0.212	No
820	16.40	289.19	160.88	128.31	0.66	0.223	1.43	0.156	0.98	1.00	0.212	No
821	16.42	289.52	161.08	128.44	0.66	0.222	1.43	0.156	0.98	1.00	0.212	No
822	16.44	289.85	161.28	128.58	0.66	0.222	1.43	0.156	0.98	1.00	0.211	No
823	16.46	290.18	161.47	128.71	0.66	0.222	1.43	0.156	0.98	1.00	0.211	No
824	16.48	290.52	161.67	128.85	0.66	0.222	1.43	0.155	0.98	1.00	0.211	No
825	16.50	290.85	161.87	128.98	0.66	0.222	1.43	0.155	0.98	1.00	0.211	No
826	16.52	291.18	162.06	129.12	0.66	0.222	1.43	0.155	0.98	1.00	0.211	No
827	16.54	291.51	162.26	129.26	0.66	0.222	1.43	0.155	0.98	1.00	0.211	No
828	16.56	291.85	162.45	129.39	0.66	0.222	1.43	0.155	0.98	1.00	0.211	No
829	16.58	292.18	162.65	129.53	0.66	0.221	1.43	0.155	0.98	1.00	0.211	No
830	16.60	292.52	162.85	129.67	0.66	0.221	1.43	0.155	0.98	1.00	0.211	No
831	16.62	292.85	163.04	129.81	0.66	0.221	1.43	0.155	0.98	1.00	0.210	No
832	16.64	293.18	163.24	129.94	0.66	0.221	1.43	0.155	0.98	1.00	0.210	No
833	16.66	293.51	163.43	130.08	0.66	0.221	1.43	0.155	0.98	1.00	0.210	No
834	16.68	293.85	163.63	130.21	0.65	0.221	1.43	0.155	0.98	1.00	0.210	No
835	16.70	294.18	163.83	130.35	0.65	0.221	1.43	0.155	0.98	1.00	0.210	No
836	16.72	294.51	164.02	130.49	0.65	0.221	1.43	0.154	0.98	1.00	0.210	No
837	16.74	294.85	164.22	130.63	0.65	0.221	1.43	0.154	0.98	1.00	0.209	No
838	16.76	295.19	164.42	130.77	0.65	0.220	1.43	0.154	0.98	1.00	0.209	No
839	16.78	295.52	164.61	130.91	0.65	0.220	1.43	0.154	0.98	1.00	0.210	No
840	16.80	295.86	164.81	131.05	0.65	0.220	1.43	0.154	0.98	1.00	0.210	No
841	16.82	296.20	165.00	131.20	0.65	0.220	1.43	0.154	0.98	1.00	0.210	No
842	16.84	296.54	165.20	131.34	0.65	0.220	1.43	0.154	0.98	1.00	0.209	No
843	16.86	296.87	165.40	131.48	0.65	0.220	1.43	0.154	0.98	1.00	0.209	No
844	16.88	297.21	165.59	131.61	0.65	0.220	1.43	0.154	0.98	1.00	0.209	No
845	16.91	297.71	165.89	131.82	0.65	0.219	1.43	0.154	0.98	1.00	0.209	No
846	16.92	297.88	165.99	131.89	0.65	0.219	1.43	0.154	0.98	1.00	0.209	No
847	16.94	298.22	166.18	132.03	0.65	0.219	1.43	0.153	0.98	1.00	0.208	No
848	16.96	298.55	166.38	132.17	0.65	0.219	1.43	0.153	0.98	1.00	0.208	No
849	16.98	298.89	166.57	132.32	0.65	0.219	1.43	0.153	0.98	1.00	0.208	No
850	17.00	299.23	166.77	132.46	0.65	0.219	1.43	0.153	0.98	1.00	0.208	No
851	17.02	299.57	166.97	132.60	0.65	0.219	1.43	0.153	0.98	1.00	0.208	No
852	17.04	299.91	167.16	132.75	0.65	0.219	1.43	0.153	0.98	1.00	0.208	No
853	17.06	300.25	167.36	132.89	0.65	0.218	1.43	0.153	0.98	1.00	0.208	No
854	17.08	300.59	167.55	133.03	0.65	0.218	1.43	0.153	0.98	1.00	0.208	No
855	17.10	300.93	167.75	133.18	0.65	0.218	1.43	0.153	0.98	1.00	0.208	No
856	17.18	302.29	168.54	133.76	0.64	0.218	1.43	0.152	0.98	1.00	0.207	No
857	17.18	302.29	168.54	133.76	0.64	0.218	1.43	0.152	0.98	1.00	0.207	No
858	17.18	302.29	168.54	133.76	0.64	0.218	1.43	0.152	0.98	1.00	0.207	No
859	17.18	302.29	168.54	133.76	0.64	0.218	1.43	0.152	0.98	1.00	0.207	No
860	17.20	302.64	168.73	133.91	0.64	0.218	1.43	0.152	0.98	1.00	0.206	No
861	17.22	302.98	168.93	134.05	0.64	0.217	1.43	0.152	0.98	1.00	0.206	No
862	17.24	303.33	169.12	134.20	0.64	0.217	1.43	0.152	0.98	1.00	0.206	No
863	17.26	303.67	169.32	134.35	0.64	0.217	1.43	0.152	0.98	1.00	0.206	No
864	17.28	304.02	169.52	134.50	0.64	0.217	1.43	0.152	0.98	1.00	0.206	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
865	17.30	304.36	169.71	134.65	0.64	0.217	1.43	0.152	0.98	1.00	0.206	No
866	17.32	304.71	169.91	134.80	0.64	0.217	1.43	0.152	0.98	1.00	0.206	No
867	17.34	305.05	170.11	134.95	0.64	0.217	1.43	0.152	0.98	1.00	0.206	No
868	17.36	305.40	170.30	135.10	0.64	0.217	1.43	0.152	0.98	1.00	0.206	No
869	17.38	305.74	170.50	135.24	0.64	0.216	1.43	0.151	0.98	1.00	0.206	No
870	17.40	306.08	170.69	135.39	0.64	0.216	1.43	0.151	0.98	1.00	0.206	No
871	17.42	306.42	170.89	135.53	0.64	0.216	1.43	0.151	0.98	1.00	0.206	No
872	17.44	306.77	171.09	135.68	0.64	0.216	1.43	0.151	0.98	1.00	0.206	No
873	17.46	307.11	171.28	135.82	0.64	0.216	1.43	0.151	0.98	1.00	0.206	No
874	17.48	307.44	171.48	135.97	0.64	0.216	1.43	0.151	0.98	1.00	0.206	No
875	17.50	307.78	171.68	136.11	0.64	0.216	1.43	0.151	0.98	1.00	0.206	No
876	17.52	308.12	171.87	136.25	0.64	0.216	1.43	0.151	0.98	1.00	0.206	No
877	17.54	308.45	172.07	136.39	0.64	0.215	1.43	0.151	0.98	1.00	0.205	No
878	17.56	308.79	172.26	136.53	0.64	0.215	1.43	0.151	0.97	1.00	0.204	No
879	17.58	309.13	172.46	136.67	0.64	0.215	1.43	0.151	0.97	1.00	0.204	No
880	17.60	309.48	172.66	136.83	0.64	0.215	1.43	0.151	0.97	1.00	0.203	No
881	17.62	309.83	172.85	136.98	0.64	0.215	1.43	0.150	0.97	1.00	0.203	No
882	17.64	310.19	173.05	137.14	0.64	0.215	1.43	0.150	0.97	1.00	0.203	No
883	17.66	310.54	173.24	137.30	0.63	0.215	1.43	0.150	0.97	1.00	0.203	No
884	17.68	310.90	173.44	137.46	0.63	0.214	1.43	0.150	0.97	1.00	0.203	No
885	17.70	311.26	173.64	137.63	0.63	0.214	1.43	0.150	0.97	1.00	0.204	No
886	17.72	311.62	173.83	137.79	0.63	0.214	1.43	0.150	0.97	1.00	0.204	No
887	17.74	311.99	174.03	137.96	0.63	0.214	1.43	0.150	0.97	1.00	0.202	No
888	17.76	312.35	174.23	138.12	0.63	0.214	1.43	0.150	0.97	1.00	0.202	No
889	17.78	312.71	174.42	138.29	0.63	0.214	1.43	0.150	0.97	1.00	0.203	No
890	17.80	313.07	174.62	138.45	0.63	0.214	1.43	0.150	0.97	1.00	0.203	No
891	17.82	313.43	174.81	138.62	0.63	0.213	1.43	0.149	0.97	1.00	0.203	No
892	17.84	313.79	175.01	138.78	0.63	0.213	1.43	0.149	0.97	1.00	0.203	No
893	17.86	314.14	175.21	138.94	0.63	0.213	1.43	0.149	0.97	1.00	0.203	No
894	17.88	314.50	175.40	139.10	0.63	0.213	1.43	0.149	0.97	1.00	0.203	No
895	17.90	314.86	175.60	139.26	0.63	0.213	1.43	0.149	0.97	1.00	0.202	No
896	17.92	315.21	175.80	139.42	0.63	0.213	1.43	0.149	0.97	1.00	0.200	No
897	17.94	315.57	175.99	139.58	0.63	0.213	1.43	0.149	0.97	1.00	0.200	No
898	17.96	315.93	176.19	139.75	0.63	0.213	1.43	0.149	0.97	1.00	0.200	No
899	17.98	316.30	176.38	139.91	0.63	0.212	1.43	0.149	0.97	1.00	0.200	No
900	18.00	316.66	176.58	140.08	0.63	0.212	1.43	0.149	0.97	1.00	0.200	No
901	18.02	317.03	176.78	140.25	0.63	0.212	1.43	0.148	0.97	1.00	0.200	No
902	18.04	317.39	176.97	140.42	0.63	0.212	1.43	0.148	0.97	1.00	0.199	No
903	18.06	317.76	177.17	140.60	0.63	0.212	1.43	0.148	0.97	1.00	0.197	No
904	18.08	318.14	177.36	140.77	0.63	0.212	1.43	0.148	0.97	1.00	0.197	No
905	18.10	318.51	177.56	140.95	0.63	0.211	1.43	0.148	0.97	1.00	0.198	No
906	18.12	318.89	177.76	141.13	0.63	0.211	1.43	0.148	0.97	1.00	0.198	No
907	18.14	319.26	177.95	141.30	0.63	0.211	1.43	0.148	0.97	1.00	0.197	No
908	18.16	319.63	178.15	141.48	0.62	0.211	1.43	0.148	0.97	1.00	0.197	No
909	18.18	320.00	178.35	141.65	0.62	0.211	1.43	0.148	0.97	1.00	0.199	No
910	18.20	320.36	178.54	141.82	0.62	0.211	1.43	0.148	0.97	1.00	0.200	No
911	18.22	320.73	178.74	141.99	0.62	0.211	1.43	0.147	0.97	1.00	0.201	No
912	18.24	321.09	178.93	142.16	0.62	0.210	1.43	0.147	0.97	1.00	0.201	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
913	18.26	321.45	179.13	142.32	0.62	0.210	1.43	0.147	0.97	1.00	0.200	No
914	18.28	321.81	179.33	142.48	0.62	0.210	1.43	0.147	0.97	1.00	0.199	No
915	18.30	322.17	179.52	142.64	0.62	0.210	1.43	0.147	0.97	1.00	0.198	No
916	18.32	322.53	179.72	142.81	0.62	0.210	1.43	0.147	0.97	1.00	0.198	No
917	18.34	322.89	179.92	142.97	0.62	0.210	1.43	0.147	0.97	1.00	0.197	No
918	18.36	323.26	180.11	143.14	0.62	0.210	1.43	0.147	0.97	1.00	0.195	No
919	18.38	323.62	180.31	143.32	0.62	0.210	1.43	0.147	0.96	1.00	0.193	No
920	18.40	324.00	180.50	143.49	0.62	0.209	1.43	0.147	0.96	1.00	0.193	No
921	18.42	324.37	180.70	143.67	0.62	0.209	1.43	0.146	0.96	1.00	0.192	No
922	18.44	324.74	180.90	143.84	0.62	0.209	1.43	0.146	0.96	1.00	0.192	No
923	18.46	325.11	181.09	144.02	0.62	0.209	1.43	0.146	0.96	1.00	0.193	No
924	18.48	325.49	181.29	144.20	0.62	0.209	1.43	0.146	0.96	1.00	0.193	No
925	18.50	325.86	181.49	144.37	0.62	0.209	1.43	0.146	0.96	1.00	0.192	No
926	18.52	326.23	181.68	144.55	0.62	0.208	1.43	0.146	0.96	1.00	0.192	No
927	18.54	326.61	181.88	144.73	0.62	0.208	1.43	0.146	0.96	1.00	0.193	No
928	18.58	327.36	182.27	145.09	0.62	0.208	1.43	0.146	0.96	1.00	0.192	No
929	18.58	327.36	182.27	145.09	0.62	0.208	1.43	0.146	0.97	1.00	0.196	No
930	18.60	327.73	182.47	145.27	0.62	0.208	1.43	0.146	0.97	1.00	2.000	Yes
931	18.62	328.11	182.66	145.44	0.62	0.208	1.43	0.145	0.97	1.00	2.000	Yes
932	18.64	328.48	182.86	145.62	0.62	0.208	1.43	0.145	0.97	1.00	2.000	Yes
933	18.66	328.85	183.05	145.79	0.62	0.207	1.43	0.145	0.97	1.00	2.000	Yes
934	18.68	329.22	183.25	145.97	0.61	0.207	1.43	0.145	0.96	1.00	2.000	Yes
935	18.70	329.60	183.45	146.15	0.61	0.207	1.43	0.145	0.96	1.00	2.000	Yes
936	18.72	329.98	183.64	146.34	0.61	0.207	1.43	0.145	0.96	1.00	2.000	Yes
937	18.74	330.36	183.84	146.52	0.61	0.207	1.43	0.145	0.96	1.00	2.000	Yes
938	18.76	330.73	184.04	146.70	0.61	0.207	1.43	0.145	0.96	1.00	2.000	Yes
939	18.78	331.10	184.23	146.87	0.61	0.207	1.43	0.145	0.96	1.00	2.000	Yes
940	18.80	331.47	184.43	147.04	0.61	0.206	1.43	0.145	0.96	1.00	2.000	Yes
941	18.82	331.83	184.62	147.21	0.61	0.206	1.43	0.144	0.96	1.00	2.000	Yes
942	18.84	332.19	184.82	147.37	0.61	0.206	1.43	0.144	0.96	1.00	2.000	Yes
943	18.86	332.54	185.02	147.53	0.61	0.206	1.43	0.144	0.96	1.00	0.192	No
944	18.88	332.89	185.21	147.68	0.61	0.206	1.43	0.144	0.96	1.00	0.192	No
945	18.90	333.25	185.41	147.84	0.61	0.206	1.43	0.144	0.96	1.00	0.192	No
946	18.92	333.60	185.61	148.00	0.61	0.206	1.43	0.144	0.96	1.00	0.191	No
947	18.94	333.96	185.80	148.16	0.61	0.206	1.43	0.144	0.96	1.00	0.190	No
948	18.96	334.33	186.00	148.33	0.61	0.205	1.43	0.144	0.96	1.00	0.189	No
949	18.98	334.70	186.19	148.51	0.61	0.205	1.43	0.144	0.96	1.00	0.187	No
950	19.07	336.38	187.08	149.30	0.61	0.205	1.43	0.143	0.96	1.00	0.186	No
951	19.07	336.38	187.08	149.30	0.61	0.205	1.43	0.143	0.96	1.00	0.186	No
952	19.07	336.38	187.08	149.30	0.61	0.205	1.43	0.143	0.96	1.00	0.186	No
953	19.08	336.57	187.17	149.39	0.61	0.205	1.43	0.143	0.96	1.00	0.183	No
954	19.10	336.95	187.37	149.58	0.61	0.204	1.43	0.143	0.95	1.00	0.177	No
955	19.12	337.33	187.57	149.77	0.61	0.204	1.43	0.143	0.95	1.00	0.175	No
956	19.22	339.24	188.55	150.69	0.60	0.204	1.43	0.142	0.95	1.00	0.176	No
957	19.22	339.24	188.55	150.69	0.60	0.204	1.43	0.142	0.95	1.00	0.177	No
958	19.14	337.74	187.76	149.98	0.61	0.204	1.43	0.143	0.95	1.00	0.178	No
959	19.22	339.21	188.55	150.66	0.60	0.204	1.43	0.142	0.96	1.00	0.186	No
960	19.24	339.56	188.74	150.82	0.60	0.203	1.43	0.142	0.96	1.00	0.188	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
961	19.26	339.92	188.94	150.97	0.60	0.203	1.43	0.142	0.96	1.00	2.000	Yes
962	19.28	340.26	189.14	151.13	0.60	0.203	1.43	0.142	0.96	1.00	2.000	Yes
963	19.30	340.61	189.33	151.28	0.60	0.203	1.43	0.142	0.96	1.00	2.000	Yes
964	19.32	340.95	189.53	151.42	0.60	0.203	1.43	0.142	0.96	1.00	2.000	Yes
965	19.34	341.29	189.73	151.56	0.60	0.203	1.43	0.142	0.96	1.00	2.000	Yes
966	19.36	341.63	189.92	151.70	0.60	0.203	1.43	0.142	0.96	1.00	2.000	Yes
967	19.38	341.97	190.12	151.85	0.60	0.203	1.43	0.142	0.96	1.00	2.000	Yes
968	19.40	342.33	190.31	152.01	0.60	0.202	1.43	0.142	0.96	1.00	2.000	Yes
969	19.42	342.68	190.51	152.17	0.60	0.202	1.43	0.142	0.96	1.00	2.000	Yes
970	19.44	343.04	190.71	152.34	0.60	0.202	1.43	0.142	0.96	1.00	2.000	Yes
971	19.46	343.41	190.90	152.51	0.60	0.202	1.43	0.141	0.96	1.00	0.192	No
972	19.48	343.78	191.10	152.68	0.60	0.202	1.43	0.141	0.96	1.00	2.000	Yes
973	19.50	344.15	191.30	152.85	0.60	0.202	1.43	0.141	0.96	1.00	2.000	Yes
974	19.52	344.53	191.49	153.03	0.60	0.202	1.43	0.141	0.96	1.00	2.000	Yes
975	19.54	344.91	191.69	153.22	0.60	0.202	1.43	0.141	0.96	1.00	2.000	Yes
976	19.56	345.29	191.88	153.41	0.60	0.201	1.43	0.141	0.95	1.00	2.000	Yes
977	19.58	345.67	192.08	153.59	0.60	0.201	1.43	0.141	0.95	1.00	2.000	Yes
978	19.60	346.06	192.28	153.78	0.60	0.201	1.43	0.141	0.95	1.00	2.000	Yes
979	19.62	346.44	192.47	153.96	0.60	0.201	1.43	0.141	0.95	1.00	2.000	Yes
980	19.64	346.81	192.67	154.14	0.60	0.201	1.43	0.141	0.95	1.00	2.000	Yes
981	19.66	347.18	192.86	154.31	0.60	0.201	1.43	0.140	0.95	1.00	0.181	No
982	19.68	347.54	193.06	154.48	0.60	0.201	1.43	0.140	0.95	1.00	0.184	No
983	19.70	347.90	193.26	154.64	0.60	0.200	1.43	0.140	0.96	1.00	0.186	No
984	19.72	348.25	193.45	154.80	0.60	0.200	1.43	0.140	0.96	1.00	0.188	No
985	19.74	348.60	193.65	154.95	0.60	0.200	1.43	0.140	0.96	1.00	0.188	No
986	19.76	348.95	193.85	155.10	0.59	0.200	1.43	0.140	0.96	1.00	0.188	No
987	19.78	349.30	194.04	155.26	0.59	0.200	1.43	0.140	0.96	1.00	0.188	No
988	19.81	349.83	194.34	155.49	0.59	0.200	1.43	0.140	0.96	1.00	0.187	No
989	19.82	350.01	194.43	155.57	0.59	0.200	1.43	0.140	0.96	1.00	0.186	No
990	19.84	350.36	194.63	155.73	0.59	0.200	1.43	0.140	0.96	1.00	0.186	No
991	19.86	350.71	194.83	155.88	0.59	0.200	1.43	0.140	0.96	1.00	2.000	Yes
992	19.88	351.06	195.02	156.04	0.59	0.199	1.43	0.140	0.96	1.00	2.000	Yes
993	19.90	351.41	195.22	156.19	0.59	0.199	1.43	0.139	0.96	1.00	2.000	Yes
994	19.92	351.75	195.42	156.33	0.59	0.199	1.43	0.139	0.96	1.00	2.000	Yes
995	19.94	352.09	195.61	156.48	0.59	0.199	1.43	0.139	0.96	1.00	2.000	Yes
996	19.96	352.43	195.81	156.62	0.59	0.199	1.43	0.139	0.96	1.00	2.000	Yes
997	19.98	352.78	196.00	156.77	0.59	0.199	1.43	0.139	0.96	1.00	2.000	Yes
998	20.00	353.14	196.20	156.94	0.59	0.199	1.43	0.139	0.96	1.00	2.000	Yes
999	20.02	353.50	196.40	157.10	0.59	0.199	1.43	0.139	0.96	1.00	2.000	Yes
1000	20.04	353.86	196.59	157.27	0.59	0.198	1.43	0.139	0.96	1.00	2.000	Yes
1001	20.06	354.23	196.79	157.44	0.59	0.198	1.43	0.139	0.96	1.00	0.190	No
1002	20.08	354.59	196.98	157.61	0.59	0.198	1.43	0.139	0.96	1.00	0.191	No
1003	20.10	354.95	197.18	157.77	0.59	0.198	1.43	0.139	0.96	1.00	0.191	No
1004	20.12	355.31	197.38	157.93	0.59	0.198	1.43	0.139	0.96	1.00	0.190	No
1005	20.14	355.67	197.57	158.09	0.59	0.198	1.43	0.138	0.96	1.00	0.190	No
1006	20.16	356.03	197.77	158.26	0.59	0.198	1.43	0.138	0.96	1.00	2.000	Yes
1007	20.18	356.40	197.97	158.43	0.59	0.198	1.43	0.138	0.96	1.00	2.000	Yes
1008	20.20	356.77	198.16	158.61	0.59	0.197	1.43	0.138	0.95	1.00	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1009	20.22	357.14	198.36	158.78	0.59	0.197	1.43	0.138	0.95	1.00	2.000	Yes
1010	20.24	357.51	198.55	158.95	0.59	0.197	1.43	0.138	0.95	1.00	2.000	Yes
1011	20.26	357.87	198.75	159.12	0.59	0.197	1.43	0.138	0.95	1.00	2.000	Yes
1012	20.28	358.23	198.95	159.28	0.59	0.197	1.43	0.138	0.95	1.00	2.000	Yes
1013	20.30	358.58	199.14	159.44	0.59	0.197	1.43	0.138	0.96	1.00	2.000	Yes
1014	20.32	358.93	199.34	159.59	0.59	0.197	1.43	0.138	0.96	1.00	0.185	No
1015	20.34	359.28	199.54	159.74	0.58	0.197	1.43	0.138	0.96	1.00	0.185	No
1016	20.36	359.63	199.73	159.90	0.58	0.197	1.43	0.138	0.95	1.00	0.184	No
1017	20.38	359.98	199.93	160.05	0.58	0.196	1.43	0.137	0.95	1.00	0.184	No
1018	20.40	360.33	200.12	160.21	0.58	0.196	1.43	0.137	0.95	1.00	0.184	No
1019	20.42	360.68	200.32	160.36	0.58	0.196	1.43	0.137	0.95	1.00	0.184	No
1020	20.44	361.03	200.52	160.52	0.58	0.196	1.43	0.137	0.95	1.00	0.184	No
1021	20.46	361.38	200.71	160.67	0.58	0.196	1.43	0.137	0.95	1.00	0.184	No
1022	20.48	361.73	200.91	160.82	0.58	0.196	1.43	0.137	0.95	1.00	0.184	No
1023	20.50	362.08	201.11	160.97	0.58	0.196	1.43	0.137	0.96	1.00	0.184	No
1024	20.52	362.43	201.30	161.12	0.58	0.196	1.43	0.137	0.96	1.00	0.185	No
1025	20.54	362.77	201.50	161.27	0.58	0.196	1.43	0.137	0.96	1.00	0.185	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (m)
σ_v: Total overburden pressure at test point (kPa)
u_0: Water pressure at test point (kPa)
σ_v': Effective overburden pressure based on GWT during earthquake (kPa)
r_d: Nonlinear shear mass factor
CSR: Cyclic Stress Ratio
MSF: Magnitude Scaling Factor
CSR_{eq}: CSR adjusted for M=7.5
K_σ: Effective overburden stress factor
CSR^*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1	0.02	0.50	100.00	3.08	0.59	1.70	7.96	0.00	7.96	4.000	No	Yes	2.00
2	0.05	0.56	100.00	3.13	0.59	1.70	9.01	0.00	9.01	4.000	No	Yes	2.00
3	0.06	0.58	100.00	3.13	0.58	1.70	10.23	0.00	10.23	4.000	No	Yes	2.00
4	0.08	0.60	100.00	3.15	0.58	1.70	10.11	0.00	10.11	4.000	No	Yes	2.00
5	0.10	0.59	100.00	3.19	0.58	1.70	9.83	0.00	9.83	4.000	No	Yes	2.00
6	0.12	0.59	100.00	3.23	0.58	1.70	9.91	0.00	9.91	4.000	No	Yes	2.00
7	0.14	0.61	100.00	3.24	0.58	1.70	9.96	0.00	9.96	4.000	No	Yes	2.00
8	0.16	0.70	100.00	3.19	0.58	1.70	10.96	0.00	10.96	4.000	No	Yes	2.00
9	0.18	0.84	100.00	3.10	0.57	1.70	13.98	0.00	13.98	4.000	No	Yes	2.00
10	0.20	1.01	100.00	3.00	0.56	1.70	17.28	0.00	17.28	4.000	No	Yes	2.00
11	0.22	1.15	97.54	2.93	0.55	1.70	19.32	0.00	19.32	4.000	No	Yes	2.00
12	0.24	1.23	95.02	2.90	0.54	1.70	21.06	0.00	21.06	4.000	No	Yes	2.00
13	0.26	1.29	93.64	2.88	0.54	1.70	21.35	0.00	21.35	4.000	No	Yes	2.00
14	0.28	1.33	93.40	2.88	0.54	1.70	22.56	0.00	22.56	4.000	No	Yes	2.00
15	0.30	1.35	94.26	2.89	0.54	1.70	22.77	0.00	22.77	4.000	No	Yes	2.00
16	0.32	1.33	96.90	2.92	0.54	1.70	22.43	0.00	22.43	4.000	No	Yes	2.00
17	0.34	1.32	100.00	2.96	0.54	1.70	21.89	0.00	21.89	4.000	No	Yes	2.00
18	0.36	1.31	100.00	2.99	0.54	1.70	21.93	0.00	21.93	4.000	No	Yes	2.00
19	0.38	1.31	100.00	3.01	0.54	1.70	22.06	0.00	22.06	4.000	No	Yes	2.00
20	0.40	1.28	100.00	3.04	0.54	1.70	21.63	0.00	21.63	4.000	No	Yes	2.00
21	0.42	1.24	100.00	3.08	0.54	1.70	20.57	0.00	20.57	4.000	No	Yes	2.00
22	0.44	1.20	100.00	3.11	0.55	1.70	19.97	0.00	19.97	4.000	No	Yes	2.00
23	0.46	1.17	100.00	3.12	0.55	1.70	19.53	0.00	19.53	4.000	No	Yes	2.00
24	0.48	1.15	100.00	3.13	0.55	1.70	19.53	0.00	19.53	4.000	No	Yes	2.00
25	0.50	1.13	100.00	3.14	0.55	1.70	18.81	0.00	18.81	4.000	No	Yes	2.00
26	0.52	1.10	100.00	3.16	0.55	1.70	18.44	0.00	18.44	4.000	No	Yes	2.00
27	0.54	1.08	100.00	3.16	0.55	1.70	17.83	0.00	17.83	4.000	No	Yes	2.00
28	0.56	1.07	100.00	3.16	0.55	1.70	17.84	0.00	17.84	4.000	No	Yes	2.00
29	0.58	1.07	100.00	3.14	0.55	1.70	17.93	0.00	17.93	4.000	No	Yes	2.00
30	0.60	1.07	100.00	3.14	0.55	1.70	18.06	0.00	18.06	4.000	No	Yes	2.00
31	0.62	1.08	100.00	3.13	0.55	1.70	18.03	0.00	18.03	4.000	No	Yes	2.00
32	0.64	1.09	100.00	3.12	0.55	1.70	18.05	0.00	18.05	4.000	No	Yes	2.00
33	0.66	1.09	100.00	3.11	0.55	1.70	18.53	0.00	18.53	4.000	No	Yes	2.00
34	0.68	1.08	100.00	3.11	0.55	1.70	18.08	0.00	18.08	4.000	No	Yes	2.00
35	0.70	1.07	100.00	3.12	0.55	1.70	17.83	0.00	17.83	4.000	No	Yes	2.00
36	0.72	1.05	100.00	3.13	0.55	1.70	17.65	0.00	17.65	4.000	No	Yes	2.00
37	0.74	1.03	100.00	3.14	0.56	1.70	17.16	0.00	17.16	4.000	No	Yes	2.00
38	0.76	1.01	100.00	3.15	0.56	1.70	16.79	0.00	16.79	4.000	No	Yes	2.00
39	0.78	1.00	100.00	3.16	0.56	1.70	16.85	0.00	16.85	4.000	No	Yes	2.00
40	0.80	0.99	100.00	3.17	0.56	1.70	16.52	0.00	16.52	4.000	No	Yes	2.00
41	0.82	0.98	100.00	3.17	0.56	1.70	16.50	0.00	16.50	4.000	No	Yes	2.00
42	0.84	0.95	100.00	3.17	0.56	1.70	16.36	0.00	16.36	4.000	No	Yes	2.00
43	1.04	0.92	100.00	3.19	0.56	1.70	15.15	0.00	15.15	4.000	No	Yes	2.00
44	1.04	0.89	100.00	3.20	0.56	1.70	15.15	0.00	15.15	4.000	No	Yes	2.00
45	1.04	0.89	100.00	3.20	0.56	1.70	14.92	0.00	14.92	4.000	No	Yes	2.00
46	1.04	0.88	100.00	3.20	0.56	1.70	14.92	0.00	14.92	4.000	No	Yes	2.00
47	1.04	0.89	100.00	3.17	0.56	1.70	14.92	0.00	14.92	4.000	No	Yes	2.00
48	0.96	0.92	100.00	3.13	0.56	1.70	15.42	0.00	15.42	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
49	0.98	0.94	100.00	3.09	0.56	1.70	16.00	0.00	16.00	4.000	No	Yes	2.00
50	1.00	0.95	100.00	3.08	0.56	1.70	15.95	0.00	15.95	4.000	No	Yes	2.00
51	1.02	0.95	100.00	3.08	0.56	1.70	16.10	0.00	16.10	4.000	No	Yes	2.00
52	1.04	0.96	100.00	3.07	0.56	1.70	16.01	0.00	16.01	4.000	No	Yes	2.00
53	1.06	0.97	100.00	3.07	0.56	1.70	16.23	0.00	16.23	4.000	No	Yes	2.00
54	1.08	0.98	100.00	3.08	0.56	1.70	16.53	0.00	16.53	4.000	No	Yes	2.00
55	1.10	0.98	100.00	3.09	0.56	1.70	16.47	0.00	16.47	4.000	No	Yes	2.00
56	1.12	0.97	100.00	3.11	0.56	1.70	16.50	0.00	16.50	4.000	No	Yes	2.00
57	1.14	0.95	100.00	3.13	0.56	1.70	15.96	0.00	15.96	4.000	No	Yes	2.00
58	1.16	0.93	100.00	3.15	0.56	1.70	15.55	0.00	15.55	4.000	No	Yes	2.00
59	1.18	0.91	100.00	3.17	0.56	1.70	15.22	0.00	15.22	4.000	No	Yes	2.00
60	1.20	0.90	100.00	3.18	0.56	1.70	14.97	0.00	14.97	4.000	No	Yes	2.00
61	1.32	0.89	100.00	3.19	0.56	1.70	14.92	0.00	14.92	4.000	No	Yes	2.00
62	1.32	0.88	100.00	3.19	0.56	1.70	14.92	0.00	14.92	4.000	No	Yes	2.00
63	1.32	0.88	100.00	3.20	0.56	1.70	14.73	0.00	14.73	4.000	No	Yes	2.00
64	1.32	0.85	100.00	3.22	0.56	1.70	14.73	0.00	14.73	4.000	No	Yes	2.00
65	1.30	0.81	100.00	3.25	0.57	1.70	13.26	0.00	13.26	4.000	No	Yes	2.00
66	1.32	0.77	100.00	3.28	0.57	1.70	12.88	0.00	12.88	4.000	No	Yes	2.00
67	1.34	0.77	100.00	3.29	0.57	1.70	12.77	0.00	12.77	4.000	No	Yes	2.00
68	1.36	0.77	100.00	3.27	0.57	1.70	12.91	0.00	12.91	4.000	No	Yes	2.00
69	1.38	0.80	100.00	3.24	0.57	1.70	13.15	0.00	13.15	4.000	No	Yes	2.00
70	1.40	0.83	100.00	3.21	0.57	1.70	14.06	0.00	14.06	4.000	No	Yes	2.00
71	1.42	0.88	100.00	3.17	0.56	1.70	14.62	0.00	14.62	4.000	No	Yes	2.00
72	1.44	0.93	100.00	3.13	0.56	1.70	15.53	0.00	15.53	4.000	No	Yes	2.00
73	1.46	1.00	100.00	3.09	0.56	1.70	16.60	0.00	16.60	4.000	No	Yes	2.00
74	1.49	1.07	100.00	3.04	0.55	1.70	18.01	0.00	18.01	4.000	No	Yes	2.00
75	1.50	1.11	100.00	3.02	0.55	1.70	19.01	0.00	19.01	4.000	No	Yes	2.00
76	1.53	1.14	100.00	3.00	0.55	1.70	18.91	0.00	18.91	4.000	No	Yes	2.00
77	1.54	1.14	100.00	3.00	0.55	1.70	19.28	0.00	19.28	4.000	No	Yes	2.00
78	1.56	1.14	100.00	3.00	0.55	1.70	18.97	0.00	18.97	4.000	No	Yes	2.00
79	1.58	1.12	100.00	3.01	0.55	1.70	18.91	0.00	18.91	4.000	No	Yes	2.00
80	1.60	1.11	100.00	3.01	0.55	1.70	18.60	0.00	18.60	4.000	No	Yes	2.00
81	1.62	1.09	100.00	3.01	0.55	1.70	18.43	0.00	18.43	4.000	No	Yes	2.00
82	1.64	1.06	100.00	3.02	0.55	1.70	17.58	0.00	17.58	4.000	No	Yes	2.00
83	1.66	1.02	100.00	3.03	0.56	1.70	17.09	0.00	17.09	4.000	No	Yes	2.00
84	1.68	0.99	100.00	3.04	0.56	1.70	16.40	0.00	16.40	4.000	No	Yes	2.00
85	1.70	0.95	100.00	3.05	0.56	1.70	16.11	0.00	16.11	4.000	No	Yes	2.00
86	1.72	0.91	100.00	3.06	0.56	1.70	15.43	0.00	15.43	4.000	No	Yes	2.00
87	1.74	0.87	100.00	3.09	0.57	1.70	14.39	0.00	14.39	4.000	No	Yes	2.00
88	1.76	0.83	100.00	3.11	0.57	1.70	13.99	0.00	13.99	4.000	No	Yes	2.00
89	1.78	0.81	100.00	3.12	0.57	1.70	13.50	0.00	13.50	4.000	No	Yes	2.00
90	1.80	0.79	100.00	3.13	0.57	1.70	13.28	0.00	13.28	4.000	No	Yes	2.00
91	1.82	0.76	100.00	3.14	0.57	1.70	12.68	0.00	12.68	4.000	No	Yes	2.00
92	1.84	0.73	100.00	3.15	0.57	1.70	12.27	0.00	12.27	4.000	No	Yes	2.00
93	1.86	0.72	100.00	3.14	0.58	1.70	11.35	0.00	11.35	4.000	No	Yes	2.00
94	1.88	0.73	100.00	3.12	0.57	1.70	12.29	0.00	12.29	4.000	No	Yes	2.00
95	1.91	0.74	100.00	3.09	0.57	1.70	12.56	0.00	12.56	4.000	No	Yes	2.00
96	1.92	0.73	100.00	3.09	0.57	1.70	12.05	0.00	12.05	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
97	1.94	0.71	100.00	3.10	0.58	1.70	11.77	0.00	11.77	4.000	No	Yes	2.00
98	1.96	0.70	100.00	3.10	0.58	1.70	11.57	0.00	11.57	4.000	No	Yes	2.00
99	1.98	0.69	100.00	3.10	0.58	1.70	11.33	0.00	11.33	4.000	No	Yes	2.00
100	2.00	0.68	100.00	3.10	0.58	1.70	11.21	0.00	11.21	4.000	No	Yes	2.00
101	2.02	0.67	100.00	3.10	0.58	1.70	10.93	0.00	10.93	4.000	No	Yes	2.00
102	2.04	0.65	100.00	3.11	0.58	1.70	10.92	0.00	10.92	4.000	No	Yes	2.00
103	2.06	0.64	100.00	3.12	0.58	1.70	10.53	0.00	10.53	4.000	No	Yes	2.00
104	2.08	0.61	100.00	3.14	0.58	1.70	9.94	0.00	9.94	4.000	No	Yes	2.00
105	2.10	0.58	100.00	3.18	0.58	1.70	9.66	0.00	9.66	4.000	No	Yes	2.00
106	2.13	0.55	100.00	3.21	0.59	1.70	9.03	0.00	9.03	4.000	No	Yes	2.00
107	2.14	0.53	100.00	3.24	0.59	1.70	8.63	0.00	8.63	4.000	No	Yes	2.00
108	2.16	0.50	100.00	3.26	0.59	1.70	8.31	0.00	8.31	4.000	No	Yes	2.00
109	2.18	0.48	100.00	3.28	0.59	1.70	7.71	0.00	7.71	4.000	No	Yes	2.00
110	2.20	0.46	100.00	3.30	0.59	1.70	7.32	0.00	7.32	4.000	No	Yes	2.00
111	2.22	0.46	100.00	3.28	0.59	1.70	7.50	0.00	7.50	4.000	No	Yes	2.00
112	2.24	0.48	100.00	3.24	0.59	1.70	7.76	0.00	7.76	4.000	No	Yes	2.00
113	2.26	0.50	100.00	3.19	0.59	1.70	8.10	0.00	8.10	4.000	No	Yes	2.00
114	2.28	0.54	100.00	3.13	0.59	1.70	8.80	0.00	8.80	4.000	No	Yes	2.00
115	2.30	0.58	100.00	3.08	0.58	1.70	9.45	0.00	9.45	4.000	No	Yes	2.00
116	2.32	0.62	100.00	3.03	0.58	1.70	10.26	0.00	10.26	4.000	No	Yes	2.00
117	2.34	0.65	100.00	2.99	0.58	1.70	10.95	0.00	10.95	4.000	No	Yes	2.00
118	2.37	0.65	100.00	2.99	0.58	1.70	10.98	0.00	10.98	4.000	No	Yes	2.00
119	2.38	0.62	100.00	3.01	0.58	1.70	10.00	0.00	10.00	4.000	No	Yes	2.00
120	2.42	0.56	100.00	3.06	0.58	1.70	9.80	0.00	9.80	4.000	No	Yes	2.00
121	2.42	0.52	100.00	3.11	0.59	1.70	7.95	0.00	7.95	4.000	No	Yes	2.00
122	2.44	0.49	100.00	3.14	0.59	1.70	7.78	0.00	7.78	4.000	No	Yes	2.00
123	2.46	0.51	100.00	3.10	0.59	1.70	8.24	0.00	8.24	4.000	No	Yes	2.00
124	2.48	0.55	100.00	3.05	0.59	1.70	8.93	0.00	8.93	4.000	No	Yes	2.00
125	2.50	0.59	100.00	3.00	0.58	1.70	9.94	0.00	9.94	4.000	No	Yes	2.00
126	2.52	0.62	100.00	2.97	0.58	1.70	10.20	0.00	10.20	4.000	No	Yes	2.00
127	2.54	0.63	99.71	2.96	0.58	1.70	10.50	0.00	10.50	4.000	No	Yes	2.00
128	2.56	0.64	99.10	2.95	0.58	1.70	10.41	0.00	10.41	4.000	No	Yes	2.00
129	2.58	0.66	97.75	2.93	0.58	1.70	10.72	0.00	10.72	4.000	No	Yes	2.00
130	2.60	0.68	96.72	2.92	0.58	1.70	11.53	0.00	11.53	4.000	No	Yes	2.00
131	2.62	0.70	95.84	2.91	0.58	1.70	11.44	0.00	11.44	4.000	No	Yes	2.00
132	2.64	0.68	98.65	2.95	0.58	1.70	11.47	0.00	11.47	4.000	No	Yes	2.00
133	2.66	0.66	100.00	2.99	0.58	1.70	10.56	0.00	10.56	4.000	No	Yes	2.00
134	2.68	0.63	100.00	3.04	0.58	1.70	10.27	0.00	10.27	4.000	No	Yes	2.00
135	2.70	0.61	100.00	3.05	0.58	1.70	9.95	0.00	9.95	4.000	No	Yes	2.00
136	2.72	0.60	100.00	3.07	0.58	1.70	9.82	0.00	9.82	4.000	No	Yes	2.00
137	2.74	0.60	100.00	3.07	0.58	1.70	9.61	0.00	9.61	4.000	No	Yes	2.00
138	2.76	0.60	100.00	3.07	0.58	1.70	9.92	0.00	9.92	4.000	No	Yes	2.00
139	2.78	0.60	100.00	3.07	0.58	1.70	10.06	0.00	10.06	4.000	No	Yes	2.00
140	2.80	0.58	100.00	3.09	0.58	1.70	9.51	0.00	9.51	4.000	No	Yes	2.00
141	2.82	0.55	100.00	3.11	0.59	1.70	8.75	0.00	8.75	4.000	No	Yes	2.00
142	2.84	0.54	100.00	3.13	0.59	1.70	8.62	0.00	8.62	4.000	No	Yes	2.00
143	2.86	0.54	100.00	3.15	0.59	1.70	9.19	0.00	9.19	4.000	No	Yes	2.00
144	2.89	0.52	100.00	3.19	0.59	1.70	8.44	0.00	8.44	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
145	2.90	0.48	100.00	3.26	0.59	1.70	7.93	0.00	7.93	4.000	No	Yes	2.00
146	2.92	0.45	100.00	3.31	0.59	1.70	7.03	0.00	7.03	4.000	No	Yes	2.00
147	2.94	0.42	100.00	3.36	0.60	1.70	6.79	0.00	6.79	4.000	No	Yes	2.00
148	2.96	0.41	100.00	3.38	0.60	1.70	6.67	0.00	6.67	4.000	No	Yes	2.00
149	2.99	0.41	100.00	3.39	0.60	1.70	6.43	0.00	6.43	4.000	No	Yes	2.00
150	3.00	0.40	100.00	3.38	0.60	1.70	6.62	0.00	6.62	4.000	No	Yes	2.00
151	3.03	0.40	100.00	3.37	0.60	1.70	6.50	0.00	6.50	4.000	No	Yes	2.00
152	3.05	0.40	100.00	3.36	0.60	1.70	6.33	0.00	6.33	4.000	No	Yes	2.00
153	3.06	0.39	100.00	3.35	0.60	1.70	6.48	0.00	6.48	4.000	No	Yes	2.00
154	3.08	0.40	100.00	3.32	0.60	1.70	6.24	0.00	6.24	4.000	No	Yes	2.00
155	3.10	0.41	100.00	3.29	0.60	1.70	6.51	0.00	6.51	4.000	No	Yes	2.00
156	3.12	0.43	100.00	3.25	0.59	1.70	7.01	0.00	7.01	4.000	No	Yes	2.00
157	3.14	0.44	100.00	3.24	0.59	1.70	7.16	0.00	7.16	4.000	No	Yes	2.00
158	3.16	0.43	100.00	3.26	0.59	1.70	6.96	0.00	6.96	4.000	No	Yes	2.00
159	3.18	0.40	100.00	3.30	0.60	1.70	6.68	0.00	6.68	4.000	No	Yes	2.00
160	3.20	0.38	100.00	3.33	0.60	1.70	5.78	0.00	5.78	4.000	No	Yes	2.00
161	3.22	0.37	100.00	3.34	0.60	1.70	5.73	0.00	5.73	4.000	No	Yes	2.00
162	3.24	0.41	100.00	3.24	0.60	1.70	6.15	0.00	6.15	4.000	No	Yes	2.00
163	3.26	0.57	100.00	3.01	0.59	1.70	8.06	0.00	8.06	4.000	No	Yes	2.00
164	3.28	0.85	82.23	2.74	0.57	1.70	13.79	0.00	13.79	4.000	Yes	Yes	2.00
165	3.30	1.15	67.17	2.55	0.56	1.70	19.98	55.90	75.88	4.000	Yes	No	2.00
166	3.32	1.36	60.44	2.47	0.55	1.70	23.16	55.32	78.48	4.000	Yes	No	2.00
167	3.34	1.49	58.21	2.44	0.55	1.70	24.58	55.13	79.71	4.000	Yes	No	2.00
168	3.36	1.58	56.81	2.42	0.54	1.70	26.54	55.28	81.83	0.118	No	No	0.43
169	3.38	1.64	56.15	2.41	0.54	1.70	27.76	55.43	83.18	4.000	Yes	No	2.00
170	3.40	1.59	58.06	2.44	0.54	1.70	27.55	55.92	83.47	4.000	Yes	No	2.00
171	3.42	1.42	62.63	2.50	0.55	1.70	23.75	56.01	79.77	4.000	Yes	No	2.00
172	3.44	1.16	71.33	2.60	0.56	1.70	19.57	0.00	19.57	4.000	Yes	Yes	2.00
173	3.46	0.92	81.82	2.74	0.57	1.70	14.38	0.00	14.38	4.000	Yes	Yes	2.00
174	3.48	0.74	92.60	2.87	0.58	1.70	11.84	0.00	11.84	4.000	Yes	Yes	2.00
175	3.50	0.65	98.64	2.95	0.58	1.70	10.31	0.00	10.31	4.000	Yes	Yes	2.00
176	3.52	0.62	99.96	2.96	0.58	1.70	9.87	0.00	9.87	4.000	No	Yes	2.00
177	3.54	0.61	99.66	2.96	0.58	1.70	10.13	0.00	10.13	4.000	No	Yes	2.00
178	3.56	0.60	99.86	2.96	0.58	1.70	9.81	0.00	9.81	4.000	No	Yes	2.00
179	3.58	0.58	100.00	2.99	0.58	1.70	9.41	0.00	9.41	4.000	No	Yes	2.00
180	3.60	0.60	100.00	2.98	0.58	1.70	9.32	0.00	9.32	4.000	No	Yes	2.00
181	3.62	0.64	99.61	2.96	0.58	1.70	10.68	0.00	10.68	4.000	No	Yes	2.00
182	3.64	0.68	97.42	2.93	0.58	1.70	11.14	0.00	11.14	4.000	No	Yes	2.00
183	3.66	0.67	98.80	2.95	0.58	1.70	11.17	0.00	11.17	4.000	No	Yes	2.00
184	3.68	0.65	100.00	2.99	0.58	1.70	10.50	0.00	10.50	4.000	No	Yes	2.00
185	3.70	0.62	100.00	3.03	0.58	1.70	10.02	0.00	10.02	4.000	No	Yes	2.00
186	3.72	0.61	100.00	3.07	0.58	1.70	9.98	0.00	9.98	4.000	No	Yes	2.00
187	3.74	0.60	100.00	3.11	0.58	1.70	9.66	0.00	9.66	4.000	No	Yes	2.00
188	3.76	0.59	100.00	3.17	0.58	1.70	9.96	0.00	9.96	4.000	No	Yes	2.00
189	3.78	0.59	100.00	3.22	0.58	1.70	9.44	0.00	9.44	4.000	No	Yes	2.00
190	3.80	0.59	100.00	3.26	0.58	1.70	9.52	0.00	9.52	4.000	No	Yes	2.00
191	3.82	0.60	100.00	3.29	0.58	1.70	9.81	0.00	9.81	4.000	No	Yes	2.00
192	3.84	0.60	100.00	3.30	0.58	1.70	9.80	0.00	9.80	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
193	3.86	0.61	100.00	3.31	0.58	1.70	9.84	0.00	9.84	4.000	No	Yes	2.00
194	3.88	0.61	100.00	3.31	0.58	1.70	10.08	0.00	10.08	4.000	No	Yes	2.00
195	3.90	0.62	100.00	3.29	0.58	1.70	9.96	0.00	9.96	4.000	No	Yes	2.00
196	3.92	0.62	100.00	3.29	0.58	1.70	10.38	0.00	10.38	4.000	No	Yes	2.00
197	3.94	0.62	100.00	3.29	0.58	1.70	10.06	0.00	10.06	4.000	No	Yes	2.00
198	3.96	0.61	100.00	3.30	0.58	1.70	9.74	0.00	9.74	4.000	No	Yes	2.00
199	3.98	0.60	100.00	3.29	0.58	1.70	9.85	0.00	9.85	4.000	No	Yes	2.00
200	4.00	0.61	100.00	3.28	0.58	1.70	9.88	0.00	9.88	4.000	No	Yes	2.00
201	4.02	0.62	100.00	3.27	0.58	1.70	9.80	0.00	9.80	4.000	No	Yes	2.00
202	4.04	0.64	100.00	3.25	0.58	1.70	10.30	0.00	10.30	4.000	No	Yes	2.00
203	4.06	0.65	100.00	3.23	0.58	1.70	10.76	0.00	10.76	4.000	No	Yes	2.00
204	4.08	0.66	100.00	3.22	0.58	1.70	10.60	0.00	10.60	4.000	No	Yes	2.00
205	4.10	0.67	100.00	3.22	0.58	1.70	10.63	0.00	10.63	4.000	No	Yes	2.00
206	4.12	0.70	100.00	3.19	0.58	1.70	11.13	0.00	11.13	4.000	No	Yes	2.00
207	4.14	0.75	100.00	3.14	0.57	1.70	12.14	0.00	12.14	4.000	No	Yes	2.00
208	4.16	0.80	100.00	3.10	0.57	1.70	13.18	0.00	13.18	4.000	No	Yes	2.00
209	4.18	0.85	100.00	3.08	0.57	1.70	14.11	0.00	14.11	4.000	No	Yes	2.00
210	4.20	0.87	100.00	3.07	0.57	1.70	14.30	0.00	14.30	4.000	No	Yes	2.00
211	4.22	0.88	100.00	3.08	0.56	1.70	14.64	0.00	14.64	4.000	No	Yes	2.00
212	4.24	0.89	100.00	3.09	0.56	1.70	14.60	0.00	14.60	4.000	No	Yes	2.00
213	4.26	0.91	100.00	3.10	0.56	1.70	14.90	0.00	14.90	4.000	No	Yes	2.00
214	4.28	0.93	100.00	3.10	0.56	1.70	15.43	0.00	15.43	4.000	No	Yes	2.00
215	4.30	0.97	100.00	3.10	0.56	1.70	15.97	0.00	15.97	4.000	No	Yes	2.00
216	4.32	0.99	100.00	3.09	0.56	1.70	16.54	0.00	16.54	4.000	No	Yes	2.00
217	4.34	1.01	100.00	3.09	0.56	1.70	16.88	0.00	16.88	4.000	No	Yes	2.00
218	4.36	1.02	100.00	3.10	0.56	1.70	16.76	0.00	16.76	4.000	No	Yes	2.00
219	4.38	1.02	100.00	3.10	0.56	1.70	16.94	0.00	16.94	4.000	No	Yes	2.00
220	4.40	1.02	100.00	3.11	0.56	1.70	16.93	0.00	16.93	4.000	No	Yes	2.00
221	4.42	1.03	100.00	3.11	0.56	1.70	17.07	0.00	17.07	4.000	No	Yes	2.00
222	4.44	1.02	100.00	3.12	0.56	1.70	17.18	0.00	17.18	4.000	No	Yes	2.00
223	4.46	1.00	100.00	3.14	0.56	1.70	16.69	0.00	16.69	4.000	No	Yes	2.00
224	4.48	0.95	100.00	3.18	0.56	1.70	15.86	0.00	15.86	4.000	No	Yes	2.00
225	4.50	0.91	100.00	3.20	0.56	1.70	14.83	0.00	14.83	4.000	No	Yes	2.00
226	4.52	0.91	100.00	3.20	0.56	1.70	14.69	0.00	14.69	4.000	No	Yes	2.00
227	4.54	0.91	100.00	3.19	0.56	1.70	15.31	0.00	15.31	4.000	No	Yes	2.00
228	4.56	0.93	100.00	3.17	0.56	1.70	15.06	0.00	15.06	4.000	No	Yes	2.00
229	4.58	0.95	100.00	3.15	0.56	1.70	15.57	0.00	15.57	4.000	No	Yes	2.00
230	4.60	0.99	100.00	3.11	0.56	1.69	16.14	0.00	16.14	4.000	No	Yes	2.00
231	4.62	1.01	100.00	3.09	0.56	1.68	16.72	0.00	16.72	4.000	No	Yes	2.00
232	4.68	1.03	100.00	3.07	0.56	1.67	16.64	0.00	16.64	4.000	No	Yes	2.00
233	4.68	1.03	100.00	3.07	0.56	1.67	16.64	0.00	16.64	4.000	No	Yes	2.00
234	4.68	1.01	100.00	3.08	0.56	1.67	16.53	0.00	16.53	4.000	No	Yes	2.00
235	4.70	0.98	100.00	3.10	0.56	1.67	15.66	0.00	15.66	4.000	No	Yes	2.00
236	4.72	0.94	100.00	3.13	0.56	1.67	15.15	0.00	15.15	4.000	No	Yes	2.00
237	4.74	0.92	100.00	3.15	0.56	1.67	14.74	0.00	14.74	4.000	No	Yes	2.00
238	4.76	0.91	100.00	3.17	0.56	1.67	14.74	0.00	14.74	4.000	No	Yes	2.00
239	4.78	0.90	100.00	3.18	0.57	1.67	14.38	0.00	14.38	4.000	No	Yes	2.00
240	4.80	0.89	100.00	3.20	0.57	1.66	14.31	0.00	14.31	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
241	4.82	0.90	100.00	3.20	0.57	1.66	14.24	0.00	14.24	4.000	No	Yes	2.00
242	4.84	0.90	100.00	3.20	0.57	1.65	14.48	0.00	14.48	4.000	No	Yes	2.00
243	4.86	0.89	100.00	3.19	0.57	1.65	14.24	0.00	14.24	4.000	No	Yes	2.00
244	4.89	0.89	100.00	3.20	0.57	1.65	14.08	0.00	14.08	4.000	No	Yes	2.00
245	4.90	0.89	100.00	3.20	0.57	1.64	14.21	0.00	14.21	4.000	No	Yes	2.00
246	4.93	0.90	100.00	3.19	0.57	1.64	14.16	0.00	14.16	4.000	No	Yes	2.00
247	4.94	0.90	100.00	3.19	0.57	1.64	14.39	0.00	14.39	4.000	No	Yes	2.00
248	4.96	0.89	100.00	3.19	0.57	1.64	14.00	0.00	14.00	4.000	No	Yes	2.00
249	4.98	0.87	100.00	3.20	0.57	1.63	13.75	0.00	13.75	4.000	No	Yes	2.00
250	5.01	0.85	100.00	3.21	0.57	1.63	13.35	0.00	13.35	4.000	No	Yes	2.00
251	5.02	0.83	100.00	3.22	0.57	1.63	13.04	0.00	13.04	4.000	No	Yes	2.00
252	5.04	0.80	100.00	3.24	0.57	1.63	12.55	0.00	12.55	4.000	No	Yes	2.00
253	5.06	0.79	100.00	3.25	0.57	1.63	12.26	0.00	12.26	4.000	No	Yes	2.00
254	5.08	0.79	100.00	3.25	0.57	1.62	12.23	0.00	12.23	4.000	No	Yes	2.00
255	5.10	0.79	100.00	3.24	0.57	1.62	12.31	0.00	12.31	4.000	No	Yes	2.00
256	5.12	0.80	100.00	3.23	0.57	1.62	12.39	0.00	12.39	4.000	No	Yes	2.00
257	5.14	0.82	100.00	3.20	0.57	1.61	12.58	0.00	12.58	4.000	No	Yes	2.00
258	5.16	0.85	100.00	3.17	0.57	1.61	13.15	0.00	13.15	4.000	No	Yes	2.00
259	5.18	0.88	100.00	3.14	0.57	1.60	13.61	0.00	13.61	4.000	No	Yes	2.00
260	5.20	0.90	100.00	3.11	0.57	1.60	13.55	0.00	13.55	4.000	No	Yes	2.00
261	5.22	0.90	100.00	3.10	0.57	1.59	13.98	0.00	13.98	4.000	No	Yes	2.00
262	5.24	0.90	100.00	3.09	0.57	1.59	13.85	0.00	13.85	4.000	No	Yes	2.00
263	5.26	0.89	100.00	3.10	0.57	1.59	13.51	0.00	13.51	4.000	No	Yes	2.00
264	5.28	0.88	100.00	3.11	0.57	1.59	13.44	0.00	13.44	4.000	No	Yes	2.00
265	5.30	0.86	100.00	3.13	0.57	1.58	13.06	0.00	13.06	4.000	No	Yes	2.00
266	5.32	0.84	100.00	3.15	0.57	1.58	12.72	0.00	12.72	4.000	No	Yes	2.00
267	5.34	0.82	100.00	3.17	0.57	1.58	12.20	0.00	12.20	4.000	No	Yes	2.00
268	5.36	0.81	100.00	3.18	0.57	1.58	12.18	0.00	12.18	4.000	No	Yes	2.00
269	5.38	0.83	100.00	3.17	0.57	1.58	12.43	0.00	12.43	4.000	No	Yes	2.00
270	5.40	0.84	100.00	3.16	0.57	1.57	12.75	0.00	12.75	4.000	No	Yes	2.00
271	5.42	0.85	100.00	3.14	0.57	1.57	12.76	0.00	12.76	4.000	No	Yes	2.00
272	5.44	0.83	100.00	3.14	0.57	1.56	12.78	0.00	12.78	4.000	No	Yes	2.00
273	5.46	0.84	100.00	3.10	0.58	1.57	11.85	0.00	11.85	4.000	No	Yes	2.00
274	5.48	0.97	100.00	2.97	0.57	1.56	13.14	0.00	13.14	4.000	No	Yes	2.00
275	5.51	1.14	88.74	2.82	0.56	1.54	17.94	0.00	17.94	4.000	No	Yes	2.00
276	5.52	1.24	83.17	2.75	0.55	1.53	19.30	0.00	19.30	4.000	No	Yes	2.00
277	5.54	1.17	88.16	2.81	0.56	1.53	17.70	0.00	17.70	4.000	No	Yes	2.00
278	5.56	1.02	96.49	2.92	0.57	1.54	14.65	0.00	14.65	4.000	No	Yes	2.00
279	5.58	0.91	100.00	2.99	0.57	1.54	12.99	0.00	12.99	4.000	No	Yes	2.00
280	5.60	0.87	100.00	3.00	0.57	1.54	12.73	0.00	12.73	4.000	No	Yes	2.00
281	5.62	0.86	100.00	2.99	0.57	1.54	12.57	0.00	12.57	4.000	No	Yes	2.00
282	5.64	0.88	100.00	2.98	0.57	1.54	12.51	0.00	12.51	4.000	No	Yes	2.00
283	5.66	0.91	99.55	2.96	0.57	1.53	13.28	0.00	13.28	4.000	No	Yes	2.00
284	5.68	0.97	96.74	2.92	0.57	1.53	13.94	0.00	13.94	4.000	No	Yes	2.00
285	5.70	1.02	94.12	2.89	0.57	1.52	14.70	0.00	14.70	4.000	No	Yes	2.00
286	5.72	1.09	91.76	2.86	0.56	1.52	15.57	0.00	15.57	4.000	No	Yes	2.00
287	5.74	1.18	89.29	2.83	0.56	1.51	16.97	0.00	16.97	4.000	No	Yes	2.00
288	5.76	1.25	87.52	2.81	0.55	1.50	18.35	0.00	18.35	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
289	5.78	1.26	88.52	2.82	0.55	1.50	18.48	0.00	18.48	4.000	No	Yes	2.00
290	5.80	1.30	88.55	2.82	0.56	1.50	17.42	0.00	17.42	4.000	No	Yes	2.00
291	5.82	1.27	91.47	2.86	0.55	1.49	19.99	0.00	19.99	4.000	No	Yes	2.00
292	5.84	1.21	94.69	2.90	0.56	1.49	17.24	0.00	17.24	4.000	No	Yes	2.00
293	5.86	1.07	100.00	2.98	0.56	1.50	15.07	0.00	15.07	4.000	No	Yes	2.00
294	5.88	1.00	100.00	3.03	0.57	1.50	13.98	0.00	13.98	4.000	No	Yes	2.00
295	5.90	0.98	100.00	3.03	0.57	1.50	13.72	0.00	13.72	4.000	No	Yes	2.00
296	5.92	0.98	100.00	3.01	0.57	1.49	13.96	0.00	13.96	4.000	No	Yes	2.00
297	5.94	1.00	100.00	2.97	0.57	1.49	13.96	0.00	13.96	4.000	No	Yes	2.00
298	5.96	1.03	98.66	2.95	0.57	1.49	14.54	0.00	14.54	4.000	No	Yes	2.00
299	5.98	1.08	96.26	2.92	0.56	1.48	15.12	0.00	15.12	4.000	No	Yes	2.00
300	6.00	1.12	95.01	2.90	0.56	1.48	15.92	0.00	15.92	4.000	No	Yes	2.00
301	6.02	1.15	94.81	2.90	0.56	1.48	16.19	0.00	16.19	4.000	No	Yes	2.00
302	6.04	1.18	95.42	2.91	0.56	1.47	16.49	0.00	16.49	4.000	No	Yes	2.00
303	6.06	1.21	96.05	2.91	0.56	1.47	17.11	0.00	17.11	4.000	No	Yes	2.00
304	6.08	1.24	96.77	2.92	0.56	1.46	17.37	0.00	17.37	4.000	No	Yes	2.00
305	6.10	1.28	97.27	2.93	0.55	1.46	17.73	0.00	17.73	4.000	No	Yes	2.00
306	6.12	1.32	97.38	2.93	0.55	1.45	18.44	0.00	18.44	4.000	No	Yes	2.00
307	6.14	1.36	97.14	2.93	0.55	1.45	18.92	0.00	18.92	4.000	No	Yes	2.00
308	6.16	1.39	97.08	2.93	0.55	1.45	19.43	0.00	19.43	4.000	No	Yes	2.00
309	6.18	1.41	97.71	2.93	0.55	1.44	19.58	0.00	19.58	4.000	No	Yes	2.00
310	6.20	1.43	98.25	2.94	0.55	1.44	19.51	0.00	19.51	4.000	No	Yes	2.00
311	6.22	1.45	98.69	2.95	0.55	1.43	20.14	0.00	20.14	4.000	No	Yes	2.00
312	6.24	1.48	98.75	2.95	0.54	1.43	20.41	0.00	20.41	4.000	No	Yes	2.00
313	6.26	1.49	99.26	2.95	0.54	1.43	20.66	0.00	20.66	4.000	No	Yes	2.00
314	6.28	1.51	100.00	2.96	0.54	1.43	20.74	0.00	20.74	4.000	No	Yes	2.00
315	6.30	1.50	100.00	2.98	0.54	1.42	20.85	0.00	20.85	4.000	No	Yes	2.00
316	6.32	1.50	100.00	2.99	0.54	1.42	20.45	0.00	20.45	4.000	No	Yes	2.00
317	6.34	1.47	100.00	3.01	0.54	1.42	20.38	0.00	20.38	4.000	No	Yes	2.00
318	6.36	1.45	100.00	3.03	0.55	1.42	19.86	0.00	19.86	4.000	No	Yes	2.00
319	6.38	1.41	100.00	3.05	0.55	1.42	19.37	0.00	19.37	4.000	No	Yes	2.00
320	6.40	1.38	100.00	3.07	0.55	1.42	18.98	0.00	18.98	4.000	No	Yes	2.00
321	6.42	1.34	100.00	3.09	0.55	1.41	18.33	0.00	18.33	4.000	No	Yes	2.00
322	6.44	1.33	100.00	3.09	0.55	1.41	17.94	0.00	17.94	4.000	No	Yes	2.00
323	6.46	1.32	100.00	3.09	0.55	1.41	18.24	0.00	18.24	4.000	No	Yes	2.00
324	6.48	1.31	100.00	3.08	0.55	1.41	17.85	0.00	17.85	4.000	No	Yes	2.00
325	6.50	1.31	100.00	3.07	0.55	1.41	17.72	0.00	17.72	4.000	No	Yes	2.00
326	6.52	1.30	100.00	3.06	0.55	1.40	17.89	0.00	17.89	4.000	No	Yes	2.00
327	6.54	1.30	100.00	3.05	0.55	1.40	17.66	0.00	17.66	4.000	No	Yes	2.00
328	6.56	1.28	100.00	3.05	0.55	1.40	17.52	0.00	17.52	4.000	No	Yes	2.00
329	6.58	1.26	100.00	3.04	0.56	1.40	17.01	0.00	17.01	4.000	No	Yes	2.00
330	6.60	1.24	100.00	3.04	0.56	1.40	16.89	0.00	16.89	4.000	No	Yes	2.00
331	6.62	1.23	100.00	3.04	0.56	1.40	16.63	0.00	16.63	4.000	No	Yes	2.00
332	6.64	1.24	100.00	3.02	0.56	1.39	16.50	0.00	16.50	4.000	No	Yes	2.00
333	6.66	1.27	100.00	3.00	0.56	1.39	16.90	0.00	16.90	4.000	No	Yes	2.00
334	6.68	1.32	99.64	2.96	0.55	1.39	17.65	0.00	17.65	4.000	No	Yes	2.00
335	6.70	1.37	97.55	2.93	0.55	1.38	18.46	0.00	18.46	4.000	No	Yes	2.00
336	6.72	1.41	96.18	2.91	0.55	1.38	18.67	0.00	18.67	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
337	6.74	1.41	96.21	2.92	0.55	1.38	19.26	0.00	19.26	4.000	No	Yes	2.00
338	6.76	1.37	98.04	2.94	0.55	1.37	18.42	0.00	18.42	4.000	No	Yes	2.00
339	6.78	1.30	100.00	2.97	0.56	1.38	16.94	0.00	16.94	4.000	No	Yes	2.00
340	6.80	1.23	100.00	3.01	0.56	1.38	16.42	0.00	16.42	4.000	No	Yes	2.00
341	6.82	1.17	100.00	3.05	0.56	1.38	15.57	0.00	15.57	4.000	No	Yes	2.00
342	6.84	1.13	100.00	3.09	0.56	1.38	14.92	0.00	14.92	4.000	No	Yes	2.00
343	6.86	1.11	100.00	3.12	0.57	1.37	14.53	0.00	14.53	4.000	No	Yes	2.00
344	6.88	1.12	100.00	3.13	0.56	1.37	14.67	0.00	14.67	4.000	No	Yes	2.00
345	6.90	1.15	100.00	3.12	0.56	1.37	15.11	0.00	15.11	4.000	No	Yes	2.00
346	6.92	1.19	100.00	3.10	0.56	1.36	15.67	0.00	15.67	4.000	No	Yes	2.00
347	6.94	1.23	100.00	3.07	0.56	1.36	16.13	0.00	16.13	4.000	No	Yes	2.00
348	6.96	1.26	100.00	3.04	0.56	1.36	16.56	0.00	16.56	4.000	No	Yes	2.00
349	6.98	1.27	100.00	3.02	0.56	1.36	16.65	0.00	16.65	4.000	No	Yes	2.00
350	7.00	1.27	100.00	3.01	0.56	1.35	16.56	0.00	16.56	4.000	No	Yes	2.00
351	7.02	1.28	100.00	3.00	0.56	1.35	16.62	0.00	16.62	4.000	No	Yes	2.00
352	7.04	1.31	100.00	2.99	0.56	1.35	16.89	0.00	16.89	4.000	No	Yes	2.00
353	7.06	1.34	100.00	2.98	0.55	1.34	17.41	0.00	17.41	4.000	No	Yes	2.00
354	7.08	1.38	100.00	2.97	0.55	1.34	17.74	0.00	17.74	4.000	No	Yes	2.00
355	7.10	1.45	98.86	2.95	0.55	1.34	18.49	0.00	18.49	4.000	No	Yes	2.00
356	7.12	1.55	96.39	2.92	0.55	1.33	19.84	0.00	19.84	4.000	No	Yes	2.00
357	7.14	1.67	93.17	2.88	0.54	1.33	21.48	0.00	21.48	4.000	No	Yes	2.00
358	7.16	1.79	90.03	2.84	0.54	1.32	22.97	0.00	22.97	4.000	No	Yes	2.00
359	7.18	1.89	88.20	2.82	0.53	1.32	24.43	0.00	24.43	4.000	No	Yes	2.00
360	7.20	1.95	87.81	2.81	0.53	1.31	24.95	0.00	24.95	4.000	No	Yes	2.00
361	7.22	1.96	88.86	2.82	0.53	1.31	25.08	0.00	25.08	4.000	No	Yes	2.00
362	7.24	1.93	90.57	2.84	0.53	1.31	24.71	0.00	24.71	4.000	No	Yes	2.00
363	7.26	1.87	93.58	2.88	0.53	1.31	24.02	0.00	24.02	4.000	No	Yes	2.00
364	7.28	1.78	97.85	2.94	0.54	1.31	22.74	0.00	22.74	4.000	No	Yes	2.00
365	7.30	1.68	100.00	2.99	0.54	1.31	21.14	0.00	21.14	4.000	No	Yes	2.00
366	7.32	1.60	100.00	3.04	0.54	1.31	20.34	0.00	20.34	4.000	No	Yes	2.00
367	7.34	1.56	100.00	3.06	0.55	1.31	19.56	0.00	19.56	4.000	No	Yes	2.00
368	7.36	1.56	100.00	3.06	0.55	1.31	19.67	0.00	19.67	4.000	No	Yes	2.00
369	7.38	1.60	100.00	3.03	0.55	1.30	20.01	0.00	20.01	4.000	No	Yes	2.00
370	7.40	1.65	100.00	2.99	0.54	1.30	20.96	0.00	20.96	4.000	No	Yes	2.00
371	7.42	1.71	99.22	2.95	0.54	1.30	21.70	0.00	21.70	4.000	No	Yes	2.00
372	7.44	1.75	96.59	2.92	0.54	1.30	21.87	0.00	21.87	4.000	No	Yes	2.00
373	7.46	1.76	95.03	2.90	0.54	1.29	22.32	0.00	22.32	4.000	No	Yes	2.00
374	7.48	1.78	93.77	2.88	0.54	1.29	22.19	0.00	22.19	4.000	No	Yes	2.00
375	7.50	1.79	93.26	2.88	0.54	1.29	22.44	0.00	22.44	4.000	No	Yes	2.00
376	7.52	1.81	93.12	2.88	0.54	1.29	22.66	0.00	22.66	4.000	No	Yes	2.00
377	7.54	1.84	93.31	2.88	0.54	1.28	23.02	0.00	23.02	4.000	No	Yes	2.00
378	7.56	1.89	93.40	2.88	0.54	1.28	23.33	0.00	23.33	4.000	No	Yes	2.00
379	7.58	1.91	93.85	2.89	0.53	1.28	24.17	0.00	24.17	4.000	No	Yes	2.00
380	7.60	1.91	95.19	2.90	0.53	1.28	23.82	0.00	23.82	4.000	No	Yes	2.00
381	7.62	1.89	96.59	2.92	0.54	1.28	23.23	0.00	23.23	4.000	No	Yes	2.00
382	7.64	1.87	97.74	2.93	0.53	1.27	23.42	0.00	23.42	4.000	No	Yes	2.00
383	7.66	1.86	98.30	2.94	0.54	1.27	22.95	0.00	22.95	4.000	No	Yes	2.00
384	7.68	1.84	98.73	2.95	0.54	1.27	22.62	0.00	22.62	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
385	7.70	1.84	98.88	2.95	0.54	1.27	22.87	0.00	22.87	4.000	No	Yes	2.00
386	7.72	1.84	99.19	2.95	0.54	1.27	22.80	0.00	22.80	4.000	No	Yes	2.00
387	7.74	1.81	100.00	2.97	0.54	1.27	22.31	0.00	22.31	4.000	No	Yes	2.00
388	7.76	1.78	100.00	2.99	0.54	1.26	21.98	0.00	21.98	4.000	No	Yes	2.00
389	7.78	1.76	100.00	2.99	0.54	1.26	21.52	0.00	21.52	4.000	No	Yes	2.00
390	7.81	1.78	100.00	2.98	0.54	1.26	21.57	0.00	21.57	4.000	No	Yes	2.00
391	7.82	1.80	100.00	2.96	0.54	1.26	22.38	0.00	22.38	4.000	No	Yes	2.00
392	7.84	1.80	99.98	2.96	0.54	1.26	22.21	0.00	22.21	4.000	No	Yes	2.00
393	7.86	1.78	100.00	2.97	0.54	1.25	21.75	0.00	21.75	4.000	No	Yes	2.00
394	7.88	1.74	100.00	2.98	0.54	1.25	21.35	0.00	21.35	4.000	No	Yes	2.00
395	7.90	1.73	100.00	2.98	0.54	1.25	20.98	0.00	20.98	4.000	No	Yes	2.00
396	7.92	1.73	100.00	2.98	0.54	1.25	21.22	0.00	21.22	4.000	No	Yes	2.00
397	7.94	1.73	100.00	2.98	0.54	1.25	21.24	0.00	21.24	4.000	No	Yes	2.00
398	7.96	1.68	100.00	2.99	0.54	1.25	20.70	0.00	20.70	4.000	No	Yes	2.00
399	7.99	1.60	100.00	3.03	0.55	1.25	19.63	0.00	19.63	4.000	No	Yes	2.00
400	8.00	1.48	100.00	3.07	0.55	1.25	18.11	0.00	18.11	4.000	No	Yes	2.00
401	8.02	1.35	100.00	3.13	0.56	1.25	16.37	0.00	16.37	4.000	No	Yes	2.00
402	8.04	1.22	100.00	3.20	0.56	1.25	14.75	0.00	14.75	4.000	No	Yes	2.00
403	8.06	1.11	100.00	3.26	0.57	1.25	13.35	0.00	13.35	4.000	No	Yes	2.00
404	8.08	1.02	100.00	3.31	0.57	1.25	12.35	0.00	12.35	4.000	No	Yes	2.00
405	8.10	0.96	100.00	3.34	0.58	1.25	11.70	0.00	11.70	4.000	No	Yes	2.00
406	8.12	0.91	100.00	3.36	0.58	1.25	10.99	0.00	10.99	4.000	No	Yes	2.00
407	8.14	0.86	100.00	3.38	0.58	1.25	10.49	0.00	10.49	4.000	No	Yes	2.00
408	8.16	0.82	100.00	3.40	0.58	1.25	9.61	0.00	9.61	4.000	No	Yes	2.00
409	8.18	0.81	100.00	3.38	0.58	1.25	9.42	0.00	9.42	4.000	No	Yes	2.00
410	8.20	0.83	100.00	3.32	0.58	1.25	9.94	0.00	9.94	4.000	No	Yes	2.00
411	8.22	0.90	100.00	3.23	0.58	1.24	10.51	0.00	10.51	4.000	No	Yes	2.00
412	8.24	1.00	100.00	3.12	0.58	1.24	11.73	0.00	11.73	4.000	No	Yes	2.00
413	8.26	1.14	100.00	3.00	0.57	1.23	13.69	0.00	13.69	4.000	No	Yes	2.00
414	8.28	1.23	97.10	2.93	0.56	1.23	15.31	0.00	15.31	4.000	No	Yes	2.00
415	8.30	1.22	96.95	2.92	0.56	1.23	15.05	0.00	15.05	4.000	No	Yes	2.00
416	8.32	1.12	100.00	2.98	0.57	1.23	13.10	0.00	13.10	4.000	No	Yes	2.00
417	8.34	1.02	100.00	3.04	0.58	1.23	11.63	0.00	11.63	4.000	No	Yes	2.00
418	8.36	0.96	100.00	3.05	0.58	1.23	11.40	0.00	11.40	4.000	No	Yes	2.00
419	8.38	0.96	100.00	3.04	0.58	1.23	11.06	0.00	11.06	4.000	No	Yes	2.00
420	8.40	0.99	100.00	3.00	0.58	1.23	11.31	0.00	11.31	4.000	No	Yes	2.00
421	8.42	1.06	99.25	2.95	0.57	1.22	12.58	0.00	12.58	4.000	No	Yes	2.00
422	8.44	1.11	96.55	2.92	0.57	1.22	13.30	0.00	13.30	4.000	No	Yes	2.00
423	8.46	1.10	97.24	2.93	0.57	1.22	13.10	0.00	13.10	4.000	No	Yes	2.00
424	8.48	1.06	100.00	2.97	0.57	1.22	12.29	0.00	12.29	4.000	No	Yes	2.00
425	8.50	1.01	100.00	3.00	0.58	1.22	11.65	0.00	11.65	4.000	No	Yes	2.00
426	8.52	0.98	100.00	3.03	0.58	1.22	11.48	0.00	11.48	4.000	No	Yes	2.00
427	8.54	1.00	100.00	3.03	0.58	1.22	11.09	0.00	11.09	4.000	No	Yes	2.00
428	8.56	1.04	100.00	3.00	0.57	1.22	12.11	0.00	12.11	4.000	No	Yes	2.00
429	8.58	1.11	100.00	2.97	0.57	1.21	13.13	0.00	13.13	4.000	No	Yes	2.00
430	8.60	1.13	99.49	2.96	0.57	1.21	13.29	0.00	13.29	4.000	No	Yes	2.00
431	8.62	1.11	100.00	2.98	0.57	1.21	12.90	0.00	12.90	4.000	No	Yes	2.00
432	8.64	1.06	100.00	3.02	0.57	1.21	12.20	0.00	12.20	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
433	8.66	1.02	100.00	3.05	0.58	1.21	11.56	0.00	11.56	4.000	No	Yes	2.00
434	8.68	1.00	100.00	3.06	0.58	1.21	11.25	0.00	11.25	4.000	No	Yes	2.00
435	8.70	1.01	100.00	3.04	0.58	1.21	11.44	0.00	11.44	4.000	No	Yes	2.00
436	8.72	1.05	100.00	3.00	0.58	1.20	11.67	0.00	11.67	4.000	No	Yes	2.00
437	8.74	1.13	97.98	2.94	0.57	1.20	12.60	0.00	12.60	4.000	No	Yes	2.00
438	8.76	1.23	92.63	2.87	0.57	1.20	14.08	0.00	14.08	4.000	No	Yes	2.00
439	8.78	1.39	87.77	2.81	0.57	1.20	15.36	0.00	15.36	4.000	No	Yes	2.00
440	8.80	1.51	85.42	2.78	0.56	1.19	18.13	0.00	18.13	4.000	No	Yes	2.00
441	8.82	1.59	85.25	2.78	0.56	1.19	18.11	0.00	18.11	4.000	No	Yes	2.00
442	8.85	1.59	87.15	2.80	0.56	1.19	18.00	0.00	18.00	4.000	No	Yes	2.00
443	8.86	1.61	88.48	2.82	0.56	1.19	17.97	0.00	17.97	4.000	No	Yes	2.00
444	8.88	1.61	90.77	2.85	0.55	1.19	18.51	0.00	18.51	4.000	No	Yes	2.00
445	8.90	1.61	93.44	2.88	0.55	1.18	18.11	0.00	18.11	4.000	No	Yes	2.00
446	8.92	1.62	95.34	2.90	0.55	1.18	17.87	0.00	17.87	4.000	No	Yes	2.00
447	8.94	1.67	94.43	2.89	0.55	1.18	18.73	0.00	18.73	4.000	No	Yes	2.00
448	8.96	1.72	93.17	2.88	0.55	1.18	19.86	0.00	19.86	4.000	No	Yes	2.00
449	8.98	1.74	93.10	2.88	0.55	1.18	19.46	0.00	19.46	4.000	No	Yes	2.00
450	9.00	1.71	94.87	2.90	0.55	1.17	19.46	0.00	19.46	4.000	No	Yes	2.00
451	9.02	1.69	96.05	2.91	0.55	1.17	18.81	0.00	18.81	4.000	No	Yes	2.00
452	9.05	1.67	96.84	2.92	0.55	1.17	18.72	0.00	18.72	4.000	No	Yes	2.00
453	9.07	1.66	97.64	2.93	0.55	1.17	18.91	0.00	18.91	4.000	No	Yes	2.00
454	9.08	1.62	100.00	2.97	0.55	1.17	18.44	0.00	18.44	4.000	No	Yes	2.00
455	9.10	1.54	100.00	3.01	0.56	1.17	17.26	0.00	17.26	4.000	No	Yes	2.00
456	9.12	1.45	100.00	3.07	0.56	1.17	16.21	0.00	16.21	4.000	No	Yes	2.00
457	9.15	1.37	100.00	3.11	0.56	1.17	15.38	0.00	15.38	4.000	No	Yes	2.00
458	9.16	1.30	100.00	3.16	0.57	1.17	14.55	0.00	14.55	4.000	No	Yes	2.00
459	9.18	1.23	100.00	3.20	0.57	1.17	13.62	0.00	13.62	4.000	No	Yes	2.00
460	9.20	1.17	100.00	3.24	0.57	1.17	13.01	0.00	13.01	4.000	No	Yes	2.00
461	9.22	1.14	100.00	3.25	0.57	1.17	12.72	0.00	12.72	4.000	No	Yes	2.00
462	9.24	1.14	100.00	3.24	0.57	1.17	12.48	0.00	12.48	4.000	No	Yes	2.00
463	9.26	1.13	100.00	3.23	0.57	1.16	12.70	0.00	12.70	4.000	No	Yes	2.00
464	9.29	1.12	100.00	3.21	0.57	1.16	12.40	0.00	12.40	4.000	No	Yes	2.00
465	9.31	1.11	100.00	3.19	0.57	1.16	12.32	0.00	12.32	4.000	No	Yes	2.00
466	9.32	1.11	100.00	3.17	0.57	1.16	12.33	0.00	12.33	4.000	No	Yes	2.00
467	9.34	1.11	100.00	3.16	0.57	1.16	12.28	0.00	12.28	4.000	No	Yes	2.00
468	9.36	1.11	100.00	3.15	0.57	1.16	12.29	0.00	12.29	4.000	No	Yes	2.00
469	9.38	1.12	100.00	3.15	0.57	1.16	12.35	0.00	12.35	4.000	No	Yes	2.00
470	9.40	1.13	100.00	3.16	0.57	1.15	12.54	0.00	12.54	4.000	No	Yes	2.00
471	9.42	1.13	100.00	3.16	0.57	1.15	12.33	0.00	12.33	4.000	No	Yes	2.00
472	9.44	1.13	100.00	3.16	0.57	1.15	12.53	0.00	12.53	4.000	No	Yes	2.00
473	9.46	1.15	100.00	3.16	0.57	1.15	12.54	0.00	12.54	4.000	No	Yes	2.00
474	9.48	1.16	100.00	3.16	0.57	1.15	12.68	0.00	12.68	4.000	No	Yes	2.00
475	9.50	1.18	100.00	3.15	0.57	1.15	13.00	0.00	13.00	4.000	No	Yes	2.00
476	9.52	1.18	100.00	3.16	0.57	1.15	13.17	0.00	13.17	4.000	No	Yes	2.00
477	9.54	1.16	100.00	3.18	0.57	1.14	12.70	0.00	12.70	4.000	No	Yes	2.00
478	9.56	1.13	100.00	3.21	0.57	1.14	12.35	0.00	12.35	4.000	No	Yes	2.00
479	9.58	1.10	100.00	3.24	0.57	1.14	12.12	0.00	12.12	4.000	No	Yes	2.00
480	9.60	1.07	100.00	3.26	0.58	1.14	11.63	0.00	11.63	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
481	9.62	1.03	100.00	3.29	0.58	1.14	11.17	0.00	11.17	4.000	No	Yes	2.00
482	9.64	1.02	100.00	3.31	0.58	1.14	10.94	0.00	10.94	4.000	No	Yes	2.00
483	9.66	1.04	100.00	3.29	0.58	1.14	11.14	0.00	11.14	4.000	No	Yes	2.00
484	9.68	1.07	100.00	3.26	0.58	1.14	11.80	0.00	11.80	4.000	No	Yes	2.00
485	9.70	1.10	100.00	3.23	0.58	1.13	11.79	0.00	11.79	4.000	No	Yes	2.00
486	9.72	1.12	100.00	3.21	0.57	1.13	12.14	0.00	12.14	4.000	No	Yes	2.00
487	9.74	1.14	100.00	3.18	0.57	1.13	12.39	0.00	12.39	4.000	No	Yes	2.00
488	9.76	1.15	100.00	3.16	0.57	1.13	12.43	0.00	12.43	4.000	No	Yes	2.00
489	9.78	1.19	100.00	3.12	0.57	1.13	12.46	0.00	12.46	4.000	No	Yes	2.00
490	9.80	1.21	100.00	3.10	0.57	1.13	13.53	0.00	13.53	4.000	No	Yes	2.00
491	9.82	1.23	100.00	3.10	0.57	1.13	13.23	0.00	13.23	4.000	No	Yes	2.00
492	9.85	1.22	100.00	3.12	0.57	1.12	13.00	0.00	13.00	4.000	No	Yes	2.00
493	9.86	1.22	100.00	3.13	0.57	1.12	13.28	0.00	13.28	4.000	No	Yes	2.00
494	9.88	1.22	100.00	3.15	0.57	1.12	13.14	0.00	13.14	4.000	No	Yes	2.00
495	9.90	1.20	100.00	3.17	0.57	1.12	12.94	0.00	12.94	4.000	No	Yes	2.00
496	9.92	1.20	100.00	3.19	0.57	1.12	12.77	0.00	12.77	4.000	No	Yes	2.00
497	9.94	1.19	100.00	3.20	0.57	1.12	12.86	0.00	12.86	4.000	No	Yes	2.00
498	9.96	1.21	100.00	3.20	0.57	1.12	12.86	0.00	12.86	4.000	No	Yes	2.00
499	9.98	1.22	100.00	3.19	0.57	1.12	13.10	0.00	13.10	4.000	No	Yes	2.00
500	10.00	1.23	100.00	3.18	0.57	1.11	13.24	0.00	13.24	4.000	No	Yes	2.00
501	10.02	1.25	100.00	3.16	0.57	1.11	13.32	0.00	13.32	4.000	No	Yes	2.00
502	10.04	1.25	100.00	3.16	0.57	1.11	13.59	0.00	13.59	4.000	No	Yes	2.00
503	10.06	1.25	100.00	3.16	0.57	1.11	13.23	0.00	13.23	4.000	No	Yes	2.00
504	10.08	1.25	100.00	3.17	0.57	1.11	13.29	0.00	13.29	4.000	No	Yes	2.00
505	10.10	1.24	100.00	3.17	0.57	1.11	13.30	0.00	13.30	4.000	No	Yes	2.00
506	10.12	1.23	100.00	3.18	0.57	1.11	13.13	0.00	13.13	4.000	No	Yes	2.00
507	10.14	1.23	100.00	3.19	0.57	1.11	12.91	0.00	12.91	4.000	No	Yes	2.00
508	10.16	1.23	100.00	3.19	0.57	1.10	13.01	0.00	13.01	4.000	No	Yes	2.00
509	10.18	1.23	100.00	3.19	0.57	1.10	13.12	0.00	13.12	4.000	No	Yes	2.00
510	10.20	1.23	100.00	3.19	0.57	1.10	12.95	0.00	12.95	4.000	No	Yes	2.00
511	10.22	1.22	100.00	3.20	0.57	1.10	12.93	0.00	12.93	4.000	No	Yes	2.00
512	10.24	1.22	100.00	3.20	0.57	1.10	12.84	0.00	12.84	4.000	No	Yes	2.00
513	10.26	1.24	100.00	3.19	0.57	1.10	12.95	0.00	12.95	4.000	No	Yes	2.00
514	10.28	1.29	100.00	3.16	0.57	1.10	13.53	0.00	13.53	4.000	No	Yes	2.00
515	10.30	1.34	100.00	3.14	0.57	1.09	14.19	0.00	14.19	4.000	No	Yes	2.00
516	10.32	1.37	100.00	3.13	0.56	1.09	14.65	0.00	14.65	4.000	No	Yes	2.00
517	10.34	1.36	100.00	3.13	0.57	1.09	14.23	0.00	14.23	4.000	No	Yes	2.00
518	10.36	1.33	100.00	3.15	0.57	1.09	14.01	0.00	14.01	4.000	No	Yes	2.00
519	10.38	1.32	100.00	3.16	0.57	1.09	13.77	0.00	13.77	4.000	No	Yes	2.00
520	10.40	1.32	100.00	3.17	0.57	1.09	13.75	0.00	13.75	4.000	No	Yes	2.00
521	10.42	1.33	100.00	3.16	0.57	1.09	13.88	0.00	13.88	4.000	No	Yes	2.00
522	10.44	1.37	100.00	3.14	0.57	1.09	14.21	0.00	14.21	4.000	No	Yes	2.00
523	10.46	1.42	100.00	3.11	0.56	1.09	14.77	0.00	14.77	4.000	No	Yes	2.00
524	10.48	1.48	100.00	3.08	0.56	1.08	15.37	0.00	15.37	4.000	No	Yes	2.00
525	10.50	1.54	100.00	3.05	0.56	1.08	16.15	0.00	16.15	4.000	No	Yes	2.00
526	10.52	1.58	100.00	3.03	0.56	1.08	16.61	0.00	16.61	4.000	No	Yes	2.00
527	10.54	1.59	100.00	3.03	0.56	1.08	16.64	0.00	16.64	4.000	No	Yes	2.00
528	10.56	1.58	100.00	3.05	0.56	1.08	16.37	0.00	16.37	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
529	10.58	1.58	100.00	3.05	0.56	1.08	16.20	0.00	16.20	4.000	No	Yes	2.00
530	10.60	1.60	100.00	3.05	0.56	1.08	16.63	0.00	16.63	4.000	No	Yes	2.00
531	10.62	1.61	100.00	3.05	0.56	1.07	16.89	0.00	16.89	4.000	No	Yes	2.00
532	10.64	1.62	100.00	3.06	0.56	1.07	16.69	0.00	16.69	4.000	No	Yes	2.00
533	10.66	1.63	100.00	3.07	0.56	1.07	16.87	0.00	16.87	4.000	No	Yes	2.00
534	10.68	1.64	100.00	3.08	0.56	1.07	16.95	0.00	16.95	4.000	No	Yes	2.00
535	10.70	1.63	100.00	3.09	0.56	1.07	16.95	0.00	16.95	4.000	No	Yes	2.00
536	10.72	1.61	100.00	3.11	0.56	1.07	16.46	0.00	16.46	4.000	No	Yes	2.00
537	10.74	1.59	100.00	3.13	0.56	1.07	16.32	0.00	16.32	4.000	No	Yes	2.00
538	10.77	1.59	100.00	3.13	0.56	1.07	16.29	0.00	16.29	4.000	No	Yes	2.00
539	10.78	1.58	100.00	3.13	0.56	1.07	16.42	0.00	16.42	4.000	No	Yes	2.00
540	10.80	1.56	100.00	3.14	0.56	1.06	16.11	0.00	16.11	4.000	No	Yes	2.00
541	10.82	1.53	100.00	3.16	0.56	1.06	15.67	0.00	15.67	4.000	No	Yes	2.00
542	10.84	1.50	100.00	3.17	0.56	1.06	15.31	0.00	15.31	4.000	No	Yes	2.00
543	10.86	1.48	100.00	3.18	0.56	1.06	15.07	0.00	15.07	4.000	No	Yes	2.00
544	10.88	1.47	100.00	3.18	0.56	1.06	15.17	0.00	15.17	4.000	No	Yes	2.00
545	10.91	1.45	100.00	3.18	0.56	1.06	14.97	0.00	14.97	4.000	No	Yes	2.00
546	10.92	1.42	100.00	3.20	0.57	1.06	14.46	0.00	14.46	4.000	No	Yes	2.00
547	10.95	1.38	100.00	3.22	0.57	1.06	14.10	0.00	14.10	4.000	No	Yes	2.00
548	10.96	1.35	100.00	3.23	0.57	1.06	13.48	0.00	13.48	4.000	No	Yes	2.00
549	10.98	1.33	100.00	3.23	0.57	1.06	13.63	0.00	13.63	4.000	No	Yes	2.00
550	11.00	1.32	100.00	3.23	0.57	1.05	13.42	0.00	13.42	4.000	No	Yes	2.00
551	11.02	1.30	100.00	3.24	0.57	1.05	13.18	0.00	13.18	4.000	No	Yes	2.00
552	11.04	1.29	100.00	3.24	0.57	1.05	12.97	0.00	12.97	4.000	No	Yes	2.00
553	11.06	1.29	100.00	3.23	0.57	1.05	12.95	0.00	12.95	4.000	No	Yes	2.00
554	11.09	1.28	100.00	3.23	0.57	1.05	13.04	0.00	13.04	4.000	No	Yes	2.00
555	11.10	1.28	100.00	3.23	0.57	1.05	12.89	0.00	12.89	4.000	No	Yes	2.00
556	11.13	1.29	100.00	3.23	0.57	1.05	12.81	0.00	12.81	4.000	No	Yes	2.00
557	11.15	1.30	100.00	3.22	0.57	1.05	13.15	0.00	13.15	4.000	No	Yes	2.00
558	11.16	1.31	100.00	3.21	0.57	1.05	13.12	0.00	13.12	4.000	No	Yes	2.00
559	11.18	1.32	100.00	3.21	0.57	1.04	13.20	0.00	13.20	4.000	No	Yes	2.00
560	11.20	1.34	100.00	3.19	0.57	1.04	13.40	0.00	13.40	4.000	No	Yes	2.00
561	11.22	1.36	100.00	3.18	0.57	1.04	13.77	0.00	13.77	4.000	No	Yes	2.00
562	11.24	1.38	100.00	3.18	0.57	1.04	13.73	0.00	13.73	4.000	No	Yes	2.00
563	11.26	1.40	100.00	3.16	0.57	1.04	13.88	0.00	13.88	4.000	No	Yes	2.00
564	11.28	1.41	100.00	3.15	0.57	1.04	14.34	0.00	14.34	4.000	No	Yes	2.00
565	11.30	1.41	100.00	3.15	0.57	1.04	14.16	0.00	14.16	4.000	No	Yes	2.00
566	11.32	1.40	100.00	3.16	0.57	1.04	13.88	0.00	13.88	4.000	No	Yes	2.00
567	11.34	1.40	100.00	3.16	0.57	1.04	13.98	0.00	13.98	4.000	No	Yes	2.00
568	11.36	1.39	100.00	3.15	0.57	1.03	13.90	0.00	13.90	4.000	No	Yes	2.00
569	11.38	1.37	100.00	3.16	0.57	1.03	13.60	0.00	13.60	4.000	No	Yes	2.00
570	11.40	1.34	100.00	3.17	0.57	1.03	13.28	0.00	13.28	4.000	No	Yes	2.00
571	11.42	1.33	100.00	3.18	0.57	1.03	13.02	0.00	13.02	4.000	No	Yes	2.00
572	11.44	1.35	100.00	3.16	0.57	1.03	13.22	0.00	13.22	4.000	No	Yes	2.00
573	11.46	1.38	100.00	3.14	0.57	1.03	14.00	0.00	14.00	4.000	No	Yes	2.00
574	11.48	1.40	100.00	3.12	0.57	1.03	13.93	0.00	13.93	4.000	No	Yes	2.00
575	11.50	1.39	100.00	3.12	0.57	1.03	13.70	0.00	13.70	4.000	No	Yes	2.00
576	11.52	1.37	100.00	3.12	0.57	1.03	13.62	0.00	13.62	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
577	11.54	1.36	100.00	3.13	0.57	1.03	13.34	0.00	13.34	4.000	No	Yes	2.00
578	11.56	1.33	100.00	3.14	0.57	1.02	13.17	0.00	13.17	4.000	No	Yes	2.00
579	11.58	1.30	100.00	3.15	0.57	1.02	12.89	0.00	12.89	4.000	No	Yes	2.00
580	11.60	1.28	100.00	3.17	0.57	1.02	12.48	0.00	12.48	4.000	No	Yes	2.00
581	11.62	1.26	100.00	3.18	0.57	1.02	12.37	0.00	12.37	4.000	No	Yes	2.00
582	11.64	1.25	100.00	3.19	0.57	1.02	12.27	0.00	12.27	4.000	No	Yes	2.00
583	11.66	1.25	100.00	3.20	0.57	1.02	12.14	0.00	12.14	4.000	No	Yes	2.00
584	11.68	1.24	100.00	3.21	0.57	1.02	12.27	0.00	12.27	4.000	No	Yes	2.00
585	11.70	1.23	100.00	3.22	0.57	1.02	12.00	0.00	12.00	4.000	No	Yes	2.00
586	11.72	1.20	100.00	3.23	0.58	1.02	11.66	0.00	11.66	4.000	No	Yes	2.00
587	11.74	1.16	100.00	3.24	0.58	1.02	11.44	0.00	11.44	4.000	No	Yes	2.00
588	11.76	1.17	100.00	3.23	0.58	1.02	10.71	0.00	10.71	4.000	No	Yes	2.00
589	11.78	1.18	100.00	3.22	0.58	1.01	11.83	0.00	11.83	4.000	No	Yes	2.00
590	11.80	1.19	100.00	3.21	0.58	1.01	11.65	0.00	11.65	4.000	No	Yes	2.00
591	11.82	1.16	100.00	3.24	0.58	1.01	11.22	0.00	11.22	4.000	No	Yes	2.00
592	11.84	1.13	100.00	3.25	0.58	1.01	10.88	0.00	10.88	4.000	No	Yes	2.00
593	11.86	1.10	100.00	3.28	0.58	1.01	10.73	0.00	10.73	4.000	No	Yes	2.00
594	11.88	1.06	100.00	3.30	0.58	1.01	10.23	0.00	10.23	4.000	No	Yes	2.00
595	11.90	1.02	100.00	3.34	0.58	1.01	9.80	0.00	9.80	4.000	No	Yes	2.00
596	11.92	0.97	100.00	3.38	0.58	1.01	9.42	0.00	9.42	4.000	No	Yes	2.00
597	11.94	0.91	100.00	3.42	0.59	1.01	8.62	0.00	8.62	4.000	No	Yes	2.00
598	11.96	0.84	100.00	3.47	0.59	1.01	8.06	0.00	8.06	4.000	No	Yes	2.00
599	11.98	0.77	100.00	3.54	0.59	1.00	7.40	0.00	7.40	4.000	No	Yes	2.00
600	12.00	0.71	100.00	3.61	0.60	1.00	6.61	0.00	6.61	4.000	No	Yes	2.00
601	12.02	0.65	100.00	3.67	0.60	1.00	6.10	0.00	6.10	4.000	No	Yes	2.00
602	12.04	0.61	100.00	3.71	0.60	1.00	5.75	0.00	5.75	4.000	No	Yes	2.00
603	12.06	0.57	100.00	3.74	0.60	1.00	5.26	0.00	5.26	4.000	No	Yes	2.00
604	12.08	0.55	100.00	3.75	0.60	1.00	5.00	0.00	5.00	4.000	No	Yes	2.00
605	12.10	0.53	100.00	3.73	0.60	1.00	4.93	0.00	4.93	4.000	No	Yes	2.00
606	12.12	0.54	100.00	3.66	0.60	1.00	4.90	0.00	4.90	4.000	No	Yes	2.00
607	12.14	0.60	100.00	3.53	0.60	1.00	5.26	0.00	5.26	4.000	No	Yes	2.00
608	12.16	0.70	100.00	3.37	0.60	1.00	6.40	0.00	6.40	4.000	No	Yes	2.00
609	12.18	0.83	100.00	3.21	0.59	1.00	7.80	0.00	7.80	4.000	No	Yes	2.00
610	12.20	0.94	100.00	3.12	0.59	1.00	9.17	0.00	9.17	4.000	No	Yes	2.00
611	12.22	1.03	100.00	3.06	0.58	1.00	9.53	0.00	9.53	4.000	No	Yes	2.00
612	12.24	1.14	100.00	3.01	0.58	0.99	10.68	0.00	10.68	4.000	No	Yes	2.00
613	12.27	1.27	99.62	2.96	0.57	0.99	12.26	0.00	12.26	4.000	No	Yes	2.00
614	12.28	1.35	98.32	2.94	0.57	0.99	13.30	0.00	13.30	4.000	No	Yes	2.00
615	12.30	1.31	100.00	2.99	0.57	0.99	13.18	0.00	13.18	4.000	No	Yes	2.00
616	12.32	1.14	100.00	3.10	0.58	0.99	10.96	0.00	10.96	4.000	No	Yes	2.00
617	12.34	0.91	100.00	3.26	0.59	0.99	8.51	0.00	8.51	4.000	No	Yes	2.00
618	12.36	0.74	100.00	3.39	0.60	0.99	6.42	0.00	6.42	4.000	No	Yes	2.00
619	12.38	0.66	100.00	3.46	0.60	0.99	5.90	0.00	5.90	4.000	No	Yes	2.00
620	12.40	0.63	100.00	3.48	0.60	0.99	6.08	0.00	6.08	4.000	No	Yes	2.00
621	12.42	0.63	100.00	3.48	0.60	0.99	5.72	0.00	5.72	4.000	No	Yes	2.00
622	12.44	0.61	100.00	3.52	0.60	0.99	5.83	0.00	5.83	4.000	No	Yes	2.00
623	12.46	0.59	100.00	3.55	0.60	0.99	5.38	0.00	5.38	4.000	No	Yes	2.00
624	12.48	0.56	100.00	3.60	0.60	0.98	4.97	0.00	4.97	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
625	12.50	0.55	100.00	3.59	0.60	0.98	4.92	0.00	4.92	4.000	No	Yes	2.00
626	12.52	0.58	100.00	3.54	0.60	0.98	5.24	0.00	5.24	4.000	No	Yes	2.00
627	12.54	0.61	100.00	3.49	0.60	0.98	5.65	0.00	5.65	4.000	No	Yes	2.00
628	12.56	0.63	100.00	3.45	0.60	0.98	5.62	0.00	5.62	4.000	No	Yes	2.00
629	12.58	0.64	100.00	3.42	0.60	0.98	5.83	0.00	5.83	4.000	No	Yes	2.00
630	12.60	0.69	100.00	3.37	0.60	0.98	6.09	0.00	6.09	4.000	No	Yes	2.00
631	12.62	0.74	100.00	3.31	0.60	0.98	6.77	0.00	6.77	4.000	No	Yes	2.00
632	12.64	0.80	100.00	3.26	0.59	0.98	7.38	0.00	7.38	4.000	No	Yes	2.00
633	12.66	0.84	100.00	3.23	0.59	0.98	7.71	0.00	7.71	4.000	No	Yes	2.00
634	12.68	0.87	100.00	3.22	0.59	0.98	8.09	0.00	8.09	4.000	No	Yes	2.00
635	12.70	0.91	100.00	3.20	0.59	0.98	8.27	0.00	8.27	4.000	No	Yes	2.00
636	12.72	0.94	100.00	3.18	0.59	0.98	8.67	0.00	8.67	4.000	No	Yes	2.00
637	12.74	0.99	100.00	3.16	0.59	0.98	9.09	0.00	9.09	4.000	No	Yes	2.00
638	12.76	1.04	100.00	3.14	0.58	0.97	9.46	0.00	9.46	4.000	No	Yes	2.00
639	12.78	1.07	100.00	3.14	0.58	0.97	10.00	0.00	10.00	4.000	No	Yes	2.00
640	12.80	1.07	100.00	3.16	0.58	0.97	9.77	0.00	9.77	4.000	No	Yes	2.00
641	12.82	1.05	100.00	3.20	0.58	0.97	9.62	0.00	9.62	4.000	No	Yes	2.00
642	12.84	1.03	100.00	3.23	0.58	0.97	9.37	0.00	9.37	4.000	No	Yes	2.00
643	12.86	1.01	100.00	3.27	0.59	0.97	9.23	0.00	9.23	4.000	No	Yes	2.00
644	12.88	0.97	100.00	3.32	0.59	0.97	8.89	0.00	8.89	4.000	No	Yes	2.00
645	12.90	0.95	100.00	3.35	0.59	0.97	8.43	0.00	8.43	4.000	No	Yes	2.00
646	12.94	0.94	100.00	3.37	0.59	0.97	8.46	0.00	8.46	4.000	No	Yes	2.00
647	12.94	0.93	100.00	3.37	0.59	0.97	8.57	0.00	8.57	4.000	No	Yes	2.00
648	12.96	0.92	100.00	3.39	0.59	0.97	8.25	0.00	8.25	4.000	No	Yes	2.00
649	12.99	0.89	100.00	3.41	0.59	0.97	7.93	0.00	7.93	4.000	No	Yes	2.00
650	13.00	0.86	100.00	3.43	0.59	0.96	7.70	0.00	7.70	4.000	No	Yes	2.00
651	13.03	0.83	100.00	3.45	0.59	0.96	7.53	0.00	7.53	4.000	No	Yes	2.00
652	13.04	0.82	100.00	3.46	0.59	0.96	7.12	0.00	7.12	4.000	No	Yes	2.00
653	13.06	0.80	100.00	3.47	0.59	0.96	7.14	0.00	7.14	4.000	No	Yes	2.00
654	13.08	0.81	100.00	3.45	0.59	0.96	7.06	0.00	7.06	4.000	No	Yes	2.00
655	13.10	0.83	100.00	3.43	0.59	0.96	7.39	0.00	7.39	4.000	No	Yes	2.00
656	13.13	0.86	100.00	3.38	0.59	0.96	7.49	0.00	7.49	4.000	No	Yes	2.00
657	13.14	0.91	100.00	3.32	0.59	0.96	8.05	0.00	8.05	4.000	No	Yes	2.00
658	13.16	0.98	100.00	3.24	0.59	0.96	8.58	0.00	8.58	4.000	No	Yes	2.00
659	13.18	1.04	100.00	3.18	0.58	0.96	9.43	0.00	9.43	4.000	No	Yes	2.00
660	13.20	1.11	100.00	3.12	0.58	0.96	9.88	0.00	9.88	4.000	No	Yes	2.00
661	13.22	1.16	100.00	3.09	0.58	0.96	10.59	0.00	10.59	4.000	No	Yes	2.00
662	13.24	1.18	100.00	3.10	0.58	0.96	10.67	0.00	10.67	4.000	No	Yes	2.00
663	13.26	1.17	100.00	3.13	0.58	0.96	10.48	0.00	10.48	4.000	No	Yes	2.00
664	13.28	1.14	100.00	3.18	0.58	0.95	10.29	0.00	10.29	4.000	No	Yes	2.00
665	13.30	1.12	100.00	3.21	0.58	0.95	9.91	0.00	9.91	4.000	No	Yes	2.00
666	13.32	1.11	100.00	3.24	0.58	0.95	9.83	0.00	9.83	4.000	No	Yes	2.00
667	13.34	1.10	100.00	3.25	0.58	0.95	9.91	0.00	9.91	4.000	No	Yes	2.00
668	13.36	1.10	100.00	3.25	0.58	0.95	9.75	0.00	9.75	4.000	No	Yes	2.00
669	13.38	1.09	100.00	3.26	0.58	0.95	9.70	0.00	9.70	4.000	No	Yes	2.00
670	13.40	1.08	100.00	3.26	0.58	0.95	9.73	0.00	9.73	4.000	No	Yes	2.00
671	13.42	1.06	100.00	3.27	0.58	0.95	9.37	0.00	9.37	4.000	No	Yes	2.00
672	13.44	1.04	100.00	3.28	0.59	0.95	9.17	0.00	9.17	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
673	13.46	1.03	100.00	3.29	0.59	0.95	9.07	0.00	9.07	4.000	No	Yes	2.00
674	13.48	1.03	100.00	3.28	0.59	0.95	9.11	0.00	9.11	4.000	No	Yes	2.00
675	13.50	1.03	100.00	3.28	0.59	0.95	9.23	0.00	9.23	4.000	No	Yes	2.00
676	13.52	1.02	100.00	3.28	0.59	0.95	9.05	0.00	9.05	4.000	No	Yes	2.00
677	13.54	1.00	100.00	3.30	0.59	0.94	8.82	0.00	8.82	4.000	No	Yes	2.00
678	13.56	0.99	100.00	3.31	0.59	0.94	8.68	0.00	8.68	4.000	No	Yes	2.00
679	13.58	0.99	100.00	3.31	0.59	0.94	8.63	0.00	8.63	4.000	No	Yes	2.00
680	13.60	1.01	100.00	3.30	0.59	0.94	8.86	0.00	8.86	4.000	No	Yes	2.00
681	13.62	1.04	100.00	3.27	0.59	0.94	9.07	0.00	9.07	4.000	No	Yes	2.00
682	13.64	1.07	100.00	3.25	0.58	0.94	9.48	0.00	9.48	4.000	No	Yes	2.00
683	13.66	1.09	100.00	3.23	0.58	0.94	9.64	0.00	9.64	4.000	No	Yes	2.00
684	13.68	1.10	100.00	3.22	0.58	0.94	9.70	0.00	9.70	4.000	No	Yes	2.00
685	13.70	1.10	100.00	3.23	0.58	0.94	9.71	0.00	9.71	4.000	No	Yes	2.00
686	13.72	1.10	100.00	3.24	0.58	0.94	9.64	0.00	9.64	4.000	No	Yes	2.00
687	13.74	1.11	100.00	3.24	0.58	0.94	9.76	0.00	9.76	4.000	No	Yes	2.00
688	13.76	1.12	100.00	3.25	0.58	0.94	9.84	0.00	9.84	4.000	No	Yes	2.00
689	13.79	1.11	100.00	3.26	0.58	0.94	9.78	0.00	9.78	4.000	No	Yes	2.00
690	13.80	1.11	100.00	3.27	0.58	0.94	9.67	0.00	9.67	4.000	No	Yes	2.00
691	13.82	1.11	100.00	3.28	0.58	0.93	9.62	0.00	9.62	4.000	No	Yes	2.00
692	13.85	1.11	100.00	3.29	0.58	0.93	9.76	0.00	9.76	4.000	No	Yes	2.00
693	13.86	1.12	100.00	3.28	0.58	0.93	9.73	0.00	9.73	4.000	No	Yes	2.00
694	13.88	1.14	100.00	3.28	0.58	0.93	9.98	0.00	9.98	4.000	No	Yes	2.00
695	13.90	1.14	100.00	3.28	0.58	0.93	10.21	0.00	10.21	4.000	No	Yes	2.00
696	13.92	1.13	100.00	3.30	0.58	0.93	9.66	0.00	9.66	4.000	No	Yes	2.00
697	13.94	1.09	100.00	3.33	0.58	0.93	9.58	0.00	9.58	4.000	No	Yes	2.00
698	13.96	1.07	100.00	3.34	0.58	0.93	9.33	0.00	9.33	4.000	No	Yes	2.00
699	13.98	1.05	100.00	3.35	0.59	0.93	8.98	0.00	8.98	4.000	No	Yes	2.00
700	14.00	1.05	100.00	3.35	0.59	0.93	9.03	0.00	9.03	4.000	No	Yes	2.00
701	14.02	1.07	100.00	3.32	0.59	0.93	9.21	0.00	9.21	4.000	No	Yes	2.00
702	14.04	1.09	100.00	3.30	0.58	0.93	9.46	0.00	9.46	4.000	No	Yes	2.00
703	14.06	1.13	100.00	3.27	0.58	0.93	9.65	0.00	9.65	4.000	No	Yes	2.00
704	14.08	1.15	100.00	3.24	0.58	0.92	10.11	0.00	10.11	4.000	No	Yes	2.00
705	14.10	1.17	100.00	3.22	0.58	0.92	10.19	0.00	10.19	4.000	No	Yes	2.00
706	14.12	1.18	100.00	3.21	0.58	0.92	10.14	0.00	10.14	4.000	No	Yes	2.00
707	14.14	1.20	100.00	3.20	0.58	0.92	10.36	0.00	10.36	4.000	No	Yes	2.00
708	14.16	1.23	100.00	3.19	0.58	0.92	10.74	0.00	10.74	4.000	No	Yes	2.00
709	14.18	1.26	100.00	3.18	0.58	0.92	10.88	0.00	10.88	4.000	No	Yes	2.00
710	14.20	1.28	100.00	3.16	0.58	0.92	11.11	0.00	11.11	4.000	No	Yes	2.00
711	14.22	1.32	100.00	3.14	0.58	0.92	11.40	0.00	11.40	4.000	No	Yes	2.00
712	14.24	1.35	100.00	3.13	0.58	0.92	11.88	0.00	11.88	4.000	No	Yes	2.00
713	14.26	1.39	100.00	3.12	0.57	0.92	11.95	0.00	11.95	4.000	No	Yes	2.00
714	14.28	1.42	100.00	3.12	0.57	0.92	12.44	0.00	12.44	4.000	No	Yes	2.00
715	14.30	1.45	100.00	3.12	0.57	0.92	12.60	0.00	12.60	4.000	No	Yes	2.00
716	14.32	1.46	100.00	3.13	0.57	0.92	12.78	0.00	12.78	4.000	No	Yes	2.00
717	14.34	1.46	100.00	3.15	0.57	0.92	12.77	0.00	12.77	4.000	No	Yes	2.00
718	14.36	1.46	100.00	3.17	0.57	0.92	12.50	0.00	12.50	4.000	No	Yes	2.00
719	14.38	1.46	100.00	3.18	0.57	0.92	12.68	0.00	12.68	4.000	No	Yes	2.00
720	14.40	1.48	100.00	3.18	0.57	0.91	12.82	0.00	12.82	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
721	14.42	1.51	100.00	3.18	0.57	0.91	13.06	0.00	13.06	4.000	No	Yes	2.00
722	14.44	1.52	100.00	3.18	0.57	0.91	13.22	0.00	13.22	4.000	No	Yes	2.00
723	14.46	1.52	100.00	3.18	0.57	0.91	13.14	0.00	13.14	4.000	No	Yes	2.00
724	14.48	1.51	100.00	3.19	0.57	0.91	13.13	0.00	13.13	4.000	No	Yes	2.00
725	14.50	1.49	100.00	3.20	0.57	0.91	12.90	0.00	12.90	4.000	No	Yes	2.00
726	14.52	1.45	100.00	3.22	0.57	0.91	12.50	0.00	12.50	4.000	No	Yes	2.00
727	14.54	1.41	100.00	3.25	0.57	0.91	12.23	0.00	12.23	4.000	No	Yes	2.00
728	14.56	1.38	100.00	3.26	0.58	0.91	11.73	0.00	11.73	4.000	No	Yes	2.00
729	14.58	1.38	100.00	3.26	0.58	0.91	11.72	0.00	11.72	4.000	No	Yes	2.00
730	14.60	1.41	100.00	3.25	0.57	0.91	12.13	0.00	12.13	4.000	No	Yes	2.00
731	14.62	1.43	100.00	3.24	0.57	0.91	12.39	0.00	12.39	4.000	No	Yes	2.00
732	14.64	1.44	100.00	3.23	0.57	0.91	12.25	0.00	12.25	4.000	No	Yes	2.00
733	14.66	1.45	100.00	3.23	0.57	0.91	12.40	0.00	12.40	4.000	No	Yes	2.00
734	14.68	1.47	100.00	3.22	0.57	0.90	12.60	0.00	12.60	4.000	No	Yes	2.00
735	14.70	1.49	100.00	3.21	0.57	0.90	12.71	0.00	12.71	4.000	No	Yes	2.00
736	14.72	1.44	100.00	3.22	0.57	0.90	12.87	0.00	12.87	4.000	No	Yes	2.00
737	14.74	1.46	100.00	3.20	0.58	0.90	11.27	0.00	11.27	4.000	No	Yes	2.00
738	14.76	1.47	100.00	3.19	0.57	0.90	13.20	0.00	13.20	4.000	No	Yes	2.00
739	14.78	1.53	100.00	3.17	0.57	0.90	13.07	0.00	13.07	4.000	No	Yes	2.00
740	14.81	1.51	100.00	3.17	0.57	0.90	12.76	0.00	12.76	4.000	No	Yes	2.00
741	14.83	1.51	100.00	3.17	0.57	0.90	12.87	0.00	12.87	4.000	No	Yes	2.00
742	14.84	1.52	100.00	3.16	0.57	0.90	12.97	0.00	12.97	4.000	No	Yes	2.00
743	14.86	1.53	100.00	3.16	0.57	0.90	13.06	0.00	13.06	4.000	No	Yes	2.00
744	14.88	1.53	100.00	3.16	0.57	0.90	13.01	0.00	13.01	4.000	No	Yes	2.00
745	14.90	1.53	100.00	3.18	0.57	0.90	13.08	0.00	13.08	4.000	No	Yes	2.00
746	14.92	1.52	100.00	3.20	0.57	0.90	12.90	0.00	12.90	4.000	No	Yes	2.00
747	14.94	1.51	100.00	3.21	0.57	0.90	12.91	0.00	12.91	4.000	No	Yes	2.00
748	14.96	1.50	100.00	3.23	0.57	0.89	12.81	0.00	12.81	4.000	No	Yes	2.00
749	14.98	1.47	100.00	3.26	0.57	0.89	12.50	0.00	12.50	4.000	No	Yes	2.00
750	15.01	1.44	100.00	3.29	0.57	0.89	12.15	0.00	12.15	4.000	No	Yes	2.00
751	15.02	1.41	100.00	3.30	0.58	0.89	11.81	0.00	11.81	4.000	No	Yes	2.00
752	15.04	1.42	100.00	3.30	0.58	0.89	11.84	0.00	11.84	4.000	No	Yes	2.00
753	15.06	1.46	100.00	3.27	0.57	0.89	12.20	0.00	12.20	4.000	No	Yes	2.00
754	15.08	1.52	100.00	3.24	0.57	0.89	12.77	0.00	12.77	4.000	No	Yes	2.00
755	15.10	1.59	100.00	3.19	0.57	0.89	13.44	0.00	13.44	4.000	No	Yes	2.00
756	15.12	1.67	100.00	3.15	0.57	0.89	14.10	0.00	14.10	4.000	No	Yes	2.00
757	15.14	1.77	100.00	3.08	0.56	0.89	14.69	0.00	14.69	4.000	No	Yes	2.00
758	15.16	1.89	100.00	3.02	0.56	0.89	16.13	0.00	16.13	4.000	No	Yes	2.00
759	15.18	2.01	99.85	2.96	0.56	0.89	17.14	0.00	17.14	4.000	No	Yes	2.00
760	15.20	2.09	97.88	2.94	0.55	0.89	17.98	0.00	17.98	4.000	No	Yes	2.00
761	15.22	2.13	98.09	2.94	0.55	0.89	18.24	0.00	18.24	4.000	No	Yes	2.00
762	15.24	2.11	100.00	2.97	0.55	0.89	18.10	0.00	18.10	4.000	No	Yes	2.00
763	15.26	2.06	100.00	3.01	0.56	0.89	17.33	0.00	17.33	4.000	No	Yes	2.00
764	15.28	1.98	100.00	3.07	0.56	0.89	16.90	0.00	16.90	4.000	No	Yes	2.00
765	15.30	1.90	100.00	3.12	0.56	0.89	16.11	0.00	16.11	4.000	No	Yes	2.00
766	15.32	1.83	100.00	3.17	0.56	0.88	15.29	0.00	15.29	4.000	No	Yes	2.00
767	15.34	1.73	100.00	3.23	0.56	0.88	14.94	0.00	14.94	4.000	No	Yes	2.00
768	15.37	1.63	100.00	3.27	0.57	0.88	13.26	0.00	13.26	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
769	15.38	1.48	100.00	3.35	0.57	0.88	12.72	0.00	12.72	4.000	No	Yes	2.00
770	15.40	1.37	100.00	3.41	0.58	0.88	10.99	0.00	10.99	4.000	No	Yes	2.00
771	15.42	1.25	100.00	3.47	0.58	0.88	10.20	0.00	10.20	4.000	No	Yes	2.00
772	15.44	1.20	100.00	3.49	0.58	0.88	9.65	0.00	9.65	4.000	No	Yes	2.00
773	15.46	1.16	100.00	3.49	0.58	0.87	9.54	0.00	9.54	4.000	No	Yes	2.00
774	15.48	1.12	100.00	3.49	0.59	0.87	9.14	0.00	9.14	4.000	No	Yes	2.00
775	15.50	1.08	100.00	3.51	0.59	0.87	8.74	0.00	8.74	4.000	No	Yes	2.00
776	15.52	1.03	100.00	3.53	0.59	0.87	8.28	0.00	8.28	4.000	No	Yes	2.00
777	15.54	0.99	100.00	3.54	0.59	0.87	7.85	0.00	7.85	4.000	No	Yes	2.00
778	15.56	0.96	100.00	3.55	0.59	0.87	7.72	0.00	7.72	4.000	No	Yes	2.00
779	15.58	0.94	100.00	3.54	0.59	0.87	7.51	0.00	7.51	4.000	No	Yes	2.00
780	15.60	0.93	100.00	3.53	0.59	0.87	7.31	0.00	7.31	4.000	No	Yes	2.00
781	15.62	0.92	100.00	3.51	0.59	0.87	7.34	0.00	7.34	4.000	No	Yes	2.00
782	15.64	0.92	100.00	3.48	0.59	0.87	7.30	0.00	7.30	4.000	No	Yes	2.00
783	15.66	0.91	100.00	3.47	0.59	0.87	7.29	0.00	7.29	4.000	No	Yes	2.00
784	15.68	0.91	100.00	3.45	0.59	0.87	7.11	0.00	7.11	4.000	No	Yes	2.00
785	15.70	0.89	100.00	3.45	0.59	0.87	7.09	0.00	7.09	4.000	No	Yes	2.00
786	15.72	0.87	100.00	3.43	0.59	0.86	6.89	0.00	6.89	4.000	No	Yes	2.00
787	15.74	0.88	100.00	3.40	0.60	0.86	6.35	0.00	6.35	4.000	No	Yes	2.00
788	15.76	0.92	100.00	3.35	0.59	0.86	7.33	0.00	7.33	4.000	No	Yes	2.00
789	15.78	0.96	100.00	3.33	0.59	0.86	7.71	0.00	7.71	4.000	No	Yes	2.00
790	15.80	0.98	100.00	3.32	0.59	0.86	7.54	0.00	7.54	4.000	No	Yes	2.00
791	15.82	0.98	100.00	3.32	0.59	0.86	7.60	0.00	7.60	4.000	No	Yes	2.00
792	15.84	1.00	100.00	3.30	0.59	0.86	7.70	0.00	7.70	4.000	No	Yes	2.00
793	15.86	1.03	100.00	3.27	0.59	0.86	7.98	0.00	7.98	4.000	No	Yes	2.00
794	15.88	1.07	100.00	3.23	0.59	0.86	8.41	0.00	8.41	4.000	No	Yes	2.00
795	15.90	1.11	100.00	3.19	0.59	0.86	8.67	0.00	8.67	4.000	No	Yes	2.00
796	15.92	1.13	100.00	3.18	0.59	0.86	8.97	0.00	8.97	4.000	No	Yes	2.00
797	15.94	1.13	100.00	3.18	0.59	0.86	8.92	0.00	8.92	4.000	No	Yes	2.00
798	15.96	1.09	100.00	3.22	0.59	0.86	8.48	0.00	8.48	4.000	No	Yes	2.00
799	15.98	1.04	100.00	3.26	0.59	0.86	7.94	0.00	7.94	4.000	No	Yes	2.00
800	16.00	1.00	100.00	3.29	0.59	0.86	7.66	0.00	7.66	4.000	No	Yes	2.00
801	16.03	0.98	100.00	3.31	0.59	0.86	7.56	0.00	7.56	4.000	No	Yes	2.00
802	16.04	0.96	100.00	3.32	0.59	0.86	7.40	0.00	7.40	4.000	No	Yes	2.00
803	16.06	0.94	100.00	3.34	0.59	0.86	7.20	0.00	7.20	4.000	No	Yes	2.00
804	16.08	0.93	100.00	3.35	0.59	0.85	7.02	0.00	7.02	4.000	No	Yes	2.00
805	16.10	0.92	100.00	3.35	0.59	0.85	6.99	0.00	6.99	4.000	No	Yes	2.00
806	16.12	0.92	100.00	3.34	0.59	0.85	7.07	0.00	7.07	4.000	No	Yes	2.00
807	16.14	0.92	100.00	3.33	0.59	0.85	6.97	0.00	6.97	4.000	No	Yes	2.00
808	16.16	0.92	100.00	3.32	0.59	0.85	7.01	0.00	7.01	4.000	No	Yes	2.00
809	16.18	0.93	100.00	3.31	0.59	0.85	7.01	0.00	7.01	4.000	No	Yes	2.00
810	16.20	0.93	100.00	3.30	0.59	0.85	7.14	0.00	7.14	4.000	No	Yes	2.00
811	16.22	0.94	100.00	3.30	0.59	0.85	7.02	0.00	7.02	4.000	No	Yes	2.00
812	16.24	0.93	100.00	3.30	0.59	0.85	7.10	0.00	7.10	4.000	No	Yes	2.00
813	16.26	0.94	100.00	3.30	0.59	0.85	7.04	0.00	7.04	4.000	No	Yes	2.00
814	16.28	0.93	100.00	3.31	0.59	0.85	7.04	0.00	7.04	4.000	No	Yes	2.00
815	16.30	0.93	100.00	3.31	0.59	0.85	6.99	0.00	6.99	4.000	No	Yes	2.00
816	16.32	0.93	100.00	3.31	0.59	0.85	6.97	0.00	6.97	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
817	16.34	0.93	100.00	3.30	0.59	0.85	7.05	0.00	7.05	4.000	No	Yes	2.00
818	16.36	0.94	100.00	3.30	0.59	0.85	7.07	0.00	7.07	4.000	No	Yes	2.00
819	16.38	0.95	100.00	3.29	0.59	0.85	7.06	0.00	7.06	4.000	No	Yes	2.00
820	16.40	0.95	100.00	3.28	0.59	0.85	7.20	0.00	7.20	4.000	No	Yes	2.00
821	16.42	0.98	100.00	3.25	0.59	0.85	7.28	0.00	7.28	4.000	No	Yes	2.00
822	16.44	1.00	100.00	3.23	0.59	0.85	7.57	0.00	7.57	4.000	No	Yes	2.00
823	16.46	1.03	100.00	3.21	0.59	0.85	7.78	0.00	7.78	4.000	No	Yes	2.00
824	16.48	1.05	100.00	3.20	0.59	0.85	8.01	0.00	8.01	4.000	No	Yes	2.00
825	16.50	1.06	100.00	3.20	0.59	0.84	8.11	0.00	8.11	4.000	No	Yes	2.00
826	16.52	1.05	100.00	3.21	0.59	0.84	7.97	0.00	7.97	4.000	No	Yes	2.00
827	16.54	1.03	100.00	3.23	0.59	0.84	7.81	0.00	7.81	4.000	No	Yes	2.00
828	16.56	1.02	100.00	3.25	0.59	0.84	7.65	0.00	7.65	4.000	No	Yes	2.00
829	16.58	1.02	100.00	3.25	0.59	0.84	7.65	0.00	7.65	4.000	No	Yes	2.00
830	16.60	1.03	100.00	3.25	0.59	0.84	7.76	0.00	7.76	4.000	No	Yes	2.00
831	16.62	1.03	100.00	3.24	0.59	0.84	7.76	0.00	7.76	4.000	No	Yes	2.00
832	16.64	1.03	100.00	3.24	0.59	0.84	7.73	0.00	7.73	4.000	No	Yes	2.00
833	16.66	1.03	100.00	3.23	0.59	0.84	7.71	0.00	7.71	4.000	No	Yes	2.00
834	16.68	1.02	100.00	3.23	0.59	0.84	7.65	0.00	7.65	4.000	No	Yes	2.00
835	16.70	1.03	100.00	3.22	0.59	0.84	7.64	0.00	7.64	4.000	No	Yes	2.00
836	16.72	1.11	100.00	3.18	0.59	0.84	7.72	0.00	7.72	4.000	No	Yes	2.00
837	16.74	1.16	100.00	3.17	0.58	0.84	9.94	0.00	9.94	4.000	No	Yes	2.00
838	16.76	1.18	100.00	3.18	0.59	0.84	9.22	0.00	9.22	4.000	No	Yes	2.00
839	16.78	1.10	100.00	3.25	0.59	0.84	8.29	0.00	8.29	4.000	No	Yes	2.00
840	16.80	1.04	100.00	3.29	0.59	0.84	7.81	0.00	7.81	4.000	No	Yes	2.00
841	16.82	1.02	100.00	3.29	0.59	0.84	7.59	0.00	7.59	4.000	No	Yes	2.00
842	16.84	1.03	100.00	3.28	0.59	0.84	7.72	0.00	7.72	4.000	No	Yes	2.00
843	16.86	1.06	100.00	3.25	0.59	0.84	7.91	0.00	7.91	4.000	No	Yes	2.00
844	16.88	1.11	100.00	3.21	0.59	0.84	8.25	0.00	8.25	4.000	No	Yes	2.00
845	16.91	1.17	100.00	3.16	0.59	0.84	8.83	0.00	8.83	4.000	No	Yes	2.00
846	16.92	1.27	100.00	3.09	0.58	0.84	9.57	0.00	9.57	4.000	No	Yes	2.00
847	16.94	1.34	100.00	3.05	0.58	0.84	10.63	0.00	10.63	4.000	No	Yes	2.00
848	16.96	1.34	100.00	3.05	0.58	0.84	10.42	0.00	10.42	4.000	No	Yes	2.00
849	16.98	1.29	100.00	3.09	0.58	0.83	9.59	0.00	9.59	4.000	No	Yes	2.00
850	17.00	1.29	100.00	3.11	0.58	0.83	9.59	0.00	9.59	4.000	No	Yes	2.00
851	17.02	1.32	100.00	3.09	0.58	0.83	10.23	0.00	10.23	4.000	No	Yes	2.00
852	17.04	1.36	100.00	3.08	0.58	0.83	10.36	0.00	10.36	4.000	No	Yes	2.00
853	17.06	1.34	100.00	3.10	0.58	0.83	10.39	0.00	10.39	4.000	No	Yes	2.00
854	17.08	1.28	100.00	3.13	0.58	0.83	9.82	0.00	9.82	4.000	No	Yes	2.00
855	17.10	1.23	100.00	3.18	0.59	0.83	9.12	0.00	9.12	4.000	No	Yes	2.00
856	17.18	1.20	100.00	3.20	0.59	0.83	9.00	0.00	9.00	4.000	No	Yes	2.00
857	17.18	1.19	100.00	3.20	0.59	0.83	9.00	0.00	9.00	4.000	No	Yes	2.00
858	17.18	1.19	100.00	3.20	0.59	0.83	9.00	0.00	9.00	4.000	No	Yes	2.00
859	17.18	1.34	100.00	3.12	0.59	0.83	9.06	0.00	9.06	4.000	No	Yes	2.00
860	17.20	1.43	100.00	3.08	0.57	0.83	12.68	0.00	12.68	4.000	No	Yes	2.00
861	17.22	1.53	100.00	3.04	0.58	0.83	11.44	0.00	11.44	4.000	No	Yes	2.00
862	17.24	1.47	100.00	3.07	0.58	0.83	11.43	0.00	11.43	4.000	No	Yes	2.00
863	17.26	1.46	100.00	3.07	0.58	0.83	11.36	0.00	11.36	4.000	No	Yes	2.00
864	17.28	1.45	100.00	3.08	0.58	0.83	11.06	0.00	11.06	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
865	17.30	1.44	100.00	3.10	0.58	0.83	11.21	0.00	11.21	4.000	No	Yes	2.00
866	17.32	1.39	100.00	3.12	0.58	0.83	10.89	0.00	10.89	4.000	No	Yes	2.00
867	17.34	1.30	100.00	3.17	0.58	0.83	9.93	0.00	9.93	4.000	No	Yes	2.00
868	17.36	1.20	100.00	3.23	0.59	0.82	8.99	0.00	8.99	4.000	No	Yes	2.00
869	17.38	1.12	100.00	3.28	0.59	0.82	8.27	0.00	8.27	4.000	No	Yes	2.00
870	17.40	1.10	100.00	3.30	0.59	0.82	8.03	0.00	8.03	4.000	No	Yes	2.00
871	17.42	1.09	100.00	3.30	0.59	0.82	8.18	0.00	8.18	4.000	No	Yes	2.00
872	17.44	1.08	100.00	3.30	0.59	0.82	8.04	0.00	8.04	4.000	No	Yes	2.00
873	17.46	1.06	100.00	3.31	0.59	0.82	7.80	0.00	7.80	4.000	No	Yes	2.00
874	17.48	1.05	100.00	3.31	0.59	0.82	7.68	0.00	7.68	4.000	No	Yes	2.00
875	17.50	1.10	100.00	3.24	0.59	0.82	7.70	0.00	7.70	4.000	No	Yes	2.00
876	17.52	1.28	100.00	3.10	0.59	0.82	9.01	0.00	9.01	4.000	No	Yes	2.00
877	17.54	1.57	97.66	2.93	0.58	0.82	11.92	0.00	11.92	4.000	No	Yes	2.00
878	17.56	1.85	88.64	2.82	0.57	0.82	14.70	0.00	14.70	4.000	No	Yes	2.00
879	17.58	2.00	86.82	2.80	0.56	0.83	16.04	0.00	16.04	4.000	No	Yes	2.00
880	17.60	2.10	87.67	2.81	0.56	0.82	15.89	0.00	15.89	4.000	No	Yes	2.00
881	17.62	2.16	89.32	2.83	0.56	0.83	17.41	0.00	17.41	4.000	No	Yes	2.00
882	17.64	2.17	92.05	2.86	0.56	0.83	17.72	0.00	17.72	4.000	No	Yes	2.00
883	17.66	2.03	98.82	2.95	0.56	0.82	16.37	0.00	16.37	4.000	No	Yes	2.00
884	17.68	1.80	100.00	3.07	0.57	0.82	14.06	0.00	14.06	4.000	No	Yes	2.00
885	17.70	1.65	100.00	3.14	0.57	0.82	12.19	0.00	12.19	4.000	No	Yes	2.00
886	17.72	1.78	100.00	3.09	0.57	0.82	12.41	0.00	12.41	4.000	No	Yes	2.00
887	17.74	1.93	100.00	3.04	0.56	0.82	17.30	0.00	17.30	4.000	No	Yes	2.00
888	17.76	2.01	100.00	3.03	0.56	0.82	15.87	0.00	15.87	4.000	No	Yes	2.00
889	17.78	1.88	100.00	3.07	0.57	0.82	14.56	0.00	14.56	4.000	No	Yes	2.00
890	17.80	1.76	100.00	3.11	0.57	0.82	13.95	0.00	13.95	4.000	No	Yes	2.00
891	17.82	1.62	100.00	3.15	0.57	0.82	12.65	0.00	12.65	4.000	No	Yes	2.00
892	17.84	1.47	100.00	3.22	0.58	0.81	11.23	0.00	11.23	4.000	No	Yes	2.00
893	17.86	1.41	100.00	3.24	0.58	0.81	10.13	0.00	10.13	4.000	No	Yes	2.00
894	17.88	1.59	100.00	3.13	0.58	0.81	11.09	0.00	11.09	4.000	No	Yes	2.00
895	17.90	1.98	99.64	2.96	0.56	0.82	15.32	0.00	15.32	4.000	No	Yes	2.00
896	17.92	2.35	90.03	2.84	0.55	0.82	19.54	0.00	19.54	4.000	No	Yes	2.00
897	17.94	2.53	87.74	2.81	0.55	0.82	20.58	0.00	20.58	4.000	No	Yes	2.00
898	17.96	2.47	90.69	2.85	0.55	0.82	19.84	0.00	19.84	4.000	No	Yes	2.00
899	17.98	2.37	94.35	2.89	0.55	0.82	18.39	0.00	18.39	4.000	No	Yes	2.00
900	18.00	2.39	94.68	2.90	0.55	0.82	18.32	0.00	18.32	4.000	No	Yes	2.00
901	18.02	2.54	92.35	2.87	0.55	0.82	20.35	0.00	20.35	4.000	No	Yes	2.00
902	18.04	2.84	87.73	2.81	0.54	0.82	22.10	0.00	22.10	4.000	No	Yes	2.00
903	18.06	3.05	86.25	2.79	0.53	0.82	25.90	0.00	25.90	4.000	No	Yes	2.00
904	18.08	3.10	87.78	2.81	0.53	0.82	25.49	0.00	25.49	4.000	No	Yes	2.00
905	18.10	3.00	90.68	2.85	0.54	0.82	23.32	0.00	23.32	4.000	No	Yes	2.00
906	18.12	2.97	90.99	2.85	0.54	0.82	23.55	0.00	23.55	4.000	No	Yes	2.00
907	18.14	2.99	89.04	2.83	0.53	0.82	24.62	0.00	24.62	4.000	No	Yes	2.00
908	18.16	2.79	91.77	2.86	0.53	0.82	24.00	0.00	24.00	4.000	No	Yes	2.00
909	18.18	2.39	100.00	2.96	0.55	0.81	18.50	0.00	18.50	4.000	No	Yes	2.00
910	18.20	1.89	100.00	3.13	0.56	0.81	14.79	0.00	14.79	4.000	No	Yes	2.00
911	18.22	1.57	100.00	3.25	0.58	0.80	11.70	0.00	11.70	4.000	No	Yes	2.00
912	18.24	1.55	100.00	3.23	0.58	0.80	10.63	0.00	10.63	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
913	18.26	1.81	100.00	3.08	0.57	0.81	13.80	0.00	13.80	4.000	No	Yes	2.00
914	18.28	2.20	96.32	2.92	0.55	0.81	17.67	0.00	17.67	4.000	No	Yes	2.00
915	18.30	2.41	90.76	2.85	0.55	0.81	19.73	0.00	19.73	4.000	No	Yes	2.00
916	18.32	2.59	87.08	2.80	0.55	0.81	19.20	0.00	19.20	4.000	No	Yes	2.00
917	18.34	2.93	81.15	2.73	0.54	0.81	22.02	0.00	22.02	4.000	No	Yes	2.00
918	18.36	3.53	72.66	2.62	0.53	0.82	28.28	0.00	28.28	4.000	No	Yes	2.00
919	18.38	4.06	66.80	2.55	0.51	0.82	33.99	59.87	93.86	0.130	No	No	0.67
920	18.40	4.33	64.81	2.52	0.51	0.82	35.30	59.80	95.10	0.131	No	No	0.68
921	18.42	4.36	65.52	2.53	0.51	0.82	35.12	59.91	95.04	0.131	No	No	0.68
922	18.44	4.31	67.17	2.55	0.51	0.82	34.69	60.15	94.84	0.131	No	No	0.68
923	18.46	4.25	67.87	2.56	0.51	0.82	34.10	60.13	94.23	0.130	No	No	0.68
924	18.48	4.21	68.12	2.56	0.51	0.82	33.69	60.06	93.75	0.130	No	No	0.67
925	18.50	4.22	68.08	2.56	0.51	0.82	33.74	60.06	93.81	0.130	No	No	0.67
926	18.52	4.15	70.36	2.59	0.51	0.82	34.20	60.65	94.84	0.131	No	No	0.68
927	18.54	4.07	73.01	2.63	0.51	0.82	32.10	0.00	32.10	4.000	No	Yes	2.00
928	18.58	3.60	81.52	2.73	0.51	0.81	31.57	0.00	31.57	4.000	No	Yes	2.00
929	18.58	3.17	89.44	2.83	0.54	0.81	22.69	0.00	22.69	4.000	No	Yes	2.00
930	18.60	2.81	95.26	2.90	0.54	0.81	21.37	0.00	21.37	4.000	Yes	Yes	2.00
931	18.62	2.90	90.83	2.85	0.54	0.81	22.74	0.00	22.74	4.000	Yes	Yes	2.00
932	18.64	3.10	85.50	2.78	0.53	0.81	24.68	0.00	24.68	4.000	Yes	Yes	2.00
933	18.66	3.38	80.74	2.72	0.53	0.81	26.21	0.00	26.21	4.000	Yes	Yes	2.00
934	18.68	3.76	77.66	2.68	0.52	0.81	29.39	0.00	29.39	4.000	Yes	Yes	2.00
935	18.70	4.21	73.45	2.63	0.51	0.81	34.15	0.00	34.15	4.000	Yes	Yes	2.00
936	18.72	4.57	69.72	2.58	0.50	0.82	37.27	61.42	98.69	4.000	Yes	No	2.00
937	18.74	4.81	65.90	2.54	0.50	0.82	38.50	60.97	99.47	4.000	Yes	No	2.00
938	18.76	4.95	61.30	2.48	0.50	0.82	39.92	60.26	100.18	4.000	Yes	No	2.00
939	18.78	5.00	56.85	2.42	0.50	0.81	40.53	59.16	99.69	4.000	Yes	No	2.00
940	18.80	4.97	52.83	2.37	0.50	0.81	39.80	57.62	97.42	4.000	Yes	No	2.00
941	18.82	4.87	49.65	2.33	0.51	0.81	38.85	56.16	95.01	4.000	Yes	No	2.00
942	18.84	4.72	47.76	2.31	0.51	0.81	37.78	55.08	92.86	4.000	Yes	No	2.00
943	18.86	4.59	46.76	2.30	0.52	0.81	36.11	54.21	90.31	0.126	No	No	0.66
944	18.88	4.47	46.40	2.29	0.52	0.80	35.27	53.83	89.10	0.125	No	No	0.65
945	18.90	4.44	46.91	2.30	0.52	0.80	34.86	53.95	88.81	0.124	No	No	0.65
946	18.92	4.50	49.06	2.33	0.52	0.80	35.31	54.98	90.29	0.126	No	No	0.66
947	18.94	4.69	51.94	2.36	0.51	0.81	36.84	56.50	93.35	0.129	No	No	0.68
948	18.96	5.00	53.21	2.38	0.50	0.81	39.48	57.67	97.15	0.134	No	No	0.71
949	18.98	5.31	53.01	2.38	0.49	0.81	43.31	58.63	101.94	0.140	No	No	0.75
950	19.07	5.52	52.39	2.37	0.49	0.81	44.52	58.73	103.25	0.142	No	No	0.76
951	19.07	5.58	52.08	2.36	0.49	0.81	44.51	58.61	103.13	0.142	No	No	0.76
952	19.07	5.86	51.18	2.35	0.49	0.81	44.74	58.33	103.07	0.142	No	No	0.76
953	19.08	6.62	47.46	2.31	0.48	0.82	51.32	58.47	109.79	0.152	No	No	0.83
954	19.10	7.66	41.23	2.23	0.45	0.82	63.93	58.19	122.12	0.176	No	No	1.00
955	19.12	8.43	35.44	2.16	0.45	0.83	70.86	55.35	126.21	0.187	No	No	1.07
956	19.22	8.71	31.83	2.11	0.45	0.82	70.37	51.65	122.02	0.176	No	No	1.00
957	19.22	8.69	30.75	2.10	0.46	0.82	70.30	50.41	120.71	0.173	No	No	0.98
958	19.14	8.12	30.20	2.09	0.46	0.82	70.17	49.74	119.91	0.171	No	No	0.96
959	19.22	7.40	29.28	2.08	0.50	0.81	55.27	45.64	100.91	0.139	No	No	0.75
960	19.24	6.60	27.52	2.06	0.51	0.80	51.65	42.75	94.40	0.131	No	No	0.69

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
961	19.26	6.16	28.65	2.07	0.51	0.80	49.44	43.73	93.18	4.000	Yes	No	2.00
962	19.28	5.64	31.32	2.10	0.52	0.80	44.19	45.61	89.80	4.000	Yes	No	2.00
963	19.30	5.01	35.03	2.15	0.53	0.79	39.00	47.81	86.81	4.000	Yes	No	2.00
964	19.32	4.44	39.37	2.20	0.54	0.79	34.17	49.78	83.95	4.000	Yes	No	2.00
965	19.34	3.96	44.43	2.27	0.54	0.79	30.24	51.61	81.86	4.000	Yes	No	2.00
966	19.36	3.57	52.44	2.37	0.54	0.79	27.61	54.20	81.81	4.000	Yes	No	2.00
967	19.38	3.21	63.44	2.51	0.54	0.79	25.01	56.55	81.56	4.000	Yes	No	2.00
968	19.40	2.86	76.96	2.67	0.55	0.78	21.79	0.00	21.79	4.000	Yes	Yes	2.00
969	19.42	2.60	86.94	2.80	0.55	0.78	19.27	0.00	19.27	4.000	Yes	Yes	2.00
970	19.44	2.51	92.22	2.87	0.55	0.78	19.08	0.00	19.08	4.000	Yes	Yes	2.00
971	19.46	2.58	92.69	2.87	0.55	0.78	19.65	0.00	19.65	4.000	No	Yes	2.00
972	19.48	2.78	91.57	2.86	0.55	0.78	20.77	0.00	20.77	4.000	Yes	Yes	2.00
973	19.50	3.14	88.71	2.82	0.54	0.79	23.93	0.00	23.93	4.000	Yes	Yes	2.00
974	19.52	3.83	80.98	2.72	0.52	0.79	28.20	0.00	28.20	4.000	Yes	Yes	2.00
975	19.54	4.90	69.13	2.58	0.50	0.80	37.37	61.33	98.69	4.000	Yes	No	2.00
976	19.56	6.18	56.70	2.42	0.47	0.81	50.14	61.76	111.90	4.000	Yes	No	2.00
977	19.58	7.20	47.52	2.31	0.46	0.81	59.86	60.71	120.57	4.000	Yes	No	2.00
978	19.60	7.73	41.41	2.23	0.46	0.81	62.72	58.00	120.72	4.000	Yes	No	2.00
979	19.62	7.77	37.63	2.18	0.46	0.81	62.99	55.38	118.37	4.000	Yes	No	2.00
980	19.64	7.53	35.38	2.15	0.47	0.81	60.35	52.92	113.26	4.000	Yes	No	2.00
981	19.66	7.04	35.17	2.15	0.48	0.80	56.33	51.83	108.15	0.149	No	No	0.82
982	19.68	6.36	35.62	2.16	0.50	0.80	50.27	50.84	101.12	0.139	No	No	0.76
983	19.70	5.51	38.79	2.20	0.51	0.79	43.20	51.56	94.76	0.131	No	No	0.70
984	19.72	4.89	41.83	2.24	0.53	0.78	35.12	51.47	86.58	0.122	No	No	0.65
985	19.74	4.53	45.88	2.29	0.52	0.78	35.01	53.52	88.53	0.124	No	No	0.66
986	19.76	4.52	46.19	2.29	0.53	0.78	34.21	53.46	87.67	0.123	No	No	0.66
987	19.78	4.63	45.81	2.29	0.52	0.78	35.07	53.50	88.58	0.124	No	No	0.66
988	19.81	4.95	42.62	2.25	0.52	0.78	37.53	52.50	90.03	0.126	No	No	0.67
989	19.82	5.38	38.00	2.19	0.51	0.79	41.95	50.72	92.67	0.129	No	No	0.69
990	19.84	5.75	33.92	2.14	0.51	0.79	45.29	48.28	93.57	0.130	No	No	0.70
991	19.86	5.82	32.59	2.12	0.51	0.79	46.43	47.32	93.75	4.000	Yes	No	2.00
992	19.88	5.48	34.89	2.15	0.52	0.79	43.40	48.69	92.09	4.000	Yes	No	2.00
993	19.90	4.86	39.30	2.20	0.53	0.78	37.23	50.46	87.69	4.000	Yes	No	2.00
994	19.92	4.24	44.39	2.27	0.54	0.78	31.58	51.93	83.51	4.000	Yes	No	2.00
995	19.94	3.79	48.23	2.32	0.54	0.77	28.50	52.86	81.37	4.000	Yes	No	2.00
996	19.96	3.52	55.84	2.41	0.54	0.77	26.75	55.05	81.80	4.000	Yes	No	2.00
997	19.98	3.26	66.09	2.54	0.54	0.77	25.07	57.15	82.23	4.000	Yes	No	2.00
998	20.00	3.01	78.51	2.69	0.54	0.77	22.68	0.00	22.68	4.000	Yes	Yes	2.00
999	20.02	2.73	89.61	2.83	0.55	0.77	20.90	0.00	20.90	4.000	Yes	Yes	2.00
1000	20.04	2.36	100.00	2.97	0.55	0.77	18.59	0.00	18.59	4.000	Yes	Yes	2.00
1001	20.06	1.99	100.00	3.11	0.57	0.76	14.21	0.00	14.21	4.000	No	Yes	2.00
1002	20.08	1.68	100.00	3.22	0.57	0.76	12.08	0.00	12.08	4.000	No	Yes	2.00
1003	20.10	1.60	100.00	3.24	0.58	0.76	11.36	0.00	11.36	4.000	No	Yes	2.00
1004	20.12	1.62	100.00	3.20	0.57	0.76	12.32	0.00	12.32	4.000	No	Yes	2.00
1005	20.14	1.80	100.00	3.13	0.57	0.76	12.51	0.00	12.51	4.000	No	Yes	2.00
1006	20.16	2.45	96.87	2.92	0.56	0.76	15.32	0.00	15.32	4.000	Yes	Yes	2.00
1007	20.18	3.62	76.54	2.67	0.53	0.77	27.49	0.00	27.49	4.000	Yes	Yes	2.00
1008	20.20	4.81	60.77	2.47	0.50	0.79	39.99	60.13	100.12	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1009	20.22	5.50	52.55	2.37	0.49	0.79	43.48	58.51	101.99	4.000	Yes	No	2.00
1010	20.24	5.63	48.77	2.32	0.50	0.79	43.90	57.12	101.02	4.000	Yes	No	2.00
1011	20.26	5.53	45.46	2.28	0.50	0.78	42.87	55.33	98.20	4.000	Yes	No	2.00
1012	20.28	5.35	42.30	2.24	0.51	0.78	40.78	53.14	93.92	4.000	Yes	No	2.00
1013	20.30	5.19	40.04	2.21	0.52	0.78	39.12	51.39	90.50	4.000	Yes	No	2.00
1014	20.32	5.14	39.10	2.20	0.52	0.77	38.66	50.68	89.35	0.125	No	No	0.68
1015	20.34	5.28	37.82	2.19	0.52	0.77	39.37	49.98	89.35	0.125	No	No	0.68
1016	20.36	5.51	35.96	2.16	0.52	0.78	42.31	49.30	91.61	0.127	No	No	0.69
1017	20.38	5.76	33.62	2.13	0.52	0.77	43.92	47.72	91.64	0.127	No	No	0.69
1018	20.40	5.95	31.48	2.11	0.52	0.77	45.33	46.00	91.33	0.127	No	No	0.69
1019	20.42	6.11	29.59	2.08	0.52	0.77	46.53	44.25	90.77	0.127	No	No	0.69
1020	20.44	6.21	28.38	2.07	0.52	0.77	47.29	42.99	90.28	0.126	No	No	0.68
1021	20.46	6.22	27.80	2.06	0.52	0.77	47.46	42.30	89.76	0.125	No	No	0.68
1022	20.48	6.12	27.97	2.06	0.52	0.77	46.63	42.37	89.00	0.125	No	No	0.68
1023	20.50	5.89	29.24	2.08	0.52	0.77	44.89	43.52	88.41	0.124	No	No	0.67
1024	20.52	5.68	30.52	2.09	0.53	0.77	41.83	44.30	86.14	0.122	No	No	0.66
1025	20.54	5.42	32.99	2.12	0.53	0.77	40.32	46.37	86.69	0.122	No	No	0.66

Abbreviations

Depth: Depth from free surface, at which CPT was performed (m)
q_t: Total cone resistance
FC: Fines content (%)
I_c: Soil behavior type index
m: Stress exponent
C_N: Overburden correction factor
q_{c1N}: Normalized and adjusted cone resistance
Δq_{c1N}: Cone resistance correction factor due to fines
$q_{c1N,cs}$: Normalized and adjusted cone resistance
$CRR_{7.5}$: Cyclic resistance ratio for M_w=7.5
FS: Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
0.02	2.00	0.00	9.99	0.03	0.00	0.05	2.00	0.00	9.98	0.03	0.00
0.06	2.00	0.00	9.97	0.01	0.00	0.08	2.00	0.00	9.96	0.02	0.00
0.10	2.00	0.00	9.95	0.02	0.00	0.12	2.00	0.00	9.94	0.02	0.00
0.14	2.00	0.00	9.93	0.02	0.00	0.16	2.00	0.00	9.92	0.02	0.00
0.18	2.00	0.00	9.91	0.02	0.00	0.20	2.00	0.00	9.90	0.02	0.00
0.22	2.00	0.00	9.89	0.02	0.00	0.24	2.00	0.00	9.88	0.02	0.00
0.26	2.00	0.00	9.87	0.02	0.00	0.28	2.00	0.00	9.86	0.02	0.00
0.30	2.00	0.00	9.85	0.02	0.00	0.32	2.00	0.00	9.84	0.02	0.00
0.34	2.00	0.00	9.83	0.02	0.00	0.36	2.00	0.00	9.82	0.02	0.00
0.38	2.00	0.00	9.81	0.02	0.00	0.40	2.00	0.00	9.80	0.02	0.00
0.42	2.00	0.00	9.79	0.02	0.00	0.44	2.00	0.00	9.78	0.02	0.00
0.46	2.00	0.00	9.77	0.02	0.00	0.48	2.00	0.00	9.76	0.02	0.00
0.50	2.00	0.00	9.75	0.02	0.00	0.52	2.00	0.00	9.74	0.02	0.00
0.54	2.00	0.00	9.73	0.02	0.00	0.56	2.00	0.00	9.72	0.02	0.00
0.58	2.00	0.00	9.71	0.02	0.00	0.60	2.00	0.00	9.70	0.02	0.00
0.62	2.00	0.00	9.69	0.02	0.00	0.64	2.00	0.00	9.68	0.02	0.00
0.66	2.00	0.00	9.67	0.02	0.00	0.68	2.00	0.00	9.66	0.02	0.00
0.70	2.00	0.00	9.65	0.02	0.00	0.72	2.00	0.00	9.64	0.02	0.00
0.74	2.00	0.00	9.63	0.02	0.00	0.76	2.00	0.00	9.62	0.02	0.00
0.78	2.00	0.00	9.61	0.02	0.00	0.80	2.00	0.00	9.60	0.02	0.00
0.82	2.00	0.00	9.59	0.02	0.00	0.84	2.00	0.00	9.58	0.02	0.00
1.04	2.00	0.00	9.48	0.20	0.00	1.04	2.00	0.00	9.48	0.00	0.00
1.04	2.00	0.00	9.48	0.00	0.00	1.04	2.00	0.00	9.48	0.00	0.00
1.04	2.00	0.00	9.48	0.00	0.00	0.96	2.00	0.00	9.52	0.08	0.00
0.98	2.00	0.00	9.51	0.02	0.00	1.00	2.00	0.00	9.50	0.02	0.00
1.02	2.00	0.00	9.49	0.02	0.00	1.04	2.00	0.00	9.48	0.02	0.00
1.06	2.00	0.00	9.47	0.02	0.00	1.08	2.00	0.00	9.46	0.02	0.00
1.10	2.00	0.00	9.45	0.02	0.00	1.12	2.00	0.00	9.44	0.02	0.00
1.14	2.00	0.00	9.43	0.02	0.00	1.16	2.00	0.00	9.42	0.02	0.00
1.18	2.00	0.00	9.41	0.02	0.00	1.20	2.00	0.00	9.40	0.02	0.00
1.32	2.00	0.00	9.34	0.12	0.00	1.32	2.00	0.00	9.34	0.00	0.00
1.32	2.00	0.00	9.34	0.00	0.00	1.32	2.00	0.00	9.34	0.00	0.00
1.30	2.00	0.00	9.35	0.02	0.00	1.32	2.00	0.00	9.34	0.02	0.00
1.34	2.00	0.00	9.33	0.02	0.00	1.36	2.00	0.00	9.32	0.02	0.00
1.38	2.00	0.00	9.31	0.02	0.00	1.40	2.00	0.00	9.30	0.02	0.00
1.42	2.00	0.00	9.29	0.02	0.00	1.44	2.00	0.00	9.28	0.02	0.00
1.46	2.00	0.00	9.27	0.02	0.00	1.49	2.00	0.00	9.26	0.03	0.00
1.50	2.00	0.00	9.25	0.01	0.00	1.53	2.00	0.00	9.24	0.03	0.00
1.54	2.00	0.00	9.23	0.01	0.00	1.56	2.00	0.00	9.22	0.02	0.00
1.58	2.00	0.00	9.21	0.02	0.00	1.60	2.00	0.00	9.20	0.02	0.00
1.62	2.00	0.00	9.19	0.02	0.00	1.64	2.00	0.00	9.18	0.02	0.00
1.66	2.00	0.00	9.17	0.02	0.00	1.68	2.00	0.00	9.16	0.02	0.00
1.70	2.00	0.00	9.15	0.02	0.00	1.72	2.00	0.00	9.14	0.02	0.00
1.74	2.00	0.00	9.13	0.02	0.00	1.76	2.00	0.00	9.12	0.02	0.00
1.78	2.00	0.00	9.11	0.02	0.00	1.80	2.00	0.00	9.10	0.02	0.00
1.82	2.00	0.00	9.09	0.02	0.00	1.84	2.00	0.00	9.08	0.02	0.00
1.86	2.00	0.00	9.07	0.02	0.00	1.88	2.00	0.00	9.06	0.02	0.00
1.91	2.00	0.00	9.05	0.03	0.00	1.92	2.00	0.00	9.04	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
1.94	2.00	0.00	9.03	0.02	0.00	1.96	2.00	0.00	9.02	0.02	0.00
1.98	2.00	0.00	9.01	0.02	0.00	2.00	2.00	0.00	9.00	0.02	0.00
2.02	2.00	0.00	8.99	0.02	0.00	2.04	2.00	0.00	8.98	0.02	0.00
2.06	2.00	0.00	8.97	0.02	0.00	2.08	2.00	0.00	8.96	0.02	0.00
2.10	2.00	0.00	8.95	0.02	0.00	2.13	2.00	0.00	8.94	0.03	0.00
2.14	2.00	0.00	8.93	0.01	0.00	2.16	2.00	0.00	8.92	0.02	0.00
2.18	2.00	0.00	8.91	0.02	0.00	2.20	2.00	0.00	8.90	0.02	0.00
2.22	2.00	0.00	8.89	0.02	0.00	2.24	2.00	0.00	8.88	0.02	0.00
2.26	2.00	0.00	8.87	0.02	0.00	2.28	2.00	0.00	8.86	0.02	0.00
2.30	2.00	0.00	8.85	0.02	0.00	2.32	2.00	0.00	8.84	0.02	0.00
2.34	2.00	0.00	8.83	0.02	0.00	2.37	2.00	0.00	8.82	0.03	0.00
2.38	2.00	0.00	8.81	0.01	0.00	2.42	2.00	0.00	8.79	0.04	0.00
2.42	2.00	0.00	8.79	0.00	0.00	2.44	2.00	0.00	8.78	0.02	0.00
2.46	2.00	0.00	8.77	0.02	0.00	2.48	2.00	0.00	8.76	0.02	0.00
2.50	2.00	0.00	8.75	0.02	0.00	2.52	2.00	0.00	8.74	0.02	0.00
2.54	2.00	0.00	8.73	0.02	0.00	2.56	2.00	0.00	8.72	0.02	0.00
2.58	2.00	0.00	8.71	0.02	0.00	2.60	2.00	0.00	8.70	0.02	0.00
2.62	2.00	0.00	8.69	0.02	0.00	2.64	2.00	0.00	8.68	0.02	0.00
2.66	2.00	0.00	8.67	0.02	0.00	2.68	2.00	0.00	8.66	0.02	0.00
2.70	2.00	0.00	8.65	0.02	0.00	2.72	2.00	0.00	8.64	0.02	0.00
2.74	2.00	0.00	8.63	0.02	0.00	2.76	2.00	0.00	8.62	0.02	0.00
2.78	2.00	0.00	8.61	0.02	0.00	2.80	2.00	0.00	8.60	0.02	0.00
2.82	2.00	0.00	8.59	0.02	0.00	2.84	2.00	0.00	8.58	0.02	0.00
2.86	2.00	0.00	8.57	0.02	0.00	2.89	2.00	0.00	8.56	0.03	0.00
2.90	2.00	0.00	8.55	0.01	0.00	2.92	2.00	0.00	8.54	0.02	0.00
2.94	2.00	0.00	8.53	0.02	0.00	2.96	2.00	0.00	8.52	0.02	0.00
2.99	2.00	0.00	8.51	0.03	0.00	3.00	2.00	0.00	8.50	0.01	0.00
3.03	2.00	0.00	8.49	0.03	0.00	3.05	2.00	0.00	8.48	0.02	0.00
3.06	2.00	0.00	8.47	0.01	0.00	3.08	2.00	0.00	8.46	0.02	0.00
3.10	2.00	0.00	8.45	0.02	0.00	3.12	2.00	0.00	8.44	0.02	0.00
3.14	2.00	0.00	8.43	0.02	0.00	3.16	2.00	0.00	8.42	0.02	0.00
3.18	2.00	0.00	8.41	0.02	0.00	3.20	2.00	0.00	8.40	0.02	0.00
3.22	2.00	0.00	8.39	0.02	0.00	3.24	2.00	0.00	8.38	0.02	0.00
3.26	2.00	0.00	8.37	0.02	0.00	3.28	2.00	0.00	8.36	0.02	0.00
3.30	2.00	0.00	8.35	0.02	0.00	3.32	2.00	0.00	8.34	0.02	0.00
3.34	2.00	0.00	8.33	0.02	0.00	3.36	0.43	0.57	8.32	0.02	0.10
3.38	2.00	0.00	8.31	0.02	0.00	3.40	2.00	0.00	8.30	0.02	0.00
3.42	2.00	0.00	8.29	0.02	0.00	3.44	2.00	0.00	8.28	0.02	0.00
3.46	2.00	0.00	8.27	0.02	0.00	3.48	2.00	0.00	8.26	0.02	0.00
3.50	2.00	0.00	8.25	0.02	0.00	3.52	2.00	0.00	8.24	0.02	0.00
3.54	2.00	0.00	8.23	0.02	0.00	3.56	2.00	0.00	8.22	0.02	0.00
3.58	2.00	0.00	8.21	0.02	0.00	3.60	2.00	0.00	8.20	0.02	0.00
3.62	2.00	0.00	8.19	0.02	0.00	3.64	2.00	0.00	8.18	0.02	0.00
3.66	2.00	0.00	8.17	0.02	0.00	3.68	2.00	0.00	8.16	0.02	0.00
3.70	2.00	0.00	8.15	0.02	0.00	3.72	2.00	0.00	8.14	0.02	0.00
3.74	2.00	0.00	8.13	0.02	0.00	3.76	2.00	0.00	8.12	0.02	0.00
3.78	2.00	0.00	8.11	0.02	0.00	3.80	2.00	0.00	8.10	0.02	0.00
3.82	2.00	0.00	8.09	0.02	0.00	3.84	2.00	0.00	8.08	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
3.86	2.00	0.00	8.07	0.02	0.00	3.88	2.00	0.00	8.06	0.02	0.00
3.90	2.00	0.00	8.05	0.02	0.00	3.92	2.00	0.00	8.04	0.02	0.00
3.94	2.00	0.00	8.03	0.02	0.00	3.96	2.00	0.00	8.02	0.02	0.00
3.98	2.00	0.00	8.01	0.02	0.00	4.00	2.00	0.00	8.00	0.02	0.00
4.02	2.00	0.00	7.99	0.02	0.00	4.04	2.00	0.00	7.98	0.02	0.00
4.06	2.00	0.00	7.97	0.02	0.00	4.08	2.00	0.00	7.96	0.02	0.00
4.10	2.00	0.00	7.95	0.02	0.00	4.12	2.00	0.00	7.94	0.02	0.00
4.14	2.00	0.00	7.93	0.02	0.00	4.16	2.00	0.00	7.92	0.02	0.00
4.18	2.00	0.00	7.91	0.02	0.00	4.20	2.00	0.00	7.90	0.02	0.00
4.22	2.00	0.00	7.89	0.02	0.00	4.24	2.00	0.00	7.88	0.02	0.00
4.26	2.00	0.00	7.87	0.02	0.00	4.28	2.00	0.00	7.86	0.02	0.00
4.30	2.00	0.00	7.85	0.02	0.00	4.32	2.00	0.00	7.84	0.02	0.00
4.34	2.00	0.00	7.83	0.02	0.00	4.36	2.00	0.00	7.82	0.02	0.00
4.38	2.00	0.00	7.81	0.02	0.00	4.40	2.00	0.00	7.80	0.02	0.00
4.42	2.00	0.00	7.79	0.02	0.00	4.44	2.00	0.00	7.78	0.02	0.00
4.46	2.00	0.00	7.77	0.02	0.00	4.48	2.00	0.00	7.76	0.02	0.00
4.50	2.00	0.00	7.75	0.02	0.00	4.52	2.00	0.00	7.74	0.02	0.00
4.54	2.00	0.00	7.73	0.02	0.00	4.56	2.00	0.00	7.72	0.02	0.00
4.58	2.00	0.00	7.71	0.02	0.00	4.60	2.00	0.00	7.70	0.02	0.00
4.62	2.00	0.00	7.69	0.02	0.00	4.68	2.00	0.00	7.66	0.06	0.00
4.68	2.00	0.00	7.66	0.00	0.00	4.68	2.00	0.00	7.66	0.00	0.00
4.70	2.00	0.00	7.65	0.02	0.00	4.72	2.00	0.00	7.64	0.02	0.00
4.74	2.00	0.00	7.63	0.02	0.00	4.76	2.00	0.00	7.62	0.02	0.00
4.78	2.00	0.00	7.61	0.02	0.00	4.80	2.00	0.00	7.60	0.02	0.00
4.82	2.00	0.00	7.59	0.02	0.00	4.84	2.00	0.00	7.58	0.02	0.00
4.86	2.00	0.00	7.57	0.02	0.00	4.89	2.00	0.00	7.56	0.03	0.00
4.90	2.00	0.00	7.55	0.01	0.00	4.93	2.00	0.00	7.54	0.03	0.00
4.94	2.00	0.00	7.53	0.01	0.00	4.96	2.00	0.00	7.52	0.02	0.00
4.98	2.00	0.00	7.51	0.02	0.00	5.01	2.00	0.00	7.50	0.03	0.00
5.02	2.00	0.00	7.49	0.01	0.00	5.04	2.00	0.00	7.48	0.02	0.00
5.06	2.00	0.00	7.47	0.02	0.00	5.08	2.00	0.00	7.46	0.02	0.00
5.10	2.00	0.00	7.45	0.02	0.00	5.12	2.00	0.00	7.44	0.02	0.00
5.14	2.00	0.00	7.43	0.02	0.00	5.16	2.00	0.00	7.42	0.02	0.00
5.18	2.00	0.00	7.41	0.02	0.00	5.20	2.00	0.00	7.40	0.02	0.00
5.22	2.00	0.00	7.39	0.02	0.00	5.24	2.00	0.00	7.38	0.02	0.00
5.26	2.00	0.00	7.37	0.02	0.00	5.28	2.00	0.00	7.36	0.02	0.00
5.30	2.00	0.00	7.35	0.02	0.00	5.32	2.00	0.00	7.34	0.02	0.00
5.34	2.00	0.00	7.33	0.02	0.00	5.36	2.00	0.00	7.32	0.02	0.00
5.38	2.00	0.00	7.31	0.02	0.00	5.40	2.00	0.00	7.30	0.02	0.00
5.42	2.00	0.00	7.29	0.02	0.00	5.44	2.00	0.00	7.28	0.02	0.00
5.46	2.00	0.00	7.27	0.02	0.00	5.48	2.00	0.00	7.26	0.02	0.00
5.51	2.00	0.00	7.25	0.03	0.00	5.52	2.00	0.00	7.24	0.01	0.00
5.54	2.00	0.00	7.23	0.02	0.00	5.56	2.00	0.00	7.22	0.02	0.00
5.58	2.00	0.00	7.21	0.02	0.00	5.60	2.00	0.00	7.20	0.02	0.00
5.62	2.00	0.00	7.19	0.02	0.00	5.64	2.00	0.00	7.18	0.02	0.00
5.66	2.00	0.00	7.17	0.02	0.00	5.68	2.00	0.00	7.16	0.02	0.00
5.70	2.00	0.00	7.15	0.02	0.00	5.72	2.00	0.00	7.14	0.02	0.00
5.74	2.00	0.00	7.13	0.02	0.00	5.76	2.00	0.00	7.12	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
5.78	2.00	0.00	7.11	0.02	0.00	5.80	2.00	0.00	7.10	0.02	0.00
5.82	2.00	0.00	7.09	0.02	0.00	5.84	2.00	0.00	7.08	0.02	0.00
5.86	2.00	0.00	7.07	0.02	0.00	5.88	2.00	0.00	7.06	0.02	0.00
5.90	2.00	0.00	7.05	0.02	0.00	5.92	2.00	0.00	7.04	0.02	0.00
5.94	2.00	0.00	7.03	0.02	0.00	5.96	2.00	0.00	7.02	0.02	0.00
5.98	2.00	0.00	7.01	0.02	0.00	6.00	2.00	0.00	7.00	0.02	0.00
6.02	2.00	0.00	6.99	0.02	0.00	6.04	2.00	0.00	6.98	0.02	0.00
6.06	2.00	0.00	6.97	0.02	0.00	6.08	2.00	0.00	6.96	0.02	0.00
6.10	2.00	0.00	6.95	0.02	0.00	6.12	2.00	0.00	6.94	0.02	0.00
6.14	2.00	0.00	6.93	0.02	0.00	6.16	2.00	0.00	6.92	0.02	0.00
6.18	2.00	0.00	6.91	0.02	0.00	6.20	2.00	0.00	6.90	0.02	0.00
6.22	2.00	0.00	6.89	0.02	0.00	6.24	2.00	0.00	6.88	0.02	0.00
6.26	2.00	0.00	6.87	0.02	0.00	6.28	2.00	0.00	6.86	0.02	0.00
6.30	2.00	0.00	6.85	0.02	0.00	6.32	2.00	0.00	6.84	0.02	0.00
6.34	2.00	0.00	6.83	0.02	0.00	6.36	2.00	0.00	6.82	0.02	0.00
6.38	2.00	0.00	6.81	0.02	0.00	6.40	2.00	0.00	6.80	0.02	0.00
6.42	2.00	0.00	6.79	0.02	0.00	6.44	2.00	0.00	6.78	0.02	0.00
6.46	2.00	0.00	6.77	0.02	0.00	6.48	2.00	0.00	6.76	0.02	0.00
6.50	2.00	0.00	6.75	0.02	0.00	6.52	2.00	0.00	6.74	0.02	0.00
6.54	2.00	0.00	6.73	0.02	0.00	6.56	2.00	0.00	6.72	0.02	0.00
6.58	2.00	0.00	6.71	0.02	0.00	6.60	2.00	0.00	6.70	0.02	0.00
6.62	2.00	0.00	6.69	0.02	0.00	6.64	2.00	0.00	6.68	0.02	0.00
6.66	2.00	0.00	6.67	0.02	0.00	6.68	2.00	0.00	6.66	0.02	0.00
6.70	2.00	0.00	6.65	0.02	0.00	6.72	2.00	0.00	6.64	0.02	0.00
6.74	2.00	0.00	6.63	0.02	0.00	6.76	2.00	0.00	6.62	0.02	0.00
6.78	2.00	0.00	6.61	0.02	0.00	6.80	2.00	0.00	6.60	0.02	0.00
6.82	2.00	0.00	6.59	0.02	0.00	6.84	2.00	0.00	6.58	0.02	0.00
6.86	2.00	0.00	6.57	0.02	0.00	6.88	2.00	0.00	6.56	0.02	0.00
6.90	2.00	0.00	6.55	0.02	0.00	6.92	2.00	0.00	6.54	0.02	0.00
6.94	2.00	0.00	6.53	0.02	0.00	6.96	2.00	0.00	6.52	0.02	0.00
6.98	2.00	0.00	6.51	0.02	0.00	7.00	2.00	0.00	6.50	0.02	0.00
7.02	2.00	0.00	6.49	0.02	0.00	7.04	2.00	0.00	6.48	0.02	0.00
7.06	2.00	0.00	6.47	0.02	0.00	7.08	2.00	0.00	6.46	0.02	0.00
7.10	2.00	0.00	6.45	0.02	0.00	7.12	2.00	0.00	6.44	0.02	0.00
7.14	2.00	0.00	6.43	0.02	0.00	7.16	2.00	0.00	6.42	0.02	0.00
7.18	2.00	0.00	6.41	0.02	0.00	7.20	2.00	0.00	6.40	0.02	0.00
7.22	2.00	0.00	6.39	0.02	0.00	7.24	2.00	0.00	6.38	0.02	0.00
7.26	2.00	0.00	6.37	0.02	0.00	7.28	2.00	0.00	6.36	0.02	0.00
7.30	2.00	0.00	6.35	0.02	0.00	7.32	2.00	0.00	6.34	0.02	0.00
7.34	2.00	0.00	6.33	0.02	0.00	7.36	2.00	0.00	6.32	0.02	0.00
7.38	2.00	0.00	6.31	0.02	0.00	7.40	2.00	0.00	6.30	0.02	0.00
7.42	2.00	0.00	6.29	0.02	0.00	7.44	2.00	0.00	6.28	0.02	0.00
7.46	2.00	0.00	6.27	0.02	0.00	7.48	2.00	0.00	6.26	0.02	0.00
7.50	2.00	0.00	6.25	0.02	0.00	7.52	2.00	0.00	6.24	0.02	0.00
7.54	2.00	0.00	6.23	0.02	0.00	7.56	2.00	0.00	6.22	0.02	0.00
7.58	2.00	0.00	6.21	0.02	0.00	7.60	2.00	0.00	6.20	0.02	0.00
7.62	2.00	0.00	6.19	0.02	0.00	7.64	2.00	0.00	6.18	0.02	0.00
7.66	2.00	0.00	6.17	0.02	0.00	7.68	2.00	0.00	6.16	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
7.70	2.00	0.00	6.15	0.02	0.00	7.72	2.00	0.00	6.14	0.02	0.00
7.74	2.00	0.00	6.13	0.02	0.00	7.76	2.00	0.00	6.12	0.02	0.00
7.78	2.00	0.00	6.11	0.02	0.00	7.81	2.00	0.00	6.10	0.03	0.00
7.82	2.00	0.00	6.09	0.01	0.00	7.84	2.00	0.00	6.08	0.02	0.00
7.86	2.00	0.00	6.07	0.02	0.00	7.88	2.00	0.00	6.06	0.02	0.00
7.90	2.00	0.00	6.05	0.02	0.00	7.92	2.00	0.00	6.04	0.02	0.00
7.94	2.00	0.00	6.03	0.02	0.00	7.96	2.00	0.00	6.02	0.02	0.00
7.99	2.00	0.00	6.01	0.03	0.00	8.00	2.00	0.00	6.00	0.01	0.00
8.02	2.00	0.00	5.99	0.02	0.00	8.04	2.00	0.00	5.98	0.02	0.00
8.06	2.00	0.00	5.97	0.02	0.00	8.08	2.00	0.00	5.96	0.02	0.00
8.10	2.00	0.00	5.95	0.02	0.00	8.12	2.00	0.00	5.94	0.02	0.00
8.14	2.00	0.00	5.93	0.02	0.00	8.16	2.00	0.00	5.92	0.02	0.00
8.18	2.00	0.00	5.91	0.02	0.00	8.20	2.00	0.00	5.90	0.02	0.00
8.22	2.00	0.00	5.89	0.02	0.00	8.24	2.00	0.00	5.88	0.02	0.00
8.26	2.00	0.00	5.87	0.02	0.00	8.28	2.00	0.00	5.86	0.02	0.00
8.30	2.00	0.00	5.85	0.02	0.00	8.32	2.00	0.00	5.84	0.02	0.00
8.34	2.00	0.00	5.83	0.02	0.00	8.36	2.00	0.00	5.82	0.02	0.00
8.38	2.00	0.00	5.81	0.02	0.00	8.40	2.00	0.00	5.80	0.02	0.00
8.42	2.00	0.00	5.79	0.02	0.00	8.44	2.00	0.00	5.78	0.02	0.00
8.46	2.00	0.00	5.77	0.02	0.00	8.48	2.00	0.00	5.76	0.02	0.00
8.50	2.00	0.00	5.75	0.02	0.00	8.52	2.00	0.00	5.74	0.02	0.00
8.54	2.00	0.00	5.73	0.02	0.00	8.56	2.00	0.00	5.72	0.02	0.00
8.58	2.00	0.00	5.71	0.02	0.00	8.60	2.00	0.00	5.70	0.02	0.00
8.62	2.00	0.00	5.69	0.02	0.00	8.64	2.00	0.00	5.68	0.02	0.00
8.66	2.00	0.00	5.67	0.02	0.00	8.68	2.00	0.00	5.66	0.02	0.00
8.70	2.00	0.00	5.65	0.02	0.00	8.72	2.00	0.00	5.64	0.02	0.00
8.74	2.00	0.00	5.63	0.02	0.00	8.76	2.00	0.00	5.62	0.02	0.00
8.78	2.00	0.00	5.61	0.02	0.00	8.80	2.00	0.00	5.60	0.02	0.00
8.82	2.00	0.00	5.59	0.02	0.00	8.85	2.00	0.00	5.58	0.03	0.00
8.86	2.00	0.00	5.57	0.01	0.00	8.88	2.00	0.00	5.56	0.02	0.00
8.90	2.00	0.00	5.55	0.02	0.00	8.92	2.00	0.00	5.54	0.02	0.00
8.94	2.00	0.00	5.53	0.02	0.00	8.96	2.00	0.00	5.52	0.02	0.00
8.98	2.00	0.00	5.51	0.02	0.00	9.00	2.00	0.00	5.50	0.02	0.00
9.02	2.00	0.00	5.49	0.02	0.00	9.05	2.00	0.00	5.47	0.03	0.00
9.07	2.00	0.00	5.47	0.02	0.00	9.08	2.00	0.00	5.46	0.01	0.00
9.10	2.00	0.00	5.45	0.02	0.00	9.12	2.00	0.00	5.44	0.02	0.00
9.15	2.00	0.00	5.43	0.03	0.00	9.16	2.00	0.00	5.42	0.01	0.00
9.18	2.00	0.00	5.41	0.02	0.00	9.20	2.00	0.00	5.40	0.02	0.00
9.22	2.00	0.00	5.39	0.02	0.00	9.24	2.00	0.00	5.38	0.02	0.00
9.26	2.00	0.00	5.37	0.02	0.00	9.29	2.00	0.00	5.36	0.03	0.00
9.31	2.00	0.00	5.35	0.02	0.00	9.32	2.00	0.00	5.34	0.01	0.00
9.34	2.00	0.00	5.33	0.02	0.00	9.36	2.00	0.00	5.32	0.02	0.00
9.38	2.00	0.00	5.31	0.02	0.00	9.40	2.00	0.00	5.30	0.02	0.00
9.42	2.00	0.00	5.29	0.02	0.00	9.44	2.00	0.00	5.28	0.02	0.00
9.46	2.00	0.00	5.27	0.02	0.00	9.48	2.00	0.00	5.26	0.02	0.00
9.50	2.00	0.00	5.25	0.02	0.00	9.52	2.00	0.00	5.24	0.02	0.00
9.54	2.00	0.00	5.23	0.02	0.00	9.56	2.00	0.00	5.22	0.02	0.00
9.58	2.00	0.00	5.21	0.02	0.00	9.60	2.00	0.00	5.20	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
9.62	2.00	0.00	5.19	0.02	0.00	9.64	2.00	0.00	5.18	0.02	0.00
9.66	2.00	0.00	5.17	0.02	0.00	9.68	2.00	0.00	5.16	0.02	0.00
9.70	2.00	0.00	5.15	0.02	0.00	9.72	2.00	0.00	5.14	0.02	0.00
9.74	2.00	0.00	5.13	0.02	0.00	9.76	2.00	0.00	5.12	0.02	0.00
9.78	2.00	0.00	5.11	0.02	0.00	9.80	2.00	0.00	5.10	0.02	0.00
9.82	2.00	0.00	5.09	0.02	0.00	9.85	2.00	0.00	5.08	0.03	0.00
9.86	2.00	0.00	5.07	0.01	0.00	9.88	2.00	0.00	5.06	0.02	0.00
9.90	2.00	0.00	5.05	0.02	0.00	9.92	2.00	0.00	5.04	0.02	0.00
9.94	2.00	0.00	5.03	0.02	0.00	9.96	2.00	0.00	5.02	0.02	0.00
9.98	2.00	0.00	5.01	0.02	0.00	10.00	2.00	0.00	5.00	0.02	0.00
10.02	2.00	0.00	4.99	0.02	0.00	10.04	2.00	0.00	4.98	0.02	0.00
10.06	2.00	0.00	4.97	0.02	0.00	10.08	2.00	0.00	4.96	0.02	0.00
10.10	2.00	0.00	4.95	0.02	0.00	10.12	2.00	0.00	4.94	0.02	0.00
10.14	2.00	0.00	4.93	0.02	0.00	10.16	2.00	0.00	4.92	0.02	0.00
10.18	2.00	0.00	4.91	0.02	0.00	10.20	2.00	0.00	4.90	0.02	0.00
10.22	2.00	0.00	4.89	0.02	0.00	10.24	2.00	0.00	4.88	0.02	0.00
10.26	2.00	0.00	4.87	0.02	0.00	10.28	2.00	0.00	4.86	0.02	0.00
10.30	2.00	0.00	4.85	0.02	0.00	10.32	2.00	0.00	4.84	0.02	0.00
10.34	2.00	0.00	4.83	0.02	0.00	10.36	2.00	0.00	4.82	0.02	0.00
10.38	2.00	0.00	4.81	0.02	0.00	10.40	2.00	0.00	4.80	0.02	0.00
10.42	2.00	0.00	4.79	0.02	0.00	10.44	2.00	0.00	4.78	0.02	0.00
10.46	2.00	0.00	4.77	0.02	0.00	10.48	2.00	0.00	4.76	0.02	0.00
10.50	2.00	0.00	4.75	0.02	0.00	10.52	2.00	0.00	4.74	0.02	0.00
10.54	2.00	0.00	4.73	0.02	0.00	10.56	2.00	0.00	4.72	0.02	0.00
10.58	2.00	0.00	4.71	0.02	0.00	10.60	2.00	0.00	4.70	0.02	0.00
10.62	2.00	0.00	4.69	0.02	0.00	10.64	2.00	0.00	4.68	0.02	0.00
10.66	2.00	0.00	4.67	0.02	0.00	10.68	2.00	0.00	4.66	0.02	0.00
10.70	2.00	0.00	4.65	0.02	0.00	10.72	2.00	0.00	4.64	0.02	0.00
10.74	2.00	0.00	4.63	0.02	0.00	10.77	2.00	0.00	4.62	0.03	0.00
10.78	2.00	0.00	4.61	0.01	0.00	10.80	2.00	0.00	4.60	0.02	0.00
10.82	2.00	0.00	4.59	0.02	0.00	10.84	2.00	0.00	4.58	0.02	0.00
10.86	2.00	0.00	4.57	0.02	0.00	10.88	2.00	0.00	4.56	0.02	0.00
10.91	2.00	0.00	4.55	0.03	0.00	10.92	2.00	0.00	4.54	0.01	0.00
10.95	2.00	0.00	4.53	0.03	0.00	10.96	2.00	0.00	4.52	0.01	0.00
10.98	2.00	0.00	4.51	0.02	0.00	11.00	2.00	0.00	4.50	0.02	0.00
11.02	2.00	0.00	4.49	0.02	0.00	11.04	2.00	0.00	4.48	0.02	0.00
11.06	2.00	0.00	4.47	0.02	0.00	11.09	2.00	0.00	4.46	0.03	0.00
11.10	2.00	0.00	4.45	0.01	0.00	11.13	2.00	0.00	4.43	0.03	0.00
11.15	2.00	0.00	4.43	0.02	0.00	11.16	2.00	0.00	4.42	0.01	0.00
11.18	2.00	0.00	4.41	0.02	0.00	11.20	2.00	0.00	4.40	0.02	0.00
11.22	2.00	0.00	4.39	0.02	0.00	11.24	2.00	0.00	4.38	0.02	0.00
11.26	2.00	0.00	4.37	0.02	0.00	11.28	2.00	0.00	4.36	0.02	0.00
11.30	2.00	0.00	4.35	0.02	0.00	11.32	2.00	0.00	4.34	0.02	0.00
11.34	2.00	0.00	4.33	0.02	0.00	11.36	2.00	0.00	4.32	0.02	0.00
11.38	2.00	0.00	4.31	0.02	0.00	11.40	2.00	0.00	4.30	0.02	0.00
11.42	2.00	0.00	4.29	0.02	0.00	11.44	2.00	0.00	4.28	0.02	0.00
11.46	2.00	0.00	4.27	0.02	0.00	11.48	2.00	0.00	4.26	0.02	0.00
11.50	2.00	0.00	4.25	0.02	0.00	11.52	2.00	0.00	4.24	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
11.54	2.00	0.00	4.23	0.02	0.00	11.56	2.00	0.00	4.22	0.02	0.00
11.58	2.00	0.00	4.21	0.02	0.00	11.60	2.00	0.00	4.20	0.02	0.00
11.62	2.00	0.00	4.19	0.02	0.00	11.64	2.00	0.00	4.18	0.02	0.00
11.66	2.00	0.00	4.17	0.02	0.00	11.68	2.00	0.00	4.16	0.02	0.00
11.70	2.00	0.00	4.15	0.02	0.00	11.72	2.00	0.00	4.14	0.02	0.00
11.74	2.00	0.00	4.13	0.02	0.00	11.76	2.00	0.00	4.12	0.02	0.00
11.78	2.00	0.00	4.11	0.02	0.00	11.80	2.00	0.00	4.10	0.02	0.00
11.82	2.00	0.00	4.09	0.02	0.00	11.84	2.00	0.00	4.08	0.02	0.00
11.86	2.00	0.00	4.07	0.02	0.00	11.88	2.00	0.00	4.06	0.02	0.00
11.90	2.00	0.00	4.05	0.02	0.00	11.92	2.00	0.00	4.04	0.02	0.00
11.94	2.00	0.00	4.03	0.02	0.00	11.96	2.00	0.00	4.02	0.02	0.00
11.98	2.00	0.00	4.01	0.02	0.00	12.00	2.00	0.00	4.00	0.02	0.00
12.02	2.00	0.00	3.99	0.02	0.00	12.04	2.00	0.00	3.98	0.02	0.00
12.06	2.00	0.00	3.97	0.02	0.00	12.08	2.00	0.00	3.96	0.02	0.00
12.10	2.00	0.00	3.95	0.02	0.00	12.12	2.00	0.00	3.94	0.02	0.00
12.14	2.00	0.00	3.93	0.02	0.00	12.16	2.00	0.00	3.92	0.02	0.00
12.18	2.00	0.00	3.91	0.02	0.00	12.20	2.00	0.00	3.90	0.02	0.00
12.22	2.00	0.00	3.89	0.02	0.00	12.24	2.00	0.00	3.88	0.02	0.00
12.27	2.00	0.00	3.87	0.03	0.00	12.28	2.00	0.00	3.86	0.01	0.00
12.30	2.00	0.00	3.85	0.02	0.00	12.32	2.00	0.00	3.84	0.02	0.00
12.34	2.00	0.00	3.83	0.02	0.00	12.36	2.00	0.00	3.82	0.02	0.00
12.38	2.00	0.00	3.81	0.02	0.00	12.40	2.00	0.00	3.80	0.02	0.00
12.42	2.00	0.00	3.79	0.02	0.00	12.44	2.00	0.00	3.78	0.02	0.00
12.46	2.00	0.00	3.77	0.02	0.00	12.48	2.00	0.00	3.76	0.02	0.00
12.50	2.00	0.00	3.75	0.02	0.00	12.52	2.00	0.00	3.74	0.02	0.00
12.54	2.00	0.00	3.73	0.02	0.00	12.56	2.00	0.00	3.72	0.02	0.00
12.58	2.00	0.00	3.71	0.02	0.00	12.60	2.00	0.00	3.70	0.02	0.00
12.62	2.00	0.00	3.69	0.02	0.00	12.64	2.00	0.00	3.68	0.02	0.00
12.66	2.00	0.00	3.67	0.02	0.00	12.68	2.00	0.00	3.66	0.02	0.00
12.70	2.00	0.00	3.65	0.02	0.00	12.72	2.00	0.00	3.64	0.02	0.00
12.74	2.00	0.00	3.63	0.02	0.00	12.76	2.00	0.00	3.62	0.02	0.00
12.78	2.00	0.00	3.61	0.02	0.00	12.80	2.00	0.00	3.60	0.02	0.00
12.82	2.00	0.00	3.59	0.02	0.00	12.84	2.00	0.00	3.58	0.02	0.00
12.86	2.00	0.00	3.57	0.02	0.00	12.88	2.00	0.00	3.56	0.02	0.00
12.90	2.00	0.00	3.55	0.02	0.00	12.94	2.00	0.00	3.53	0.04	0.00
12.94	2.00	0.00	3.53	0.00	0.00	12.96	2.00	0.00	3.52	0.02	0.00
12.99	2.00	0.00	3.51	0.03	0.00	13.00	2.00	0.00	3.50	0.01	0.00
13.03	2.00	0.00	3.49	0.03	0.00	13.04	2.00	0.00	3.48	0.01	0.00
13.06	2.00	0.00	3.47	0.02	0.00	13.08	2.00	0.00	3.46	0.02	0.00
13.10	2.00	0.00	3.45	0.02	0.00	13.13	2.00	0.00	3.44	0.03	0.00
13.14	2.00	0.00	3.43	0.01	0.00	13.16	2.00	0.00	3.42	0.02	0.00
13.18	2.00	0.00	3.41	0.02	0.00	13.20	2.00	0.00	3.40	0.02	0.00
13.22	2.00	0.00	3.39	0.02	0.00	13.24	2.00	0.00	3.38	0.02	0.00
13.26	2.00	0.00	3.37	0.02	0.00	13.28	2.00	0.00	3.36	0.02	0.00
13.30	2.00	0.00	3.35	0.02	0.00	13.32	2.00	0.00	3.34	0.02	0.00
13.34	2.00	0.00	3.33	0.02	0.00	13.36	2.00	0.00	3.32	0.02	0.00
13.38	2.00	0.00	3.31	0.02	0.00	13.40	2.00	0.00	3.30	0.02	0.00
13.42	2.00	0.00	3.29	0.02	0.00	13.44	2.00	0.00	3.28	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
13.46	2.00	0.00	3.27	0.02	0.00	13.48	2.00	0.00	3.26	0.02	0.00
13.50	2.00	0.00	3.25	0.02	0.00	13.52	2.00	0.00	3.24	0.02	0.00
13.54	2.00	0.00	3.23	0.02	0.00	13.56	2.00	0.00	3.22	0.02	0.00
13.58	2.00	0.00	3.21	0.02	0.00	13.60	2.00	0.00	3.20	0.02	0.00
13.62	2.00	0.00	3.19	0.02	0.00	13.64	2.00	0.00	3.18	0.02	0.00
13.66	2.00	0.00	3.17	0.02	0.00	13.68	2.00	0.00	3.16	0.02	0.00
13.70	2.00	0.00	3.15	0.02	0.00	13.72	2.00	0.00	3.14	0.02	0.00
13.74	2.00	0.00	3.13	0.02	0.00	13.76	2.00	0.00	3.12	0.02	0.00
13.79	2.00	0.00	3.11	0.03	0.00	13.80	2.00	0.00	3.10	0.01	0.00
13.82	2.00	0.00	3.09	0.02	0.00	13.85	2.00	0.00	3.08	0.03	0.00
13.86	2.00	0.00	3.07	0.01	0.00	13.88	2.00	0.00	3.06	0.02	0.00
13.90	2.00	0.00	3.05	0.02	0.00	13.92	2.00	0.00	3.04	0.02	0.00
13.94	2.00	0.00	3.03	0.02	0.00	13.96	2.00	0.00	3.02	0.02	0.00
13.98	2.00	0.00	3.01	0.02	0.00	14.00	2.00	0.00	3.00	0.02	0.00
14.02	2.00	0.00	2.99	0.02	0.00	14.04	2.00	0.00	2.98	0.02	0.00
14.06	2.00	0.00	2.97	0.02	0.00	14.08	2.00	0.00	2.96	0.02	0.00
14.10	2.00	0.00	2.95	0.02	0.00	14.12	2.00	0.00	2.94	0.02	0.00
14.14	2.00	0.00	2.93	0.02	0.00	14.16	2.00	0.00	2.92	0.02	0.00
14.18	2.00	0.00	2.91	0.02	0.00	14.20	2.00	0.00	2.90	0.02	0.00
14.22	2.00	0.00	2.89	0.02	0.00	14.24	2.00	0.00	2.88	0.02	0.00
14.26	2.00	0.00	2.87	0.02	0.00	14.28	2.00	0.00	2.86	0.02	0.00
14.30	2.00	0.00	2.85	0.02	0.00	14.32	2.00	0.00	2.84	0.02	0.00
14.34	2.00	0.00	2.83	0.02	0.00	14.36	2.00	0.00	2.82	0.02	0.00
14.38	2.00	0.00	2.81	0.02	0.00	14.40	2.00	0.00	2.80	0.02	0.00
14.42	2.00	0.00	2.79	0.02	0.00	14.44	2.00	0.00	2.78	0.02	0.00
14.46	2.00	0.00	2.77	0.02	0.00	14.48	2.00	0.00	2.76	0.02	0.00
14.50	2.00	0.00	2.75	0.02	0.00	14.52	2.00	0.00	2.74	0.02	0.00
14.54	2.00	0.00	2.73	0.02	0.00	14.56	2.00	0.00	2.72	0.02	0.00
14.58	2.00	0.00	2.71	0.02	0.00	14.60	2.00	0.00	2.70	0.02	0.00
14.62	2.00	0.00	2.69	0.02	0.00	14.64	2.00	0.00	2.68	0.02	0.00
14.66	2.00	0.00	2.67	0.02	0.00	14.68	2.00	0.00	2.66	0.02	0.00
14.70	2.00	0.00	2.65	0.02	0.00	14.72	2.00	0.00	2.64	0.02	0.00
14.74	2.00	0.00	2.63	0.02	0.00	14.76	2.00	0.00	2.62	0.02	0.00
14.78	2.00	0.00	2.61	0.02	0.00	14.81	2.00	0.00	2.60	0.03	0.00
14.83	2.00	0.00	2.59	0.02	0.00	14.84	2.00	0.00	2.58	0.01	0.00
14.86	2.00	0.00	2.57	0.02	0.00	14.88	2.00	0.00	2.56	0.02	0.00
14.90	2.00	0.00	2.55	0.02	0.00	14.92	2.00	0.00	2.54	0.02	0.00
14.94	2.00	0.00	2.53	0.02	0.00	14.96	2.00	0.00	2.52	0.02	0.00
14.98	2.00	0.00	2.51	0.02	0.00	15.01	2.00	0.00	2.50	0.03	0.00
15.02	2.00	0.00	2.49	0.01	0.00	15.04	2.00	0.00	2.48	0.02	0.00
15.06	2.00	0.00	2.47	0.02	0.00	15.08	2.00	0.00	2.46	0.02	0.00
15.10	2.00	0.00	2.45	0.02	0.00	15.12	2.00	0.00	2.44	0.02	0.00
15.14	2.00	0.00	2.43	0.02	0.00	15.16	2.00	0.00	2.42	0.02	0.00
15.18	2.00	0.00	2.41	0.02	0.00	15.20	2.00	0.00	2.40	0.02	0.00
15.22	2.00	0.00	2.39	0.02	0.00	15.24	2.00	0.00	2.38	0.02	0.00
15.26	2.00	0.00	2.37	0.02	0.00	15.28	2.00	0.00	2.36	0.02	0.00
15.30	2.00	0.00	2.35	0.02	0.00	15.32	2.00	0.00	2.34	0.02	0.00
15.34	2.00	0.00	2.33	0.02	0.00	15.37	2.00	0.00	2.32	0.03	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
15.38	2.00	0.00	2.31	0.01	0.00	15.40	2.00	0.00	2.30	0.02	0.00
15.42	2.00	0.00	2.29	0.02	0.00	15.44	2.00	0.00	2.28	0.02	0.00
15.46	2.00	0.00	2.27	0.02	0.00	15.48	2.00	0.00	2.26	0.02	0.00
15.50	2.00	0.00	2.25	0.02	0.00	15.52	2.00	0.00	2.24	0.02	0.00
15.54	2.00	0.00	2.23	0.02	0.00	15.56	2.00	0.00	2.22	0.02	0.00
15.58	2.00	0.00	2.21	0.02	0.00	15.60	2.00	0.00	2.20	0.02	0.00
15.62	2.00	0.00	2.19	0.02	0.00	15.64	2.00	0.00	2.18	0.02	0.00
15.66	2.00	0.00	2.17	0.02	0.00	15.68	2.00	0.00	2.16	0.02	0.00
15.70	2.00	0.00	2.15	0.02	0.00	15.72	2.00	0.00	2.14	0.02	0.00
15.74	2.00	0.00	2.13	0.02	0.00	15.76	2.00	0.00	2.12	0.02	0.00
15.78	2.00	0.00	2.11	0.02	0.00	15.80	2.00	0.00	2.10	0.02	0.00
15.82	2.00	0.00	2.09	0.02	0.00	15.84	2.00	0.00	2.08	0.02	0.00
15.86	2.00	0.00	2.07	0.02	0.00	15.88	2.00	0.00	2.06	0.02	0.00
15.90	2.00	0.00	2.05	0.02	0.00	15.92	2.00	0.00	2.04	0.02	0.00
15.94	2.00	0.00	2.03	0.02	0.00	15.96	2.00	0.00	2.02	0.02	0.00
15.98	2.00	0.00	2.01	0.02	0.00	16.00	2.00	0.00	2.00	0.02	0.00
16.03	2.00	0.00	1.99	0.03	0.00	16.04	2.00	0.00	1.98	0.01	0.00
16.06	2.00	0.00	1.97	0.02	0.00	16.08	2.00	0.00	1.96	0.02	0.00
16.10	2.00	0.00	1.95	0.02	0.00	16.12	2.00	0.00	1.94	0.02	0.00
16.14	2.00	0.00	1.93	0.02	0.00	16.16	2.00	0.00	1.92	0.02	0.00
16.18	2.00	0.00	1.91	0.02	0.00	16.20	2.00	0.00	1.90	0.02	0.00
16.22	2.00	0.00	1.89	0.02	0.00	16.24	2.00	0.00	1.88	0.02	0.00
16.26	2.00	0.00	1.87	0.02	0.00	16.28	2.00	0.00	1.86	0.02	0.00
16.30	2.00	0.00	1.85	0.02	0.00	16.32	2.00	0.00	1.84	0.02	0.00
16.34	2.00	0.00	1.83	0.02	0.00	16.36	2.00	0.00	1.82	0.02	0.00
16.38	2.00	0.00	1.81	0.02	0.00	16.40	2.00	0.00	1.80	0.02	0.00
16.42	2.00	0.00	1.79	0.02	0.00	16.44	2.00	0.00	1.78	0.02	0.00
16.46	2.00	0.00	1.77	0.02	0.00	16.48	2.00	0.00	1.76	0.02	0.00
16.50	2.00	0.00	1.75	0.02	0.00	16.52	2.00	0.00	1.74	0.02	0.00
16.54	2.00	0.00	1.73	0.02	0.00	16.56	2.00	0.00	1.72	0.02	0.00
16.58	2.00	0.00	1.71	0.02	0.00	16.60	2.00	0.00	1.70	0.02	0.00
16.62	2.00	0.00	1.69	0.02	0.00	16.64	2.00	0.00	1.68	0.02	0.00
16.66	2.00	0.00	1.67	0.02	0.00	16.68	2.00	0.00	1.66	0.02	0.00
16.70	2.00	0.00	1.65	0.02	0.00	16.72	2.00	0.00	1.64	0.02	0.00
16.74	2.00	0.00	1.63	0.02	0.00	16.76	2.00	0.00	1.62	0.02	0.00
16.78	2.00	0.00	1.61	0.02	0.00	16.80	2.00	0.00	1.60	0.02	0.00
16.82	2.00	0.00	1.59	0.02	0.00	16.84	2.00	0.00	1.58	0.02	0.00
16.86	2.00	0.00	1.57	0.02	0.00	16.88	2.00	0.00	1.56	0.02	0.00
16.91	2.00	0.00	1.55	0.03	0.00	16.92	2.00	0.00	1.54	0.01	0.00
16.94	2.00	0.00	1.53	0.02	0.00	16.96	2.00	0.00	1.52	0.02	0.00
16.98	2.00	0.00	1.51	0.02	0.00	17.00	2.00	0.00	1.50	0.02	0.00
17.02	2.00	0.00	1.49	0.02	0.00	17.04	2.00	0.00	1.48	0.02	0.00
17.06	2.00	0.00	1.47	0.02	0.00	17.08	2.00	0.00	1.46	0.02	0.00
17.10	2.00	0.00	1.45	0.02	0.00	17.18	2.00	0.00	1.41	0.08	0.00
17.18	2.00	0.00	1.41	0.00	0.00	17.18	2.00	0.00	1.41	0.00	0.00
17.18	2.00	0.00	1.41	0.00	0.00	17.20	2.00	0.00	1.40	0.02	0.00
17.22	2.00	0.00	1.39	0.02	0.00	17.24	2.00	0.00	1.38	0.02	0.00
17.26	2.00	0.00	1.37	0.02	0.00	17.28	2.00	0.00	1.36	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
17.30	2.00	0.00	1.35	0.02	0.00	17.32	2.00	0.00	1.34	0.02	0.00
17.34	2.00	0.00	1.33	0.02	0.00	17.36	2.00	0.00	1.32	0.02	0.00
17.38	2.00	0.00	1.31	0.02	0.00	17.40	2.00	0.00	1.30	0.02	0.00
17.42	2.00	0.00	1.29	0.02	0.00	17.44	2.00	0.00	1.28	0.02	0.00
17.46	2.00	0.00	1.27	0.02	0.00	17.48	2.00	0.00	1.26	0.02	0.00
17.50	2.00	0.00	1.25	0.02	0.00	17.52	2.00	0.00	1.24	0.02	0.00
17.54	2.00	0.00	1.23	0.02	0.00	17.56	2.00	0.00	1.22	0.02	0.00
17.58	2.00	0.00	1.21	0.02	0.00	17.60	2.00	0.00	1.20	0.02	0.00
17.62	2.00	0.00	1.19	0.02	0.00	17.64	2.00	0.00	1.18	0.02	0.00
17.66	2.00	0.00	1.17	0.02	0.00	17.68	2.00	0.00	1.16	0.02	0.00
17.70	2.00	0.00	1.15	0.02	0.00	17.72	2.00	0.00	1.14	0.02	0.00
17.74	2.00	0.00	1.13	0.02	0.00	17.76	2.00	0.00	1.12	0.02	0.00
17.78	2.00	0.00	1.11	0.02	0.00	17.80	2.00	0.00	1.10	0.02	0.00
17.82	2.00	0.00	1.09	0.02	0.00	17.84	2.00	0.00	1.08	0.02	0.00
17.86	2.00	0.00	1.07	0.02	0.00	17.88	2.00	0.00	1.06	0.02	0.00
17.90	2.00	0.00	1.05	0.02	0.00	17.92	2.00	0.00	1.04	0.02	0.00
17.94	2.00	0.00	1.03	0.02	0.00	17.96	2.00	0.00	1.02	0.02	0.00
17.98	2.00	0.00	1.01	0.02	0.00	18.00	2.00	0.00	1.00	0.02	0.00
18.02	2.00	0.00	0.99	0.02	0.00	18.04	2.00	0.00	0.98	0.02	0.00
18.06	2.00	0.00	0.97	0.02	0.00	18.08	2.00	0.00	0.96	0.02	0.00
18.10	2.00	0.00	0.95	0.02	0.00	18.12	2.00	0.00	0.94	0.02	0.00
18.14	2.00	0.00	0.93	0.02	0.00	18.16	2.00	0.00	0.92	0.02	0.00
18.18	2.00	0.00	0.91	0.02	0.00	18.20	2.00	0.00	0.90	0.02	0.00
18.22	2.00	0.00	0.89	0.02	0.00	18.24	2.00	0.00	0.88	0.02	0.00
18.26	2.00	0.00	0.87	0.02	0.00	18.28	2.00	0.00	0.86	0.02	0.00
18.30	2.00	0.00	0.85	0.02	0.00	18.32	2.00	0.00	0.84	0.02	0.00
18.34	2.00	0.00	0.83	0.02	0.00	18.36	2.00	0.00	0.82	0.02	0.00
18.38	0.67	0.33	0.81	0.02	0.01	18.40	0.68	0.32	0.80	0.02	0.01
18.42	0.68	0.32	0.79	0.02	0.01	18.44	0.68	0.32	0.78	0.02	0.00
18.46	0.68	0.32	0.77	0.02	0.00	18.48	0.67	0.33	0.76	0.02	0.00
18.50	0.67	0.33	0.75	0.02	0.00	18.52	0.68	0.32	0.74	0.02	0.00
18.54	2.00	0.00	0.73	0.02	0.00	18.58	2.00	0.00	0.71	0.04	0.00
18.58	2.00	0.00	0.71	0.00	0.00	18.60	2.00	0.00	0.70	0.02	0.00
18.62	2.00	0.00	0.69	0.02	0.00	18.64	2.00	0.00	0.68	0.02	0.00
18.66	2.00	0.00	0.67	0.02	0.00	18.68	2.00	0.00	0.66	0.02	0.00
18.70	2.00	0.00	0.65	0.02	0.00	18.72	2.00	0.00	0.64	0.02	0.00
18.74	2.00	0.00	0.63	0.02	0.00	18.76	2.00	0.00	0.62	0.02	0.00
18.78	2.00	0.00	0.61	0.02	0.00	18.80	2.00	0.00	0.60	0.02	0.00
18.82	2.00	0.00	0.59	0.02	0.00	18.84	2.00	0.00	0.58	0.02	0.00
18.86	0.66	0.34	0.57	0.02	0.00	18.88	0.65	0.35	0.56	0.02	0.00
18.90	0.65	0.35	0.55	0.02	0.00	18.92	0.66	0.34	0.54	0.02	0.00
18.94	0.68	0.32	0.53	0.02	0.00	18.96	0.71	0.29	0.52	0.02	0.00
18.98	0.75	0.25	0.51	0.02	0.00	19.07	0.76	0.24	0.47	0.09	0.01
19.07	0.76	0.24	0.47	0.00	0.00	19.07	0.76	0.24	0.47	0.00	0.00
19.08	0.83	0.17	0.46	0.01	0.00	19.10	1.00	0.00	0.45	0.02	0.00
19.12	1.07	0.00	0.44	0.02	0.00	19.22	1.00	0.00	0.39	0.10	0.00
19.22	0.98	0.02	0.39	0.00	0.00	19.14	0.96	0.04	0.43	0.08	0.00
19.22	0.75	0.25	0.39	0.08	0.01	19.24	0.69	0.31	0.38	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
19.26	2.00	0.00	0.37	0.02	0.00	19.28	2.00	0.00	0.36	0.02	0.00
19.30	2.00	0.00	0.35	0.02	0.00	19.32	2.00	0.00	0.34	0.02	0.00
19.34	2.00	0.00	0.33	0.02	0.00	19.36	2.00	0.00	0.32	0.02	0.00
19.38	2.00	0.00	0.31	0.02	0.00	19.40	2.00	0.00	0.30	0.02	0.00
19.42	2.00	0.00	0.29	0.02	0.00	19.44	2.00	0.00	0.28	0.02	0.00
19.46	2.00	0.00	0.27	0.02	0.00	19.48	2.00	0.00	0.26	0.02	0.00
19.50	2.00	0.00	0.25	0.02	0.00	19.52	2.00	0.00	0.24	0.02	0.00
19.54	2.00	0.00	0.23	0.02	0.00	19.56	2.00	0.00	0.22	0.02	0.00
19.58	2.00	0.00	0.21	0.02	0.00	19.60	2.00	0.00	0.20	0.02	0.00
19.62	2.00	0.00	0.19	0.02	0.00	19.64	2.00	0.00	0.18	0.02	0.00
19.66	0.82	0.18	0.17	0.02	0.00	19.68	0.76	0.24	0.16	0.02	0.00
19.70	0.70	0.30	0.15	0.02	0.00	19.72	0.65	0.35	0.14	0.02	0.00
19.74	0.66	0.34	0.13	0.02	0.00	19.76	0.66	0.34	0.12	0.02	0.00
19.78	0.66	0.34	0.11	0.02	0.00	19.81	0.67	0.33	0.10	0.03	0.00
19.82	0.69	0.31	0.09	0.01	0.00	19.84	0.70	0.30	0.08	0.02	0.00
19.86	2.00	0.00	0.07	0.02	0.00	19.88	2.00	0.00	0.06	0.02	0.00
19.90	2.00	0.00	0.05	0.02	0.00	19.92	2.00	0.00	0.04	0.02	0.00
19.94	2.00	0.00	0.03	0.02	0.00	19.96	2.00	0.00	0.02	0.02	0.00
19.98	2.00	0.00	0.01	0.02	0.00	20.00	2.00	0.00	0.00	0.02	0.00
20.02	2.00	0.00	0.00	0.00	0.00	20.04	2.00	0.00	0.00	0.00	0.00
20.06	2.00	0.00	0.00	0.00	0.00	20.08	2.00	0.00	0.00	0.00	0.00
20.10	2.00	0.00	0.00	0.00	0.00	20.12	2.00	0.00	0.00	0.00	0.00
20.14	2.00	0.00	0.00	0.00	0.00	20.16	2.00	0.00	0.00	0.00	0.00
20.18	2.00	0.00	0.00	0.00	0.00	20.20	2.00	0.00	0.00	0.00	0.00
20.22	2.00	0.00	0.00	0.00	0.00	20.24	2.00	0.00	0.00	0.00	0.00
20.26	2.00	0.00	0.00	0.00	0.00	20.28	2.00	0.00	0.00	0.00	0.00
20.30	2.00	0.00	0.00	0.00	0.00	20.32	0.68	0.00	0.00	0.00	0.00
20.34	0.68	0.00	0.00	0.00	0.00	20.36	0.69	0.00	0.00	0.00	0.00
20.38	0.69	0.00	0.00	0.00	0.00	20.40	0.69	0.00	0.00	0.00	0.00
20.42	0.69	0.00	0.00	0.00	0.00	20.44	0.68	0.00	0.00	0.00	0.00
20.46	0.68	0.00	0.00	0.00	0.00	20.48	0.68	0.00	0.00	0.00	0.00
20.50	0.67	0.00	0.00	0.00	0.00	20.52	0.66	0.00	0.00	0.00	0.00
20.54	0.66	0.00	0.00	0.00	0.00						

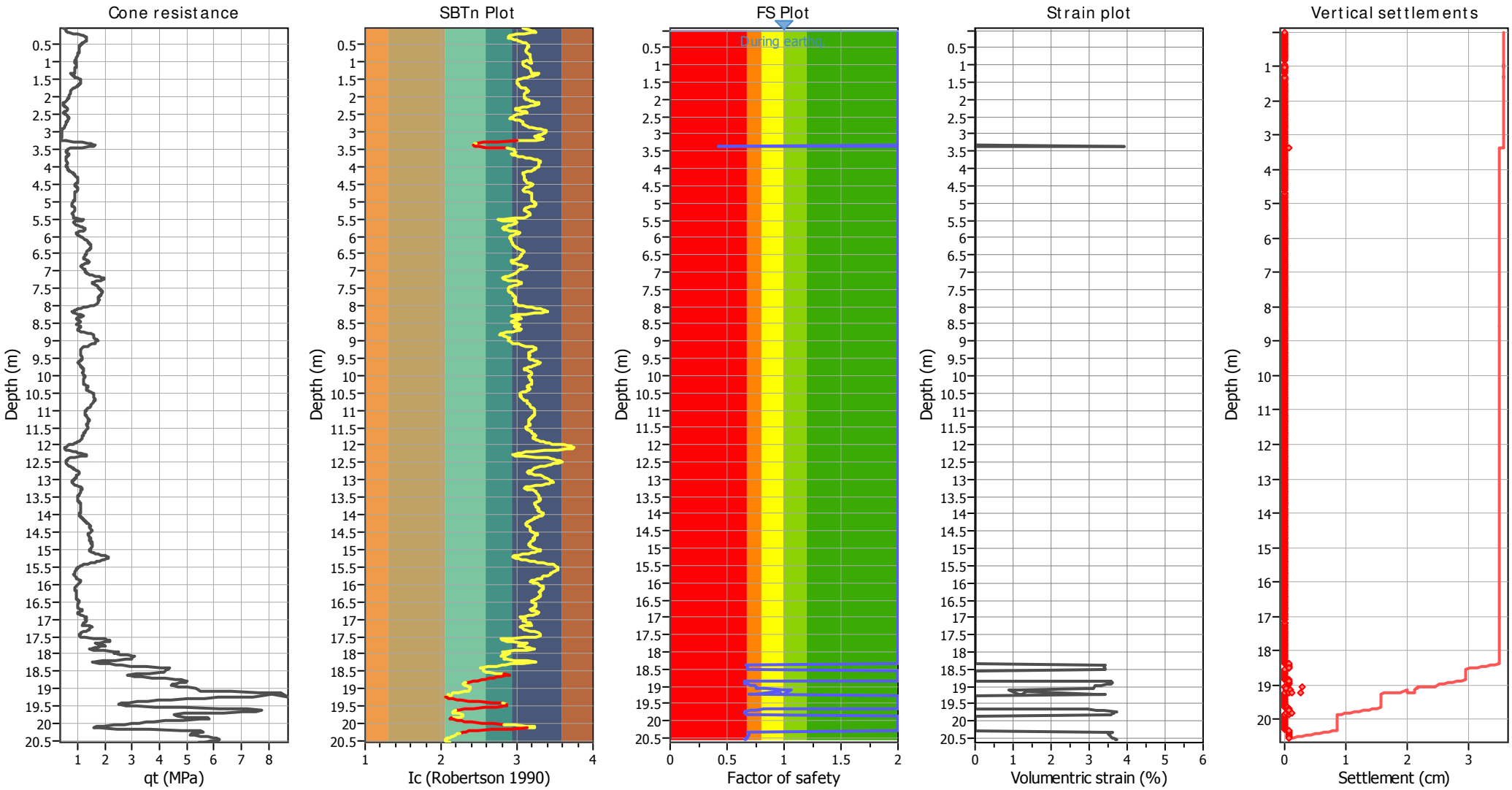
Overall liquefaction potential: 0.19

LPI = 0.00 - Liquefaction risk very low
LPI between 0.00 and 5.00 - Liquefaction risk low
LPI between 5.00 and 15.00 - Liquefaction risk high
LPI > 15.00 - Liquefaction risk very high

Abbreviations

FS: Calculated factor of safety for test point
F_L: 1 - FS
w_z: Function value of the extend of soil liquefaction according to depth
d_z: Layer thickness (m)
LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

q_t:	Total cone resistance (cone resistance q_c corrected for pore water effects)
I_c:	Soil Behaviour Type Index
FS:	Calculated Factor of Safety against liquefaction
Volumentric strain:	Post-liquefaction volumentric strain

:: Post-earthquake settlement due to soil liquefaction ::

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
0.02	7.96	2.00	0.00	1.00	0.00	0.05	9.01	2.00	0.00	1.00	0.00
0.06	10.23	2.00	0.00	1.00	0.00	0.08	10.11	2.00	0.00	1.00	0.00
0.10	9.83	2.00	0.00	1.00	0.00	0.12	9.91	2.00	0.00	1.00	0.00
0.14	9.96	2.00	0.00	1.00	0.00	0.16	10.96	2.00	0.00	1.00	0.00
0.18	13.98	2.00	0.00	1.00	0.00	0.20	17.28	2.00	0.00	1.00	0.00
0.22	19.32	2.00	0.00	1.00	0.00	0.24	21.06	2.00	0.00	1.00	0.00
0.26	21.35	2.00	0.00	1.00	0.00	0.28	22.56	2.00	0.00	1.00	0.00
0.30	22.77	2.00	0.00	1.00	0.00	0.32	22.43	2.00	0.00	1.00	0.00
0.34	21.89	2.00	0.00	1.00	0.00	0.36	21.93	2.00	0.00	1.00	0.00
0.38	22.06	2.00	0.00	1.00	0.00	0.40	21.63	2.00	0.00	1.00	0.00
0.42	20.57	2.00	0.00	1.00	0.00	0.44	19.97	2.00	0.00	1.00	0.00
0.46	19.53	2.00	0.00	1.00	0.00	0.48	19.53	2.00	0.00	1.00	0.00
0.50	18.81	2.00	0.00	1.00	0.00	0.52	18.44	2.00	0.00	1.00	0.00
0.54	17.83	2.00	0.00	1.00	0.00	0.56	17.84	2.00	0.00	1.00	0.00
0.58	17.93	2.00	0.00	1.00	0.00	0.60	18.06	2.00	0.00	1.00	0.00
0.62	18.03	2.00	0.00	1.00	0.00	0.64	18.05	2.00	0.00	1.00	0.00
0.66	18.53	2.00	0.00	1.00	0.00	0.68	18.08	2.00	0.00	1.00	0.00
0.70	17.83	2.00	0.00	1.00	0.00	0.72	17.65	2.00	0.00	1.00	0.00
0.74	17.16	2.00	0.00	1.00	0.00	0.76	16.79	2.00	0.00	1.00	0.00
0.78	16.85	2.00	0.00	1.00	0.00	0.80	16.52	2.00	0.00	1.00	0.00
0.82	16.50	2.00	0.00	1.00	0.00	0.84	16.36	2.00	0.00	1.00	0.00
1.04	15.15	2.00	0.00	1.00	0.00	1.04	15.15	2.00	0.00	1.00	0.00
1.04	14.92	2.00	0.00	1.00	0.00	1.04	14.92	2.00	0.00	1.00	0.00
1.04	14.92	2.00	0.00	1.00	0.00	0.96	15.42	2.00	0.00	1.00	0.00
0.98	16.00	2.00	0.00	1.00	0.00	1.00	15.95	2.00	0.00	1.00	0.00
1.02	16.10	2.00	0.00	1.00	0.00	1.04	16.01	2.00	0.00	1.00	0.00
1.06	16.23	2.00	0.00	1.00	0.00	1.08	16.53	2.00	0.00	1.00	0.00
1.10	16.47	2.00	0.00	1.00	0.00	1.12	16.50	2.00	0.00	1.00	0.00
1.14	15.96	2.00	0.00	1.00	0.00	1.16	15.55	2.00	0.00	1.00	0.00
1.18	15.22	2.00	0.00	1.00	0.00	1.20	14.97	2.00	0.00	1.00	0.00
1.32	14.92	2.00	0.00	1.00	0.00	1.32	14.92	2.00	0.00	1.00	0.00
1.32	14.73	2.00	0.00	1.00	0.00	1.32	14.73	2.00	0.00	1.00	0.00
1.30	13.26	2.00	0.00	1.00	0.00	1.32	12.88	2.00	0.00	1.00	0.00
1.34	12.77	2.00	0.00	1.00	0.00	1.36	12.91	2.00	0.00	1.00	0.00
1.38	13.15	2.00	0.00	1.00	0.00	1.40	14.06	2.00	0.00	1.00	0.00
1.42	14.62	2.00	0.00	1.00	0.00	1.44	15.53	2.00	0.00	1.00	0.00
1.46	16.60	2.00	0.00	1.00	0.00	1.49	18.01	2.00	0.00	1.00	0.00
1.50	19.01	2.00	0.00	1.00	0.00	1.53	18.91	2.00	0.00	1.00	0.00
1.54	19.28	2.00	0.00	1.00	0.00	1.56	18.97	2.00	0.00	1.00	0.00
1.58	18.91	2.00	0.00	1.00	0.00	1.60	18.60	2.00	0.00	1.00	0.00
1.62	18.43	2.00	0.00	1.00	0.00	1.64	17.58	2.00	0.00	1.00	0.00
1.66	17.09	2.00	0.00	1.00	0.00	1.68	16.40	2.00	0.00	1.00	0.00
1.70	16.11	2.00	0.00	1.00	0.00	1.72	15.43	2.00	0.00	1.00	0.00
1.74	14.39	2.00	0.00	1.00	0.00	1.76	13.99	2.00	0.00	1.00	0.00
1.78	13.50	2.00	0.00	1.00	0.00	1.80	13.28	2.00	0.00	1.00	0.00
1.82	12.68	2.00	0.00	1.00	0.00	1.84	12.27	2.00	0.00	1.00	0.00
1.86	11.35	2.00	0.00	1.00	0.00	1.88	12.29	2.00	0.00	1.00	0.00
1.91	12.56	2.00	0.00	1.00	0.00	1.92	12.05	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
1.94	11.77	2.00	0.00	1.00	0.00	1.96	11.57	2.00	0.00	1.00	0.00
1.98	11.33	2.00	0.00	1.00	0.00	2.00	11.21	2.00	0.00	1.00	0.00
2.02	10.93	2.00	0.00	1.00	0.00	2.04	10.92	2.00	0.00	1.00	0.00
2.06	10.53	2.00	0.00	1.00	0.00	2.08	9.94	2.00	0.00	1.00	0.00
2.10	9.66	2.00	0.00	1.00	0.00	2.13	9.03	2.00	0.00	1.00	0.00
2.14	8.63	2.00	0.00	1.00	0.00	2.16	8.31	2.00	0.00	1.00	0.00
2.18	7.71	2.00	0.00	1.00	0.00	2.20	7.32	2.00	0.00	1.00	0.00
2.22	7.50	2.00	0.00	1.00	0.00	2.24	7.76	2.00	0.00	1.00	0.00
2.26	8.10	2.00	0.00	1.00	0.00	2.28	8.80	2.00	0.00	1.00	0.00
2.30	9.45	2.00	0.00	1.00	0.00	2.32	10.26	2.00	0.00	1.00	0.00
2.34	10.95	2.00	0.00	1.00	0.00	2.37	10.98	2.00	0.00	1.00	0.00
2.38	10.00	2.00	0.00	1.00	0.00	2.42	9.80	2.00	0.00	1.00	0.00
2.42	7.95	2.00	0.00	1.00	0.00	2.44	7.78	2.00	0.00	1.00	0.00
2.46	8.24	2.00	0.00	1.00	0.00	2.48	8.93	2.00	0.00	1.00	0.00
2.50	9.94	2.00	0.00	1.00	0.00	2.52	10.20	2.00	0.00	1.00	0.00
2.54	10.50	2.00	0.00	1.00	0.00	2.56	10.41	2.00	0.00	1.00	0.00
2.58	10.72	2.00	0.00	1.00	0.00	2.60	11.53	2.00	0.00	1.00	0.00
2.62	11.44	2.00	0.00	1.00	0.00	2.64	11.47	2.00	0.00	1.00	0.00
2.66	10.56	2.00	0.00	1.00	0.00	2.68	10.27	2.00	0.00	1.00	0.00
2.70	9.95	2.00	0.00	1.00	0.00	2.72	9.82	2.00	0.00	1.00	0.00
2.74	9.61	2.00	0.00	1.00	0.00	2.76	9.92	2.00	0.00	1.00	0.00
2.78	10.06	2.00	0.00	1.00	0.00	2.80	9.51	2.00	0.00	1.00	0.00
2.82	8.75	2.00	0.00	1.00	0.00	2.84	8.62	2.00	0.00	1.00	0.00
2.86	9.19	2.00	0.00	1.00	0.00	2.89	8.44	2.00	0.00	1.00	0.00
2.90	7.93	2.00	0.00	1.00	0.00	2.92	7.03	2.00	0.00	1.00	0.00
2.94	6.79	2.00	0.00	1.00	0.00	2.96	6.67	2.00	0.00	1.00	0.00
2.99	6.43	2.00	0.00	1.00	0.00	3.00	6.62	2.00	0.00	1.00	0.00
3.03	6.50	2.00	0.00	1.00	0.00	3.05	6.33	2.00	0.00	1.00	0.00
3.06	6.48	2.00	0.00	1.00	0.00	3.08	6.24	2.00	0.00	1.00	0.00
3.10	6.51	2.00	0.00	1.00	0.00	3.12	7.01	2.00	0.00	1.00	0.00
3.14	7.16	2.00	0.00	1.00	0.00	3.16	6.96	2.00	0.00	1.00	0.00
3.18	6.68	2.00	0.00	1.00	0.00	3.20	5.78	2.00	0.00	1.00	0.00
3.22	5.73	2.00	0.00	1.00	0.00	3.24	6.15	2.00	0.00	1.00	0.00
3.26	8.06	2.00	0.00	1.00	0.00	3.28	13.79	2.00	0.00	1.00	0.00
3.30	75.88	2.00	0.00	1.00	0.00	3.32	78.48	2.00	0.00	1.00	0.00
3.34	79.71	2.00	0.00	1.00	0.00	3.36	81.83	0.43	3.92	1.00	0.08
3.38	83.18	2.00	0.00	1.00	0.00	3.40	83.47	2.00	0.00	1.00	0.00
3.42	79.77	2.00	0.00	1.00	0.00	3.44	19.57	2.00	0.00	1.00	0.00
3.46	14.38	2.00	0.00	1.00	0.00	3.48	11.84	2.00	0.00	1.00	0.00
3.50	10.31	2.00	0.00	1.00	0.00	3.52	9.87	2.00	0.00	1.00	0.00
3.54	10.13	2.00	0.00	1.00	0.00	3.56	9.81	2.00	0.00	1.00	0.00
3.58	9.41	2.00	0.00	1.00	0.00	3.60	9.32	2.00	0.00	1.00	0.00
3.62	10.68	2.00	0.00	1.00	0.00	3.64	11.14	2.00	0.00	1.00	0.00
3.66	11.17	2.00	0.00	1.00	0.00	3.68	10.50	2.00	0.00	1.00	0.00
3.70	10.02	2.00	0.00	1.00	0.00	3.72	9.98	2.00	0.00	1.00	0.00
3.74	9.66	2.00	0.00	1.00	0.00	3.76	9.96	2.00	0.00	1.00	0.00
3.78	9.44	2.00	0.00	1.00	0.00	3.80	9.52	2.00	0.00	1.00	0.00
3.82	9.81	2.00	0.00	1.00	0.00	3.84	9.80	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
3.86	9.84	2.00	0.00	1.00	0.00	3.88	10.08	2.00	0.00	1.00	0.00
3.90	9.96	2.00	0.00	1.00	0.00	3.92	10.38	2.00	0.00	1.00	0.00
3.94	10.06	2.00	0.00	1.00	0.00	3.96	9.74	2.00	0.00	1.00	0.00
3.98	9.85	2.00	0.00	1.00	0.00	4.00	9.88	2.00	0.00	1.00	0.00
4.02	9.80	2.00	0.00	1.00	0.00	4.04	10.30	2.00	0.00	1.00	0.00
4.06	10.76	2.00	0.00	1.00	0.00	4.08	10.60	2.00	0.00	1.00	0.00
4.10	10.63	2.00	0.00	1.00	0.00	4.12	11.13	2.00	0.00	1.00	0.00
4.14	12.14	2.00	0.00	1.00	0.00	4.16	13.18	2.00	0.00	1.00	0.00
4.18	14.11	2.00	0.00	1.00	0.00	4.20	14.30	2.00	0.00	1.00	0.00
4.22	14.64	2.00	0.00	1.00	0.00	4.24	14.60	2.00	0.00	1.00	0.00
4.26	14.90	2.00	0.00	1.00	0.00	4.28	15.43	2.00	0.00	1.00	0.00
4.30	15.97	2.00	0.00	1.00	0.00	4.32	16.54	2.00	0.00	1.00	0.00
4.34	16.88	2.00	0.00	1.00	0.00	4.36	16.76	2.00	0.00	1.00	0.00
4.38	16.94	2.00	0.00	1.00	0.00	4.40	16.93	2.00	0.00	1.00	0.00
4.42	17.07	2.00	0.00	1.00	0.00	4.44	17.18	2.00	0.00	1.00	0.00
4.46	16.69	2.00	0.00	1.00	0.00	4.48	15.86	2.00	0.00	1.00	0.00
4.50	14.83	2.00	0.00	1.00	0.00	4.52	14.69	2.00	0.00	1.00	0.00
4.54	15.31	2.00	0.00	1.00	0.00	4.56	15.06	2.00	0.00	1.00	0.00
4.58	15.57	2.00	0.00	1.00	0.00	4.60	16.14	2.00	0.00	1.00	0.00
4.62	16.72	2.00	0.00	1.00	0.00	4.68	16.64	2.00	0.00	1.00	0.00
4.68	16.64	2.00	0.00	1.00	0.00	4.68	16.53	2.00	0.00	1.00	0.00
4.70	15.66	2.00	0.00	1.00	0.00	4.72	15.15	2.00	0.00	1.00	0.00
4.74	14.74	2.00	0.00	1.00	0.00	4.76	14.74	2.00	0.00	1.00	0.00
4.78	14.38	2.00	0.00	1.00	0.00	4.80	14.31	2.00	0.00	1.00	0.00
4.82	14.24	2.00	0.00	1.00	0.00	4.84	14.48	2.00	0.00	1.00	0.00
4.86	14.24	2.00	0.00	1.00	0.00	4.89	14.08	2.00	0.00	1.00	0.00
4.90	14.21	2.00	0.00	1.00	0.00	4.93	14.16	2.00	0.00	1.00	0.00
4.94	14.39	2.00	0.00	1.00	0.00	4.96	14.00	2.00	0.00	1.00	0.00
4.98	13.75	2.00	0.00	1.00	0.00	5.01	13.35	2.00	0.00	1.00	0.00
5.02	13.04	2.00	0.00	1.00	0.00	5.04	12.55	2.00	0.00	1.00	0.00
5.06	12.26	2.00	0.00	1.00	0.00	5.08	12.23	2.00	0.00	1.00	0.00
5.10	12.31	2.00	0.00	1.00	0.00	5.12	12.39	2.00	0.00	1.00	0.00
5.14	12.58	2.00	0.00	1.00	0.00	5.16	13.15	2.00	0.00	1.00	0.00
5.18	13.61	2.00	0.00	1.00	0.00	5.20	13.55	2.00	0.00	1.00	0.00
5.22	13.98	2.00	0.00	1.00	0.00	5.24	13.85	2.00	0.00	1.00	0.00
5.26	13.51	2.00	0.00	1.00	0.00	5.28	13.44	2.00	0.00	1.00	0.00
5.30	13.06	2.00	0.00	1.00	0.00	5.32	12.72	2.00	0.00	1.00	0.00
5.34	12.20	2.00	0.00	1.00	0.00	5.36	12.18	2.00	0.00	1.00	0.00
5.38	12.43	2.00	0.00	1.00	0.00	5.40	12.75	2.00	0.00	1.00	0.00
5.42	12.76	2.00	0.00	1.00	0.00	5.44	12.78	2.00	0.00	1.00	0.00
5.46	11.85	2.00	0.00	1.00	0.00	5.48	13.14	2.00	0.00	1.00	0.00
5.51	17.94	2.00	0.00	1.00	0.00	5.52	19.30	2.00	0.00	1.00	0.00
5.54	17.70	2.00	0.00	1.00	0.00	5.56	14.65	2.00	0.00	1.00	0.00
5.58	12.99	2.00	0.00	1.00	0.00	5.60	12.73	2.00	0.00	1.00	0.00
5.62	12.57	2.00	0.00	1.00	0.00	5.64	12.51	2.00	0.00	1.00	0.00
5.66	13.28	2.00	0.00	1.00	0.00	5.68	13.94	2.00	0.00	1.00	0.00
5.70	14.70	2.00	0.00	1.00	0.00	5.72	15.57	2.00	0.00	1.00	0.00
5.74	16.97	2.00	0.00	1.00	0.00	5.76	18.35	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
5.78	18.48	2.00	0.00	1.00	0.00	5.80	17.42	2.00	0.00	1.00	0.00
5.82	19.99	2.00	0.00	1.00	0.00	5.84	17.24	2.00	0.00	1.00	0.00
5.86	15.07	2.00	0.00	1.00	0.00	5.88	13.98	2.00	0.00	1.00	0.00
5.90	13.72	2.00	0.00	1.00	0.00	5.92	13.96	2.00	0.00	1.00	0.00
5.94	13.96	2.00	0.00	1.00	0.00	5.96	14.54	2.00	0.00	1.00	0.00
5.98	15.12	2.00	0.00	1.00	0.00	6.00	15.92	2.00	0.00	1.00	0.00
6.02	16.19	2.00	0.00	1.00	0.00	6.04	16.49	2.00	0.00	1.00	0.00
6.06	17.11	2.00	0.00	1.00	0.00	6.08	17.37	2.00	0.00	1.00	0.00
6.10	17.73	2.00	0.00	1.00	0.00	6.12	18.44	2.00	0.00	1.00	0.00
6.14	18.92	2.00	0.00	1.00	0.00	6.16	19.43	2.00	0.00	1.00	0.00
6.18	19.58	2.00	0.00	1.00	0.00	6.20	19.51	2.00	0.00	1.00	0.00
6.22	20.14	2.00	0.00	1.00	0.00	6.24	20.41	2.00	0.00	1.00	0.00
6.26	20.66	2.00	0.00	1.00	0.00	6.28	20.74	2.00	0.00	1.00	0.00
6.30	20.85	2.00	0.00	1.00	0.00	6.32	20.45	2.00	0.00	1.00	0.00
6.34	20.38	2.00	0.00	1.00	0.00	6.36	19.86	2.00	0.00	1.00	0.00
6.38	19.37	2.00	0.00	1.00	0.00	6.40	18.98	2.00	0.00	1.00	0.00
6.42	18.33	2.00	0.00	1.00	0.00	6.44	17.94	2.00	0.00	1.00	0.00
6.46	18.24	2.00	0.00	1.00	0.00	6.48	17.85	2.00	0.00	1.00	0.00
6.50	17.72	2.00	0.00	1.00	0.00	6.52	17.89	2.00	0.00	1.00	0.00
6.54	17.66	2.00	0.00	1.00	0.00	6.56	17.52	2.00	0.00	1.00	0.00
6.58	17.01	2.00	0.00	1.00	0.00	6.60	16.89	2.00	0.00	1.00	0.00
6.62	16.63	2.00	0.00	1.00	0.00	6.64	16.50	2.00	0.00	1.00	0.00
6.66	16.90	2.00	0.00	1.00	0.00	6.68	17.65	2.00	0.00	1.00	0.00
6.70	18.46	2.00	0.00	1.00	0.00	6.72	18.67	2.00	0.00	1.00	0.00
6.74	19.26	2.00	0.00	1.00	0.00	6.76	18.42	2.00	0.00	1.00	0.00
6.78	16.94	2.00	0.00	1.00	0.00	6.80	16.42	2.00	0.00	1.00	0.00
6.82	15.57	2.00	0.00	1.00	0.00	6.84	14.92	2.00	0.00	1.00	0.00
6.86	14.53	2.00	0.00	1.00	0.00	6.88	14.67	2.00	0.00	1.00	0.00
6.90	15.11	2.00	0.00	1.00	0.00	6.92	15.67	2.00	0.00	1.00	0.00
6.94	16.13	2.00	0.00	1.00	0.00	6.96	16.56	2.00	0.00	1.00	0.00
6.98	16.65	2.00	0.00	1.00	0.00	7.00	16.56	2.00	0.00	1.00	0.00
7.02	16.62	2.00	0.00	1.00	0.00	7.04	16.89	2.00	0.00	1.00	0.00
7.06	17.41	2.00	0.00	1.00	0.00	7.08	17.74	2.00	0.00	1.00	0.00
7.10	18.49	2.00	0.00	1.00	0.00	7.12	19.84	2.00	0.00	1.00	0.00
7.14	21.48	2.00	0.00	1.00	0.00	7.16	22.97	2.00	0.00	1.00	0.00
7.18	24.43	2.00	0.00	1.00	0.00	7.20	24.95	2.00	0.00	1.00	0.00
7.22	25.08	2.00	0.00	1.00	0.00	7.24	24.71	2.00	0.00	1.00	0.00
7.26	24.02	2.00	0.00	1.00	0.00	7.28	22.74	2.00	0.00	1.00	0.00
7.30	21.14	2.00	0.00	1.00	0.00	7.32	20.34	2.00	0.00	1.00	0.00
7.34	19.56	2.00	0.00	1.00	0.00	7.36	19.67	2.00	0.00	1.00	0.00
7.38	20.01	2.00	0.00	1.00	0.00	7.40	20.96	2.00	0.00	1.00	0.00
7.42	21.70	2.00	0.00	1.00	0.00	7.44	21.87	2.00	0.00	1.00	0.00
7.46	22.32	2.00	0.00	1.00	0.00	7.48	22.19	2.00	0.00	1.00	0.00
7.50	22.44	2.00	0.00	1.00	0.00	7.52	22.66	2.00	0.00	1.00	0.00
7.54	23.02	2.00	0.00	1.00	0.00	7.56	23.33	2.00	0.00	1.00	0.00
7.58	24.17	2.00	0.00	1.00	0.00	7.60	23.82	2.00	0.00	1.00	0.00
7.62	23.23	2.00	0.00	1.00	0.00	7.64	23.42	2.00	0.00	1.00	0.00
7.66	22.95	2.00	0.00	1.00	0.00	7.68	22.62	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
7.70	22.87	2.00	0.00	1.00	0.00	7.72	22.80	2.00	0.00	1.00	0.00
7.74	22.31	2.00	0.00	1.00	0.00	7.76	21.98	2.00	0.00	1.00	0.00
7.78	21.52	2.00	0.00	1.00	0.00	7.81	21.57	2.00	0.00	1.00	0.00
7.82	22.38	2.00	0.00	1.00	0.00	7.84	22.21	2.00	0.00	1.00	0.00
7.86	21.75	2.00	0.00	1.00	0.00	7.88	21.35	2.00	0.00	1.00	0.00
7.90	20.98	2.00	0.00	1.00	0.00	7.92	21.22	2.00	0.00	1.00	0.00
7.94	21.24	2.00	0.00	1.00	0.00	7.96	20.70	2.00	0.00	1.00	0.00
7.99	19.63	2.00	0.00	1.00	0.00	8.00	18.11	2.00	0.00	1.00	0.00
8.02	16.37	2.00	0.00	1.00	0.00	8.04	14.75	2.00	0.00	1.00	0.00
8.06	13.35	2.00	0.00	1.00	0.00	8.08	12.35	2.00	0.00	1.00	0.00
8.10	11.70	2.00	0.00	1.00	0.00	8.12	10.99	2.00	0.00	1.00	0.00
8.14	10.49	2.00	0.00	1.00	0.00	8.16	9.61	2.00	0.00	1.00	0.00
8.18	9.42	2.00	0.00	1.00	0.00	8.20	9.94	2.00	0.00	1.00	0.00
8.22	10.51	2.00	0.00	1.00	0.00	8.24	11.73	2.00	0.00	1.00	0.00
8.26	13.69	2.00	0.00	1.00	0.00	8.28	15.31	2.00	0.00	1.00	0.00
8.30	15.05	2.00	0.00	1.00	0.00	8.32	13.10	2.00	0.00	1.00	0.00
8.34	11.63	2.00	0.00	1.00	0.00	8.36	11.40	2.00	0.00	1.00	0.00
8.38	11.06	2.00	0.00	1.00	0.00	8.40	11.31	2.00	0.00	1.00	0.00
8.42	12.58	2.00	0.00	1.00	0.00	8.44	13.30	2.00	0.00	1.00	0.00
8.46	13.10	2.00	0.00	1.00	0.00	8.48	12.29	2.00	0.00	1.00	0.00
8.50	11.65	2.00	0.00	1.00	0.00	8.52	11.48	2.00	0.00	1.00	0.00
8.54	11.09	2.00	0.00	1.00	0.00	8.56	12.11	2.00	0.00	1.00	0.00
8.58	13.13	2.00	0.00	1.00	0.00	8.60	13.29	2.00	0.00	1.00	0.00
8.62	12.90	2.00	0.00	1.00	0.00	8.64	12.20	2.00	0.00	1.00	0.00
8.66	11.56	2.00	0.00	1.00	0.00	8.68	11.25	2.00	0.00	1.00	0.00
8.70	11.44	2.00	0.00	1.00	0.00	8.72	11.67	2.00	0.00	1.00	0.00
8.74	12.60	2.00	0.00	1.00	0.00	8.76	14.08	2.00	0.00	1.00	0.00
8.78	15.36	2.00	0.00	1.00	0.00	8.80	18.13	2.00	0.00	1.00	0.00
8.82	18.11	2.00	0.00	1.00	0.00	8.85	18.00	2.00	0.00	1.00	0.00
8.86	17.97	2.00	0.00	1.00	0.00	8.88	18.51	2.00	0.00	1.00	0.00
8.90	18.11	2.00	0.00	1.00	0.00	8.92	17.87	2.00	0.00	1.00	0.00
8.94	18.73	2.00	0.00	1.00	0.00	8.96	19.86	2.00	0.00	1.00	0.00
8.98	19.46	2.00	0.00	1.00	0.00	9.00	19.46	2.00	0.00	1.00	0.00
9.02	18.81	2.00	0.00	1.00	0.00	9.05	18.72	2.00	0.00	1.00	0.00
9.07	18.91	2.00	0.00	1.00	0.00	9.08	18.44	2.00	0.00	1.00	0.00
9.10	17.26	2.00	0.00	1.00	0.00	9.12	16.21	2.00	0.00	1.00	0.00
9.15	15.38	2.00	0.00	1.00	0.00	9.16	14.55	2.00	0.00	1.00	0.00
9.18	13.62	2.00	0.00	1.00	0.00	9.20	13.01	2.00	0.00	1.00	0.00
9.22	12.72	2.00	0.00	1.00	0.00	9.24	12.48	2.00	0.00	1.00	0.00
9.26	12.70	2.00	0.00	1.00	0.00	9.29	12.40	2.00	0.00	1.00	0.00
9.31	12.32	2.00	0.00	1.00	0.00	9.32	12.33	2.00	0.00	1.00	0.00
9.34	12.28	2.00	0.00	1.00	0.00	9.36	12.29	2.00	0.00	1.00	0.00
9.38	12.35	2.00	0.00	1.00	0.00	9.40	12.54	2.00	0.00	1.00	0.00
9.42	12.33	2.00	0.00	1.00	0.00	9.44	12.53	2.00	0.00	1.00	0.00
9.46	12.54	2.00	0.00	1.00	0.00	9.48	12.68	2.00	0.00	1.00	0.00
9.50	13.00	2.00	0.00	1.00	0.00	9.52	13.17	2.00	0.00	1.00	0.00
9.54	12.70	2.00	0.00	1.00	0.00	9.56	12.35	2.00	0.00	1.00	0.00
9.58	12.12	2.00	0.00	1.00	0.00	9.60	11.63	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
9.62	11.17	2.00	0.00	1.00	0.00	9.64	10.94	2.00	0.00	1.00	0.00
9.66	11.14	2.00	0.00	1.00	0.00	9.68	11.80	2.00	0.00	1.00	0.00
9.70	11.79	2.00	0.00	1.00	0.00	9.72	12.14	2.00	0.00	1.00	0.00
9.74	12.39	2.00	0.00	1.00	0.00	9.76	12.43	2.00	0.00	1.00	0.00
9.78	12.46	2.00	0.00	1.00	0.00	9.80	13.53	2.00	0.00	1.00	0.00
9.82	13.23	2.00	0.00	1.00	0.00	9.85	13.00	2.00	0.00	1.00	0.00
9.86	13.28	2.00	0.00	1.00	0.00	9.88	13.14	2.00	0.00	1.00	0.00
9.90	12.94	2.00	0.00	1.00	0.00	9.92	12.77	2.00	0.00	1.00	0.00
9.94	12.86	2.00	0.00	1.00	0.00	9.96	12.86	2.00	0.00	1.00	0.00
9.98	13.10	2.00	0.00	1.00	0.00	10.00	13.24	2.00	0.00	1.00	0.00
10.02	13.32	2.00	0.00	1.00	0.00	10.04	13.59	2.00	0.00	1.00	0.00
10.06	13.23	2.00	0.00	1.00	0.00	10.08	13.29	2.00	0.00	1.00	0.00
10.10	13.30	2.00	0.00	1.00	0.00	10.12	13.13	2.00	0.00	1.00	0.00
10.14	12.91	2.00	0.00	1.00	0.00	10.16	13.01	2.00	0.00	1.00	0.00
10.18	13.12	2.00	0.00	1.00	0.00	10.20	12.95	2.00	0.00	1.00	0.00
10.22	12.93	2.00	0.00	1.00	0.00	10.24	12.84	2.00	0.00	1.00	0.00
10.26	12.95	2.00	0.00	1.00	0.00	10.28	13.53	2.00	0.00	1.00	0.00
10.30	14.19	2.00	0.00	1.00	0.00	10.32	14.65	2.00	0.00	1.00	0.00
10.34	14.23	2.00	0.00	1.00	0.00	10.36	14.01	2.00	0.00	1.00	0.00
10.38	13.77	2.00	0.00	1.00	0.00	10.40	13.75	2.00	0.00	1.00	0.00
10.42	13.88	2.00	0.00	1.00	0.00	10.44	14.21	2.00	0.00	1.00	0.00
10.46	14.77	2.00	0.00	1.00	0.00	10.48	15.37	2.00	0.00	1.00	0.00
10.50	16.15	2.00	0.00	1.00	0.00	10.52	16.61	2.00	0.00	1.00	0.00
10.54	16.64	2.00	0.00	1.00	0.00	10.56	16.37	2.00	0.00	1.00	0.00
10.58	16.20	2.00	0.00	1.00	0.00	10.60	16.63	2.00	0.00	1.00	0.00
10.62	16.89	2.00	0.00	1.00	0.00	10.64	16.69	2.00	0.00	1.00	0.00
10.66	16.87	2.00	0.00	1.00	0.00	10.68	16.95	2.00	0.00	1.00	0.00
10.70	16.95	2.00	0.00	1.00	0.00	10.72	16.46	2.00	0.00	1.00	0.00
10.74	16.32	2.00	0.00	1.00	0.00	10.77	16.29	2.00	0.00	1.00	0.00
10.78	16.42	2.00	0.00	1.00	0.00	10.80	16.11	2.00	0.00	1.00	0.00
10.82	15.67	2.00	0.00	1.00	0.00	10.84	15.31	2.00	0.00	1.00	0.00
10.86	15.07	2.00	0.00	1.00	0.00	10.88	15.17	2.00	0.00	1.00	0.00
10.91	14.97	2.00	0.00	1.00	0.00	10.92	14.46	2.00	0.00	1.00	0.00
10.95	14.10	2.00	0.00	1.00	0.00	10.96	13.48	2.00	0.00	1.00	0.00
10.98	13.63	2.00	0.00	1.00	0.00	11.00	13.42	2.00	0.00	1.00	0.00
11.02	13.18	2.00	0.00	1.00	0.00	11.04	12.97	2.00	0.00	1.00	0.00
11.06	12.95	2.00	0.00	1.00	0.00	11.09	13.04	2.00	0.00	1.00	0.00
11.10	12.89	2.00	0.00	1.00	0.00	11.13	12.81	2.00	0.00	1.00	0.00
11.15	13.15	2.00	0.00	1.00	0.00	11.16	13.12	2.00	0.00	1.00	0.00
11.18	13.20	2.00	0.00	1.00	0.00	11.20	13.40	2.00	0.00	1.00	0.00
11.22	13.77	2.00	0.00	1.00	0.00	11.24	13.73	2.00	0.00	1.00	0.00
11.26	13.88	2.00	0.00	1.00	0.00	11.28	14.34	2.00	0.00	1.00	0.00
11.30	14.16	2.00	0.00	1.00	0.00	11.32	13.88	2.00	0.00	1.00	0.00
11.34	13.98	2.00	0.00	1.00	0.00	11.36	13.90	2.00	0.00	1.00	0.00
11.38	13.60	2.00	0.00	1.00	0.00	11.40	13.28	2.00	0.00	1.00	0.00
11.42	13.02	2.00	0.00	1.00	0.00	11.44	13.22	2.00	0.00	1.00	0.00
11.46	14.00	2.00	0.00	1.00	0.00	11.48	13.93	2.00	0.00	1.00	0.00
11.50	13.70	2.00	0.00	1.00	0.00	11.52	13.62	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
11.54	13.34	2.00	0.00	1.00	0.00	11.56	13.17	2.00	0.00	1.00	0.00
11.58	12.89	2.00	0.00	1.00	0.00	11.60	12.48	2.00	0.00	1.00	0.00
11.62	12.37	2.00	0.00	1.00	0.00	11.64	12.27	2.00	0.00	1.00	0.00
11.66	12.14	2.00	0.00	1.00	0.00	11.68	12.27	2.00	0.00	1.00	0.00
11.70	12.00	2.00	0.00	1.00	0.00	11.72	11.66	2.00	0.00	1.00	0.00
11.74	11.44	2.00	0.00	1.00	0.00	11.76	10.71	2.00	0.00	1.00	0.00
11.78	11.83	2.00	0.00	1.00	0.00	11.80	11.65	2.00	0.00	1.00	0.00
11.82	11.22	2.00	0.00	1.00	0.00	11.84	10.88	2.00	0.00	1.00	0.00
11.86	10.73	2.00	0.00	1.00	0.00	11.88	10.23	2.00	0.00	1.00	0.00
11.90	9.80	2.00	0.00	1.00	0.00	11.92	9.42	2.00	0.00	1.00	0.00
11.94	8.62	2.00	0.00	1.00	0.00	11.96	8.06	2.00	0.00	1.00	0.00
11.98	7.40	2.00	0.00	1.00	0.00	12.00	6.61	2.00	0.00	1.00	0.00
12.02	6.10	2.00	0.00	1.00	0.00	12.04	5.75	2.00	0.00	1.00	0.00
12.06	5.26	2.00	0.00	1.00	0.00	12.08	5.00	2.00	0.00	1.00	0.00
12.10	4.93	2.00	0.00	1.00	0.00	12.12	4.90	2.00	0.00	1.00	0.00
12.14	5.26	2.00	0.00	1.00	0.00	12.16	6.40	2.00	0.00	1.00	0.00
12.18	7.80	2.00	0.00	1.00	0.00	12.20	9.17	2.00	0.00	1.00	0.00
12.22	9.53	2.00	0.00	1.00	0.00	12.24	10.68	2.00	0.00	1.00	0.00
12.27	12.26	2.00	0.00	1.00	0.00	12.28	13.30	2.00	0.00	1.00	0.00
12.30	13.18	2.00	0.00	1.00	0.00	12.32	10.96	2.00	0.00	1.00	0.00
12.34	8.51	2.00	0.00	1.00	0.00	12.36	6.42	2.00	0.00	1.00	0.00
12.38	5.90	2.00	0.00	1.00	0.00	12.40	6.08	2.00	0.00	1.00	0.00
12.42	5.72	2.00	0.00	1.00	0.00	12.44	5.83	2.00	0.00	1.00	0.00
12.46	5.38	2.00	0.00	1.00	0.00	12.48	4.97	2.00	0.00	1.00	0.00
12.50	4.92	2.00	0.00	1.00	0.00	12.52	5.24	2.00	0.00	1.00	0.00
12.54	5.65	2.00	0.00	1.00	0.00	12.56	5.62	2.00	0.00	1.00	0.00
12.58	5.83	2.00	0.00	1.00	0.00	12.60	6.09	2.00	0.00	1.00	0.00
12.62	6.77	2.00	0.00	1.00	0.00	12.64	7.38	2.00	0.00	1.00	0.00
12.66	7.71	2.00	0.00	1.00	0.00	12.68	8.09	2.00	0.00	1.00	0.00
12.70	8.27	2.00	0.00	1.00	0.00	12.72	8.67	2.00	0.00	1.00	0.00
12.74	9.09	2.00	0.00	1.00	0.00	12.76	9.46	2.00	0.00	1.00	0.00
12.78	10.00	2.00	0.00	1.00	0.00	12.80	9.77	2.00	0.00	1.00	0.00
12.82	9.62	2.00	0.00	1.00	0.00	12.84	9.37	2.00	0.00	1.00	0.00
12.86	9.23	2.00	0.00	1.00	0.00	12.88	8.89	2.00	0.00	1.00	0.00
12.90	8.43	2.00	0.00	1.00	0.00	12.94	8.46	2.00	0.00	1.00	0.00
12.94	8.57	2.00	0.00	1.00	0.00	12.96	8.25	2.00	0.00	1.00	0.00
12.99	7.93	2.00	0.00	1.00	0.00	13.00	7.70	2.00	0.00	1.00	0.00
13.03	7.53	2.00	0.00	1.00	0.00	13.04	7.12	2.00	0.00	1.00	0.00
13.06	7.14	2.00	0.00	1.00	0.00	13.08	7.06	2.00	0.00	1.00	0.00
13.10	7.39	2.00	0.00	1.00	0.00	13.13	7.49	2.00	0.00	1.00	0.00
13.14	8.05	2.00	0.00	1.00	0.00	13.16	8.58	2.00	0.00	1.00	0.00
13.18	9.43	2.00	0.00	1.00	0.00	13.20	9.88	2.00	0.00	1.00	0.00
13.22	10.59	2.00	0.00	1.00	0.00	13.24	10.67	2.00	0.00	1.00	0.00
13.26	10.48	2.00	0.00	1.00	0.00	13.28	10.29	2.00	0.00	1.00	0.00
13.30	9.91	2.00	0.00	1.00	0.00	13.32	9.83	2.00	0.00	1.00	0.00
13.34	9.91	2.00	0.00	1.00	0.00	13.36	9.75	2.00	0.00	1.00	0.00
13.38	9.70	2.00	0.00	1.00	0.00	13.40	9.73	2.00	0.00	1.00	0.00
13.42	9.37	2.00	0.00	1.00	0.00	13.44	9.17	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
13.46	9.07	2.00	0.00	1.00	0.00	13.48	9.11	2.00	0.00	1.00	0.00
13.50	9.23	2.00	0.00	1.00	0.00	13.52	9.05	2.00	0.00	1.00	0.00
13.54	8.82	2.00	0.00	1.00	0.00	13.56	8.68	2.00	0.00	1.00	0.00
13.58	8.63	2.00	0.00	1.00	0.00	13.60	8.86	2.00	0.00	1.00	0.00
13.62	9.07	2.00	0.00	1.00	0.00	13.64	9.48	2.00	0.00	1.00	0.00
13.66	9.64	2.00	0.00	1.00	0.00	13.68	9.70	2.00	0.00	1.00	0.00
13.70	9.71	2.00	0.00	1.00	0.00	13.72	9.64	2.00	0.00	1.00	0.00
13.74	9.76	2.00	0.00	1.00	0.00	13.76	9.84	2.00	0.00	1.00	0.00
13.79	9.78	2.00	0.00	1.00	0.00	13.80	9.67	2.00	0.00	1.00	0.00
13.82	9.62	2.00	0.00	1.00	0.00	13.85	9.76	2.00	0.00	1.00	0.00
13.86	9.73	2.00	0.00	1.00	0.00	13.88	9.98	2.00	0.00	1.00	0.00
13.90	10.21	2.00	0.00	1.00	0.00	13.92	9.66	2.00	0.00	1.00	0.00
13.94	9.58	2.00	0.00	1.00	0.00	13.96	9.33	2.00	0.00	1.00	0.00
13.98	8.98	2.00	0.00	1.00	0.00	14.00	9.03	2.00	0.00	1.00	0.00
14.02	9.21	2.00	0.00	1.00	0.00	14.04	9.46	2.00	0.00	1.00	0.00
14.06	9.65	2.00	0.00	1.00	0.00	14.08	10.11	2.00	0.00	1.00	0.00
14.10	10.19	2.00	0.00	1.00	0.00	14.12	10.14	2.00	0.00	1.00	0.00
14.14	10.36	2.00	0.00	1.00	0.00	14.16	10.74	2.00	0.00	1.00	0.00
14.18	10.88	2.00	0.00	1.00	0.00	14.20	11.11	2.00	0.00	1.00	0.00
14.22	11.40	2.00	0.00	1.00	0.00	14.24	11.88	2.00	0.00	1.00	0.00
14.26	11.95	2.00	0.00	1.00	0.00	14.28	12.44	2.00	0.00	1.00	0.00
14.30	12.60	2.00	0.00	1.00	0.00	14.32	12.78	2.00	0.00	1.00	0.00
14.34	12.77	2.00	0.00	1.00	0.00	14.36	12.50	2.00	0.00	1.00	0.00
14.38	12.68	2.00	0.00	1.00	0.00	14.40	12.82	2.00	0.00	1.00	0.00
14.42	13.06	2.00	0.00	1.00	0.00	14.44	13.22	2.00	0.00	1.00	0.00
14.46	13.14	2.00	0.00	1.00	0.00	14.48	13.13	2.00	0.00	1.00	0.00
14.50	12.90	2.00	0.00	1.00	0.00	14.52	12.50	2.00	0.00	1.00	0.00
14.54	12.23	2.00	0.00	1.00	0.00	14.56	11.73	2.00	0.00	1.00	0.00
14.58	11.72	2.00	0.00	1.00	0.00	14.60	12.13	2.00	0.00	1.00	0.00
14.62	12.39	2.00	0.00	1.00	0.00	14.64	12.25	2.00	0.00	1.00	0.00
14.66	12.40	2.00	0.00	1.00	0.00	14.68	12.60	2.00	0.00	1.00	0.00
14.70	12.71	2.00	0.00	1.00	0.00	14.72	12.87	2.00	0.00	1.00	0.00
14.74	11.27	2.00	0.00	1.00	0.00	14.76	13.20	2.00	0.00	1.00	0.00
14.78	13.07	2.00	0.00	1.00	0.00	14.81	12.76	2.00	0.00	1.00	0.00
14.83	12.87	2.00	0.00	1.00	0.00	14.84	12.97	2.00	0.00	1.00	0.00
14.86	13.06	2.00	0.00	1.00	0.00	14.88	13.01	2.00	0.00	1.00	0.00
14.90	13.08	2.00	0.00	1.00	0.00	14.92	12.90	2.00	0.00	1.00	0.00
14.94	12.91	2.00	0.00	1.00	0.00	14.96	12.81	2.00	0.00	1.00	0.00
14.98	12.50	2.00	0.00	1.00	0.00	15.01	12.15	2.00	0.00	1.00	0.00
15.02	11.81	2.00	0.00	1.00	0.00	15.04	11.84	2.00	0.00	1.00	0.00
15.06	12.20	2.00	0.00	1.00	0.00	15.08	12.77	2.00	0.00	1.00	0.00
15.10	13.44	2.00	0.00	1.00	0.00	15.12	14.10	2.00	0.00	1.00	0.00
15.14	14.69	2.00	0.00	1.00	0.00	15.16	16.13	2.00	0.00	1.00	0.00
15.18	17.14	2.00	0.00	1.00	0.00	15.20	17.98	2.00	0.00	1.00	0.00
15.22	18.24	2.00	0.00	1.00	0.00	15.24	18.10	2.00	0.00	1.00	0.00
15.26	17.33	2.00	0.00	1.00	0.00	15.28	16.90	2.00	0.00	1.00	0.00
15.30	16.11	2.00	0.00	1.00	0.00	15.32	15.29	2.00	0.00	1.00	0.00
15.34	14.94	2.00	0.00	1.00	0.00	15.37	13.26	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
15.38	12.72	2.00	0.00	1.00	0.00	15.40	10.99	2.00	0.00	1.00	0.00
15.42	10.20	2.00	0.00	1.00	0.00	15.44	9.65	2.00	0.00	1.00	0.00
15.46	9.54	2.00	0.00	1.00	0.00	15.48	9.14	2.00	0.00	1.00	0.00
15.50	8.74	2.00	0.00	1.00	0.00	15.52	8.28	2.00	0.00	1.00	0.00
15.54	7.85	2.00	0.00	1.00	0.00	15.56	7.72	2.00	0.00	1.00	0.00
15.58	7.51	2.00	0.00	1.00	0.00	15.60	7.31	2.00	0.00	1.00	0.00
15.62	7.34	2.00	0.00	1.00	0.00	15.64	7.30	2.00	0.00	1.00	0.00
15.66	7.29	2.00	0.00	1.00	0.00	15.68	7.11	2.00	0.00	1.00	0.00
15.70	7.09	2.00	0.00	1.00	0.00	15.72	6.89	2.00	0.00	1.00	0.00
15.74	6.35	2.00	0.00	1.00	0.00	15.76	7.33	2.00	0.00	1.00	0.00
15.78	7.71	2.00	0.00	1.00	0.00	15.80	7.54	2.00	0.00	1.00	0.00
15.82	7.60	2.00	0.00	1.00	0.00	15.84	7.70	2.00	0.00	1.00	0.00
15.86	7.98	2.00	0.00	1.00	0.00	15.88	8.41	2.00	0.00	1.00	0.00
15.90	8.67	2.00	0.00	1.00	0.00	15.92	8.97	2.00	0.00	1.00	0.00
15.94	8.92	2.00	0.00	1.00	0.00	15.96	8.48	2.00	0.00	1.00	0.00
15.98	7.94	2.00	0.00	1.00	0.00	16.00	7.66	2.00	0.00	1.00	0.00
16.03	7.56	2.00	0.00	1.00	0.00	16.04	7.40	2.00	0.00	1.00	0.00
16.06	7.20	2.00	0.00	1.00	0.00	16.08	7.02	2.00	0.00	1.00	0.00
16.10	6.99	2.00	0.00	1.00	0.00	16.12	7.07	2.00	0.00	1.00	0.00
16.14	6.97	2.00	0.00	1.00	0.00	16.16	7.01	2.00	0.00	1.00	0.00
16.18	7.01	2.00	0.00	1.00	0.00	16.20	7.14	2.00	0.00	1.00	0.00
16.22	7.02	2.00	0.00	1.00	0.00	16.24	7.10	2.00	0.00	1.00	0.00
16.26	7.04	2.00	0.00	1.00	0.00	16.28	7.04	2.00	0.00	1.00	0.00
16.30	6.99	2.00	0.00	1.00	0.00	16.32	6.97	2.00	0.00	1.00	0.00
16.34	7.05	2.00	0.00	1.00	0.00	16.36	7.07	2.00	0.00	1.00	0.00
16.38	7.06	2.00	0.00	1.00	0.00	16.40	7.20	2.00	0.00	1.00	0.00
16.42	7.28	2.00	0.00	1.00	0.00	16.44	7.57	2.00	0.00	1.00	0.00
16.46	7.78	2.00	0.00	1.00	0.00	16.48	8.01	2.00	0.00	1.00	0.00
16.50	8.11	2.00	0.00	1.00	0.00	16.52	7.97	2.00	0.00	1.00	0.00
16.54	7.81	2.00	0.00	1.00	0.00	16.56	7.65	2.00	0.00	1.00	0.00
16.58	7.65	2.00	0.00	1.00	0.00	16.60	7.76	2.00	0.00	1.00	0.00
16.62	7.76	2.00	0.00	1.00	0.00	16.64	7.73	2.00	0.00	1.00	0.00
16.66	7.71	2.00	0.00	1.00	0.00	16.68	7.65	2.00	0.00	1.00	0.00
16.70	7.64	2.00	0.00	1.00	0.00	16.72	7.72	2.00	0.00	1.00	0.00
16.74	9.94	2.00	0.00	1.00	0.00	16.76	9.22	2.00	0.00	1.00	0.00
16.78	8.29	2.00	0.00	1.00	0.00	16.80	7.81	2.00	0.00	1.00	0.00
16.82	7.59	2.00	0.00	1.00	0.00	16.84	7.72	2.00	0.00	1.00	0.00
16.86	7.91	2.00	0.00	1.00	0.00	16.88	8.25	2.00	0.00	1.00	0.00
16.91	8.83	2.00	0.00	1.00	0.00	16.92	9.57	2.00	0.00	1.00	0.00
16.94	10.63	2.00	0.00	1.00	0.00	16.96	10.42	2.00	0.00	1.00	0.00
16.98	9.59	2.00	0.00	1.00	0.00	17.00	9.59	2.00	0.00	1.00	0.00
17.02	10.23	2.00	0.00	1.00	0.00	17.04	10.36	2.00	0.00	1.00	0.00
17.06	10.39	2.00	0.00	1.00	0.00	17.08	9.82	2.00	0.00	1.00	0.00
17.10	9.12	2.00	0.00	1.00	0.00	17.18	9.00	2.00	0.00	1.00	0.00
17.18	9.00	2.00	0.00	1.00	0.00	17.18	9.00	2.00	0.00	1.00	0.00
17.18	9.06	2.00	0.00	1.00	0.00	17.20	12.68	2.00	0.00	1.00	0.00
17.22	11.44	2.00	0.00	1.00	0.00	17.24	11.43	2.00	0.00	1.00	0.00
17.26	11.36	2.00	0.00	1.00	0.00	17.28	11.06	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
17.30	11.21	2.00	0.00	1.00	0.00	17.32	10.89	2.00	0.00	1.00	0.00
17.34	9.93	2.00	0.00	1.00	0.00	17.36	8.99	2.00	0.00	1.00	0.00
17.38	8.27	2.00	0.00	1.00	0.00	17.40	8.03	2.00	0.00	1.00	0.00
17.42	8.18	2.00	0.00	1.00	0.00	17.44	8.04	2.00	0.00	1.00	0.00
17.46	7.80	2.00	0.00	1.00	0.00	17.48	7.68	2.00	0.00	1.00	0.00
17.50	7.70	2.00	0.00	1.00	0.00	17.52	9.01	2.00	0.00	1.00	0.00
17.54	11.92	2.00	0.00	1.00	0.00	17.56	14.70	2.00	0.00	1.00	0.00
17.58	16.04	2.00	0.00	1.00	0.00	17.60	15.89	2.00	0.00	1.00	0.00
17.62	17.41	2.00	0.00	1.00	0.00	17.64	17.72	2.00	0.00	1.00	0.00
17.66	16.37	2.00	0.00	1.00	0.00	17.68	14.06	2.00	0.00	1.00	0.00
17.70	12.19	2.00	0.00	1.00	0.00	17.72	12.41	2.00	0.00	1.00	0.00
17.74	17.30	2.00	0.00	1.00	0.00	17.76	15.87	2.00	0.00	1.00	0.00
17.78	14.56	2.00	0.00	1.00	0.00	17.80	13.95	2.00	0.00	1.00	0.00
17.82	12.65	2.00	0.00	1.00	0.00	17.84	11.23	2.00	0.00	1.00	0.00
17.86	10.13	2.00	0.00	1.00	0.00	17.88	11.09	2.00	0.00	1.00	0.00
17.90	15.32	2.00	0.00	1.00	0.00	17.92	19.54	2.00	0.00	1.00	0.00
17.94	20.58	2.00	0.00	1.00	0.00	17.96	19.84	2.00	0.00	1.00	0.00
17.98	18.39	2.00	0.00	1.00	0.00	18.00	18.32	2.00	0.00	1.00	0.00
18.02	20.35	2.00	0.00	1.00	0.00	18.04	22.10	2.00	0.00	1.00	0.00
18.06	25.90	2.00	0.00	1.00	0.00	18.08	25.49	2.00	0.00	1.00	0.00
18.10	23.32	2.00	0.00	1.00	0.00	18.12	23.55	2.00	0.00	1.00	0.00
18.14	24.62	2.00	0.00	1.00	0.00	18.16	24.00	2.00	0.00	1.00	0.00
18.18	18.50	2.00	0.00	1.00	0.00	18.20	14.79	2.00	0.00	1.00	0.00
18.22	11.70	2.00	0.00	1.00	0.00	18.24	10.63	2.00	0.00	1.00	0.00
18.26	13.80	2.00	0.00	1.00	0.00	18.28	17.67	2.00	0.00	1.00	0.00
18.30	19.73	2.00	0.00	1.00	0.00	18.32	19.20	2.00	0.00	1.00	0.00
18.34	22.02	2.00	0.00	1.00	0.00	18.36	28.28	2.00	0.00	1.00	0.00
18.38	93.86	0.67	3.43	1.00	0.07	18.40	95.10	0.68	3.38	1.00	0.07
18.42	95.04	0.68	3.38	1.00	0.07	18.44	94.84	0.68	3.39	1.00	0.07
18.46	94.23	0.68	3.41	1.00	0.07	18.48	93.75	0.67	3.43	1.00	0.07
18.50	93.81	0.67	3.43	1.00	0.07	18.52	94.84	0.68	3.39	1.00	0.07
18.54	32.10	2.00	0.00	1.00	0.00	18.58	31.57	2.00	0.00	1.00	0.00
18.58	22.69	2.00	0.00	1.00	0.00	18.60	21.37	2.00	0.00	1.00	0.00
18.62	22.74	2.00	0.00	1.00	0.00	18.64	24.68	2.00	0.00	1.00	0.00
18.66	26.21	2.00	0.00	1.00	0.00	18.68	29.39	2.00	0.00	1.00	0.00
18.70	34.15	2.00	0.00	1.00	0.00	18.72	98.69	2.00	0.00	1.00	0.00
18.74	99.47	2.00	0.00	1.00	0.00	18.76	100.18	2.00	0.00	1.00	0.00
18.78	99.69	2.00	0.00	1.00	0.00	18.80	97.42	2.00	0.00	1.00	0.00
18.82	95.01	2.00	0.00	1.00	0.00	18.84	92.86	2.00	0.00	1.00	0.00
18.86	90.31	0.66	3.56	1.00	0.07	18.88	89.10	0.65	3.61	1.00	0.07
18.90	88.81	0.65	3.62	1.00	0.07	18.92	90.29	0.66	3.56	1.00	0.07
18.94	93.35	0.68	3.44	1.00	0.07	18.96	97.15	0.71	3.31	1.00	0.07
18.98	101.94	0.75	3.15	1.00	0.06	19.07	103.25	0.76	3.11	1.00	0.28
19.07	103.13	0.76	3.11	1.00	0.00	19.07	103.07	0.76	3.12	1.00	0.00
19.08	109.79	0.83	2.92	1.00	0.03	19.10	122.12	1.00	1.15	1.00	0.02
19.12	126.21	1.07	0.89	1.00	0.02	19.22	122.02	1.00	1.15	1.00	0.11
19.22	120.71	0.98	1.25	1.00	0.00	19.14	119.91	0.96	1.33	1.00	0.11
19.22	100.91	0.75	3.18	1.00	0.25	19.24	94.40	0.69	3.41	1.00	0.07

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
19.26	93.18	2.00	0.00	1.00	0.00	19.28	89.80	2.00	0.00	1.00	0.00
19.30	86.81	2.00	0.00	1.00	0.00	19.32	83.95	2.00	0.00	1.00	0.00
19.34	81.86	2.00	0.00	1.00	0.00	19.36	81.81	2.00	0.00	1.00	0.00
19.38	81.56	2.00	0.00	1.00	0.00	19.40	21.79	2.00	0.00	1.00	0.00
19.42	19.27	2.00	0.00	1.00	0.00	19.44	19.08	2.00	0.00	1.00	0.00
19.46	19.65	2.00	0.00	1.00	0.00	19.48	20.77	2.00	0.00	1.00	0.00
19.50	23.93	2.00	0.00	1.00	0.00	19.52	28.20	2.00	0.00	1.00	0.00
19.54	98.69	2.00	0.00	1.00	0.00	19.56	111.90	2.00	0.00	1.00	0.00
19.58	120.57	2.00	0.00	1.00	0.00	19.60	120.72	2.00	0.00	1.00	0.00
19.62	118.37	2.00	0.00	1.00	0.00	19.64	113.26	2.00	0.00	1.00	0.00
19.66	108.15	0.82	2.96	1.00	0.06	19.68	101.12	0.76	3.18	1.00	0.06
19.70	94.76	0.70	3.39	1.00	0.07	19.72	86.58	0.65	3.71	1.00	0.07
19.74	88.53	0.66	3.63	1.00	0.07	19.76	87.67	0.66	3.67	1.00	0.07
19.78	88.58	0.66	3.63	1.00	0.07	19.81	90.03	0.67	3.57	1.00	0.11
19.82	92.67	0.69	3.47	1.00	0.03	19.84	93.57	0.70	3.44	1.00	0.07
19.86	93.75	2.00	0.00	1.00	0.00	19.88	92.09	2.00	0.00	1.00	0.00
19.90	87.69	2.00	0.00	1.00	0.00	19.92	83.51	2.00	0.00	1.00	0.00
19.94	81.37	2.00	0.00	1.00	0.00	19.96	81.80	2.00	0.00	1.00	0.00
19.98	82.23	2.00	0.00	1.00	0.00	20.00	22.68	2.00	0.00	1.00	0.00
20.02	20.90	2.00	0.00	1.00	0.00	20.04	18.59	2.00	0.00	1.00	0.00
20.06	14.21	2.00	0.00	1.00	0.00	20.08	12.08	2.00	0.00	1.00	0.00
20.10	11.36	2.00	0.00	1.00	0.00	20.12	12.32	2.00	0.00	1.00	0.00
20.14	12.51	2.00	0.00	1.00	0.00	20.16	15.32	2.00	0.00	1.00	0.00
20.18	27.49	2.00	0.00	1.00	0.00	20.20	100.12	2.00	0.00	1.00	0.00
20.22	101.99	2.00	0.00	1.00	0.00	20.24	101.02	2.00	0.00	1.00	0.00
20.26	98.20	2.00	0.00	1.00	0.00	20.28	93.92	2.00	0.00	1.00	0.00
20.30	90.50	2.00	0.00	1.00	0.00	20.32	89.35	0.68	3.60	1.00	0.07
20.34	89.35	0.68	3.60	1.00	0.07	20.36	91.61	0.69	3.51	1.00	0.07
20.38	91.64	0.69	3.51	1.00	0.07	20.40	91.33	0.69	3.52	1.00	0.07
20.42	90.77	0.69	3.54	1.00	0.07	20.44	90.28	0.68	3.56	1.00	0.07
20.46	89.76	0.68	3.58	1.00	0.07	20.48	89.00	0.68	3.61	1.00	0.07
20.50	88.41	0.67	3.64	1.00	0.07	20.52	86.14	0.66	3.73	1.00	0.07
20.54	86.69	0.66	3.71	1.00	0.07						

Total estimated settlement: 3.56

Abbreviations

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumentric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

:: Strength loss calculation Idriss & Boulanger (2008) ::

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.02	0.50	8.44	7.71	65.07	3.08	0.06	111.25
0.05	0.56	9.56	8.25	78.84	3.13	0.06	49.29
0.06	0.58	9.93	8.26	81.96	3.13	0.06	42.51
0.08	0.60	10.20	8.51	86.81	3.15	0.06	32.52
0.10	0.59	10.08	9.16	92.31	3.19	0.06	25.57
0.12	0.59	10.03	9.72	97.45	3.23	0.06	21.07
0.14	0.61	10.40	9.86	102.58	3.24	0.06	18.64
0.16	0.70	11.77	9.15	107.73	3.19	0.06	18.36
0.18	0.84	14.24	7.89	112.36	3.10	0.07	19.64
0.20	1.01	17.06	6.75	115.20	3.00	0.07	21.09
0.22	1.15	19.45	6.02	116.98	2.93	0.07	21.76
0.24	1.23	20.82	5.70	118.68	2.90	0.08	21.27
0.26	1.29	21.90	5.53	121.20	2.88	0.08	20.58
0.28	1.33	22.47	5.50	123.72	2.88	0.08	19.55
0.30	1.35	22.83	5.61	128.03	2.89	0.08	18.47
0.32	1.33	22.60	5.93	134.10	2.92	0.08	17.09
0.34	1.32	22.31	6.35	141.73	2.96	0.08	15.82
0.36	1.31	22.18	6.67	147.90	2.99	0.08	14.81
0.38	1.31	22.08	6.90	152.30	3.01	0.08	13.93
0.40	1.28	21.61	7.24	156.47	3.04	0.08	12.92
0.42	1.24	20.90	7.68	160.53	3.08	0.07	11.86
0.44	1.20	20.19	8.08	163.04	3.11	0.07	10.91
0.46	1.17	19.83	8.22	162.92	3.12	0.07	10.23
0.48	1.15	19.43	8.32	161.64	3.13	0.07	9.58
0.50	1.13	19.05	8.43	160.56	3.14	0.07	9.00
0.52	1.10	18.47	8.64	159.64	3.16	0.07	8.38
0.54	1.08	18.14	8.70	157.75	3.16	0.07	7.91
0.56	1.07	17.96	8.64	155.25	3.16	0.07	7.55
0.58	1.07	18.03	8.48	152.91	3.14	0.07	7.31
0.60	1.07	18.09	8.38	151.64	3.14	0.07	7.08
0.62	1.08	18.12	8.33	150.87	3.13	0.07	6.98
0.64	1.09	18.28	8.19	149.63	3.12	0.07	6.93
0.66	1.09	18.29	8.09	147.85	3.11	0.07	6.83
0.68	1.08	18.21	8.04	146.40	3.11	0.07	6.70
0.70	1.07	17.90	8.14	145.65	3.12	0.07	6.49
0.72	1.05	17.59	8.28	145.71	3.13	0.07	6.29
0.74	1.03	17.23	8.46	145.82	3.14	0.07	6.07
0.76	1.01	16.96	8.62	146.16	3.15	0.07	5.89
0.78	1.00	16.74	8.75	146.47	3.16	0.07	5.73
0.80	0.99	16.63	8.79	146.14	3.17	0.07	5.62
0.82	0.98	16.46	8.81	145.10	3.17	0.07	5.49
0.84	0.95	15.95	8.89	141.79	3.17	0.07	5.25
1.04	0.92	15.38	9.04	139.07	3.19	0.07	4.48
1.04	0.89	14.84	9.20	136.53	3.20	0.07	4.32
1.04	0.89	14.76	9.22	136.14	3.20	0.07	4.30
1.04	0.88	14.68	9.25	135.76	3.20	0.07	4.27
1.04	0.89	14.88	8.88	132.08	3.17	0.07	4.33
0.96	0.92	15.30	8.33	127.40	3.13	0.07	4.66

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.98	0.94	15.67	7.80	122.28	3.09	0.07	4.72
1.00	0.95	15.89	7.64	121.36	3.08	0.07	4.73
1.02	0.95	15.89	7.62	121.13	3.08	0.07	4.68
1.04	0.96	15.98	7.57	120.92	3.07	0.07	4.65
1.06	0.97	16.12	7.54	121.50	3.07	0.07	4.64
1.08	0.98	16.27	7.62	124.08	3.08	0.07	4.64
1.10	0.98	16.36	7.78	127.28	3.09	0.07	4.61
1.12	0.97	16.16	8.05	130.08	3.11	0.07	4.50
1.14	0.95	15.85	8.29	131.34	3.13	0.07	4.37
1.16	0.93	15.41	8.59	132.32	3.15	0.07	4.20
1.18	0.91	15.07	8.82	132.98	3.17	0.07	4.07
1.20	0.90	14.85	8.99	133.56	3.18	0.07	3.97
1.32	0.89	14.71	9.09	133.77	3.19	0.07	3.70
1.32	0.88	14.63	9.14	133.79	3.19	0.07	3.68
1.32	0.88	14.57	9.18	133.73	3.20	0.07	3.66
1.32	0.85	14.00	9.55	133.72	3.22	0.07	3.52
1.30	0.81	13.39	9.99	133.78	3.25	0.07	3.40
1.32	0.77	12.72	10.48	133.28	3.28	0.06	3.20
1.34	0.77	12.60	10.52	132.48	3.29	0.06	3.14
1.36	0.77	12.68	10.33	131.05	3.27	0.06	3.13
1.38	0.80	13.12	9.88	129.54	3.24	0.07	3.20
1.40	0.83	13.69	9.37	128.33	3.21	0.07	3.31
1.42	0.88	14.49	8.82	127.86	3.17	0.07	3.47
1.44	0.93	15.35	8.33	127.89	3.13	0.07	3.64
1.46	1.00	16.49	7.76	127.95	3.09	0.07	3.88
1.49	1.07	17.66	7.24	127.83	3.04	0.07	4.10
1.50	1.11	18.44	6.95	128.08	3.02	0.07	4.26
1.53	1.14	18.86	6.79	128.02	3.00	0.07	4.30
1.54	1.14	18.84	6.79	127.95	3.00	0.07	4.28
1.56	1.14	18.84	6.76	127.40	3.00	0.07	4.24
1.58	1.12	18.61	6.83	127.02	3.01	0.07	4.15
1.60	1.11	18.42	6.83	125.74	3.01	0.07	4.07
1.62	1.09	17.97	6.88	123.64	3.01	0.07	3.94
1.64	1.06	17.45	6.92	120.84	3.02	0.07	3.79
1.66	1.02	16.77	7.06	118.29	3.03	0.07	3.62
1.68	0.99	16.27	7.14	116.19	3.04	0.07	3.48
1.70	0.95	15.70	7.27	114.19	3.05	0.07	3.33
1.72	0.91	15.02	7.50	112.59	3.06	0.07	3.16
1.74	0.87	14.30	7.79	111.32	3.09	0.07	2.99
1.76	0.83	13.64	8.06	109.98	3.11	0.07	2.83
1.78	0.81	13.27	8.14	107.99	3.12	0.07	2.73
1.80	0.79	12.83	8.25	105.77	3.13	0.07	2.62
1.82	0.76	12.42	8.39	104.16	3.14	0.06	2.52
1.84	0.73	11.80	8.62	101.67	3.15	0.06	2.37
1.86	0.72	11.69	8.49	99.30	3.14	0.06	2.34
1.88	0.73	11.82	8.14	96.20	3.12	0.06	2.35
1.91	0.74	12.05	7.83	94.32	3.09	0.06	2.37
1.92	0.73	11.88	7.78	92.43	3.09	0.06	2.33

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
1.94	0.71	11.54	7.88	90.93	3.10	0.06	2.24
1.96	0.70	11.30	7.92	89.43	3.10	0.06	2.18
1.98	0.69	11.11	7.91	87.84	3.10	0.06	2.13
2.00	0.68	10.89	7.96	86.71	3.10	0.06	2.08
2.02	0.67	10.75	7.96	85.57	3.10	0.06	2.04
2.04	0.65	10.52	8.04	84.57	3.11	0.06	1.98
2.06	0.64	10.17	8.21	83.56	3.12	0.06	1.90
2.08	0.61	9.74	8.50	82.82	3.14	0.06	1.81
2.10	0.58	9.23	8.94	82.54	3.18	0.06	1.71
2.13	0.55	8.78	9.36	82.19	3.21	0.06	1.61
2.14	0.53	8.33	9.75	81.20	3.24	0.06	1.52
2.16	0.50	7.88	10.10	79.58	3.26	0.06	1.43
2.18	0.48	7.43	10.47	77.81	3.28	0.06	1.34
2.20	0.46	7.15	10.66	76.27	3.30	0.06	1.29
2.22	0.46	7.17	10.40	74.56	3.28	0.06	1.28
2.24	0.48	7.43	9.78	72.67	3.24	0.06	1.32
2.26	0.50	7.87	9.05	71.24	3.19	0.06	1.39
2.28	0.54	8.44	8.35	70.48	3.13	0.06	1.48
2.30	0.58	9.16	7.66	70.16	3.08	0.06	1.60
2.32	0.62	9.89	7.06	69.76	3.03	0.06	1.72
2.34	0.65	10.40	6.63	68.90	2.99	0.06	1.80
2.37	0.65	10.30	6.61	68.11	2.99	0.06	1.77
2.38	0.62	9.90	6.82	67.53	3.01	0.06	1.70
2.42	0.56	8.87	7.49	66.47	3.06	0.06	1.50
2.42	0.52	8.12	8.01	65.07	3.11	0.06	1.38
2.44	0.49	7.59	8.38	63.65	3.14	0.06	1.28
2.46	0.51	7.93	7.97	63.23	3.10	0.06	1.33
2.48	0.55	8.66	7.30	63.23	3.05	0.06	1.45
2.50	0.59	9.32	6.77	63.05	3.00	0.06	1.55
2.52	0.62	9.84	6.39	62.90	2.97	0.06	1.63
2.54	0.63	10.00	6.30	62.98	2.96	0.06	1.65
2.56	0.64	10.17	6.22	63.25	2.95	0.06	1.67
2.58	0.66	10.52	6.04	63.55	2.93	0.06	1.71
2.60	0.68	10.86	5.91	64.21	2.92	0.07	1.76
2.62	0.70	11.11	5.80	64.45	2.91	0.07	1.79
2.64	0.68	10.77	6.16	66.34	2.95	0.06	1.73
2.66	0.66	10.37	6.61	68.51	2.99	0.06	1.66
2.68	0.63	9.85	7.16	70.50	3.04	0.06	1.57
2.70	0.61	9.59	7.37	70.68	3.05	0.06	1.52
2.72	0.60	9.37	7.56	70.78	3.07	0.06	1.48
2.74	0.60	9.35	7.59	71.00	3.07	0.06	1.47
2.76	0.60	9.43	7.58	71.51	3.07	0.06	1.47
2.78	0.60	9.39	7.56	70.95	3.07	0.06	1.46
2.80	0.58	8.99	7.79	69.96	3.09	0.06	1.39
2.82	0.55	8.49	8.05	68.37	3.11	0.06	1.31
2.84	0.54	8.38	8.26	69.28	3.13	0.06	1.28
2.86	0.54	8.28	8.62	71.31	3.15	0.06	1.26
2.89	0.52	8.03	9.17	73.71	3.19	0.06	1.22

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
2.90	0.48	7.30	10.12	73.92	3.26	0.06	1.10
2.92	0.45	6.74	10.94	73.73	3.31	0.06	1.01
2.94	0.42	6.31	11.65	73.50	3.36	0.06	0.94
2.96	0.41	6.11	12.02	73.42	3.38	0.06	0.91
2.99	0.41	6.05	12.08	73.05	3.39	0.06	0.89
3.00	0.40	5.99	12.05	72.16	3.38	0.06	0.88
3.03	0.40	5.95	11.89	70.76	3.37	0.06	0.87
3.05	0.40	5.90	11.61	68.50	3.36	0.06	0.86
3.06	0.39	5.81	11.46	66.60	3.35	0.06	0.85
3.08	0.40	5.87	11.05	64.85	3.32	0.06	0.85
3.10	0.41	6.04	10.62	64.20	3.29	0.06	0.87
3.12	0.43	6.35	10.03	63.66	3.25	0.06	0.91
3.14	0.44	6.50	9.81	63.74	3.24	0.06	0.93
3.16	0.43	6.38	10.04	64.02	3.26	0.06	0.91
3.18	0.40	5.90	10.75	63.47	3.30	0.06	0.84
3.20	0.38	5.48	11.24	61.63	3.33	0.06	0.78
3.22	0.37	5.30	11.29	59.86	3.34	0.06	0.75
3.24	0.41	6.07	9.86	59.89	3.24	0.06	0.85
3.26	0.57	8.80	6.83	60.17	3.01	0.06	1.23
3.28	0.85	13.47	4.30	57.94	2.74	0.07	1.88
3.30	1.15	18.56	3.05	56.53	2.55	0.08	0.61
3.32	1.36	22.17	2.61	57.92	2.47	0.08	0.63
3.34	1.49	24.37	2.48	60.53	2.44	0.08	0.65
3.36	1.58	25.91	2.41	62.37	2.42	0.08	0.65
3.38	1.64	26.90	2.37	63.82	2.41	0.08	0.66
3.40	1.59	25.95	2.48	64.24	2.44	0.09	0.65
3.42	1.42	23.17	2.75	63.62	2.50	0.08	0.64
3.44	1.16	18.71	3.35	62.72	2.60	0.08	2.52
3.46	0.92	14.68	4.26	62.53	2.74	0.08	1.97
3.48	0.74	11.54	5.41	62.46	2.87	0.07	1.54
3.50	0.65	10.02	6.16	61.72	2.95	0.06	1.33
3.52	0.62	9.46	6.33	59.89	2.96	0.06	1.25
3.54	0.61	9.30	6.29	58.53	2.96	0.06	1.23
3.56	0.60	9.16	6.32	57.87	2.96	0.06	1.20
3.58	0.58	8.90	6.63	58.99	2.99	0.06	1.17
3.60	0.60	9.20	6.54	60.20	2.98	0.06	1.20
3.62	0.64	9.79	6.28	61.54	2.96	0.06	1.27
3.64	0.68	10.42	6.00	62.54	2.93	0.06	1.35
3.66	0.67	10.36	6.18	64.03	2.95	0.06	1.34
3.68	0.65	9.98	6.60	65.89	2.99	0.06	1.28
3.70	0.62	9.55	7.03	67.16	3.03	0.06	1.22
3.72	0.61	9.23	7.55	69.71	3.07	0.06	1.18
3.74	0.60	9.18	8.04	73.80	3.11	0.06	1.17
3.76	0.59	8.99	8.90	80.07	3.17	0.06	1.14
3.78	0.59	8.95	9.57	85.65	3.22	0.06	1.13
3.80	0.59	8.91	10.13	90.25	3.26	0.06	1.12
3.82	0.60	9.03	10.49	94.78	3.29	0.06	1.13
3.84	0.60	9.14	10.76	98.39	3.30	0.06	1.14

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
3.86	0.61	9.23	10.90	100.61	3.31	0.06	1.14
3.88	0.61	9.28	10.84	100.63	3.31	0.06	1.14
3.90	0.62	9.46	10.59	100.20	3.29	0.06	1.16
3.92	0.62	9.44	10.53	99.43	3.29	0.06	1.15
3.94	0.62	9.35	10.56	98.67	3.29	0.06	1.14
3.96	0.61	9.16	10.66	97.65	3.30	0.06	1.11
3.98	0.60	9.12	10.62	96.80	3.29	0.06	1.10
4.00	0.61	9.17	10.49	96.13	3.28	0.06	1.10
4.02	0.62	9.34	10.26	95.80	3.27	0.06	1.12
4.04	0.64	9.64	9.92	95.69	3.25	0.06	1.15
4.06	0.65	9.92	9.67	95.87	3.23	0.06	1.18
4.08	0.66	10.03	9.58	96.08	3.22	0.06	1.19
4.10	0.67	10.15	9.49	96.32	3.22	0.06	1.19
4.12	0.70	10.65	9.07	96.57	3.19	0.06	1.25
4.14	0.75	11.50	8.48	97.47	3.14	0.06	1.34
4.16	0.80	12.48	7.93	98.97	3.10	0.07	1.45
4.18	0.85	13.17	7.66	100.86	3.08	0.07	1.53
4.20	0.87	13.63	7.58	103.28	3.07	0.07	1.57
4.22	0.88	13.75	7.71	106.02	3.08	0.07	1.58
4.24	0.89	13.92	7.85	109.30	3.09	0.07	1.59
4.26	0.91	14.17	7.96	112.71	3.10	0.07	1.61
4.28	0.93	14.62	7.95	116.17	3.10	0.07	1.66
4.30	0.97	15.16	7.87	119.40	3.10	0.07	1.71
4.32	0.99	15.64	7.80	121.98	3.09	0.07	1.76
4.34	1.01	15.89	7.81	124.08	3.09	0.07	1.78
4.36	1.02	16.00	7.87	125.95	3.10	0.07	1.78
4.38	1.02	16.00	7.97	127.56	3.10	0.07	1.78
4.40	1.02	16.11	8.02	129.23	3.11	0.07	1.78
4.42	1.03	16.19	8.07	130.64	3.11	0.07	1.78
4.44	1.02	16.11	8.19	131.91	3.12	0.07	1.76
4.46	1.00	15.69	8.46	132.77	3.14	0.07	1.71
4.48	0.95	14.90	8.94	133.19	3.18	0.07	1.62
4.50	0.91	14.24	9.31	132.57	3.20	0.07	1.54
4.52	0.91	14.08	9.30	131.02	3.20	0.07	1.52
4.54	0.91	14.18	9.11	129.16	3.19	0.07	1.52
4.56	0.93	14.50	8.81	127.71	3.17	0.07	1.55
4.58	0.95	14.83	8.56	126.86	3.15	0.07	1.58
4.60	0.99	15.45	8.11	125.26	3.11	0.07	1.64
4.62	1.01	15.90	7.76	123.40	3.09	0.07	1.68
4.68	1.03	16.11	7.56	121.79	3.07	0.07	1.68
4.68	1.03	16.08	7.53	121.02	3.07	0.07	1.68
4.68	1.01	15.73	7.65	120.36	3.08	0.07	1.64
4.70	0.98	15.21	7.90	120.19	3.10	0.07	1.58
4.72	0.94	14.59	8.28	120.75	3.13	0.07	1.51
4.74	0.92	14.28	8.55	122.05	3.15	0.07	1.47
4.76	0.91	14.04	8.81	123.71	3.17	0.07	1.44
4.78	0.90	13.91	9.04	125.76	3.18	0.07	1.42
4.80	0.89	13.76	9.27	127.47	3.20	0.07	1.40

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
4.82	0.90	13.82	9.24	127.65	3.20	0.07	1.40
4.84	0.90	13.81	9.19	126.93	3.20	0.07	1.40
4.86	0.89	13.78	9.15	126.12	3.19	0.07	1.39
4.89	0.89	13.71	9.20	126.08	3.20	0.07	1.37
4.90	0.89	13.71	9.19	126.01	3.20	0.07	1.37
4.93	0.90	13.85	9.09	125.85	3.19	0.07	1.37
4.94	0.90	13.80	9.10	125.53	3.19	0.07	1.37
4.96	0.89	13.67	9.12	124.77	3.19	0.07	1.35
4.98	0.87	13.32	9.27	123.41	3.20	0.07	1.31
5.01	0.85	12.99	9.37	121.73	3.21	0.07	1.27
5.02	0.83	12.58	9.57	120.35	3.22	0.06	1.23
5.04	0.80	12.21	9.81	119.73	3.24	0.06	1.19
5.06	0.79	11.95	9.97	119.05	3.25	0.06	1.16
5.08	0.79	11.90	9.94	118.29	3.25	0.06	1.15
5.10	0.79	11.98	9.79	117.26	3.24	0.06	1.15
5.12	0.80	12.14	9.60	116.60	3.23	0.06	1.16
5.14	0.82	12.49	9.27	115.81	3.20	0.06	1.19
5.16	0.85	12.99	8.81	114.47	3.17	0.07	1.24
5.18	0.88	13.38	8.43	112.85	3.14	0.07	1.27
5.20	0.90	13.72	8.07	110.72	3.11	0.07	1.30
5.22	0.90	13.83	7.88	109.01	3.10	0.07	1.30
5.24	0.90	13.84	7.80	107.91	3.09	0.07	1.30
5.26	0.89	13.66	7.90	107.86	3.10	0.07	1.28
5.28	0.88	13.38	8.08	108.10	3.11	0.07	1.25
5.30	0.86	13.10	8.25	108.09	3.13	0.06	1.22
5.32	0.84	12.65	8.58	108.52	3.15	0.06	1.17
5.34	0.82	12.33	8.83	108.93	3.17	0.06	1.14
5.36	0.81	12.24	8.94	109.48	3.18	0.06	1.13
5.38	0.83	12.48	8.85	110.39	3.17	0.06	1.14
5.40	0.84	12.73	8.71	110.83	3.16	0.06	1.16
5.42	0.85	12.89	8.47	109.12	3.14	0.06	1.17
5.44	0.83	12.57	8.38	105.35	3.14	0.06	1.14
5.46	0.84	12.76	7.87	100.37	3.10	0.06	1.15
5.48	0.97	14.81	6.39	94.58	2.97	0.07	1.34
5.51	1.14	17.72	4.97	88.11	2.82	0.08	1.59
5.52	1.24	19.48	4.39	85.55	2.75	0.08	1.75
5.54	1.17	18.19	4.91	89.32	2.81	0.08	1.62
5.56	1.02	15.76	5.88	92.74	2.92	0.07	1.40
5.58	0.91	13.88	6.62	91.93	2.99	0.06	1.23
5.60	0.87	13.14	6.73	88.41	3.00	0.06	1.16
5.62	0.86	13.02	6.62	86.20	2.99	0.06	1.15
5.64	0.88	13.29	6.50	86.39	2.98	0.06	1.17
5.66	0.91	13.87	6.28	87.05	2.96	0.07	1.22
5.68	0.97	14.74	5.91	87.20	2.92	0.07	1.29
5.70	1.02	15.66	5.59	87.57	2.89	0.07	1.37
5.72	1.09	16.88	5.31	89.68	2.86	0.07	1.47
5.74	1.18	18.36	5.03	92.38	2.83	0.08	1.59
5.76	1.25	19.53	4.84	94.54	2.81	0.08	1.69

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
5.78	1.26	19.72	4.95	97.59	2.82	0.08	1.70
5.80	1.30	20.39	4.95	100.99	2.82	0.08	1.75
5.82	1.27	19.89	5.28	104.98	2.86	0.08	1.70
5.84	1.21	18.94	5.66	107.20	2.90	0.07	1.62
5.86	1.07	16.55	6.56	108.49	2.98	0.07	1.41
5.88	1.00	15.22	7.13	108.48	3.03	0.07	1.29
5.90	0.98	14.86	7.13	106.04	3.03	0.07	1.26
5.92	0.98	14.92	6.85	102.22	3.01	0.07	1.26
5.94	1.00	15.27	6.45	98.58	2.97	0.07	1.28
5.96	1.03	15.76	6.16	97.09	2.95	0.07	1.32
5.98	1.08	16.58	5.85	97.03	2.92	0.07	1.38
6.00	1.12	17.27	5.70	98.44	2.90	0.07	1.44
6.02	1.15	17.85	5.68	101.31	2.90	0.07	1.48
6.04	1.18	18.35	5.75	105.49	2.91	0.07	1.52
6.06	1.21	18.84	5.83	109.81	2.91	0.07	1.55
6.08	1.24	19.38	5.92	114.70	2.92	0.07	1.59
6.10	1.28	19.97	5.98	119.46	2.93	0.07	1.64
6.12	1.32	20.66	6.00	123.87	2.93	0.07	1.69
6.14	1.36	21.37	5.97	127.50	2.93	0.07	1.74
6.16	1.39	21.85	5.96	130.19	2.93	0.07	1.77
6.18	1.41	22.10	6.04	133.44	2.93	0.07	1.79
6.20	1.43	22.41	6.11	136.83	2.94	0.07	1.81
6.22	1.45	22.77	6.16	140.36	2.95	0.07	1.83
6.24	1.48	23.27	6.17	143.60	2.95	0.07	1.86
6.26	1.49	23.54	6.24	146.85	2.95	0.07	1.88
6.28	1.51	23.75	6.35	150.75	2.96	0.07	1.89
6.30	1.50	23.69	6.51	154.24	2.98	0.07	1.88
6.32	1.50	23.56	6.65	156.60	2.99	0.07	1.86
6.34	1.47	23.16	6.85	158.56	3.01	0.07	1.83
6.36	1.45	22.72	7.06	160.32	3.03	0.07	1.78
6.38	1.41	22.14	7.31	161.85	3.05	0.07	1.73
6.40	1.38	21.52	7.56	162.67	3.07	0.07	1.68
6.42	1.34	20.94	7.77	162.65	3.09	0.07	1.63
6.44	1.33	20.66	7.85	162.07	3.09	0.07	1.60
6.46	1.32	20.48	7.82	160.09	3.09	0.07	1.58
6.48	1.31	20.41	7.71	157.44	3.08	0.07	1.57
6.50	1.31	20.30	7.60	154.26	3.07	0.07	1.56
6.52	1.30	20.25	7.48	151.54	3.06	0.07	1.55
6.54	1.30	20.20	7.33	148.13	3.05	0.07	1.54
6.56	1.28	19.86	7.30	144.91	3.05	0.07	1.51
6.58	1.26	19.56	7.26	141.99	3.04	0.07	1.48
6.60	1.24	19.22	7.25	139.29	3.04	0.07	1.45
6.62	1.23	19.04	7.20	137.16	3.04	0.07	1.44
6.64	1.24	19.09	7.02	133.96	3.02	0.07	1.43
6.66	1.27	19.57	6.70	131.13	3.00	0.07	1.47
6.68	1.32	20.44	6.29	128.57	2.96	0.07	1.53
6.70	1.37	21.23	6.02	127.76	2.93	0.07	1.58
6.72	1.41	21.96	5.84	128.36	2.91	0.07	1.63

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
6.74	1.41	21.98	5.85	128.54	2.92	0.08	1.63
6.76	1.37	21.26	6.08	129.27	2.94	0.07	1.57
6.78	1.30	20.05	6.44	129.17	2.97	0.07	1.48
6.80	1.23	18.82	6.91	129.98	3.01	0.07	1.38
6.82	1.17	17.96	7.34	131.77	3.05	0.07	1.31
6.84	1.13	17.17	7.86	134.99	3.09	0.07	1.25
6.86	1.11	16.84	8.22	138.41	3.12	0.07	1.23
6.88	1.12	16.99	8.29	140.88	3.13	0.07	1.23
6.90	1.15	17.53	8.15	142.89	3.12	0.07	1.27
6.92	1.19	18.21	7.90	143.79	3.10	0.07	1.31
6.94	1.23	18.88	7.58	143.19	3.07	0.07	1.36
6.96	1.26	19.34	7.25	140.23	3.04	0.07	1.39
6.98	1.27	19.55	7.00	136.89	3.02	0.07	1.40
7.00	1.27	19.57	6.85	134.13	3.01	0.07	1.40
7.02	1.28	19.65	6.78	133.16	3.00	0.07	1.40
7.04	1.31	20.00	6.66	133.16	2.99	0.07	1.43
7.06	1.34	20.47	6.53	133.76	2.98	0.07	1.46
7.08	1.38	21.15	6.40	135.28	2.97	0.07	1.51
7.10	1.45	22.20	6.19	137.31	2.95	0.07	1.59
7.12	1.55	23.70	5.87	139.11	2.92	0.08	1.70
7.14	1.67	25.43	5.48	139.29	2.88	0.08	1.84
7.16	1.79	27.17	5.12	139.00	2.84	0.08	1.98
7.18	1.89	28.49	4.91	139.97	2.82	0.09	2.08
7.20	1.95	29.31	4.87	142.79	2.81	0.09	2.15
7.22	1.96	29.45	4.99	146.82	2.82	0.09	2.15
7.24	1.93	29.12	5.18	150.73	2.84	0.09	2.12
7.26	1.87	28.26	5.53	156.19	2.88	0.08	2.04
7.28	1.78	26.93	6.05	163.08	2.94	0.08	1.92
7.30	1.68	25.29	6.67	168.69	2.99	0.07	1.81
7.32	1.60	23.86	7.20	171.87	3.04	0.07	1.70
7.34	1.56	23.19	7.43	172.21	3.06	0.07	1.66
7.36	1.56	23.01	7.43	170.89	3.06	0.07	1.64
7.38	1.60	23.59	7.10	167.55	3.03	0.07	1.68
7.40	1.65	24.44	6.66	162.80	2.99	0.07	1.75
7.42	1.71	25.20	6.23	157.10	2.95	0.08	1.80
7.44	1.75	25.67	5.89	151.32	2.92	0.08	1.84
7.46	1.76	25.75	5.70	146.82	2.90	0.08	1.85
7.48	1.78	25.88	5.55	143.63	2.88	0.08	1.87
7.50	1.79	25.95	5.49	142.45	2.88	0.08	1.87
7.52	1.81	26.26	5.47	143.68	2.88	0.08	1.89
7.54	1.84	26.61	5.49	146.20	2.88	0.08	1.92
7.56	1.89	27.22	5.51	149.86	2.88	0.08	1.96
7.58	1.91	27.54	5.56	153.13	2.89	0.08	1.98
7.60	1.91	27.54	5.72	157.60	2.90	0.08	1.98
7.62	1.89	27.26	5.90	160.70	2.92	0.08	1.95
7.64	1.87	26.92	6.04	162.62	2.93	0.08	1.92
7.66	1.86	26.62	6.11	162.71	2.94	0.08	1.90
7.68	1.84	26.34	6.17	162.51	2.95	0.08	1.88

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
7.70	1.84	26.24	6.19	162.36	2.95	0.08	1.87
7.72	1.84	26.06	6.23	162.35	2.95	0.08	1.86
7.74	1.81	25.65	6.37	163.38	2.97	0.08	1.83
7.76	1.78	25.07	6.58	164.97	2.99	0.08	1.79
7.78	1.76	24.74	6.62	163.75	2.99	0.08	1.77
7.81	1.78	24.83	6.51	161.70	2.98	0.08	1.77
7.82	1.80	25.11	6.34	159.24	2.96	0.08	1.79
7.84	1.80	25.10	6.33	159.00	2.96	0.08	1.79
7.86	1.78	24.62	6.42	158.14	2.97	0.08	1.76
7.88	1.74	24.08	6.53	157.31	2.98	0.08	1.72
7.90	1.73	23.84	6.55	156.06	2.98	0.07	1.70
7.92	1.73	23.77	6.52	155.05	2.98	0.07	1.70
7.94	1.73	23.61	6.52	153.81	2.98	0.07	1.69
7.96	1.68	22.91	6.67	152.78	2.99	0.07	1.64
7.99	1.60	21.55	7.04	151.79	3.03	0.07	1.54
8.00	1.48	19.77	7.60	150.13	3.07	0.07	1.41
8.02	1.35	17.73	8.34	147.82	3.13	0.07	1.27
8.04	1.22	15.77	9.20	145.06	3.20	0.07	1.13
8.06	1.11	14.13	10.08	142.44	3.26	0.07	1.01
8.08	1.02	12.89	10.82	139.47	3.31	0.06	0.92
8.10	0.96	11.95	11.33	135.35	3.34	0.06	0.85
8.12	0.91	11.21	11.66	130.66	3.36	0.06	0.80
8.14	0.86	10.39	12.07	125.44	3.38	0.06	0.74
8.16	0.82	9.78	12.27	119.94	3.40	0.06	0.70
8.18	0.81	9.57	11.98	114.61	3.38	0.06	0.68
8.20	0.83	9.93	11.05	109.70	3.32	0.06	0.71
8.22	0.90	10.84	9.73	105.44	3.23	0.06	0.77
8.24	1.00	12.33	8.20	101.03	3.12	0.06	0.88
8.26	1.14	14.23	6.77	96.32	3.00	0.07	1.02
8.28	1.23	15.53	5.96	92.54	2.93	0.07	1.11
8.30	1.22	15.25	5.94	90.62	2.92	0.07	1.09
8.32	1.12	13.77	6.55	90.23	2.98	0.07	0.98
8.34	1.02	12.33	7.17	88.38	3.04	0.06	0.88
8.36	0.96	11.54	7.37	85.09	3.05	0.06	0.82
8.38	0.96	11.43	7.15	81.77	3.04	0.06	0.82
8.40	0.99	11.90	6.75	80.32	3.00	0.06	0.85
8.42	1.06	12.79	6.24	79.75	2.95	0.06	0.91
8.44	1.11	13.47	5.89	79.37	2.92	0.07	0.96
8.46	1.10	13.36	5.98	79.84	2.93	0.07	0.95
8.48	1.06	12.69	6.37	80.88	2.97	0.06	0.91
8.50	1.01	12.04	6.78	81.67	3.00	0.06	0.86
8.52	0.98	11.56	7.12	82.34	3.03	0.06	0.83
8.54	1.00	11.74	7.09	83.24	3.03	0.06	0.84
8.56	1.04	12.40	6.77	83.95	3.00	0.06	0.89
8.58	1.11	13.26	6.37	84.47	2.97	0.07	0.95
8.60	1.13	13.56	6.27	85.01	2.96	0.07	0.97
8.62	1.11	13.19	6.53	86.21	2.98	0.06	0.94
8.64	1.06	12.53	6.93	86.76	3.02	0.06	0.89

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
8.66	1.02	11.90	7.28	86.67	3.05	0.06	0.85
8.68	1.00	11.61	7.39	85.75	3.06	0.06	0.83
8.70	1.01	11.67	7.23	84.31	3.04	0.06	0.83
8.72	1.05	12.21	6.76	82.50	3.00	0.06	0.87
8.74	1.13	13.24	6.07	80.43	2.94	0.07	0.95
8.76	1.23	14.59	5.41	78.97	2.87	0.07	1.05
8.78	1.39	16.60	4.87	80.80	2.81	0.07	1.20
8.80	1.51	18.08	4.62	83.53	2.78	0.08	1.31
8.82	1.59	19.10	4.60	87.88	2.78	0.08	1.39
8.85	1.59	19.08	4.80	91.57	2.80	0.08	1.38
8.86	1.61	19.27	4.94	95.26	2.82	0.08	1.39
8.88	1.61	19.33	5.20	100.49	2.85	0.08	1.39
8.90	1.61	19.34	5.51	106.57	2.88	0.08	1.39
8.92	1.62	19.48	5.74	111.82	2.90	0.07	1.39
8.94	1.67	20.12	5.63	113.28	2.89	0.08	1.44
8.96	1.72	20.66	5.48	113.15	2.88	0.08	1.48
8.98	1.74	20.87	5.47	114.15	2.88	0.08	1.50
9.00	1.71	20.46	5.68	116.25	2.90	0.08	1.46
9.02	1.69	20.16	5.83	117.50	2.91	0.07	1.44
9.05	1.67	19.91	5.93	117.98	2.92	0.07	1.42
9.07	1.66	19.73	6.03	118.94	2.93	0.07	1.41
9.08	1.62	19.15	6.37	122.06	2.97	0.07	1.37
9.10	1.54	18.07	6.89	124.56	3.01	0.07	1.29
9.12	1.45	16.86	7.51	126.56	3.07	0.07	1.20
9.15	1.37	15.76	8.02	126.49	3.11	0.07	1.13
9.16	1.30	14.76	8.64	127.58	3.16	0.07	1.05
9.18	1.23	13.83	9.29	128.43	3.20	0.07	0.99
9.20	1.17	13.12	9.78	128.28	3.24	0.06	0.94
9.22	1.14	12.67	10.00	126.67	3.25	0.06	0.91
9.24	1.14	12.54	9.88	123.94	3.24	0.06	0.90
9.26	1.13	12.41	9.70	120.36	3.23	0.06	0.89
9.29	1.12	12.32	9.42	116.10	3.21	0.06	0.88
9.31	1.11	12.17	9.12	111.04	3.19	0.06	0.87
9.32	1.11	12.13	8.84	107.26	3.17	0.06	0.87
9.34	1.11	12.10	8.66	104.79	3.16	0.06	0.86
9.36	1.11	12.09	8.63	104.33	3.15	0.06	0.86
9.38	1.12	12.17	8.60	104.75	3.15	0.06	0.87
9.40	1.13	12.17	8.66	105.39	3.16	0.06	0.87
9.42	1.13	12.23	8.69	106.23	3.16	0.06	0.87
9.44	1.13	12.21	8.76	107.05	3.16	0.06	0.87
9.46	1.15	12.33	8.72	107.49	3.16	0.06	0.88
9.48	1.16	12.50	8.64	107.94	3.16	0.06	0.89
9.50	1.18	12.72	8.57	109.04	3.15	0.06	0.91
9.52	1.18	12.71	8.70	110.63	3.16	0.07	0.91
9.54	1.16	12.45	9.01	112.16	3.18	0.06	0.89
9.56	1.13	12.04	9.37	112.79	3.21	0.06	0.86
9.58	1.10	11.62	9.75	113.33	3.24	0.06	0.83
9.60	1.07	11.17	10.18	113.71	3.26	0.06	0.80

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.62	1.03	10.71	10.64	113.94	3.29	0.06	0.77
9.64	1.02	10.52	10.80	113.62	3.31	0.06	0.75
9.66	1.04	10.75	10.52	113.03	3.29	0.06	0.77
9.68	1.07	11.06	10.14	112.11	3.26	0.06	0.79
9.70	1.10	11.42	9.71	110.98	3.23	0.06	0.82
9.72	1.12	11.64	9.39	109.22	3.21	0.06	0.83
9.74	1.14	11.86	9.01	106.88	3.18	0.06	0.85
9.76	1.15	11.97	8.73	104.55	3.16	0.06	0.85
9.78	1.19	12.37	8.23	101.84	3.12	0.06	0.88
9.80	1.21	12.64	7.98	100.90	3.10	0.07	0.90
9.82	1.23	12.82	7.90	101.20	3.10	0.07	0.92
9.85	1.22	12.68	8.14	103.26	3.12	0.06	0.91
9.86	1.22	12.64	8.31	105.04	3.13	0.07	0.90
9.88	1.22	12.60	8.51	107.23	3.15	0.07	0.90
9.90	1.20	12.39	8.85	109.67	3.17	0.06	0.89
9.92	1.20	12.28	9.12	112.03	3.19	0.06	0.88
9.94	1.19	12.24	9.27	113.41	3.20	0.06	0.87
9.96	1.21	12.35	9.24	114.10	3.20	0.06	0.88
9.98	1.22	12.48	9.13	113.98	3.19	0.07	0.89
10.00	1.23	12.63	8.95	113.00	3.18	0.07	0.90
10.02	1.25	12.79	8.73	111.69	3.16	0.07	0.91
10.04	1.25	12.78	8.66	110.71	3.16	0.07	0.91
10.06	1.25	12.76	8.67	110.62	3.16	0.07	0.91
10.08	1.25	12.64	8.78	110.91	3.17	0.07	0.90
10.10	1.24	12.59	8.84	111.34	3.17	0.07	0.90
10.12	1.23	12.44	8.98	111.72	3.18	0.07	0.89
10.14	1.23	12.33	9.08	111.98	3.19	0.06	0.88
10.16	1.23	12.31	9.11	112.16	3.19	0.06	0.88
10.18	1.23	12.32	9.12	112.30	3.19	0.07	0.88
10.20	1.23	12.28	9.15	112.30	3.19	0.06	0.88
10.22	1.22	12.16	9.22	112.17	3.20	0.06	0.87
10.24	1.22	12.15	9.23	112.12	3.20	0.06	0.87
10.26	1.24	12.36	9.08	112.19	3.19	0.06	0.88
10.28	1.29	12.84	8.76	112.49	3.16	0.07	0.92
10.30	1.34	13.44	8.38	112.65	3.14	0.07	0.96
10.32	1.37	13.68	8.26	113.00	3.13	0.07	0.98
10.34	1.36	13.60	8.35	113.57	3.13	0.07	0.97
10.36	1.33	13.26	8.61	114.18	3.15	0.07	0.95
10.38	1.32	13.07	8.77	114.62	3.16	0.07	0.93
10.40	1.32	13.01	8.79	114.46	3.17	0.07	0.93
10.42	1.33	13.16	8.67	114.13	3.16	0.07	0.94
10.44	1.37	13.52	8.43	113.97	3.14	0.07	0.97
10.46	1.42	14.04	8.10	113.73	3.11	0.07	1.00
10.48	1.48	14.73	7.67	112.92	3.08	0.07	1.05
10.50	1.54	15.37	7.28	111.92	3.05	0.07	1.10
10.52	1.58	15.81	7.08	111.91	3.03	0.07	1.13
10.54	1.59	15.87	7.13	113.18	3.03	0.07	1.13
10.56	1.58	15.71	7.29	114.62	3.05	0.07	1.12

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
10.58	1.58	15.70	7.34	115.22	3.05	0.07	1.12
10.60	1.60	15.86	7.29	115.69	3.05	0.07	1.13
10.62	1.61	16.02	7.30	116.95	3.05	0.07	1.14
10.64	1.62	16.09	7.41	119.20	3.06	0.07	1.15
10.66	1.63	16.09	7.55	121.45	3.07	0.07	1.15
10.68	1.64	16.17	7.63	123.35	3.08	0.07	1.15
10.70	1.63	16.01	7.84	125.44	3.09	0.07	1.14
10.72	1.61	15.76	8.09	127.56	3.11	0.07	1.13
10.74	1.59	15.52	8.31	128.92	3.13	0.07	1.11
10.77	1.59	15.46	8.32	128.70	3.13	0.07	1.10
10.78	1.58	15.38	8.34	128.32	3.13	0.07	1.10
10.80	1.56	15.14	8.45	127.95	3.14	0.07	1.08
10.82	1.53	14.73	8.67	127.73	3.16	0.07	1.05
10.84	1.50	14.35	8.85	127.03	3.17	0.07	1.02
10.86	1.48	14.16	8.91	126.12	3.18	0.07	1.01
10.88	1.47	14.02	8.95	125.49	3.18	0.07	1.00
10.91	1.45	13.78	9.03	124.48	3.18	0.07	0.98
10.92	1.42	13.41	9.22	123.60	3.20	0.07	0.96
10.95	1.38	12.86	9.50	122.18	3.22	0.07	0.92
10.96	1.35	12.57	9.62	120.89	3.23	0.07	0.90
10.98	1.33	12.32	9.69	119.44	3.23	0.07	0.88
11.00	1.32	12.21	9.67	118.02	3.23	0.07	0.87
11.02	1.30	11.96	9.75	116.66	3.24	0.07	0.85
11.04	1.29	11.79	9.80	115.53	3.24	0.06	0.84
11.06	1.29	11.74	9.75	114.41	3.23	0.06	0.84
11.09	1.28	11.69	9.70	113.42	3.23	0.06	0.83
11.10	1.28	11.64	9.68	112.72	3.23	0.06	0.83
11.13	1.29	11.66	9.62	112.22	3.23	0.06	0.83
11.15	1.30	11.73	9.54	111.88	3.22	0.07	0.84
11.16	1.31	11.87	9.40	111.61	3.21	0.07	0.85
11.18	1.32	11.94	9.33	111.40	3.21	0.07	0.85
11.20	1.34	12.15	9.15	111.22	3.19	0.07	0.87
11.22	1.36	12.32	9.02	111.20	3.18	0.07	0.88
11.24	1.38	12.48	8.91	111.20	3.18	0.07	0.89
11.26	1.40	12.66	8.77	111.05	3.16	0.07	0.90
11.28	1.41	12.80	8.63	110.54	3.15	0.07	0.91
11.30	1.41	12.79	8.60	110.00	3.15	0.07	0.91
11.32	1.40	12.66	8.64	109.38	3.16	0.07	0.90
11.34	1.40	12.56	8.64	108.48	3.16	0.07	0.90
11.36	1.39	12.45	8.60	107.08	3.15	0.07	0.89
11.38	1.37	12.19	8.69	105.99	3.16	0.07	0.87
11.40	1.34	11.88	8.86	105.23	3.17	0.07	0.85
11.42	1.33	11.74	8.94	104.95	3.18	0.06	0.84
11.44	1.35	11.98	8.73	104.50	3.16	0.07	0.86
11.46	1.38	12.28	8.44	103.68	3.14	0.07	0.88
11.48	1.40	12.43	8.24	102.43	3.12	0.07	0.89
11.50	1.39	12.29	8.20	100.80	3.12	0.07	0.88
11.52	1.37	12.08	8.23	99.39	3.12	0.07	0.86

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
11.54	1.36	11.88	8.27	98.25	3.13	0.07	0.85
11.56	1.33	11.62	8.41	97.72	3.14	0.07	0.83
11.58	1.30	11.31	8.60	97.25	3.15	0.06	0.81
11.60	1.28	11.03	8.82	97.24	3.17	0.06	0.79
11.62	1.26	10.81	9.02	97.47	3.18	0.06	0.77
11.64	1.25	10.69	9.17	98.00	3.19	0.06	0.76
11.66	1.25	10.64	9.25	98.45	3.20	0.06	0.76
11.68	1.24	10.55	9.38	98.99	3.21	0.06	0.75
11.70	1.23	10.38	9.56	99.15	3.22	0.06	0.74
11.72	1.20	10.08	9.72	98.07	3.23	0.06	0.72
11.74	1.16	9.65	9.86	95.19	3.24	0.06	0.69
11.76	1.17	9.71	9.61	93.35	3.23	0.06	0.69
11.78	1.18	9.78	9.49	92.79	3.22	0.06	0.70
11.80	1.19	9.94	9.42	93.64	3.21	0.06	0.71
11.82	1.16	9.61	9.76	93.74	3.24	0.06	0.69
11.84	1.13	9.28	10.04	93.19	3.25	0.06	0.66
11.86	1.10	8.94	10.39	92.84	3.28	0.06	0.64
11.88	1.06	8.56	10.78	92.32	3.30	0.06	0.61
11.90	1.02	8.11	11.31	91.79	3.34	0.06	0.58
11.92	0.97	7.56	11.94	90.27	3.38	0.06	0.54
11.94	0.91	6.97	12.63	87.97	3.42	0.06	0.50
11.96	0.84	6.28	13.56	85.10	3.47	0.06	0.45
11.98	0.77	5.59	14.74	82.43	3.54	0.06	0.40
12.00	0.71	4.93	16.16	79.69	3.61	0.06	0.35
12.02	0.65	4.38	17.38	76.06	3.67	0.06	0.31
12.04	0.61	3.92	18.28	71.68	3.71	0.06	0.28
12.06	0.57	3.55	18.80	66.84	3.74	0.06	0.25
12.08	0.55	3.28	19.06	62.52	3.75	0.06	0.23
12.10	0.53	3.16	18.63	58.88	3.73	0.06	0.23
12.12	0.54	3.25	17.27	56.12	3.66	0.06	0.23
12.14	0.60	3.75	14.72	55.15	3.53	0.06	0.27
12.16	0.70	4.72	11.81	55.72	3.37	0.06	0.34
12.18	0.83	6.02	9.41	56.64	3.21	0.06	0.43
12.20	0.94	7.06	8.21	57.96	3.12	0.06	0.50
12.22	1.03	8.01	7.44	59.55	3.06	0.06	0.57
12.24	1.14	9.02	6.86	61.94	3.01	0.06	0.64
12.27	1.27	10.25	6.29	64.40	2.96	0.06	0.73
12.28	1.35	11.05	6.12	67.60	2.94	0.07	0.79
12.30	1.31	10.59	6.63	70.22	2.99	0.07	0.76
12.32	1.14	8.97	7.91	70.99	3.10	0.06	0.64
12.34	0.91	6.71	10.05	67.43	3.26	0.06	0.48
12.36	0.74	5.03	12.24	61.56	3.39	0.06	0.36
12.38	0.66	4.23	13.35	56.49	3.46	0.06	0.30
12.40	0.63	4.01	13.66	54.80	3.48	0.06	0.29
12.42	0.63	4.00	13.72	54.94	3.48	0.06	0.29
12.44	0.61	3.78	14.43	54.51	3.52	0.06	0.27
12.46	0.59	3.54	15.11	53.45	3.55	0.06	0.25
12.48	0.56	3.24	15.94	51.70	3.60	0.06	0.23

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
12.50	0.55	3.21	15.89	50.99	3.59	0.06	0.23
12.52	0.58	3.45	14.83	51.09	3.54	0.06	0.25
12.54	0.61	3.69	13.85	51.04	3.49	0.06	0.26
12.56	0.63	3.88	13.14	51.02	3.45	0.06	0.28
12.58	0.64	4.04	12.69	51.19	3.42	0.06	0.29
12.60	0.69	4.42	11.81	52.16	3.37	0.06	0.32
12.62	0.74	4.93	10.80	53.22	3.31	0.06	0.35
12.64	0.80	5.46	10.05	54.91	3.26	0.06	0.39
12.66	0.84	5.90	9.66	56.97	3.23	0.06	0.42
12.68	0.87	6.19	9.54	59.04	3.22	0.06	0.44
12.70	0.91	6.50	9.32	60.54	3.20	0.06	0.46
12.72	0.94	6.82	9.04	61.66	3.18	0.06	0.49
12.74	0.99	7.24	8.71	63.06	3.16	0.06	0.52
12.76	1.04	7.69	8.42	64.75	3.14	0.06	0.55
12.78	1.07	7.92	8.45	66.97	3.14	0.06	0.57
12.80	1.07	7.96	8.69	69.18	3.16	0.06	0.57
12.82	1.05	7.74	9.21	71.29	3.20	0.06	0.55
12.84	1.03	7.56	9.68	73.19	3.23	0.06	0.54
12.86	1.01	7.31	10.28	75.19	3.27	0.06	0.52
12.88	0.97	7.01	10.98	76.94	3.32	0.06	0.50
12.90	0.95	6.76	11.57	78.14	3.35	0.06	0.48
12.94	0.94	6.64	11.82	78.50	3.37	0.06	0.47
12.94	0.93	6.59	11.89	78.36	3.37	0.06	0.47
12.96	0.92	6.41	12.14	77.79	3.39	0.06	0.46
12.99	0.89	6.11	12.56	76.77	3.41	0.06	0.44
13.00	0.86	5.88	12.88	75.72	3.43	0.06	0.42
13.03	0.83	5.61	13.21	74.10	3.45	0.06	0.40
13.04	0.82	5.43	13.40	72.79	3.46	0.06	0.39
13.06	0.80	5.28	13.57	71.67	3.47	0.06	0.38
13.08	0.81	5.37	13.21	70.89	3.45	0.06	0.38
13.10	0.83	5.49	12.83	70.38	3.43	0.06	0.39
13.13	0.86	5.80	11.98	69.53	3.38	0.06	0.41
13.14	0.91	6.20	11.08	68.72	3.32	0.06	0.44
13.16	0.98	6.83	9.85	67.29	3.24	0.06	0.49
13.18	1.04	7.42	8.92	66.16	3.18	0.06	0.53
13.20	1.11	8.06	8.14	65.66	3.12	0.06	0.58
13.22	1.16	8.46	7.86	66.49	3.09	0.06	0.60
13.24	1.18	8.64	7.93	68.44	3.10	0.06	0.62
13.26	1.17	8.53	8.32	70.98	3.13	0.06	0.61
13.28	1.14	8.27	8.91	73.69	3.18	0.06	0.59
13.30	1.12	8.05	9.44	76.03	3.21	0.06	0.58
13.32	1.11	7.92	9.81	77.75	3.24	0.06	0.57
13.34	1.10	7.87	9.98	78.53	3.25	0.06	0.56
13.36	1.10	7.82	10.03	78.45	3.25	0.06	0.56
13.38	1.09	7.75	10.05	77.89	3.26	0.06	0.55
13.40	1.08	7.62	10.11	77.10	3.26	0.06	0.54
13.42	1.06	7.45	10.24	76.24	3.27	0.06	0.53
13.44	1.04	7.23	10.43	75.40	3.28	0.06	0.52

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
13.46	1.03	7.13	10.49	74.82	3.29	0.06	0.51
13.48	1.03	7.15	10.43	74.53	3.28	0.06	0.51
13.50	1.03	7.13	10.41	74.22	3.28	0.06	0.51
13.52	1.02	7.03	10.48	73.70	3.28	0.06	0.50
13.54	1.00	6.85	10.69	73.23	3.30	0.06	0.49
13.56	0.99	6.71	10.86	72.83	3.31	0.06	0.48
13.58	0.99	6.72	10.83	72.74	3.31	0.06	0.48
13.60	1.01	6.84	10.65	72.82	3.30	0.06	0.49
13.62	1.04	7.11	10.26	72.94	3.27	0.06	0.51
13.64	1.07	7.36	9.89	72.77	3.25	0.06	0.53
13.66	1.09	7.55	9.62	72.61	3.23	0.06	0.54
13.68	1.10	7.62	9.56	72.81	3.22	0.06	0.54
13.70	1.10	7.61	9.66	73.55	3.23	0.06	0.54
13.72	1.10	7.63	9.76	74.49	3.24	0.06	0.54
13.74	1.11	7.67	9.85	75.50	3.24	0.06	0.55
13.76	1.12	7.71	9.91	76.45	3.25	0.06	0.55
13.79	1.11	7.67	10.09	77.42	3.26	0.06	0.55
13.80	1.11	7.60	10.31	78.39	3.27	0.06	0.54
13.82	1.11	7.59	10.44	79.22	3.28	0.06	0.54
13.85	1.11	7.59	10.53	79.95	3.29	0.06	0.54
13.86	1.12	7.71	10.47	80.71	3.28	0.06	0.55
13.88	1.14	7.84	10.36	81.25	3.28	0.06	0.56
13.90	1.14	7.81	10.46	81.75	3.28	0.06	0.56
13.92	1.13	7.68	10.70	82.18	3.30	0.06	0.55
13.94	1.09	7.39	11.14	82.35	3.33	0.06	0.53
13.96	1.07	7.17	11.42	81.88	3.34	0.06	0.51
13.98	1.05	7.00	11.56	80.88	3.35	0.06	0.50
14.00	1.05	6.96	11.44	79.63	3.35	0.06	0.50
14.02	1.07	7.11	11.05	78.61	3.32	0.06	0.51
14.04	1.09	7.30	10.64	77.73	3.30	0.06	0.52
14.06	1.13	7.58	10.20	77.33	3.27	0.06	0.54
14.08	1.15	7.81	9.81	76.63	3.24	0.06	0.56
14.10	1.17	7.96	9.56	76.07	3.22	0.06	0.57
14.12	1.18	8.03	9.42	75.65	3.21	0.06	0.57
14.14	1.20	8.20	9.28	76.08	3.20	0.06	0.59
14.16	1.23	8.42	9.11	76.77	3.19	0.06	0.60
14.18	1.26	8.65	8.92	77.17	3.18	0.06	0.62
14.20	1.28	8.85	8.74	77.33	3.16	0.06	0.63
14.22	1.32	9.16	8.46	77.49	3.14	0.06	0.65
14.24	1.35	9.42	8.34	78.61	3.13	0.06	0.67
14.26	1.39	9.74	8.20	79.90	3.12	0.06	0.70
14.28	1.42	9.96	8.19	81.52	3.12	0.06	0.71
14.30	1.45	10.20	8.14	83.09	3.12	0.06	0.73
14.32	1.46	10.30	8.27	85.15	3.13	0.06	0.74
14.34	1.46	10.26	8.55	87.72	3.15	0.06	0.73
14.36	1.46	10.22	8.83	90.16	3.17	0.06	0.73
14.38	1.46	10.22	9.00	91.98	3.18	0.06	0.73
14.40	1.48	10.39	8.98	93.28	3.18	0.06	0.74

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
14.42	1.51	10.55	8.91	94.03	3.18	0.06	0.75
14.44	1.52	10.64	8.91	94.80	3.18	0.07	0.76
14.46	1.52	10.65	8.94	95.23	3.18	0.07	0.76
14.48	1.51	10.54	9.08	95.64	3.19	0.07	0.75
14.50	1.49	10.33	9.28	95.81	3.20	0.06	0.74
14.52	1.45	10.04	9.55	95.84	3.22	0.06	0.72
14.54	1.41	9.66	9.92	95.85	3.25	0.06	0.69
14.56	1.38	9.41	10.17	95.68	3.26	0.06	0.67
14.58	1.38	9.36	10.18	95.35	3.26	0.06	0.67
14.60	1.41	9.56	9.94	95.02	3.25	0.06	0.68
14.62	1.43	9.72	9.76	94.89	3.24	0.06	0.69
14.64	1.44	9.81	9.70	95.18	3.23	0.06	0.70
14.66	1.45	9.87	9.65	95.28	3.23	0.06	0.71
14.68	1.47	10.01	9.54	95.49	3.22	0.06	0.71
14.70	1.49	10.14	9.40	95.38	3.21	0.06	0.72
14.72	1.44	9.75	9.56	93.20	3.22	0.06	0.70
14.74	1.46	9.90	9.31	92.23	3.20	0.06	0.71
14.76	1.47	9.97	9.16	91.25	3.19	0.07	0.71
14.78	1.53	10.41	8.86	92.23	3.17	0.06	0.74
14.81	1.51	10.28	8.90	91.50	3.17	0.06	0.73
14.83	1.51	10.24	8.85	90.67	3.17	0.06	0.73
14.84	1.52	10.33	8.73	90.12	3.16	0.06	0.74
14.86	1.53	10.35	8.70	90.06	3.16	0.06	0.74
14.88	1.53	10.37	8.76	90.89	3.16	0.06	0.74
14.90	1.53	10.31	8.97	92.50	3.18	0.06	0.74
14.92	1.52	10.27	9.18	94.31	3.20	0.06	0.73
14.94	1.51	10.18	9.44	96.08	3.21	0.06	0.73
14.96	1.50	10.05	9.73	97.73	3.23	0.06	0.72
14.98	1.47	9.81	10.11	99.18	3.26	0.06	0.70
15.01	1.44	9.49	10.53	99.92	3.29	0.06	0.68
15.02	1.41	9.30	10.76	100.03	3.30	0.06	0.66
15.04	1.42	9.32	10.69	99.64	3.30	0.06	0.67
15.06	1.46	9.61	10.33	99.27	3.27	0.06	0.69
15.08	1.52	10.10	9.79	98.87	3.24	0.06	0.72
15.10	1.59	10.68	9.18	97.98	3.19	0.07	0.76
15.12	1.67	11.26	8.54	96.07	3.15	0.07	0.80
15.14	1.77	12.07	7.72	93.22	3.08	0.07	0.86
15.16	1.89	12.99	6.95	90.35	3.02	0.07	0.93
15.18	2.01	13.98	6.32	88.28	2.96	0.07	1.00
15.20	2.09	14.59	6.06	88.42	2.94	0.07	1.04
15.22	2.13	14.86	6.09	90.47	2.94	0.07	1.06
15.24	2.11	14.65	6.44	94.36	2.97	0.07	1.05
15.26	2.06	14.22	6.89	98.05	3.01	0.07	1.02
15.28	1.98	13.59	7.51	102.07	3.07	0.07	0.97
15.30	1.90	12.96	8.16	105.73	3.12	0.07	0.93
15.32	1.83	12.38	8.82	109.14	3.17	0.07	0.88
15.34	1.73	11.54	9.62	111.00	3.23	0.07	0.82
15.37	1.63	10.76	10.33	111.15	3.27	0.07	0.77

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
15.38	1.48	9.57	11.48	109.82	3.35	0.06	0.68
15.40	1.37	8.63	12.46	107.57	3.41	0.06	0.62
15.42	1.25	7.70	13.55	104.36	3.47	0.06	0.55
15.44	1.20	7.26	13.86	100.64	3.49	0.06	0.52
15.46	1.16	6.94	13.94	96.67	3.49	0.06	0.50
15.48	1.12	6.66	13.95	92.90	3.49	0.06	0.48
15.50	1.08	6.29	14.27	89.68	3.51	0.06	0.45
15.52	1.03	5.90	14.68	86.61	3.53	0.06	0.42
15.54	0.99	5.59	14.91	83.40	3.54	0.06	0.40
15.56	0.96	5.36	14.93	80.08	3.55	0.06	0.38
15.58	0.94	5.20	14.81	76.98	3.54	0.06	0.37
15.60	0.93	5.09	14.58	74.15	3.53	0.06	0.36
15.62	0.92	5.02	14.24	71.52	3.51	0.06	0.36
15.64	0.92	5.02	13.77	69.08	3.48	0.06	0.36
15.66	0.91	4.95	13.47	66.63	3.47	0.06	0.35
15.68	0.91	4.88	13.21	64.47	3.45	0.06	0.35
15.70	0.89	4.76	13.11	62.41	3.45	0.06	0.34
15.72	0.87	4.55	12.91	58.79	3.43	0.06	0.33
15.74	0.88	4.65	12.30	57.18	3.40	0.06	0.33
15.76	0.92	4.92	11.52	56.66	3.35	0.06	0.35
15.78	0.96	5.28	11.12	58.71	3.33	0.06	0.38
15.80	0.98	5.37	11.07	59.43	3.32	0.06	0.38
15.82	0.98	5.37	11.08	59.52	3.32	0.06	0.38
15.84	1.00	5.51	10.76	59.28	3.30	0.06	0.39
15.86	1.03	5.76	10.21	58.86	3.27	0.06	0.41
15.88	1.07	6.06	9.64	58.46	3.23	0.06	0.43
15.90	1.11	6.37	9.16	58.33	3.19	0.06	0.45
15.92	1.13	6.52	8.93	58.26	3.18	0.06	0.47
15.94	1.13	6.46	9.01	58.23	3.18	0.06	0.46
15.96	1.09	6.14	9.47	58.20	3.22	0.06	0.44
15.98	1.04	5.76	10.11	58.22	3.26	0.06	0.41
16.00	1.00	5.48	10.61	58.10	3.29	0.06	0.39
16.03	0.98	5.31	10.89	57.79	3.31	0.06	0.38
16.04	0.96	5.17	11.09	57.32	3.32	0.06	0.37
16.06	0.94	5.00	11.35	56.76	3.34	0.06	0.36
16.08	0.93	4.88	11.48	56.02	3.35	0.06	0.35
16.10	0.92	4.84	11.43	55.30	3.35	0.06	0.35
16.12	0.92	4.82	11.29	54.47	3.34	0.06	0.34
16.14	0.92	4.83	11.11	53.64	3.33	0.06	0.34
16.16	0.92	4.80	11.03	53.01	3.32	0.06	0.34
16.18	0.93	4.86	10.84	52.66	3.31	0.06	0.35
16.20	0.93	4.86	10.79	52.46	3.30	0.06	0.35
16.22	0.94	4.89	10.66	52.18	3.30	0.06	0.35
16.24	0.93	4.86	10.69	51.97	3.30	0.06	0.35
16.26	0.94	4.87	10.72	52.14	3.30	0.06	0.35
16.28	0.93	4.83	10.84	52.39	3.31	0.06	0.35
16.30	0.93	4.81	10.90	52.44	3.31	0.06	0.34
16.32	0.93	4.81	10.85	52.20	3.31	0.06	0.34

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
16.34	0.93	4.83	10.76	51.97	3.30	0.06	0.34
16.36	0.94	4.85	10.69	51.86	3.30	0.06	0.35
16.38	0.95	4.90	10.58	51.83	3.29	0.06	0.35
16.40	0.95	4.96	10.38	51.50	3.28	0.06	0.35
16.42	0.98	5.11	10.02	51.21	3.25	0.06	0.36
16.44	1.00	5.28	9.68	51.11	3.23	0.06	0.38
16.46	1.03	5.50	9.35	51.41	3.21	0.06	0.39
16.48	1.05	5.66	9.19	51.98	3.20	0.06	0.40
16.50	1.06	5.71	9.19	52.47	3.20	0.06	0.41
16.52	1.05	5.64	9.41	53.09	3.21	0.06	0.40
16.54	1.03	5.50	9.70	53.38	3.23	0.06	0.39
16.56	1.02	5.40	9.94	53.71	3.25	0.06	0.39
16.58	1.02	5.39	9.98	53.79	3.25	0.06	0.38
16.60	1.03	5.42	9.95	53.90	3.25	0.06	0.39
16.62	1.03	5.44	9.84	53.59	3.24	0.06	0.39
16.64	1.03	5.43	9.80	53.22	3.24	0.06	0.39
16.66	1.03	5.39	9.70	52.32	3.23	0.06	0.39
16.68	1.02	5.37	9.61	51.58	3.23	0.06	0.38
16.70	1.03	5.37	9.50	51.00	3.22	0.06	0.38
16.72	1.11	5.97	8.92	53.27	3.18	0.06	0.43
16.74	1.16	6.36	8.80	55.98	3.17	0.06	0.45
16.76	1.18	6.47	9.03	58.41	3.18	0.06	0.46
16.78	1.10	5.86	9.96	58.39	3.25	0.06	0.42
16.80	1.04	5.42	10.59	57.33	3.29	0.06	0.39
16.82	1.02	5.28	10.64	56.13	3.29	0.06	0.38
16.84	1.03	5.33	10.37	55.34	3.28	0.06	0.38
16.86	1.06	5.54	9.92	54.98	3.25	0.06	0.40
16.88	1.11	5.88	9.39	55.14	3.21	0.06	0.42
16.91	1.17	6.36	8.70	55.36	3.16	0.06	0.45
16.92	1.27	7.07	7.80	55.18	3.09	0.06	0.51
16.94	1.34	7.52	7.26	54.63	3.05	0.06	0.54
16.96	1.34	7.51	7.35	55.17	3.05	0.06	0.54
16.98	1.29	7.19	7.82	56.24	3.09	0.06	0.51
17.00	1.29	7.15	8.05	57.50	3.11	0.06	0.51
17.02	1.32	7.39	7.85	58.00	3.09	0.06	0.53
17.04	1.36	7.62	7.65	58.27	3.08	0.06	0.54
17.06	1.34	7.46	7.89	58.91	3.10	0.06	0.53
17.08	1.28	7.07	8.37	59.18	3.13	0.06	0.51
17.10	1.23	6.65	8.93	59.45	3.18	0.06	0.48
17.18	1.20	6.40	9.25	59.16	3.20	0.06	0.46
17.18	1.19	6.37	9.27	59.10	3.20	0.06	0.46
17.18	1.19	6.39	9.25	59.10	3.20	0.06	0.46
17.18	1.34	7.43	8.20	60.94	3.12	0.06	0.53
17.20	1.43	8.10	7.68	62.17	3.08	0.06	0.58
17.22	1.53	8.75	7.21	63.08	3.04	0.06	0.62
17.24	1.47	8.36	7.52	62.80	3.07	0.06	0.60
17.26	1.46	8.25	7.61	62.82	3.07	0.06	0.59
17.28	1.45	8.19	7.73	63.33	3.08	0.06	0.59

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
17.30	1.44	8.06	7.89	63.61	3.10	0.06	0.58
17.32	1.39	7.74	8.20	63.43	3.12	0.06	0.55
17.34	1.30	7.09	8.86	62.80	3.17	0.06	0.51
17.36	1.20	6.33	9.73	61.58	3.23	0.06	0.45
17.38	1.12	5.80	10.44	60.55	3.28	0.06	0.41
17.40	1.10	5.59	10.67	59.69	3.30	0.06	0.40
17.42	1.09	5.55	10.69	59.31	3.30	0.06	0.40
17.44	1.08	5.48	10.74	58.84	3.30	0.06	0.39
17.46	1.06	5.33	10.87	57.97	3.31	0.06	0.38
17.48	1.05	5.24	10.82	56.64	3.31	0.06	0.37
17.50	1.10	5.60	9.87	55.26	3.24	0.06	0.40
17.52	1.28	6.84	7.94	54.28	3.10	0.06	0.49
17.54	1.57	8.87	6.03	53.52	2.93	0.07	0.63
17.56	1.85	10.84	4.96	53.80	2.82	0.07	0.77
17.58	2.00	11.93	4.77	56.86	2.80	0.08	0.85
17.60	2.10	12.59	4.86	61.11	2.81	0.08	0.90
17.62	2.16	12.96	5.04	65.28	2.83	0.08	0.93
17.64	2.17	13.02	5.35	69.59	2.86	0.08	0.93
17.66	2.03	11.99	6.18	74.09	2.95	0.07	0.86
17.68	1.80	10.38	7.50	77.90	3.07	0.07	0.74
17.70	1.65	9.32	8.42	78.46	3.14	0.06	0.67
17.72	1.78	10.25	7.84	80.32	3.09	0.06	0.73
17.74	1.93	11.27	7.23	81.48	3.04	0.07	0.81
17.76	2.01	11.82	7.07	83.48	3.03	0.07	0.84
17.78	1.88	10.89	7.58	82.52	3.07	0.07	0.78
17.80	1.76	10.00	8.04	80.42	3.11	0.07	0.71
17.82	1.62	9.07	8.60	77.99	3.15	0.06	0.65
17.84	1.47	7.99	9.47	75.67	3.22	0.06	0.57
17.86	1.41	7.58	9.75	73.91	3.24	0.06	0.54
17.88	1.59	8.78	8.32	73.03	3.13	0.06	0.63
17.90	1.98	11.44	6.29	71.97	2.96	0.07	0.82
17.92	2.35	14.04	5.12	71.81	2.84	0.08	1.00
17.94	2.53	15.23	4.86	74.07	2.81	0.08	1.09
17.96	2.47	14.76	5.19	76.60	2.85	0.08	1.05
17.98	2.37	14.08	5.62	79.10	2.89	0.08	1.01
18.00	2.39	14.19	5.66	80.29	2.90	0.08	1.01
18.02	2.54	15.20	5.38	81.78	2.87	0.08	1.09
18.04	2.84	17.31	4.86	84.18	2.81	0.08	1.23
18.06	3.05	18.75	4.70	88.22	2.79	0.09	1.33
18.08	3.10	18.99	4.87	92.45	2.81	0.09	1.35
18.10	3.00	18.27	5.19	94.80	2.85	0.08	1.30
18.12	2.97	18.01	5.22	94.09	2.85	0.08	1.29
18.14	2.99	18.18	5.01	90.98	2.83	0.09	1.30
18.16	2.79	16.77	5.31	89.09	2.86	0.08	1.20
18.18	2.39	14.04	6.34	89.01	2.96	0.07	1.00
18.20	1.89	10.63	8.30	88.26	3.13	0.07	0.76
18.22	1.57	8.48	10.00	84.81	3.25	0.06	0.61
18.24	1.55	8.31	9.67	80.33	3.23	0.06	0.59

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
18.26	1.81	10.07	7.66	77.13	3.08	0.07	0.72
18.28	2.20	12.64	5.86	74.07	2.92	0.07	0.90
18.30	2.41	14.09	5.20	73.23	2.85	0.08	1.01
18.32	2.59	15.27	4.79	73.18	2.80	0.08	1.09
18.34	2.93	17.79	4.20	74.62	2.73	0.08	1.25
18.36	3.53	22.18	3.46	76.66	2.62	0.09	1.54
18.38	4.06	26.13	3.02	78.91	2.55	0.10	0.65
18.40	4.33	28.10	2.89	81.06	2.52	0.10	0.66
18.42	4.36	28.20	2.93	82.70	2.53	0.10	0.66
18.44	4.31	27.73	3.05	84.48	2.55	0.10	0.66
18.46	4.25	27.26	3.10	84.38	2.56	0.10	0.66
18.48	4.21	26.95	3.11	83.92	2.56	0.10	0.66
18.50	4.22	26.95	3.11	83.82	2.56	0.10	0.66
18.52	4.15	26.36	3.28	86.40	2.59	0.10	0.66
18.54	4.07	25.59	3.48	89.17	2.63	0.10	1.77
18.58	3.60	21.99	4.23	93.05	2.73	0.10	1.55
18.58	3.17	18.82	5.05	95.00	2.83	0.08	1.34
18.60	2.81	16.45	5.73	94.29	2.90	0.08	1.18
18.62	2.90	17.00	5.21	88.51	2.85	0.08	1.21
18.64	3.10	18.43	4.63	85.26	2.78	0.09	1.31
18.66	3.38	20.40	4.16	84.81	2.72	0.09	1.43
18.68	3.76	23.08	3.88	89.46	2.68	0.09	1.61
18.70	4.21	26.27	3.52	92.46	2.63	0.10	1.82
18.72	4.57	28.95	3.23	93.50	2.58	0.10	0.67
18.74	4.81	30.75	2.96	90.97	2.54	0.11	0.67
18.76	4.95	31.94	2.66	85.06	2.48	0.10	0.68
18.78	5.00	32.59	2.41	78.52	2.42	0.10	0.68
18.80	4.97	32.58	2.21	71.83	2.37	0.10	0.68
18.82	4.87	32.04	2.06	65.98	2.33	0.09	0.68
18.84	4.72	31.13	1.98	61.61	2.31	0.09	0.68
18.86	4.59	30.18	1.94	58.52	2.30	0.09	0.67
18.88	4.47	29.36	1.93	56.52	2.29	0.09	0.67
18.90	4.44	29.08	1.95	56.57	2.30	0.09	0.67
18.92	4.50	29.36	2.03	59.72	2.33	0.09	0.67
18.94	4.69	30.43	2.16	65.82	2.36	0.09	0.67
18.96	5.00	32.54	2.22	72.36	2.38	0.10	0.68
18.98	5.31	34.69	2.21	76.79	2.38	0.10	0.69
19.07	5.52	36.00	2.18	78.62	2.37	0.11	0.69
19.07	5.58	36.45	2.17	79.08	2.36	0.10	0.69
19.07	5.86	38.42	2.13	81.75	2.35	0.10	0.70
19.08	6.62	44.10	1.97	86.76	2.31	0.11	0.72
19.10	7.66	51.99	1.74	90.36	2.23	0.12	0.74
19.12	8.43	58.11	1.56	90.91	2.16	0.13	0.75
19.22	8.71	60.25	1.47	88.80	2.11	0.12	0.76
19.22	8.69	60.30	1.45	87.38	2.10	0.12	0.76
19.14	8.12	56.40	1.44	81.05	2.09	0.12	0.75
19.22	7.40	51.13	1.42	72.46	2.08	0.10	0.74
19.24	6.60	45.50	1.38	62.85	2.06	0.09	0.72

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
19.26	6.16	42.16	1.40	59.19	2.07	0.09	0.71
19.28	5.64	38.15	1.46	55.78	2.10	0.08	0.70
19.30	5.01	33.33	1.00	33.33	2.15	0.08	0.68
19.32	4.44	28.90	1.00	28.90	2.20	0.08	0.67
19.34	3.96	25.24	1.85	46.68	2.27	0.08	0.65
19.36	3.57	22.12	2.19	48.37	2.37	0.08	0.63
19.38	3.21	19.17	2.80	53.61	2.51	0.09	0.62
19.40	2.86	16.30	3.81	62.19	2.67	0.08	1.14
19.42	2.60	14.34	4.78	68.51	2.80	0.08	1.02
19.44	2.51	13.72	5.37	73.62	2.87	0.08	0.98
19.46	2.58	14.10	5.42	76.47	2.87	0.08	1.01
19.48	2.78	15.37	5.29	81.32	2.86	0.08	1.10
19.50	3.14	17.60	4.97	87.47	2.82	0.09	1.26
19.52	3.83	22.23	4.18	92.94	2.72	0.09	1.56
19.54	4.90	29.80	3.19	94.96	2.58	0.10	0.67
19.56	6.18	39.21	2.40	94.15	2.42	0.12	0.70
19.58	7.20	47.00	1.97	92.58	2.31	0.12	0.73
19.60	7.73	51.25	1.74	89.37	2.23	0.12	0.74
19.62	7.77	51.92	1.63	84.41	2.18	0.12	0.74
19.64	7.53	50.48	1.56	78.89	2.15	0.11	0.74
19.66	7.04	47.00	1.56	73.18	2.15	0.10	0.73
19.68	6.36	42.12	1.57	66.11	2.16	0.10	0.71
19.70	5.51	35.88	1.66	59.58	2.20	0.09	0.69
19.72	4.89	31.35	1.76	55.11	2.24	0.08	0.68
19.74	4.53	28.56	1.90	54.40	2.29	0.09	0.66
19.76	4.52	28.49	1.92	54.61	2.29	0.09	0.66
19.78	4.63	29.22	1.90	55.57	2.29	0.09	0.67
19.81	4.95	31.60	1.78	56.41	2.25	0.09	0.68
19.82	5.38	34.89	1.64	57.10	2.19	0.09	0.69
19.84	5.75	37.79	1.52	57.62	2.14	0.09	0.70
19.86	5.82	38.31	1.49	57.16	2.12	0.09	0.70
19.88	5.48	35.75	1.55	55.40	2.15	0.09	0.69
19.90	4.86	31.08	1.68	52.09	2.20	0.08	0.67
19.92	4.24	26.45	1.85	48.90	2.27	0.08	0.66
19.94	3.79	23.21	2.00	46.40	2.32	0.08	0.64
19.96	3.52	20.94	2.36	49.32	2.41	0.08	0.63
19.98	3.26	18.78	2.97	55.81	2.54	0.09	0.62
20.00	3.01	16.64	3.95	65.75	2.69	0.09	1.16
20.02	2.73	14.57	5.07	73.83	2.83	0.08	1.04
20.04	2.36	12.33	6.43	79.30	2.97	0.07	0.88
20.06	1.99	9.99	8.04	80.33	3.11	0.07	0.71
20.08	1.68	8.09	9.58	77.50	3.22	0.06	0.58
20.10	1.60	7.61	9.75	74.22	3.24	0.06	0.54
20.12	1.62	7.75	9.26	71.78	3.20	0.06	0.55
20.14	1.80	8.82	8.27	72.89	3.13	0.06	0.63
20.16	2.45	12.78	5.93	75.79	2.92	0.07	0.91
20.18	3.62	20.36	3.78	76.94	2.67	0.09	1.42
20.20	4.81	28.82	2.63	75.84	2.47	0.10	0.67

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
20.22	5.50	33.92	2.19	74.34	2.37	0.10	0.69
20.24	5.63	35.06	2.02	70.88	2.32	0.10	0.69
20.26	5.53	34.65	1.89	65.43	2.28	0.10	0.69
20.28	5.35	33.64	1.77	59.68	2.24	0.09	0.68
20.30	5.19	32.69	1.70	55.55	2.21	0.09	0.68
20.32	5.14	32.40	1.67	54.11	2.20	0.08	0.68
20.34	5.28	33.42	1.63	54.52	2.19	0.08	0.68
20.36	5.51	35.10	1.58	55.41	2.16	0.09	0.69
20.38	5.76	37.05	1.52	56.21	2.13	0.09	0.70
20.40	5.95	38.51	1.47	56.45	2.11	0.08	0.70
20.42	6.11	39.72	1.00	39.72	2.08	0.08	0.71
20.44	6.21	40.50	1.00	40.50	2.07	0.08	0.71
20.46	6.22	40.61	1.00	40.61	2.06	0.08	0.71
20.48	6.12	39.88	1.00	39.88	2.06	0.08	0.71
20.50	5.89	38.10	1.00	38.10	2.08	0.08	0.70
20.52	5.68	36.56	1.00	36.56	2.09	0.08	0.69
20.54	5.42	34.52	1.00	34.52	2.12	0.08	0.69

Abbreviations

q_t:	Total cone resistance
K_c:	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c:	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

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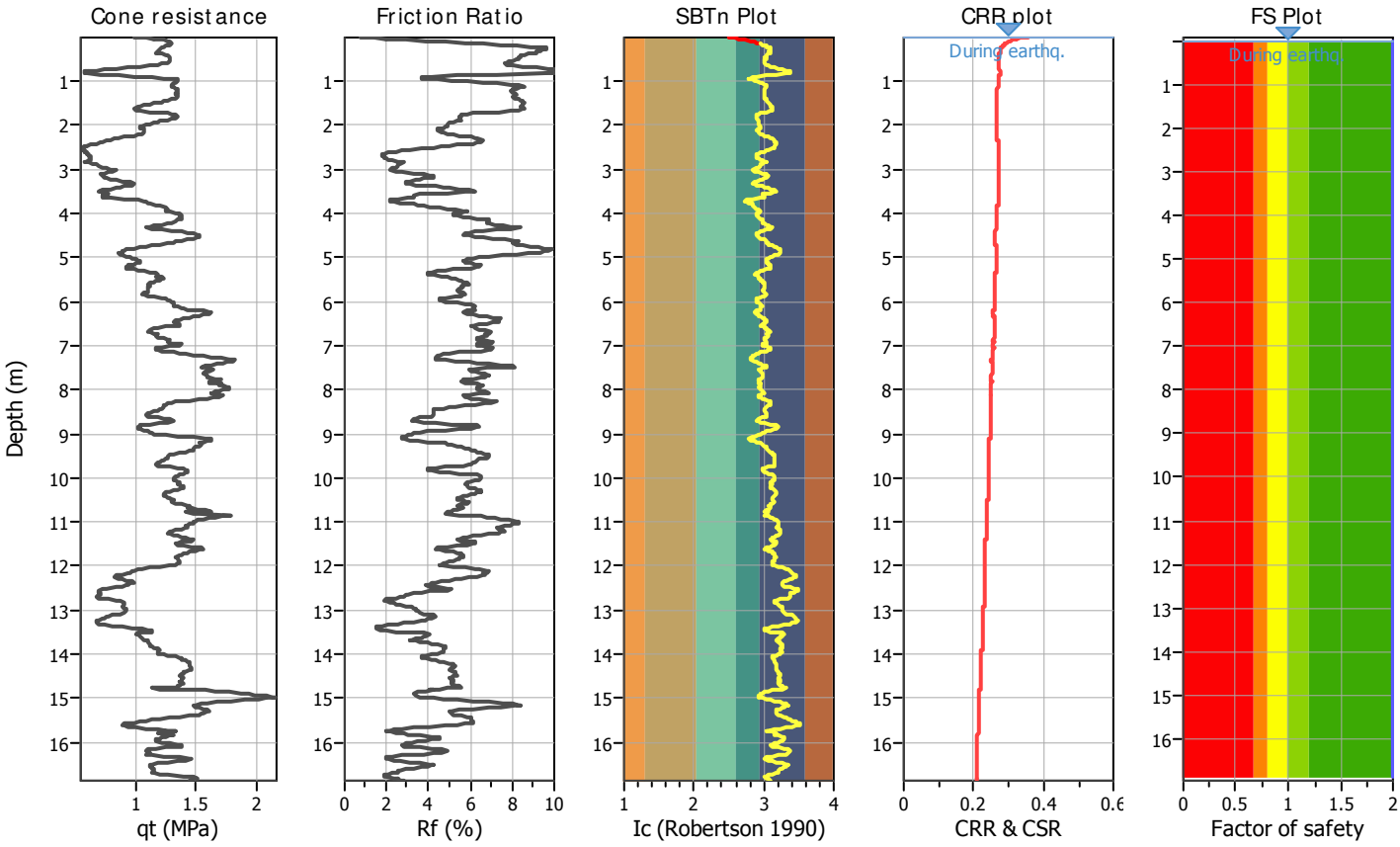
LIQUEFACTION ANALYSIS REPORT

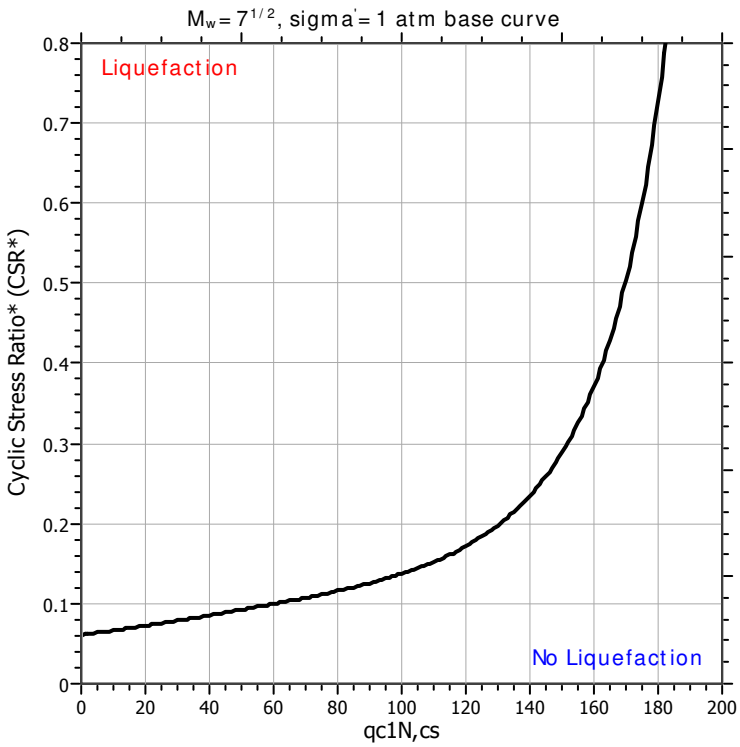
Project title : Location :

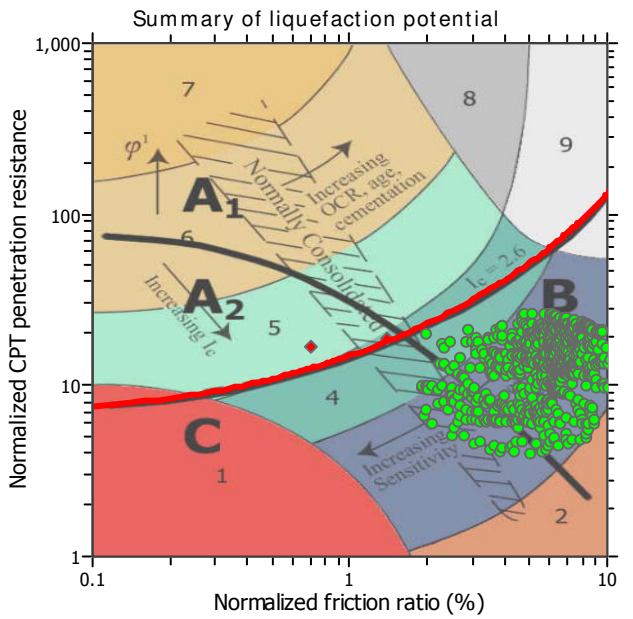
CPT file : CPTu-02_Biancolina

Input parameters and analysis data

Analysis method:	B&I (2014)	G.W.T. (in-situ):	0.60 m	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	0.00 m	Fill height:	N/A	Limit depth applied:	No
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	N/A
Earthquake magnitude M_w:	6.14	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.23	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		

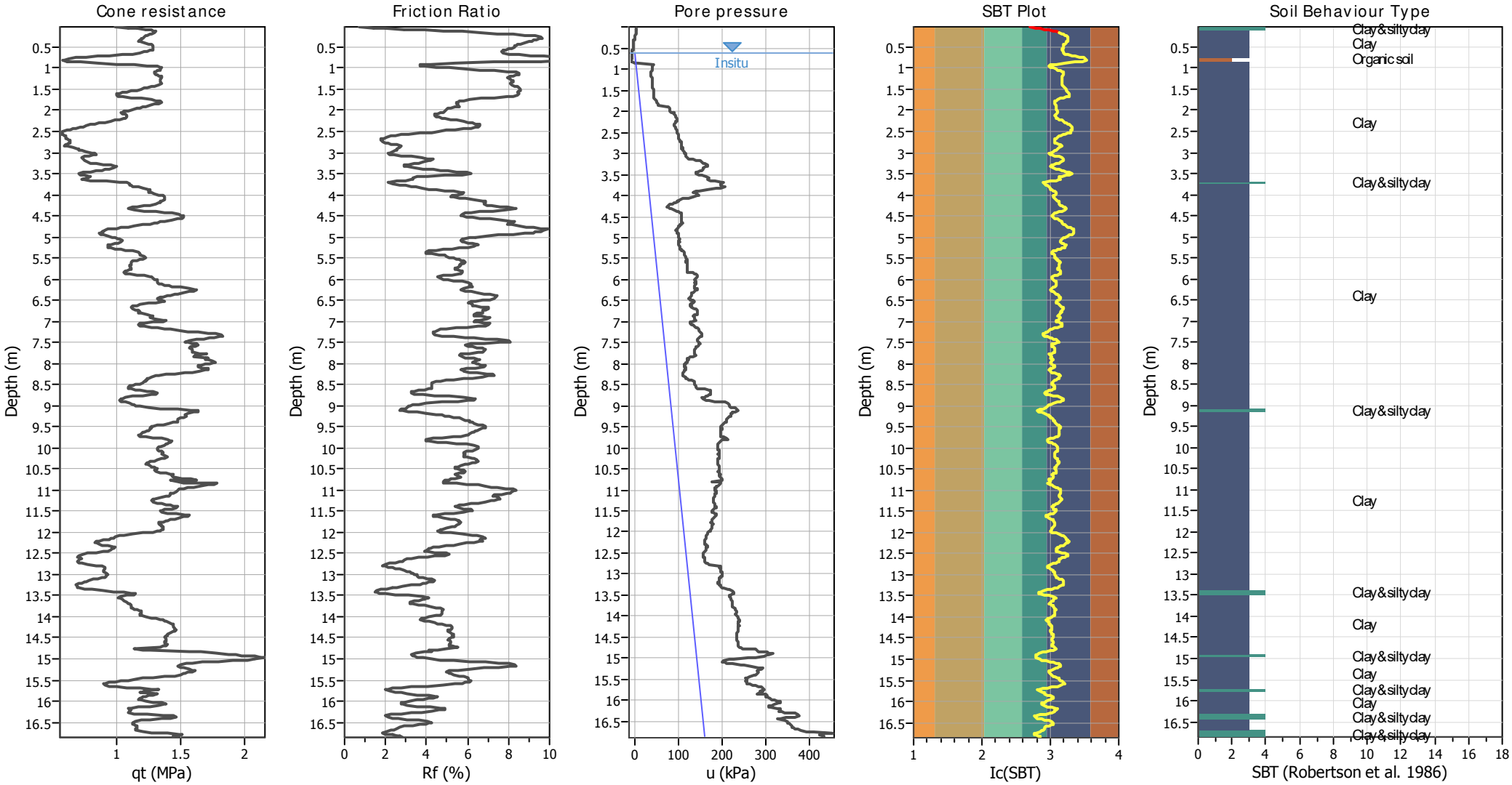






Zone A_1: Cyclic liquefaction likely depending on size and duration of cyclic loading
Zone A_2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



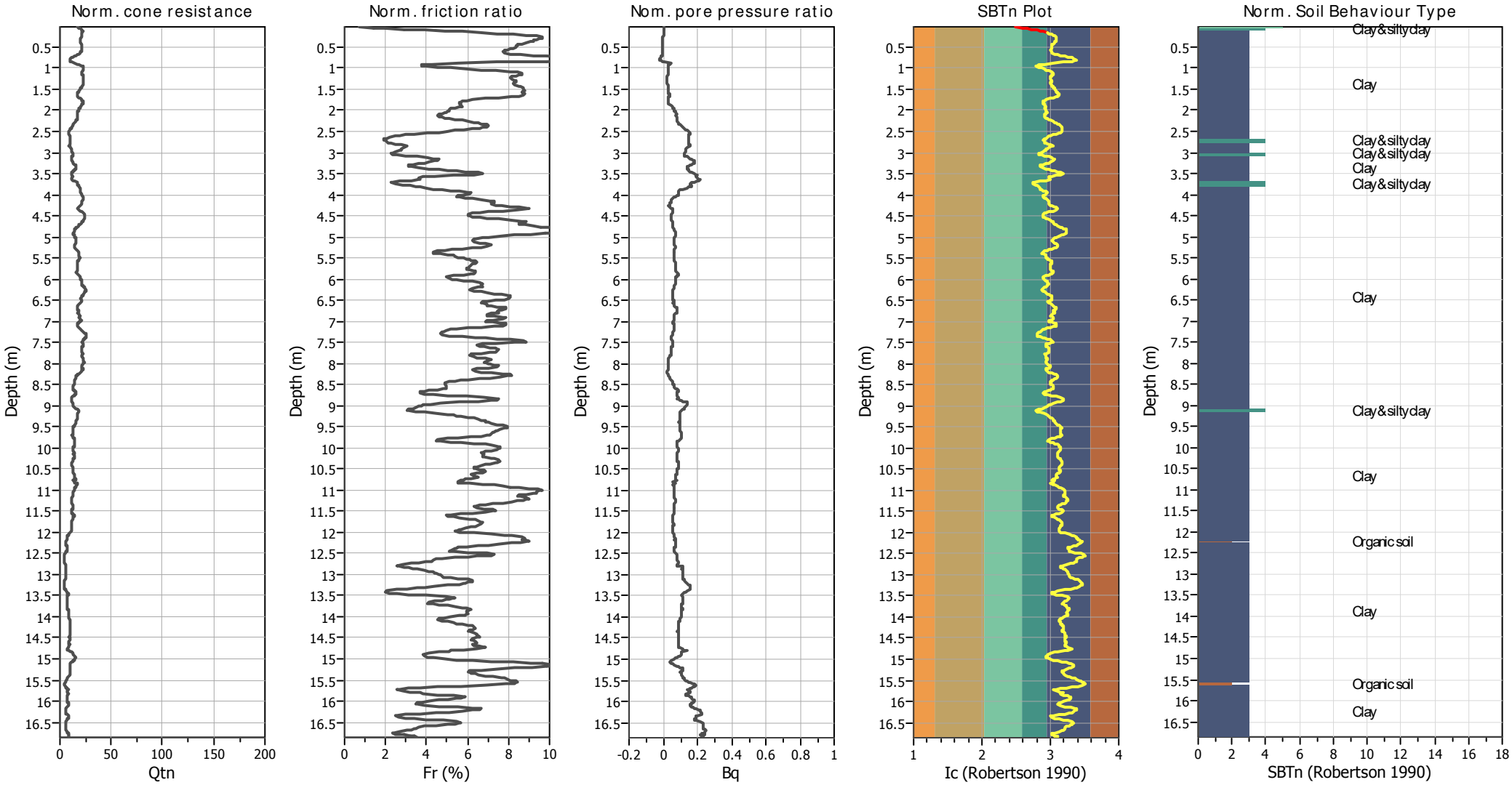
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	0.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.23	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	0.60 m	Fill height:	N/A	Limit depth:	N/A

SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

CPT basic interpretation plots (normalized)



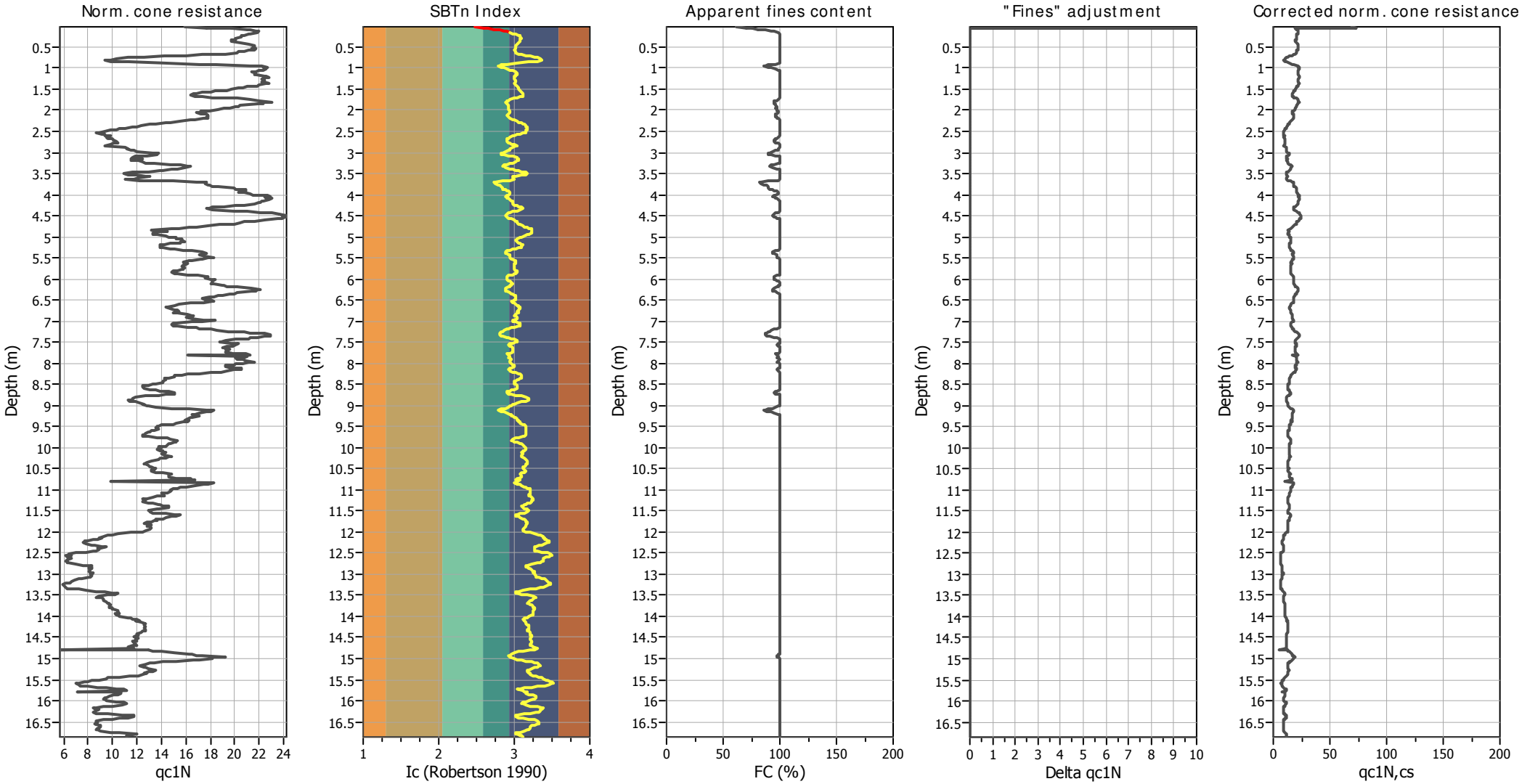
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	0.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.23	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	0.60 m	Fill height:	N/A	Limit depth:	N/A

SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

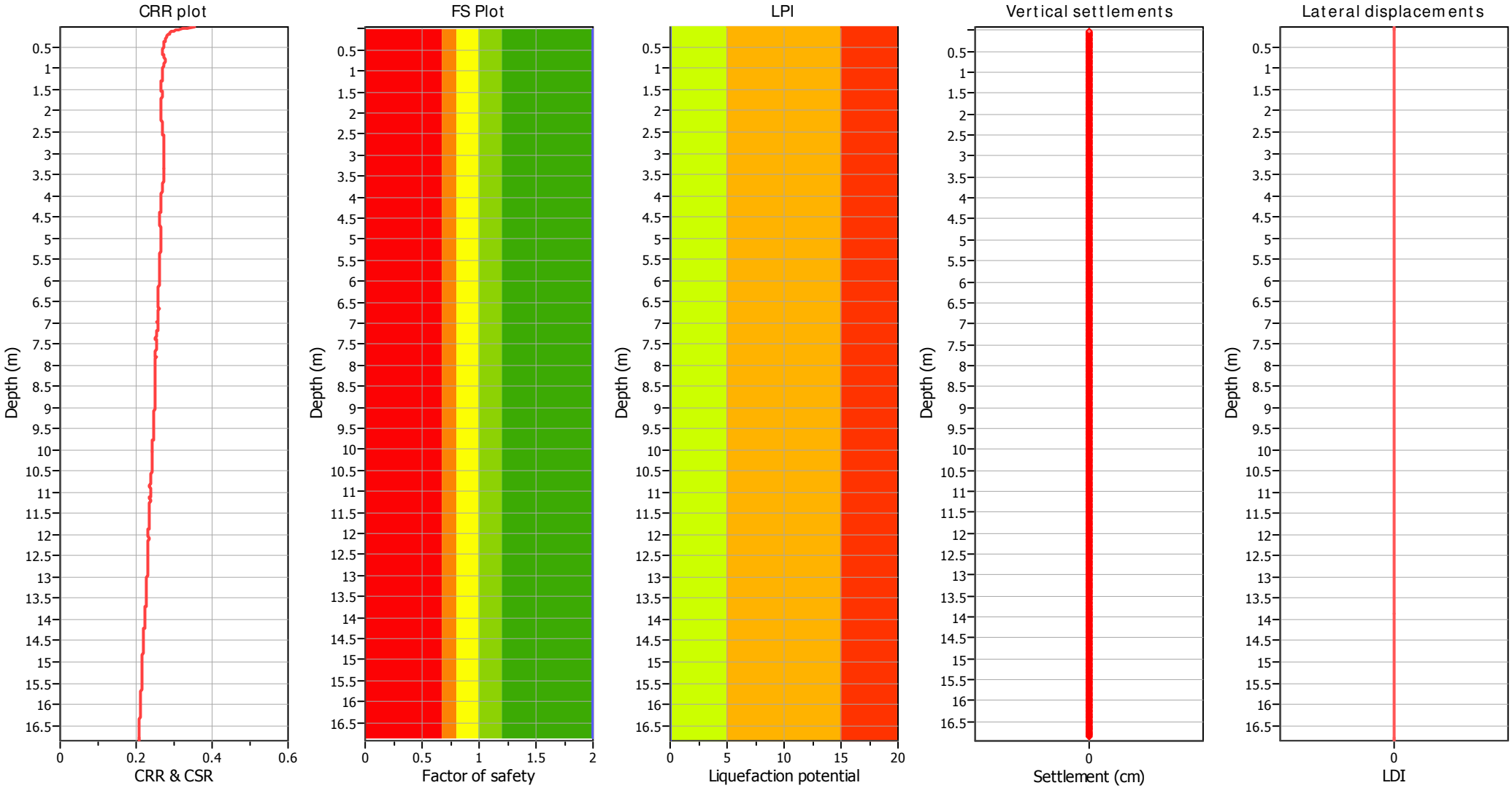
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	0.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.23	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	0.60 m	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	0.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.23	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	0.60 m	Fill height:	N/A	Limit depth:	N/A

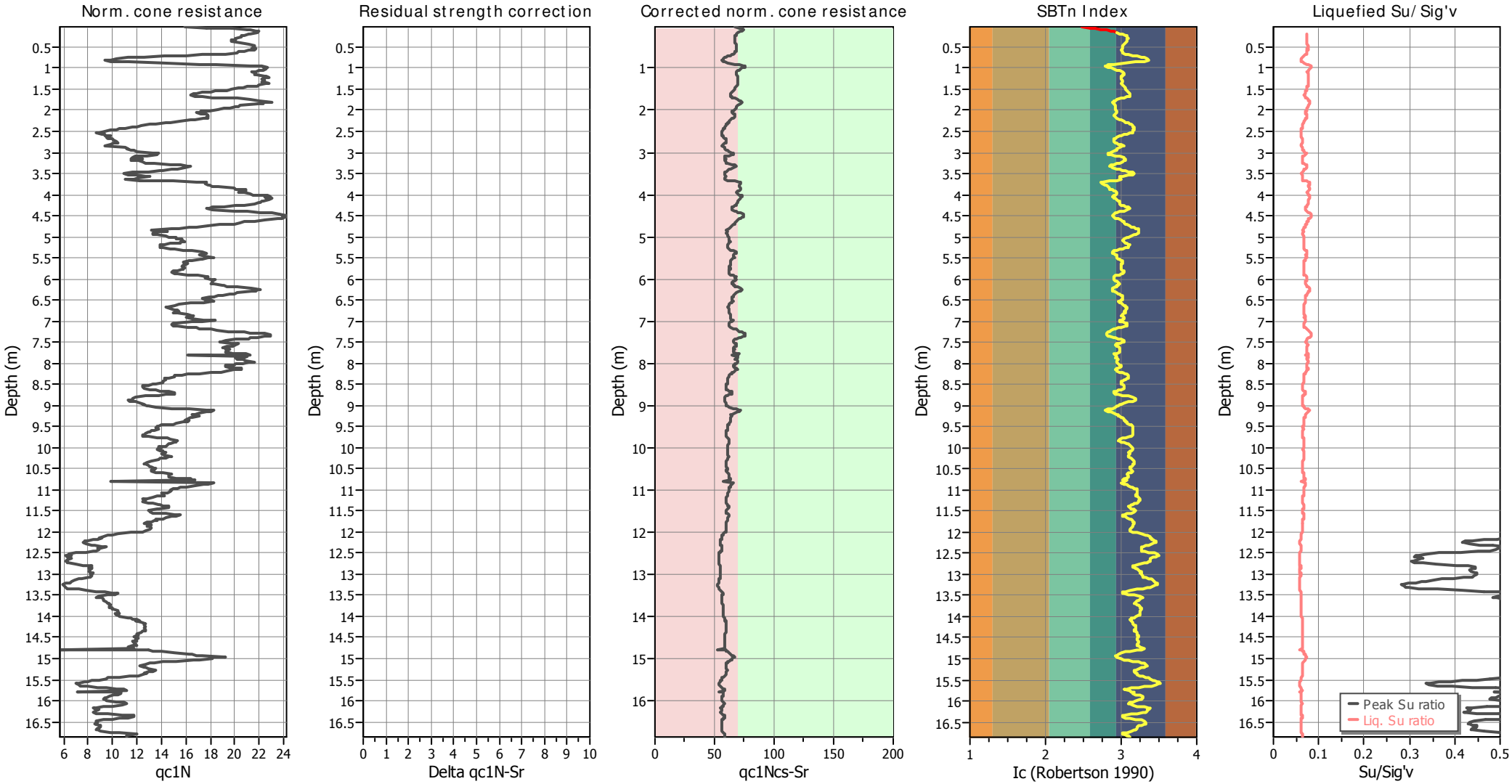
F.S. color scheme

- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

LPI color scheme

- Very high risk
- High risk
- Low risk

Check for strength loss plots (Idriss & Boulanger (2008))



Input parameters and analysis data

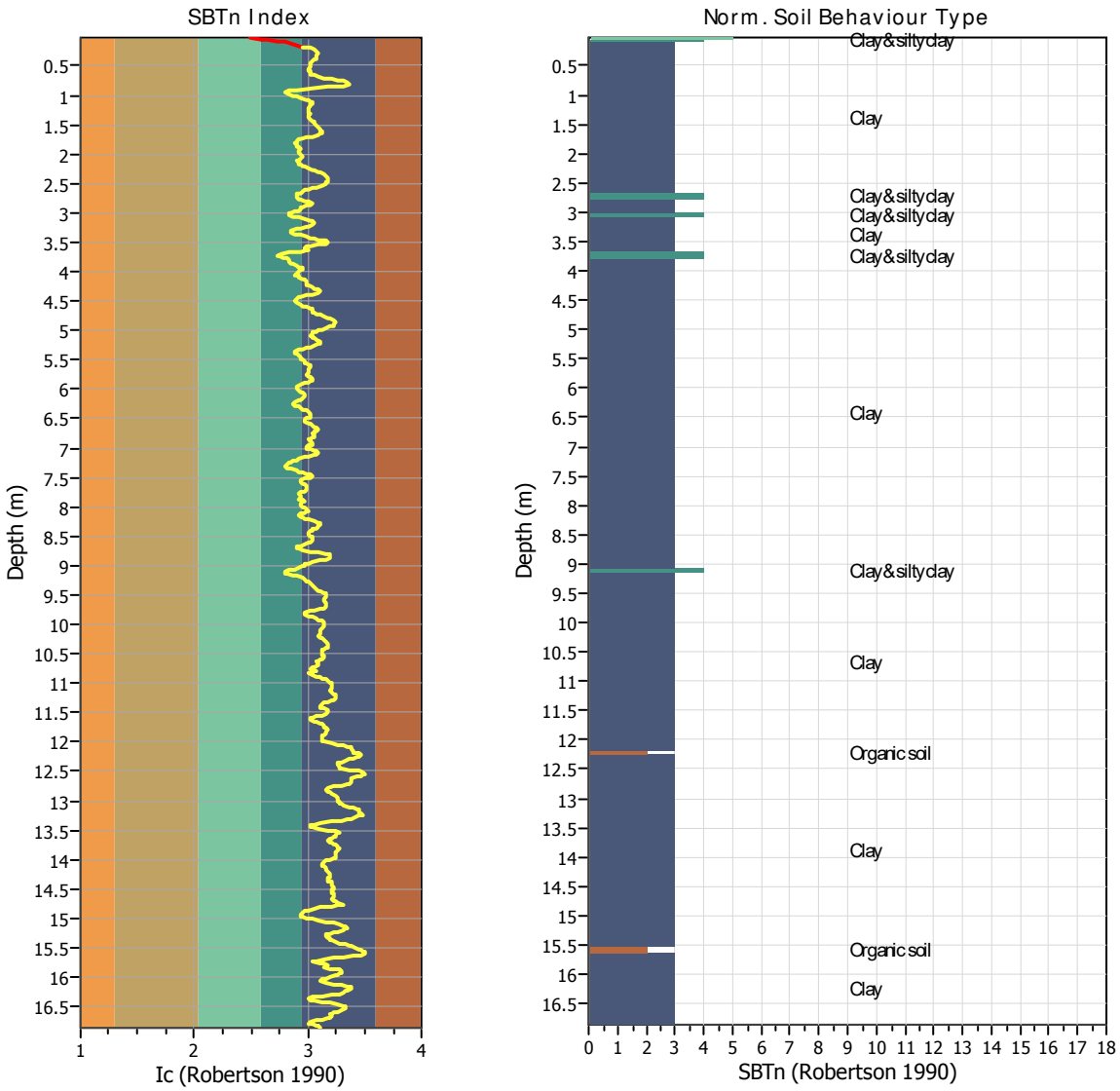
Analysis method:	B&I (2014)	Depth to GWT (erthq.):	0.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.23	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	0.60 m	Fill height:	N/A	Limit depth:	N/A

TRANSITION LAYER DETECTION ALGORITHM REPORT
Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vise-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between $1.80 < I_c < 3.0$) and a rate of change of I_c. Transitions typically occur when the rate of change of I_c is fast (i.e. delta I_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties		General statistics	
I_c minimum check value:	1.70	Total points in CPT file:	843
I_c maximum check value:	3.00	Total points excluded:	9
I_c change ratio value:	0.0100	Exclusion percentage:	1.07%
Minimum number of points in layer:	4	Number of layers detected:	1

Transition layer No	Number of points	Depth	SBT_n number	SBT_n description
Transition layer 1	9	Start depth: 0.02 (m)	5	Silty sand & sandy silt
		End depth: 0.18 (m)	3	Clay

Start depth: Depth where the transition layer begins
End depth: Depth where the transition layer ends

:: Field input data ::

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
1	0.02	0.95	4.60	2.89	30.15	15.22
2	0.04	1.05	11.71	3.02	34.81	16.15
3	0.06	1.17	22.25	3.32	37.99	16.65
4	0.08	1.25	35.14	3.32	42.06	17.18
5	0.10	1.27	49.59	3.08	45.94	17.56
6	0.12	1.29	63.01	2.83	49.44	17.84
7	0.14	1.31	75.12	2.65	52.21	18.05
8	0.17	1.30	85.19	2.28	55.16	18.21
9	0.18	1.27	96.79	1.85	57.72	18.32
10	0.20	1.26	102.85	1.42	60.18	18.41
11	0.23	1.24	110.51	0.68	61.93	18.48
12	0.24	1.23	115.87	0.12	63.28	18.52
13	0.26	1.23	117.70	-0.37	64.23	18.54
14	0.29	1.19	116.00	-0.98	64.53	18.53
15	0.30	1.20	114.09	-1.29	64.37	18.50
16	0.32	1.20	109.86	-1.78	64.19	18.47
17	0.34	1.17	109.19	-2.15	64.01	18.44
18	0.36	1.17	106.96	-2.52	64.15	18.43
19	0.38	1.17	106.77	-2.83	63.53	18.43
20	0.40	1.22	107.64	-3.14	62.45	18.44
21	0.42	1.26	106.78	-3.26	61.42	18.45
22	0.44	1.26	107.01	-3.45	60.55	18.45
23	0.46	1.29	106.82	-3.75	60.31	18.46
24	0.48	1.29	106.99	-4.00	60.05	18.46
25	0.50	1.29	107.18	-4.18	60.15	18.45
26	0.53	1.27	105.14	-4.43	59.75	18.44
27	0.54	1.30	102.67	-4.68	59.32	18.42
28	0.56	1.29	101.04	-4.92	59.01	18.39
29	0.58	1.26	97.97	-5.11	59.12	18.35
30	0.60	1.24	94.74	-5.35	59.49	18.31
31	0.62	1.21	93.65	-5.48	59.57	18.28
32	0.64	1.21	91.06	-5.60	60.39	18.25
33	0.66	1.14	90.55	-5.85	62.26	18.21
34	0.68	1.04	89.34	-6.34	65.35	18.17
35	0.70	0.96	86.74	-6.71	69.24	18.09
36	0.72	0.85	82.23	-7.14	73.44	18.00
37	0.74	0.75	78.83	-7.69	78.15	17.90
38	0.76	0.67	74.35	-8.80	82.50	17.80
39	0.78	0.62	70.38	-9.48	85.38	17.70
40	0.80	0.59	65.86	-9.54	87.35	17.61
41	0.82	0.56	62.88	-6.34	86.58	17.53
42	0.84	0.59	58.11	0.00	82.24	17.47
43	0.86	0.67	53.85	7.51	71.71	17.39
44	0.88	0.85	43.07	44.74	60.87	17.34
45	0.90	1.02	41.62	42.15	52.62	17.28
46	0.92	1.10	40.57	40.18	47.93	17.34
47	0.94	1.26	44.41	39.69	46.06	17.46
48	0.96	1.32	51.56	39.69	45.66	17.63

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
49	0.98	1.36	58.22	39.51	47.63	17.81
50	1.00	1.33	70.46	39.08	49.85	17.98
51	1.02	1.35	78.95	38.89	52.51	18.13
52	1.04	1.33	88.02	38.77	54.85	18.25
53	1.07	1.31	97.57	38.58	57.17	18.35
54	1.08	1.30	103.81	38.46	59.25	18.43
55	1.10	1.28	109.64	38.34	60.30	18.48
56	1.12	1.30	111.59	38.40	60.87	18.50
57	1.14	1.29	111.11	38.40	60.71	18.51
58	1.16	1.30	110.63	38.65	60.17	18.51
59	1.18	1.34	109.60	38.89	59.50	18.50
60	1.20	1.34	109.31	39.08	58.73	18.50
61	1.22	1.36	108.28	39.45	58.50	18.49
62	1.24	1.35	106.96	39.51	58.58	18.49
63	1.26	1.33	107.79	39.63	58.93	18.49
64	1.28	1.34	109.80	39.88	59.22	18.50
65	1.30	1.34	109.76	40.12	59.40	18.50
66	1.32	1.32	109.63	40.37	59.48	18.50
67	1.34	1.33	109.69	40.68	59.15	18.50
68	1.36	1.36	108.76	41.17	58.86	18.50
69	1.38	1.35	109.20	41.42	58.92	18.50
70	1.40	1.31	108.11	41.66	59.50	18.49
71	1.42	1.30	107.46	41.91	60.48	18.47
72	1.44	1.25	107.88	41.97	61.23	18.45
73	1.46	1.23	105.24	42.15	62.00	18.43
74	1.48	1.21	102.96	42.46	62.52	18.40
75	1.50	1.18	102.61	42.58	63.06	18.37
76	1.52	1.15	99.24	42.83	63.85	18.33
77	1.54	1.10	94.72	43.02	64.37	18.27
78	1.56	1.07	90.77	43.14	65.10	18.21
79	1.58	1.04	87.88	43.20	65.80	18.16
80	1.60	1.00	86.21	43.45	66.56	18.13
81	1.62	0.99	85.22	43.69	67.24	18.10
82	1.64	0.97	84.44	44.06	67.06	18.09
83	1.66	1.00	82.87	44.62	66.25	18.08
84	1.68	1.03	83.25	45.11	64.49	18.09
85	1.70	1.08	82.89	46.40	61.36	18.10
86	1.72	1.20	79.40	47.88	57.99	18.10
87	1.74	1.27	77.54	49.54	54.87	18.09
88	1.76	1.31	75.84	50.09	53.45	18.08
89	1.78	1.31	75.61	50.58	52.12	18.07
90	1.80	1.37	74.00	51.94	51.79	18.06
91	1.82	1.33	74.45	52.74	51.48	18.06
92	1.84	1.33	73.87	53.91	51.84	18.04
93	1.86	1.31	71.30	53.48	52.53	18.00
94	1.88	1.22	69.71	74.65	53.28	17.96
95	1.90	1.21	68.82	75.75	54.04	17.92
96	1.92	1.19	66.25	78.65	53.83	17.87

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
97	1.94	1.17	61.29	79.94	53.52	17.80
98	1.96	1.14	57.73	81.35	53.31	17.72
99	1.98	1.11	55.13	80.98	53.68	17.65
100	2.01	1.07	53.82	83.63	54.35	17.60
101	2.02	1.03	51.42	88.80	54.86	17.55
102	2.04	1.02	49.84	87.82	55.06	17.50
103	2.06	1.01	48.79	89.66	54.67	17.47
104	2.08	1.02	47.60	93.42	53.92	17.45
105	2.10	1.05	46.83	93.78	52.97	17.44
106	2.12	1.06	46.96	93.72	52.62	17.45
107	2.14	1.06	48.27	94.83	52.96	17.48
108	2.16	1.05	49.68	96.25	53.48	17.50
109	2.18	1.06	50.54	96.74	54.10	17.53
110	2.20	1.04	51.47	96.37	55.21	17.55
111	2.22	1.00	53.20	96.31	56.80	17.57
112	2.24	0.98	54.57	94.58	58.85	17.58
113	2.26	0.93	55.05	91.88	60.93	17.57
114	2.28	0.88	54.76	91.94	62.79	17.55
115	2.30	0.85	53.25	89.85	64.67	17.51
116	2.32	0.80	52.90	90.28	66.25	17.48
117	2.34	0.78	52.26	91.14	68.21	17.44
118	2.36	0.74	50.78	92.62	69.41	17.39
119	2.38	0.72	48.25	94.09	70.18	17.32
120	2.40	0.69	44.56	94.58	70.66	17.23
121	2.42	0.66	42.06	94.89	71.21	17.13
122	2.44	0.63	38.56	95.26	71.16	17.02
123	2.46	0.62	33.98	95.57	70.71	16.87
124	2.48	0.58	29.62	96.55	70.08	16.71
125	2.50	0.56	26.77	97.05	70.18	16.56
126	2.52	0.53	23.85	97.60	69.65	16.40
127	2.54	0.52	20.04	98.77	67.13	16.22
128	2.56	0.55	16.96	99.32	63.72	16.07
129	2.58	0.56	15.90	99.94	60.79	15.96
130	2.60	0.56	14.81	100.37	58.32	15.87
131	2.62	0.59	13.08	100.80	56.88	15.78
132	2.64	0.57	12.56	101.05	55.05	15.67
133	2.66	0.58	11.06	101.78	53.80	15.59
134	2.68	0.60	10.38	102.71	52.56	15.55
135	2.70	0.60	11.31	104.31	52.22	15.57
136	2.72	0.60	11.63	105.72	52.48	15.63
137	2.74	0.61	11.92	107.02	52.40	15.66
138	2.76	0.62	12.17	107.32	53.02	15.71
139	2.78	0.60	13.01	107.20	54.49	15.77
140	2.80	0.59	14.29	107.14	56.39	15.85
141	2.82	0.59	15.15	107.69	58.79	15.94
142	2.84	0.56	16.75	108.31	60.67	16.00
143	2.86	0.56	17.23	109.23	59.69	16.07
144	2.88	0.66	17.41	108.37	57.24	16.11

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
145	2.90	0.68	17.73	108.62	55.27	16.16
146	2.92	0.66	18.24	109.35	54.80	16.17
147	2.94	0.69	17.82	110.34	54.50	16.19
148	2.96	0.70	18.27	112.49	53.34	16.19
149	2.98	0.72	17.79	115.08	51.03	16.18
150	3.00	0.79	16.57	116.31	48.88	16.19
151	3.02	0.82	17.95	116.92	47.68	16.22
152	3.04	0.81	18.56	117.78	48.01	16.28
153	3.06	0.81	18.94	117.97	49.93	16.34
154	3.08	0.76	21.79	116.68	53.13	16.44
155	3.10	0.71	24.58	118.77	57.12	16.54
156	3.12	0.69	26.44	123.38	60.62	16.66
157	3.14	0.68	30.28	133.72	61.36	16.76
158	3.16	0.74	31.63	140.18	62.64	16.83
159	3.18	0.69	32.33	148.43	61.83	16.84
160	3.20	0.72	30.25	152.62	61.26	16.81
161	3.22	0.74	29.25	157.42	59.15	16.78
162	3.24	0.75	28.67	160.80	57.20	16.76
163	3.26	0.80	28.09	165.05	54.71	16.77
164	3.28	0.87	28.32	167.63	51.88	16.79
165	3.30	0.93	28.06	166.22	49.47	16.81
166	3.32	0.96	27.80	161.78	48.61	16.85
167	3.34	0.98	30.78	157.60	49.31	16.92
168	3.36	0.95	33.41	156.37	51.30	17.01
169	3.38	0.91	35.36	155.32	54.15	17.10
170	3.40	0.89	40.23	151.69	57.19	17.18
171	3.42	0.84	42.37	148.92	59.69	17.23
172	3.44	0.83	41.95	144.98	62.15	17.24
173	3.46	0.77	43.17	141.48	65.34	17.23
174	3.48	0.70	44.45	140.74	69.45	17.23
175	3.50	0.65	44.57	147.63	71.57	17.19
176	3.52	0.67	41.27	153.97	69.71	17.12
177	3.54	0.71	36.30	164.74	64.92	17.01
178	3.56	0.76	31.21	164.62	60.05	16.87
179	3.58	0.78	27.65	170.65	57.60	16.73
180	3.60	0.72	24.92	168.25	57.03	16.61
181	3.62	0.70	23.51	167.82	58.70	16.54
182	3.64	0.66	24.47	172.06	58.29	16.52
183	3.66	0.73	23.96	181.60	54.50	16.55
184	3.68	0.89	23.12	200.18	48.38	16.56
185	3.70	1.01	21.97	202.46	43.66	16.57
186	3.72	1.06	21.84	196.86	42.38	16.63
187	3.74	1.05	25.55	195.45	43.15	16.75
188	3.76	1.06	29.27	196.62	45.13	16.92
189	3.78	1.07	33.53	202.83	46.66	17.07
190	3.80	1.08	37.47	205.66	47.79	17.19
191	3.82	1.11	40.29	197.54	47.87	17.30
192	3.84	1.19	43.68	186.46	48.47	17.44

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
193	3.86	1.20	51.10	166.09	49.17	17.59
194	3.88	1.25	57.73	146.77	50.57	17.72
195	3.90	1.24	60.87	140.18	52.03	17.82
196	3.92	1.22	67.06	134.65	53.71	17.90
197	3.94	1.21	71.22	137.11	55.10	17.98
198	3.96	1.24	75.39	143.88	55.19	18.03
199	3.98	1.27	74.90	145.78	54.62	18.04
200	4.00	1.28	73.05	142.22	53.00	18.03
201	4.02	1.35	70.42	134.89	51.70	18.01
202	4.05	1.36	70.16	123.82	51.28	18.02
203	4.06	1.34	73.55	117.11	51.91	18.05
204	4.08	1.34	76.27	111.51	52.81	18.11
205	4.10	1.37	81.46	103.82	53.73	18.18
206	4.12	1.36	87.23	97.97	55.05	18.24
207	4.14	1.33	91.71	99.32	56.54	18.29
208	4.16	1.32	93.92	94.03	57.34	18.31
209	4.18	1.32	92.60	90.65	57.46	18.30
210	4.20	1.31	89.97	86.40	57.30	18.27
211	4.22	1.30	87.69	80.98	57.75	18.25
212	4.24	1.25	87.56	77.35	58.89	18.22
213	4.26	1.20	87.53	74.58	60.65	18.20
214	4.28	1.15	87.01	75.32	62.80	18.19
215	4.30	1.09	88.90	79.26	64.82	18.19
216	4.32	1.07	90.98	84.00	66.49	18.21
217	4.34	1.06	92.35	90.40	66.57	18.22
218	4.36	1.09	90.68	97.11	64.31	18.22
219	4.38	1.21	87.32	101.35	60.91	18.22
220	4.40	1.28	86.48	104.92	57.31	18.22
221	4.42	1.36	84.97	106.77	54.83	18.23
222	4.44	1.43	84.97	107.26	52.93	18.24
223	4.46	1.47	85.00	108.00	51.66	18.25
224	4.48	1.50	85.71	107.75	51.25	18.27
225	4.50	1.49	86.70	106.89	51.24	18.30
226	4.52	1.51	90.76	106.52	51.85	18.33
227	4.54	1.51	94.38	106.40	52.68	18.39
228	4.56	1.50	100.08	105.91	53.97	18.44
229	4.58	1.48	105.21	105.35	55.94	18.50
230	4.60	1.41	110.65	105.48	58.18	18.53
231	4.62	1.36	113.34	107.08	60.43	18.54
232	4.64	1.30	111.90	108.62	61.61	18.52
233	4.66	1.28	107.38	107.51	61.71	18.47
234	4.68	1.29	102.73	106.03	61.54	18.43
235	4.70	1.25	100.61	104.74	62.20	18.38
236	4.72	1.18	98.33	102.09	63.95	18.34
237	4.74	1.12	96.57	100.55	66.28	18.30
238	4.76	1.06	96.38	98.71	68.43	18.27
239	4.78	1.02	95.86	97.23	70.70	18.25
240	4.80	0.97	94.86	95.51	72.74	18.22

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
241	4.82	0.93	94.41	94.95	75.58	18.16
242	4.84	0.82	86.35	96.74	75.71	18.11
243	4.86	0.92	84.98	97.85	76.01	18.05
244	4.88	0.87	83.47	97.91	75.19	18.03
245	4.91	0.84	81.26	99.32	75.76	17.98
246	4.92	0.84	75.59	100.55	75.01	17.92
247	4.94	0.85	71.46	100.74	73.06	17.85
248	4.96	0.87	67.61	100.92	70.22	17.79
249	4.98	0.92	63.12	101.05	67.52	17.75
250	5.00	0.93	61.75	101.35	64.82	17.71
251	5.02	0.97	59.89	102.03	63.30	17.69
252	5.04	0.98	58.57	101.85	61.68	17.68
253	5.06	1.01	58.22	101.60	61.00	17.68
254	5.08	1.01	59.31	101.78	60.42	17.69
255	5.10	1.03	59.69	101.91	60.78	17.71
256	5.12	1.01	60.62	101.60	60.87	17.71
257	5.14	1.01	59.92	101.23	62.37	17.72
258	5.16	0.96	62.74	101.29	63.76	17.72
259	5.18	0.93	61.97	101.78	65.68	17.71
260	5.20	0.90	60.59	102.34	66.00	17.68
261	5.22	0.91	58.35	103.51	65.71	17.64
262	5.24	0.91	56.26	104.18	64.60	17.60
263	5.26	0.92	53.99	105.05	62.65	17.55
264	5.28	0.97	50.91	106.09	60.33	17.51
265	5.30	1.00	49.08	107.08	57.60	17.48
266	5.32	1.05	47.51	110.71	55.28	17.46
267	5.34	1.10	46.94	113.60	52.72	17.45
268	5.36	1.15	45.08	113.85	51.09	17.46
269	5.38	1.18	47.19	113.35	50.80	17.49
270	5.40	1.16	50.05	113.29	52.02	17.57
271	5.42	1.15	55.08	113.85	53.64	17.65
272	5.44	1.15	58.44	115.14	54.34	17.72
273	5.46	1.19	59.56	116.18	54.14	17.77
274	5.48	1.23	62.25	116.55	54.39	17.83
275	5.50	1.20	66.87	118.34	55.23	17.88
276	5.52	1.18	67.00	119.02	56.28	17.88
277	5.54	1.17	64.88	118.58	57.13	17.86
278	5.56	1.12	65.14	117.72	57.94	17.85
279	5.58	1.11	65.97	117.72	59.28	17.84
280	5.60	1.07	65.62	118.58	59.82	17.84
281	5.62	1.08	64.98	119.32	59.48	17.82
282	5.64	1.10	62.19	119.51	58.94	17.80
283	5.66	1.09	62.09	119.57	58.75	17.78
284	5.68	1.08	62.93	119.88	59.12	17.78
285	5.70	1.08	62.12	120.31	58.84	17.77
286	5.72	1.09	59.82	120.62	58.52	17.75
287	5.74	1.09	60.39	121.17	58.07	17.74
288	5.76	1.09	59.56	121.35	58.16	17.74

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
289	5.78	1.09	59.91	120.80	58.72	17.74
290	5.80	1.05	61.45	120.68	59.96	17.76
291	5.82	1.03	63.15	120.86	60.68	17.75
292	5.84	1.03	59.21	132.43	60.80	17.74
293	5.86	1.04	61.23	136.12	60.25	17.74
294	5.88	1.06	62.60	139.94	59.13	17.77
295	5.90	1.13	61.99	142.34	56.81	17.77
296	5.92	1.19	57.96	144.55	53.94	17.75
297	5.94	1.24	56.13	143.26	52.01	17.73
298	5.96	1.25	56.93	140.86	51.82	17.75
299	5.98	1.24	60.77	140.43	52.02	17.79
300	6.00	1.28	61.77	138.03	52.28	17.85
301	6.02	1.30	65.29	140.25	52.72	17.91
302	6.04	1.29	70.77	139.63	53.85	17.99
303	6.06	1.29	76.28	138.83	55.30	18.07
304	6.08	1.29	80.41	137.17	56.22	18.13
305	6.10	1.29	82.27	140.43	56.62	18.16
306	6.12	1.31	83.07	139.14	56.11	18.18
307	6.14	1.36	83.45	137.11	55.59	18.21
308	6.16	1.37	86.33	135.20	55.24	18.25
309	6.18	1.40	90.27	135.08	54.84	18.29
310	6.20	1.46	91.10	137.66	53.48	18.33
311	6.22	1.55	91.36	142.83	51.59	18.35
312	6.24	1.61	90.69	142.71	50.53	18.37
313	6.26	1.60	92.41	139.38	50.47	18.39
314	6.28	1.59	95.26	137.35	51.27	18.41
315	6.30	1.56	96.45	134.46	52.78	18.42
316	6.32	1.47	98.98	130.95	54.21	18.43
317	6.34	1.46	99.14	129.35	55.94	18.44
318	6.36	1.43	102.88	129.05	57.26	18.46
319	6.38	1.39	106.76	129.35	58.60	18.47
320	6.40	1.36	104.03	128.06	59.32	18.45
321	6.42	1.35	99.90	126.09	59.61	18.41
322	6.44	1.32	98.45	124.98	60.18	18.38
323	6.46	1.27	97.04	125.17	60.43	18.36
324	6.48	1.29	95.08	127.69	59.71	18.33
325	6.50	1.33	91.27	133.35	58.17	18.30
326	6.52	1.35	88.51	135.51	56.70	18.25
327	6.54	1.35	83.00	132.98	56.17	18.20
328	6.56	1.30	79.05	129.54	56.73	18.12
329	6.58	1.21	76.20	128.18	58.33	18.06
330	6.60	1.15	73.67	128.74	60.04	18.00
331	6.62	1.11	72.19	129.05	60.73	17.96
332	6.64	1.12	70.14	127.69	61.84	17.96
333	6.66	1.07	74.79	131.14	63.07	17.99
334	6.68	1.07	78.86	136.55	64.29	18.03
335	6.70	1.09	79.02	140.49	63.88	18.06
336	6.72	1.13	78.89	142.22	62.78	18.07

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
337	6.74	1.15	78.89	142.83	61.97	18.08
338	6.76	1.16	79.50	142.34	61.73	18.09
339	6.78	1.16	80.01	142.52	62.16	18.08
340	6.80	1.12	78.70	142.40	62.16	18.07
341	6.82	1.15	77.61	143.02	60.94	18.05
342	6.84	1.22	74.79	136.62	59.55	18.08
343	6.86	1.25	80.82	134.77	58.93	18.12
344	6.88	1.26	84.98	136.68	59.90	18.19
345	6.90	1.24	88.89	137.85	61.18	18.23
346	6.92	1.22	91.00	137.23	61.78	18.26
347	6.94	1.25	90.43	136.74	60.78	18.27
348	6.96	1.34	89.88	140.06	58.45	18.28
349	6.98	1.42	89.27	139.88	57.37	18.27
350	7.00	1.33	85.46	131.45	57.61	18.23
351	7.02	1.27	82.22	127.51	60.19	18.18
352	7.04	1.17	84.08	127.88	62.35	18.15
353	7.06	1.14	82.92	130.95	64.15	18.13
354	7.08	1.14	81.93	133.11	64.28	18.12
355	7.10	1.15	81.67	135.14	63.66	18.11
356	7.12	1.18	80.71	136.49	61.87	18.10
357	7.14	1.24	76.90	138.52	58.95	18.06
358	7.16	1.30	70.30	143.02	56.17	18.01
359	7.18	1.33	68.44	145.91	53.58	17.97
360	7.20	1.40	66.29	147.75	51.93	17.96
361	7.22	1.44	66.16	147.26	50.25	17.98
362	7.24	1.52	68.47	149.05	48.86	18.02
363	7.26	1.63	71.61	151.14	47.73	18.08
364	7.28	1.67	73.47	152.31	46.77	18.16
365	7.30	1.77	79.23	154.89	46.06	18.21
366	7.32	1.81	79.07	154.71	45.88	18.27
367	7.34	1.81	84.49	152.55	47.08	18.36
368	7.36	1.78	98.20	150.22	49.20	18.46
369	7.38	1.73	104.16	148.31	51.69	18.55
370	7.40	1.68	110.12	145.66	53.41	18.60
371	7.42	1.68	114.03	144.55	55.72	18.65
372	7.44	1.59	123.10	143.14	58.16	18.70
373	7.46	1.53	128.09	144.55	60.54	18.72
374	7.48	1.50	125.30	146.89	61.40	18.70
375	7.50	1.49	119.53	148.25	59.83	18.64
376	7.52	1.57	107.26	148.80	57.03	18.55
377	7.54	1.62	97.33	147.20	54.61	18.48
378	7.56	1.61	96.49	146.46	53.84	18.44
379	7.58	1.60	97.04	144.55	54.57	18.44
380	7.60	1.55	98.19	141.42	55.71	18.45
381	7.62	1.52	101.10	139.38	56.81	18.48
382	7.64	1.55	105.62	138.71	57.64	18.52
383	7.66	1.56	110.29	137.66	57.63	18.56
384	7.68	1.59	109.56	137.29	57.70	18.57

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
385	7.70	1.57	108.56	136.62	57.57	18.56
386	7.72	1.56	107.34	136.00	57.54	18.54
387	7.74	1.57	105.00	135.94	56.67	18.52
388	7.76	1.62	101.03	137.29	54.74	18.49
389	7.78	1.70	96.54	138.03	52.80	18.46
390	7.80	1.74	95.20	138.52	54.04	18.36
391	7.82	1.31	80.69	132.06	53.88	18.36
392	7.84	1.72	95.85	127.14	54.69	18.38
393	7.86	1.70	100.68	123.32	53.63	18.51
394	7.88	1.65	106.93	121.35	55.23	18.56
395	7.90	1.66	112.25	121.29	56.07	18.61
396	7.92	1.70	113.47	121.91	55.81	18.63
397	7.94	1.72	112.63	120.92	54.74	18.63
398	7.96	1.78	109.81	119.45	54.30	18.63
399	7.98	1.75	111.58	117.48	54.49	18.63
400	8.00	1.71	112.69	116.18	55.50	18.62
401	8.02	1.67	109.58	114.40	56.30	18.61
402	8.04	1.65	110.22	112.92	57.35	18.60
403	8.06	1.60	112.75	113.66	58.32	18.61
404	8.08	1.59	113.84	115.32	58.27	18.60
405	8.10	1.65	107.78	116.25	56.47	18.56
406	8.12	1.72	100.16	116.68	54.48	18.51
407	8.14	1.71	97.65	115.45	53.61	18.47
408	8.16	1.67	96.63	113.97	54.21	18.45
409	8.18	1.62	95.73	112.00	55.23	18.43
410	8.20	1.58	94.89	110.58	56.95	18.42
411	8.22	1.51	99.25	108.74	59.26	18.44
412	8.24	1.43	102.39	110.34	62.23	18.44
413	8.26	1.36	102.39	110.03	64.34	18.42
414	8.28	1.32	97.00	110.46	65.72	18.36
415	8.30	1.26	91.88	111.02	65.64	18.29
416	8.32	1.27	85.69	116.31	65.44	18.20
417	8.34	1.22	78.93	117.60	64.53	18.09
418	8.36	1.20	70.92	118.46	63.35	17.98
419	8.38	1.21	64.45	123.57	61.79	17.88
420	8.40	1.21	61.40	130.15	60.64	17.80
421	8.42	1.19	58.13	135.51	59.71	17.73
422	8.44	1.19	53.39	137.17	58.86	17.65
423	8.46	1.19	50.86	137.42	58.52	17.59
424	8.48	1.14	49.97	137.60	58.97	17.55
425	8.50	1.13	49.36	138.22	59.83	17.52
426	8.52	1.10	47.44	139.63	60.78	17.48
427	8.54	1.06	47.15	139.94	61.33	17.45
428	8.56	1.06	45.71	141.42	61.70	17.43
429	8.58	1.07	46.32	144.49	61.60	17.44
430	8.60	1.07	47.54	159.57	60.61	17.43
431	8.62	1.11	44.18	168.37	58.85	17.41
432	8.64	1.15	42.32	171.69	56.38	17.37

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
433	8.66	1.19	41.74	172.62	54.33	17.37
434	8.68	1.25	42.00	174.22	52.65	17.38
435	8.70	1.29	41.52	173.54	51.96	17.41
436	8.72	1.29	44.41	171.69	52.92	17.46
437	8.74	1.24	48.19	169.97	55.64	17.55
438	8.76	1.19	52.90	165.42	59.83	17.62
439	8.78	1.09	57.04	162.09	64.88	17.70
440	8.80	1.02	63.35	159.51	69.45	17.76
441	8.82	1.00	65.60	153.42	72.23	17.82
442	8.84	1.01	68.26	156.43	72.62	17.82
443	8.86	1.01	64.35	162.83	72.66	17.80
444	8.88	0.97	62.20	171.51	72.02	17.74
445	8.91	0.98	59.29	182.40	69.72	17.65
446	8.92	1.03	49.74	206.83	65.75	17.53
447	8.94	1.06	43.65	212.98	61.30	17.38
448	8.96	1.09	38.91	215.69	58.91	17.28
449	8.98	1.08	38.04	216.31	57.13	17.22
450	9.00	1.12	36.57	215.82	56.26	17.19
451	9.02	1.13	36.19	215.88	55.03	17.20
452	9.04	1.18	38.01	221.11	53.33	17.26
453	9.06	1.30	39.97	228.80	50.75	17.34
454	9.08	1.43	41.15	234.58	47.56	17.40
455	9.10	1.56	41.22	237.11	45.70	17.48
456	9.12	1.61	45.93	235.69	45.52	17.58
457	9.14	1.59	50.61	228.18	47.10	17.70
458	9.16	1.56	55.99	224.55	49.56	17.81
459	9.18	1.51	62.56	222.09	52.32	17.92
460	9.20	1.48	69.32	220.12	54.99	18.02
461	9.22	1.46	74.64	219.57	56.10	18.09
462	9.24	1.52	75.37	218.22	56.44	18.13
463	9.26	1.52	77.23	215.88	57.16	18.18
464	9.28	1.47	83.70	214.03	58.58	18.21
465	9.30	1.45	83.57	212.18	60.09	18.24
466	9.32	1.44	84.34	210.15	61.05	18.25
467	9.34	1.42	87.77	209.72	61.62	18.28
468	9.36	1.45	90.23	210.03	62.19	18.32
469	9.38	1.44	92.09	208.86	62.45	18.32
470	9.40	1.42	89.85	207.45	63.43	18.31
471	9.42	1.36	88.88	204.80	64.45	18.29
472	9.44	1.34	88.63	201.97	66.42	18.27
473	9.46	1.26	89.59	199.32	68.10	18.25
474	9.48	1.23	88.05	198.03	69.56	18.24
475	9.50	1.23	87.02	198.15	69.88	18.22
476	9.52	1.23	87.56	198.15	70.05	18.22
477	9.54	1.22	86.66	198.65	69.60	18.20
478	9.56	1.24	83.43	199.20	69.20	18.17
479	9.58	1.22	80.00	196.68	68.94	18.12
480	9.60	1.19	78.49	196.18	69.22	18.09

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
481	9.62	1.19	77.01	196.00	69.53	18.06
482	9.64	1.17	75.03	195.94	69.70	18.02
483	9.66	1.15	72.72	195.20	69.87	17.99
484	9.68	1.14	71.08	195.69	70.00	17.96
485	9.70	1.13	70.06	195.45	69.83	17.93
486	9.72	1.13	67.94	197.85	68.71	17.90
487	9.74	1.17	64.87	201.85	66.21	17.87
488	9.76	1.25	62.01	208.37	62.60	17.83
489	9.78	1.32	57.91	211.26	59.53	17.79
490	9.80	1.35	56.18	211.82	56.88	17.74
491	9.82	1.40	53.14	199.88	56.34	17.75
492	9.84	1.39	58.91	195.32	56.88	17.81
493	9.86	1.39	64.29	193.78	58.82	17.92
494	9.88	1.38	70.02	192.49	61.05	18.02
495	9.90	1.36	77.81	191.14	63.29	18.11
496	9.92	1.34	82.71	191.14	65.46	18.19
497	9.94	1.33	87.58	190.40	66.89	18.24
498	9.96	1.32	88.74	188.55	68.28	18.25
499	9.98	1.27	86.97	188.74	68.72	18.24
500	10.00	1.30	86.01	189.35	69.12	18.22
501	10.02	1.27	85.14	189.35	69.11	18.21
502	10.04	1.26	85.37	190.95	68.88	18.19
503	10.06	1.29	82.26	192.18	67.93	18.17
504	10.08	1.32	80.21	192.37	66.76	18.15
505	10.10	1.32	79.40	192.18	65.93	18.14
506	10.12	1.34	78.31	192.31	65.84	18.13
507	10.14	1.32	78.57	191.51	66.15	18.13
508	10.16	1.30	80.39	191.57	66.42	18.14
509	10.18	1.33	80.46	192.55	65.81	18.16
510	10.20	1.38	80.26	192.68	65.44	18.18
511	10.22	1.36	84.04	192.98	65.80	18.21
512	10.24	1.35	86.22	192.49	67.35	18.23
513	10.26	1.30	86.70	191.08	68.38	18.23
514	10.28	1.29	84.55	189.48	69.82	18.20
515	10.30	1.23	84.10	188.80	70.39	18.17
516	10.32	1.23	80.99	188.25	71.32	18.15
517	10.34	1.21	80.83	189.60	71.23	18.11
518	10.36	1.20	77.40	190.46	71.37	18.07
519	10.38	1.18	73.91	190.34	70.77	18.03
520	10.40	1.20	72.44	191.20	70.03	18.00
521	10.42	1.22	71.54	191.94	68.85	17.98
522	10.44	1.24	69.33	192.18	67.94	17.97
523	10.46	1.25	69.68	192.62	67.09	17.97
524	10.48	1.27	69.90	192.68	66.82	17.98
525	10.50	1.28	71.76	192.62	66.93	18.01
526	10.52	1.27	73.75	191.63	67.83	18.04
527	10.54	1.25	75.35	191.94	68.64	18.06
528	10.56	1.26	76.57	191.45	68.93	18.09

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
529	10.58	1.29	78.87	192.55	67.82	18.11
530	10.60	1.35	77.78	194.58	65.80	18.12
531	10.62	1.41	75.92	195.08	64.36	18.12
532	10.64	1.40	76.34	193.91	64.02	18.13
533	10.66	1.40	79.83	193.29	64.70	18.16
534	10.68	1.40	81.50	192.68	65.39	18.19
535	10.70	1.40	84.13	195.20	64.91	18.21
536	10.72	1.46	82.30	197.48	62.85	18.21
537	10.74	1.57	79.13	198.46	60.89	18.23
538	10.76	1.59	84.06	198.71	59.88	18.27
539	10.78	1.61	87.49	200.68	63.16	18.01
540	10.80	0.94	38.08	176.18	61.75	18.04
541	10.82	1.75	88.13	197.78	60.87	18.10
542	10.84	1.77	95.72	196.25	58.73	18.48
543	10.86	1.73	107.90	194.89	60.91	18.57
544	10.88	1.69	112.93	191.75	63.47	18.62
545	10.90	1.62	114.56	189.23	65.56	18.63
546	10.92	1.56	113.60	187.63	67.62	18.62
547	10.94	1.52	114.91	186.09	69.57	18.63
548	10.96	1.49	119.94	183.82	71.52	18.65
549	10.98	1.45	123.56	182.34	73.15	18.68
550	11.00	1.44	124.84	183.51	73.86	18.68
551	11.02	1.44	122.27	184.98	73.78	18.67
552	11.04	1.44	119.39	186.15	73.64	18.64
553	11.06	1.41	117.11	186.22	74.02	18.60
554	11.08	1.37	113.46	185.91	74.11	18.56
555	11.10	1.38	107.88	184.37	73.59	18.51
556	11.12	1.39	104.16	183.69	72.46	18.47
557	11.14	1.40	101.18	183.08	72.62	18.45
558	11.16	1.34	102.01	181.60	73.71	18.43
559	11.18	1.30	102.42	181.23	75.45	18.41
560	11.20	1.26	98.19	180.12	76.72	18.37
561	11.22	1.23	96.36	180.18	76.88	18.33
562	11.24	1.25	93.44	180.98	76.63	18.30
563	11.26	1.24	91.10	180.74	75.98	18.28
564	11.28	1.24	89.37	180.31	75.01	18.25
565	11.30	1.28	86.23	180.55	73.24	18.22
566	11.32	1.32	82.68	182.28	70.83	18.19
567	11.34	1.36	80.98	182.95	69.02	18.17
568	11.36	1.38	79.76	183.51	67.65	18.16
569	11.38	1.41	78.93	184.80	66.46	18.16
570	11.40	1.45	79.70	186.15	65.66	18.17
571	11.42	1.46	80.85	185.42	66.59	18.20
572	11.44	1.37	84.47	182.65	68.19	18.22
573	11.46	1.36	85.33	180.86	70.78	18.22
574	11.48	1.29	85.88	178.77	71.61	18.21
575	11.50	1.30	82.51	177.97	71.74	18.17
576	11.52	1.31	77.84	177.60	70.27	18.12

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
577	11.54	1.33	75.34	180.68	67.48	18.08
578	11.56	1.44	71.04	184.25	64.23	18.05
579	11.58	1.51	68.25	186.52	60.99	18.02
580	11.60	1.56	66.49	186.83	59.80	18.01
581	11.62	1.53	67.81	184.98	60.09	18.01
582	11.64	1.49	69.31	183.08	61.83	18.03
583	11.66	1.45	72.36	181.35	63.66	18.06
584	11.68	1.43	74.70	179.69	66.10	18.10
585	11.70	1.37	79.38	178.09	67.57	18.13
586	11.72	1.37	77.94	177.72	68.80	18.13
587	11.74	1.35	76.94	176.74	68.99	18.11
588	11.76	1.33	75.44	175.69	70.07	18.10
589	11.78	1.29	77.49	174.58	70.86	18.07
590	11.80	1.27	72.98	179.88	70.80	18.07
591	11.82	1.34	74.74	178.77	70.14	18.05
592	11.84	1.32	73.65	176.43	69.87	18.06
593	11.86	1.30	74.58	175.82	69.68	18.04
594	11.88	1.33	71.38	175.82	68.79	18.01
595	11.90	1.34	66.99	175.88	67.60	17.96
596	11.92	1.33	65.00	175.02	66.93	17.91
597	11.94	1.33	63.78	173.48	67.12	17.88
598	11.96	1.29	62.08	172.62	66.86	17.84
599	11.98	1.30	58.75	172.06	67.09	17.80
600	12.00	1.27	58.59	169.66	68.78	17.79
601	12.02	1.18	61.92	166.46	73.36	17.82
602	12.04	1.06	67.05	166.89	78.51	17.83
603	12.06	1.02	65.19	166.09	82.67	17.83
604	12.08	0.99	65.44	164.62	85.12	17.81
605	12.10	0.95	66.28	164.43	87.76	17.81
606	12.13	0.92	67.69	164.55	88.90	17.80
607	12.14	0.94	65.38	164.18	89.31	17.77
608	12.17	0.91	61.09	162.28	89.82	17.71
609	12.18	0.86	59.49	161.29	92.13	17.65
610	12.20	0.82	58.36	159.94	94.36	17.59
611	12.22	0.80	55.13	159.51	95.34	17.54
612	12.24	0.80	52.63	160.86	94.90	17.47
613	12.26	0.79	49.36	160.31	93.37	17.42
614	12.29	0.81	47.75	160.43	90.45	17.38
615	12.30	0.87	46.38	162.09	87.42	17.38
616	12.32	0.89	47.34	164.80	83.67	17.38
617	12.34	0.95	45.58	166.65	80.32	17.35
618	12.36	0.98	41.86	166.22	78.18	17.30
619	12.38	0.94	40.84	164.31	78.21	17.25
620	12.40	0.91	40.61	164.68	78.66	17.20
621	12.42	0.93	37.34	164.92	78.81	17.16
622	12.44	0.90	36.67	164.06	78.74	17.10
623	12.46	0.87	35.10	161.48	81.39	17.07
624	12.48	0.81	36.16	158.77	86.61	17.07

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
625	12.50	0.74	39.56	156.80	93.79	17.07
626	12.52	0.67	38.53	156.06	97.61	17.03
627	12.54	0.69	33.44	156.06	100.00	16.92
628	12.56	0.65	30.69	155.88	97.09	16.78
629	12.58	0.65	27.67	156.12	95.67	16.68
630	12.60	0.68	25.59	157.60	92.21	16.59
631	12.62	0.69	23.96	159.32	88.48	16.49
632	12.64	0.70	20.95	159.69	87.54	16.41
633	12.66	0.66	20.92	158.71	87.74	16.33
634	12.68	0.65	19.86	158.83	88.45	16.27
635	12.70	0.66	18.10	160.25	87.16	16.19
636	12.72	0.66	17.08	160.37	84.79	16.12
637	12.74	0.68	16.34	162.28	80.95	16.07
638	12.76	0.74	15.16	165.48	75.59	16.03
639	12.78	0.80	14.58	169.72	70.71	16.09
640	12.80	0.87	17.43	194.22	69.31	16.22
641	12.82	0.86	19.83	195.45	69.72	16.37
642	12.84	0.88	21.40	195.38	71.05	16.46
643	12.86	0.88	22.08	194.40	72.55	16.54
644	12.88	0.85	24.51	195.94	74.07	16.61
645	12.90	0.86	25.54	196.06	76.13	16.69
646	12.92	0.85	27.59	196.86	77.06	16.75
647	12.94	0.86	29.03	197.29	77.97	16.82
648	12.96	0.87	30.18	198.77	77.69	16.86
649	12.98	0.89	30.57	199.14	77.82	16.91
650	13.00	0.89	32.14	198.65	78.33	16.93
651	13.02	0.87	32.49	198.71	79.03	16.96
652	13.04	0.88	32.72	198.22	79.65	16.96
653	13.06	0.87	32.65	197.85	80.25	16.97
654	13.08	0.86	33.07	197.29	82.90	16.98
655	13.10	0.80	34.70	194.71	86.12	16.99
656	13.12	0.77	34.67	192.31	89.99	16.98
657	13.14	0.74	34.32	191.94	92.56	16.96
658	13.16	0.72	33.55	191.69	93.82	16.90
659	13.19	0.71	30.34	191.75	94.19	16.82
660	13.20	0.69	28.48	190.95	94.93	16.73
661	13.22	0.66	27.81	190.58	96.29	16.65
662	13.24	0.64	24.99	191.88	96.79	16.54
663	13.26	0.64	22.14	192.98	94.79	16.41
664	13.28	0.64	19.61	195.51	91.10	16.27
665	13.30	0.66	17.30	197.48	88.28	16.16
666	13.32	0.66	16.69	199.69	85.64	16.08
667	13.34	0.67	15.70	203.08	80.38	16.02
668	13.36	0.77	13.94	212.80	73.51	15.97
669	13.38	0.84	13.36	217.11	66.38	15.95
670	13.40	0.93	13.68	224.31	62.28	16.04
671	13.42	1.01	15.99	225.48	60.06	16.21
672	13.44	1.07	18.91	226.28	59.65	16.43

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
673	13.46	1.12	22.94	227.32	61.09	16.64
674	13.48	1.10	26.95	224.31	64.82	16.86
675	13.50	1.05	33.74	219.32	71.06	17.06
676	13.52	0.96	40.21	216.31	77.02	17.20
677	13.54	0.94	42.17	217.35	79.50	17.27
678	13.56	0.99	41.43	219.94	78.70	17.28
679	13.58	1.01	40.86	220.31	77.18	17.27
680	13.60	1.00	40.41	220.92	76.66	17.25
681	13.62	1.00	38.87	221.23	75.70	17.20
682	13.64	1.01	35.53	221.97	73.88	17.13
683	13.66	1.03	33.04	222.40	72.13	17.08
684	13.68	1.05	33.90	222.34	71.50	17.09
685	13.70	1.06	36.24	222.15	72.33	17.18
686	13.72	1.06	40.79	222.09	73.52	17.28
687	13.74	1.08	43.74	222.52	75.12	17.38
688	13.76	1.07	46.84	222.46	76.47	17.45
689	13.78	1.07	49.76	222.40	77.72	17.53
690	13.80	1.09	53.19	231.20	78.49	17.60
691	13.82	1.09	55.63	230.15	78.77	17.65
692	13.84	1.10	56.17	230.28	78.14	17.67
693	13.86	1.14	55.50	231.08	77.26	17.68
694	13.88	1.15	56.52	231.82	76.62	17.69
695	13.90	1.15	57.13	232.80	76.52	17.70
696	13.92	1.16	56.43	231.82	76.88	17.70
697	13.94	1.13	56.20	230.77	76.99	17.68
698	13.96	1.13	55.37	230.95	76.80	17.66
699	13.98	1.15	53.51	231.51	75.55	17.63
700	14.00	1.17	51.14	233.72	72.86	17.59
701	14.02	1.24	48.47	235.57	70.39	17.57
702	14.04	1.27	48.57	236.25	68.49	17.57
703	14.06	1.28	49.66	237.17	67.42	17.58
704	14.08	1.33	49.63	238.09	66.85	17.62
705	14.10	1.35	52.38	238.09	67.65	17.69
706	14.12	1.31	58.63	237.60	68.67	17.78
707	14.14	1.37	61.73	239.14	69.37	17.86
708	14.16	1.40	64.71	237.72	69.37	17.93
709	14.18	1.40	68.43	237.72	70.13	17.99
710	14.20	1.40	72.34	237.85	71.34	18.05
711	14.22	1.39	75.44	238.28	71.89	18.09
712	14.24	1.41	75.63	237.85	72.20	18.11
713	14.26	1.40	75.67	237.29	72.29	18.12
714	14.28	1.41	77.65	237.97	72.29	18.12
715	14.30	1.41	75.28	237.97	71.92	18.11
716	14.32	1.42	74.35	237.78	71.31	18.09
717	14.34	1.42	72.68	237.48	71.27	18.07
718	14.36	1.40	72.39	236.86	71.85	18.06
719	14.38	1.38	73.80	235.20	73.23	18.07
720	14.40	1.34	74.63	234.58	73.96	18.07

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
721	14.42	1.36	73.38	234.52	74.31	18.06
722	14.44	1.35	73.57	233.29	74.23	18.06
723	14.46	1.34	73.60	232.31	74.87	18.06
724	14.48	1.32	74.02	232.12	75.34	18.05
725	14.50	1.32	72.51	233.11	74.71	18.03
726	14.52	1.36	69.62	234.28	73.99	18.01
727	14.54	1.34	69.27	233.29	73.70	18.00
728	14.56	1.33	71.58	234.34	74.04	18.01
729	14.58	1.35	71.03	234.34	74.74	18.03
730	14.60	1.32	72.63	235.57	74.95	18.03
731	14.62	1.32	71.73	236.06	75.12	18.02
732	14.64	1.34	70.20	236.74	74.61	18.02
733	14.66	1.35	71.35	237.05	74.14	18.02
734	14.68	1.36	71.19	237.72	74.56	18.02
735	14.70	1.32	71.48	236.74	75.81	18.03
736	14.72	1.28	73.69	236.25	77.27	18.04
737	14.74	1.29	74.61	240.62	77.54	18.06
738	14.76	1.33	75.22	241.66	82.17	17.67
739	14.78	0.65	18.89	245.85	77.91	17.65
740	14.80	1.47	68.23	275.69	73.89	17.61
741	14.82	1.51	67.91	279.88	66.49	18.00
742	14.84	1.59	64.93	284.49	62.97	17.97
743	14.86	1.72	60.09	301.48	59.02	17.96
744	14.88	1.85	61.98	307.63	56.29	17.97
745	14.90	1.87	62.49	316.55	55.39	18.02
746	14.92	1.91	67.11	307.32	55.24	18.08
747	14.94	1.97	70.05	302.09	54.02	18.17
748	14.96	2.18	74.86	295.08	54.19	18.26
749	14.98	2.07	82.81	277.35	54.99	18.36
750	15.00	2.07	89.05	260.74	58.15	18.43
751	15.02	1.96	94.34	227.63	60.97	18.50
752	15.04	1.91	102.83	215.38	65.25	18.56
753	15.06	1.74	109.27	202.15	70.02	18.61
754	15.08	1.62	115.90	200.37	75.27	18.65
755	15.10	1.55	122.46	205.29	79.12	18.68
756	15.12	1.50	123.49	209.85	81.77	18.69
757	15.14	1.46	124.38	224.37	83.83	18.69
758	15.16	1.41	125.15	241.85	84.80	18.67
759	15.18	1.41	119.60	249.97	83.98	18.64
760	15.20	1.45	112.74	266.28	81.58	18.57
761	15.22	1.47	104.51	283.26	78.70	18.50
762	15.24	1.50	96.85	292.98	75.39	18.41
763	15.26	1.56	87.07	290.95	72.33	18.32
764	15.28	1.56	80.21	286.46	70.43	18.24
765	15.30	1.54	78.74	278.95	70.41	18.19
766	15.32	1.50	78.45	280.98	71.55	18.18
767	15.34	1.47	79.25	282.28	72.24	18.17
768	15.36	1.48	78.12	279.57	73.15	18.18

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
769	15.38	1.45	80.62	278.09	74.10	18.18
770	15.40	1.41	81.04	276.74	76.58	18.19
771	15.42	1.33	81.26	272.80	79.65	18.15
772	15.44	1.23	77.55	263.26	83.55	18.08
773	15.46	1.13	72.84	256.49	86.29	17.99
774	15.48	1.10	67.90	253.60	88.71	17.91
775	15.50	1.04	66.11	255.63	91.11	17.85
776	15.52	0.97	64.73	255.26	94.24	17.78
777	15.54	0.93	60.18	255.08	96.62	17.69
778	15.56	0.90	55.44	252.92	98.37	17.59
779	15.58	0.85	52.07	254.71	100.00	17.50
780	15.60	0.83	49.60	257.78	100.00	17.41
781	15.62	0.85	43.65	264.43	96.07	17.29
782	15.64	0.87	37.37	269.29	89.51	17.14
783	15.66	0.94	32.21	276.00	81.97	17.01
784	15.68	1.03	29.17	283.38	74.85	16.92
785	15.70	1.11	28.11	288.49	68.49	16.88
786	15.72	1.22	26.61	293.29	63.81	16.87
787	15.74	1.29	26.03	296.18	61.01	16.89
788	15.76	1.32	28.02	295.20	66.15	16.83
789	15.78	0.85	25.40	286.77	68.55	16.95
790	15.80	1.26	35.11	293.23	71.65	17.08
791	15.82	1.26	38.89	287.57	68.92	17.33
792	15.85	1.24	45.21	281.17	72.86	17.49
793	15.86	1.19	53.60	297.91	77.08	17.62
794	15.88	1.16	57.09	301.42	79.85	17.67
795	15.90	1.15	54.21	299.88	80.72	17.66
796	15.92	1.13	51.77	299.51	80.29	17.59
797	15.94	1.12	48.51	301.54	80.09	17.52
798	15.96	1.09	45.56	308.25	78.64	17.42
799	15.98	1.12	40.37	314.22	76.75	17.33
800	16.00	1.13	38.12	320.25	73.08	17.27
801	16.02	1.23	37.39	327.38	69.77	17.26
802	16.04	1.30	37.67	332.37	66.88	17.28
803	16.06	1.32	37.83	334.03	65.64	17.29
804	16.08	1.33	37.99	328.55	66.20	17.32
805	16.10	1.29	40.33	320.49	69.28	17.37
806	16.12	1.19	44.72	311.38	74.61	17.45
807	16.14	1.11	49.88	307.26	80.99	17.52
808	16.16	1.04	52.28	305.05	85.84	17.57
809	16.18	1.01	53.15	308.68	88.04	17.60
810	16.20	1.04	55.36	325.72	87.44	17.61
811	16.22	1.06	52.51	332.06	85.74	17.56
812	16.24	1.04	46.48	332.18	84.35	17.46
813	16.26	1.01	42.03	330.95	82.52	17.29
814	16.28	1.01	34.72	334.46	79.80	17.14
815	16.30	1.04	30.85	343.02	74.18	17.00
816	16.32	1.16	28.35	364.86	67.51	16.92

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
817	16.34	1.30	26.14	372.62	61.52	16.91
818	16.36	1.41	27.48	376.68	59.15	16.98
819	16.38	1.41	31.94	375.02	59.82	17.09
820	16.40	1.36	33.89	366.40	62.88	17.17
821	16.42	1.27	35.30	346.40	66.83	17.22
822	16.44	1.20	38.09	332.68	72.14	17.28
823	16.46	1.12	42.90	326.22	78.12	17.39
824	16.48	1.05	48.57	342.83	82.36	17.45
825	16.50	1.05	47.77	350.65	84.03	17.47
826	16.52	1.06	46.23	348.12	83.53	17.45
827	16.54	1.05	45.27	349.11	83.12	17.41
828	16.56	1.04	43.09	352.43	81.22	17.33
829	16.58	1.08	37.45	356.62	78.44	17.22
830	16.60	1.09	33.09	357.60	75.10	17.09
831	16.62	1.09	30.37	358.71	73.68	17.00
832	16.64	1.09	30.08	360.74	73.16	16.95
833	16.66	1.07	28.99	362.52	73.35	16.91
834	16.68	1.05	27.77	367.57	72.45	16.84
835	16.70	1.08	25.15	373.78	70.99	16.78
836	16.72	1.10	24.51	380.12	67.45	16.73
837	16.74	1.20	23.61	392.98	63.48	16.72
838	16.76	1.29	22.62	408.80	60.16	16.87
839	16.79	1.45	31.89	452.43	59.21	17.05
840	16.80	1.46	35.16	425.91	61.12	17.25
841	16.82	1.36	38.94	424.18	63.39	17.31
842	16.84	1.36	38.53	423.45	65.29	17.33
843	16.86	1.37	41.99	431.82	66.05	17.40

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (m)
q_c:	Measured cone resistance (MPa)
f_s:	Sleeve friction resistance (kPa)
u:	Pore pressure (kPa)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (kN/m^3)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1	0.02	0.30	0.20	0.11	1.00	0.421	1.43	0.295	1.10	1.00	2.000	Yes
2	0.04	0.63	0.39	0.24	1.00	0.399	1.43	0.279	1.10	1.00	2.000	Yes
3	0.06	0.96	0.59	0.37	1.00	0.386	1.43	0.270	1.10	1.00	2.000	Yes
4	0.08	1.30	0.78	0.52	1.00	0.375	1.43	0.263	1.10	1.00	2.000	Yes
5	0.10	1.66	0.98	0.67	1.00	0.367	1.43	0.257	1.10	1.00	2.000	Yes
6	0.12	2.01	1.18	0.83	1.00	0.360	1.43	0.252	1.10	1.00	2.000	Yes
7	0.14	2.37	1.37	1.00	1.00	0.355	1.43	0.248	1.10	1.00	2.000	Yes
8	0.17	2.92	1.67	1.25	1.00	0.349	1.43	0.244	1.10	1.00	2.000	Yes
9	0.18	3.10	1.77	1.34	1.00	0.347	1.43	0.243	1.10	1.00	2.000	Yes
10	0.20	3.47	1.96	1.51	1.00	0.344	1.43	0.241	1.10	1.00	0.285	No
11	0.23	4.02	2.26	1.77	1.00	0.340	1.43	0.238	1.10	1.00	0.282	No
12	0.24	4.21	2.35	1.86	1.00	0.339	1.43	0.237	1.10	1.00	0.281	No
13	0.26	4.58	2.55	2.03	1.00	0.337	1.43	0.236	1.10	1.00	0.280	No
14	0.29	5.14	2.84	2.29	1.00	0.335	1.43	0.235	1.10	1.00	0.278	No
15	0.30	5.32	2.94	2.38	1.00	0.334	1.43	0.234	1.10	1.00	0.277	No
16	0.32	5.69	3.14	2.55	1.00	0.333	1.43	0.233	1.10	1.00	0.277	No
17	0.34	6.06	3.34	2.72	1.00	0.333	1.43	0.233	1.10	1.00	0.276	No
18	0.36	6.43	3.53	2.90	1.00	0.332	1.43	0.232	1.10	1.00	0.275	No
19	0.38	6.80	3.73	3.07	1.00	0.331	1.43	0.232	1.10	1.00	0.275	No
20	0.40	7.17	3.92	3.24	1.00	0.330	1.43	0.231	1.10	1.00	0.274	No
21	0.42	7.54	4.12	3.41	1.00	0.330	1.43	0.231	1.10	1.00	0.273	No
22	0.44	7.90	4.32	3.59	1.00	0.329	1.43	0.231	1.10	1.00	0.273	No
23	0.46	8.27	4.51	3.76	1.00	0.329	1.43	0.230	1.10	1.00	0.272	No
24	0.48	8.64	4.71	3.93	1.00	0.328	1.43	0.230	1.10	1.00	0.272	No
25	0.50	9.01	4.91	4.11	1.00	0.328	1.43	0.230	1.10	1.00	0.271	No
26	0.53	9.56	5.20	4.37	1.00	0.328	1.43	0.229	1.10	1.00	0.271	No
27	0.54	9.75	5.30	4.45	1.00	0.327	1.43	0.229	1.10	1.00	0.271	No
28	0.56	10.12	5.49	4.62	1.00	0.327	1.43	0.229	1.10	1.00	0.270	No
29	0.58	10.48	5.69	4.79	1.00	0.327	1.43	0.229	1.10	1.00	0.271	No
30	0.60	10.85	5.89	4.96	1.00	0.327	1.43	0.229	1.10	1.00	0.271	No
31	0.62	11.22	6.08	5.13	1.00	0.327	1.43	0.229	1.10	1.00	0.271	No
32	0.64	11.58	6.28	5.30	1.00	0.326	1.43	0.228	1.10	1.00	0.271	No
33	0.66	11.94	6.47	5.47	1.00	0.326	1.43	0.228	1.10	1.00	0.271	No
34	0.68	12.31	6.67	5.64	1.00	0.326	1.43	0.228	1.10	1.00	0.272	No
35	0.70	12.67	6.87	5.80	1.00	0.326	1.43	0.228	1.10	1.00	0.273	No
36	0.72	13.03	7.06	5.97	1.00	0.326	1.43	0.228	1.10	1.00	0.274	No
37	0.74	13.39	7.26	6.13	1.00	0.326	1.43	0.228	1.10	1.00	0.274	No
38	0.76	13.74	7.46	6.29	1.00	0.326	1.43	0.228	1.10	1.00	0.275	No
39	0.78	14.10	7.65	6.45	1.00	0.326	1.43	0.228	1.10	1.00	0.275	No
40	0.80	14.45	7.85	6.60	1.00	0.326	1.43	0.228	1.10	1.00	0.276	No
41	0.82	14.80	8.04	6.76	1.00	0.327	1.43	0.229	1.10	1.00	0.276	No
42	0.84	15.15	8.24	6.91	1.00	0.327	1.43	0.229	1.10	1.00	0.276	No
43	0.86	15.50	8.44	7.06	1.00	0.327	1.43	0.229	1.10	1.00	0.276	No
44	0.88	15.84	8.63	7.21	1.00	0.327	1.43	0.229	1.10	1.00	0.275	No
45	0.90	16.19	8.83	7.36	1.00	0.327	1.43	0.229	1.10	1.00	0.273	No
46	0.92	16.54	9.03	7.51	1.00	0.328	1.43	0.229	1.10	1.00	0.273	No
47	0.94	16.89	9.22	7.66	1.00	0.328	1.43	0.229	1.10	1.00	0.272	No
48	0.96	17.24	9.42	7.82	1.00	0.328	1.43	0.230	1.10	1.00	0.271	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
49	0.98	17.60	9.61	7.98	0.99	0.328	1.43	0.229	1.10	1.00	0.271	No
50	1.00	17.95	9.81	8.14	0.99	0.328	1.43	0.229	1.10	1.00	0.271	No
51	1.02	18.32	10.01	8.31	0.99	0.328	1.43	0.229	1.10	1.00	0.270	No
52	1.04	18.68	10.20	8.48	0.99	0.327	1.43	0.229	1.10	1.00	0.270	No
53	1.07	19.23	10.50	8.74	0.99	0.327	1.43	0.229	1.10	1.00	0.270	No
54	1.08	19.42	10.59	8.82	0.99	0.327	1.43	0.229	1.10	1.00	0.270	No
55	1.10	19.79	10.79	9.00	0.99	0.327	1.43	0.229	1.10	1.00	0.270	No
56	1.12	20.16	10.99	9.17	0.99	0.326	1.43	0.228	1.10	1.00	0.270	No
57	1.14	20.53	11.18	9.34	0.99	0.326	1.43	0.228	1.10	1.00	0.269	No
58	1.16	20.90	11.38	9.52	0.99	0.326	1.43	0.228	1.10	1.00	0.269	No
59	1.18	21.27	11.58	9.69	0.99	0.325	1.43	0.228	1.10	1.00	0.269	No
60	1.20	21.64	11.77	9.87	0.99	0.325	1.43	0.228	1.10	1.00	0.268	No
61	1.22	22.01	11.97	10.04	0.99	0.325	1.43	0.227	1.10	1.00	0.268	No
62	1.24	22.38	12.16	10.21	0.99	0.325	1.43	0.227	1.10	1.00	0.268	No
63	1.26	22.75	12.36	10.39	0.99	0.324	1.43	0.227	1.10	1.00	0.268	No
64	1.28	23.12	12.56	10.56	0.99	0.324	1.43	0.227	1.10	1.00	0.267	No
65	1.30	23.49	12.75	10.73	0.99	0.324	1.43	0.227	1.10	1.00	0.267	No
66	1.32	23.86	12.95	10.91	0.99	0.324	1.43	0.227	1.10	1.00	0.267	No
67	1.34	24.23	13.15	11.08	0.99	0.323	1.43	0.226	1.10	1.00	0.267	No
68	1.36	24.60	13.34	11.26	0.99	0.323	1.43	0.226	1.10	1.00	0.266	No
69	1.38	24.97	13.54	11.43	0.99	0.323	1.43	0.226	1.10	1.00	0.266	No
70	1.40	25.34	13.73	11.60	0.99	0.323	1.43	0.226	1.10	1.00	0.267	No
71	1.42	25.71	13.93	11.78	0.99	0.322	1.43	0.226	1.10	1.00	0.267	No
72	1.44	26.07	14.13	11.95	0.99	0.322	1.43	0.226	1.10	1.00	0.267	No
73	1.46	26.44	14.32	12.12	0.99	0.322	1.43	0.225	1.10	1.00	0.267	No
74	1.48	26.81	14.52	12.29	0.99	0.322	1.43	0.225	1.10	1.00	0.267	No
75	1.50	27.18	14.72	12.46	0.99	0.322	1.43	0.225	1.10	1.00	0.267	No
76	1.52	27.55	14.91	12.63	0.99	0.322	1.43	0.225	1.10	1.00	0.267	No
77	1.54	27.91	15.11	12.80	0.99	0.321	1.43	0.225	1.10	1.00	0.268	No
78	1.56	28.27	15.30	12.97	0.99	0.321	1.43	0.225	1.10	1.00	0.268	No
79	1.58	28.64	15.50	13.14	0.99	0.321	1.43	0.225	1.10	1.00	0.268	No
80	1.60	29.00	15.70	13.30	0.99	0.321	1.43	0.225	1.10	1.00	0.268	No
81	1.62	29.36	15.89	13.47	0.99	0.321	1.43	0.225	1.10	1.00	0.268	No
82	1.64	29.72	16.09	13.64	0.98	0.321	1.43	0.225	1.10	1.00	0.268	No
83	1.66	30.09	16.28	13.80	0.98	0.321	1.43	0.225	1.10	1.00	0.268	No
84	1.68	30.45	16.48	13.97	0.98	0.321	1.43	0.224	1.10	1.00	0.268	No
85	1.70	30.81	16.68	14.13	0.98	0.321	1.43	0.224	1.10	1.00	0.267	No
86	1.72	31.17	16.87	14.30	0.98	0.321	1.43	0.224	1.10	1.00	0.266	No
87	1.74	31.53	17.07	14.46	0.98	0.320	1.43	0.224	1.10	1.00	0.265	No
88	1.76	31.89	17.27	14.63	0.98	0.320	1.43	0.224	1.10	1.00	0.265	No
89	1.78	32.26	17.46	14.79	0.98	0.320	1.43	0.224	1.10	1.00	0.265	No
90	1.80	32.62	17.66	14.96	0.98	0.320	1.43	0.224	1.10	1.00	0.264	No
91	1.82	32.98	17.85	15.12	0.98	0.320	1.43	0.224	1.10	1.00	0.264	No
92	1.84	33.34	18.05	15.29	0.98	0.320	1.43	0.224	1.10	1.00	0.264	No
93	1.86	33.70	18.25	15.45	0.98	0.320	1.43	0.224	1.10	1.00	0.264	No
94	1.88	34.06	18.44	15.62	0.98	0.320	1.43	0.224	1.10	1.00	0.265	No
95	1.90	34.42	18.64	15.78	0.98	0.320	1.43	0.224	1.10	1.00	0.265	No
96	1.92	34.77	18.84	15.94	0.98	0.320	1.43	0.224	1.10	1.00	0.265	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
97	1.94	35.13	19.03	16.10	0.98	0.320	1.43	0.224	1.10	1.00	0.266	No
98	1.96	35.48	19.23	16.26	0.98	0.320	1.43	0.224	1.10	1.00	0.266	No
99	1.98	35.84	19.42	16.41	0.98	0.320	1.43	0.224	1.10	1.00	0.266	No
100	2.01	36.37	19.72	16.65	0.98	0.320	1.43	0.224	1.10	1.00	0.266	No
101	2.02	36.54	19.82	16.72	0.98	0.320	1.43	0.224	1.10	1.00	0.267	No
102	2.04	36.89	20.01	16.88	0.98	0.320	1.43	0.224	1.10	1.00	0.267	No
103	2.06	37.24	20.21	17.03	0.98	0.320	1.43	0.224	1.10	1.00	0.267	No
104	2.08	37.59	20.40	17.18	0.98	0.320	1.43	0.224	1.10	1.00	0.267	No
105	2.10	37.94	20.60	17.34	0.98	0.320	1.43	0.224	1.10	1.00	0.267	No
106	2.12	38.29	20.80	17.49	0.98	0.320	1.43	0.224	1.10	1.00	0.267	No
107	2.14	38.64	20.99	17.64	0.98	0.320	1.43	0.224	1.10	1.00	0.267	No
108	2.16	38.99	21.19	17.80	0.98	0.320	1.43	0.224	1.10	1.00	0.267	No
109	2.18	39.34	21.39	17.95	0.98	0.320	1.43	0.224	1.10	1.00	0.267	No
110	2.20	39.69	21.58	18.11	0.98	0.320	1.43	0.224	1.10	1.00	0.267	No
111	2.22	40.04	21.78	18.26	0.98	0.320	1.43	0.224	1.10	1.00	0.267	No
112	2.24	40.39	21.97	18.42	0.97	0.320	1.43	0.224	1.10	1.00	0.267	No
113	2.26	40.74	22.17	18.57	0.97	0.320	1.43	0.224	1.10	1.00	0.268	No
114	2.28	41.09	22.37	18.73	0.97	0.320	1.43	0.224	1.10	1.00	0.268	No
115	2.30	41.44	22.56	18.88	0.97	0.320	1.43	0.224	1.10	1.00	0.268	No
116	2.32	41.79	22.76	19.03	0.97	0.320	1.43	0.224	1.10	1.00	0.268	No
117	2.34	42.14	22.96	19.19	0.97	0.320	1.43	0.224	1.10	1.00	0.269	No
118	2.36	42.49	23.15	19.34	0.97	0.320	1.43	0.224	1.10	1.00	0.269	No
119	2.38	42.84	23.35	19.49	0.97	0.320	1.43	0.224	1.10	1.00	0.269	No
120	2.40	43.18	23.54	19.64	0.97	0.320	1.43	0.224	1.10	1.00	0.269	No
121	2.42	43.52	23.74	19.78	0.97	0.320	1.43	0.224	1.10	1.00	0.270	No
122	2.44	43.86	23.94	19.93	0.97	0.320	1.43	0.224	1.10	1.00	0.270	No
123	2.46	44.20	24.13	20.07	0.97	0.320	1.43	0.224	1.10	1.00	0.270	No
124	2.48	44.54	24.33	20.21	0.97	0.320	1.43	0.224	1.10	1.00	0.270	No
125	2.50	44.87	24.53	20.34	0.97	0.320	1.43	0.224	1.10	1.00	0.271	No
126	2.52	45.20	24.72	20.47	0.97	0.320	1.43	0.224	1.10	1.00	0.271	No
127	2.54	45.52	24.92	20.60	0.97	0.320	1.43	0.224	1.10	1.00	0.271	No
128	2.56	45.84	25.11	20.73	0.97	0.321	1.43	0.224	1.10	1.00	0.271	No
129	2.58	46.16	25.31	20.85	0.97	0.321	1.43	0.224	1.10	1.00	0.271	No
130	2.60	46.48	25.51	20.97	0.97	0.321	1.43	0.225	1.10	1.00	0.271	No
131	2.62	46.79	25.70	21.09	0.97	0.321	1.43	0.225	1.10	1.00	0.271	No
132	2.64	47.11	25.90	21.21	0.97	0.321	1.43	0.225	1.10	1.00	0.272	No
133	2.66	47.42	26.09	21.32	0.97	0.322	1.43	0.225	1.10	1.00	0.272	No
134	2.68	47.73	26.29	21.44	0.97	0.322	1.43	0.225	1.10	1.00	0.272	No
135	2.70	48.04	26.49	21.55	0.97	0.322	1.43	0.226	1.10	1.00	0.272	No
136	2.72	48.35	26.68	21.67	0.97	0.322	1.43	0.226	1.10	1.00	0.272	No
137	2.74	48.67	26.88	21.79	0.97	0.323	1.43	0.226	1.10	1.00	0.273	No
138	2.76	48.98	27.08	21.91	0.97	0.323	1.43	0.226	1.10	1.00	0.273	No
139	2.78	49.30	27.27	22.02	0.97	0.323	1.43	0.226	1.10	1.00	0.273	No
140	2.80	49.61	27.47	22.15	0.97	0.323	1.43	0.226	1.10	1.00	0.273	No
141	2.82	49.93	27.66	22.27	0.96	0.323	1.43	0.226	1.10	1.00	0.273	No
142	2.84	50.25	27.86	22.39	0.96	0.324	1.43	0.226	1.10	1.00	0.274	No
143	2.86	50.57	28.06	22.52	0.96	0.324	1.43	0.227	1.10	1.00	0.274	No
144	2.88	50.90	28.25	22.64	0.96	0.324	1.43	0.227	1.10	1.00	0.273	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
145	2.90	51.22	28.45	22.77	0.96	0.324	1.43	0.227	1.10	1.00	0.273	No
146	2.92	51.54	28.65	22.90	0.96	0.324	1.43	0.227	1.10	1.00	0.273	No
147	2.94	51.87	28.84	23.02	0.96	0.324	1.43	0.227	1.10	1.00	0.273	No
148	2.96	52.19	29.04	23.15	0.96	0.324	1.43	0.227	1.10	1.00	0.273	No
149	2.98	52.51	29.23	23.28	0.96	0.324	1.43	0.227	1.10	1.00	0.273	No
150	3.00	52.84	29.43	23.41	0.96	0.324	1.43	0.227	1.10	1.00	0.273	No
151	3.02	53.16	29.63	23.54	0.96	0.325	1.43	0.227	1.10	1.00	0.273	No
152	3.04	53.49	29.82	23.66	0.96	0.325	1.43	0.227	1.10	1.00	0.273	No
153	3.06	53.81	30.02	23.80	0.96	0.325	1.43	0.227	1.10	1.00	0.273	No
154	3.08	54.14	30.21	23.93	0.96	0.325	1.43	0.227	1.10	1.00	0.273	No
155	3.10	54.47	30.41	24.06	0.96	0.325	1.43	0.227	1.10	1.00	0.274	No
156	3.12	54.81	30.61	24.20	0.96	0.325	1.43	0.227	1.10	1.00	0.274	No
157	3.14	55.14	30.80	24.34	0.96	0.325	1.43	0.227	1.10	1.00	0.274	No
158	3.16	55.48	31.00	24.48	0.96	0.325	1.43	0.227	1.10	1.00	0.273	No
159	3.18	55.82	31.20	24.62	0.96	0.325	1.43	0.227	1.10	1.00	0.274	No
160	3.20	56.15	31.39	24.76	0.96	0.325	1.43	0.227	1.10	1.00	0.273	No
161	3.22	56.49	31.59	24.90	0.96	0.325	1.43	0.227	1.10	1.00	0.273	No
162	3.24	56.82	31.78	25.04	0.96	0.325	1.43	0.227	1.10	1.00	0.273	No
163	3.26	57.16	31.98	25.18	0.96	0.325	1.43	0.227	1.10	1.00	0.273	No
164	3.28	57.49	32.18	25.32	0.96	0.325	1.43	0.227	1.10	1.00	0.272	No
165	3.30	57.83	32.37	25.46	0.96	0.325	1.43	0.227	1.10	1.00	0.272	No
166	3.32	58.17	32.57	25.60	0.96	0.325	1.43	0.227	1.10	1.00	0.272	No
167	3.34	58.50	32.77	25.74	0.96	0.325	1.43	0.227	1.10	1.00	0.272	No
168	3.36	58.85	32.96	25.88	0.95	0.325	1.43	0.227	1.10	1.00	0.272	No
169	3.38	59.19	33.16	26.03	0.95	0.324	1.43	0.227	1.10	1.00	0.272	No
170	3.40	59.53	33.35	26.18	0.95	0.324	1.43	0.227	1.10	1.00	0.272	No
171	3.42	59.88	33.55	26.32	0.95	0.324	1.43	0.227	1.10	1.00	0.272	No
172	3.44	60.22	33.75	26.47	0.95	0.324	1.43	0.227	1.10	1.00	0.272	No
173	3.46	60.56	33.94	26.62	0.95	0.324	1.43	0.227	1.10	1.00	0.273	No
174	3.48	60.91	34.14	26.77	0.95	0.324	1.43	0.227	1.10	1.00	0.273	No
175	3.50	61.25	34.34	26.92	0.95	0.324	1.43	0.227	1.10	1.00	0.273	No
176	3.52	61.60	34.53	27.06	0.95	0.324	1.43	0.227	1.10	1.00	0.273	No
177	3.54	61.94	34.73	27.21	0.95	0.324	1.43	0.227	1.10	1.00	0.273	No
178	3.56	62.27	34.92	27.35	0.95	0.324	1.43	0.227	1.10	1.00	0.272	No
179	3.58	62.61	35.12	27.49	0.95	0.324	1.43	0.227	1.10	1.00	0.272	No
180	3.60	62.94	35.32	27.62	0.95	0.324	1.43	0.227	1.10	1.00	0.273	No
181	3.62	63.27	35.51	27.76	0.95	0.324	1.43	0.227	1.10	1.00	0.273	No
182	3.64	63.60	35.71	27.89	0.95	0.324	1.43	0.227	1.10	1.00	0.273	No
183	3.66	63.93	35.90	28.03	0.95	0.324	1.43	0.227	1.10	1.00	0.273	No
184	3.68	64.26	36.10	28.16	0.95	0.324	1.43	0.227	1.10	1.00	0.272	No
185	3.70	64.59	36.30	28.30	0.95	0.324	1.43	0.227	1.10	1.00	0.271	No
186	3.72	64.93	36.49	28.43	0.95	0.324	1.43	0.227	1.10	1.00	0.271	No
187	3.74	65.26	36.69	28.57	0.95	0.324	1.43	0.226	1.10	1.00	0.270	No
188	3.76	65.60	36.89	28.71	0.95	0.324	1.43	0.226	1.10	1.00	0.270	No
189	3.78	65.94	37.08	28.86	0.95	0.323	1.43	0.226	1.10	1.00	0.270	No
190	3.80	66.29	37.28	29.01	0.95	0.323	1.43	0.226	1.10	1.00	0.270	No
191	3.82	66.63	37.47	29.16	0.95	0.323	1.43	0.226	1.10	1.00	0.269	No
192	3.84	66.98	37.67	29.31	0.95	0.323	1.43	0.226	1.10	1.00	0.268	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
193	3.86	67.33	37.87	29.47	0.95	0.323	1.43	0.226	1.10	1.00	0.268	No
194	3.88	67.69	38.06	29.62	0.94	0.323	1.43	0.226	1.10	1.00	0.268	No
195	3.90	68.04	38.26	29.78	0.94	0.323	1.43	0.226	1.10	1.00	0.267	No
196	3.92	68.40	38.46	29.95	0.94	0.322	1.43	0.226	1.10	1.00	0.267	No
197	3.94	68.76	38.65	30.11	0.94	0.322	1.43	0.226	1.10	1.00	0.267	No
198	3.96	69.12	38.85	30.27	0.94	0.322	1.43	0.225	1.10	1.00	0.267	No
199	3.98	69.48	39.04	30.44	0.94	0.322	1.43	0.225	1.10	1.00	0.266	No
200	4.00	69.84	39.24	30.60	0.94	0.322	1.43	0.225	1.10	1.00	0.266	No
201	4.02	70.20	39.44	30.77	0.94	0.321	1.43	0.225	1.10	1.00	0.265	No
202	4.05	70.74	39.73	31.01	0.94	0.321	1.43	0.225	1.10	1.00	0.265	No
203	4.06	70.92	39.83	31.10	0.94	0.321	1.43	0.225	1.10	1.00	0.265	No
204	4.08	71.29	40.02	31.26	0.94	0.321	1.43	0.225	1.10	1.00	0.265	No
205	4.10	71.65	40.22	31.43	0.94	0.321	1.43	0.224	1.10	1.00	0.264	No
206	4.12	72.01	40.42	31.60	0.94	0.320	1.43	0.224	1.10	1.00	0.264	No
207	4.14	72.38	40.61	31.77	0.94	0.320	1.43	0.224	1.10	1.00	0.264	No
208	4.16	72.75	40.81	31.94	0.94	0.320	1.43	0.224	1.10	1.00	0.264	No
209	4.18	73.11	41.01	32.11	0.94	0.320	1.43	0.224	1.10	1.00	0.264	No
210	4.20	73.48	41.20	32.28	0.94	0.319	1.43	0.224	1.10	1.00	0.264	No
211	4.22	73.84	41.40	32.44	0.94	0.319	1.43	0.223	1.10	1.00	0.264	No
212	4.24	74.21	41.59	32.61	0.94	0.319	1.43	0.223	1.10	1.00	0.264	No
213	4.26	74.57	41.79	32.78	0.94	0.319	1.43	0.223	1.10	1.00	0.264	No
214	4.28	74.94	41.99	32.95	0.94	0.319	1.43	0.223	1.10	1.00	0.265	No
215	4.30	75.30	42.18	33.12	0.94	0.318	1.43	0.223	1.10	1.00	0.265	No
216	4.32	75.66	42.38	33.28	0.94	0.318	1.43	0.223	1.10	1.00	0.265	No
217	4.34	76.03	42.58	33.45	0.94	0.318	1.43	0.223	1.10	1.00	0.265	No
218	4.36	76.39	42.77	33.62	0.94	0.318	1.43	0.222	1.10	1.00	0.265	No
219	4.38	76.76	42.97	33.79	0.93	0.318	1.43	0.222	1.10	1.00	0.264	No
220	4.40	77.12	43.16	33.96	0.93	0.317	1.43	0.222	1.10	1.00	0.263	No
221	4.42	77.49	43.36	34.12	0.93	0.317	1.43	0.222	1.10	1.00	0.262	No
222	4.44	77.85	43.56	34.29	0.93	0.317	1.43	0.222	1.10	1.00	0.261	No
223	4.46	78.21	43.75	34.46	0.93	0.317	1.43	0.222	1.10	1.00	0.261	No
224	4.48	78.58	43.95	34.63	0.93	0.316	1.43	0.222	1.10	1.00	0.260	No
225	4.50	78.95	44.15	34.80	0.93	0.316	1.43	0.221	1.10	1.00	0.260	No
226	4.52	79.31	44.34	34.97	0.93	0.316	1.43	0.221	1.10	1.00	0.260	No
227	4.54	79.68	44.54	35.14	0.93	0.316	1.43	0.221	1.10	1.00	0.260	No
228	4.56	80.05	44.73	35.32	0.93	0.316	1.43	0.221	1.10	1.00	0.260	No
229	4.58	80.42	44.93	35.49	0.93	0.315	1.43	0.221	1.10	1.00	0.260	No
230	4.60	80.79	45.13	35.66	0.93	0.315	1.43	0.221	1.10	1.00	0.261	No
231	4.62	81.16	45.32	35.84	0.93	0.315	1.43	0.220	1.10	1.00	0.261	No
232	4.64	81.53	45.52	36.01	0.93	0.315	1.43	0.220	1.09	1.00	0.262	No
233	4.66	81.90	45.71	36.19	0.93	0.314	1.43	0.220	1.09	1.00	0.262	No
234	4.68	82.27	45.91	36.36	0.93	0.314	1.43	0.220	1.09	1.00	0.262	No
235	4.70	82.64	46.11	36.53	0.93	0.314	1.43	0.220	1.09	1.00	0.262	No
236	4.72	83.00	46.30	36.70	0.93	0.314	1.43	0.220	1.09	1.00	0.263	No
237	4.74	83.37	46.50	36.87	0.93	0.314	1.43	0.219	1.09	1.00	0.264	No
238	4.76	83.73	46.70	37.04	0.93	0.313	1.43	0.219	1.09	1.00	0.264	No
239	4.78	84.10	46.89	37.21	0.93	0.313	1.43	0.219	1.09	1.00	0.265	No
240	4.80	84.46	47.09	37.38	0.93	0.313	1.43	0.219	1.09	1.00	0.265	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
241	4.82	84.83	47.28	37.54	0.93	0.313	1.43	0.219	1.09	1.00	0.266	No
242	4.84	85.19	47.48	37.71	0.93	0.313	1.43	0.219	1.08	1.00	0.267	No
243	4.86	85.55	47.68	37.87	0.93	0.312	1.43	0.219	1.08	1.00	0.266	No
244	4.88	85.91	47.87	38.04	0.92	0.312	1.43	0.219	1.08	1.00	0.266	No
245	4.91	86.45	48.17	38.28	0.92	0.312	1.43	0.218	1.08	1.00	0.266	No
246	4.92	86.63	48.27	38.36	0.92	0.312	1.43	0.218	1.08	1.00	0.266	No
247	4.94	86.99	48.46	38.53	0.92	0.312	1.43	0.218	1.08	1.00	0.266	No
248	4.96	87.34	48.66	38.68	0.92	0.312	1.43	0.218	1.08	1.00	0.266	No
249	4.98	87.70	48.85	38.84	0.92	0.311	1.43	0.218	1.08	1.00	0.265	No
250	5.00	88.05	49.05	39.00	0.92	0.311	1.43	0.218	1.08	1.00	0.265	No
251	5.02	88.41	49.25	39.16	0.92	0.311	1.43	0.218	1.08	1.00	0.265	No
252	5.04	88.76	49.44	39.32	0.92	0.311	1.43	0.218	1.08	1.00	0.265	No
253	5.06	89.11	49.64	39.47	0.92	0.311	1.43	0.218	1.08	1.00	0.264	No
254	5.08	89.47	49.83	39.63	0.92	0.311	1.43	0.217	1.08	1.00	0.264	No
255	5.10	89.82	50.03	39.79	0.92	0.311	1.43	0.217	1.08	1.00	0.264	No
256	5.12	90.18	50.23	39.95	0.92	0.310	1.43	0.217	1.08	1.00	0.264	No
257	5.14	90.53	50.42	40.11	0.92	0.310	1.43	0.217	1.08	1.00	0.264	No
258	5.16	90.88	50.62	40.26	0.92	0.310	1.43	0.217	1.08	1.00	0.265	No
259	5.18	91.24	50.82	40.42	0.92	0.310	1.43	0.217	1.08	1.00	0.265	No
260	5.20	91.59	51.01	40.58	0.92	0.310	1.43	0.217	1.08	1.00	0.265	No
261	5.22	91.94	51.21	40.74	0.92	0.310	1.43	0.217	1.08	1.00	0.265	No
262	5.24	92.30	51.40	40.89	0.92	0.309	1.43	0.217	1.08	1.00	0.265	No
263	5.26	92.65	51.60	41.05	0.92	0.309	1.43	0.217	1.08	1.00	0.265	No
264	5.28	93.00	51.80	41.20	0.92	0.309	1.43	0.216	1.08	1.00	0.265	No
265	5.30	93.35	51.99	41.35	0.92	0.309	1.43	0.216	1.08	1.00	0.264	No
266	5.32	93.70	52.19	41.51	0.92	0.309	1.43	0.216	1.08	1.00	0.264	No
267	5.34	94.05	52.39	41.66	0.92	0.309	1.43	0.216	1.08	1.00	0.263	No
268	5.36	94.39	52.58	41.81	0.91	0.309	1.43	0.216	1.08	1.00	0.263	No
269	5.38	94.74	52.78	41.97	0.91	0.309	1.43	0.216	1.08	1.00	0.263	No
270	5.40	95.10	52.97	42.12	0.91	0.308	1.43	0.216	1.08	1.00	0.263	No
271	5.42	95.45	53.17	42.28	0.91	0.308	1.43	0.216	1.08	1.00	0.263	No
272	5.44	95.80	53.37	42.44	0.91	0.308	1.43	0.216	1.08	1.00	0.263	No
273	5.46	96.16	53.56	42.60	0.91	0.308	1.43	0.216	1.08	1.00	0.262	No
274	5.48	96.52	53.76	42.76	0.91	0.308	1.43	0.215	1.08	1.00	0.262	No
275	5.50	96.87	53.96	42.92	0.91	0.308	1.43	0.215	1.08	1.00	0.262	No
276	5.52	97.23	54.15	43.08	0.91	0.307	1.43	0.215	1.08	1.00	0.262	No
277	5.54	97.59	54.35	43.24	0.91	0.307	1.43	0.215	1.08	1.00	0.262	No
278	5.56	97.95	54.54	43.40	0.91	0.307	1.43	0.215	1.07	1.00	0.263	No
279	5.58	98.30	54.74	43.56	0.91	0.307	1.43	0.215	1.07	1.00	0.263	No
280	5.60	98.66	54.94	43.72	0.91	0.307	1.43	0.215	1.07	1.00	0.263	No
281	5.62	99.02	55.13	43.88	0.91	0.307	1.43	0.215	1.07	1.00	0.263	No
282	5.64	99.37	55.33	44.04	0.91	0.306	1.43	0.215	1.07	1.00	0.263	No
283	5.66	99.73	55.52	44.20	0.91	0.306	1.43	0.214	1.07	1.00	0.263	No
284	5.68	100.08	55.72	44.36	0.91	0.306	1.43	0.214	1.07	1.00	0.263	No
285	5.70	100.44	55.92	44.52	0.91	0.306	1.43	0.214	1.07	1.00	0.263	No
286	5.72	100.79	56.11	44.68	0.91	0.306	1.43	0.214	1.07	1.00	0.263	No
287	5.74	101.15	56.31	44.84	0.91	0.306	1.43	0.214	1.07	1.00	0.263	No
288	5.76	101.50	56.51	45.00	0.91	0.306	1.43	0.214	1.07	1.00	0.263	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
289	5.78	101.86	56.70	45.16	0.91	0.305	1.43	0.214	1.07	1.00	0.263	No
290	5.80	102.21	56.90	45.31	0.91	0.305	1.43	0.214	1.07	1.00	0.263	No
291	5.82	102.57	57.09	45.47	0.90	0.305	1.43	0.214	1.07	1.00	0.263	No
292	5.84	102.92	57.29	45.63	0.90	0.305	1.43	0.213	1.07	1.00	0.263	No
293	5.86	103.28	57.49	45.79	0.90	0.305	1.43	0.213	1.07	1.00	0.263	No
294	5.88	103.63	57.68	45.95	0.90	0.305	1.43	0.213	1.07	1.00	0.263	No
295	5.90	103.99	57.88	46.11	0.90	0.304	1.43	0.213	1.07	1.00	0.262	No
296	5.92	104.34	58.08	46.27	0.90	0.304	1.43	0.213	1.07	1.00	0.261	No
297	5.94	104.70	58.27	46.43	0.90	0.304	1.43	0.213	1.07	1.00	0.261	No
298	5.96	105.05	58.47	46.58	0.90	0.304	1.43	0.213	1.07	1.00	0.261	No
299	5.98	105.41	58.66	46.74	0.90	0.304	1.43	0.213	1.07	1.00	0.261	No
300	6.00	105.76	58.86	46.90	0.90	0.304	1.43	0.213	1.07	1.00	0.261	No
301	6.02	106.12	59.06	47.07	0.90	0.303	1.43	0.212	1.07	1.00	0.260	No
302	6.04	106.48	59.25	47.23	0.90	0.303	1.43	0.212	1.07	1.00	0.260	No
303	6.06	106.84	59.45	47.40	0.90	0.303	1.43	0.212	1.07	1.00	0.260	No
304	6.08	107.21	59.64	47.56	0.90	0.303	1.43	0.212	1.07	1.00	0.260	No
305	6.10	107.57	59.84	47.73	0.90	0.303	1.43	0.212	1.07	1.00	0.260	No
306	6.12	107.93	60.04	47.90	0.90	0.303	1.43	0.212	1.07	1.00	0.260	No
307	6.14	108.30	60.23	48.06	0.90	0.302	1.43	0.212	1.07	1.00	0.259	No
308	6.16	108.66	60.43	48.23	0.90	0.302	1.43	0.212	1.07	1.00	0.259	No
309	6.18	109.03	60.63	48.40	0.90	0.302	1.43	0.211	1.07	1.00	0.259	No
310	6.20	109.40	60.82	48.57	0.90	0.302	1.43	0.211	1.07	1.00	0.258	No
311	6.22	109.76	61.02	48.74	0.90	0.302	1.43	0.211	1.07	1.00	0.257	No
312	6.24	110.13	61.21	48.92	0.90	0.301	1.43	0.211	1.07	1.00	0.257	No
313	6.26	110.50	61.41	49.09	0.89	0.301	1.43	0.211	1.07	1.00	0.257	No
314	6.28	110.87	61.61	49.26	0.89	0.301	1.43	0.211	1.07	1.00	0.257	No
315	6.30	111.23	61.80	49.43	0.89	0.301	1.43	0.211	1.07	1.00	0.257	No
316	6.32	111.60	62.00	49.60	0.89	0.301	1.43	0.210	1.07	1.00	0.258	No
317	6.34	111.97	62.20	49.78	0.89	0.300	1.43	0.210	1.06	1.00	0.258	No
318	6.36	112.34	62.39	49.95	0.89	0.300	1.43	0.210	1.06	1.00	0.258	No
319	6.38	112.71	62.59	50.12	0.89	0.300	1.43	0.210	1.06	1.00	0.258	No
320	6.40	113.08	62.78	50.30	0.89	0.300	1.43	0.210	1.06	1.00	0.258	No
321	6.42	113.45	62.98	50.47	0.89	0.300	1.43	0.210	1.06	1.00	0.258	No
322	6.44	113.82	63.18	50.64	0.89	0.299	1.43	0.210	1.06	1.00	0.258	No
323	6.46	114.18	63.37	50.81	0.89	0.299	1.43	0.209	1.06	1.00	0.259	No
324	6.48	114.55	63.57	50.98	0.89	0.299	1.43	0.209	1.06	1.00	0.258	No
325	6.50	114.91	63.77	51.15	0.89	0.299	1.43	0.209	1.06	1.00	0.258	No
326	6.52	115.28	63.96	51.32	0.89	0.299	1.43	0.209	1.06	1.00	0.258	No
327	6.54	115.64	64.16	51.49	0.89	0.298	1.43	0.209	1.06	1.00	0.258	No
328	6.56	116.01	64.35	51.65	0.89	0.298	1.43	0.209	1.06	1.00	0.258	No
329	6.58	116.37	64.55	51.82	0.89	0.298	1.43	0.209	1.06	1.00	0.259	No
330	6.60	116.73	64.75	51.98	0.89	0.298	1.43	0.209	1.06	1.00	0.259	No
331	6.62	117.09	64.94	52.14	0.89	0.298	1.43	0.208	1.06	1.00	0.259	No
332	6.64	117.45	65.14	52.31	0.89	0.298	1.43	0.208	1.06	1.00	0.259	No
333	6.66	117.81	65.33	52.47	0.89	0.297	1.43	0.208	1.06	1.00	0.260	No
334	6.68	118.17	65.53	52.64	0.89	0.297	1.43	0.208	1.06	1.00	0.260	No
335	6.70	118.53	65.73	52.80	0.89	0.297	1.43	0.208	1.06	1.00	0.259	No
336	6.72	118.89	65.92	52.97	0.88	0.297	1.43	0.208	1.06	1.00	0.259	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
337	6.74	119.25	66.12	53.13	0.88	0.297	1.43	0.208	1.06	1.00	0.259	No
338	6.76	119.61	66.32	53.30	0.88	0.297	1.43	0.208	1.06	1.00	0.259	No
339	6.78	119.97	66.51	53.46	0.88	0.296	1.43	0.207	1.06	1.00	0.259	No
340	6.80	120.34	66.71	53.63	0.88	0.296	1.43	0.207	1.05	1.00	0.259	No
341	6.82	120.70	66.90	53.79	0.88	0.296	1.43	0.207	1.05	1.00	0.258	No
342	6.84	121.06	67.10	53.96	0.88	0.296	1.43	0.207	1.06	1.00	0.258	No
343	6.86	121.42	67.30	54.12	0.88	0.296	1.43	0.207	1.06	1.00	0.258	No
344	6.88	121.78	67.49	54.29	0.88	0.295	1.43	0.207	1.05	1.00	0.257	No
345	6.90	122.15	67.69	54.46	0.88	0.295	1.43	0.207	1.05	1.00	0.257	No
346	6.92	122.51	67.89	54.63	0.88	0.295	1.43	0.207	1.05	1.00	0.258	No
347	6.94	122.88	68.08	54.80	0.88	0.295	1.43	0.206	1.05	1.00	0.257	No
348	6.96	123.24	68.28	54.97	0.88	0.295	1.43	0.206	1.05	1.00	0.256	No
349	6.98	123.61	68.47	55.14	0.88	0.295	1.43	0.206	1.05	1.00	0.256	No
350	7.00	123.97	68.67	55.30	0.88	0.294	1.43	0.206	1.05	1.00	0.256	No
351	7.02	124.34	68.87	55.47	0.88	0.294	1.43	0.206	1.05	1.00	0.257	No
352	7.04	124.70	69.06	55.64	0.88	0.294	1.43	0.206	1.05	1.00	0.258	No
353	7.06	125.06	69.26	55.81	0.88	0.294	1.43	0.206	1.05	1.00	0.258	No
354	7.08	125.43	69.45	55.97	0.88	0.294	1.43	0.206	1.05	1.00	0.258	No
355	7.10	125.79	69.65	56.14	0.88	0.293	1.43	0.205	1.05	1.00	0.257	No
356	7.12	126.15	69.85	56.30	0.88	0.293	1.43	0.205	1.05	1.00	0.257	No
357	7.14	126.51	70.04	56.47	0.88	0.293	1.43	0.205	1.05	1.00	0.257	No
358	7.16	126.87	70.24	56.63	0.87	0.293	1.43	0.205	1.05	1.00	0.256	No
359	7.18	127.23	70.44	56.80	0.87	0.293	1.43	0.205	1.05	1.00	0.256	No
360	7.20	127.59	70.63	56.96	0.87	0.293	1.43	0.205	1.05	1.00	0.255	No
361	7.22	127.95	70.83	57.12	0.87	0.292	1.43	0.205	1.05	1.00	0.255	No
362	7.24	128.31	71.02	57.29	0.87	0.292	1.43	0.205	1.05	1.00	0.254	No
363	7.26	128.67	71.22	57.45	0.87	0.292	1.43	0.204	1.05	1.00	0.254	No
364	7.28	129.04	71.42	57.62	0.87	0.292	1.43	0.204	1.05	1.00	0.253	No
365	7.30	129.40	71.61	57.79	0.87	0.292	1.43	0.204	1.05	1.00	0.252	No
366	7.32	129.77	71.81	57.96	0.87	0.292	1.43	0.204	1.05	1.00	0.252	No
367	7.34	130.13	72.01	58.13	0.87	0.291	1.43	0.204	1.05	1.00	0.252	No
368	7.36	130.50	72.20	58.30	0.87	0.291	1.43	0.204	1.05	1.00	0.252	No
369	7.38	130.87	72.40	58.47	0.87	0.291	1.43	0.204	1.05	1.00	0.252	No
370	7.40	131.24	72.59	58.65	0.87	0.291	1.43	0.204	1.05	1.00	0.252	No
371	7.42	131.62	72.79	58.83	0.87	0.291	1.43	0.203	1.05	1.00	0.252	No
372	7.44	131.99	72.99	59.01	0.87	0.290	1.43	0.203	1.05	1.00	0.253	No
373	7.46	132.37	73.18	59.18	0.87	0.290	1.43	0.203	1.05	1.00	0.253	No
374	7.48	132.74	73.38	59.36	0.87	0.290	1.43	0.203	1.05	1.00	0.253	No
375	7.50	133.11	73.58	59.54	0.87	0.290	1.43	0.203	1.05	1.00	0.253	No
376	7.52	133.48	73.77	59.71	0.87	0.290	1.43	0.203	1.05	1.00	0.252	No
377	7.54	133.85	73.97	59.89	0.87	0.289	1.43	0.203	1.05	1.00	0.252	No
378	7.56	134.22	74.16	60.06	0.87	0.289	1.43	0.202	1.05	1.00	0.252	No
379	7.58	134.59	74.36	60.23	0.87	0.289	1.43	0.202	1.05	1.00	0.252	No
380	7.60	134.96	74.56	60.40	0.86	0.289	1.43	0.202	1.05	1.00	0.252	No
381	7.62	135.33	74.75	60.58	0.86	0.289	1.43	0.202	1.05	1.00	0.252	No
382	7.64	135.70	74.95	60.75	0.86	0.288	1.43	0.202	1.05	1.00	0.252	No
383	7.66	136.07	75.14	60.93	0.86	0.288	1.43	0.202	1.05	1.00	0.252	No
384	7.68	136.44	75.34	61.10	0.86	0.288	1.43	0.202	1.05	1.00	0.252	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
385	7.70	136.81	75.54	61.28	0.86	0.288	1.43	0.201	1.05	1.00	0.252	No
386	7.72	137.18	75.73	61.45	0.86	0.288	1.43	0.201	1.05	1.00	0.252	No
387	7.74	137.55	75.93	61.63	0.86	0.287	1.43	0.201	1.04	1.00	0.251	No
388	7.76	137.92	76.13	61.80	0.86	0.287	1.43	0.201	1.04	1.00	0.251	No
389	7.78	138.29	76.32	61.97	0.86	0.287	1.43	0.201	1.05	1.00	0.250	No
390	7.80	138.66	76.52	62.14	0.86	0.287	1.43	0.201	1.05	1.00	0.250	No
391	7.82	139.03	76.71	62.31	0.86	0.287	1.43	0.201	1.04	1.00	0.253	No
392	7.84	139.40	76.91	62.49	0.86	0.286	1.43	0.201	1.04	1.00	0.250	No
393	7.86	139.77	77.11	62.66	0.86	0.286	1.43	0.200	1.04	1.00	0.250	No
394	7.88	140.14	77.30	62.83	0.86	0.286	1.43	0.200	1.04	1.00	0.250	No
395	7.90	140.51	77.50	63.01	0.86	0.286	1.43	0.200	1.04	1.00	0.250	No
396	7.92	140.88	77.70	63.19	0.86	0.286	1.43	0.200	1.04	1.00	0.250	No
397	7.94	141.25	77.89	63.36	0.86	0.286	1.43	0.200	1.04	1.00	0.249	No
398	7.96	141.63	78.09	63.54	0.86	0.285	1.43	0.200	1.04	1.00	0.249	No
399	7.98	142.00	78.28	63.72	0.86	0.285	1.43	0.200	1.04	1.00	0.249	No
400	8.00	142.37	78.48	63.89	0.86	0.285	1.43	0.199	1.04	1.00	0.249	No
401	8.02	142.74	78.68	64.07	0.85	0.285	1.43	0.199	1.04	1.00	0.249	No
402	8.04	143.12	78.87	64.24	0.85	0.285	1.43	0.199	1.04	1.00	0.249	No
403	8.06	143.49	79.07	64.42	0.85	0.284	1.43	0.199	1.04	1.00	0.250	No
404	8.08	143.86	79.26	64.60	0.85	0.284	1.43	0.199	1.04	1.00	0.250	No
405	8.10	144.23	79.46	64.77	0.85	0.284	1.43	0.199	1.04	1.00	0.249	No
406	8.12	144.60	79.66	64.94	0.85	0.284	1.43	0.199	1.04	1.00	0.249	No
407	8.14	144.97	79.85	65.12	0.85	0.284	1.43	0.198	1.04	1.00	0.249	No
408	8.16	145.34	80.05	65.29	0.85	0.283	1.43	0.198	1.04	1.00	0.249	No
409	8.18	145.71	80.25	65.46	0.85	0.283	1.43	0.198	1.04	1.00	0.249	No
410	8.20	146.08	80.44	65.63	0.85	0.283	1.43	0.198	1.04	1.00	0.249	No
411	8.22	146.45	80.64	65.81	0.85	0.283	1.43	0.198	1.04	1.00	0.250	No
412	8.24	146.81	80.83	65.98	0.85	0.283	1.43	0.198	1.04	1.00	0.250	No
413	8.26	147.18	81.03	66.15	0.85	0.282	1.43	0.198	1.04	1.00	0.250	No
414	8.28	147.55	81.23	66.32	0.85	0.282	1.43	0.198	1.04	1.00	0.251	No
415	8.30	147.92	81.42	66.49	0.85	0.282	1.43	0.197	1.04	1.00	0.251	No
416	8.32	148.28	81.62	66.66	0.85	0.282	1.43	0.197	1.04	1.00	0.251	No
417	8.34	148.64	81.82	66.83	0.85	0.282	1.43	0.197	1.04	1.00	0.251	No
418	8.36	149.00	82.01	66.99	0.85	0.282	1.43	0.197	1.04	1.00	0.251	No
419	8.38	149.36	82.21	67.15	0.85	0.281	1.43	0.197	1.04	1.00	0.251	No
420	8.40	149.71	82.40	67.31	0.85	0.281	1.43	0.197	1.04	1.00	0.251	No
421	8.42	150.07	82.60	67.47	0.85	0.281	1.43	0.197	1.03	1.00	0.251	No
422	8.44	150.42	82.80	67.63	0.84	0.281	1.43	0.197	1.03	1.00	0.251	No
423	8.46	150.77	82.99	67.78	0.84	0.281	1.43	0.197	1.03	1.00	0.251	No
424	8.48	151.13	83.19	67.94	0.84	0.281	1.43	0.196	1.03	1.00	0.251	No
425	8.50	151.48	83.39	68.09	0.84	0.281	1.43	0.196	1.03	1.00	0.251	No
426	8.52	151.83	83.58	68.24	0.84	0.280	1.43	0.196	1.03	1.00	0.251	No
427	8.54	152.17	83.78	68.40	0.84	0.280	1.43	0.196	1.03	1.00	0.251	No
428	8.56	152.52	83.97	68.55	0.84	0.280	1.43	0.196	1.03	1.00	0.251	No
429	8.58	152.87	84.17	68.70	0.84	0.280	1.43	0.196	1.03	1.00	0.251	No
430	8.60	153.22	84.37	68.85	0.84	0.280	1.43	0.196	1.03	1.00	0.251	No
431	8.62	153.57	84.56	69.01	0.84	0.280	1.43	0.196	1.03	1.00	0.251	No
432	8.64	153.92	84.76	69.16	0.84	0.280	1.43	0.196	1.03	1.00	0.250	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
433	8.66	154.26	84.95	69.31	0.84	0.279	1.43	0.196	1.03	1.00	0.250	No
434	8.68	154.61	85.15	69.46	0.84	0.279	1.43	0.195	1.03	1.00	0.250	No
435	8.70	154.96	85.35	69.61	0.84	0.279	1.43	0.195	1.03	1.00	0.249	No
436	8.72	155.31	85.54	69.77	0.84	0.279	1.43	0.195	1.03	1.00	0.249	No
437	8.74	155.66	85.74	69.92	0.84	0.279	1.43	0.195	1.03	1.00	0.249	No
438	8.76	156.01	85.94	70.08	0.84	0.279	1.43	0.195	1.03	1.00	0.250	No
439	8.78	156.37	86.13	70.23	0.84	0.279	1.43	0.195	1.03	1.00	0.250	No
440	8.80	156.72	86.33	70.39	0.84	0.278	1.43	0.195	1.03	1.00	0.250	No
441	8.82	157.08	86.52	70.55	0.84	0.278	1.43	0.195	1.03	1.00	0.250	No
442	8.84	157.43	86.72	70.71	0.84	0.278	1.43	0.195	1.03	1.00	0.250	No
443	8.86	157.79	86.92	70.87	0.83	0.278	1.43	0.195	1.03	1.00	0.250	No
444	8.88	158.14	87.11	71.03	0.83	0.278	1.43	0.194	1.03	1.00	0.250	No
445	8.91	158.67	87.41	71.27	0.83	0.278	1.43	0.194	1.03	1.00	0.250	No
446	8.92	158.85	87.51	71.34	0.83	0.277	1.43	0.194	1.03	1.00	0.250	No
447	8.94	159.20	87.70	71.50	0.83	0.277	1.43	0.194	1.03	1.00	0.250	No
448	8.96	159.54	87.90	71.65	0.83	0.277	1.43	0.194	1.03	1.00	0.249	No
449	8.98	159.89	88.09	71.79	0.83	0.277	1.43	0.194	1.03	1.00	0.249	No
450	9.00	160.23	88.29	71.94	0.83	0.277	1.43	0.194	1.03	1.00	0.249	No
451	9.02	160.58	88.49	72.09	0.83	0.277	1.43	0.194	1.03	1.00	0.249	No
452	9.04	160.92	88.68	72.24	0.83	0.277	1.43	0.194	1.03	1.00	0.249	No
453	9.06	161.27	88.88	72.39	0.83	0.277	1.43	0.194	1.03	1.00	0.248	No
454	9.08	161.62	89.07	72.54	0.83	0.276	1.43	0.193	1.03	1.00	0.247	No
455	9.10	161.96	89.27	72.69	0.83	0.276	1.43	0.193	1.03	1.00	0.247	No
456	9.12	162.32	89.47	72.85	0.83	0.276	1.43	0.193	1.03	1.00	0.246	No
457	9.14	162.67	89.66	73.01	0.83	0.276	1.43	0.193	1.03	1.00	0.246	No
458	9.16	163.03	89.86	73.17	0.83	0.276	1.43	0.193	1.03	1.00	0.246	No
459	9.18	163.38	90.06	73.33	0.83	0.276	1.43	0.193	1.03	1.00	0.246	No
460	9.20	163.75	90.25	73.49	0.83	0.275	1.43	0.193	1.03	1.00	0.246	No
461	9.22	164.11	90.45	73.66	0.83	0.275	1.43	0.193	1.03	1.00	0.246	No
462	9.24	164.47	90.64	73.83	0.83	0.275	1.43	0.193	1.03	1.00	0.246	No
463	9.26	164.83	90.84	73.99	0.83	0.275	1.43	0.192	1.03	1.00	0.246	No
464	9.28	165.20	91.04	74.16	0.83	0.275	1.43	0.192	1.03	1.00	0.246	No
465	9.30	165.56	91.23	74.33	0.82	0.275	1.43	0.192	1.03	1.00	0.246	No
466	9.32	165.93	91.43	74.50	0.82	0.274	1.43	0.192	1.03	1.00	0.246	No
467	9.34	166.29	91.63	74.67	0.82	0.274	1.43	0.192	1.03	1.00	0.246	No
468	9.36	166.66	91.82	74.84	0.82	0.274	1.43	0.192	1.03	1.00	0.245	No
469	9.38	167.03	92.02	75.01	0.82	0.274	1.43	0.192	1.03	1.00	0.245	No
470	9.40	167.39	92.21	75.18	0.82	0.274	1.43	0.192	1.03	1.00	0.245	No
471	9.42	167.76	92.41	75.35	0.82	0.273	1.43	0.191	1.03	1.00	0.246	No
472	9.44	168.12	92.61	75.52	0.82	0.273	1.43	0.191	1.03	1.00	0.246	No
473	9.46	168.49	92.80	75.69	0.82	0.273	1.43	0.191	1.02	1.00	0.246	No
474	9.48	168.85	93.00	75.85	0.82	0.273	1.43	0.191	1.02	1.00	0.246	No
475	9.50	169.22	93.19	76.02	0.82	0.273	1.43	0.191	1.02	1.00	0.246	No
476	9.52	169.58	93.39	76.19	0.82	0.273	1.43	0.191	1.02	1.00	0.246	No
477	9.54	169.95	93.59	76.36	0.82	0.272	1.43	0.191	1.02	1.00	0.246	No
478	9.56	170.31	93.78	76.53	0.82	0.272	1.43	0.191	1.02	1.00	0.246	No
479	9.58	170.67	93.98	76.69	0.82	0.272	1.43	0.190	1.02	1.00	0.246	No
480	9.60	171.03	94.18	76.86	0.82	0.272	1.43	0.190	1.02	1.00	0.246	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
481	9.62	171.39	94.37	77.02	0.82	0.272	1.43	0.190	1.02	1.00	0.246	No
482	9.64	171.75	94.57	77.19	0.82	0.272	1.43	0.190	1.02	1.00	0.246	No
483	9.66	172.11	94.76	77.35	0.82	0.271	1.43	0.190	1.02	1.00	0.246	No
484	9.68	172.47	94.96	77.51	0.82	0.271	1.43	0.190	1.02	1.00	0.246	No
485	9.70	172.83	95.16	77.68	0.81	0.271	1.43	0.190	1.02	1.00	0.245	No
486	9.72	173.19	95.35	77.84	0.81	0.271	1.43	0.190	1.02	1.00	0.245	No
487	9.74	173.55	95.55	78.00	0.81	0.271	1.43	0.190	1.02	1.00	0.245	No
488	9.76	173.90	95.75	78.16	0.81	0.271	1.43	0.189	1.02	1.00	0.245	No
489	9.78	174.26	95.94	78.32	0.81	0.270	1.43	0.189	1.02	1.00	0.244	No
490	9.80	174.61	96.14	78.48	0.81	0.270	1.43	0.189	1.02	1.00	0.244	No
491	9.82	174.97	96.33	78.64	0.81	0.270	1.43	0.189	1.02	1.00	0.244	No
492	9.84	175.33	96.53	78.80	0.81	0.270	1.43	0.189	1.02	1.00	0.243	No
493	9.86	175.68	96.73	78.96	0.81	0.270	1.43	0.189	1.02	1.00	0.243	No
494	9.88	176.04	96.92	79.12	0.81	0.270	1.43	0.189	1.02	1.00	0.243	No
495	9.90	176.41	97.12	79.29	0.81	0.269	1.43	0.189	1.02	1.00	0.243	No
496	9.92	176.77	97.32	79.46	0.81	0.269	1.43	0.189	1.02	1.00	0.243	No
497	9.94	177.14	97.51	79.62	0.81	0.269	1.43	0.188	1.02	1.00	0.243	No
498	9.96	177.50	97.71	79.79	0.81	0.269	1.43	0.188	1.02	1.00	0.243	No
499	9.98	177.87	97.90	79.96	0.81	0.269	1.43	0.188	1.02	1.00	0.243	No
500	10.00	178.23	98.10	80.13	0.81	0.269	1.43	0.188	1.02	1.00	0.243	No
501	10.02	178.59	98.30	80.30	0.81	0.268	1.43	0.188	1.02	1.00	0.243	No
502	10.04	178.96	98.49	80.47	0.81	0.268	1.43	0.188	1.02	1.00	0.243	No
503	10.06	179.32	98.69	80.63	0.81	0.268	1.43	0.188	1.02	1.00	0.243	No
504	10.08	179.68	98.88	80.80	0.81	0.268	1.43	0.188	1.02	1.00	0.243	No
505	10.10	180.05	99.08	80.97	0.81	0.268	1.43	0.187	1.02	1.00	0.242	No
506	10.12	180.41	99.28	81.13	0.80	0.268	1.43	0.187	1.02	1.00	0.242	No
507	10.14	180.77	99.47	81.30	0.80	0.267	1.43	0.187	1.02	1.00	0.242	No
508	10.16	181.13	99.67	81.47	0.80	0.267	1.43	0.187	1.02	1.00	0.242	No
509	10.18	181.50	99.87	81.63	0.80	0.267	1.43	0.187	1.02	1.00	0.242	No
510	10.20	181.86	100.06	81.80	0.80	0.267	1.43	0.187	1.02	1.00	0.242	No
511	10.22	182.23	100.26	81.97	0.80	0.267	1.43	0.187	1.02	1.00	0.242	No
512	10.24	182.59	100.45	82.14	0.80	0.267	1.43	0.187	1.02	1.00	0.242	No
513	10.26	182.95	100.65	82.30	0.80	0.266	1.43	0.186	1.02	1.00	0.242	No
514	10.28	183.32	100.85	82.47	0.80	0.266	1.43	0.186	1.02	1.00	0.242	No
515	10.30	183.68	101.04	82.64	0.80	0.266	1.43	0.186	1.02	1.00	0.242	No
516	10.32	184.05	101.24	82.81	0.80	0.266	1.43	0.186	1.02	1.00	0.242	No
517	10.34	184.41	101.44	82.97	0.80	0.266	1.43	0.186	1.02	1.00	0.242	No
518	10.36	184.77	101.63	83.14	0.80	0.266	1.43	0.186	1.02	1.00	0.242	No
519	10.38	185.13	101.83	83.30	0.80	0.265	1.43	0.186	1.02	1.00	0.242	No
520	10.40	185.49	102.02	83.47	0.80	0.265	1.43	0.186	1.02	1.00	0.241	No
521	10.42	185.85	102.22	83.63	0.80	0.265	1.43	0.186	1.02	1.00	0.241	No
522	10.44	186.21	102.42	83.79	0.80	0.265	1.43	0.185	1.02	1.00	0.241	No
523	10.46	186.57	102.61	83.96	0.80	0.265	1.43	0.185	1.02	1.00	0.241	No
524	10.48	186.93	102.81	84.12	0.80	0.265	1.43	0.185	1.02	1.00	0.241	No
525	10.50	187.29	103.01	84.28	0.80	0.264	1.43	0.185	1.02	1.00	0.241	No
526	10.52	187.65	103.20	84.45	0.80	0.264	1.43	0.185	1.02	1.00	0.240	No
527	10.54	188.01	103.40	84.61	0.79	0.264	1.43	0.185	1.02	1.00	0.241	No
528	10.56	188.37	103.59	84.78	0.79	0.264	1.43	0.185	1.02	1.00	0.240	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
529	10.58	188.73	103.79	84.94	0.79	0.264	1.43	0.185	1.02	1.00	0.240	No
530	10.60	189.10	103.99	85.11	0.79	0.264	1.43	0.184	1.01	1.00	0.240	No
531	10.62	189.46	104.18	85.28	0.79	0.263	1.43	0.184	1.01	1.00	0.239	No
532	10.64	189.82	104.38	85.44	0.79	0.263	1.43	0.184	1.01	1.00	0.239	No
533	10.66	190.18	104.57	85.61	0.79	0.263	1.43	0.184	1.01	1.00	0.239	No
534	10.68	190.55	104.77	85.78	0.79	0.263	1.43	0.184	1.01	1.00	0.239	No
535	10.70	190.91	104.97	85.95	0.79	0.263	1.43	0.184	1.01	1.00	0.239	No
536	10.72	191.28	105.16	86.11	0.79	0.263	1.43	0.184	1.01	1.00	0.239	No
537	10.74	191.64	105.36	86.28	0.79	0.262	1.43	0.184	1.01	1.00	0.238	No
538	10.76	192.01	105.56	86.45	0.79	0.262	1.43	0.184	1.01	1.00	0.238	No
539	10.78	192.37	105.75	86.61	0.79	0.262	1.43	0.183	1.01	1.00	0.237	No
540	10.80	192.73	105.95	86.78	0.79	0.262	1.43	0.183	1.01	1.00	0.240	No
541	10.82	193.09	106.14	86.95	0.79	0.262	1.43	0.183	1.01	1.00	0.237	No
542	10.84	193.46	106.34	87.12	0.79	0.262	1.43	0.183	1.01	1.00	0.236	No
543	10.86	193.83	106.54	87.29	0.79	0.261	1.43	0.183	1.01	1.00	0.236	No
544	10.88	194.20	106.73	87.47	0.79	0.261	1.43	0.183	1.01	1.00	0.236	No
545	10.90	194.58	106.93	87.65	0.79	0.261	1.43	0.183	1.01	1.00	0.237	No
546	10.92	194.95	107.13	87.82	0.79	0.261	1.43	0.183	1.01	1.00	0.237	No
547	10.94	195.32	107.32	88.00	0.79	0.261	1.43	0.182	1.01	1.00	0.237	No
548	10.96	195.69	107.52	88.18	0.78	0.260	1.43	0.182	1.01	1.00	0.237	No
549	10.98	196.07	107.71	88.35	0.78	0.260	1.43	0.182	1.01	1.00	0.237	No
550	11.00	196.44	107.91	88.53	0.78	0.260	1.43	0.182	1.01	1.00	0.237	No
551	11.02	196.81	108.11	88.71	0.78	0.260	1.43	0.182	1.01	1.00	0.237	No
552	11.04	197.19	108.30	88.88	0.78	0.260	1.43	0.182	1.01	1.00	0.237	No
553	11.06	197.56	108.50	89.06	0.78	0.259	1.43	0.182	1.01	1.00	0.237	No
554	11.08	197.93	108.69	89.23	0.78	0.259	1.43	0.182	1.01	1.00	0.237	No
555	11.10	198.30	108.89	89.41	0.78	0.259	1.43	0.181	1.01	1.00	0.237	No
556	11.12	198.67	109.09	89.58	0.78	0.259	1.43	0.181	1.01	1.00	0.237	No
557	11.14	199.04	109.28	89.75	0.78	0.259	1.43	0.181	1.01	1.00	0.236	No
558	11.16	199.41	109.48	89.93	0.78	0.259	1.43	0.181	1.01	1.00	0.237	No
559	11.18	199.77	109.68	90.10	0.78	0.258	1.43	0.181	1.01	1.00	0.237	No
560	11.20	200.14	109.87	90.27	0.78	0.258	1.43	0.181	1.01	1.00	0.237	No
561	11.22	200.51	110.07	90.44	0.78	0.258	1.43	0.181	1.01	1.00	0.237	No
562	11.24	200.88	110.26	90.61	0.78	0.258	1.43	0.181	1.01	1.00	0.236	No
563	11.26	201.24	110.46	90.78	0.78	0.258	1.43	0.180	1.01	1.00	0.236	No
564	11.28	201.61	110.66	90.95	0.78	0.258	1.43	0.180	1.01	1.00	0.236	No
565	11.30	201.97	110.85	91.12	0.78	0.257	1.43	0.180	1.01	1.00	0.236	No
566	11.32	202.33	111.05	91.28	0.78	0.257	1.43	0.180	1.01	1.00	0.236	No
567	11.34	202.70	111.25	91.45	0.78	0.257	1.43	0.180	1.01	1.00	0.235	No
568	11.36	203.06	111.44	91.62	0.78	0.257	1.43	0.180	1.01	1.00	0.235	No
569	11.38	203.42	111.64	91.79	0.77	0.257	1.43	0.180	1.01	1.00	0.235	No
570	11.40	203.79	111.83	91.95	0.77	0.257	1.43	0.180	1.01	1.00	0.235	No
571	11.42	204.15	112.03	92.12	0.77	0.256	1.43	0.179	1.01	1.00	0.235	No
572	11.44	204.52	112.23	92.29	0.77	0.256	1.43	0.179	1.01	1.00	0.235	No
573	11.46	204.88	112.42	92.46	0.77	0.256	1.43	0.179	1.01	1.00	0.235	No
574	11.48	205.24	112.62	92.63	0.77	0.256	1.43	0.179	1.01	1.00	0.235	No
575	11.50	205.61	112.82	92.79	0.77	0.256	1.43	0.179	1.01	1.00	0.235	No
576	11.52	205.97	113.01	92.96	0.77	0.256	1.43	0.179	1.01	1.00	0.235	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
577	11.54	206.33	113.21	93.12	0.77	0.255	1.43	0.179	1.01	1.00	0.234	No
578	11.56	206.69	113.40	93.29	0.77	0.255	1.43	0.179	1.01	1.00	0.234	No
579	11.58	207.05	113.60	93.45	0.77	0.255	1.43	0.179	1.01	1.00	0.233	No
580	11.60	207.41	113.80	93.62	0.77	0.255	1.43	0.178	1.01	1.00	0.233	No
581	11.62	207.77	113.99	93.78	0.77	0.255	1.43	0.178	1.01	1.00	0.233	No
582	11.64	208.13	114.19	93.95	0.77	0.255	1.43	0.178	1.01	1.00	0.233	No
583	11.66	208.50	114.38	94.11	0.77	0.254	1.43	0.178	1.01	1.00	0.233	No
584	11.68	208.86	114.58	94.28	0.77	0.254	1.43	0.178	1.01	1.00	0.233	No
585	11.70	209.22	114.78	94.44	0.77	0.254	1.43	0.178	1.01	1.00	0.233	No
586	11.72	209.58	114.97	94.61	0.77	0.254	1.43	0.178	1.01	1.00	0.233	No
587	11.74	209.94	115.17	94.78	0.77	0.254	1.43	0.178	1.01	1.00	0.233	No
588	11.76	210.31	115.37	94.94	0.77	0.254	1.43	0.178	1.01	1.00	0.233	No
589	11.78	210.67	115.56	95.11	0.77	0.253	1.43	0.177	1.01	1.00	0.233	No
590	11.80	211.03	115.76	95.27	0.76	0.253	1.43	0.177	1.01	1.00	0.233	No
591	11.82	211.39	115.95	95.44	0.76	0.253	1.43	0.177	1.01	1.00	0.233	No
592	11.84	211.75	116.15	95.60	0.76	0.253	1.43	0.177	1.00	1.00	0.233	No
593	11.86	212.11	116.35	95.77	0.76	0.253	1.43	0.177	1.00	1.00	0.233	No
594	11.88	212.47	116.54	95.93	0.76	0.253	1.43	0.177	1.00	1.00	0.233	No
595	11.90	212.83	116.74	96.09	0.76	0.252	1.43	0.177	1.00	1.00	0.232	No
596	11.92	213.19	116.94	96.25	0.76	0.252	1.43	0.177	1.00	1.00	0.232	No
597	11.94	213.55	117.13	96.42	0.76	0.252	1.43	0.176	1.00	1.00	0.232	No
598	11.96	213.90	117.33	96.58	0.76	0.252	1.43	0.176	1.00	1.00	0.232	No
599	11.98	214.26	117.52	96.74	0.76	0.252	1.43	0.176	1.00	1.00	0.232	No
600	12.00	214.62	117.72	96.90	0.76	0.252	1.43	0.176	1.00	1.00	0.232	No
601	12.02	214.97	117.92	97.06	0.76	0.252	1.43	0.176	1.00	1.00	0.232	No
602	12.04	215.33	118.11	97.22	0.76	0.251	1.43	0.176	1.00	1.00	0.233	No
603	12.06	215.69	118.31	97.38	0.76	0.251	1.43	0.176	1.00	1.00	0.233	No
604	12.08	216.04	118.50	97.54	0.76	0.251	1.43	0.176	1.00	1.00	0.233	No
605	12.10	216.40	118.70	97.70	0.76	0.251	1.43	0.176	1.00	1.00	0.233	No
606	12.13	216.93	119.00	97.94	0.76	0.251	1.43	0.175	1.00	1.00	0.233	No
607	12.14	217.11	119.09	98.02	0.76	0.251	1.43	0.175	1.00	1.00	0.233	No
608	12.17	217.64	119.39	98.25	0.76	0.250	1.43	0.175	1.00	1.00	0.233	No
609	12.18	217.82	119.49	98.33	0.76	0.250	1.43	0.175	1.00	1.00	0.233	No
610	12.20	218.17	119.68	98.49	0.76	0.250	1.43	0.175	1.00	1.00	0.233	No
611	12.22	218.52	119.88	98.64	0.75	0.250	1.43	0.175	1.00	1.00	0.233	No
612	12.24	218.87	120.07	98.79	0.75	0.250	1.43	0.175	1.00	1.00	0.232	No
613	12.26	219.22	120.27	98.95	0.75	0.250	1.43	0.175	1.00	1.00	0.232	No
614	12.29	219.74	120.56	99.17	0.75	0.249	1.43	0.175	1.00	1.00	0.232	No
615	12.30	219.91	120.66	99.25	0.75	0.249	1.43	0.175	1.00	1.00	0.232	No
616	12.32	220.26	120.86	99.40	0.75	0.249	1.43	0.174	1.00	1.00	0.232	No
617	12.34	220.61	121.06	99.55	0.75	0.249	1.43	0.174	1.00	1.00	0.232	No
618	12.36	220.95	121.25	99.70	0.75	0.249	1.43	0.174	1.00	1.00	0.231	No
619	12.38	221.30	121.45	99.85	0.75	0.249	1.43	0.174	1.00	1.00	0.231	No
620	12.40	221.64	121.64	100.00	0.75	0.249	1.43	0.174	1.00	1.00	0.231	No
621	12.42	221.99	121.84	100.15	0.75	0.249	1.43	0.174	1.00	1.00	0.231	No
622	12.44	222.33	122.04	100.29	0.75	0.248	1.43	0.174	1.00	1.00	0.231	No
623	12.46	222.67	122.23	100.44	0.75	0.248	1.43	0.174	1.00	1.00	0.231	No
624	12.48	223.01	122.43	100.58	0.75	0.248	1.43	0.174	1.00	1.00	0.231	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
625	12.50	223.35	122.63	100.73	0.75	0.248	1.43	0.174	1.00	1.00	0.231	No
626	12.52	223.69	122.82	100.87	0.75	0.248	1.43	0.174	1.00	1.00	0.231	No
627	12.54	224.03	123.02	101.01	0.75	0.248	1.43	0.173	1.00	1.00	0.231	No
628	12.56	224.37	123.21	101.15	0.75	0.248	1.43	0.173	1.00	1.00	0.231	No
629	12.58	224.70	123.41	101.29	0.75	0.248	1.43	0.173	1.00	1.00	0.231	No
630	12.60	225.03	123.61	101.43	0.75	0.247	1.43	0.173	1.00	1.00	0.231	No
631	12.62	225.36	123.80	101.56	0.75	0.247	1.43	0.173	1.00	1.00	0.231	No
632	12.64	225.69	124.00	101.69	0.74	0.247	1.43	0.173	1.00	1.00	0.231	No
633	12.66	226.02	124.19	101.82	0.74	0.247	1.43	0.173	1.00	1.00	0.231	No
634	12.68	226.34	124.39	101.95	0.74	0.247	1.43	0.173	1.00	1.00	0.231	No
635	12.70	226.67	124.59	102.08	0.74	0.247	1.43	0.173	1.00	1.00	0.231	No
636	12.72	226.99	124.78	102.21	0.74	0.247	1.43	0.173	1.00	1.00	0.231	No
637	12.74	227.31	124.98	102.33	0.74	0.247	1.43	0.173	1.00	1.00	0.231	No
638	12.76	227.63	125.18	102.45	0.74	0.247	1.43	0.173	1.00	1.00	0.230	No
639	12.78	227.95	125.37	102.58	0.74	0.246	1.43	0.172	1.00	1.00	0.230	No
640	12.80	228.28	125.57	102.71	0.74	0.246	1.43	0.172	1.00	1.00	0.230	No
641	12.82	228.60	125.76	102.84	0.74	0.246	1.43	0.172	1.00	1.00	0.230	No
642	12.84	228.93	125.96	102.97	0.74	0.246	1.43	0.172	1.00	1.00	0.230	No
643	12.86	229.26	126.16	103.11	0.74	0.246	1.43	0.172	1.00	1.00	0.229	No
644	12.88	229.60	126.35	103.24	0.74	0.246	1.43	0.172	1.00	1.00	0.229	No
645	12.90	229.93	126.55	103.38	0.74	0.246	1.43	0.172	1.00	1.00	0.229	No
646	12.92	230.26	126.75	103.52	0.74	0.246	1.43	0.172	1.00	1.00	0.229	No
647	12.94	230.60	126.94	103.66	0.74	0.245	1.43	0.172	1.00	1.00	0.229	No
648	12.96	230.94	127.14	103.80	0.74	0.245	1.43	0.172	1.00	1.00	0.229	No
649	12.98	231.28	127.33	103.94	0.74	0.245	1.43	0.172	1.00	1.00	0.229	No
650	13.00	231.62	127.53	104.09	0.74	0.245	1.43	0.172	1.00	1.00	0.229	No
651	13.02	231.95	127.73	104.23	0.74	0.245	1.43	0.171	1.00	1.00	0.229	No
652	13.04	232.29	127.92	104.37	0.74	0.245	1.43	0.171	1.00	1.00	0.229	No
653	13.06	232.63	128.12	104.51	0.74	0.245	1.43	0.171	1.00	1.00	0.229	No
654	13.08	232.97	128.31	104.66	0.73	0.244	1.43	0.171	1.00	1.00	0.228	No
655	13.10	233.31	128.51	104.80	0.73	0.244	1.43	0.171	1.00	1.00	0.229	No
656	13.12	233.65	128.71	104.94	0.73	0.244	1.43	0.171	1.00	1.00	0.229	No
657	13.14	233.99	128.90	105.09	0.73	0.244	1.43	0.171	1.00	1.00	0.229	No
658	13.16	234.33	129.10	105.23	0.73	0.244	1.43	0.171	1.00	1.00	0.228	No
659	13.19	234.83	129.39	105.44	0.73	0.244	1.43	0.171	1.00	1.00	0.228	No
660	13.20	235.00	129.49	105.51	0.73	0.244	1.43	0.171	1.00	1.00	0.228	No
661	13.22	235.33	129.69	105.65	0.73	0.244	1.43	0.170	1.00	1.00	0.228	No
662	13.24	235.66	129.88	105.78	0.73	0.243	1.43	0.170	1.00	1.00	0.228	No
663	13.26	235.99	130.08	105.91	0.73	0.243	1.43	0.170	1.00	1.00	0.228	No
664	13.28	236.32	130.28	106.04	0.73	0.243	1.43	0.170	1.00	1.00	0.228	No
665	13.30	236.64	130.47	106.17	0.73	0.243	1.43	0.170	1.00	1.00	0.228	No
666	13.32	236.96	130.67	106.29	0.73	0.243	1.43	0.170	1.00	1.00	0.228	No
667	13.34	237.28	130.87	106.42	0.73	0.243	1.43	0.170	1.00	1.00	0.228	No
668	13.36	237.60	131.06	106.54	0.73	0.243	1.43	0.170	1.00	1.00	0.227	No
669	13.38	237.92	131.26	106.66	0.73	0.243	1.43	0.170	1.00	1.00	0.227	No
670	13.40	238.24	131.45	106.79	0.73	0.243	1.43	0.170	1.00	1.00	0.227	No
671	13.42	238.57	131.65	106.92	0.73	0.242	1.43	0.170	1.00	1.00	0.227	No
672	13.44	238.90	131.85	107.05	0.73	0.242	1.43	0.170	1.00	1.00	0.226	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
673	13.46	239.23	132.04	107.19	0.73	0.242	1.43	0.170	1.00	1.00	0.226	No
674	13.48	239.57	132.24	107.33	0.73	0.242	1.43	0.169	1.00	1.00	0.226	No
675	13.50	239.91	132.44	107.47	0.72	0.242	1.43	0.169	1.00	1.00	0.226	No
676	13.52	240.25	132.63	107.62	0.72	0.242	1.43	0.169	1.00	1.00	0.226	No
677	13.54	240.60	132.83	107.77	0.72	0.242	1.43	0.169	1.00	1.00	0.226	No
678	13.56	240.94	133.02	107.92	0.72	0.242	1.43	0.169	0.99	1.00	0.226	No
679	13.58	241.29	133.22	108.07	0.72	0.241	1.43	0.169	0.99	1.00	0.226	No
680	13.60	241.63	133.42	108.22	0.72	0.241	1.43	0.169	0.99	1.00	0.226	No
681	13.62	241.98	133.61	108.36	0.72	0.241	1.43	0.169	0.99	1.00	0.226	No
682	13.64	242.32	133.81	108.51	0.72	0.241	1.43	0.169	0.99	1.00	0.225	No
683	13.66	242.66	134.00	108.66	0.72	0.241	1.43	0.169	0.99	1.00	0.225	No
684	13.68	243.00	134.20	108.80	0.72	0.241	1.43	0.168	0.99	1.00	0.225	No
685	13.70	243.35	134.40	108.95	0.72	0.241	1.43	0.168	0.99	1.00	0.225	No
686	13.72	243.69	134.59	109.10	0.72	0.240	1.43	0.168	0.99	1.00	0.225	No
687	13.74	244.04	134.79	109.25	0.72	0.240	1.43	0.168	0.99	1.00	0.225	No
688	13.76	244.39	134.99	109.40	0.72	0.240	1.43	0.168	0.99	1.00	0.225	No
689	13.78	244.74	135.18	109.56	0.72	0.240	1.43	0.168	0.99	1.00	0.225	No
690	13.80	245.09	135.38	109.71	0.72	0.240	1.43	0.168	0.99	1.00	0.224	No
691	13.82	245.44	135.57	109.87	0.72	0.240	1.43	0.168	0.99	1.00	0.224	No
692	13.84	245.80	135.77	110.03	0.72	0.239	1.43	0.168	0.99	1.00	0.224	No
693	13.86	246.15	135.97	110.18	0.72	0.239	1.43	0.168	0.99	1.00	0.224	No
694	13.88	246.50	136.16	110.34	0.72	0.239	1.43	0.167	0.99	1.00	0.224	No
695	13.90	246.86	136.36	110.50	0.72	0.239	1.43	0.167	0.99	1.00	0.224	No
696	13.92	247.21	136.56	110.66	0.72	0.239	1.43	0.167	0.99	1.00	0.223	No
697	13.94	247.57	136.75	110.81	0.71	0.239	1.43	0.167	0.99	1.00	0.223	No
698	13.96	247.92	136.95	110.97	0.71	0.239	1.43	0.167	0.99	1.00	0.223	No
699	13.98	248.27	137.14	111.13	0.71	0.238	1.43	0.167	0.99	1.00	0.223	No
700	14.00	248.62	137.34	111.28	0.71	0.238	1.43	0.167	0.99	1.00	0.223	No
701	14.02	248.98	137.54	111.44	0.71	0.238	1.43	0.167	0.99	1.00	0.223	No
702	14.04	249.33	137.73	111.59	0.71	0.238	1.43	0.167	0.99	1.00	0.222	No
703	14.06	249.68	137.93	111.75	0.71	0.238	1.43	0.166	0.99	1.00	0.222	No
704	14.08	250.03	138.12	111.91	0.71	0.238	1.43	0.166	0.99	1.00	0.222	No
705	14.10	250.38	138.32	112.06	0.71	0.238	1.43	0.166	0.99	1.00	0.222	No
706	14.12	250.74	138.52	112.22	0.71	0.237	1.43	0.166	0.99	1.00	0.222	No
707	14.14	251.10	138.71	112.38	0.71	0.237	1.43	0.166	0.99	1.00	0.222	No
708	14.16	251.46	138.91	112.55	0.71	0.237	1.43	0.166	0.99	1.00	0.221	No
709	14.18	251.82	139.11	112.71	0.71	0.237	1.43	0.166	0.99	1.00	0.221	No
710	14.20	252.18	139.30	112.87	0.71	0.237	1.43	0.166	0.99	1.00	0.221	No
711	14.22	252.54	139.50	113.04	0.71	0.237	1.43	0.166	0.99	1.00	0.221	No
712	14.24	252.90	139.69	113.21	0.71	0.236	1.43	0.166	0.99	1.00	0.221	No
713	14.26	253.26	139.89	113.37	0.71	0.236	1.43	0.165	0.99	1.00	0.221	No
714	14.28	253.63	140.09	113.54	0.71	0.236	1.43	0.165	0.99	1.00	0.221	No
715	14.30	253.99	140.28	113.70	0.71	0.236	1.43	0.165	0.99	1.00	0.221	No
716	14.32	254.35	140.48	113.87	0.71	0.236	1.43	0.165	0.99	1.00	0.220	No
717	14.34	254.71	140.68	114.04	0.71	0.236	1.43	0.165	0.99	1.00	0.220	No
718	14.36	255.07	140.87	114.20	0.71	0.236	1.43	0.165	0.99	1.00	0.220	No
719	14.38	255.43	141.07	114.37	0.70	0.235	1.43	0.165	0.99	1.00	0.220	No
720	14.40	255.79	141.26	114.53	0.70	0.235	1.43	0.165	0.99	1.00	0.220	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
721	14.42	256.16	141.46	114.70	0.70	0.235	1.43	0.165	0.99	1.00	0.220	No
722	14.44	256.52	141.66	114.86	0.70	0.235	1.43	0.164	0.99	1.00	0.220	No
723	14.46	256.88	141.85	115.03	0.70	0.235	1.43	0.164	0.99	1.00	0.220	No
724	14.48	257.24	142.05	115.19	0.70	0.235	1.43	0.164	0.99	1.00	0.220	No
725	14.50	257.60	142.25	115.35	0.70	0.234	1.43	0.164	0.99	1.00	0.220	No
726	14.52	257.96	142.44	115.52	0.70	0.234	1.43	0.164	0.99	1.00	0.219	No
727	14.54	258.32	142.64	115.68	0.70	0.234	1.43	0.164	0.99	1.00	0.219	No
728	14.56	258.68	142.83	115.85	0.70	0.234	1.43	0.164	0.99	1.00	0.219	No
729	14.58	259.04	143.03	116.01	0.70	0.234	1.43	0.164	0.99	1.00	0.219	No
730	14.60	259.40	143.23	116.18	0.70	0.234	1.43	0.164	0.99	1.00	0.219	No
731	14.62	259.76	143.42	116.34	0.70	0.233	1.43	0.163	0.99	1.00	0.219	No
732	14.64	260.12	143.62	116.50	0.70	0.233	1.43	0.163	0.99	1.00	0.219	No
733	14.66	260.48	143.81	116.67	0.70	0.233	1.43	0.163	0.99	1.00	0.219	No
734	14.68	260.84	144.01	116.83	0.70	0.233	1.43	0.163	0.99	1.00	0.218	No
735	14.70	261.20	144.21	117.00	0.70	0.233	1.43	0.163	0.99	1.00	0.218	No
736	14.72	261.56	144.40	117.16	0.70	0.233	1.43	0.163	0.99	1.00	0.218	No
737	14.74	261.93	144.60	117.33	0.70	0.233	1.43	0.163	0.99	1.00	0.218	No
738	14.76	262.28	144.80	117.48	0.70	0.232	1.43	0.163	0.99	1.00	0.218	No
739	14.78	262.63	144.99	117.64	0.70	0.232	1.43	0.163	0.99	1.00	0.220	No
740	14.80	262.98	145.19	117.80	0.70	0.232	1.43	0.162	0.99	1.00	0.217	No
741	14.82	263.34	145.38	117.96	0.69	0.232	1.43	0.162	0.99	1.00	0.217	No
742	14.84	263.70	145.58	118.12	0.69	0.232	1.43	0.162	0.99	1.00	0.217	No
743	14.86	264.06	145.78	118.29	0.69	0.232	1.43	0.162	0.99	1.00	0.216	No
744	14.88	264.42	145.97	118.45	0.69	0.231	1.43	0.162	0.99	1.00	0.216	No
745	14.90	264.78	146.17	118.61	0.69	0.231	1.43	0.162	0.99	1.00	0.216	No
746	14.92	265.14	146.37	118.78	0.69	0.231	1.43	0.162	0.99	1.00	0.215	No
747	14.94	265.51	146.56	118.95	0.69	0.231	1.43	0.162	0.99	1.00	0.215	No
748	14.96	265.87	146.76	119.12	0.69	0.231	1.43	0.162	0.99	1.00	0.214	No
749	14.98	266.24	146.95	119.29	0.69	0.231	1.43	0.161	0.99	1.00	0.214	No
750	15.00	266.61	147.15	119.46	0.69	0.231	1.43	0.161	0.99	1.00	0.214	No
751	15.02	266.98	147.35	119.63	0.69	0.230	1.43	0.161	0.99	1.00	0.215	No
752	15.04	267.35	147.54	119.81	0.69	0.230	1.43	0.161	0.99	1.00	0.215	No
753	15.06	267.72	147.74	119.98	0.69	0.230	1.43	0.161	0.99	1.00	0.215	No
754	15.08	268.10	147.93	120.16	0.69	0.230	1.43	0.161	0.99	1.00	0.215	No
755	15.10	268.47	148.13	120.34	0.69	0.230	1.43	0.161	0.99	1.00	0.215	No
756	15.12	268.84	148.33	120.52	0.69	0.230	1.43	0.161	0.99	1.00	0.215	No
757	15.14	269.22	148.52	120.69	0.69	0.229	1.43	0.161	0.99	1.00	0.215	No
758	15.16	269.59	148.72	120.87	0.69	0.229	1.43	0.160	0.99	1.00	0.215	No
759	15.18	269.96	148.92	121.05	0.69	0.229	1.43	0.160	0.99	1.00	0.215	No
760	15.20	270.33	149.11	121.22	0.69	0.229	1.43	0.160	0.98	1.00	0.215	No
761	15.22	270.70	149.31	121.40	0.69	0.229	1.43	0.160	0.98	1.00	0.215	No
762	15.24	271.07	149.50	121.57	0.69	0.229	1.43	0.160	0.98	1.00	0.215	No
763	15.26	271.44	149.70	121.74	0.69	0.228	1.43	0.160	0.98	1.00	0.214	No
764	15.28	271.80	149.90	121.91	0.68	0.228	1.43	0.160	0.98	1.00	0.214	No
765	15.30	272.17	150.09	122.07	0.68	0.228	1.43	0.160	0.98	1.00	0.214	No
766	15.32	272.53	150.29	122.24	0.68	0.228	1.43	0.160	0.98	1.00	0.214	No
767	15.34	272.89	150.49	122.41	0.68	0.228	1.43	0.159	0.98	1.00	0.214	No
768	15.36	273.26	150.68	122.58	0.68	0.228	1.43	0.159	0.98	1.00	0.214	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
769	15.38	273.62	150.88	122.74	0.68	0.227	1.43	0.159	0.98	1.00	0.214	No
770	15.40	273.99	151.07	122.91	0.68	0.227	1.43	0.159	0.98	1.00	0.214	No
771	15.42	274.35	151.27	123.08	0.68	0.227	1.43	0.159	0.98	1.00	0.214	No
772	15.44	274.71	151.47	123.24	0.68	0.227	1.43	0.159	0.98	1.00	0.214	No
773	15.46	275.07	151.66	123.41	0.68	0.227	1.43	0.159	0.98	1.00	0.214	No
774	15.48	275.43	151.86	123.57	0.68	0.227	1.43	0.159	0.98	1.00	0.214	No
775	15.50	275.79	152.06	123.73	0.68	0.227	1.43	0.159	0.98	1.00	0.214	No
776	15.52	276.14	152.25	123.89	0.68	0.226	1.43	0.158	0.98	1.00	0.214	No
777	15.54	276.49	152.45	124.05	0.68	0.226	1.43	0.158	0.98	1.00	0.214	No
778	15.56	276.85	152.64	124.20	0.68	0.226	1.43	0.158	0.98	1.00	0.214	No
779	15.58	277.20	152.84	124.36	0.68	0.226	1.43	0.158	0.98	1.00	0.214	No
780	15.60	277.54	153.04	124.51	0.68	0.226	1.43	0.158	0.98	1.00	0.214	No
781	15.62	277.89	153.23	124.66	0.68	0.226	1.43	0.158	0.98	1.00	0.214	No
782	15.64	278.23	153.43	124.80	0.68	0.226	1.43	0.158	0.98	1.00	0.214	No
783	15.66	278.57	153.62	124.95	0.68	0.225	1.43	0.158	0.98	1.00	0.214	No
784	15.68	278.91	153.82	125.09	0.68	0.225	1.43	0.158	0.98	1.00	0.213	No
785	15.70	279.25	154.02	125.23	0.68	0.225	1.43	0.158	0.98	1.00	0.213	No
786	15.72	279.59	154.21	125.37	0.68	0.225	1.43	0.158	0.98	1.00	0.213	No
787	15.74	279.92	154.41	125.52	0.67	0.225	1.43	0.157	0.98	1.00	0.213	No
788	15.76	280.26	154.61	125.66	0.67	0.225	1.43	0.157	0.98	1.00	0.212	No
789	15.78	280.60	154.80	125.80	0.67	0.225	1.43	0.157	0.98	1.00	0.213	No
790	15.80	280.94	155.00	125.94	0.67	0.225	1.43	0.157	0.98	1.00	0.212	No
791	15.82	281.29	155.19	126.09	0.67	0.224	1.43	0.157	0.98	1.00	0.212	No
792	15.85	281.81	155.49	126.32	0.67	0.224	1.43	0.157	0.98	1.00	0.212	No
793	15.86	281.99	155.59	126.40	0.67	0.224	1.43	0.157	0.98	1.00	0.212	No
794	15.88	282.34	155.78	126.56	0.67	0.224	1.43	0.157	0.98	1.00	0.212	No
795	15.90	282.70	155.98	126.72	0.67	0.224	1.43	0.157	0.98	1.00	0.212	No
796	15.92	283.05	156.18	126.87	0.67	0.224	1.43	0.157	0.98	1.00	0.212	No
797	15.94	283.40	156.37	127.03	0.67	0.224	1.43	0.157	0.98	1.00	0.212	No
798	15.96	283.75	156.57	127.18	0.67	0.223	1.43	0.156	0.98	1.00	0.212	No
799	15.98	284.09	156.76	127.33	0.67	0.223	1.43	0.156	0.98	1.00	0.212	No
800	16.00	284.44	156.96	127.48	0.67	0.223	1.43	0.156	0.98	1.00	0.212	No
801	16.02	284.78	157.16	127.63	0.67	0.223	1.43	0.156	0.98	1.00	0.211	No
802	16.04	285.13	157.35	127.78	0.67	0.223	1.43	0.156	0.98	1.00	0.211	No
803	16.06	285.47	157.55	127.93	0.67	0.223	1.43	0.156	0.98	1.00	0.211	No
804	16.08	285.82	157.74	128.08	0.67	0.223	1.43	0.156	0.98	1.00	0.211	No
805	16.10	286.17	157.94	128.23	0.67	0.223	1.43	0.156	0.98	1.00	0.211	No
806	16.12	286.52	158.14	128.38	0.67	0.222	1.43	0.156	0.98	1.00	0.211	No
807	16.14	286.87	158.33	128.53	0.67	0.222	1.43	0.156	0.98	1.00	0.211	No
808	16.16	287.22	158.53	128.69	0.67	0.222	1.43	0.155	0.98	1.00	0.211	No
809	16.18	287.57	158.73	128.85	0.67	0.222	1.43	0.155	0.98	1.00	0.211	No
810	16.20	287.92	158.92	129.00	0.66	0.222	1.43	0.155	0.98	1.00	0.211	No
811	16.22	288.28	159.12	129.16	0.66	0.222	1.43	0.155	0.98	1.00	0.211	No
812	16.24	288.62	159.31	129.31	0.66	0.222	1.43	0.155	0.98	1.00	0.210	No
813	16.26	288.97	159.51	129.46	0.66	0.221	1.43	0.155	0.98	1.00	0.210	No
814	16.28	289.31	159.71	129.61	0.66	0.221	1.43	0.155	0.98	1.00	0.210	No
815	16.30	289.65	159.90	129.75	0.66	0.221	1.43	0.155	0.98	1.00	0.210	No
816	16.32	289.99	160.10	129.89	0.66	0.221	1.43	0.155	0.98	1.00	0.210	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
817	16.34	290.33	160.30	130.03	0.66	0.221	1.43	0.155	0.98	1.00	0.209	No
818	16.36	290.67	160.49	130.18	0.66	0.221	1.43	0.155	0.98	1.00	0.209	No
819	16.38	291.01	160.69	130.32	0.66	0.221	1.43	0.154	0.98	1.00	0.209	No
820	16.40	291.35	160.88	130.47	0.66	0.221	1.43	0.154	0.98	1.00	0.209	No
821	16.42	291.70	161.08	130.62	0.66	0.220	1.43	0.154	0.98	1.00	0.209	No
822	16.44	292.04	161.28	130.77	0.66	0.220	1.43	0.154	0.98	1.00	0.209	No
823	16.46	292.39	161.47	130.92	0.66	0.220	1.43	0.154	0.98	1.00	0.209	No
824	16.48	292.74	161.67	131.07	0.66	0.220	1.43	0.154	0.98	1.00	0.209	No
825	16.50	293.09	161.87	131.23	0.66	0.220	1.43	0.154	0.98	1.00	0.209	No
826	16.52	293.44	162.06	131.38	0.66	0.220	1.43	0.154	0.98	1.00	0.209	No
827	16.54	293.79	162.26	131.53	0.66	0.220	1.43	0.154	0.98	1.00	0.209	No
828	16.56	294.13	162.45	131.68	0.66	0.219	1.43	0.154	0.98	1.00	0.209	No
829	16.58	294.48	162.65	131.83	0.66	0.219	1.43	0.154	0.98	1.00	0.209	No
830	16.60	294.82	162.85	131.97	0.66	0.219	1.43	0.153	0.98	1.00	0.209	No
831	16.62	295.16	163.04	132.12	0.66	0.219	1.43	0.153	0.98	1.00	0.208	No
832	16.64	295.50	163.24	132.26	0.66	0.219	1.43	0.153	0.98	1.00	0.208	No
833	16.66	295.84	163.43	132.40	0.66	0.219	1.43	0.153	0.98	1.00	0.208	No
834	16.68	296.17	163.63	132.54	0.65	0.219	1.43	0.153	0.98	1.00	0.208	No
835	16.70	296.51	163.83	132.68	0.65	0.219	1.43	0.153	0.98	1.00	0.208	No
836	16.72	296.84	164.02	132.82	0.65	0.218	1.43	0.153	0.98	1.00	0.208	No
837	16.74	297.18	164.22	132.96	0.65	0.218	1.43	0.153	0.98	1.00	0.208	No
838	16.76	297.52	164.42	133.10	0.65	0.218	1.43	0.153	0.98	1.00	0.207	No
839	16.79	298.03	164.71	133.32	0.65	0.218	1.43	0.153	0.98	1.00	0.207	No
840	16.80	298.20	164.81	133.39	0.65	0.218	1.43	0.153	0.98	1.00	0.207	No
841	16.82	298.55	165.00	133.54	0.65	0.218	1.43	0.152	0.98	1.00	0.207	No
842	16.84	298.89	165.20	133.69	0.65	0.218	1.43	0.152	0.98	1.00	0.207	No
843	16.86	299.24	165.40	133.84	0.65	0.218	1.43	0.152	0.98	1.00	0.207	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (m)
σ_v: Total overburden pressure at test point (kPa)
u_0: Water pressure at test point (kPa)
σ_v': Effective overburden pressure based on GWT during earthquake (kPa)
r_d: Nonlinear shear mass factor
CSR: Cyclic Stress Ratio
MSF: Magnitude Scaling Factor
CSR_{eq}: CSR adjusted for M=7.5
K_σ: Effective overburden stress factor
CSR^*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1	0.02	0.98	62.05	2.49	0.57	1.70	15.93	53.66	69.59	4.000	Yes	No	2.00
2	0.04	1.09	70.10	2.59	0.56	1.70	17.69	55.79	73.47	4.000	Yes	No	2.00
3	0.06	1.16	75.21	2.65	0.55	1.70	19.69	0.00	19.69	4.000	Yes	Yes	2.00
4	0.08	1.23	81.39	2.73	0.55	1.70	20.99	0.00	20.99	4.000	Yes	Yes	2.00
5	0.10	1.27	86.92	2.80	0.54	1.70	21.23	0.00	21.23	4.000	Yes	Yes	2.00
6	0.12	1.29	91.67	2.86	0.54	1.70	21.71	0.00	21.71	4.000	Yes	Yes	2.00
7	0.14	1.30	95.27	2.90	0.54	1.70	21.95	0.00	21.95	4.000	Yes	Yes	2.00
8	0.17	1.29	98.98	2.95	0.54	1.70	21.88	0.00	21.88	4.000	Yes	Yes	2.00
9	0.18	1.28	100.00	2.99	0.54	1.70	21.27	0.00	21.27	4.000	Yes	Yes	2.00
10	0.20	1.26	100.00	3.02	0.54	1.70	21.13	0.00	21.13	4.000	No	Yes	2.00
11	0.23	1.24	100.00	3.05	0.54	1.70	20.84	0.00	20.84	4.000	No	Yes	2.00
12	0.24	1.23	100.00	3.07	0.54	1.70	20.59	0.00	20.59	4.000	No	Yes	2.00
13	0.26	1.22	100.00	3.08	0.54	1.70	20.59	0.00	20.59	4.000	No	Yes	2.00
14	0.29	1.21	100.00	3.09	0.55	1.70	20.03	0.00	20.03	4.000	No	Yes	2.00
15	0.30	1.20	100.00	3.08	0.55	1.70	20.06	0.00	20.06	4.000	No	Yes	2.00
16	0.32	1.19	100.00	3.08	0.55	1.70	20.13	0.00	20.13	4.000	No	Yes	2.00
17	0.34	1.18	100.00	3.08	0.55	1.70	19.69	0.00	19.69	4.000	No	Yes	2.00
18	0.36	1.17	100.00	3.08	0.55	1.70	19.68	0.00	19.68	4.000	No	Yes	2.00
19	0.38	1.19	100.00	3.07	0.55	1.70	19.67	0.00	19.67	4.000	No	Yes	2.00
20	0.40	1.22	100.00	3.06	0.54	1.70	20.41	0.00	20.41	4.000	No	Yes	2.00
21	0.42	1.25	100.00	3.04	0.54	1.70	21.19	0.00	21.19	4.000	No	Yes	2.00
22	0.44	1.27	100.00	3.03	0.54	1.70	21.18	0.00	21.18	4.000	No	Yes	2.00
23	0.46	1.28	100.00	3.03	0.54	1.70	21.64	0.00	21.64	4.000	No	Yes	2.00
24	0.48	1.29	100.00	3.02	0.54	1.70	21.59	0.00	21.59	4.000	No	Yes	2.00
25	0.50	1.28	100.00	3.02	0.54	1.70	21.62	0.00	21.62	4.000	No	Yes	2.00
26	0.53	1.29	100.00	3.02	0.54	1.70	21.34	0.00	21.34	4.000	No	Yes	2.00
27	0.54	1.29	100.00	3.01	0.54	1.70	21.79	0.00	21.79	4.000	No	Yes	2.00
28	0.56	1.28	100.00	3.01	0.54	1.70	21.66	0.00	21.66	4.000	No	Yes	2.00
29	0.58	1.26	100.00	3.01	0.54	1.70	21.09	0.00	21.09	4.000	No	Yes	2.00
30	0.60	1.24	100.00	3.01	0.54	1.70	20.80	0.00	20.80	4.000	No	Yes	2.00
31	0.62	1.22	100.00	3.02	0.54	1.70	20.34	0.00	20.34	4.000	No	Yes	2.00
32	0.64	1.19	100.00	3.03	0.54	1.70	20.25	0.00	20.25	4.000	No	Yes	2.00
33	0.66	1.13	100.00	3.05	0.55	1.70	19.20	0.00	19.20	4.000	No	Yes	2.00
34	0.68	1.04	100.00	3.10	0.55	1.70	17.39	0.00	17.39	4.000	No	Yes	2.00
35	0.70	0.95	100.00	3.15	0.56	1.70	16.03	0.00	16.03	4.000	No	Yes	2.00
36	0.72	0.85	100.00	3.21	0.57	1.70	14.21	0.00	14.21	4.000	No	Yes	2.00
37	0.74	0.75	100.00	3.26	0.57	1.70	12.54	0.00	12.54	4.000	No	Yes	2.00
38	0.76	0.68	100.00	3.32	0.58	1.70	11.27	0.00	11.27	4.000	No	Yes	2.00
39	0.78	0.62	100.00	3.35	0.58	1.70	10.34	0.00	10.34	4.000	No	Yes	2.00
40	0.80	0.59	100.00	3.37	0.58	1.70	9.88	0.00	9.88	4.000	No	Yes	2.00
41	0.82	0.58	100.00	3.36	0.58	1.70	9.39	0.00	9.39	4.000	No	Yes	2.00
42	0.84	0.61	100.00	3.31	0.58	1.70	9.87	0.00	9.87	4.000	No	Yes	2.00
43	0.86	0.71	100.00	3.18	0.58	1.70	11.32	0.00	11.32	4.000	No	Yes	2.00
44	0.88	0.85	100.00	3.03	0.57	1.70	14.29	0.00	14.29	4.000	No	Yes	2.00
45	0.90	1.00	95.80	2.91	0.56	1.70	17.06	0.00	17.06	4.000	No	Yes	2.00
46	0.92	1.14	89.64	2.83	0.55	1.70	18.47	0.00	18.47	4.000	No	Yes	2.00
47	0.94	1.24	87.10	2.80	0.54	1.70	21.22	0.00	21.22	4.000	No	Yes	2.00
48	0.96	1.32	86.54	2.79	0.54	1.70	22.16	0.00	22.16	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
49	0.98	1.35	89.24	2.83	0.54	1.70	22.75	0.00	22.75	4.000	No	Yes	2.00
50	1.00	1.35	92.21	2.87	0.54	1.70	22.39	0.00	22.39	4.000	No	Yes	2.00
51	1.02	1.35	95.66	2.91	0.54	1.70	22.63	0.00	22.63	4.000	No	Yes	2.00
52	1.04	1.34	98.60	2.94	0.54	1.70	22.39	0.00	22.39	4.000	No	Yes	2.00
53	1.07	1.32	100.00	2.98	0.54	1.70	21.95	0.00	21.95	4.000	No	Yes	2.00
54	1.08	1.30	100.00	3.01	0.54	1.70	21.78	0.00	21.78	4.000	No	Yes	2.00
55	1.10	1.30	100.00	3.03	0.54	1.70	21.44	0.00	21.44	4.000	No	Yes	2.00
56	1.12	1.30	100.00	3.03	0.54	1.70	21.78	0.00	21.78	4.000	No	Yes	2.00
57	1.14	1.30	100.00	3.03	0.54	1.70	21.65	0.00	21.65	4.000	No	Yes	2.00
58	1.16	1.32	100.00	3.02	0.54	1.70	21.79	0.00	21.79	4.000	No	Yes	2.00
59	1.18	1.33	100.00	3.01	0.54	1.70	22.44	0.00	22.44	4.000	No	Yes	2.00
60	1.20	1.35	100.00	3.00	0.54	1.70	22.54	0.00	22.54	4.000	No	Yes	2.00
61	1.22	1.36	100.00	3.00	0.54	1.70	22.79	0.00	22.79	4.000	No	Yes	2.00
62	1.24	1.35	100.00	3.00	0.54	1.70	22.57	0.00	22.57	4.000	No	Yes	2.00
63	1.26	1.34	100.00	3.01	0.54	1.70	22.26	0.00	22.26	4.000	No	Yes	2.00
64	1.28	1.34	100.00	3.01	0.54	1.70	22.40	0.00	22.40	4.000	No	Yes	2.00
65	1.30	1.34	100.00	3.01	0.54	1.70	22.41	0.00	22.41	4.000	No	Yes	2.00
66	1.32	1.34	100.00	3.01	0.54	1.70	22.19	0.00	22.19	4.000	No	Yes	2.00
67	1.34	1.35	100.00	3.01	0.54	1.70	22.28	0.00	22.28	4.000	No	Yes	2.00
68	1.36	1.35	100.00	3.01	0.54	1.70	22.84	0.00	22.84	4.000	No	Yes	2.00
69	1.38	1.35	100.00	3.01	0.54	1.70	22.62	0.00	22.62	4.000	No	Yes	2.00
70	1.40	1.33	100.00	3.01	0.54	1.70	22.04	0.00	22.04	4.000	No	Yes	2.00
71	1.42	1.30	100.00	3.03	0.54	1.70	21.81	0.00	21.81	4.000	No	Yes	2.00
72	1.44	1.27	100.00	3.04	0.54	1.70	20.99	0.00	20.99	4.000	No	Yes	2.00
73	1.46	1.24	100.00	3.05	0.54	1.70	20.65	0.00	20.65	4.000	No	Yes	2.00
74	1.48	1.21	100.00	3.06	0.54	1.70	20.27	0.00	20.27	4.000	No	Yes	2.00
75	1.50	1.19	100.00	3.07	0.55	1.70	19.78	0.00	19.78	4.000	No	Yes	2.00
76	1.52	1.15	100.00	3.08	0.55	1.70	19.35	0.00	19.35	4.000	No	Yes	2.00
77	1.54	1.12	100.00	3.08	0.55	1.70	18.47	0.00	18.47	4.000	No	Yes	2.00
78	1.56	1.08	100.00	3.09	0.55	1.70	18.01	0.00	18.01	4.000	No	Yes	2.00
79	1.58	1.05	100.00	3.10	0.55	1.70	17.39	0.00	17.39	4.000	No	Yes	2.00
80	1.60	1.02	100.00	3.11	0.56	1.70	16.86	0.00	16.86	4.000	No	Yes	2.00
81	1.62	1.00	100.00	3.12	0.56	1.70	16.64	0.00	16.64	4.000	No	Yes	2.00
82	1.64	1.00	100.00	3.12	0.56	1.70	16.34	0.00	16.34	4.000	No	Yes	2.00
83	1.66	1.01	100.00	3.11	0.56	1.70	16.75	0.00	16.75	4.000	No	Yes	2.00
84	1.68	1.05	100.00	3.09	0.56	1.70	17.35	0.00	17.35	4.000	No	Yes	2.00
85	1.70	1.12	100.00	3.04	0.55	1.70	18.19	0.00	18.19	4.000	No	Yes	2.00
86	1.72	1.19	100.00	2.99	0.55	1.70	20.21	0.00	20.21	4.000	No	Yes	2.00
87	1.74	1.27	98.62	2.95	0.54	1.70	21.26	0.00	21.26	4.000	No	Yes	2.00
88	1.76	1.31	96.84	2.92	0.54	1.70	21.99	0.00	21.99	4.000	No	Yes	2.00
89	1.78	1.34	95.15	2.90	0.54	1.70	22.01	0.00	22.01	4.000	No	Yes	2.00
90	1.80	1.35	94.74	2.90	0.54	1.70	23.01	0.00	23.01	4.000	No	Yes	2.00
91	1.82	1.36	94.34	2.89	0.54	1.70	22.36	0.00	22.36	4.000	No	Yes	2.00
92	1.84	1.34	94.80	2.90	0.54	1.70	22.31	0.00	22.31	4.000	No	Yes	2.00
93	1.86	1.30	95.68	2.91	0.54	1.70	22.01	0.00	22.01	4.000	No	Yes	2.00
94	1.88	1.26	96.63	2.92	0.54	1.70	20.48	0.00	20.48	4.000	No	Yes	2.00
95	1.90	1.22	97.58	2.93	0.55	1.70	20.32	0.00	20.32	4.000	No	Yes	2.00
96	1.92	1.21	97.32	2.93	0.55	1.70	20.05	0.00	20.05	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
97	1.94	1.18	96.93	2.92	0.55	1.70	19.61	0.00	19.61	4.000	No	Yes	2.00
98	1.96	1.16	96.67	2.92	0.55	1.70	19.17	0.00	19.17	4.000	No	Yes	2.00
99	1.98	1.13	97.13	2.93	0.55	1.70	18.70	0.00	18.70	4.000	No	Yes	2.00
100	2.01	1.09	97.98	2.94	0.55	1.70	17.95	0.00	17.95	4.000	No	Yes	2.00
101	2.02	1.06	98.61	2.95	0.56	1.70	17.28	0.00	17.28	4.000	No	Yes	2.00
102	2.04	1.04	98.86	2.95	0.56	1.70	17.20	0.00	17.20	4.000	No	Yes	2.00
103	2.06	1.04	98.38	2.94	0.56	1.70	16.91	0.00	16.91	4.000	No	Yes	2.00
104	2.08	1.05	97.43	2.93	0.56	1.70	17.18	0.00	17.18	4.000	No	Yes	2.00
105	2.10	1.07	96.24	2.92	0.55	1.70	17.68	0.00	17.68	4.000	No	Yes	2.00
106	2.12	1.08	95.79	2.91	0.55	1.70	17.87	0.00	17.87	4.000	No	Yes	2.00
107	2.14	1.08	96.23	2.92	0.55	1.70	17.78	0.00	17.78	4.000	No	Yes	2.00
108	2.16	1.08	96.89	2.92	0.55	1.70	17.69	0.00	17.69	4.000	No	Yes	2.00
109	2.18	1.07	97.66	2.93	0.55	1.70	17.76	0.00	17.76	4.000	No	Yes	2.00
110	2.20	1.05	99.04	2.95	0.55	1.70	17.48	0.00	17.48	4.000	No	Yes	2.00
111	2.22	1.03	100.00	2.97	0.56	1.70	16.81	0.00	16.81	4.000	No	Yes	2.00
112	2.24	0.99	100.00	3.01	0.56	1.70	16.40	0.00	16.40	4.000	No	Yes	2.00
113	2.26	0.95	100.00	3.04	0.56	1.70	15.57	0.00	15.57	4.000	No	Yes	2.00
114	2.28	0.91	100.00	3.06	0.56	1.70	14.74	0.00	14.74	4.000	No	Yes	2.00
115	2.30	0.86	100.00	3.09	0.57	1.70	14.34	0.00	14.34	4.000	No	Yes	2.00
116	2.32	0.83	100.00	3.11	0.57	1.70	13.50	0.00	13.50	4.000	No	Yes	2.00
117	2.34	0.79	100.00	3.14	0.57	1.70	13.02	0.00	13.02	4.000	No	Yes	2.00
118	2.36	0.76	100.00	3.15	0.57	1.70	12.38	0.00	12.38	4.000	No	Yes	2.00
119	2.38	0.73	100.00	3.16	0.57	1.70	12.02	0.00	12.02	4.000	No	Yes	2.00
120	2.40	0.71	100.00	3.17	0.58	1.70	11.58	0.00	11.58	4.000	No	Yes	2.00
121	2.42	0.68	100.00	3.18	0.58	1.70	11.06	0.00	11.06	4.000	No	Yes	2.00
122	2.44	0.65	100.00	3.18	0.58	1.70	10.54	0.00	10.54	4.000	No	Yes	2.00
123	2.46	0.63	100.00	3.17	0.58	1.70	10.37	0.00	10.37	4.000	No	Yes	2.00
124	2.48	0.61	100.00	3.16	0.58	1.70	9.81	0.00	9.81	4.000	No	Yes	2.00
125	2.50	0.58	100.00	3.16	0.58	1.70	9.37	0.00	9.37	4.000	No	Yes	2.00
126	2.52	0.56	100.00	3.16	0.59	1.70	8.89	0.00	8.89	4.000	No	Yes	2.00
127	2.54	0.55	100.00	3.12	0.59	1.70	8.69	0.00	8.69	4.000	No	Yes	2.00
128	2.56	0.56	100.00	3.08	0.59	1.70	9.19	0.00	9.19	4.000	No	Yes	2.00
129	2.58	0.58	100.00	3.03	0.58	1.70	9.41	0.00	9.41	4.000	No	Yes	2.00
130	2.60	0.59	100.00	3.00	0.58	1.70	9.40	0.00	9.40	4.000	No	Yes	2.00
131	2.62	0.59	100.00	2.98	0.58	1.70	9.91	0.00	9.91	4.000	No	Yes	2.00
132	2.64	0.60	98.84	2.95	0.58	1.70	9.55	0.00	9.55	4.000	No	Yes	2.00
133	2.66	0.60	97.29	2.93	0.58	1.70	9.66	0.00	9.66	4.000	No	Yes	2.00
134	2.68	0.61	95.72	2.91	0.58	1.70	10.01	0.00	10.01	4.000	No	Yes	2.00
135	2.70	0.62	95.28	2.90	0.58	1.70	10.08	0.00	10.08	4.000	No	Yes	2.00
136	2.72	0.63	95.61	2.91	0.58	1.70	10.11	0.00	10.11	4.000	No	Yes	2.00
137	2.74	0.63	95.51	2.91	0.58	1.70	10.31	0.00	10.31	4.000	No	Yes	2.00
138	2.76	0.63	96.31	2.92	0.58	1.70	10.42	0.00	10.42	4.000	No	Yes	2.00
139	2.78	0.63	98.15	2.94	0.58	1.70	10.06	0.00	10.06	4.000	No	Yes	2.00
140	2.80	0.61	100.00	2.97	0.58	1.70	9.90	0.00	9.90	4.000	No	Yes	2.00
141	2.82	0.60	100.00	3.00	0.58	1.70	9.85	0.00	9.85	4.000	No	Yes	2.00
142	2.84	0.59	100.00	3.03	0.58	1.70	9.34	0.00	9.34	4.000	No	Yes	2.00
143	2.86	0.61	100.00	3.02	0.58	1.70	9.34	0.00	9.34	4.000	No	Yes	2.00
144	2.88	0.65	100.00	2.98	0.58	1.70	11.03	0.00	11.03	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
145	2.90	0.69	99.12	2.95	0.58	1.70	11.34	0.00	11.34	4.000	No	Yes	2.00
146	2.92	0.70	98.53	2.94	0.58	1.70	11.14	0.00	11.14	4.000	No	Yes	2.00
147	2.94	0.71	98.16	2.94	0.58	1.70	11.53	0.00	11.53	4.000	No	Yes	2.00
148	2.96	0.72	96.70	2.92	0.58	1.70	11.73	0.00	11.73	4.000	No	Yes	2.00
149	2.98	0.76	93.75	2.88	0.58	1.70	12.03	0.00	12.03	4.000	No	Yes	2.00
150	3.00	0.80	90.92	2.85	0.57	1.70	13.32	0.00	13.32	4.000	No	Yes	2.00
151	3.02	0.83	89.31	2.83	0.57	1.70	13.79	0.00	13.79	4.000	No	Yes	2.00
152	3.04	0.84	89.75	2.83	0.57	1.70	13.55	0.00	13.55	4.000	No	Yes	2.00
153	3.06	0.82	92.31	2.87	0.57	1.70	13.66	0.00	13.66	4.000	No	Yes	2.00
154	3.08	0.78	96.44	2.92	0.57	1.70	12.80	0.00	12.80	4.000	No	Yes	2.00
155	3.10	0.75	100.00	2.98	0.58	1.70	11.86	0.00	11.86	4.000	No	Yes	2.00
156	3.12	0.72	100.00	3.03	0.58	1.70	11.66	0.00	11.66	4.000	No	Yes	2.00
157	3.14	0.73	100.00	3.04	0.58	1.70	11.46	0.00	11.46	4.000	No	Yes	2.00
158	3.16	0.73	100.00	3.06	0.57	1.70	12.43	0.00	12.43	4.000	No	Yes	2.00
159	3.18	0.74	100.00	3.05	0.58	1.70	11.53	0.00	11.53	4.000	No	Yes	2.00
160	3.20	0.75	100.00	3.04	0.57	1.70	12.06	0.00	12.06	4.000	No	Yes	2.00
161	3.22	0.77	100.00	3.01	0.57	1.70	12.47	0.00	12.47	4.000	No	Yes	2.00
162	3.24	0.80	100.00	2.98	0.57	1.70	12.66	0.00	12.66	4.000	No	Yes	2.00
163	3.26	0.84	98.42	2.94	0.57	1.70	13.39	0.00	13.39	4.000	No	Yes	2.00
164	3.28	0.90	94.86	2.90	0.57	1.70	14.67	0.00	14.67	4.000	No	Yes	2.00
165	3.30	0.95	91.71	2.86	0.56	1.70	15.52	0.00	15.52	4.000	No	Yes	2.00
166	3.32	0.99	90.57	2.84	0.56	1.70	16.18	0.00	16.18	4.000	No	Yes	2.00
167	3.34	0.99	91.50	2.86	0.56	1.70	16.37	0.00	16.37	4.000	No	Yes	2.00
168	3.36	0.98	94.10	2.89	0.56	1.70	15.89	0.00	15.89	4.000	No	Yes	2.00
169	3.38	0.95	97.72	2.93	0.56	1.70	15.33	0.00	15.33	4.000	No	Yes	2.00
170	3.40	0.91	100.00	2.98	0.56	1.70	14.85	0.00	14.85	4.000	No	Yes	2.00
171	3.42	0.88	100.00	3.02	0.57	1.70	14.14	0.00	14.14	4.000	No	Yes	2.00
172	3.44	0.84	100.00	3.05	0.57	1.70	13.86	0.00	13.86	4.000	No	Yes	2.00
173	3.46	0.79	100.00	3.10	0.57	1.70	12.98	0.00	12.98	4.000	No	Yes	2.00
174	3.48	0.74	100.00	3.15	0.58	1.70	11.68	0.00	11.68	4.000	No	Yes	2.00
175	3.50	0.70	100.00	3.18	0.58	1.70	10.97	0.00	10.97	4.000	No	Yes	2.00
176	3.52	0.71	100.00	3.16	0.58	1.70	11.23	0.00	11.23	4.000	No	Yes	2.00
177	3.54	0.75	100.00	3.09	0.57	1.70	11.96	0.00	11.96	4.000	No	Yes	2.00
178	3.56	0.78	100.00	3.02	0.57	1.70	12.73	0.00	12.73	4.000	No	Yes	2.00
179	3.58	0.79	100.00	2.99	0.57	1.70	13.11	0.00	13.11	4.000	No	Yes	2.00
180	3.60	0.77	100.00	2.98	0.57	1.70	12.12	0.00	12.12	4.000	No	Yes	2.00
181	3.62	0.73	100.00	3.00	0.58	1.70	11.75	0.00	11.75	4.000	No	Yes	2.00
182	3.64	0.73	100.00	3.00	0.58	1.70	11.08	0.00	11.08	4.000	No	Yes	2.00
183	3.66	0.80	98.15	2.94	0.57	1.70	12.24	0.00	12.24	4.000	No	Yes	2.00
184	3.68	0.91	90.26	2.84	0.57	1.70	14.93	0.00	14.93	4.000	No	Yes	2.00
185	3.70	1.02	83.71	2.76	0.56	1.70	16.87	0.00	16.87	4.000	No	Yes	2.00
186	3.72	1.08	81.85	2.74	0.56	1.70	17.76	0.00	17.76	4.000	No	Yes	2.00
187	3.74	1.10	82.98	2.75	0.56	1.70	17.59	0.00	17.59	4.000	No	Yes	2.00
188	3.76	1.10	85.79	2.78	0.56	1.70	17.86	0.00	17.86	4.000	No	Yes	2.00
189	3.78	1.11	87.92	2.81	0.56	1.70	17.89	0.00	17.89	4.000	No	Yes	2.00
190	3.80	1.13	89.46	2.83	0.55	1.70	18.16	0.00	18.16	4.000	No	Yes	2.00
191	3.82	1.17	89.57	2.83	0.55	1.70	18.63	0.00	18.63	4.000	No	Yes	2.00
192	3.84	1.20	90.38	2.84	0.55	1.70	19.96	0.00	19.96	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
193	3.86	1.24	91.32	2.85	0.55	1.70	20.07	0.00	20.07	4.000	No	Yes	2.00
194	3.88	1.26	93.15	2.88	0.54	1.70	20.94	0.00	20.94	4.000	No	Yes	2.00
195	3.90	1.26	95.04	2.90	0.54	1.70	20.86	0.00	20.86	4.000	No	Yes	2.00
196	3.92	1.25	97.17	2.93	0.55	1.70	20.42	0.00	20.42	4.000	No	Yes	2.00
197	3.94	1.25	98.91	2.95	0.54	1.70	20.38	0.00	20.38	4.000	No	Yes	2.00
198	3.96	1.27	99.02	2.95	0.54	1.70	20.76	0.00	20.76	4.000	No	Yes	2.00
199	3.98	1.29	98.31	2.94	0.54	1.70	21.31	0.00	21.31	4.000	No	Yes	2.00
200	4.00	1.33	96.28	2.92	0.54	1.70	21.50	0.00	21.50	4.000	No	Yes	2.00
201	4.02	1.36	94.61	2.90	0.54	1.70	22.71	0.00	22.71	4.000	No	Yes	2.00
202	4.05	1.38	94.07	2.89	0.54	1.70	22.90	0.00	22.90	4.000	No	Yes	2.00
203	4.06	1.37	94.89	2.90	0.54	1.70	22.41	0.00	22.41	4.000	No	Yes	2.00
204	4.08	1.37	96.03	2.91	0.54	1.70	22.55	0.00	22.55	4.000	No	Yes	2.00
205	4.10	1.38	97.20	2.93	0.54	1.70	23.05	0.00	23.05	4.000	No	Yes	2.00
206	4.12	1.37	98.84	2.95	0.54	1.70	22.76	0.00	22.76	4.000	No	Yes	2.00
207	4.14	1.36	100.00	2.97	0.54	1.70	22.39	0.00	22.39	4.000	No	Yes	2.00
208	4.16	1.34	100.00	2.98	0.54	1.70	22.17	0.00	22.17	4.000	No	Yes	2.00
209	4.18	1.34	100.00	2.98	0.54	1.70	22.11	0.00	22.11	4.000	No	Yes	2.00
210	4.20	1.33	100.00	2.98	0.54	1.69	21.97	0.00	21.97	4.000	No	Yes	2.00
211	4.22	1.30	100.00	2.99	0.54	1.69	21.64	0.00	21.64	4.000	No	Yes	2.00
212	4.24	1.26	100.00	3.01	0.54	1.69	20.85	0.00	20.85	4.000	No	Yes	2.00
213	4.26	1.21	100.00	3.03	0.55	1.69	20.05	0.00	20.05	4.000	No	Yes	2.00
214	4.28	1.16	100.00	3.06	0.55	1.69	19.18	0.00	19.18	4.000	No	Yes	2.00
215	4.30	1.12	100.00	3.09	0.55	1.69	18.23	0.00	18.23	4.000	No	Yes	2.00
216	4.32	1.09	100.00	3.11	0.55	1.69	17.92	0.00	17.92	4.000	No	Yes	2.00
217	4.34	1.09	100.00	3.12	0.55	1.69	17.68	0.00	17.68	4.000	No	Yes	2.00
218	4.36	1.14	100.00	3.08	0.55	1.68	18.14	0.00	18.14	4.000	No	Yes	2.00
219	4.38	1.22	100.00	3.04	0.55	1.67	19.91	0.00	19.91	4.000	No	Yes	2.00
220	4.40	1.31	100.00	2.98	0.54	1.66	21.01	0.00	21.01	4.000	No	Yes	2.00
221	4.42	1.38	98.56	2.94	0.54	1.65	22.15	0.00	22.15	4.000	No	Yes	2.00
222	4.44	1.44	96.19	2.91	0.54	1.64	23.10	0.00	23.10	4.000	No	Yes	2.00
223	4.46	1.49	94.57	2.89	0.53	1.64	23.66	0.00	23.66	4.000	No	Yes	2.00
224	4.48	1.51	94.03	2.89	0.53	1.63	24.20	0.00	24.20	4.000	No	Yes	2.00
225	4.50	1.52	94.03	2.89	0.53	1.63	23.89	0.00	23.89	4.000	No	Yes	2.00
226	4.52	1.52	94.81	2.90	0.53	1.62	24.24	0.00	24.24	4.000	No	Yes	2.00
227	4.54	1.53	95.87	2.91	0.53	1.62	24.07	0.00	24.07	4.000	No	Yes	2.00
228	4.56	1.52	97.50	2.93	0.53	1.62	23.89	0.00	23.89	4.000	No	Yes	2.00
229	4.58	1.48	99.93	2.96	0.53	1.61	23.53	0.00	23.53	4.000	No	Yes	2.00
230	4.60	1.44	100.00	3.00	0.54	1.61	22.45	0.00	22.45	4.000	No	Yes	2.00
231	4.62	1.38	100.00	3.03	0.54	1.61	21.62	0.00	21.62	4.000	No	Yes	2.00
232	4.64	1.34	100.00	3.05	0.54	1.62	20.79	0.00	20.79	4.000	No	Yes	2.00
233	4.66	1.31	100.00	3.05	0.54	1.61	20.45	0.00	20.45	4.000	No	Yes	2.00
234	4.68	1.30	100.00	3.04	0.54	1.61	20.47	0.00	20.47	4.000	No	Yes	2.00
235	4.70	1.26	100.00	3.05	0.55	1.61	19.92	0.00	19.92	4.000	No	Yes	2.00
236	4.72	1.20	100.00	3.08	0.55	1.61	18.74	0.00	18.74	4.000	No	Yes	2.00
237	4.74	1.14	100.00	3.11	0.55	1.61	17.77	0.00	17.77	4.000	No	Yes	2.00
238	4.76	1.09	100.00	3.14	0.56	1.61	16.90	0.00	16.90	4.000	No	Yes	2.00
239	4.78	1.04	100.00	3.17	0.56	1.61	16.26	0.00	16.26	4.000	No	Yes	2.00
240	4.80	0.99	100.00	3.20	0.56	1.61	15.39	0.00	15.39	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
241	4.82	0.93	100.00	3.23	0.56	1.61	14.86	0.00	14.86	4.000	No	Yes	2.00
242	4.84	0.91	100.00	3.23	0.57	1.62	13.16	0.00	13.16	4.000	No	Yes	2.00
243	4.86	0.89	100.00	3.24	0.57	1.61	14.52	0.00	14.52	4.000	No	Yes	2.00
244	4.88	0.90	100.00	3.23	0.57	1.61	13.79	0.00	13.79	4.000	No	Yes	2.00
245	4.91	0.87	100.00	3.24	0.57	1.60	13.32	0.00	13.32	4.000	No	Yes	2.00
246	4.92	0.86	100.00	3.23	0.57	1.60	13.35	0.00	13.35	4.000	No	Yes	2.00
247	4.94	0.87	100.00	3.20	0.57	1.60	13.36	0.00	13.36	4.000	No	Yes	2.00
248	4.96	0.90	100.00	3.16	0.57	1.59	13.65	0.00	13.65	4.000	No	Yes	2.00
249	4.98	0.93	100.00	3.13	0.57	1.59	14.42	0.00	14.42	4.000	No	Yes	2.00
250	5.00	0.96	100.00	3.09	0.56	1.58	14.60	0.00	14.60	4.000	No	Yes	2.00
251	5.02	0.98	100.00	3.07	0.56	1.58	15.16	0.00	15.16	4.000	No	Yes	2.00
252	5.04	1.01	100.00	3.05	0.56	1.57	15.26	0.00	15.26	4.000	No	Yes	2.00
253	5.06	1.02	100.00	3.04	0.56	1.57	15.68	0.00	15.68	4.000	No	Yes	2.00
254	5.08	1.04	100.00	3.03	0.56	1.57	15.68	0.00	15.68	4.000	No	Yes	2.00
255	5.10	1.04	100.00	3.03	0.56	1.56	15.89	0.00	15.89	4.000	No	Yes	2.00
256	5.12	1.04	100.00	3.03	0.56	1.56	15.52	0.00	15.52	4.000	No	Yes	2.00
257	5.14	1.01	100.00	3.06	0.56	1.56	15.59	0.00	15.59	4.000	No	Yes	2.00
258	5.16	0.99	100.00	3.08	0.56	1.56	14.70	0.00	14.70	4.000	No	Yes	2.00
259	5.18	0.95	100.00	3.10	0.57	1.56	14.30	0.00	14.30	4.000	No	Yes	2.00
260	5.20	0.93	100.00	3.11	0.57	1.56	13.89	0.00	13.89	4.000	No	Yes	2.00
261	5.22	0.93	100.00	3.10	0.57	1.55	13.93	0.00	13.93	4.000	No	Yes	2.00
262	5.24	0.93	100.00	3.09	0.57	1.55	13.91	0.00	13.91	4.000	No	Yes	2.00
263	5.26	0.95	100.00	3.06	0.57	1.55	14.09	0.00	14.09	4.000	No	Yes	2.00
264	5.28	0.98	100.00	3.03	0.56	1.54	14.74	0.00	14.74	4.000	No	Yes	2.00
265	5.30	1.03	100.00	2.99	0.56	1.54	15.12	0.00	15.12	4.000	No	Yes	2.00
266	5.32	1.07	99.12	2.95	0.56	1.53	15.84	0.00	15.84	4.000	No	Yes	2.00
267	5.34	1.12	95.92	2.91	0.56	1.53	16.54	0.00	16.54	4.000	No	Yes	2.00
268	5.36	1.17	93.83	2.89	0.56	1.52	17.33	0.00	17.33	4.000	No	Yes	2.00
269	5.38	1.19	93.46	2.88	0.56	1.52	17.67	0.00	17.67	4.000	No	Yes	2.00
270	5.40	1.19	95.03	2.90	0.56	1.52	17.30	0.00	17.30	4.000	No	Yes	2.00
271	5.42	1.18	97.08	2.93	0.56	1.51	17.20	0.00	17.20	4.000	No	Yes	2.00
272	5.44	1.19	97.96	2.94	0.56	1.51	17.17	0.00	17.17	4.000	No	Yes	2.00
273	5.46	1.21	97.71	2.93	0.55	1.50	17.60	0.00	17.60	4.000	No	Yes	2.00
274	5.48	1.23	98.02	2.94	0.55	1.50	18.24	0.00	18.24	4.000	No	Yes	2.00
275	5.50	1.23	99.06	2.95	0.55	1.50	17.81	0.00	17.81	4.000	No	Yes	2.00
276	5.52	1.21	100.00	2.97	0.55	1.50	17.38	0.00	17.38	4.000	No	Yes	2.00
277	5.54	1.18	100.00	2.98	0.56	1.49	17.21	0.00	17.21	4.000	No	Yes	2.00
278	5.56	1.16	100.00	2.99	0.56	1.49	16.55	0.00	16.55	4.000	No	Yes	2.00
279	5.58	1.12	100.00	3.01	0.56	1.49	16.29	0.00	16.29	4.000	No	Yes	2.00
280	5.60	1.11	100.00	3.02	0.56	1.49	15.80	0.00	15.80	4.000	No	Yes	2.00
281	5.62	1.11	100.00	3.01	0.56	1.49	15.90	0.00	15.90	4.000	No	Yes	2.00
282	5.64	1.11	100.00	3.01	0.56	1.49	16.17	0.00	16.17	4.000	No	Yes	2.00
283	5.66	1.11	100.00	3.00	0.56	1.48	15.91	0.00	15.91	4.000	No	Yes	2.00
284	5.68	1.11	100.00	3.01	0.56	1.48	15.81	0.00	15.81	4.000	No	Yes	2.00
285	5.70	1.11	100.00	3.01	0.56	1.48	15.71	0.00	15.71	4.000	No	Yes	2.00
286	5.72	1.11	100.00	3.00	0.56	1.48	15.88	0.00	15.88	4.000	No	Yes	2.00
287	5.74	1.11	100.00	2.99	0.56	1.47	15.79	0.00	15.79	4.000	No	Yes	2.00
288	5.76	1.11	100.00	3.00	0.56	1.47	15.83	0.00	15.83	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
289	5.78	1.10	100.00	3.00	0.56	1.47	15.73	0.00	15.73	4.000	No	Yes	2.00
290	5.80	1.08	100.00	3.02	0.56	1.47	15.28	0.00	15.28	4.000	No	Yes	2.00
291	5.82	1.06	100.00	3.03	0.56	1.47	14.92	0.00	14.92	4.000	No	Yes	2.00
292	5.84	1.06	100.00	3.03	0.56	1.46	14.87	0.00	14.87	4.000	No	Yes	2.00
293	5.86	1.07	100.00	3.03	0.56	1.46	15.04	0.00	15.04	4.000	No	Yes	2.00
294	5.88	1.11	100.00	3.01	0.56	1.46	15.28	0.00	15.28	4.000	No	Yes	2.00
295	5.90	1.16	100.00	2.97	0.56	1.45	16.16	0.00	16.16	4.000	No	Yes	2.00
296	5.92	1.21	97.46	2.93	0.56	1.45	17.01	0.00	17.01	4.000	No	Yes	2.00
297	5.94	1.26	95.02	2.90	0.56	1.44	17.66	0.00	17.66	4.000	No	Yes	2.00
298	5.96	1.27	94.77	2.90	0.55	1.44	17.79	0.00	17.79	4.000	No	Yes	2.00
299	5.98	1.28	95.02	2.90	0.56	1.44	17.56	0.00	17.56	4.000	No	Yes	2.00
300	6.00	1.30	95.36	2.90	0.55	1.43	18.08	0.00	18.08	4.000	No	Yes	2.00
301	6.02	1.32	95.92	2.91	0.55	1.43	18.42	0.00	18.42	4.000	No	Yes	2.00
302	6.04	1.32	97.35	2.93	0.55	1.43	18.13	0.00	18.13	4.000	No	Yes	2.00
303	6.06	1.32	99.14	2.95	0.55	1.43	18.22	0.00	18.22	4.000	No	Yes	2.00
304	6.08	1.32	100.00	2.97	0.55	1.42	18.18	0.00	18.18	4.000	No	Yes	2.00
305	6.10	1.33	100.00	2.97	0.55	1.42	18.08	0.00	18.08	4.000	No	Yes	2.00
306	6.12	1.35	100.00	2.96	0.55	1.42	18.33	0.00	18.33	4.000	No	Yes	2.00
307	6.14	1.38	99.50	2.96	0.55	1.41	19.02	0.00	19.02	4.000	No	Yes	2.00
308	6.16	1.40	99.08	2.95	0.55	1.41	19.08	0.00	19.08	4.000	No	Yes	2.00
309	6.18	1.44	98.58	2.94	0.55	1.41	19.42	0.00	19.42	4.000	No	Yes	2.00
310	6.20	1.50	96.89	2.92	0.55	1.40	20.23	0.00	20.23	4.000	No	Yes	2.00
311	6.22	1.57	94.47	2.89	0.54	1.40	21.35	0.00	21.35	4.000	No	Yes	2.00
312	6.24	1.61	93.11	2.88	0.54	1.39	22.15	0.00	22.15	4.000	No	Yes	2.00
313	6.26	1.63	93.03	2.88	0.54	1.39	21.92	0.00	21.92	4.000	No	Yes	2.00
314	6.28	1.61	94.06	2.89	0.54	1.39	21.78	0.00	21.78	4.000	No	Yes	2.00
315	6.30	1.57	96.00	2.91	0.54	1.39	21.42	0.00	21.42	4.000	No	Yes	2.00
316	6.32	1.53	97.80	2.94	0.55	1.39	20.20	0.00	20.20	4.000	No	Yes	2.00
317	6.34	1.48	99.93	2.96	0.55	1.39	20.00	0.00	20.00	4.000	No	Yes	2.00
318	6.36	1.45	100.00	2.98	0.55	1.39	19.55	0.00	19.55	4.000	No	Yes	2.00
319	6.38	1.42	100.00	3.00	0.55	1.38	19.05	0.00	19.05	4.000	No	Yes	2.00
320	6.40	1.39	100.00	3.01	0.55	1.38	18.63	0.00	18.63	4.000	No	Yes	2.00
321	6.42	1.37	100.00	3.02	0.55	1.38	18.35	0.00	18.35	4.000	No	Yes	2.00
322	6.44	1.34	100.00	3.02	0.55	1.38	17.96	0.00	17.96	4.000	No	Yes	2.00
323	6.46	1.32	100.00	3.03	0.56	1.38	17.33	0.00	17.33	4.000	No	Yes	2.00
324	6.48	1.33	100.00	3.02	0.55	1.38	17.60	0.00	17.60	4.000	No	Yes	2.00
325	6.50	1.35	100.00	3.00	0.55	1.37	18.09	0.00	18.09	4.000	No	Yes	2.00
326	6.52	1.37	100.00	2.97	0.55	1.37	18.29	0.00	18.29	4.000	No	Yes	2.00
327	6.54	1.36	100.00	2.97	0.55	1.37	18.20	0.00	18.20	4.000	No	Yes	2.00
328	6.56	1.31	100.00	2.97	0.55	1.37	17.52	0.00	17.52	4.000	No	Yes	2.00
329	6.58	1.24	100.00	3.00	0.56	1.37	16.41	0.00	16.41	4.000	No	Yes	2.00
330	6.60	1.18	100.00	3.02	0.56	1.37	15.49	0.00	15.49	4.000	No	Yes	2.00
331	6.62	1.15	100.00	3.03	0.56	1.37	15.06	0.00	15.06	4.000	No	Yes	2.00
332	6.64	1.13	100.00	3.05	0.56	1.37	15.13	0.00	15.13	4.000	No	Yes	2.00
333	6.66	1.12	100.00	3.07	0.57	1.37	14.48	0.00	14.48	4.000	No	Yes	2.00
334	6.68	1.11	100.00	3.08	0.57	1.36	14.43	0.00	14.43	4.000	No	Yes	2.00
335	6.70	1.13	100.00	3.08	0.56	1.36	14.68	0.00	14.68	4.000	No	Yes	2.00
336	6.72	1.15	100.00	3.06	0.56	1.36	15.10	0.00	15.10	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
337	6.74	1.17	100.00	3.05	0.56	1.35	15.38	0.00	15.38	4.000	No	Yes	2.00
338	6.76	1.18	100.00	3.05	0.56	1.35	15.49	0.00	15.49	4.000	No	Yes	2.00
339	6.78	1.18	100.00	3.05	0.56	1.35	15.43	0.00	15.43	4.000	No	Yes	2.00
340	6.80	1.17	100.00	3.05	0.56	1.35	14.95	0.00	14.95	4.000	No	Yes	2.00
341	6.82	1.19	100.00	3.04	0.56	1.35	15.33	0.00	15.33	4.000	No	Yes	2.00
342	6.84	1.24	100.00	3.02	0.56	1.34	16.18	0.00	16.18	4.000	No	Yes	2.00
343	6.86	1.27	100.00	3.01	0.56	1.34	16.56	0.00	16.56	4.000	No	Yes	2.00
344	6.88	1.28	100.00	3.02	0.56	1.34	16.65	0.00	16.65	4.000	No	Yes	2.00
345	6.90	1.27	100.00	3.04	0.56	1.34	16.39	0.00	16.39	4.000	No	Yes	2.00
346	6.92	1.27	100.00	3.05	0.56	1.33	16.06	0.00	16.06	4.000	No	Yes	2.00
347	6.94	1.30	100.00	3.03	0.56	1.33	16.48	0.00	16.48	4.000	No	Yes	2.00
348	6.96	1.36	100.00	3.00	0.55	1.33	17.49	0.00	17.49	4.000	No	Yes	2.00
349	6.98	1.39	100.00	2.98	0.55	1.32	18.47	0.00	18.47	4.000	No	Yes	2.00
350	7.00	1.36	100.00	2.99	0.56	1.32	17.31	0.00	17.31	4.000	No	Yes	2.00
351	7.02	1.28	100.00	3.03	0.56	1.32	16.57	0.00	16.57	4.000	No	Yes	2.00
352	7.04	1.22	100.00	3.06	0.56	1.32	15.23	0.00	15.23	4.000	No	Yes	2.00
353	7.06	1.18	100.00	3.08	0.56	1.32	14.93	0.00	14.93	4.000	No	Yes	2.00
354	7.08	1.17	100.00	3.08	0.56	1.32	14.85	0.00	14.85	4.000	No	Yes	2.00
355	7.10	1.18	100.00	3.07	0.56	1.32	14.91	0.00	14.91	4.000	No	Yes	2.00
356	7.12	1.22	100.00	3.05	0.56	1.32	15.31	0.00	15.31	4.000	No	Yes	2.00
357	7.14	1.27	100.00	3.01	0.56	1.31	16.11	0.00	16.11	4.000	No	Yes	2.00
358	7.16	1.32	100.00	2.97	0.56	1.31	16.82	0.00	16.82	4.000	No	Yes	2.00
359	7.18	1.37	97.01	2.93	0.56	1.31	17.13	0.00	17.13	4.000	No	Yes	2.00
360	7.20	1.42	94.92	2.90	0.55	1.30	18.04	0.00	18.04	4.000	No	Yes	2.00
361	7.22	1.49	92.74	2.87	0.55	1.30	18.52	0.00	18.52	4.000	No	Yes	2.00
362	7.24	1.56	90.90	2.85	0.55	1.30	19.46	0.00	19.46	4.000	No	Yes	2.00
363	7.26	1.63	89.38	2.83	0.55	1.29	20.74	0.00	20.74	4.000	No	Yes	2.00
364	7.28	1.72	88.07	2.81	0.54	1.29	21.21	0.00	21.21	4.000	No	Yes	2.00
365	7.30	1.78	87.10	2.80	0.54	1.29	22.40	0.00	22.40	4.000	No	Yes	2.00
366	7.32	1.83	86.85	2.80	0.54	1.28	22.92	0.00	22.92	4.000	No	Yes	2.00
367	7.34	1.83	88.49	2.82	0.54	1.28	22.91	0.00	22.91	4.000	No	Yes	2.00
368	7.36	1.81	91.35	2.85	0.54	1.28	22.46	0.00	22.46	4.000	No	Yes	2.00
369	7.38	1.76	94.61	2.90	0.54	1.28	21.88	0.00	21.88	4.000	No	Yes	2.00
370	7.40	1.73	96.79	2.92	0.54	1.28	21.23	0.00	21.23	4.000	No	Yes	2.00
371	7.42	1.68	99.66	2.96	0.54	1.28	21.14	0.00	21.14	4.000	No	Yes	2.00
372	7.44	1.63	100.00	3.00	0.55	1.28	20.07	0.00	20.07	4.000	No	Yes	2.00
373	7.46	1.57	100.00	3.03	0.55	1.27	19.29	0.00	19.29	4.000	No	Yes	2.00
374	7.48	1.54	100.00	3.04	0.55	1.27	18.88	0.00	18.88	4.000	No	Yes	2.00
375	7.50	1.55	100.00	3.02	0.55	1.27	18.76	0.00	18.76	4.000	No	Yes	2.00
376	7.52	1.59	100.00	2.98	0.55	1.27	19.70	0.00	19.70	4.000	No	Yes	2.00
377	7.54	1.63	98.30	2.94	0.55	1.27	20.27	0.00	20.27	4.000	No	Yes	2.00
378	7.56	1.64	97.33	2.93	0.55	1.26	20.07	0.00	20.07	4.000	No	Yes	2.00
379	7.58	1.61	98.25	2.94	0.55	1.26	19.89	0.00	19.89	4.000	No	Yes	2.00
380	7.60	1.59	99.66	2.96	0.55	1.26	19.34	0.00	19.34	4.000	No	Yes	2.00
381	7.62	1.57	100.00	2.97	0.55	1.26	18.96	0.00	18.96	4.000	No	Yes	2.00
382	7.64	1.57	100.00	2.99	0.55	1.26	19.21	0.00	19.21	4.000	No	Yes	2.00
383	7.66	1.59	100.00	2.99	0.55	1.26	19.29	0.00	19.29	4.000	No	Yes	2.00
384	7.68	1.60	100.00	2.99	0.55	1.25	19.66	0.00	19.66	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
385	7.70	1.60	100.00	2.99	0.55	1.25	19.37	0.00	19.37	4.000	No	Yes	2.00
386	7.72	1.59	100.00	2.99	0.55	1.25	19.22	0.00	19.22	4.000	No	Yes	2.00
387	7.74	1.61	100.00	2.97	0.55	1.25	19.33	0.00	19.33	4.000	No	Yes	2.00
388	7.76	1.66	98.46	2.94	0.55	1.25	19.87	0.00	19.87	4.000	No	Yes	2.00
389	7.78	1.71	96.02	2.91	0.54	1.24	20.89	0.00	20.89	4.000	No	Yes	2.00
390	7.80	1.61	97.58	2.93	0.54	1.24	21.27	0.00	21.27	4.000	No	Yes	2.00
391	7.82	1.62	97.38	2.93	0.56	1.25	16.16	0.00	16.16	4.000	No	Yes	2.00
392	7.84	1.60	98.40	2.94	0.54	1.24	21.06	0.00	21.06	4.000	No	Yes	2.00
393	7.86	1.71	97.07	2.93	0.54	1.24	20.73	0.00	20.73	4.000	No	Yes	2.00
394	7.88	1.69	99.06	2.95	0.55	1.24	20.08	0.00	20.08	4.000	No	Yes	2.00
395	7.90	1.69	100.00	2.96	0.54	1.23	20.24	0.00	20.24	4.000	No	Yes	2.00
396	7.92	1.72	99.78	2.96	0.54	1.23	20.63	0.00	20.63	4.000	No	Yes	2.00
397	7.94	1.76	98.46	2.94	0.54	1.23	20.91	0.00	20.91	4.000	No	Yes	2.00
398	7.96	1.77	97.91	2.94	0.54	1.23	21.58	0.00	21.58	4.000	No	Yes	2.00
399	7.98	1.77	98.15	2.94	0.54	1.23	21.13	0.00	21.13	4.000	No	Yes	2.00
400	8.00	1.73	99.39	2.95	0.54	1.22	20.64	0.00	20.64	4.000	No	Yes	2.00
401	8.02	1.70	100.00	2.97	0.55	1.22	20.14	0.00	20.14	4.000	No	Yes	2.00
402	8.04	1.66	100.00	2.98	0.55	1.22	19.91	0.00	19.91	4.000	No	Yes	2.00
403	8.06	1.64	100.00	3.00	0.55	1.22	19.26	0.00	19.26	4.000	No	Yes	2.00
404	8.08	1.64	100.00	3.00	0.55	1.22	19.21	0.00	19.21	4.000	No	Yes	2.00
405	8.10	1.68	100.00	2.97	0.55	1.22	19.78	0.00	19.78	4.000	No	Yes	2.00
406	8.12	1.72	98.14	2.94	0.54	1.22	20.60	0.00	20.60	4.000	No	Yes	2.00
407	8.14	1.72	97.05	2.93	0.54	1.21	20.54	0.00	20.54	4.000	No	Yes	2.00
408	8.16	1.69	97.80	2.94	0.55	1.21	20.01	0.00	20.01	4.000	No	Yes	2.00
409	8.18	1.65	99.07	2.95	0.55	1.21	19.37	0.00	19.37	4.000	No	Yes	2.00
410	8.20	1.59	100.00	2.98	0.55	1.21	18.93	0.00	18.93	4.000	No	Yes	2.00
411	8.22	1.53	100.00	3.01	0.55	1.21	18.04	0.00	18.04	4.000	No	Yes	2.00
412	8.24	1.46	100.00	3.05	0.56	1.21	17.14	0.00	17.14	4.000	No	Yes	2.00
413	8.26	1.39	100.00	3.08	0.56	1.21	16.20	0.00	16.20	4.000	No	Yes	2.00
414	8.28	1.33	100.00	3.10	0.56	1.21	15.71	0.00	15.71	4.000	No	Yes	2.00
415	8.30	1.30	100.00	3.10	0.56	1.21	15.08	0.00	15.08	4.000	No	Yes	2.00
416	8.32	1.27	100.00	3.10	0.56	1.21	15.08	0.00	15.08	4.000	No	Yes	2.00
417	8.34	1.25	100.00	3.09	0.57	1.21	14.56	0.00	14.56	4.000	No	Yes	2.00
418	8.36	1.24	100.00	3.07	0.57	1.21	14.27	0.00	14.27	4.000	No	Yes	2.00
419	8.38	1.23	100.00	3.05	0.57	1.20	14.39	0.00	14.39	4.000	No	Yes	2.00
420	8.40	1.23	100.00	3.03	0.57	1.20	14.40	0.00	14.40	4.000	No	Yes	2.00
421	8.42	1.22	100.00	3.02	0.57	1.20	14.08	0.00	14.08	4.000	No	Yes	2.00
422	8.44	1.22	100.00	3.01	0.57	1.20	14.12	0.00	14.12	4.000	No	Yes	2.00
423	8.46	1.20	100.00	3.00	0.57	1.20	14.08	0.00	14.08	4.000	No	Yes	2.00
424	8.48	1.18	100.00	3.01	0.57	1.20	13.52	0.00	13.52	4.000	No	Yes	2.00
425	8.50	1.15	100.00	3.02	0.57	1.20	13.29	0.00	13.29	4.000	No	Yes	2.00
426	8.52	1.12	100.00	3.03	0.57	1.20	12.98	0.00	12.98	4.000	No	Yes	2.00
427	8.54	1.10	100.00	3.04	0.57	1.19	12.45	0.00	12.45	4.000	No	Yes	2.00
428	8.56	1.09	100.00	3.05	0.57	1.19	12.47	0.00	12.47	4.000	No	Yes	2.00
429	8.58	1.09	100.00	3.05	0.57	1.19	12.57	0.00	12.57	4.000	No	Yes	2.00
430	8.60	1.11	100.00	3.03	0.57	1.19	12.53	0.00	12.53	4.000	No	Yes	2.00
431	8.62	1.14	100.00	3.01	0.57	1.19	13.01	0.00	13.01	4.000	No	Yes	2.00
432	8.64	1.19	100.00	2.97	0.57	1.19	13.50	0.00	13.50	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
433	8.66	1.23	97.95	2.94	0.57	1.18	13.95	0.00	13.95	4.000	No	Yes	2.00
434	8.68	1.28	95.84	2.91	0.57	1.18	14.62	0.00	14.62	4.000	No	Yes	2.00
435	8.70	1.31	94.96	2.90	0.56	1.18	15.07	0.00	15.07	4.000	No	Yes	2.00
436	8.72	1.31	96.18	2.91	0.56	1.18	15.06	0.00	15.06	4.000	No	Yes	2.00
437	8.74	1.27	99.57	2.96	0.57	1.18	14.43	0.00	14.43	4.000	No	Yes	2.00
438	8.76	1.20	100.00	3.02	0.57	1.18	13.78	0.00	13.78	4.000	No	Yes	2.00
439	8.78	1.13	100.00	3.09	0.57	1.18	12.66	0.00	12.66	4.000	No	Yes	2.00
440	8.80	1.07	100.00	3.15	0.58	1.18	11.82	0.00	11.82	4.000	No	Yes	2.00
441	8.82	1.04	100.00	3.19	0.58	1.18	11.58	0.00	11.58	4.000	No	Yes	2.00
442	8.84	1.04	100.00	3.20	0.58	1.17	11.68	0.00	11.68	4.000	No	Yes	2.00
443	8.86	1.03	100.00	3.20	0.58	1.17	11.64	0.00	11.64	4.000	No	Yes	2.00
444	8.88	1.02	100.00	3.19	0.58	1.17	11.28	0.00	11.28	4.000	No	Yes	2.00
445	8.91	1.03	100.00	3.16	0.58	1.17	11.37	0.00	11.37	4.000	No	Yes	2.00
446	8.92	1.07	100.00	3.10	0.57	1.17	11.92	0.00	11.92	4.000	No	Yes	2.00
447	8.94	1.10	100.00	3.04	0.57	1.17	12.25	0.00	12.25	4.000	No	Yes	2.00
448	8.96	1.12	100.00	3.01	0.57	1.17	12.53	0.00	12.53	4.000	No	Yes	2.00
449	8.98	1.14	100.00	2.98	0.57	1.16	12.44	0.00	12.44	4.000	No	Yes	2.00
450	9.00	1.15	100.00	2.97	0.57	1.16	12.82	0.00	12.82	4.000	No	Yes	2.00
451	9.02	1.18	98.82	2.95	0.57	1.16	12.91	0.00	12.91	4.000	No	Yes	2.00
452	9.04	1.25	96.69	2.92	0.57	1.16	13.49	0.00	13.49	4.000	No	Yes	2.00
453	9.06	1.35	93.39	2.88	0.57	1.16	14.83	0.00	14.83	4.000	No	Yes	2.00
454	9.08	1.48	89.15	2.83	0.56	1.15	16.27	0.00	16.27	4.000	No	Yes	2.00
455	9.10	1.58	86.59	2.79	0.56	1.15	17.73	0.00	17.73	4.000	No	Yes	2.00
456	9.12	1.63	86.33	2.79	0.56	1.15	18.27	0.00	18.27	4.000	No	Yes	2.00
457	9.14	1.63	88.52	2.82	0.56	1.15	18.06	0.00	18.06	4.000	No	Yes	2.00
458	9.16	1.60	91.83	2.86	0.56	1.15	17.69	0.00	17.69	4.000	No	Yes	2.00
459	9.18	1.56	95.41	2.91	0.56	1.15	17.14	0.00	17.14	4.000	No	Yes	2.00
460	9.20	1.53	98.77	2.95	0.56	1.15	16.75	0.00	16.75	4.000	No	Yes	2.00
461	9.22	1.53	100.00	2.96	0.56	1.14	16.52	0.00	16.52	4.000	No	Yes	2.00
462	9.24	1.55	100.00	2.97	0.56	1.14	17.16	0.00	17.16	4.000	No	Yes	2.00
463	9.26	1.55	100.00	2.98	0.56	1.14	17.14	0.00	17.14	4.000	No	Yes	2.00
464	9.28	1.52	100.00	3.00	0.56	1.14	16.57	0.00	16.57	4.000	No	Yes	2.00
465	9.30	1.50	100.00	3.02	0.56	1.14	16.34	0.00	16.34	4.000	No	Yes	2.00
466	9.32	1.48	100.00	3.04	0.56	1.14	16.13	0.00	16.13	4.000	No	Yes	2.00
467	9.34	1.48	100.00	3.05	0.56	1.14	15.93	0.00	15.93	4.000	No	Yes	2.00
468	9.36	1.48	100.00	3.05	0.56	1.14	16.29	0.00	16.29	4.000	No	Yes	2.00
469	9.38	1.48	100.00	3.06	0.56	1.13	16.16	0.00	16.16	4.000	No	Yes	2.00
470	9.40	1.45	100.00	3.07	0.56	1.13	15.83	0.00	15.83	4.000	No	Yes	2.00
471	9.42	1.41	100.00	3.09	0.56	1.13	15.23	0.00	15.23	4.000	No	Yes	2.00
472	9.44	1.36	100.00	3.11	0.56	1.13	14.95	0.00	14.95	4.000	No	Yes	2.00
473	9.46	1.32	100.00	3.14	0.57	1.13	14.04	0.00	14.04	4.000	No	Yes	2.00
474	9.48	1.28	100.00	3.16	0.57	1.13	13.76	0.00	13.76	4.000	No	Yes	2.00
475	9.50	1.27	100.00	3.16	0.57	1.13	13.66	0.00	13.66	4.000	No	Yes	2.00
476	9.52	1.26	100.00	3.16	0.57	1.13	13.67	0.00	13.67	4.000	No	Yes	2.00
477	9.54	1.27	100.00	3.16	0.57	1.13	13.54	0.00	13.54	4.000	No	Yes	2.00
478	9.56	1.26	100.00	3.15	0.57	1.12	13.78	0.00	13.78	4.000	No	Yes	2.00
479	9.58	1.26	100.00	3.15	0.57	1.12	13.47	0.00	13.47	4.000	No	Yes	2.00
480	9.60	1.24	100.00	3.15	0.57	1.12	13.19	0.00	13.19	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
481	9.62	1.22	100.00	3.15	0.57	1.12	13.12	0.00	13.12	4.000	No	Yes	2.00
482	9.64	1.21	100.00	3.16	0.57	1.12	12.90	0.00	12.90	4.000	No	Yes	2.00
483	9.66	1.19	100.00	3.16	0.57	1.12	12.67	0.00	12.67	4.000	No	Yes	2.00
484	9.68	1.18	100.00	3.16	0.57	1.12	12.58	0.00	12.58	4.000	No	Yes	2.00
485	9.70	1.17	100.00	3.16	0.57	1.12	12.46	0.00	12.46	4.000	No	Yes	2.00
486	9.72	1.18	100.00	3.14	0.57	1.12	12.44	0.00	12.44	4.000	No	Yes	2.00
487	9.74	1.22	100.00	3.11	0.57	1.11	12.92	0.00	12.92	4.000	No	Yes	2.00
488	9.76	1.29	100.00	3.06	0.57	1.11	13.67	0.00	13.67	4.000	No	Yes	2.00
489	9.78	1.35	100.00	3.02	0.57	1.11	14.47	0.00	14.47	4.000	No	Yes	2.00
490	9.80	1.40	100.00	2.98	0.56	1.11	14.79	0.00	14.79	4.000	No	Yes	2.00
491	9.82	1.42	100.00	2.97	0.56	1.11	15.30	0.00	15.30	4.000	No	Yes	2.00
492	9.84	1.43	100.00	2.98	0.56	1.11	15.16	0.00	15.16	4.000	No	Yes	2.00
493	9.86	1.43	100.00	3.00	0.56	1.11	15.15	0.00	15.15	4.000	No	Yes	2.00
494	9.88	1.41	100.00	3.04	0.56	1.10	15.08	0.00	15.08	4.000	No	Yes	2.00
495	9.90	1.40	100.00	3.07	0.56	1.10	14.76	0.00	14.76	4.000	No	Yes	2.00
496	9.92	1.38	100.00	3.10	0.56	1.10	14.61	0.00	14.61	4.000	No	Yes	2.00
497	9.94	1.37	100.00	3.12	0.57	1.10	14.50	0.00	14.50	4.000	No	Yes	2.00
498	9.96	1.35	100.00	3.14	0.57	1.10	14.33	0.00	14.33	4.000	No	Yes	2.00
499	9.98	1.33	100.00	3.14	0.57	1.10	13.75	0.00	13.75	4.000	No	Yes	2.00
500	10.00	1.32	100.00	3.15	0.57	1.10	14.04	0.00	14.04	4.000	No	Yes	2.00
501	10.02	1.31	100.00	3.15	0.57	1.10	13.77	0.00	13.77	4.000	No	Yes	2.00
502	10.04	1.31	100.00	3.15	0.57	1.10	13.65	0.00	13.65	4.000	No	Yes	2.00
503	10.06	1.33	100.00	3.13	0.57	1.09	13.96	0.00	13.96	4.000	No	Yes	2.00
504	10.08	1.35	100.00	3.12	0.57	1.09	14.19	0.00	14.19	4.000	No	Yes	2.00
505	10.10	1.36	100.00	3.11	0.57	1.09	14.19	0.00	14.19	4.000	No	Yes	2.00
506	10.12	1.36	100.00	3.10	0.57	1.09	14.37	0.00	14.37	4.000	No	Yes	2.00
507	10.14	1.36	100.00	3.11	0.57	1.09	14.15	0.00	14.15	4.000	No	Yes	2.00
508	10.16	1.36	100.00	3.11	0.57	1.09	14.00	0.00	14.00	4.000	No	Yes	2.00
509	10.18	1.38	100.00	3.10	0.57	1.09	14.31	0.00	14.31	4.000	No	Yes	2.00
510	10.20	1.40	100.00	3.10	0.56	1.08	14.79	0.00	14.79	4.000	No	Yes	2.00
511	10.22	1.40	100.00	3.10	0.56	1.08	14.59	0.00	14.59	4.000	No	Yes	2.00
512	10.24	1.38	100.00	3.13	0.57	1.08	14.42	0.00	14.42	4.000	No	Yes	2.00
513	10.26	1.35	100.00	3.14	0.57	1.08	13.93	0.00	13.93	4.000	No	Yes	2.00
514	10.28	1.31	100.00	3.16	0.57	1.08	13.79	0.00	13.79	4.000	No	Yes	2.00
515	10.30	1.29	100.00	3.17	0.57	1.08	13.14	0.00	13.14	4.000	No	Yes	2.00
516	10.32	1.26	100.00	3.18	0.57	1.08	13.13	0.00	13.13	4.000	No	Yes	2.00
517	10.34	1.25	100.00	3.18	0.57	1.08	12.86	0.00	12.86	4.000	No	Yes	2.00
518	10.36	1.24	100.00	3.18	0.57	1.08	12.77	0.00	12.77	4.000	No	Yes	2.00
519	10.38	1.23	100.00	3.17	0.57	1.08	12.56	0.00	12.56	4.000	No	Yes	2.00
520	10.40	1.24	100.00	3.16	0.57	1.07	12.71	0.00	12.71	4.000	No	Yes	2.00
521	10.42	1.26	100.00	3.15	0.57	1.07	12.90	0.00	12.90	4.000	No	Yes	2.00
522	10.44	1.27	100.00	3.13	0.57	1.07	13.08	0.00	13.08	4.000	No	Yes	2.00
523	10.46	1.29	100.00	3.12	0.57	1.07	13.19	0.00	13.19	4.000	No	Yes	2.00
524	10.48	1.30	100.00	3.12	0.57	1.07	13.42	0.00	13.42	4.000	No	Yes	2.00
525	10.50	1.31	100.00	3.12	0.57	1.07	13.48	0.00	13.48	4.000	No	Yes	2.00
526	10.52	1.30	100.00	3.13	0.57	1.07	13.42	0.00	13.42	4.000	No	Yes	2.00
527	10.54	1.30	100.00	3.14	0.57	1.07	13.13	0.00	13.13	4.000	No	Yes	2.00
528	10.56	1.30	100.00	3.15	0.57	1.07	13.22	0.00	13.22	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
529	10.58	1.34	100.00	3.13	0.57	1.06	13.57	0.00	13.57	4.000	No	Yes	2.00
530	10.60	1.39	100.00	3.10	0.57	1.06	14.17	0.00	14.17	4.000	No	Yes	2.00
531	10.62	1.43	100.00	3.08	0.56	1.06	14.81	0.00	14.81	4.000	No	Yes	2.00
532	10.64	1.44	100.00	3.08	0.56	1.06	14.63	0.00	14.63	4.000	No	Yes	2.00
533	10.66	1.44	100.00	3.09	0.56	1.06	14.63	0.00	14.63	4.000	No	Yes	2.00
534	10.68	1.44	100.00	3.10	0.56	1.06	14.64	0.00	14.64	4.000	No	Yes	2.00
535	10.70	1.46	100.00	3.09	0.56	1.06	14.60	0.00	14.60	4.000	No	Yes	2.00
536	10.72	1.52	100.00	3.06	0.56	1.06	15.24	0.00	15.24	4.000	No	Yes	2.00
537	10.74	1.58	100.00	3.04	0.56	1.05	16.35	0.00	16.35	4.000	No	Yes	2.00
538	10.76	1.63	100.00	3.02	0.56	1.05	16.53	0.00	16.53	4.000	No	Yes	2.00
539	10.78	1.42	100.00	3.07	0.56	1.05	16.73	0.00	16.73	4.000	No	Yes	2.00
540	10.80	1.47	100.00	3.05	0.58	1.05	9.82	0.00	9.82	4.000	No	Yes	2.00
541	10.82	1.52	100.00	3.03	0.55	1.05	18.14	0.00	18.14	4.000	No	Yes	2.00
542	10.84	1.79	100.00	3.00	0.55	1.05	18.27	0.00	18.27	4.000	No	Yes	2.00
543	10.86	1.77	100.00	3.04	0.55	1.05	17.86	0.00	17.86	4.000	No	Yes	2.00
544	10.88	1.72	100.00	3.07	0.55	1.05	17.50	0.00	17.50	4.000	No	Yes	2.00
545	10.90	1.66	100.00	3.10	0.56	1.05	16.76	0.00	16.76	4.000	No	Yes	2.00
546	10.92	1.60	100.00	3.13	0.56	1.04	16.07	0.00	16.07	4.000	No	Yes	2.00
547	10.94	1.56	100.00	3.16	0.56	1.04	15.61	0.00	15.61	4.000	No	Yes	2.00
548	10.96	1.52	100.00	3.18	0.56	1.04	15.28	0.00	15.28	4.000	No	Yes	2.00
549	10.98	1.49	100.00	3.20	0.56	1.04	14.92	0.00	14.92	4.000	No	Yes	2.00
550	11.00	1.48	100.00	3.21	0.56	1.04	14.77	0.00	14.77	4.000	No	Yes	2.00
551	11.02	1.48	100.00	3.21	0.56	1.04	14.82	0.00	14.82	4.000	No	Yes	2.00
552	11.04	1.47	100.00	3.21	0.56	1.04	14.77	0.00	14.77	4.000	No	Yes	2.00
553	11.06	1.45	100.00	3.21	0.57	1.04	14.48	0.00	14.48	4.000	No	Yes	2.00
554	11.08	1.43	100.00	3.21	0.57	1.04	14.05	0.00	14.05	4.000	No	Yes	2.00
555	11.10	1.42	100.00	3.21	0.57	1.04	14.09	0.00	14.09	4.000	No	Yes	2.00
556	11.12	1.43	100.00	3.19	0.57	1.03	14.19	0.00	14.19	4.000	No	Yes	2.00
557	11.14	1.41	100.00	3.20	0.57	1.03	14.26	0.00	14.26	4.000	No	Yes	2.00
558	11.16	1.38	100.00	3.21	0.57	1.03	13.64	0.00	13.64	4.000	No	Yes	2.00
559	11.18	1.34	100.00	3.23	0.57	1.03	13.26	0.00	13.26	4.000	No	Yes	2.00
560	11.20	1.30	100.00	3.25	0.57	1.03	12.84	0.00	12.84	4.000	No	Yes	2.00
561	11.22	1.28	100.00	3.25	0.57	1.03	12.46	0.00	12.46	4.000	No	Yes	2.00
562	11.24	1.28	100.00	3.25	0.57	1.03	12.68	0.00	12.68	4.000	No	Yes	2.00
563	11.26	1.28	100.00	3.24	0.57	1.03	12.62	0.00	12.62	4.000	No	Yes	2.00
564	11.28	1.29	100.00	3.23	0.57	1.03	12.51	0.00	12.51	4.000	No	Yes	2.00
565	11.30	1.31	100.00	3.20	0.57	1.03	12.92	0.00	12.92	4.000	No	Yes	2.00
566	11.32	1.36	100.00	3.17	0.57	1.02	13.34	0.00	13.34	4.000	No	Yes	2.00
567	11.34	1.39	100.00	3.15	0.57	1.02	13.73	0.00	13.73	4.000	No	Yes	2.00
568	11.36	1.42	100.00	3.13	0.57	1.02	13.87	0.00	13.87	4.000	No	Yes	2.00
569	11.38	1.45	100.00	3.11	0.57	1.02	14.17	0.00	14.17	4.000	No	Yes	2.00
570	11.40	1.47	100.00	3.10	0.56	1.02	14.60	0.00	14.60	4.000	No	Yes	2.00
571	11.42	1.46	100.00	3.12	0.56	1.02	14.63	0.00	14.63	4.000	No	Yes	2.00
572	11.44	1.43	100.00	3.14	0.57	1.02	13.79	0.00	13.79	4.000	No	Yes	2.00
573	11.46	1.38	100.00	3.17	0.57	1.02	13.68	0.00	13.68	4.000	No	Yes	2.00
574	11.48	1.36	100.00	3.18	0.57	1.02	12.96	0.00	12.96	4.000	No	Yes	2.00
575	11.50	1.34	100.00	3.18	0.57	1.02	13.06	0.00	13.06	4.000	No	Yes	2.00
576	11.52	1.35	100.00	3.16	0.57	1.01	13.12	0.00	13.12	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
577	11.54	1.40	100.00	3.13	0.57	1.01	13.34	0.00	13.34	4.000	No	Yes	2.00
578	11.56	1.46	100.00	3.08	0.57	1.01	14.39	0.00	14.39	4.000	No	Yes	2.00
579	11.58	1.54	100.00	3.04	0.56	1.01	15.05	0.00	15.05	4.000	No	Yes	2.00
580	11.60	1.57	100.00	3.02	0.56	1.01	15.51	0.00	15.51	4.000	No	Yes	2.00
581	11.62	1.56	100.00	3.02	0.56	1.01	15.24	0.00	15.24	4.000	No	Yes	2.00
582	11.64	1.53	100.00	3.05	0.56	1.01	14.88	0.00	14.88	4.000	No	Yes	2.00
583	11.66	1.49	100.00	3.07	0.57	1.01	14.40	0.00	14.40	4.000	No	Yes	2.00
584	11.68	1.45	100.00	3.11	0.57	1.01	14.18	0.00	14.18	4.000	No	Yes	2.00
585	11.70	1.43	100.00	3.13	0.57	1.01	13.59	0.00	13.59	4.000	No	Yes	2.00
586	11.72	1.40	100.00	3.15	0.57	1.00	13.62	0.00	13.62	4.000	No	Yes	2.00
587	11.74	1.39	100.00	3.15	0.57	1.00	13.38	0.00	13.38	4.000	No	Yes	2.00
588	11.76	1.36	100.00	3.16	0.57	1.00	13.18	0.00	13.18	4.000	No	Yes	2.00
589	11.78	1.33	100.00	3.17	0.57	1.00	12.80	0.00	12.80	4.000	No	Yes	2.00
590	11.80	1.33	100.00	3.17	0.57	1.00	12.53	0.00	12.53	4.000	No	Yes	2.00
591	11.82	1.34	100.00	3.16	0.57	1.00	13.18	0.00	13.18	4.000	No	Yes	2.00
592	11.84	1.35	100.00	3.16	0.57	1.00	13.00	0.00	13.00	4.000	No	Yes	2.00
593	11.86	1.35	100.00	3.16	0.57	1.00	12.85	0.00	12.85	4.000	No	Yes	2.00
594	11.88	1.36	100.00	3.14	0.57	1.00	13.09	0.00	13.09	4.000	No	Yes	2.00
595	11.90	1.37	100.00	3.13	0.57	1.00	13.19	0.00	13.19	4.000	No	Yes	2.00
596	11.92	1.37	100.00	3.12	0.57	1.00	13.04	0.00	13.04	4.000	No	Yes	2.00
597	11.94	1.35	100.00	3.12	0.57	0.99	13.02	0.00	13.02	4.000	No	Yes	2.00
598	11.96	1.34	100.00	3.12	0.57	0.99	12.68	0.00	12.68	4.000	No	Yes	2.00
599	11.98	1.32	100.00	3.12	0.57	0.99	12.74	0.00	12.74	4.000	No	Yes	2.00
600	12.00	1.28	100.00	3.14	0.57	0.99	12.45	0.00	12.45	4.000	No	Yes	2.00
601	12.02	1.20	100.00	3.20	0.58	0.99	11.49	0.00	11.49	4.000	No	Yes	2.00
602	12.04	1.12	100.00	3.27	0.58	0.99	10.40	0.00	10.40	4.000	No	Yes	2.00
603	12.06	1.06	100.00	3.32	0.58	0.99	9.96	0.00	9.96	4.000	No	Yes	2.00
604	12.08	1.02	100.00	3.35	0.58	0.99	9.61	0.00	9.61	4.000	No	Yes	2.00
605	12.10	0.98	100.00	3.38	0.59	0.99	9.24	0.00	9.24	4.000	No	Yes	2.00
606	12.13	0.97	100.00	3.39	0.59	0.99	8.96	0.00	8.96	4.000	No	Yes	2.00
607	12.14	0.96	100.00	3.40	0.59	0.99	9.16	0.00	9.16	4.000	No	Yes	2.00
608	12.17	0.94	100.00	3.40	0.59	0.98	8.81	0.00	8.81	4.000	No	Yes	2.00
609	12.18	0.90	100.00	3.43	0.59	0.98	8.37	0.00	8.37	4.000	No	Yes	2.00
610	12.20	0.86	100.00	3.45	0.59	0.98	7.96	0.00	7.96	4.000	No	Yes	2.00
611	12.22	0.84	100.00	3.46	0.59	0.98	7.76	0.00	7.76	4.000	No	Yes	2.00
612	12.24	0.83	100.00	3.46	0.59	0.98	7.73	0.00	7.73	4.000	No	Yes	2.00
613	12.26	0.83	100.00	3.44	0.59	0.98	7.65	0.00	7.65	4.000	No	Yes	2.00
614	12.29	0.86	100.00	3.41	0.59	0.98	7.87	0.00	7.87	4.000	No	Yes	2.00
615	12.30	0.89	100.00	3.37	0.59	0.98	8.36	0.00	8.36	4.000	No	Yes	2.00
616	12.32	0.93	100.00	3.33	0.59	0.98	8.58	0.00	8.58	4.000	No	Yes	2.00
617	12.34	0.97	100.00	3.29	0.59	0.98	9.16	0.00	9.16	4.000	No	Yes	2.00
618	12.36	0.99	100.00	3.27	0.58	0.98	9.44	0.00	9.44	4.000	No	Yes	2.00
619	12.38	0.98	100.00	3.27	0.59	0.98	9.06	0.00	9.06	4.000	No	Yes	2.00
620	12.40	0.96	100.00	3.27	0.59	0.97	8.78	0.00	8.78	4.000	No	Yes	2.00
621	12.42	0.95	100.00	3.27	0.59	0.97	8.91	0.00	8.91	4.000	No	Yes	2.00
622	12.44	0.93	100.00	3.27	0.59	0.97	8.68	0.00	8.68	4.000	No	Yes	2.00
623	12.46	0.90	100.00	3.30	0.59	0.97	8.39	0.00	8.39	4.000	No	Yes	2.00
624	12.48	0.84	100.00	3.36	0.59	0.97	7.78	0.00	7.78	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
625	12.50	0.77	100.00	3.45	0.59	0.97	7.04	0.00	7.04	4.000	No	Yes	2.00
626	12.52	0.73	100.00	3.49	0.60	0.97	6.41	0.00	6.41	4.000	No	Yes	2.00
627	12.54	0.70	100.00	3.50	0.60	0.97	6.61	0.00	6.61	4.000	No	Yes	2.00
628	12.56	0.70	100.00	3.48	0.60	0.97	6.21	0.00	6.21	4.000	No	Yes	2.00
629	12.58	0.69	100.00	3.47	0.60	0.97	6.23	0.00	6.23	4.000	No	Yes	2.00
630	12.60	0.70	100.00	3.43	0.60	0.97	6.45	0.00	6.45	4.000	No	Yes	2.00
631	12.62	0.72	100.00	3.39	0.60	0.97	6.58	0.00	6.58	4.000	No	Yes	2.00
632	12.64	0.72	100.00	3.38	0.60	0.96	6.67	0.00	6.67	4.000	No	Yes	2.00
633	12.66	0.70	100.00	3.38	0.60	0.96	6.32	0.00	6.32	4.000	No	Yes	2.00
634	12.68	0.69	100.00	3.39	0.60	0.96	6.18	0.00	6.18	4.000	No	Yes	2.00
635	12.70	0.69	100.00	3.37	0.60	0.96	6.25	0.00	6.25	4.000	No	Yes	2.00
636	12.72	0.70	100.00	3.34	0.60	0.96	6.29	0.00	6.29	4.000	No	Yes	2.00
637	12.74	0.73	100.00	3.30	0.60	0.96	6.45	0.00	6.45	4.000	No	Yes	2.00
638	12.76	0.77	100.00	3.23	0.59	0.96	6.98	0.00	6.98	4.000	No	Yes	2.00
639	12.78	0.84	100.00	3.17	0.59	0.96	7.62	0.00	7.62	4.000	No	Yes	2.00
640	12.80	0.88	100.00	3.15	0.59	0.96	8.26	0.00	8.26	4.000	No	Yes	2.00
641	12.82	0.91	100.00	3.16	0.59	0.96	8.13	0.00	8.13	4.000	No	Yes	2.00
642	12.84	0.91	100.00	3.17	0.59	0.96	8.30	0.00	8.30	4.000	No	Yes	2.00
643	12.86	0.91	100.00	3.19	0.59	0.96	8.28	0.00	8.28	4.000	No	Yes	2.00
644	12.88	0.90	100.00	3.21	0.59	0.96	8.05	0.00	8.05	4.000	No	Yes	2.00
645	12.90	0.89	100.00	3.24	0.59	0.96	8.13	0.00	8.13	4.000	No	Yes	2.00
646	12.92	0.90	100.00	3.25	0.59	0.96	8.02	0.00	8.02	4.000	No	Yes	2.00
647	12.94	0.90	100.00	3.26	0.59	0.96	8.12	0.00	8.12	4.000	No	Yes	2.00
648	12.96	0.91	100.00	3.26	0.59	0.95	8.20	0.00	8.20	4.000	No	Yes	2.00
649	12.98	0.92	100.00	3.26	0.59	0.95	8.40	0.00	8.40	4.000	No	Yes	2.00
650	13.00	0.92	100.00	3.27	0.59	0.95	8.34	0.00	8.34	4.000	No	Yes	2.00
651	13.02	0.92	100.00	3.28	0.59	0.95	8.21	0.00	8.21	4.000	No	Yes	2.00
652	13.04	0.92	100.00	3.28	0.59	0.95	8.31	0.00	8.31	4.000	No	Yes	2.00
653	13.06	0.91	100.00	3.29	0.59	0.95	8.15	0.00	8.15	4.000	No	Yes	2.00
654	13.08	0.88	100.00	3.32	0.59	0.95	8.03	0.00	8.03	4.000	No	Yes	2.00
655	13.10	0.85	100.00	3.36	0.59	0.95	7.50	0.00	7.50	4.000	No	Yes	2.00
656	13.12	0.81	100.00	3.40	0.59	0.95	7.21	0.00	7.21	4.000	No	Yes	2.00
657	13.14	0.78	100.00	3.43	0.59	0.95	6.92	0.00	6.92	4.000	No	Yes	2.00
658	13.16	0.76	100.00	3.45	0.60	0.95	6.70	0.00	6.70	4.000	No	Yes	2.00
659	13.19	0.74	100.00	3.45	0.60	0.95	6.60	0.00	6.60	4.000	No	Yes	2.00
660	13.20	0.72	100.00	3.46	0.60	0.95	6.47	0.00	6.47	4.000	No	Yes	2.00
661	13.22	0.70	100.00	3.47	0.60	0.94	6.14	0.00	6.14	4.000	No	Yes	2.00
662	13.24	0.68	100.00	3.48	0.60	0.94	5.93	0.00	5.93	4.000	No	Yes	2.00
663	13.26	0.68	100.00	3.46	0.60	0.94	5.93	0.00	5.93	4.000	No	Yes	2.00
664	13.28	0.69	100.00	3.42	0.60	0.94	5.99	0.00	5.99	4.000	No	Yes	2.00
665	13.30	0.69	100.00	3.38	0.60	0.94	6.16	0.00	6.16	4.000	No	Yes	2.00
666	13.32	0.71	100.00	3.35	0.60	0.94	6.11	0.00	6.11	4.000	No	Yes	2.00
667	13.34	0.74	100.00	3.29	0.60	0.94	6.26	0.00	6.26	4.000	No	Yes	2.00
668	13.36	0.81	100.00	3.21	0.59	0.94	7.19	0.00	7.19	4.000	No	Yes	2.00
669	13.38	0.89	100.00	3.11	0.59	0.94	7.81	0.00	7.81	4.000	No	Yes	2.00
670	13.40	0.97	100.00	3.06	0.59	0.94	8.63	0.00	8.63	4.000	No	Yes	2.00
671	13.42	1.05	100.00	3.02	0.58	0.94	9.39	0.00	9.39	4.000	No	Yes	2.00
672	13.44	1.11	100.00	3.02	0.58	0.94	9.92	0.00	9.92	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
673	13.46	1.14	100.00	3.04	0.58	0.94	10.40	0.00	10.40	4.000	No	Yes	2.00
674	13.48	1.13	100.00	3.09	0.58	0.94	10.17	0.00	10.17	4.000	No	Yes	2.00
675	13.50	1.08	100.00	3.17	0.58	0.94	9.67	0.00	9.67	4.000	No	Yes	2.00
676	13.52	1.03	100.00	3.25	0.59	0.94	8.90	0.00	8.90	4.000	No	Yes	2.00
677	13.54	1.01	100.00	3.28	0.59	0.93	8.68	0.00	8.68	4.000	No	Yes	2.00
678	13.56	1.03	100.00	3.27	0.59	0.93	9.17	0.00	9.17	4.000	No	Yes	2.00
679	13.58	1.05	100.00	3.25	0.59	0.93	9.29	0.00	9.29	4.000	No	Yes	2.00
680	13.60	1.05	100.00	3.25	0.59	0.93	9.22	0.00	9.22	4.000	No	Yes	2.00
681	13.62	1.05	100.00	3.23	0.59	0.93	9.21	0.00	9.21	4.000	No	Yes	2.00
682	13.64	1.06	100.00	3.21	0.58	0.93	9.31	0.00	9.31	4.000	No	Yes	2.00
683	13.66	1.07	100.00	3.19	0.58	0.93	9.46	0.00	9.46	4.000	No	Yes	2.00
684	13.68	1.09	100.00	3.18	0.58	0.93	9.62	0.00	9.62	4.000	No	Yes	2.00
685	13.70	1.10	100.00	3.19	0.58	0.93	9.70	0.00	9.70	4.000	No	Yes	2.00
686	13.72	1.11	100.00	3.21	0.58	0.93	9.75	0.00	9.75	4.000	No	Yes	2.00
687	13.74	1.11	100.00	3.23	0.58	0.93	9.87	0.00	9.87	4.000	No	Yes	2.00
688	13.76	1.11	100.00	3.24	0.58	0.93	9.75	0.00	9.75	4.000	No	Yes	2.00
689	13.78	1.12	100.00	3.26	0.58	0.93	9.76	0.00	9.76	4.000	No	Yes	2.00
690	13.80	1.13	100.00	3.27	0.58	0.93	9.93	0.00	9.93	4.000	No	Yes	2.00
691	13.82	1.14	100.00	3.27	0.58	0.93	9.96	0.00	9.96	4.000	No	Yes	2.00
692	13.84	1.16	100.00	3.26	0.58	0.92	10.04	0.00	10.04	4.000	No	Yes	2.00
693	13.86	1.18	100.00	3.25	0.58	0.92	10.40	0.00	10.40	4.000	No	Yes	2.00
694	13.88	1.19	100.00	3.25	0.58	0.92	10.47	0.00	10.47	4.000	No	Yes	2.00
695	13.90	1.20	100.00	3.24	0.58	0.92	10.44	0.00	10.44	4.000	No	Yes	2.00
696	13.92	1.19	100.00	3.25	0.58	0.92	10.52	0.00	10.52	4.000	No	Yes	2.00
697	13.94	1.19	100.00	3.25	0.58	0.92	10.27	0.00	10.27	4.000	No	Yes	2.00
698	13.96	1.18	100.00	3.25	0.58	0.92	10.28	0.00	10.28	4.000	No	Yes	2.00
699	13.98	1.19	100.00	3.23	0.58	0.92	10.42	0.00	10.42	4.000	No	Yes	2.00
700	14.00	1.23	100.00	3.20	0.58	0.92	10.58	0.00	10.58	4.000	No	Yes	2.00
701	14.02	1.27	100.00	3.17	0.58	0.92	11.25	0.00	11.25	4.000	No	Yes	2.00
702	14.04	1.31	100.00	3.14	0.58	0.92	11.48	0.00	11.48	4.000	No	Yes	2.00
703	14.06	1.34	100.00	3.13	0.58	0.92	11.64	0.00	11.64	4.000	No	Yes	2.00
704	14.08	1.37	100.00	3.12	0.57	0.92	12.05	0.00	12.05	4.000	No	Yes	2.00
705	14.10	1.38	100.00	3.13	0.57	0.92	12.19	0.00	12.19	4.000	No	Yes	2.00
706	14.12	1.39	100.00	3.14	0.58	0.92	11.86	0.00	11.86	4.000	No	Yes	2.00
707	14.14	1.41	100.00	3.15	0.57	0.92	12.34	0.00	12.34	4.000	No	Yes	2.00
708	14.16	1.44	100.00	3.15	0.57	0.91	12.66	0.00	12.66	4.000	No	Yes	2.00
709	14.18	1.45	100.00	3.16	0.57	0.91	12.59	0.00	12.59	4.000	No	Yes	2.00
710	14.20	1.44	100.00	3.18	0.57	0.91	12.57	0.00	12.57	4.000	No	Yes	2.00
711	14.22	1.45	100.00	3.19	0.57	0.91	12.56	0.00	12.56	4.000	No	Yes	2.00
712	14.24	1.45	100.00	3.19	0.57	0.91	12.69	0.00	12.69	4.000	No	Yes	2.00
713	14.26	1.45	100.00	3.19	0.57	0.91	12.57	0.00	12.57	4.000	No	Yes	2.00
714	14.28	1.45	100.00	3.19	0.57	0.91	12.65	0.00	12.65	4.000	No	Yes	2.00
715	14.30	1.46	100.00	3.19	0.57	0.91	12.68	0.00	12.68	4.000	No	Yes	2.00
716	14.32	1.47	100.00	3.18	0.57	0.91	12.75	0.00	12.75	4.000	No	Yes	2.00
717	14.34	1.46	100.00	3.18	0.57	0.91	12.75	0.00	12.75	4.000	No	Yes	2.00
718	14.36	1.45	100.00	3.19	0.57	0.91	12.52	0.00	12.52	4.000	No	Yes	2.00
719	14.38	1.42	100.00	3.20	0.57	0.91	12.32	0.00	12.32	4.000	No	Yes	2.00
720	14.40	1.40	100.00	3.21	0.57	0.91	11.96	0.00	11.96	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
721	14.42	1.40	100.00	3.22	0.57	0.90	12.12	0.00	12.12	4.000	No	Yes	2.00
722	14.44	1.40	100.00	3.22	0.57	0.90	12.08	0.00	12.08	4.000	No	Yes	2.00
723	14.46	1.38	100.00	3.22	0.57	0.90	11.96	0.00	11.96	4.000	No	Yes	2.00
724	14.48	1.37	100.00	3.23	0.58	0.90	11.76	0.00	11.76	4.000	No	Yes	2.00
725	14.50	1.38	100.00	3.22	0.58	0.90	11.72	0.00	11.72	4.000	No	Yes	2.00
726	14.52	1.39	100.00	3.21	0.57	0.90	12.11	0.00	12.11	4.000	No	Yes	2.00
727	14.54	1.39	100.00	3.21	0.57	0.90	11.91	0.00	11.91	4.000	No	Yes	2.00
728	14.56	1.39	100.00	3.21	0.58	0.90	11.85	0.00	11.85	4.000	No	Yes	2.00
729	14.58	1.38	100.00	3.22	0.57	0.90	11.99	0.00	11.99	4.000	No	Yes	2.00
730	14.60	1.38	100.00	3.22	0.58	0.90	11.68	0.00	11.68	4.000	No	Yes	2.00
731	14.62	1.37	100.00	3.23	0.58	0.90	11.73	0.00	11.73	4.000	No	Yes	2.00
732	14.64	1.38	100.00	3.22	0.58	0.90	11.83	0.00	11.83	4.000	No	Yes	2.00
733	14.66	1.39	100.00	3.21	0.57	0.90	11.92	0.00	11.92	4.000	No	Yes	2.00
734	14.68	1.39	100.00	3.22	0.57	0.90	11.99	0.00	11.99	4.000	No	Yes	2.00
735	14.70	1.37	100.00	3.24	0.58	0.89	11.65	0.00	11.65	4.000	No	Yes	2.00
736	14.72	1.34	100.00	3.25	0.58	0.89	11.30	0.00	11.30	4.000	No	Yes	2.00
737	14.74	1.35	100.00	3.26	0.58	0.89	11.34	0.00	11.34	4.000	No	Yes	2.00
738	14.76	1.14	100.00	3.31	0.58	0.89	11.70	0.00	11.70	4.000	No	Yes	2.00
739	14.78	1.20	100.00	3.26	0.60	0.89	5.69	0.00	5.69	4.000	No	Yes	2.00
740	14.80	1.26	100.00	3.21	0.57	0.89	12.91	0.00	12.91	4.000	No	Yes	2.00
741	14.82	1.58	100.00	3.11	0.57	0.89	13.26	0.00	13.26	4.000	No	Yes	2.00
742	14.84	1.66	100.00	3.06	0.57	0.89	13.96	0.00	13.96	4.000	No	Yes	2.00
743	14.86	1.78	100.00	3.01	0.56	0.89	15.11	0.00	15.11	4.000	No	Yes	2.00
744	14.88	1.88	100.00	2.97	0.56	0.89	16.32	0.00	16.32	4.000	No	Yes	2.00
745	14.90	1.94	99.26	2.95	0.56	0.89	16.47	0.00	16.47	4.000	No	Yes	2.00
746	14.92	1.98	99.07	2.95	0.56	0.89	16.81	0.00	16.81	4.000	No	Yes	2.00
747	14.94	2.08	97.57	2.93	0.56	0.89	17.32	0.00	17.32	4.000	No	Yes	2.00
748	14.96	2.13	97.78	2.93	0.55	0.89	19.21	0.00	19.21	4.000	No	Yes	2.00
749	14.98	2.17	98.77	2.95	0.55	0.89	18.21	0.00	18.21	4.000	No	Yes	2.00
750	15.00	2.09	100.00	2.99	0.55	0.89	18.18	0.00	18.18	4.000	No	Yes	2.00
751	15.02	2.03	100.00	3.04	0.56	0.89	17.16	0.00	17.16	4.000	No	Yes	2.00
752	15.04	1.91	100.00	3.10	0.56	0.89	16.68	0.00	16.68	4.000	No	Yes	2.00
753	15.06	1.80	100.00	3.16	0.56	0.89	15.22	0.00	15.22	4.000	No	Yes	2.00
754	15.08	1.68	100.00	3.23	0.57	0.88	14.11	0.00	14.11	4.000	No	Yes	2.00
755	15.10	1.60	100.00	3.28	0.57	0.88	13.47	0.00	13.47	4.000	No	Yes	2.00
756	15.12	1.54	100.00	3.31	0.57	0.88	13.08	0.00	13.08	4.000	No	Yes	2.00
757	15.14	1.50	100.00	3.33	0.57	0.88	12.65	0.00	12.65	4.000	No	Yes	2.00
758	15.16	1.47	100.00	3.34	0.57	0.88	12.21	0.00	12.21	4.000	No	Yes	2.00
759	15.18	1.48	100.00	3.33	0.57	0.88	12.27	0.00	12.27	4.000	No	Yes	2.00
760	15.20	1.50	100.00	3.31	0.57	0.88	12.60	0.00	12.60	4.000	No	Yes	2.00
761	15.22	1.53	100.00	3.27	0.57	0.88	12.72	0.00	12.72	4.000	No	Yes	2.00
762	15.24	1.57	100.00	3.23	0.57	0.88	12.99	0.00	12.99	4.000	No	Yes	2.00
763	15.26	1.60	100.00	3.19	0.57	0.88	13.48	0.00	13.48	4.000	No	Yes	2.00
764	15.28	1.61	100.00	3.17	0.57	0.88	13.53	0.00	13.53	4.000	No	Yes	2.00
765	15.30	1.59	100.00	3.17	0.57	0.88	13.31	0.00	13.31	4.000	No	Yes	2.00
766	15.32	1.56	100.00	3.18	0.57	0.87	12.97	0.00	12.97	4.000	No	Yes	2.00
767	15.34	1.54	100.00	3.19	0.57	0.87	12.65	0.00	12.65	4.000	No	Yes	2.00
768	15.36	1.52	100.00	3.20	0.57	0.87	12.78	0.00	12.78	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
769	15.38	1.50	100.00	3.21	0.57	0.87	12.48	0.00	12.48	4.000	No	Yes	2.00
770	15.40	1.45	100.00	3.25	0.57	0.87	12.13	0.00	12.13	4.000	No	Yes	2.00
771	15.42	1.37	100.00	3.28	0.58	0.87	11.38	0.00	11.38	4.000	No	Yes	2.00
772	15.44	1.28	100.00	3.33	0.58	0.87	10.52	0.00	10.52	4.000	No	Yes	2.00
773	15.46	1.20	100.00	3.36	0.58	0.87	9.65	0.00	9.65	4.000	No	Yes	2.00
774	15.48	1.14	100.00	3.39	0.58	0.87	9.44	0.00	9.44	4.000	No	Yes	2.00
775	15.50	1.09	100.00	3.42	0.59	0.87	8.92	0.00	8.92	4.000	No	Yes	2.00
776	15.52	1.03	100.00	3.45	0.59	0.86	8.31	0.00	8.31	4.000	No	Yes	2.00
777	15.54	0.99	100.00	3.48	0.59	0.86	7.94	0.00	7.94	4.000	No	Yes	2.00
778	15.56	0.94	100.00	3.49	0.59	0.86	7.66	0.00	7.66	4.000	No	Yes	2.00
779	15.58	0.91	100.00	3.51	0.59	0.86	7.21	0.00	7.21	4.000	No	Yes	2.00
780	15.60	0.89	100.00	3.51	0.59	0.86	7.01	0.00	7.01	4.000	No	Yes	2.00
781	15.62	0.90	100.00	3.47	0.59	0.86	7.23	0.00	7.23	4.000	No	Yes	2.00
782	15.64	0.94	100.00	3.40	0.59	0.86	7.41	0.00	7.41	4.000	No	Yes	2.00
783	15.66	1.00	100.00	3.31	0.59	0.86	7.95	0.00	7.95	4.000	No	Yes	2.00
784	15.68	1.08	100.00	3.22	0.59	0.86	8.76	0.00	8.76	4.000	No	Yes	2.00
785	15.70	1.18	100.00	3.14	0.58	0.86	9.44	0.00	9.44	4.000	No	Yes	2.00
786	15.72	1.27	100.00	3.08	0.58	0.86	10.37	0.00	10.37	4.000	No	Yes	2.00
787	15.74	1.34	100.00	3.04	0.58	0.86	10.97	0.00	10.97	4.000	No	Yes	2.00
788	15.76	1.21	100.00	3.11	0.58	0.86	11.17	0.00	11.17	4.000	No	Yes	2.00
789	15.78	1.20	100.00	3.14	0.59	0.86	7.18	0.00	7.18	4.000	No	Yes	2.00
790	15.80	1.18	100.00	3.18	0.58	0.86	10.71	0.00	10.71	4.000	No	Yes	2.00
791	15.82	1.31	100.00	3.15	0.58	0.86	10.68	0.00	10.68	4.000	No	Yes	2.00
792	15.85	1.29	100.00	3.20	0.58	0.86	10.49	0.00	10.49	4.000	No	Yes	2.00
793	15.86	1.25	100.00	3.25	0.58	0.86	10.07	0.00	10.07	4.000	No	Yes	2.00
794	15.88	1.23	100.00	3.29	0.58	0.86	9.76	0.00	9.76	4.000	No	Yes	2.00
795	15.90	1.21	100.00	3.30	0.58	0.85	9.69	0.00	9.69	4.000	No	Yes	2.00
796	15.92	1.19	100.00	3.29	0.58	0.85	9.54	0.00	9.54	4.000	No	Yes	2.00
797	15.94	1.18	100.00	3.29	0.58	0.85	9.42	0.00	9.42	4.000	No	Yes	2.00
798	15.96	1.17	100.00	3.27	0.59	0.85	9.21	0.00	9.21	4.000	No	Yes	2.00
799	15.98	1.18	100.00	3.25	0.58	0.85	9.40	0.00	9.40	4.000	No	Yes	2.00
800	16.00	1.22	100.00	3.20	0.58	0.85	9.49	0.00	9.49	4.000	No	Yes	2.00
801	16.02	1.28	100.00	3.16	0.58	0.85	10.31	0.00	10.31	4.000	No	Yes	2.00
802	16.04	1.35	100.00	3.12	0.58	0.85	10.90	0.00	10.90	4.000	No	Yes	2.00
803	16.06	1.38	100.00	3.10	0.58	0.85	11.13	0.00	11.13	4.000	No	Yes	2.00
804	16.08	1.38	100.00	3.11	0.58	0.85	11.14	0.00	11.14	4.000	No	Yes	2.00
805	16.10	1.33	100.00	3.15	0.58	0.85	10.84	0.00	10.84	4.000	No	Yes	2.00
806	16.12	1.26	100.00	3.22	0.58	0.85	9.95	0.00	9.95	4.000	No	Yes	2.00
807	16.14	1.17	100.00	3.30	0.59	0.85	9.25	0.00	9.25	4.000	No	Yes	2.00
808	16.16	1.11	100.00	3.36	0.59	0.85	8.67	0.00	8.67	4.000	No	Yes	2.00
809	16.18	1.09	100.00	3.38	0.59	0.85	8.44	0.00	8.44	4.000	No	Yes	2.00
810	16.20	1.10	100.00	3.37	0.59	0.85	8.67	0.00	8.67	4.000	No	Yes	2.00
811	16.22	1.11	100.00	3.35	0.59	0.84	8.86	0.00	8.86	4.000	No	Yes	2.00
812	16.24	1.11	100.00	3.34	0.59	0.84	8.70	0.00	8.70	4.000	No	Yes	2.00
813	16.26	1.09	100.00	3.32	0.59	0.84	8.42	0.00	8.42	4.000	No	Yes	2.00
814	16.28	1.09	100.00	3.28	0.59	0.84	8.43	0.00	8.43	4.000	No	Yes	2.00
815	16.30	1.14	100.00	3.22	0.59	0.84	8.64	0.00	8.64	4.000	No	Yes	2.00
816	16.32	1.24	100.00	3.13	0.58	0.84	9.62	0.00	9.62	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
817	16.34	1.36	100.00	3.04	0.58	0.84	10.80	0.00	10.80	4.000	No	Yes	2.00
818	16.36	1.45	100.00	3.01	0.58	0.84	11.73	0.00	11.73	4.000	No	Yes	2.00
819	16.38	1.47	100.00	3.02	0.58	0.84	11.70	0.00	11.70	4.000	No	Yes	2.00
820	16.40	1.42	100.00	3.06	0.58	0.84	11.34	0.00	11.34	4.000	No	Yes	2.00
821	16.42	1.35	100.00	3.12	0.58	0.84	10.58	0.00	10.58	4.000	No	Yes	2.00
822	16.44	1.26	100.00	3.19	0.58	0.84	9.92	0.00	9.92	4.000	No	Yes	2.00
823	16.46	1.19	100.00	3.26	0.59	0.84	9.27	0.00	9.27	4.000	No	Yes	2.00
824	16.48	1.14	100.00	3.32	0.59	0.84	8.71	0.00	8.71	4.000	No	Yes	2.00
825	16.50	1.13	100.00	3.34	0.59	0.84	8.71	0.00	8.71	4.000	No	Yes	2.00
826	16.52	1.13	100.00	3.33	0.59	0.84	8.77	0.00	8.77	4.000	No	Yes	2.00
827	16.54	1.12	100.00	3.32	0.59	0.84	8.70	0.00	8.70	4.000	No	Yes	2.00
828	16.56	1.13	100.00	3.30	0.59	0.84	8.58	0.00	8.58	4.000	No	Yes	2.00
829	16.58	1.14	100.00	3.27	0.59	0.84	8.94	0.00	8.94	4.000	No	Yes	2.00
830	16.60	1.16	100.00	3.23	0.59	0.83	8.98	0.00	8.98	4.000	No	Yes	2.00
831	16.62	1.16	100.00	3.21	0.59	0.83	9.01	0.00	9.01	4.000	No	Yes	2.00
832	16.64	1.16	100.00	3.20	0.59	0.83	8.93	0.00	8.93	4.000	No	Yes	2.00
833	16.66	1.14	100.00	3.20	0.59	0.83	8.83	0.00	8.83	4.000	No	Yes	2.00
834	16.68	1.14	100.00	3.19	0.59	0.83	8.67	0.00	8.67	4.000	No	Yes	2.00
835	16.70	1.15	100.00	3.17	0.59	0.83	8.84	0.00	8.84	4.000	No	Yes	2.00
836	16.72	1.20	100.00	3.13	0.59	0.83	9.01	0.00	9.01	4.000	No	Yes	2.00
837	16.74	1.28	100.00	3.07	0.58	0.83	9.88	0.00	9.88	4.000	No	Yes	2.00
838	16.76	1.40	100.00	3.02	0.58	0.83	10.62	0.00	10.62	4.000	No	Yes	2.00
839	16.79	1.49	100.00	3.01	0.57	0.83	11.94	0.00	11.94	4.000	No	Yes	2.00
840	16.80	1.51	100.00	3.04	0.57	0.83	12.03	0.00	12.03	4.000	No	Yes	2.00
841	16.82	1.48	100.00	3.07	0.58	0.83	11.18	0.00	11.18	4.000	No	Yes	2.00
842	16.84	1.44	100.00	3.10	0.58	0.83	11.12	0.00	11.12	4.000	No	Yes	2.00
843	16.86	1.45	100.00	3.11	0.58	0.83	11.21	0.00	11.21	4.000	No	Yes	2.00

Abbreviations

Depth: Depth from free surface, at which CPT was performed (m)
q_t: Total cone resistance
FC: Fines content (%)
I_c: Soil behavior type index
m: Stress exponent
C_N: Overburden correction factor
q_{c1N}: Normalized and adjusted cone resistance
Δq_{c1N}: Cone resistance correction factor due to fines
$q_{c1N,cs}$: Normalized and adjusted cone resistance
$CRR_{7.5}$: Cyclic resistance ratio for M_w=7.5
FS: Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
0.02	2.00	0.00	9.99	0.02	0.00	0.04	2.00	0.00	9.98	0.02	0.00
0.06	2.00	0.00	9.97	0.02	0.00	0.08	2.00	0.00	9.96	0.02	0.00
0.10	2.00	0.00	9.95	0.02	0.00	0.12	2.00	0.00	9.94	0.02	0.00
0.14	2.00	0.00	9.93	0.02	0.00	0.17	2.00	0.00	9.91	0.03	0.00
0.18	2.00	0.00	9.91	0.01	0.00	0.20	2.00	0.00	9.90	0.02	0.00
0.23	2.00	0.00	9.89	0.03	0.00	0.24	2.00	0.00	9.88	0.01	0.00
0.26	2.00	0.00	9.87	0.02	0.00	0.29	2.00	0.00	9.86	0.03	0.00
0.30	2.00	0.00	9.85	0.01	0.00	0.32	2.00	0.00	9.84	0.02	0.00
0.34	2.00	0.00	9.83	0.02	0.00	0.36	2.00	0.00	9.82	0.02	0.00
0.38	2.00	0.00	9.81	0.02	0.00	0.40	2.00	0.00	9.80	0.02	0.00
0.42	2.00	0.00	9.79	0.02	0.00	0.44	2.00	0.00	9.78	0.02	0.00
0.46	2.00	0.00	9.77	0.02	0.00	0.48	2.00	0.00	9.76	0.02	0.00
0.50	2.00	0.00	9.75	0.02	0.00	0.53	2.00	0.00	9.74	0.03	0.00
0.54	2.00	0.00	9.73	0.01	0.00	0.56	2.00	0.00	9.72	0.02	0.00
0.58	2.00	0.00	9.71	0.02	0.00	0.60	2.00	0.00	9.70	0.02	0.00
0.62	2.00	0.00	9.69	0.02	0.00	0.64	2.00	0.00	9.68	0.02	0.00
0.66	2.00	0.00	9.67	0.02	0.00	0.68	2.00	0.00	9.66	0.02	0.00
0.70	2.00	0.00	9.65	0.02	0.00	0.72	2.00	0.00	9.64	0.02	0.00
0.74	2.00	0.00	9.63	0.02	0.00	0.76	2.00	0.00	9.62	0.02	0.00
0.78	2.00	0.00	9.61	0.02	0.00	0.80	2.00	0.00	9.60	0.02	0.00
0.82	2.00	0.00	9.59	0.02	0.00	0.84	2.00	0.00	9.58	0.02	0.00
0.86	2.00	0.00	9.57	0.02	0.00	0.88	2.00	0.00	9.56	0.02	0.00
0.90	2.00	0.00	9.55	0.02	0.00	0.92	2.00	0.00	9.54	0.02	0.00
0.94	2.00	0.00	9.53	0.02	0.00	0.96	2.00	0.00	9.52	0.02	0.00
0.98	2.00	0.00	9.51	0.02	0.00	1.00	2.00	0.00	9.50	0.02	0.00
1.02	2.00	0.00	9.49	0.02	0.00	1.04	2.00	0.00	9.48	0.02	0.00
1.07	2.00	0.00	9.47	0.03	0.00	1.08	2.00	0.00	9.46	0.01	0.00
1.10	2.00	0.00	9.45	0.02	0.00	1.12	2.00	0.00	9.44	0.02	0.00
1.14	2.00	0.00	9.43	0.02	0.00	1.16	2.00	0.00	9.42	0.02	0.00
1.18	2.00	0.00	9.41	0.02	0.00	1.20	2.00	0.00	9.40	0.02	0.00
1.22	2.00	0.00	9.39	0.02	0.00	1.24	2.00	0.00	9.38	0.02	0.00
1.26	2.00	0.00	9.37	0.02	0.00	1.28	2.00	0.00	9.36	0.02	0.00
1.30	2.00	0.00	9.35	0.02	0.00	1.32	2.00	0.00	9.34	0.02	0.00
1.34	2.00	0.00	9.33	0.02	0.00	1.36	2.00	0.00	9.32	0.02	0.00
1.38	2.00	0.00	9.31	0.02	0.00	1.40	2.00	0.00	9.30	0.02	0.00
1.42	2.00	0.00	9.29	0.02	0.00	1.44	2.00	0.00	9.28	0.02	0.00
1.46	2.00	0.00	9.27	0.02	0.00	1.48	2.00	0.00	9.26	0.02	0.00
1.50	2.00	0.00	9.25	0.02	0.00	1.52	2.00	0.00	9.24	0.02	0.00
1.54	2.00	0.00	9.23	0.02	0.00	1.56	2.00	0.00	9.22	0.02	0.00
1.58	2.00	0.00	9.21	0.02	0.00	1.60	2.00	0.00	9.20	0.02	0.00
1.62	2.00	0.00	9.19	0.02	0.00	1.64	2.00	0.00	9.18	0.02	0.00
1.66	2.00	0.00	9.17	0.02	0.00	1.68	2.00	0.00	9.16	0.02	0.00
1.70	2.00	0.00	9.15	0.02	0.00	1.72	2.00	0.00	9.14	0.02	0.00
1.74	2.00	0.00	9.13	0.02	0.00	1.76	2.00	0.00	9.12	0.02	0.00
1.78	2.00	0.00	9.11	0.02	0.00	1.80	2.00	0.00	9.10	0.02	0.00
1.82	2.00	0.00	9.09	0.02	0.00	1.84	2.00	0.00	9.08	0.02	0.00
1.86	2.00	0.00	9.07	0.02	0.00	1.88	2.00	0.00	9.06	0.02	0.00
1.90	2.00	0.00	9.05	0.02	0.00	1.92	2.00	0.00	9.04	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
1.94	2.00	0.00	9.03	0.02	0.00	1.96	2.00	0.00	9.02	0.02	0.00
1.98	2.00	0.00	9.01	0.02	0.00	2.01	2.00	0.00	8.99	0.03	0.00
2.02	2.00	0.00	8.99	0.01	0.00	2.04	2.00	0.00	8.98	0.02	0.00
2.06	2.00	0.00	8.97	0.02	0.00	2.08	2.00	0.00	8.96	0.02	0.00
2.10	2.00	0.00	8.95	0.02	0.00	2.12	2.00	0.00	8.94	0.02	0.00
2.14	2.00	0.00	8.93	0.02	0.00	2.16	2.00	0.00	8.92	0.02	0.00
2.18	2.00	0.00	8.91	0.02	0.00	2.20	2.00	0.00	8.90	0.02	0.00
2.22	2.00	0.00	8.89	0.02	0.00	2.24	2.00	0.00	8.88	0.02	0.00
2.26	2.00	0.00	8.87	0.02	0.00	2.28	2.00	0.00	8.86	0.02	0.00
2.30	2.00	0.00	8.85	0.02	0.00	2.32	2.00	0.00	8.84	0.02	0.00
2.34	2.00	0.00	8.83	0.02	0.00	2.36	2.00	0.00	8.82	0.02	0.00
2.38	2.00	0.00	8.81	0.02	0.00	2.40	2.00	0.00	8.80	0.02	0.00
2.42	2.00	0.00	8.79	0.02	0.00	2.44	2.00	0.00	8.78	0.02	0.00
2.46	2.00	0.00	8.77	0.02	0.00	2.48	2.00	0.00	8.76	0.02	0.00
2.50	2.00	0.00	8.75	0.02	0.00	2.52	2.00	0.00	8.74	0.02	0.00
2.54	2.00	0.00	8.73	0.02	0.00	2.56	2.00	0.00	8.72	0.02	0.00
2.58	2.00	0.00	8.71	0.02	0.00	2.60	2.00	0.00	8.70	0.02	0.00
2.62	2.00	0.00	8.69	0.02	0.00	2.64	2.00	0.00	8.68	0.02	0.00
2.66	2.00	0.00	8.67	0.02	0.00	2.68	2.00	0.00	8.66	0.02	0.00
2.70	2.00	0.00	8.65	0.02	0.00	2.72	2.00	0.00	8.64	0.02	0.00
2.74	2.00	0.00	8.63	0.02	0.00	2.76	2.00	0.00	8.62	0.02	0.00
2.78	2.00	0.00	8.61	0.02	0.00	2.80	2.00	0.00	8.60	0.02	0.00
2.82	2.00	0.00	8.59	0.02	0.00	2.84	2.00	0.00	8.58	0.02	0.00
2.86	2.00	0.00	8.57	0.02	0.00	2.88	2.00	0.00	8.56	0.02	0.00
2.90	2.00	0.00	8.55	0.02	0.00	2.92	2.00	0.00	8.54	0.02	0.00
2.94	2.00	0.00	8.53	0.02	0.00	2.96	2.00	0.00	8.52	0.02	0.00
2.98	2.00	0.00	8.51	0.02	0.00	3.00	2.00	0.00	8.50	0.02	0.00
3.02	2.00	0.00	8.49	0.02	0.00	3.04	2.00	0.00	8.48	0.02	0.00
3.06	2.00	0.00	8.47	0.02	0.00	3.08	2.00	0.00	8.46	0.02	0.00
3.10	2.00	0.00	8.45	0.02	0.00	3.12	2.00	0.00	8.44	0.02	0.00
3.14	2.00	0.00	8.43	0.02	0.00	3.16	2.00	0.00	8.42	0.02	0.00
3.18	2.00	0.00	8.41	0.02	0.00	3.20	2.00	0.00	8.40	0.02	0.00
3.22	2.00	0.00	8.39	0.02	0.00	3.24	2.00	0.00	8.38	0.02	0.00
3.26	2.00	0.00	8.37	0.02	0.00	3.28	2.00	0.00	8.36	0.02	0.00
3.30	2.00	0.00	8.35	0.02	0.00	3.32	2.00	0.00	8.34	0.02	0.00
3.34	2.00	0.00	8.33	0.02	0.00	3.36	2.00	0.00	8.32	0.02	0.00
3.38	2.00	0.00	8.31	0.02	0.00	3.40	2.00	0.00	8.30	0.02	0.00
3.42	2.00	0.00	8.29	0.02	0.00	3.44	2.00	0.00	8.28	0.02	0.00
3.46	2.00	0.00	8.27	0.02	0.00	3.48	2.00	0.00	8.26	0.02	0.00
3.50	2.00	0.00	8.25	0.02	0.00	3.52	2.00	0.00	8.24	0.02	0.00
3.54	2.00	0.00	8.23	0.02	0.00	3.56	2.00	0.00	8.22	0.02	0.00
3.58	2.00	0.00	8.21	0.02	0.00	3.60	2.00	0.00	8.20	0.02	0.00
3.62	2.00	0.00	8.19	0.02	0.00	3.64	2.00	0.00	8.18	0.02	0.00
3.66	2.00	0.00	8.17	0.02	0.00	3.68	2.00	0.00	8.16	0.02	0.00
3.70	2.00	0.00	8.15	0.02	0.00	3.72	2.00	0.00	8.14	0.02	0.00
3.74	2.00	0.00	8.13	0.02	0.00	3.76	2.00	0.00	8.12	0.02	0.00
3.78	2.00	0.00	8.11	0.02	0.00	3.80	2.00	0.00	8.10	0.02	0.00
3.82	2.00	0.00	8.09	0.02	0.00	3.84	2.00	0.00	8.08	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
3.86	2.00	0.00	8.07	0.02	0.00	3.88	2.00	0.00	8.06	0.02	0.00
3.90	2.00	0.00	8.05	0.02	0.00	3.92	2.00	0.00	8.04	0.02	0.00
3.94	2.00	0.00	8.03	0.02	0.00	3.96	2.00	0.00	8.02	0.02	0.00
3.98	2.00	0.00	8.01	0.02	0.00	4.00	2.00	0.00	8.00	0.02	0.00
4.02	2.00	0.00	7.99	0.02	0.00	4.05	2.00	0.00	7.98	0.03	0.00
4.06	2.00	0.00	7.97	0.01	0.00	4.08	2.00	0.00	7.96	0.02	0.00
4.10	2.00	0.00	7.95	0.02	0.00	4.12	2.00	0.00	7.94	0.02	0.00
4.14	2.00	0.00	7.93	0.02	0.00	4.16	2.00	0.00	7.92	0.02	0.00
4.18	2.00	0.00	7.91	0.02	0.00	4.20	2.00	0.00	7.90	0.02	0.00
4.22	2.00	0.00	7.89	0.02	0.00	4.24	2.00	0.00	7.88	0.02	0.00
4.26	2.00	0.00	7.87	0.02	0.00	4.28	2.00	0.00	7.86	0.02	0.00
4.30	2.00	0.00	7.85	0.02	0.00	4.32	2.00	0.00	7.84	0.02	0.00
4.34	2.00	0.00	7.83	0.02	0.00	4.36	2.00	0.00	7.82	0.02	0.00
4.38	2.00	0.00	7.81	0.02	0.00	4.40	2.00	0.00	7.80	0.02	0.00
4.42	2.00	0.00	7.79	0.02	0.00	4.44	2.00	0.00	7.78	0.02	0.00
4.46	2.00	0.00	7.77	0.02	0.00	4.48	2.00	0.00	7.76	0.02	0.00
4.50	2.00	0.00	7.75	0.02	0.00	4.52	2.00	0.00	7.74	0.02	0.00
4.54	2.00	0.00	7.73	0.02	0.00	4.56	2.00	0.00	7.72	0.02	0.00
4.58	2.00	0.00	7.71	0.02	0.00	4.60	2.00	0.00	7.70	0.02	0.00
4.62	2.00	0.00	7.69	0.02	0.00	4.64	2.00	0.00	7.68	0.02	0.00
4.66	2.00	0.00	7.67	0.02	0.00	4.68	2.00	0.00	7.66	0.02	0.00
4.70	2.00	0.00	7.65	0.02	0.00	4.72	2.00	0.00	7.64	0.02	0.00
4.74	2.00	0.00	7.63	0.02	0.00	4.76	2.00	0.00	7.62	0.02	0.00
4.78	2.00	0.00	7.61	0.02	0.00	4.80	2.00	0.00	7.60	0.02	0.00
4.82	2.00	0.00	7.59	0.02	0.00	4.84	2.00	0.00	7.58	0.02	0.00
4.86	2.00	0.00	7.57	0.02	0.00	4.88	2.00	0.00	7.56	0.02	0.00
4.91	2.00	0.00	7.55	0.03	0.00	4.92	2.00	0.00	7.54	0.01	0.00
4.94	2.00	0.00	7.53	0.02	0.00	4.96	2.00	0.00	7.52	0.02	0.00
4.98	2.00	0.00	7.51	0.02	0.00	5.00	2.00	0.00	7.50	0.02	0.00
5.02	2.00	0.00	7.49	0.02	0.00	5.04	2.00	0.00	7.48	0.02	0.00
5.06	2.00	0.00	7.47	0.02	0.00	5.08	2.00	0.00	7.46	0.02	0.00
5.10	2.00	0.00	7.45	0.02	0.00	5.12	2.00	0.00	7.44	0.02	0.00
5.14	2.00	0.00	7.43	0.02	0.00	5.16	2.00	0.00	7.42	0.02	0.00
5.18	2.00	0.00	7.41	0.02	0.00	5.20	2.00	0.00	7.40	0.02	0.00
5.22	2.00	0.00	7.39	0.02	0.00	5.24	2.00	0.00	7.38	0.02	0.00
5.26	2.00	0.00	7.37	0.02	0.00	5.28	2.00	0.00	7.36	0.02	0.00
5.30	2.00	0.00	7.35	0.02	0.00	5.32	2.00	0.00	7.34	0.02	0.00
5.34	2.00	0.00	7.33	0.02	0.00	5.36	2.00	0.00	7.32	0.02	0.00
5.38	2.00	0.00	7.31	0.02	0.00	5.40	2.00	0.00	7.30	0.02	0.00
5.42	2.00	0.00	7.29	0.02	0.00	5.44	2.00	0.00	7.28	0.02	0.00
5.46	2.00	0.00	7.27	0.02	0.00	5.48	2.00	0.00	7.26	0.02	0.00
5.50	2.00	0.00	7.25	0.02	0.00	5.52	2.00	0.00	7.24	0.02	0.00
5.54	2.00	0.00	7.23	0.02	0.00	5.56	2.00	0.00	7.22	0.02	0.00
5.58	2.00	0.00	7.21	0.02	0.00	5.60	2.00	0.00	7.20	0.02	0.00
5.62	2.00	0.00	7.19	0.02	0.00	5.64	2.00	0.00	7.18	0.02	0.00
5.66	2.00	0.00	7.17	0.02	0.00	5.68	2.00	0.00	7.16	0.02	0.00
5.70	2.00	0.00	7.15	0.02	0.00	5.72	2.00	0.00	7.14	0.02	0.00
5.74	2.00	0.00	7.13	0.02	0.00	5.76	2.00	0.00	7.12	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
5.78	2.00	0.00	7.11	0.02	0.00	5.80	2.00	0.00	7.10	0.02	0.00
5.82	2.00	0.00	7.09	0.02	0.00	5.84	2.00	0.00	7.08	0.02	0.00
5.86	2.00	0.00	7.07	0.02	0.00	5.88	2.00	0.00	7.06	0.02	0.00
5.90	2.00	0.00	7.05	0.02	0.00	5.92	2.00	0.00	7.04	0.02	0.00
5.94	2.00	0.00	7.03	0.02	0.00	5.96	2.00	0.00	7.02	0.02	0.00
5.98	2.00	0.00	7.01	0.02	0.00	6.00	2.00	0.00	7.00	0.02	0.00
6.02	2.00	0.00	6.99	0.02	0.00	6.04	2.00	0.00	6.98	0.02	0.00
6.06	2.00	0.00	6.97	0.02	0.00	6.08	2.00	0.00	6.96	0.02	0.00
6.10	2.00	0.00	6.95	0.02	0.00	6.12	2.00	0.00	6.94	0.02	0.00
6.14	2.00	0.00	6.93	0.02	0.00	6.16	2.00	0.00	6.92	0.02	0.00
6.18	2.00	0.00	6.91	0.02	0.00	6.20	2.00	0.00	6.90	0.02	0.00
6.22	2.00	0.00	6.89	0.02	0.00	6.24	2.00	0.00	6.88	0.02	0.00
6.26	2.00	0.00	6.87	0.02	0.00	6.28	2.00	0.00	6.86	0.02	0.00
6.30	2.00	0.00	6.85	0.02	0.00	6.32	2.00	0.00	6.84	0.02	0.00
6.34	2.00	0.00	6.83	0.02	0.00	6.36	2.00	0.00	6.82	0.02	0.00
6.38	2.00	0.00	6.81	0.02	0.00	6.40	2.00	0.00	6.80	0.02	0.00
6.42	2.00	0.00	6.79	0.02	0.00	6.44	2.00	0.00	6.78	0.02	0.00
6.46	2.00	0.00	6.77	0.02	0.00	6.48	2.00	0.00	6.76	0.02	0.00
6.50	2.00	0.00	6.75	0.02	0.00	6.52	2.00	0.00	6.74	0.02	0.00
6.54	2.00	0.00	6.73	0.02	0.00	6.56	2.00	0.00	6.72	0.02	0.00
6.58	2.00	0.00	6.71	0.02	0.00	6.60	2.00	0.00	6.70	0.02	0.00
6.62	2.00	0.00	6.69	0.02	0.00	6.64	2.00	0.00	6.68	0.02	0.00
6.66	2.00	0.00	6.67	0.02	0.00	6.68	2.00	0.00	6.66	0.02	0.00
6.70	2.00	0.00	6.65	0.02	0.00	6.72	2.00	0.00	6.64	0.02	0.00
6.74	2.00	0.00	6.63	0.02	0.00	6.76	2.00	0.00	6.62	0.02	0.00
6.78	2.00	0.00	6.61	0.02	0.00	6.80	2.00	0.00	6.60	0.02	0.00
6.82	2.00	0.00	6.59	0.02	0.00	6.84	2.00	0.00	6.58	0.02	0.00
6.86	2.00	0.00	6.57	0.02	0.00	6.88	2.00	0.00	6.56	0.02	0.00
6.90	2.00	0.00	6.55	0.02	0.00	6.92	2.00	0.00	6.54	0.02	0.00
6.94	2.00	0.00	6.53	0.02	0.00	6.96	2.00	0.00	6.52	0.02	0.00
6.98	2.00	0.00	6.51	0.02	0.00	7.00	2.00	0.00	6.50	0.02	0.00
7.02	2.00	0.00	6.49	0.02	0.00	7.04	2.00	0.00	6.48	0.02	0.00
7.06	2.00	0.00	6.47	0.02	0.00	7.08	2.00	0.00	6.46	0.02	0.00
7.10	2.00	0.00	6.45	0.02	0.00	7.12	2.00	0.00	6.44	0.02	0.00
7.14	2.00	0.00	6.43	0.02	0.00	7.16	2.00	0.00	6.42	0.02	0.00
7.18	2.00	0.00	6.41	0.02	0.00	7.20	2.00	0.00	6.40	0.02	0.00
7.22	2.00	0.00	6.39	0.02	0.00	7.24	2.00	0.00	6.38	0.02	0.00
7.26	2.00	0.00	6.37	0.02	0.00	7.28	2.00	0.00	6.36	0.02	0.00
7.30	2.00	0.00	6.35	0.02	0.00	7.32	2.00	0.00	6.34	0.02	0.00
7.34	2.00	0.00	6.33	0.02	0.00	7.36	2.00	0.00	6.32	0.02	0.00
7.38	2.00	0.00	6.31	0.02	0.00	7.40	2.00	0.00	6.30	0.02	0.00
7.42	2.00	0.00	6.29	0.02	0.00	7.44	2.00	0.00	6.28	0.02	0.00
7.46	2.00	0.00	6.27	0.02	0.00	7.48	2.00	0.00	6.26	0.02	0.00
7.50	2.00	0.00	6.25	0.02	0.00	7.52	2.00	0.00	6.24	0.02	0.00
7.54	2.00	0.00	6.23	0.02	0.00	7.56	2.00	0.00	6.22	0.02	0.00
7.58	2.00	0.00	6.21	0.02	0.00	7.60	2.00	0.00	6.20	0.02	0.00
7.62	2.00	0.00	6.19	0.02	0.00	7.64	2.00	0.00	6.18	0.02	0.00
7.66	2.00	0.00	6.17	0.02	0.00	7.68	2.00	0.00	6.16	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
7.70	2.00	0.00	6.15	0.02	0.00	7.72	2.00	0.00	6.14	0.02	0.00
7.74	2.00	0.00	6.13	0.02	0.00	7.76	2.00	0.00	6.12	0.02	0.00
7.78	2.00	0.00	6.11	0.02	0.00	7.80	2.00	0.00	6.10	0.02	0.00
7.82	2.00	0.00	6.09	0.02	0.00	7.84	2.00	0.00	6.08	0.02	0.00
7.86	2.00	0.00	6.07	0.02	0.00	7.88	2.00	0.00	6.06	0.02	0.00
7.90	2.00	0.00	6.05	0.02	0.00	7.92	2.00	0.00	6.04	0.02	0.00
7.94	2.00	0.00	6.03	0.02	0.00	7.96	2.00	0.00	6.02	0.02	0.00
7.98	2.00	0.00	6.01	0.02	0.00	8.00	2.00	0.00	6.00	0.02	0.00
8.02	2.00	0.00	5.99	0.02	0.00	8.04	2.00	0.00	5.98	0.02	0.00
8.06	2.00	0.00	5.97	0.02	0.00	8.08	2.00	0.00	5.96	0.02	0.00
8.10	2.00	0.00	5.95	0.02	0.00	8.12	2.00	0.00	5.94	0.02	0.00
8.14	2.00	0.00	5.93	0.02	0.00	8.16	2.00	0.00	5.92	0.02	0.00
8.18	2.00	0.00	5.91	0.02	0.00	8.20	2.00	0.00	5.90	0.02	0.00
8.22	2.00	0.00	5.89	0.02	0.00	8.24	2.00	0.00	5.88	0.02	0.00
8.26	2.00	0.00	5.87	0.02	0.00	8.28	2.00	0.00	5.86	0.02	0.00
8.30	2.00	0.00	5.85	0.02	0.00	8.32	2.00	0.00	5.84	0.02	0.00
8.34	2.00	0.00	5.83	0.02	0.00	8.36	2.00	0.00	5.82	0.02	0.00
8.38	2.00	0.00	5.81	0.02	0.00	8.40	2.00	0.00	5.80	0.02	0.00
8.42	2.00	0.00	5.79	0.02	0.00	8.44	2.00	0.00	5.78	0.02	0.00
8.46	2.00	0.00	5.77	0.02	0.00	8.48	2.00	0.00	5.76	0.02	0.00
8.50	2.00	0.00	5.75	0.02	0.00	8.52	2.00	0.00	5.74	0.02	0.00
8.54	2.00	0.00	5.73	0.02	0.00	8.56	2.00	0.00	5.72	0.02	0.00
8.58	2.00	0.00	5.71	0.02	0.00	8.60	2.00	0.00	5.70	0.02	0.00
8.62	2.00	0.00	5.69	0.02	0.00	8.64	2.00	0.00	5.68	0.02	0.00
8.66	2.00	0.00	5.67	0.02	0.00	8.68	2.00	0.00	5.66	0.02	0.00
8.70	2.00	0.00	5.65	0.02	0.00	8.72	2.00	0.00	5.64	0.02	0.00
8.74	2.00	0.00	5.63	0.02	0.00	8.76	2.00	0.00	5.62	0.02	0.00
8.78	2.00	0.00	5.61	0.02	0.00	8.80	2.00	0.00	5.60	0.02	0.00
8.82	2.00	0.00	5.59	0.02	0.00	8.84	2.00	0.00	5.58	0.02	0.00
8.86	2.00	0.00	5.57	0.02	0.00	8.88	2.00	0.00	5.56	0.02	0.00
8.91	2.00	0.00	5.55	0.03	0.00	8.92	2.00	0.00	5.54	0.01	0.00
8.94	2.00	0.00	5.53	0.02	0.00	8.96	2.00	0.00	5.52	0.02	0.00
8.98	2.00	0.00	5.51	0.02	0.00	9.00	2.00	0.00	5.50	0.02	0.00
9.02	2.00	0.00	5.49	0.02	0.00	9.04	2.00	0.00	5.48	0.02	0.00
9.06	2.00	0.00	5.47	0.02	0.00	9.08	2.00	0.00	5.46	0.02	0.00
9.10	2.00	0.00	5.45	0.02	0.00	9.12	2.00	0.00	5.44	0.02	0.00
9.14	2.00	0.00	5.43	0.02	0.00	9.16	2.00	0.00	5.42	0.02	0.00
9.18	2.00	0.00	5.41	0.02	0.00	9.20	2.00	0.00	5.40	0.02	0.00
9.22	2.00	0.00	5.39	0.02	0.00	9.24	2.00	0.00	5.38	0.02	0.00
9.26	2.00	0.00	5.37	0.02	0.00	9.28	2.00	0.00	5.36	0.02	0.00
9.30	2.00	0.00	5.35	0.02	0.00	9.32	2.00	0.00	5.34	0.02	0.00
9.34	2.00	0.00	5.33	0.02	0.00	9.36	2.00	0.00	5.32	0.02	0.00
9.38	2.00	0.00	5.31	0.02	0.00	9.40	2.00	0.00	5.30	0.02	0.00
9.42	2.00	0.00	5.29	0.02	0.00	9.44	2.00	0.00	5.28	0.02	0.00
9.46	2.00	0.00	5.27	0.02	0.00	9.48	2.00	0.00	5.26	0.02	0.00
9.50	2.00	0.00	5.25	0.02	0.00	9.52	2.00	0.00	5.24	0.02	0.00
9.54	2.00	0.00	5.23	0.02	0.00	9.56	2.00	0.00	5.22	0.02	0.00
9.58	2.00	0.00	5.21	0.02	0.00	9.60	2.00	0.00	5.20	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
9.62	2.00	0.00	5.19	0.02	0.00	9.64	2.00	0.00	5.18	0.02	0.00
9.66	2.00	0.00	5.17	0.02	0.00	9.68	2.00	0.00	5.16	0.02	0.00
9.70	2.00	0.00	5.15	0.02	0.00	9.72	2.00	0.00	5.14	0.02	0.00
9.74	2.00	0.00	5.13	0.02	0.00	9.76	2.00	0.00	5.12	0.02	0.00
9.78	2.00	0.00	5.11	0.02	0.00	9.80	2.00	0.00	5.10	0.02	0.00
9.82	2.00	0.00	5.09	0.02	0.00	9.84	2.00	0.00	5.08	0.02	0.00
9.86	2.00	0.00	5.07	0.02	0.00	9.88	2.00	0.00	5.06	0.02	0.00
9.90	2.00	0.00	5.05	0.02	0.00	9.92	2.00	0.00	5.04	0.02	0.00
9.94	2.00	0.00	5.03	0.02	0.00	9.96	2.00	0.00	5.02	0.02	0.00
9.98	2.00	0.00	5.01	0.02	0.00	10.00	2.00	0.00	5.00	0.02	0.00
10.02	2.00	0.00	4.99	0.02	0.00	10.04	2.00	0.00	4.98	0.02	0.00
10.06	2.00	0.00	4.97	0.02	0.00	10.08	2.00	0.00	4.96	0.02	0.00
10.10	2.00	0.00	4.95	0.02	0.00	10.12	2.00	0.00	4.94	0.02	0.00
10.14	2.00	0.00	4.93	0.02	0.00	10.16	2.00	0.00	4.92	0.02	0.00
10.18	2.00	0.00	4.91	0.02	0.00	10.20	2.00	0.00	4.90	0.02	0.00
10.22	2.00	0.00	4.89	0.02	0.00	10.24	2.00	0.00	4.88	0.02	0.00
10.26	2.00	0.00	4.87	0.02	0.00	10.28	2.00	0.00	4.86	0.02	0.00
10.30	2.00	0.00	4.85	0.02	0.00	10.32	2.00	0.00	4.84	0.02	0.00
10.34	2.00	0.00	4.83	0.02	0.00	10.36	2.00	0.00	4.82	0.02	0.00
10.38	2.00	0.00	4.81	0.02	0.00	10.40	2.00	0.00	4.80	0.02	0.00
10.42	2.00	0.00	4.79	0.02	0.00	10.44	2.00	0.00	4.78	0.02	0.00
10.46	2.00	0.00	4.77	0.02	0.00	10.48	2.00	0.00	4.76	0.02	0.00
10.50	2.00	0.00	4.75	0.02	0.00	10.52	2.00	0.00	4.74	0.02	0.00
10.54	2.00	0.00	4.73	0.02	0.00	10.56	2.00	0.00	4.72	0.02	0.00
10.58	2.00	0.00	4.71	0.02	0.00	10.60	2.00	0.00	4.70	0.02	0.00
10.62	2.00	0.00	4.69	0.02	0.00	10.64	2.00	0.00	4.68	0.02	0.00
10.66	2.00	0.00	4.67	0.02	0.00	10.68	2.00	0.00	4.66	0.02	0.00
10.70	2.00	0.00	4.65	0.02	0.00	10.72	2.00	0.00	4.64	0.02	0.00
10.74	2.00	0.00	4.63	0.02	0.00	10.76	2.00	0.00	4.62	0.02	0.00
10.78	2.00	0.00	4.61	0.02	0.00	10.80	2.00	0.00	4.60	0.02	0.00
10.82	2.00	0.00	4.59	0.02	0.00	10.84	2.00	0.00	4.58	0.02	0.00
10.86	2.00	0.00	4.57	0.02	0.00	10.88	2.00	0.00	4.56	0.02	0.00
10.90	2.00	0.00	4.55	0.02	0.00	10.92	2.00	0.00	4.54	0.02	0.00
10.94	2.00	0.00	4.53	0.02	0.00	10.96	2.00	0.00	4.52	0.02	0.00
10.98	2.00	0.00	4.51	0.02	0.00	11.00	2.00	0.00	4.50	0.02	0.00
11.02	2.00	0.00	4.49	0.02	0.00	11.04	2.00	0.00	4.48	0.02	0.00
11.06	2.00	0.00	4.47	0.02	0.00	11.08	2.00	0.00	4.46	0.02	0.00
11.10	2.00	0.00	4.45	0.02	0.00	11.12	2.00	0.00	4.44	0.02	0.00
11.14	2.00	0.00	4.43	0.02	0.00	11.16	2.00	0.00	4.42	0.02	0.00
11.18	2.00	0.00	4.41	0.02	0.00	11.20	2.00	0.00	4.40	0.02	0.00
11.22	2.00	0.00	4.39	0.02	0.00	11.24	2.00	0.00	4.38	0.02	0.00
11.26	2.00	0.00	4.37	0.02	0.00	11.28	2.00	0.00	4.36	0.02	0.00
11.30	2.00	0.00	4.35	0.02	0.00	11.32	2.00	0.00	4.34	0.02	0.00
11.34	2.00	0.00	4.33	0.02	0.00	11.36	2.00	0.00	4.32	0.02	0.00
11.38	2.00	0.00	4.31	0.02	0.00	11.40	2.00	0.00	4.30	0.02	0.00
11.42	2.00	0.00	4.29	0.02	0.00	11.44	2.00	0.00	4.28	0.02	0.00
11.46	2.00	0.00	4.27	0.02	0.00	11.48	2.00	0.00	4.26	0.02	0.00
11.50	2.00	0.00	4.25	0.02	0.00	11.52	2.00	0.00	4.24	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
11.54	2.00	0.00	4.23	0.02	0.00	11.56	2.00	0.00	4.22	0.02	0.00
11.58	2.00	0.00	4.21	0.02	0.00	11.60	2.00	0.00	4.20	0.02	0.00
11.62	2.00	0.00	4.19	0.02	0.00	11.64	2.00	0.00	4.18	0.02	0.00
11.66	2.00	0.00	4.17	0.02	0.00	11.68	2.00	0.00	4.16	0.02	0.00
11.70	2.00	0.00	4.15	0.02	0.00	11.72	2.00	0.00	4.14	0.02	0.00
11.74	2.00	0.00	4.13	0.02	0.00	11.76	2.00	0.00	4.12	0.02	0.00
11.78	2.00	0.00	4.11	0.02	0.00	11.80	2.00	0.00	4.10	0.02	0.00
11.82	2.00	0.00	4.09	0.02	0.00	11.84	2.00	0.00	4.08	0.02	0.00
11.86	2.00	0.00	4.07	0.02	0.00	11.88	2.00	0.00	4.06	0.02	0.00
11.90	2.00	0.00	4.05	0.02	0.00	11.92	2.00	0.00	4.04	0.02	0.00
11.94	2.00	0.00	4.03	0.02	0.00	11.96	2.00	0.00	4.02	0.02	0.00
11.98	2.00	0.00	4.01	0.02	0.00	12.00	2.00	0.00	4.00	0.02	0.00
12.02	2.00	0.00	3.99	0.02	0.00	12.04	2.00	0.00	3.98	0.02	0.00
12.06	2.00	0.00	3.97	0.02	0.00	12.08	2.00	0.00	3.96	0.02	0.00
12.10	2.00	0.00	3.95	0.02	0.00	12.13	2.00	0.00	3.94	0.03	0.00
12.14	2.00	0.00	3.93	0.01	0.00	12.17	2.00	0.00	3.92	0.03	0.00
12.18	2.00	0.00	3.91	0.01	0.00	12.20	2.00	0.00	3.90	0.02	0.00
12.22	2.00	0.00	3.89	0.02	0.00	12.24	2.00	0.00	3.88	0.02	0.00
12.26	2.00	0.00	3.87	0.02	0.00	12.29	2.00	0.00	3.86	0.03	0.00
12.30	2.00	0.00	3.85	0.01	0.00	12.32	2.00	0.00	3.84	0.02	0.00
12.34	2.00	0.00	3.83	0.02	0.00	12.36	2.00	0.00	3.82	0.02	0.00
12.38	2.00	0.00	3.81	0.02	0.00	12.40	2.00	0.00	3.80	0.02	0.00
12.42	2.00	0.00	3.79	0.02	0.00	12.44	2.00	0.00	3.78	0.02	0.00
12.46	2.00	0.00	3.77	0.02	0.00	12.48	2.00	0.00	3.76	0.02	0.00
12.50	2.00	0.00	3.75	0.02	0.00	12.52	2.00	0.00	3.74	0.02	0.00
12.54	2.00	0.00	3.73	0.02	0.00	12.56	2.00	0.00	3.72	0.02	0.00
12.58	2.00	0.00	3.71	0.02	0.00	12.60	2.00	0.00	3.70	0.02	0.00
12.62	2.00	0.00	3.69	0.02	0.00	12.64	2.00	0.00	3.68	0.02	0.00
12.66	2.00	0.00	3.67	0.02	0.00	12.68	2.00	0.00	3.66	0.02	0.00
12.70	2.00	0.00	3.65	0.02	0.00	12.72	2.00	0.00	3.64	0.02	0.00
12.74	2.00	0.00	3.63	0.02	0.00	12.76	2.00	0.00	3.62	0.02	0.00
12.78	2.00	0.00	3.61	0.02	0.00	12.80	2.00	0.00	3.60	0.02	0.00
12.82	2.00	0.00	3.59	0.02	0.00	12.84	2.00	0.00	3.58	0.02	0.00
12.86	2.00	0.00	3.57	0.02	0.00	12.88	2.00	0.00	3.56	0.02	0.00
12.90	2.00	0.00	3.55	0.02	0.00	12.92	2.00	0.00	3.54	0.02	0.00
12.94	2.00	0.00	3.53	0.02	0.00	12.96	2.00	0.00	3.52	0.02	0.00
12.98	2.00	0.00	3.51	0.02	0.00	13.00	2.00	0.00	3.50	0.02	0.00
13.02	2.00	0.00	3.49	0.02	0.00	13.04	2.00	0.00	3.48	0.02	0.00
13.06	2.00	0.00	3.47	0.02	0.00	13.08	2.00	0.00	3.46	0.02	0.00
13.10	2.00	0.00	3.45	0.02	0.00	13.12	2.00	0.00	3.44	0.02	0.00
13.14	2.00	0.00	3.43	0.02	0.00	13.16	2.00	0.00	3.42	0.02	0.00
13.19	2.00	0.00	3.41	0.03	0.00	13.20	2.00	0.00	3.40	0.01	0.00
13.22	2.00	0.00	3.39	0.02	0.00	13.24	2.00	0.00	3.38	0.02	0.00
13.26	2.00	0.00	3.37	0.02	0.00	13.28	2.00	0.00	3.36	0.02	0.00
13.30	2.00	0.00	3.35	0.02	0.00	13.32	2.00	0.00	3.34	0.02	0.00
13.34	2.00	0.00	3.33	0.02	0.00	13.36	2.00	0.00	3.32	0.02	0.00
13.38	2.00	0.00	3.31	0.02	0.00	13.40	2.00	0.00	3.30	0.02	0.00
13.42	2.00	0.00	3.29	0.02	0.00	13.44	2.00	0.00	3.28	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
13.46	2.00	0.00	3.27	0.02	0.00	13.48	2.00	0.00	3.26	0.02	0.00
13.50	2.00	0.00	3.25	0.02	0.00	13.52	2.00	0.00	3.24	0.02	0.00
13.54	2.00	0.00	3.23	0.02	0.00	13.56	2.00	0.00	3.22	0.02	0.00
13.58	2.00	0.00	3.21	0.02	0.00	13.60	2.00	0.00	3.20	0.02	0.00
13.62	2.00	0.00	3.19	0.02	0.00	13.64	2.00	0.00	3.18	0.02	0.00
13.66	2.00	0.00	3.17	0.02	0.00	13.68	2.00	0.00	3.16	0.02	0.00
13.70	2.00	0.00	3.15	0.02	0.00	13.72	2.00	0.00	3.14	0.02	0.00
13.74	2.00	0.00	3.13	0.02	0.00	13.76	2.00	0.00	3.12	0.02	0.00
13.78	2.00	0.00	3.11	0.02	0.00	13.80	2.00	0.00	3.10	0.02	0.00
13.82	2.00	0.00	3.09	0.02	0.00	13.84	2.00	0.00	3.08	0.02	0.00
13.86	2.00	0.00	3.07	0.02	0.00	13.88	2.00	0.00	3.06	0.02	0.00
13.90	2.00	0.00	3.05	0.02	0.00	13.92	2.00	0.00	3.04	0.02	0.00
13.94	2.00	0.00	3.03	0.02	0.00	13.96	2.00	0.00	3.02	0.02	0.00
13.98	2.00	0.00	3.01	0.02	0.00	14.00	2.00	0.00	3.00	0.02	0.00
14.02	2.00	0.00	2.99	0.02	0.00	14.04	2.00	0.00	2.98	0.02	0.00
14.06	2.00	0.00	2.97	0.02	0.00	14.08	2.00	0.00	2.96	0.02	0.00
14.10	2.00	0.00	2.95	0.02	0.00	14.12	2.00	0.00	2.94	0.02	0.00
14.14	2.00	0.00	2.93	0.02	0.00	14.16	2.00	0.00	2.92	0.02	0.00
14.18	2.00	0.00	2.91	0.02	0.00	14.20	2.00	0.00	2.90	0.02	0.00
14.22	2.00	0.00	2.89	0.02	0.00	14.24	2.00	0.00	2.88	0.02	0.00
14.26	2.00	0.00	2.87	0.02	0.00	14.28	2.00	0.00	2.86	0.02	0.00
14.30	2.00	0.00	2.85	0.02	0.00	14.32	2.00	0.00	2.84	0.02	0.00
14.34	2.00	0.00	2.83	0.02	0.00	14.36	2.00	0.00	2.82	0.02	0.00
14.38	2.00	0.00	2.81	0.02	0.00	14.40	2.00	0.00	2.80	0.02	0.00
14.42	2.00	0.00	2.79	0.02	0.00	14.44	2.00	0.00	2.78	0.02	0.00
14.46	2.00	0.00	2.77	0.02	0.00	14.48	2.00	0.00	2.76	0.02	0.00
14.50	2.00	0.00	2.75	0.02	0.00	14.52	2.00	0.00	2.74	0.02	0.00
14.54	2.00	0.00	2.73	0.02	0.00	14.56	2.00	0.00	2.72	0.02	0.00
14.58	2.00	0.00	2.71	0.02	0.00	14.60	2.00	0.00	2.70	0.02	0.00
14.62	2.00	0.00	2.69	0.02	0.00	14.64	2.00	0.00	2.68	0.02	0.00
14.66	2.00	0.00	2.67	0.02	0.00	14.68	2.00	0.00	2.66	0.02	0.00
14.70	2.00	0.00	2.65	0.02	0.00	14.72	2.00	0.00	2.64	0.02	0.00
14.74	2.00	0.00	2.63	0.02	0.00	14.76	2.00	0.00	2.62	0.02	0.00
14.78	2.00	0.00	2.61	0.02	0.00	14.80	2.00	0.00	2.60	0.02	0.00
14.82	2.00	0.00	2.59	0.02	0.00	14.84	2.00	0.00	2.58	0.02	0.00
14.86	2.00	0.00	2.57	0.02	0.00	14.88	2.00	0.00	2.56	0.02	0.00
14.90	2.00	0.00	2.55	0.02	0.00	14.92	2.00	0.00	2.54	0.02	0.00
14.94	2.00	0.00	2.53	0.02	0.00	14.96	2.00	0.00	2.52	0.02	0.00
14.98	2.00	0.00	2.51	0.02	0.00	15.00	2.00	0.00	2.50	0.02	0.00
15.02	2.00	0.00	2.49	0.02	0.00	15.04	2.00	0.00	2.48	0.02	0.00
15.06	2.00	0.00	2.47	0.02	0.00	15.08	2.00	0.00	2.46	0.02	0.00
15.10	2.00	0.00	2.45	0.02	0.00	15.12	2.00	0.00	2.44	0.02	0.00
15.14	2.00	0.00	2.43	0.02	0.00	15.16	2.00	0.00	2.42	0.02	0.00
15.18	2.00	0.00	2.41	0.02	0.00	15.20	2.00	0.00	2.40	0.02	0.00
15.22	2.00	0.00	2.39	0.02	0.00	15.24	2.00	0.00	2.38	0.02	0.00
15.26	2.00	0.00	2.37	0.02	0.00	15.28	2.00	0.00	2.36	0.02	0.00
15.30	2.00	0.00	2.35	0.02	0.00	15.32	2.00	0.00	2.34	0.02	0.00
15.34	2.00	0.00	2.33	0.02	0.00	15.36	2.00	0.00	2.32	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
15.38	2.00	0.00	2.31	0.02	0.00	15.40	2.00	0.00	2.30	0.02	0.00
15.42	2.00	0.00	2.29	0.02	0.00	15.44	2.00	0.00	2.28	0.02	0.00
15.46	2.00	0.00	2.27	0.02	0.00	15.48	2.00	0.00	2.26	0.02	0.00
15.50	2.00	0.00	2.25	0.02	0.00	15.52	2.00	0.00	2.24	0.02	0.00
15.54	2.00	0.00	2.23	0.02	0.00	15.56	2.00	0.00	2.22	0.02	0.00
15.58	2.00	0.00	2.21	0.02	0.00	15.60	2.00	0.00	2.20	0.02	0.00
15.62	2.00	0.00	2.19	0.02	0.00	15.64	2.00	0.00	2.18	0.02	0.00
15.66	2.00	0.00	2.17	0.02	0.00	15.68	2.00	0.00	2.16	0.02	0.00
15.70	2.00	0.00	2.15	0.02	0.00	15.72	2.00	0.00	2.14	0.02	0.00
15.74	2.00	0.00	2.13	0.02	0.00	15.76	2.00	0.00	2.12	0.02	0.00
15.78	2.00	0.00	2.11	0.02	0.00	15.80	2.00	0.00	2.10	0.02	0.00
15.82	2.00	0.00	2.09	0.02	0.00	15.85	2.00	0.00	2.08	0.03	0.00
15.86	2.00	0.00	2.07	0.01	0.00	15.88	2.00	0.00	2.06	0.02	0.00
15.90	2.00	0.00	2.05	0.02	0.00	15.92	2.00	0.00	2.04	0.02	0.00
15.94	2.00	0.00	2.03	0.02	0.00	15.96	2.00	0.00	2.02	0.02	0.00
15.98	2.00	0.00	2.01	0.02	0.00	16.00	2.00	0.00	2.00	0.02	0.00
16.02	2.00	0.00	1.99	0.02	0.00	16.04	2.00	0.00	1.98	0.02	0.00
16.06	2.00	0.00	1.97	0.02	0.00	16.08	2.00	0.00	1.96	0.02	0.00
16.10	2.00	0.00	1.95	0.02	0.00	16.12	2.00	0.00	1.94	0.02	0.00
16.14	2.00	0.00	1.93	0.02	0.00	16.16	2.00	0.00	1.92	0.02	0.00
16.18	2.00	0.00	1.91	0.02	0.00	16.20	2.00	0.00	1.90	0.02	0.00
16.22	2.00	0.00	1.89	0.02	0.00	16.24	2.00	0.00	1.88	0.02	0.00
16.26	2.00	0.00	1.87	0.02	0.00	16.28	2.00	0.00	1.86	0.02	0.00
16.30	2.00	0.00	1.85	0.02	0.00	16.32	2.00	0.00	1.84	0.02	0.00
16.34	2.00	0.00	1.83	0.02	0.00	16.36	2.00	0.00	1.82	0.02	0.00
16.38	2.00	0.00	1.81	0.02	0.00	16.40	2.00	0.00	1.80	0.02	0.00
16.42	2.00	0.00	1.79	0.02	0.00	16.44	2.00	0.00	1.78	0.02	0.00
16.46	2.00	0.00	1.77	0.02	0.00	16.48	2.00	0.00	1.76	0.02	0.00
16.50	2.00	0.00	1.75	0.02	0.00	16.52	2.00	0.00	1.74	0.02	0.00
16.54	2.00	0.00	1.73	0.02	0.00	16.56	2.00	0.00	1.72	0.02	0.00
16.58	2.00	0.00	1.71	0.02	0.00	16.60	2.00	0.00	1.70	0.02	0.00
16.62	2.00	0.00	1.69	0.02	0.00	16.64	2.00	0.00	1.68	0.02	0.00
16.66	2.00	0.00	1.67	0.02	0.00	16.68	2.00	0.00	1.66	0.02	0.00
16.70	2.00	0.00	1.65	0.02	0.00	16.72	2.00	0.00	1.64	0.02	0.00
16.74	2.00	0.00	1.63	0.02	0.00	16.76	2.00	0.00	1.62	0.02	0.00
16.79	2.00	0.00	1.61	0.03	0.00	16.80	2.00	0.00	1.60	0.01	0.00
16.82	2.00	0.00	1.59	0.02	0.00	16.84	2.00	0.00	1.58	0.02	0.00
16.86	2.00	0.00	1.57	0.02	0.00						

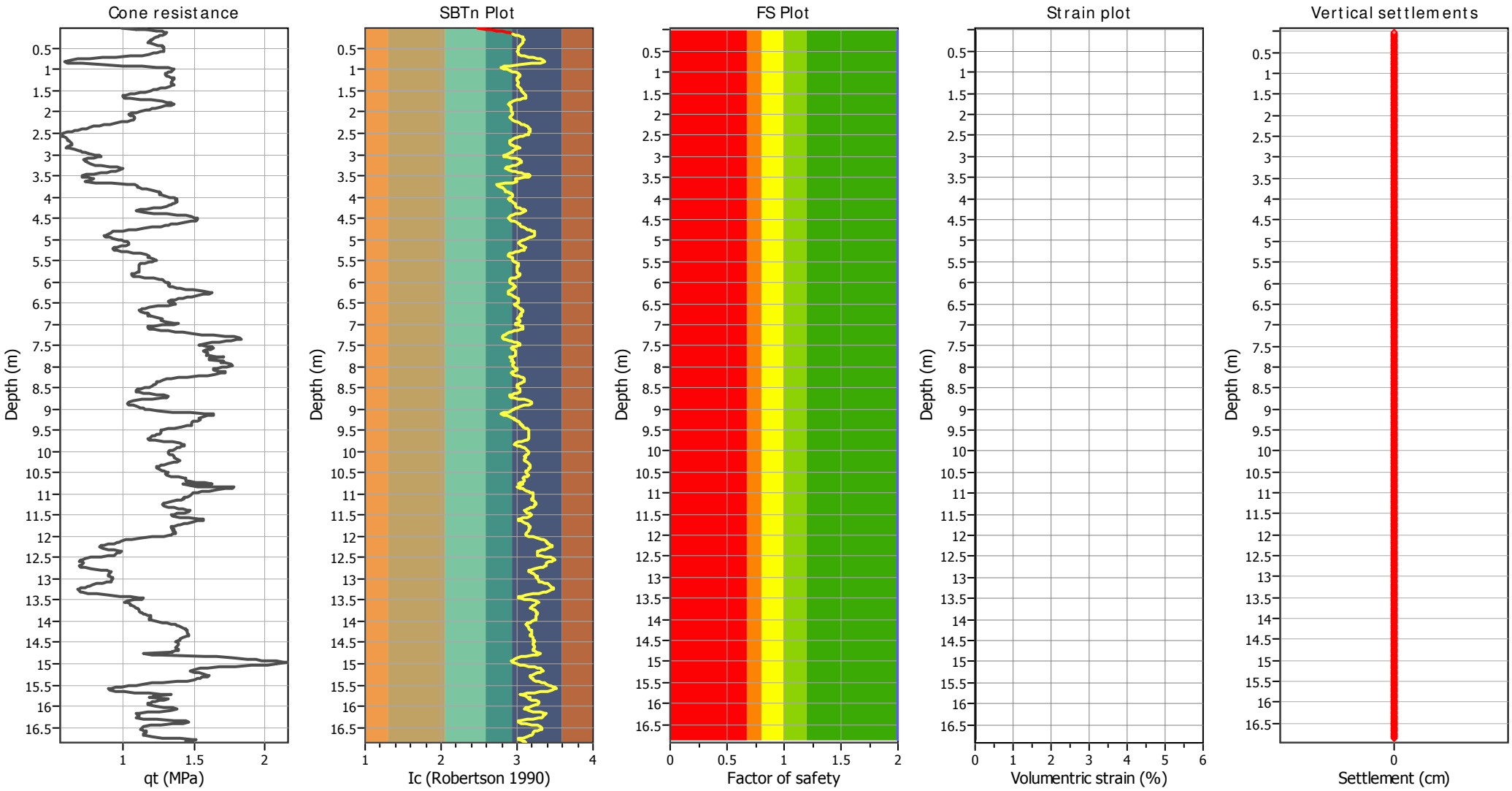
Overall liquefaction potential: 0.00

LPI = 0.00 - Liquefaction risk very low
LPI between 0.00 and 5.00 - Liquefaction risk low
LPI between 5.00 and 15.00 - Liquefaction risk high
LPI > 15.00 - Liquefaction risk very high

Abbreviations

FS: Calculated factor of safety for test point
F_L: 1 - FS
w_z: Function value of the extend of soil liquefaction according to depth
d_z: Layer thickness (m)
LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

q_t:	Total cone resistance (cone resistance q_c corrected for pore water effects)
I_c:	Soil Behaviour Type Index
FS:	Calculated Factor of Safety against liquefaction
Volumentric strain:	Post-liquefaction volumentric strain

:: Post-earthquake settlement due to soil liquefaction ::

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
0.02	69.59	2.00	0.00	1.00	0.00	0.04	73.47	2.00	0.00	1.00	0.00
0.06	19.69	2.00	0.00	1.00	0.00	0.08	20.99	2.00	0.00	1.00	0.00
0.10	21.23	2.00	0.00	1.00	0.00	0.12	21.71	2.00	0.00	1.00	0.00
0.14	21.95	2.00	0.00	1.00	0.00	0.17	21.88	2.00	0.00	1.00	0.00
0.18	21.27	2.00	0.00	1.00	0.00	0.20	21.13	2.00	0.00	1.00	0.00
0.23	20.84	2.00	0.00	1.00	0.00	0.24	20.59	2.00	0.00	1.00	0.00
0.26	20.59	2.00	0.00	1.00	0.00	0.29	20.03	2.00	0.00	1.00	0.00
0.30	20.06	2.00	0.00	1.00	0.00	0.32	20.13	2.00	0.00	1.00	0.00
0.34	19.69	2.00	0.00	1.00	0.00	0.36	19.68	2.00	0.00	1.00	0.00
0.38	19.67	2.00	0.00	1.00	0.00	0.40	20.41	2.00	0.00	1.00	0.00
0.42	21.19	2.00	0.00	1.00	0.00	0.44	21.18	2.00	0.00	1.00	0.00
0.46	21.64	2.00	0.00	1.00	0.00	0.48	21.59	2.00	0.00	1.00	0.00
0.50	21.62	2.00	0.00	1.00	0.00	0.53	21.34	2.00	0.00	1.00	0.00
0.54	21.79	2.00	0.00	1.00	0.00	0.56	21.66	2.00	0.00	1.00	0.00
0.58	21.09	2.00	0.00	1.00	0.00	0.60	20.80	2.00	0.00	1.00	0.00
0.62	20.34	2.00	0.00	1.00	0.00	0.64	20.25	2.00	0.00	1.00	0.00
0.66	19.20	2.00	0.00	1.00	0.00	0.68	17.39	2.00	0.00	1.00	0.00
0.70	16.03	2.00	0.00	1.00	0.00	0.72	14.21	2.00	0.00	1.00	0.00
0.74	12.54	2.00	0.00	1.00	0.00	0.76	11.27	2.00	0.00	1.00	0.00
0.78	10.34	2.00	0.00	1.00	0.00	0.80	9.88	2.00	0.00	1.00	0.00
0.82	9.39	2.00	0.00	1.00	0.00	0.84	9.87	2.00	0.00	1.00	0.00
0.86	11.32	2.00	0.00	1.00	0.00	0.88	14.29	2.00	0.00	1.00	0.00
0.90	17.06	2.00	0.00	1.00	0.00	0.92	18.47	2.00	0.00	1.00	0.00
0.94	21.22	2.00	0.00	1.00	0.00	0.96	22.16	2.00	0.00	1.00	0.00
0.98	22.75	2.00	0.00	1.00	0.00	1.00	22.39	2.00	0.00	1.00	0.00
1.02	22.63	2.00	0.00	1.00	0.00	1.04	22.39	2.00	0.00	1.00	0.00
1.07	21.95	2.00	0.00	1.00	0.00	1.08	21.78	2.00	0.00	1.00	0.00
1.10	21.44	2.00	0.00	1.00	0.00	1.12	21.78	2.00	0.00	1.00	0.00
1.14	21.65	2.00	0.00	1.00	0.00	1.16	21.79	2.00	0.00	1.00	0.00
1.18	22.44	2.00	0.00	1.00	0.00	1.20	22.54	2.00	0.00	1.00	0.00
1.22	22.79	2.00	0.00	1.00	0.00	1.24	22.57	2.00	0.00	1.00	0.00
1.26	22.26	2.00	0.00	1.00	0.00	1.28	22.40	2.00	0.00	1.00	0.00
1.30	22.41	2.00	0.00	1.00	0.00	1.32	22.19	2.00	0.00	1.00	0.00
1.34	22.28	2.00	0.00	1.00	0.00	1.36	22.84	2.00	0.00	1.00	0.00
1.38	22.62	2.00	0.00	1.00	0.00	1.40	22.04	2.00	0.00	1.00	0.00
1.42	21.81	2.00	0.00	1.00	0.00	1.44	20.99	2.00	0.00	1.00	0.00
1.46	20.65	2.00	0.00	1.00	0.00	1.48	20.27	2.00	0.00	1.00	0.00
1.50	19.78	2.00	0.00	1.00	0.00	1.52	19.35	2.00	0.00	1.00	0.00
1.54	18.47	2.00	0.00	1.00	0.00	1.56	18.01	2.00	0.00	1.00	0.00
1.58	17.39	2.00	0.00	1.00	0.00	1.60	16.86	2.00	0.00	1.00	0.00
1.62	16.64	2.00	0.00	1.00	0.00	1.64	16.34	2.00	0.00	1.00	0.00
1.66	16.75	2.00	0.00	1.00	0.00	1.68	17.35	2.00	0.00	1.00	0.00
1.70	18.19	2.00	0.00	1.00	0.00	1.72	20.21	2.00	0.00	1.00	0.00
1.74	21.26	2.00	0.00	1.00	0.00	1.76	21.99	2.00	0.00	1.00	0.00
1.78	22.01	2.00	0.00	1.00	0.00	1.80	23.01	2.00	0.00	1.00	0.00
1.82	22.36	2.00	0.00	1.00	0.00	1.84	22.31	2.00	0.00	1.00	0.00
1.86	22.01	2.00	0.00	1.00	0.00	1.88	20.48	2.00	0.00	1.00	0.00
1.90	20.32	2.00	0.00	1.00	0.00	1.92	20.05	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
1.94	19.61	2.00	0.00	1.00	0.00	1.96	19.17	2.00	0.00	1.00	0.00
1.98	18.70	2.00	0.00	1.00	0.00	2.01	17.95	2.00	0.00	1.00	0.00
2.02	17.28	2.00	0.00	1.00	0.00	2.04	17.20	2.00	0.00	1.00	0.00
2.06	16.91	2.00	0.00	1.00	0.00	2.08	17.18	2.00	0.00	1.00	0.00
2.10	17.68	2.00	0.00	1.00	0.00	2.12	17.87	2.00	0.00	1.00	0.00
2.14	17.78	2.00	0.00	1.00	0.00	2.16	17.69	2.00	0.00	1.00	0.00
2.18	17.76	2.00	0.00	1.00	0.00	2.20	17.48	2.00	0.00	1.00	0.00
2.22	16.81	2.00	0.00	1.00	0.00	2.24	16.40	2.00	0.00	1.00	0.00
2.26	15.57	2.00	0.00	1.00	0.00	2.28	14.74	2.00	0.00	1.00	0.00
2.30	14.34	2.00	0.00	1.00	0.00	2.32	13.50	2.00	0.00	1.00	0.00
2.34	13.02	2.00	0.00	1.00	0.00	2.36	12.38	2.00	0.00	1.00	0.00
2.38	12.02	2.00	0.00	1.00	0.00	2.40	11.58	2.00	0.00	1.00	0.00
2.42	11.06	2.00	0.00	1.00	0.00	2.44	10.54	2.00	0.00	1.00	0.00
2.46	10.37	2.00	0.00	1.00	0.00	2.48	9.81	2.00	0.00	1.00	0.00
2.50	9.37	2.00	0.00	1.00	0.00	2.52	8.89	2.00	0.00	1.00	0.00
2.54	8.69	2.00	0.00	1.00	0.00	2.56	9.19	2.00	0.00	1.00	0.00
2.58	9.41	2.00	0.00	1.00	0.00	2.60	9.40	2.00	0.00	1.00	0.00
2.62	9.91	2.00	0.00	1.00	0.00	2.64	9.55	2.00	0.00	1.00	0.00
2.66	9.66	2.00	0.00	1.00	0.00	2.68	10.01	2.00	0.00	1.00	0.00
2.70	10.08	2.00	0.00	1.00	0.00	2.72	10.11	2.00	0.00	1.00	0.00
2.74	10.31	2.00	0.00	1.00	0.00	2.76	10.42	2.00	0.00	1.00	0.00
2.78	10.06	2.00	0.00	1.00	0.00	2.80	9.90	2.00	0.00	1.00	0.00
2.82	9.85	2.00	0.00	1.00	0.00	2.84	9.34	2.00	0.00	1.00	0.00
2.86	9.34	2.00	0.00	1.00	0.00	2.88	11.03	2.00	0.00	1.00	0.00
2.90	11.34	2.00	0.00	1.00	0.00	2.92	11.14	2.00	0.00	1.00	0.00
2.94	11.53	2.00	0.00	1.00	0.00	2.96	11.73	2.00	0.00	1.00	0.00
2.98	12.03	2.00	0.00	1.00	0.00	3.00	13.32	2.00	0.00	1.00	0.00
3.02	13.79	2.00	0.00	1.00	0.00	3.04	13.55	2.00	0.00	1.00	0.00
3.06	13.66	2.00	0.00	1.00	0.00	3.08	12.80	2.00	0.00	1.00	0.00
3.10	11.86	2.00	0.00	1.00	0.00	3.12	11.66	2.00	0.00	1.00	0.00
3.14	11.46	2.00	0.00	1.00	0.00	3.16	12.43	2.00	0.00	1.00	0.00
3.18	11.53	2.00	0.00	1.00	0.00	3.20	12.06	2.00	0.00	1.00	0.00
3.22	12.47	2.00	0.00	1.00	0.00	3.24	12.66	2.00	0.00	1.00	0.00
3.26	13.39	2.00	0.00	1.00	0.00	3.28	14.67	2.00	0.00	1.00	0.00
3.30	15.52	2.00	0.00	1.00	0.00	3.32	16.18	2.00	0.00	1.00	0.00
3.34	16.37	2.00	0.00	1.00	0.00	3.36	15.89	2.00	0.00	1.00	0.00
3.38	15.33	2.00	0.00	1.00	0.00	3.40	14.85	2.00	0.00	1.00	0.00
3.42	14.14	2.00	0.00	1.00	0.00	3.44	13.86	2.00	0.00	1.00	0.00
3.46	12.98	2.00	0.00	1.00	0.00	3.48	11.68	2.00	0.00	1.00	0.00
3.50	10.97	2.00	0.00	1.00	0.00	3.52	11.23	2.00	0.00	1.00	0.00
3.54	11.96	2.00	0.00	1.00	0.00	3.56	12.73	2.00	0.00	1.00	0.00
3.58	13.11	2.00	0.00	1.00	0.00	3.60	12.12	2.00	0.00	1.00	0.00
3.62	11.75	2.00	0.00	1.00	0.00	3.64	11.08	2.00	0.00	1.00	0.00
3.66	12.24	2.00	0.00	1.00	0.00	3.68	14.93	2.00	0.00	1.00	0.00
3.70	16.87	2.00	0.00	1.00	0.00	3.72	17.76	2.00	0.00	1.00	0.00
3.74	17.59	2.00	0.00	1.00	0.00	3.76	17.86	2.00	0.00	1.00	0.00
3.78	17.89	2.00	0.00	1.00	0.00	3.80	18.16	2.00	0.00	1.00	0.00
3.82	18.63	2.00	0.00	1.00	0.00	3.84	19.96	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
3.86	20.07	2.00	0.00	1.00	0.00	3.88	20.94	2.00	0.00	1.00	0.00
3.90	20.86	2.00	0.00	1.00	0.00	3.92	20.42	2.00	0.00	1.00	0.00
3.94	20.38	2.00	0.00	1.00	0.00	3.96	20.76	2.00	0.00	1.00	0.00
3.98	21.31	2.00	0.00	1.00	0.00	4.00	21.50	2.00	0.00	1.00	0.00
4.02	22.71	2.00	0.00	1.00	0.00	4.05	22.90	2.00	0.00	1.00	0.00
4.06	22.41	2.00	0.00	1.00	0.00	4.08	22.55	2.00	0.00	1.00	0.00
4.10	23.05	2.00	0.00	1.00	0.00	4.12	22.76	2.00	0.00	1.00	0.00
4.14	22.39	2.00	0.00	1.00	0.00	4.16	22.17	2.00	0.00	1.00	0.00
4.18	22.11	2.00	0.00	1.00	0.00	4.20	21.97	2.00	0.00	1.00	0.00
4.22	21.64	2.00	0.00	1.00	0.00	4.24	20.85	2.00	0.00	1.00	0.00
4.26	20.05	2.00	0.00	1.00	0.00	4.28	19.18	2.00	0.00	1.00	0.00
4.30	18.23	2.00	0.00	1.00	0.00	4.32	17.92	2.00	0.00	1.00	0.00
4.34	17.68	2.00	0.00	1.00	0.00	4.36	18.14	2.00	0.00	1.00	0.00
4.38	19.91	2.00	0.00	1.00	0.00	4.40	21.01	2.00	0.00	1.00	0.00
4.42	22.15	2.00	0.00	1.00	0.00	4.44	23.10	2.00	0.00	1.00	0.00
4.46	23.66	2.00	0.00	1.00	0.00	4.48	24.20	2.00	0.00	1.00	0.00
4.50	23.89	2.00	0.00	1.00	0.00	4.52	24.24	2.00	0.00	1.00	0.00
4.54	24.07	2.00	0.00	1.00	0.00	4.56	23.89	2.00	0.00	1.00	0.00
4.58	23.53	2.00	0.00	1.00	0.00	4.60	22.45	2.00	0.00	1.00	0.00
4.62	21.62	2.00	0.00	1.00	0.00	4.64	20.79	2.00	0.00	1.00	0.00
4.66	20.45	2.00	0.00	1.00	0.00	4.68	20.47	2.00	0.00	1.00	0.00
4.70	19.92	2.00	0.00	1.00	0.00	4.72	18.74	2.00	0.00	1.00	0.00
4.74	17.77	2.00	0.00	1.00	0.00	4.76	16.90	2.00	0.00	1.00	0.00
4.78	16.26	2.00	0.00	1.00	0.00	4.80	15.39	2.00	0.00	1.00	0.00
4.82	14.86	2.00	0.00	1.00	0.00	4.84	13.16	2.00	0.00	1.00	0.00
4.86	14.52	2.00	0.00	1.00	0.00	4.88	13.79	2.00	0.00	1.00	0.00
4.91	13.32	2.00	0.00	1.00	0.00	4.92	13.35	2.00	0.00	1.00	0.00
4.94	13.36	2.00	0.00	1.00	0.00	4.96	13.65	2.00	0.00	1.00	0.00
4.98	14.42	2.00	0.00	1.00	0.00	5.00	14.60	2.00	0.00	1.00	0.00
5.02	15.16	2.00	0.00	1.00	0.00	5.04	15.26	2.00	0.00	1.00	0.00
5.06	15.68	2.00	0.00	1.00	0.00	5.08	15.68	2.00	0.00	1.00	0.00
5.10	15.89	2.00	0.00	1.00	0.00	5.12	15.52	2.00	0.00	1.00	0.00
5.14	15.59	2.00	0.00	1.00	0.00	5.16	14.70	2.00	0.00	1.00	0.00
5.18	14.30	2.00	0.00	1.00	0.00	5.20	13.89	2.00	0.00	1.00	0.00
5.22	13.93	2.00	0.00	1.00	0.00	5.24	13.91	2.00	0.00	1.00	0.00
5.26	14.09	2.00	0.00	1.00	0.00	5.28	14.74	2.00	0.00	1.00	0.00
5.30	15.12	2.00	0.00	1.00	0.00	5.32	15.84	2.00	0.00	1.00	0.00
5.34	16.54	2.00	0.00	1.00	0.00	5.36	17.33	2.00	0.00	1.00	0.00
5.38	17.67	2.00	0.00	1.00	0.00	5.40	17.30	2.00	0.00	1.00	0.00
5.42	17.20	2.00	0.00	1.00	0.00	5.44	17.17	2.00	0.00	1.00	0.00
5.46	17.60	2.00	0.00	1.00	0.00	5.48	18.24	2.00	0.00	1.00	0.00
5.50	17.81	2.00	0.00	1.00	0.00	5.52	17.38	2.00	0.00	1.00	0.00
5.54	17.21	2.00	0.00	1.00	0.00	5.56	16.55	2.00	0.00	1.00	0.00
5.58	16.29	2.00	0.00	1.00	0.00	5.60	15.80	2.00	0.00	1.00	0.00
5.62	15.90	2.00	0.00	1.00	0.00	5.64	16.17	2.00	0.00	1.00	0.00
5.66	15.91	2.00	0.00	1.00	0.00	5.68	15.81	2.00	0.00	1.00	0.00
5.70	15.71	2.00	0.00	1.00	0.00	5.72	15.88	2.00	0.00	1.00	0.00
5.74	15.79	2.00	0.00	1.00	0.00	5.76	15.83	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
5.78	15.73	2.00	0.00	1.00	0.00	5.80	15.28	2.00	0.00	1.00	0.00
5.82	14.92	2.00	0.00	1.00	0.00	5.84	14.87	2.00	0.00	1.00	0.00
5.86	15.04	2.00	0.00	1.00	0.00	5.88	15.28	2.00	0.00	1.00	0.00
5.90	16.16	2.00	0.00	1.00	0.00	5.92	17.01	2.00	0.00	1.00	0.00
5.94	17.66	2.00	0.00	1.00	0.00	5.96	17.79	2.00	0.00	1.00	0.00
5.98	17.56	2.00	0.00	1.00	0.00	6.00	18.08	2.00	0.00	1.00	0.00
6.02	18.42	2.00	0.00	1.00	0.00	6.04	18.13	2.00	0.00	1.00	0.00
6.06	18.22	2.00	0.00	1.00	0.00	6.08	18.18	2.00	0.00	1.00	0.00
6.10	18.08	2.00	0.00	1.00	0.00	6.12	18.33	2.00	0.00	1.00	0.00
6.14	19.02	2.00	0.00	1.00	0.00	6.16	19.08	2.00	0.00	1.00	0.00
6.18	19.42	2.00	0.00	1.00	0.00	6.20	20.23	2.00	0.00	1.00	0.00
6.22	21.35	2.00	0.00	1.00	0.00	6.24	22.15	2.00	0.00	1.00	0.00
6.26	21.92	2.00	0.00	1.00	0.00	6.28	21.78	2.00	0.00	1.00	0.00
6.30	21.42	2.00	0.00	1.00	0.00	6.32	20.20	2.00	0.00	1.00	0.00
6.34	20.00	2.00	0.00	1.00	0.00	6.36	19.55	2.00	0.00	1.00	0.00
6.38	19.05	2.00	0.00	1.00	0.00	6.40	18.63	2.00	0.00	1.00	0.00
6.42	18.35	2.00	0.00	1.00	0.00	6.44	17.96	2.00	0.00	1.00	0.00
6.46	17.33	2.00	0.00	1.00	0.00	6.48	17.60	2.00	0.00	1.00	0.00
6.50	18.09	2.00	0.00	1.00	0.00	6.52	18.29	2.00	0.00	1.00	0.00
6.54	18.20	2.00	0.00	1.00	0.00	6.56	17.52	2.00	0.00	1.00	0.00
6.58	16.41	2.00	0.00	1.00	0.00	6.60	15.49	2.00	0.00	1.00	0.00
6.62	15.06	2.00	0.00	1.00	0.00	6.64	15.13	2.00	0.00	1.00	0.00
6.66	14.48	2.00	0.00	1.00	0.00	6.68	14.43	2.00	0.00	1.00	0.00
6.70	14.68	2.00	0.00	1.00	0.00	6.72	15.10	2.00	0.00	1.00	0.00
6.74	15.38	2.00	0.00	1.00	0.00	6.76	15.49	2.00	0.00	1.00	0.00
6.78	15.43	2.00	0.00	1.00	0.00	6.80	14.95	2.00	0.00	1.00	0.00
6.82	15.33	2.00	0.00	1.00	0.00	6.84	16.18	2.00	0.00	1.00	0.00
6.86	16.56	2.00	0.00	1.00	0.00	6.88	16.65	2.00	0.00	1.00	0.00
6.90	16.39	2.00	0.00	1.00	0.00	6.92	16.06	2.00	0.00	1.00	0.00
6.94	16.48	2.00	0.00	1.00	0.00	6.96	17.49	2.00	0.00	1.00	0.00
6.98	18.47	2.00	0.00	1.00	0.00	7.00	17.31	2.00	0.00	1.00	0.00
7.02	16.57	2.00	0.00	1.00	0.00	7.04	15.23	2.00	0.00	1.00	0.00
7.06	14.93	2.00	0.00	1.00	0.00	7.08	14.85	2.00	0.00	1.00	0.00
7.10	14.91	2.00	0.00	1.00	0.00	7.12	15.31	2.00	0.00	1.00	0.00
7.14	16.11	2.00	0.00	1.00	0.00	7.16	16.82	2.00	0.00	1.00	0.00
7.18	17.13	2.00	0.00	1.00	0.00	7.20	18.04	2.00	0.00	1.00	0.00
7.22	18.52	2.00	0.00	1.00	0.00	7.24	19.46	2.00	0.00	1.00	0.00
7.26	20.74	2.00	0.00	1.00	0.00	7.28	21.21	2.00	0.00	1.00	0.00
7.30	22.40	2.00	0.00	1.00	0.00	7.32	22.92	2.00	0.00	1.00	0.00
7.34	22.91	2.00	0.00	1.00	0.00	7.36	22.46	2.00	0.00	1.00	0.00
7.38	21.88	2.00	0.00	1.00	0.00	7.40	21.23	2.00	0.00	1.00	0.00
7.42	21.14	2.00	0.00	1.00	0.00	7.44	20.07	2.00	0.00	1.00	0.00
7.46	19.29	2.00	0.00	1.00	0.00	7.48	18.88	2.00	0.00	1.00	0.00
7.50	18.76	2.00	0.00	1.00	0.00	7.52	19.70	2.00	0.00	1.00	0.00
7.54	20.27	2.00	0.00	1.00	0.00	7.56	20.07	2.00	0.00	1.00	0.00
7.58	19.89	2.00	0.00	1.00	0.00	7.60	19.34	2.00	0.00	1.00	0.00
7.62	18.96	2.00	0.00	1.00	0.00	7.64	19.21	2.00	0.00	1.00	0.00
7.66	19.29	2.00	0.00	1.00	0.00	7.68	19.66	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
7.70	19.37	2.00	0.00	1.00	0.00	7.72	19.22	2.00	0.00	1.00	0.00
7.74	19.33	2.00	0.00	1.00	0.00	7.76	19.87	2.00	0.00	1.00	0.00
7.78	20.89	2.00	0.00	1.00	0.00	7.80	21.27	2.00	0.00	1.00	0.00
7.82	16.16	2.00	0.00	1.00	0.00	7.84	21.06	2.00	0.00	1.00	0.00
7.86	20.73	2.00	0.00	1.00	0.00	7.88	20.08	2.00	0.00	1.00	0.00
7.90	20.24	2.00	0.00	1.00	0.00	7.92	20.63	2.00	0.00	1.00	0.00
7.94	20.91	2.00	0.00	1.00	0.00	7.96	21.58	2.00	0.00	1.00	0.00
7.98	21.13	2.00	0.00	1.00	0.00	8.00	20.64	2.00	0.00	1.00	0.00
8.02	20.14	2.00	0.00	1.00	0.00	8.04	19.91	2.00	0.00	1.00	0.00
8.06	19.26	2.00	0.00	1.00	0.00	8.08	19.21	2.00	0.00	1.00	0.00
8.10	19.78	2.00	0.00	1.00	0.00	8.12	20.60	2.00	0.00	1.00	0.00
8.14	20.54	2.00	0.00	1.00	0.00	8.16	20.01	2.00	0.00	1.00	0.00
8.18	19.37	2.00	0.00	1.00	0.00	8.20	18.93	2.00	0.00	1.00	0.00
8.22	18.04	2.00	0.00	1.00	0.00	8.24	17.14	2.00	0.00	1.00	0.00
8.26	16.20	2.00	0.00	1.00	0.00	8.28	15.71	2.00	0.00	1.00	0.00
8.30	15.08	2.00	0.00	1.00	0.00	8.32	15.08	2.00	0.00	1.00	0.00
8.34	14.56	2.00	0.00	1.00	0.00	8.36	14.27	2.00	0.00	1.00	0.00
8.38	14.39	2.00	0.00	1.00	0.00	8.40	14.40	2.00	0.00	1.00	0.00
8.42	14.08	2.00	0.00	1.00	0.00	8.44	14.12	2.00	0.00	1.00	0.00
8.46	14.08	2.00	0.00	1.00	0.00	8.48	13.52	2.00	0.00	1.00	0.00
8.50	13.29	2.00	0.00	1.00	0.00	8.52	12.98	2.00	0.00	1.00	0.00
8.54	12.45	2.00	0.00	1.00	0.00	8.56	12.47	2.00	0.00	1.00	0.00
8.58	12.57	2.00	0.00	1.00	0.00	8.60	12.53	2.00	0.00	1.00	0.00
8.62	13.01	2.00	0.00	1.00	0.00	8.64	13.50	2.00	0.00	1.00	0.00
8.66	13.95	2.00	0.00	1.00	0.00	8.68	14.62	2.00	0.00	1.00	0.00
8.70	15.07	2.00	0.00	1.00	0.00	8.72	15.06	2.00	0.00	1.00	0.00
8.74	14.43	2.00	0.00	1.00	0.00	8.76	13.78	2.00	0.00	1.00	0.00
8.78	12.66	2.00	0.00	1.00	0.00	8.80	11.82	2.00	0.00	1.00	0.00
8.82	11.58	2.00	0.00	1.00	0.00	8.84	11.68	2.00	0.00	1.00	0.00
8.86	11.64	2.00	0.00	1.00	0.00	8.88	11.28	2.00	0.00	1.00	0.00
8.91	11.37	2.00	0.00	1.00	0.00	8.92	11.92	2.00	0.00	1.00	0.00
8.94	12.25	2.00	0.00	1.00	0.00	8.96	12.53	2.00	0.00	1.00	0.00
8.98	12.44	2.00	0.00	1.00	0.00	9.00	12.82	2.00	0.00	1.00	0.00
9.02	12.91	2.00	0.00	1.00	0.00	9.04	13.49	2.00	0.00	1.00	0.00
9.06	14.83	2.00	0.00	1.00	0.00	9.08	16.27	2.00	0.00	1.00	0.00
9.10	17.73	2.00	0.00	1.00	0.00	9.12	18.27	2.00	0.00	1.00	0.00
9.14	18.06	2.00	0.00	1.00	0.00	9.16	17.69	2.00	0.00	1.00	0.00
9.18	17.14	2.00	0.00	1.00	0.00	9.20	16.75	2.00	0.00	1.00	0.00
9.22	16.52	2.00	0.00	1.00	0.00	9.24	17.16	2.00	0.00	1.00	0.00
9.26	17.14	2.00	0.00	1.00	0.00	9.28	16.57	2.00	0.00	1.00	0.00
9.30	16.34	2.00	0.00	1.00	0.00	9.32	16.13	2.00	0.00	1.00	0.00
9.34	15.93	2.00	0.00	1.00	0.00	9.36	16.29	2.00	0.00	1.00	0.00
9.38	16.16	2.00	0.00	1.00	0.00	9.40	15.83	2.00	0.00	1.00	0.00
9.42	15.23	2.00	0.00	1.00	0.00	9.44	14.95	2.00	0.00	1.00	0.00
9.46	14.04	2.00	0.00	1.00	0.00	9.48	13.76	2.00	0.00	1.00	0.00
9.50	13.66	2.00	0.00	1.00	0.00	9.52	13.67	2.00	0.00	1.00	0.00
9.54	13.54	2.00	0.00	1.00	0.00	9.56	13.78	2.00	0.00	1.00	0.00
9.58	13.47	2.00	0.00	1.00	0.00	9.60	13.19	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
9.62	13.12	2.00	0.00	1.00	0.00	9.64	12.90	2.00	0.00	1.00	0.00
9.66	12.67	2.00	0.00	1.00	0.00	9.68	12.58	2.00	0.00	1.00	0.00
9.70	12.46	2.00	0.00	1.00	0.00	9.72	12.44	2.00	0.00	1.00	0.00
9.74	12.92	2.00	0.00	1.00	0.00	9.76	13.67	2.00	0.00	1.00	0.00
9.78	14.47	2.00	0.00	1.00	0.00	9.80	14.79	2.00	0.00	1.00	0.00
9.82	15.30	2.00	0.00	1.00	0.00	9.84	15.16	2.00	0.00	1.00	0.00
9.86	15.15	2.00	0.00	1.00	0.00	9.88	15.08	2.00	0.00	1.00	0.00
9.90	14.76	2.00	0.00	1.00	0.00	9.92	14.61	2.00	0.00	1.00	0.00
9.94	14.50	2.00	0.00	1.00	0.00	9.96	14.33	2.00	0.00	1.00	0.00
9.98	13.75	2.00	0.00	1.00	0.00	10.00	14.04	2.00	0.00	1.00	0.00
10.02	13.77	2.00	0.00	1.00	0.00	10.04	13.65	2.00	0.00	1.00	0.00
10.06	13.96	2.00	0.00	1.00	0.00	10.08	14.19	2.00	0.00	1.00	0.00
10.10	14.19	2.00	0.00	1.00	0.00	10.12	14.37	2.00	0.00	1.00	0.00
10.14	14.15	2.00	0.00	1.00	0.00	10.16	14.00	2.00	0.00	1.00	0.00
10.18	14.31	2.00	0.00	1.00	0.00	10.20	14.79	2.00	0.00	1.00	0.00
10.22	14.59	2.00	0.00	1.00	0.00	10.24	14.42	2.00	0.00	1.00	0.00
10.26	13.93	2.00	0.00	1.00	0.00	10.28	13.79	2.00	0.00	1.00	0.00
10.30	13.14	2.00	0.00	1.00	0.00	10.32	13.13	2.00	0.00	1.00	0.00
10.34	12.86	2.00	0.00	1.00	0.00	10.36	12.77	2.00	0.00	1.00	0.00
10.38	12.56	2.00	0.00	1.00	0.00	10.40	12.71	2.00	0.00	1.00	0.00
10.42	12.90	2.00	0.00	1.00	0.00	10.44	13.08	2.00	0.00	1.00	0.00
10.46	13.19	2.00	0.00	1.00	0.00	10.48	13.42	2.00	0.00	1.00	0.00
10.50	13.48	2.00	0.00	1.00	0.00	10.52	13.42	2.00	0.00	1.00	0.00
10.54	13.13	2.00	0.00	1.00	0.00	10.56	13.22	2.00	0.00	1.00	0.00
10.58	13.57	2.00	0.00	1.00	0.00	10.60	14.17	2.00	0.00	1.00	0.00
10.62	14.81	2.00	0.00	1.00	0.00	10.64	14.63	2.00	0.00	1.00	0.00
10.66	14.63	2.00	0.00	1.00	0.00	10.68	14.64	2.00	0.00	1.00	0.00
10.70	14.60	2.00	0.00	1.00	0.00	10.72	15.24	2.00	0.00	1.00	0.00
10.74	16.35	2.00	0.00	1.00	0.00	10.76	16.53	2.00	0.00	1.00	0.00
10.78	16.73	2.00	0.00	1.00	0.00	10.80	9.82	2.00	0.00	1.00	0.00
10.82	18.14	2.00	0.00	1.00	0.00	10.84	18.27	2.00	0.00	1.00	0.00
10.86	17.86	2.00	0.00	1.00	0.00	10.88	17.50	2.00	0.00	1.00	0.00
10.90	16.76	2.00	0.00	1.00	0.00	10.92	16.07	2.00	0.00	1.00	0.00
10.94	15.61	2.00	0.00	1.00	0.00	10.96	15.28	2.00	0.00	1.00	0.00
10.98	14.92	2.00	0.00	1.00	0.00	11.00	14.77	2.00	0.00	1.00	0.00
11.02	14.82	2.00	0.00	1.00	0.00	11.04	14.77	2.00	0.00	1.00	0.00
11.06	14.48	2.00	0.00	1.00	0.00	11.08	14.05	2.00	0.00	1.00	0.00
11.10	14.09	2.00	0.00	1.00	0.00	11.12	14.19	2.00	0.00	1.00	0.00
11.14	14.26	2.00	0.00	1.00	0.00	11.16	13.64	2.00	0.00	1.00	0.00
11.18	13.26	2.00	0.00	1.00	0.00	11.20	12.84	2.00	0.00	1.00	0.00
11.22	12.46	2.00	0.00	1.00	0.00	11.24	12.68	2.00	0.00	1.00	0.00
11.26	12.62	2.00	0.00	1.00	0.00	11.28	12.51	2.00	0.00	1.00	0.00
11.30	12.92	2.00	0.00	1.00	0.00	11.32	13.34	2.00	0.00	1.00	0.00
11.34	13.73	2.00	0.00	1.00	0.00	11.36	13.87	2.00	0.00	1.00	0.00
11.38	14.17	2.00	0.00	1.00	0.00	11.40	14.60	2.00	0.00	1.00	0.00
11.42	14.63	2.00	0.00	1.00	0.00	11.44	13.79	2.00	0.00	1.00	0.00
11.46	13.68	2.00	0.00	1.00	0.00	11.48	12.96	2.00	0.00	1.00	0.00
11.50	13.06	2.00	0.00	1.00	0.00	11.52	13.12	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
11.54	13.34	2.00	0.00	1.00	0.00	11.56	14.39	2.00	0.00	1.00	0.00
11.58	15.05	2.00	0.00	1.00	0.00	11.60	15.51	2.00	0.00	1.00	0.00
11.62	15.24	2.00	0.00	1.00	0.00	11.64	14.88	2.00	0.00	1.00	0.00
11.66	14.40	2.00	0.00	1.00	0.00	11.68	14.18	2.00	0.00	1.00	0.00
11.70	13.59	2.00	0.00	1.00	0.00	11.72	13.62	2.00	0.00	1.00	0.00
11.74	13.38	2.00	0.00	1.00	0.00	11.76	13.18	2.00	0.00	1.00	0.00
11.78	12.80	2.00	0.00	1.00	0.00	11.80	12.53	2.00	0.00	1.00	0.00
11.82	13.18	2.00	0.00	1.00	0.00	11.84	13.00	2.00	0.00	1.00	0.00
11.86	12.85	2.00	0.00	1.00	0.00	11.88	13.09	2.00	0.00	1.00	0.00
11.90	13.19	2.00	0.00	1.00	0.00	11.92	13.04	2.00	0.00	1.00	0.00
11.94	13.02	2.00	0.00	1.00	0.00	11.96	12.68	2.00	0.00	1.00	0.00
11.98	12.74	2.00	0.00	1.00	0.00	12.00	12.45	2.00	0.00	1.00	0.00
12.02	11.49	2.00	0.00	1.00	0.00	12.04	10.40	2.00	0.00	1.00	0.00
12.06	9.96	2.00	0.00	1.00	0.00	12.08	9.61	2.00	0.00	1.00	0.00
12.10	9.24	2.00	0.00	1.00	0.00	12.13	8.96	2.00	0.00	1.00	0.00
12.14	9.16	2.00	0.00	1.00	0.00	12.17	8.81	2.00	0.00	1.00	0.00
12.18	8.37	2.00	0.00	1.00	0.00	12.20	7.96	2.00	0.00	1.00	0.00
12.22	7.76	2.00	0.00	1.00	0.00	12.24	7.73	2.00	0.00	1.00	0.00
12.26	7.65	2.00	0.00	1.00	0.00	12.29	7.87	2.00	0.00	1.00	0.00
12.30	8.36	2.00	0.00	1.00	0.00	12.32	8.58	2.00	0.00	1.00	0.00
12.34	9.16	2.00	0.00	1.00	0.00	12.36	9.44	2.00	0.00	1.00	0.00
12.38	9.06	2.00	0.00	1.00	0.00	12.40	8.78	2.00	0.00	1.00	0.00
12.42	8.91	2.00	0.00	1.00	0.00	12.44	8.68	2.00	0.00	1.00	0.00
12.46	8.39	2.00	0.00	1.00	0.00	12.48	7.78	2.00	0.00	1.00	0.00
12.50	7.04	2.00	0.00	1.00	0.00	12.52	6.41	2.00	0.00	1.00	0.00
12.54	6.61	2.00	0.00	1.00	0.00	12.56	6.21	2.00	0.00	1.00	0.00
12.58	6.23	2.00	0.00	1.00	0.00	12.60	6.45	2.00	0.00	1.00	0.00
12.62	6.58	2.00	0.00	1.00	0.00	12.64	6.67	2.00	0.00	1.00	0.00
12.66	6.32	2.00	0.00	1.00	0.00	12.68	6.18	2.00	0.00	1.00	0.00
12.70	6.25	2.00	0.00	1.00	0.00	12.72	6.29	2.00	0.00	1.00	0.00
12.74	6.45	2.00	0.00	1.00	0.00	12.76	6.98	2.00	0.00	1.00	0.00
12.78	7.62	2.00	0.00	1.00	0.00	12.80	8.26	2.00	0.00	1.00	0.00
12.82	8.13	2.00	0.00	1.00	0.00	12.84	8.30	2.00	0.00	1.00	0.00
12.86	8.28	2.00	0.00	1.00	0.00	12.88	8.05	2.00	0.00	1.00	0.00
12.90	8.13	2.00	0.00	1.00	0.00	12.92	8.02	2.00	0.00	1.00	0.00
12.94	8.12	2.00	0.00	1.00	0.00	12.96	8.20	2.00	0.00	1.00	0.00
12.98	8.40	2.00	0.00	1.00	0.00	13.00	8.34	2.00	0.00	1.00	0.00
13.02	8.21	2.00	0.00	1.00	0.00	13.04	8.31	2.00	0.00	1.00	0.00
13.06	8.15	2.00	0.00	1.00	0.00	13.08	8.03	2.00	0.00	1.00	0.00
13.10	7.50	2.00	0.00	1.00	0.00	13.12	7.21	2.00	0.00	1.00	0.00
13.14	6.92	2.00	0.00	1.00	0.00	13.16	6.70	2.00	0.00	1.00	0.00
13.19	6.60	2.00	0.00	1.00	0.00	13.20	6.47	2.00	0.00	1.00	0.00
13.22	6.14	2.00	0.00	1.00	0.00	13.24	5.93	2.00	0.00	1.00	0.00
13.26	5.93	2.00	0.00	1.00	0.00	13.28	5.99	2.00	0.00	1.00	0.00
13.30	6.16	2.00	0.00	1.00	0.00	13.32	6.11	2.00	0.00	1.00	0.00
13.34	6.26	2.00	0.00	1.00	0.00	13.36	7.19	2.00	0.00	1.00	0.00
13.38	7.81	2.00	0.00	1.00	0.00	13.40	8.63	2.00	0.00	1.00	0.00
13.42	9.39	2.00	0.00	1.00	0.00	13.44	9.92	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
13.46	10.40	2.00	0.00	1.00	0.00	13.48	10.17	2.00	0.00	1.00	0.00
13.50	9.67	2.00	0.00	1.00	0.00	13.52	8.90	2.00	0.00	1.00	0.00
13.54	8.68	2.00	0.00	1.00	0.00	13.56	9.17	2.00	0.00	1.00	0.00
13.58	9.29	2.00	0.00	1.00	0.00	13.60	9.22	2.00	0.00	1.00	0.00
13.62	9.21	2.00	0.00	1.00	0.00	13.64	9.31	2.00	0.00	1.00	0.00
13.66	9.46	2.00	0.00	1.00	0.00	13.68	9.62	2.00	0.00	1.00	0.00
13.70	9.70	2.00	0.00	1.00	0.00	13.72	9.75	2.00	0.00	1.00	0.00
13.74	9.87	2.00	0.00	1.00	0.00	13.76	9.75	2.00	0.00	1.00	0.00
13.78	9.76	2.00	0.00	1.00	0.00	13.80	9.93	2.00	0.00	1.00	0.00
13.82	9.96	2.00	0.00	1.00	0.00	13.84	10.04	2.00	0.00	1.00	0.00
13.86	10.40	2.00	0.00	1.00	0.00	13.88	10.47	2.00	0.00	1.00	0.00
13.90	10.44	2.00	0.00	1.00	0.00	13.92	10.52	2.00	0.00	1.00	0.00
13.94	10.27	2.00	0.00	1.00	0.00	13.96	10.28	2.00	0.00	1.00	0.00
13.98	10.42	2.00	0.00	1.00	0.00	14.00	10.58	2.00	0.00	1.00	0.00
14.02	11.25	2.00	0.00	1.00	0.00	14.04	11.48	2.00	0.00	1.00	0.00
14.06	11.64	2.00	0.00	1.00	0.00	14.08	12.05	2.00	0.00	1.00	0.00
14.10	12.19	2.00	0.00	1.00	0.00	14.12	11.86	2.00	0.00	1.00	0.00
14.14	12.34	2.00	0.00	1.00	0.00	14.16	12.66	2.00	0.00	1.00	0.00
14.18	12.59	2.00	0.00	1.00	0.00	14.20	12.57	2.00	0.00	1.00	0.00
14.22	12.56	2.00	0.00	1.00	0.00	14.24	12.69	2.00	0.00	1.00	0.00
14.26	12.57	2.00	0.00	1.00	0.00	14.28	12.65	2.00	0.00	1.00	0.00
14.30	12.68	2.00	0.00	1.00	0.00	14.32	12.75	2.00	0.00	1.00	0.00
14.34	12.75	2.00	0.00	1.00	0.00	14.36	12.52	2.00	0.00	1.00	0.00
14.38	12.32	2.00	0.00	1.00	0.00	14.40	11.96	2.00	0.00	1.00	0.00
14.42	12.12	2.00	0.00	1.00	0.00	14.44	12.08	2.00	0.00	1.00	0.00
14.46	11.96	2.00	0.00	1.00	0.00	14.48	11.76	2.00	0.00	1.00	0.00
14.50	11.72	2.00	0.00	1.00	0.00	14.52	12.11	2.00	0.00	1.00	0.00
14.54	11.91	2.00	0.00	1.00	0.00	14.56	11.85	2.00	0.00	1.00	0.00
14.58	11.99	2.00	0.00	1.00	0.00	14.60	11.68	2.00	0.00	1.00	0.00
14.62	11.73	2.00	0.00	1.00	0.00	14.64	11.83	2.00	0.00	1.00	0.00
14.66	11.92	2.00	0.00	1.00	0.00	14.68	11.99	2.00	0.00	1.00	0.00
14.70	11.65	2.00	0.00	1.00	0.00	14.72	11.30	2.00	0.00	1.00	0.00
14.74	11.34	2.00	0.00	1.00	0.00	14.76	11.70	2.00	0.00	1.00	0.00
14.78	5.69	2.00	0.00	1.00	0.00	14.80	12.91	2.00	0.00	1.00	0.00
14.82	13.26	2.00	0.00	1.00	0.00	14.84	13.96	2.00	0.00	1.00	0.00
14.86	15.11	2.00	0.00	1.00	0.00	14.88	16.32	2.00	0.00	1.00	0.00
14.90	16.47	2.00	0.00	1.00	0.00	14.92	16.81	2.00	0.00	1.00	0.00
14.94	17.32	2.00	0.00	1.00	0.00	14.96	19.21	2.00	0.00	1.00	0.00
14.98	18.21	2.00	0.00	1.00	0.00	15.00	18.18	2.00	0.00	1.00	0.00
15.02	17.16	2.00	0.00	1.00	0.00	15.04	16.68	2.00	0.00	1.00	0.00
15.06	15.22	2.00	0.00	1.00	0.00	15.08	14.11	2.00	0.00	1.00	0.00
15.10	13.47	2.00	0.00	1.00	0.00	15.12	13.08	2.00	0.00	1.00	0.00
15.14	12.65	2.00	0.00	1.00	0.00	15.16	12.21	2.00	0.00	1.00	0.00
15.18	12.27	2.00	0.00	1.00	0.00	15.20	12.60	2.00	0.00	1.00	0.00
15.22	12.72	2.00	0.00	1.00	0.00	15.24	12.99	2.00	0.00	1.00	0.00
15.26	13.48	2.00	0.00	1.00	0.00	15.28	13.53	2.00	0.00	1.00	0.00
15.30	13.31	2.00	0.00	1.00	0.00	15.32	12.97	2.00	0.00	1.00	0.00
15.34	12.65	2.00	0.00	1.00	0.00	15.36	12.78	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
15.38	12.48	2.00	0.00	1.00	0.00	15.40	12.13	2.00	0.00	1.00	0.00
15.42	11.38	2.00	0.00	1.00	0.00	15.44	10.52	2.00	0.00	1.00	0.00
15.46	9.65	2.00	0.00	1.00	0.00	15.48	9.44	2.00	0.00	1.00	0.00
15.50	8.92	2.00	0.00	1.00	0.00	15.52	8.31	2.00	0.00	1.00	0.00
15.54	7.94	2.00	0.00	1.00	0.00	15.56	7.66	2.00	0.00	1.00	0.00
15.58	7.21	2.00	0.00	1.00	0.00	15.60	7.01	2.00	0.00	1.00	0.00
15.62	7.23	2.00	0.00	1.00	0.00	15.64	7.41	2.00	0.00	1.00	0.00
15.66	7.95	2.00	0.00	1.00	0.00	15.68	8.76	2.00	0.00	1.00	0.00
15.70	9.44	2.00	0.00	1.00	0.00	15.72	10.37	2.00	0.00	1.00	0.00
15.74	10.97	2.00	0.00	1.00	0.00	15.76	11.17	2.00	0.00	1.00	0.00
15.78	7.18	2.00	0.00	1.00	0.00	15.80	10.71	2.00	0.00	1.00	0.00
15.82	10.68	2.00	0.00	1.00	0.00	15.85	10.49	2.00	0.00	1.00	0.00
15.86	10.07	2.00	0.00	1.00	0.00	15.88	9.76	2.00	0.00	1.00	0.00
15.90	9.69	2.00	0.00	1.00	0.00	15.92	9.54	2.00	0.00	1.00	0.00
15.94	9.42	2.00	0.00	1.00	0.00	15.96	9.21	2.00	0.00	1.00	0.00
15.98	9.40	2.00	0.00	1.00	0.00	16.00	9.49	2.00	0.00	1.00	0.00
16.02	10.31	2.00	0.00	1.00	0.00	16.04	10.90	2.00	0.00	1.00	0.00
16.06	11.13	2.00	0.00	1.00	0.00	16.08	11.14	2.00	0.00	1.00	0.00
16.10	10.84	2.00	0.00	1.00	0.00	16.12	9.95	2.00	0.00	1.00	0.00
16.14	9.25	2.00	0.00	1.00	0.00	16.16	8.67	2.00	0.00	1.00	0.00
16.18	8.44	2.00	0.00	1.00	0.00	16.20	8.67	2.00	0.00	1.00	0.00
16.22	8.86	2.00	0.00	1.00	0.00	16.24	8.70	2.00	0.00	1.00	0.00
16.26	8.42	2.00	0.00	1.00	0.00	16.28	8.43	2.00	0.00	1.00	0.00
16.30	8.64	2.00	0.00	1.00	0.00	16.32	9.62	2.00	0.00	1.00	0.00
16.34	10.80	2.00	0.00	1.00	0.00	16.36	11.73	2.00	0.00	1.00	0.00
16.38	11.70	2.00	0.00	1.00	0.00	16.40	11.34	2.00	0.00	1.00	0.00
16.42	10.58	2.00	0.00	1.00	0.00	16.44	9.92	2.00	0.00	1.00	0.00
16.46	9.27	2.00	0.00	1.00	0.00	16.48	8.71	2.00	0.00	1.00	0.00
16.50	8.71	2.00	0.00	1.00	0.00	16.52	8.77	2.00	0.00	1.00	0.00
16.54	8.70	2.00	0.00	1.00	0.00	16.56	8.58	2.00	0.00	1.00	0.00
16.58	8.94	2.00	0.00	1.00	0.00	16.60	8.98	2.00	0.00	1.00	0.00
16.62	9.01	2.00	0.00	1.00	0.00	16.64	8.93	2.00	0.00	1.00	0.00
16.66	8.83	2.00	0.00	1.00	0.00	16.68	8.67	2.00	0.00	1.00	0.00
16.70	8.84	2.00	0.00	1.00	0.00	16.72	9.01	2.00	0.00	1.00	0.00
16.74	9.88	2.00	0.00	1.00	0.00	16.76	10.62	2.00	0.00	1.00	0.00
16.79	11.94	2.00	0.00	1.00	0.00	16.80	12.03	2.00	0.00	1.00	0.00
16.82	11.18	2.00	0.00	1.00	0.00	16.84	11.12	2.00	0.00	1.00	0.00
16.86	11.21	2.00	0.00	1.00	0.00						

Total estimated settlement: 0.00

Abbreviations

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumentric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

:: Strength loss calculation Idriss & Boulanger (2008) ::

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.02	0.98	16.74	2.71	45.35	2.49	0.07	0.60
0.04	1.09	18.60	3.26	60.60	2.59	0.08	0.61
0.06	1.16	19.71	3.66	72.24	2.65	0.08	86.22
0.08	1.23	20.90	4.22	88.18	2.73	0.08	67.34
0.10	1.27	21.58	4.78	103.05	2.80	0.08	54.77
0.12	1.29	21.89	5.30	116.09	2.86	0.08	45.71
0.14	1.30	22.11	5.73	126.68	2.90	0.08	39.14
0.17	1.29	21.95	6.20	136.11	2.95	0.08	31.59
0.18	1.28	21.66	6.62	143.39	2.99	0.07	29.34
0.20	1.26	21.31	7.03	149.69	3.02	0.07	25.79
0.23	1.24	21.07	7.32	154.22	3.05	0.07	21.99
0.24	1.23	20.88	7.55	157.62	3.07	0.07	20.84
0.26	1.22	20.60	7.71	158.82	3.08	0.07	18.89
0.29	1.21	20.40	7.76	158.39	3.09	0.07	16.69
0.30	1.20	20.24	7.73	156.59	3.08	0.07	15.98
0.32	1.19	20.12	7.70	155.02	3.08	0.07	14.85
0.34	1.18	19.99	7.67	153.36	3.08	0.07	13.86
0.36	1.17	19.82	7.70	152.62	3.08	0.07	12.96
0.38	1.19	20.06	7.59	152.29	3.07	0.07	12.40
0.40	1.22	20.56	7.41	152.30	3.06	0.07	12.06
0.42	1.25	21.06	7.23	152.39	3.04	0.07	11.75
0.44	1.27	21.47	7.09	152.20	3.03	0.07	11.41
0.46	1.28	21.60	7.05	152.25	3.03	0.08	10.97
0.48	1.29	21.74	7.00	152.28	3.02	0.08	10.57
0.50	1.28	21.63	7.02	151.89	3.02	0.08	10.09
0.53	1.29	21.69	6.95	150.85	3.02	0.08	9.53
0.54	1.29	21.70	6.88	149.36	3.01	0.08	9.35
0.56	1.28	21.61	6.83	147.61	3.01	0.08	8.98
0.58	1.26	21.27	6.85	145.67	3.01	0.07	8.52
0.60	1.24	20.82	6.91	143.85	3.01	0.07	8.06
0.62	1.22	20.53	6.92	142.13	3.02	0.07	7.83
0.64	1.19	19.98	7.06	141.08	3.03	0.07	7.50
0.66	1.13	18.97	7.38	139.96	3.05	0.07	7.02
0.68	1.04	17.54	7.90	138.67	3.10	0.07	6.40
0.70	0.95	15.85	8.58	136.05	3.15	0.07	5.70
0.72	0.85	14.21	9.33	132.55	3.21	0.07	5.04
0.74	0.75	12.59	10.18	128.16	3.26	0.06	4.40
0.76	0.68	11.27	10.98	123.78	3.32	0.06	3.89
0.78	0.62	10.36	11.52	119.38	3.35	0.06	3.53
0.80	0.59	9.73	11.89	115.59	3.37	0.06	3.27
0.82	0.58	9.57	11.74	112.37	3.36	0.06	3.18
0.84	0.61	10.07	10.93	110.11	3.31	0.06	3.31
0.86	0.71	11.78	9.02	106.24	3.18	0.06	3.82
0.88	0.85	14.25	7.14	101.76	3.03	0.07	4.57
0.90	1.00	16.70	5.80	96.78	2.91	0.07	5.30
0.92	1.14	19.03	5.07	96.50	2.83	0.08	5.97
0.94	1.24	20.74	4.79	99.44	2.80	0.08	6.43
0.96	1.32	22.18	4.74	105.02	2.79	0.08	6.80

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.98	1.35	22.57	5.03	113.46	2.83	0.08	6.84
1.00	1.35	22.72	5.36	121.87	2.87	0.08	6.80
1.02	1.35	22.59	5.78	130.55	2.91	0.08	6.69
1.04	1.34	22.43	6.15	137.99	2.94	0.08	6.56
1.07	1.32	22.13	6.53	144.49	2.98	0.08	6.36
1.08	1.30	21.81	6.87	149.88	3.01	0.08	6.23
1.10	1.30	21.75	7.05	153.25	3.03	0.08	6.14
1.12	1.30	21.70	7.14	154.97	3.03	0.08	6.06
1.14	1.30	21.81	7.12	155.20	3.03	0.08	6.02
1.16	1.32	22.03	7.02	154.73	3.02	0.08	6.01
1.18	1.33	22.32	6.91	154.29	3.01	0.08	6.02
1.20	1.35	22.65	6.79	153.71	3.00	0.08	6.04
1.22	1.36	22.69	6.75	153.08	3.00	0.08	5.99
1.24	1.35	22.59	6.76	152.72	3.00	0.08	5.90
1.26	1.34	22.46	6.82	153.10	3.01	0.08	5.80
1.28	1.34	22.40	6.87	153.77	3.01	0.08	5.72
1.30	1.34	22.37	6.89	154.21	3.01	0.08	5.65
1.32	1.34	22.32	6.91	154.19	3.01	0.08	5.58
1.34	1.35	22.46	6.85	153.94	3.01	0.08	5.56
1.36	1.35	22.60	6.81	153.83	3.01	0.08	5.54
1.38	1.35	22.51	6.82	153.46	3.01	0.08	5.46
1.40	1.33	22.16	6.91	153.17	3.01	0.08	5.32
1.42	1.30	21.61	7.08	152.87	3.03	0.08	5.14
1.44	1.27	21.13	7.20	152.19	3.04	0.07	4.98
1.46	1.24	20.61	7.33	151.10	3.05	0.07	4.81
1.48	1.21	20.19	7.42	149.82	3.06	0.07	4.67
1.50	1.19	19.75	7.51	148.34	3.07	0.07	4.52
1.52	1.15	19.13	7.65	146.28	3.08	0.07	4.34
1.54	1.12	18.53	7.74	143.32	3.08	0.07	4.17
1.56	1.08	17.86	7.86	140.41	3.09	0.07	3.98
1.58	1.05	17.31	7.98	138.18	3.10	0.07	3.82
1.60	1.02	16.84	8.11	136.67	3.11	0.07	3.69
1.62	1.00	16.48	8.23	135.69	3.12	0.07	3.58
1.64	1.00	16.44	8.20	134.84	3.12	0.07	3.54
1.66	1.01	16.68	8.06	134.42	3.11	0.07	3.56
1.68	1.05	17.30	7.76	134.17	3.09	0.07	3.66
1.70	1.12	18.47	7.22	133.39	3.04	0.07	3.88
1.72	1.19	19.78	6.66	131.81	2.99	0.07	4.12
1.74	1.27	21.07	6.15	129.64	2.95	0.08	4.35
1.76	1.31	21.67	5.93	128.43	2.92	0.08	4.44
1.78	1.34	22.26	5.72	127.25	2.90	0.08	4.52
1.80	1.35	22.38	5.67	126.81	2.90	0.08	4.51
1.82	1.36	22.48	5.62	126.28	2.89	0.08	4.50
1.84	1.34	22.14	5.67	125.60	2.90	0.08	4.39
1.86	1.30	21.52	5.78	124.41	2.91	0.08	4.24
1.88	1.26	20.87	5.90	123.12	2.92	0.08	4.08
1.90	1.22	20.23	6.02	121.80	2.93	0.08	3.92
1.92	1.21	19.93	5.99	119.35	2.93	0.08	3.84

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
1.94	1.18	19.55	5.94	116.07	2.92	0.08	3.74
1.96	1.16	19.09	5.91	112.71	2.92	0.07	3.62
1.98	1.13	18.52	5.96	110.47	2.93	0.07	3.49
2.01	1.09	17.88	6.07	108.58	2.94	0.07	3.33
2.02	1.06	17.38	6.15	106.95	2.95	0.07	3.23
2.04	1.04	17.03	6.19	105.35	2.95	0.07	3.14
2.06	1.04	17.00	6.12	104.07	2.94	0.07	3.12
2.08	1.05	17.16	6.00	103.01	2.93	0.07	3.13
2.10	1.07	17.48	5.85	102.29	2.92	0.07	3.16
2.12	1.08	17.68	5.80	102.47	2.91	0.07	3.18
2.14	1.08	17.68	5.85	103.45	2.92	0.07	3.16
2.16	1.08	17.64	5.93	104.68	2.92	0.07	3.13
2.18	1.07	17.54	6.03	105.79	2.93	0.07	3.09
2.20	1.05	17.23	6.21	107.02	2.95	0.07	3.02
2.22	1.03	16.77	6.47	108.42	2.97	0.07	2.92
2.24	0.99	16.11	6.81	109.63	3.01	0.07	2.79
2.26	0.95	15.40	7.15	110.14	3.04	0.07	2.65
2.28	0.91	14.69	7.47	109.68	3.06	0.07	2.51
2.30	0.86	13.98	7.79	108.90	3.09	0.07	2.37
2.32	0.83	13.40	8.06	107.99	3.11	0.07	2.26
2.34	0.79	12.74	8.40	107.00	3.14	0.06	2.13
2.36	0.76	12.23	8.61	105.36	3.15	0.06	2.04
2.38	0.73	11.74	8.75	102.74	3.16	0.06	1.94
2.40	0.71	11.29	8.83	99.76	3.17	0.06	1.86
2.42	0.68	10.79	8.93	96.34	3.18	0.06	1.77
2.44	0.65	10.38	8.92	92.57	3.18	0.06	1.69
2.46	0.63	9.95	8.84	87.98	3.17	0.06	1.61
2.48	0.61	9.55	8.73	83.41	3.16	0.06	1.54
2.50	0.58	9.05	8.75	79.18	3.16	0.06	1.45
2.52	0.56	8.67	8.65	75.02	3.16	0.06	1.38
2.54	0.55	8.60	8.21	70.66	3.12	0.06	1.36
2.56	0.56	8.78	7.62	66.91	3.08	0.06	1.39
2.58	0.58	9.01	7.13	64.26	3.03	0.06	1.42
2.60	0.59	9.25	6.72	62.16	3.00	0.06	1.45
2.62	0.59	9.30	6.48	60.25	2.98	0.06	1.45
2.64	0.60	9.38	6.18	58.00	2.95	0.06	1.45
2.66	0.60	9.41	5.98	56.31	2.93	0.06	1.45
2.68	0.61	9.59	5.79	55.48	2.91	0.06	1.47
2.70	0.62	9.74	5.73	55.83	2.90	0.06	1.49
2.72	0.63	9.84	5.77	56.81	2.91	0.06	1.50
2.74	0.63	9.95	5.76	57.34	2.91	0.06	1.51
2.76	0.63	9.93	5.86	58.19	2.92	0.06	1.50
2.78	0.63	9.79	6.09	59.65	2.94	0.06	1.47
2.80	0.61	9.59	6.40	61.40	2.97	0.06	1.44
2.82	0.60	9.34	6.79	63.49	3.00	0.06	1.39
2.84	0.59	9.15	7.11	65.05	3.03	0.06	1.36
2.86	0.61	9.54	6.94	66.27	3.02	0.06	1.41
2.88	0.65	10.21	6.54	66.79	2.98	0.06	1.50

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
2.90	0.69	10.82	6.22	67.27	2.95	0.06	1.59
2.92	0.70	10.98	6.14	67.47	2.94	0.06	1.60
2.94	0.71	11.11	6.10	67.74	2.94	0.06	1.62
2.96	0.72	11.42	5.91	67.46	2.92	0.07	1.65
2.98	0.76	12.02	5.55	66.68	2.88	0.07	1.73
3.00	0.80	12.72	5.22	66.32	2.85	0.07	1.82
3.02	0.83	13.22	5.03	66.59	2.83	0.07	1.89
3.04	0.84	13.34	5.08	67.81	2.83	0.07	1.90
3.06	0.82	13.00	5.38	69.89	2.87	0.07	1.84
3.08	0.78	12.42	5.88	73.00	2.92	0.07	1.75
3.10	0.75	11.75	6.52	76.58	2.98	0.06	1.65
3.12	0.72	11.31	7.10	80.28	3.03	0.06	1.58
3.14	0.73	11.52	7.22	83.21	3.04	0.06	1.60
3.16	0.73	11.50	7.44	85.55	3.06	0.06	1.59
3.18	0.74	11.72	7.30	85.57	3.05	0.06	1.61
3.20	0.75	11.74	7.21	84.63	3.04	0.06	1.61
3.22	0.77	12.13	6.85	83.16	3.01	0.06	1.66
3.24	0.80	12.59	6.53	82.25	2.98	0.06	1.71
3.26	0.84	13.34	6.13	81.75	2.94	0.07	1.80
3.28	0.90	14.31	5.68	81.28	2.90	0.07	1.93
3.30	0.95	15.24	5.31	80.88	2.86	0.07	2.04
3.32	0.99	15.80	5.18	81.77	2.84	0.07	2.11
3.34	0.99	15.90	5.28	84.01	2.86	0.07	2.11
3.36	0.98	15.60	5.59	87.22	2.89	0.07	2.06
3.38	0.95	15.08	6.04	91.08	2.93	0.07	1.99
3.40	0.91	14.48	6.53	94.54	2.98	0.07	1.90
3.42	0.88	13.96	6.94	96.94	3.02	0.07	1.82
3.44	0.84	13.31	7.36	97.94	3.05	0.07	1.73
3.46	0.79	12.46	7.90	98.50	3.10	0.06	1.61
3.48	0.74	11.49	8.62	99.00	3.15	0.06	1.48
3.50	0.70	10.90	9.00	98.07	3.18	0.06	1.40
3.52	0.71	11.02	8.66	95.47	3.16	0.06	1.41
3.54	0.75	11.63	7.83	91.05	3.09	0.06	1.48
3.56	0.78	12.28	7.00	85.98	3.02	0.06	1.55
3.58	0.79	12.33	6.60	81.33	2.99	0.07	1.55
3.60	0.77	11.99	6.51	78.02	2.98	0.06	1.50
3.62	0.73	11.30	6.78	76.64	3.00	0.06	1.41
3.64	0.73	11.36	6.71	76.21	3.00	0.06	1.41
3.66	0.80	12.46	6.09	75.92	2.94	0.07	1.54
3.68	0.91	14.44	5.14	74.25	2.84	0.07	1.78
3.70	1.02	16.32	4.45	72.55	2.76	0.08	2.01
3.72	1.08	17.21	4.26	73.37	2.74	0.08	2.11
3.74	1.10	17.53	4.37	76.66	2.75	0.08	2.14
3.76	1.10	17.58	4.66	81.85	2.78	0.08	2.13
3.78	1.11	17.77	4.88	86.77	2.81	0.08	2.15
3.80	1.13	18.03	5.05	91.07	2.83	0.08	2.17
3.82	1.17	18.70	5.06	94.70	2.83	0.08	2.24
3.84	1.20	19.30	5.16	99.48	2.84	0.08	2.30

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
3.86	1.24	20.01	5.26	105.31	2.85	0.08	2.38
3.88	1.26	20.26	5.48	110.93	2.88	0.08	2.40
3.90	1.26	20.34	5.70	115.97	2.90	0.08	2.40
3.92	1.25	20.13	5.97	120.14	2.93	0.08	2.36
3.94	1.25	20.09	6.19	124.42	2.95	0.07	2.35
3.96	1.27	20.40	6.21	126.61	2.95	0.08	2.37
3.98	1.29	20.78	6.11	127.05	2.94	0.08	2.40
4.00	1.33	21.42	5.86	125.45	2.92	0.08	2.47
4.02	1.36	21.93	5.65	123.92	2.90	0.08	2.51
4.05	1.38	22.20	5.59	123.98	2.89	0.08	2.53
4.06	1.37	22.11	5.69	125.72	2.90	0.08	2.51
4.08	1.37	22.13	5.83	128.95	2.91	0.08	2.50
4.10	1.38	22.23	5.97	132.74	2.93	0.08	2.50
4.12	1.37	22.15	6.18	136.95	2.95	0.08	2.48
4.14	1.36	21.84	6.42	140.29	2.97	0.08	2.44
4.16	1.34	21.62	6.55	141.71	2.98	0.08	2.40
4.18	1.34	21.49	6.57	141.28	2.98	0.08	2.38
4.20	1.33	21.33	6.55	139.70	2.98	0.08	2.35
4.22	1.30	20.90	6.62	138.44	2.99	0.08	2.29
4.24	1.26	20.24	6.81	137.87	3.01	0.07	2.21
4.26	1.21	19.38	7.11	137.72	3.03	0.07	2.11
4.28	1.16	18.48	7.47	138.02	3.06	0.07	2.00
4.30	1.12	17.76	7.81	138.78	3.09	0.07	1.91
4.32	1.09	17.28	8.10	139.98	3.11	0.07	1.85
4.34	1.09	17.30	8.12	140.42	3.12	0.07	1.85
4.36	1.14	18.08	7.73	139.71	3.08	0.07	1.92
4.38	1.22	19.35	7.15	138.34	3.04	0.07	2.05
4.40	1.31	20.88	6.55	136.75	2.98	0.07	2.20
4.42	1.38	22.11	6.15	135.89	2.94	0.08	2.32
4.44	1.44	23.13	5.85	135.23	2.91	0.08	2.42
4.46	1.49	23.95	5.65	135.18	2.89	0.08	2.49
4.48	1.51	24.29	5.58	135.54	2.89	0.08	2.52
4.50	1.52	24.56	5.58	137.02	2.89	0.08	2.54
4.52	1.52	24.56	5.67	139.35	2.90	0.08	2.53
4.54	1.53	24.61	5.81	142.86	2.91	0.08	2.52
4.56	1.52	24.40	6.01	146.63	2.93	0.08	2.49
4.58	1.48	23.84	6.33	150.82	2.96	0.08	2.42
4.60	1.44	23.03	6.69	154.16	3.00	0.08	2.33
4.62	1.38	22.04	7.07	155.80	3.03	0.08	2.22
4.64	1.34	21.33	7.27	155.02	3.05	0.07	2.14
4.66	1.31	20.94	7.28	152.52	3.05	0.07	2.09
4.68	1.30	20.65	7.25	149.82	3.04	0.07	2.05
4.70	1.26	20.04	7.37	147.61	3.05	0.07	1.99
4.72	1.20	19.06	7.66	146.02	3.08	0.07	1.88
4.74	1.14	17.95	8.07	144.77	3.11	0.07	1.76
4.76	1.09	17.05	8.44	143.88	3.14	0.07	1.67
4.78	1.04	16.19	8.84	143.07	3.17	0.07	1.58
4.80	0.99	15.45	9.20	142.18	3.20	0.07	1.50

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
4.82	0.93	14.32	9.71	139.15	3.23	0.07	1.39
4.84	0.91	14.03	9.74	136.64	3.23	0.07	1.35
4.86	0.89	13.66	9.79	133.77	3.24	0.07	1.31
4.88	0.90	13.76	9.64	132.65	3.23	0.07	1.32
4.91	0.87	13.34	9.75	130.06	3.24	0.07	1.27
4.92	0.86	13.22	9.61	127.03	3.23	0.07	1.25
4.94	0.87	13.36	9.26	123.70	3.20	0.07	1.26
4.96	0.90	13.78	8.75	120.68	3.16	0.07	1.30
4.98	0.93	14.28	8.28	118.23	3.13	0.07	1.34
5.00	0.96	14.87	7.81	116.20	3.09	0.07	1.39
5.02	0.98	15.22	7.55	114.93	3.07	0.07	1.42
5.04	1.01	15.65	7.28	113.92	3.05	0.07	1.46
5.06	1.02	15.88	7.16	113.75	3.04	0.07	1.47
5.08	1.04	16.15	7.07	114.10	3.03	0.07	1.49
5.10	1.04	16.11	7.13	114.82	3.03	0.07	1.48
5.12	1.04	16.10	7.14	115.00	3.03	0.07	1.48
5.14	1.01	15.67	7.39	115.89	3.06	0.07	1.43
5.16	0.99	15.23	7.63	116.23	3.08	0.07	1.39
5.18	0.95	14.61	7.96	116.29	3.10	0.07	1.33
5.20	0.93	14.34	8.02	114.95	3.11	0.07	1.30
5.22	0.93	14.22	7.97	113.25	3.10	0.07	1.28
5.24	0.93	14.32	7.77	111.31	3.09	0.07	1.29
5.26	0.95	14.66	7.44	109.09	3.06	0.07	1.31
5.28	0.98	15.15	7.05	106.84	3.03	0.07	1.35
5.30	1.03	15.87	6.60	104.69	2.99	0.07	1.41
5.32	1.07	16.60	6.22	103.24	2.95	0.07	1.47
5.34	1.12	17.49	5.81	101.65	2.91	0.07	1.55
5.36	1.17	18.23	5.56	101.32	2.89	0.07	1.61
5.38	1.19	18.56	5.51	102.30	2.88	0.08	1.63
5.40	1.19	18.54	5.70	105.73	2.90	0.07	1.62
5.42	1.18	18.38	5.96	109.50	2.93	0.07	1.60
5.44	1.19	18.54	6.07	112.51	2.94	0.07	1.61
5.46	1.21	18.99	6.04	114.66	2.93	0.07	1.65
5.48	1.23	19.28	6.08	117.19	2.94	0.07	1.67
5.50	1.23	19.23	6.21	119.45	2.95	0.07	1.66
5.52	1.21	18.85	6.38	120.30	2.97	0.07	1.62
5.54	1.18	18.38	6.52	119.86	2.98	0.07	1.57
5.56	1.16	17.97	6.65	119.61	2.99	0.07	1.53
5.58	1.12	17.44	6.88	119.87	3.01	0.07	1.48
5.60	1.11	17.20	6.97	119.83	3.02	0.07	1.46
5.62	1.11	17.18	6.91	118.72	3.01	0.07	1.45
5.64	1.11	17.25	6.82	117.68	3.01	0.07	1.45
5.66	1.11	17.25	6.79	117.06	3.00	0.07	1.45
5.68	1.11	17.09	6.85	117.05	3.01	0.07	1.43
5.70	1.11	17.11	6.80	116.37	3.01	0.07	1.43
5.72	1.11	17.13	6.75	115.61	3.00	0.07	1.42
5.74	1.11	17.20	6.68	114.82	2.99	0.07	1.42
5.76	1.11	17.17	6.69	114.85	3.00	0.07	1.42

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
5.78	1.10	16.98	6.78	115.19	3.00	0.07	1.40
5.80	1.08	16.64	6.99	116.29	3.02	0.07	1.37
5.82	1.06	16.33	7.11	116.08	3.03	0.07	1.34
5.84	1.06	16.27	7.13	116.01	3.03	0.07	1.33
5.86	1.07	16.46	7.04	115.85	3.03	0.07	1.34
5.88	1.11	17.03	6.85	116.66	3.01	0.07	1.38
5.90	1.16	17.87	6.47	115.59	2.97	0.07	1.44
5.92	1.21	18.88	6.01	113.38	2.93	0.07	1.52
5.94	1.26	19.57	5.70	111.58	2.90	0.07	1.57
5.96	1.27	19.82	5.67	112.40	2.90	0.07	1.59
5.98	1.28	20.02	5.70	114.13	2.90	0.07	1.60
6.00	1.30	20.31	5.74	116.65	2.90	0.07	1.62
6.02	1.32	20.58	5.81	119.62	2.91	0.07	1.63
6.04	1.32	20.68	5.99	123.90	2.93	0.07	1.64
6.06	1.32	20.61	6.22	128.25	2.95	0.07	1.63
6.08	1.32	20.62	6.37	131.45	2.97	0.07	1.62
6.10	1.33	20.70	6.44	133.29	2.97	0.07	1.62
6.12	1.35	21.09	6.36	134.04	2.96	0.07	1.65
6.14	1.38	21.54	6.27	135.05	2.96	0.07	1.68
6.16	1.40	22.03	6.21	136.88	2.95	0.07	1.71
6.18	1.44	22.57	6.15	138.80	2.94	0.07	1.75
6.20	1.50	23.58	5.93	139.87	2.92	0.08	1.82
6.22	1.57	24.78	5.63	139.62	2.89	0.08	1.91
6.24	1.61	25.54	5.47	139.72	2.88	0.08	1.96
6.26	1.63	25.76	5.46	140.68	2.88	0.08	1.97
6.28	1.61	25.48	5.58	142.30	2.89	0.08	1.94
6.30	1.57	24.77	5.82	144.23	2.91	0.08	1.88
6.32	1.53	24.04	6.05	145.42	2.94	0.08	1.82
6.34	1.48	23.27	6.33	147.22	2.96	0.07	1.76
6.36	1.45	22.81	6.54	149.23	2.98	0.07	1.72
6.38	1.42	22.25	6.76	150.49	3.00	0.07	1.67
6.40	1.39	21.76	6.88	149.80	3.01	0.07	1.63
6.42	1.37	21.32	6.93	147.80	3.02	0.07	1.59
6.44	1.34	20.79	7.03	146.10	3.02	0.07	1.55
6.46	1.32	20.50	7.07	144.91	3.03	0.07	1.52
6.48	1.33	20.60	6.95	143.12	3.02	0.07	1.52
6.50	1.35	21.06	6.69	140.92	3.00	0.07	1.55
6.52	1.37	21.35	6.45	137.73	2.97	0.07	1.57
6.54	1.36	21.13	6.36	134.51	2.97	0.07	1.55
6.56	1.31	20.34	6.46	131.30	2.97	0.07	1.49
6.58	1.24	19.19	6.72	128.88	3.00	0.07	1.40
6.60	1.18	18.14	7.00	127.05	3.02	0.07	1.32
6.62	1.15	17.61	7.12	125.37	3.03	0.07	1.28
6.64	1.13	17.20	7.30	125.66	3.05	0.07	1.24
6.66	1.12	16.96	7.51	127.47	3.07	0.07	1.22
6.68	1.11	16.81	7.72	129.82	3.08	0.07	1.21
6.70	1.13	17.11	7.65	130.95	3.08	0.07	1.23
6.72	1.15	17.55	7.46	130.99	3.06	0.07	1.25

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
6.74	1.17	17.87	7.33	130.97	3.05	0.07	1.28
6.76	1.18	17.99	7.29	131.09	3.05	0.07	1.29
6.78	1.18	17.78	7.36	130.85	3.05	0.07	1.27
6.80	1.17	17.69	7.36	130.17	3.05	0.07	1.26
6.82	1.19	17.98	7.15	128.62	3.04	0.07	1.28
6.84	1.24	18.64	6.92	129.01	3.02	0.07	1.33
6.86	1.27	19.18	6.82	130.78	3.01	0.07	1.37
6.88	1.28	19.24	6.98	134.29	3.02	0.07	1.37
6.90	1.27	19.00	7.19	136.71	3.04	0.07	1.36
6.92	1.27	18.90	7.29	137.88	3.05	0.07	1.35
6.94	1.30	19.36	7.13	137.95	3.03	0.07	1.38
6.96	1.36	20.37	6.74	137.28	3.00	0.07	1.46
6.98	1.39	20.70	6.56	135.79	2.98	0.07	1.48
7.00	1.36	20.26	6.60	133.69	2.99	0.07	1.45
7.02	1.28	18.82	7.03	132.28	3.03	0.07	1.34
7.04	1.22	17.78	7.39	131.43	3.06	0.07	1.27
7.06	1.18	17.03	7.70	131.10	3.08	0.07	1.22
7.08	1.17	16.88	7.72	130.30	3.08	0.07	1.21
7.10	1.18	17.02	7.61	129.60	3.07	0.07	1.22
7.12	1.22	17.54	7.31	128.21	3.05	0.07	1.25
7.14	1.27	18.33	6.82	125.06	3.01	0.07	1.31
7.16	1.32	19.09	6.36	121.48	2.97	0.07	1.36
7.18	1.37	19.85	5.95	118.06	2.93	0.07	1.42
7.20	1.42	20.45	5.69	116.29	2.90	0.07	1.47
7.22	1.49	21.30	5.43	115.60	2.87	0.08	1.54
7.24	1.56	22.32	5.21	116.38	2.85	0.08	1.62
7.26	1.63	23.34	5.04	117.70	2.83	0.08	1.70
7.28	1.72	24.48	4.90	119.92	2.81	0.08	1.79
7.30	1.78	25.31	4.79	121.33	2.80	0.08	1.85
7.32	1.83	25.97	4.77	123.83	2.80	0.08	1.90
7.34	1.83	26.05	4.95	128.84	2.82	0.08	1.90
7.36	1.81	25.74	5.27	135.56	2.85	0.08	1.86
7.38	1.76	25.18	5.65	142.29	2.90	0.08	1.81
7.40	1.73	24.71	5.92	146.29	2.92	0.08	1.77
7.42	1.68	23.96	6.29	150.72	2.96	0.08	1.71
7.44	1.63	23.11	6.69	154.60	3.00	0.07	1.65
7.46	1.57	22.13	7.09	156.84	3.03	0.07	1.58
7.48	1.54	21.56	7.23	155.87	3.04	0.07	1.54
7.50	1.55	21.71	6.97	151.23	3.02	0.07	1.55
7.52	1.59	22.26	6.51	144.79	2.98	0.07	1.59
7.54	1.63	22.76	6.11	139.16	2.94	0.08	1.63
7.56	1.64	22.79	5.99	136.51	2.93	0.08	1.63
7.58	1.61	22.38	6.11	136.66	2.94	0.07	1.60
7.60	1.59	21.89	6.29	137.68	2.96	0.07	1.56
7.62	1.57	21.57	6.47	139.55	2.97	0.07	1.54
7.64	1.57	21.52	6.60	142.14	2.99	0.07	1.54
7.66	1.59	21.78	6.60	143.81	2.99	0.07	1.56
7.68	1.60	21.81	6.61	144.28	2.99	0.07	1.56

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
7.70	1.60	21.75	6.59	143.44	2.99	0.07	1.55
7.72	1.59	21.59	6.59	142.26	2.99	0.07	1.54
7.74	1.61	21.77	6.45	140.35	2.97	0.07	1.56
7.76	1.66	22.43	6.13	137.57	2.94	0.07	1.60
7.78	1.71	23.13	5.82	134.73	2.91	0.08	1.66
7.80	1.61	21.64	6.02	130.29	2.93	0.08	1.55
7.82	1.62	21.67	6.00	129.94	2.93	0.07	1.55
7.84	1.60	21.41	6.13	131.16	2.94	0.08	1.53
7.86	1.71	22.96	5.96	136.73	2.93	0.08	1.64
7.88	1.69	22.60	6.21	140.39	2.95	0.07	1.61
7.90	1.69	22.53	6.35	143.05	2.96	0.07	1.61
7.92	1.72	22.84	6.31	144.05	2.96	0.07	1.63
7.94	1.76	23.35	6.13	143.22	2.94	0.08	1.67
7.96	1.77	23.52	6.06	142.58	2.94	0.08	1.68
7.98	1.77	23.37	6.09	142.44	2.94	0.08	1.67
8.00	1.73	22.75	6.26	142.34	2.95	0.07	1.63
8.02	1.70	22.23	6.39	141.97	2.97	0.07	1.59
8.04	1.66	21.64	6.56	141.89	2.98	0.07	1.55
8.06	1.64	21.24	6.72	142.67	3.00	0.07	1.52
8.08	1.64	21.17	6.71	141.98	3.00	0.07	1.51
8.10	1.68	21.68	6.41	139.02	2.97	0.07	1.55
8.12	1.72	22.19	6.09	135.16	2.94	0.08	1.58
8.14	1.72	22.25	5.95	132.45	2.93	0.08	1.59
8.16	1.69	21.72	6.05	131.41	2.94	0.08	1.55
8.18	1.65	21.05	6.21	130.77	2.95	0.07	1.50
8.20	1.59	20.23	6.49	131.36	2.98	0.07	1.45
8.22	1.53	19.32	6.87	132.78	3.01	0.07	1.38
8.24	1.46	18.21	7.37	134.25	3.05	0.07	1.30
8.26	1.39	17.27	7.73	133.50	3.08	0.07	1.23
8.28	1.33	16.44	7.97	130.95	3.10	0.07	1.17
8.30	1.30	15.98	7.95	127.12	3.10	0.07	1.14
8.32	1.27	15.52	7.92	122.90	3.10	0.07	1.11
8.34	1.25	15.19	7.76	117.94	3.09	0.07	1.09
8.36	1.24	14.91	7.56	112.73	3.07	0.07	1.06
8.38	1.23	14.84	7.30	108.26	3.05	0.07	1.06
8.40	1.23	14.76	7.10	104.85	3.03	0.07	1.05
8.42	1.22	14.65	6.95	101.80	3.02	0.07	1.05
8.44	1.22	14.52	6.81	98.82	3.01	0.07	1.04
8.46	1.20	14.29	6.75	96.43	3.00	0.07	1.02
8.48	1.18	13.95	6.82	95.20	3.01	0.07	1.00
8.50	1.15	13.51	6.97	94.14	3.02	0.07	0.96
8.52	1.12	13.08	7.13	93.23	3.03	0.06	0.93
8.54	1.10	12.75	7.22	92.07	3.04	0.06	0.91
8.56	1.09	12.59	7.28	91.65	3.05	0.06	0.90
8.58	1.09	12.62	7.26	91.68	3.05	0.06	0.90
8.60	1.11	12.84	7.10	91.16	3.03	0.06	0.92
8.62	1.14	13.21	6.80	89.90	3.01	0.06	0.94
8.64	1.19	13.75	6.40	88.01	2.97	0.07	0.98

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
8.66	1.23	14.36	6.07	87.16	2.94	0.07	1.03
8.68	1.28	14.94	5.80	86.66	2.91	0.07	1.07
8.70	1.31	15.33	5.69	87.27	2.90	0.07	1.10
8.72	1.31	15.26	5.84	89.19	2.91	0.07	1.09
8.74	1.27	14.75	6.28	92.63	2.96	0.07	1.05
8.76	1.20	13.81	6.97	96.20	3.02	0.07	0.99
8.78	1.13	12.79	7.82	100.03	3.09	0.06	0.91
8.80	1.07	11.92	8.62	102.79	3.15	0.06	0.85
8.82	1.04	11.53	9.11	105.11	3.19	0.06	0.82
8.84	1.04	11.46	9.18	105.19	3.20	0.06	0.82
8.86	1.03	11.35	9.19	104.24	3.20	0.06	0.81
8.88	1.02	11.24	9.08	101.99	3.19	0.06	0.80
8.91	1.03	11.35	8.67	98.41	3.16	0.06	0.81
8.92	1.07	11.76	7.97	93.76	3.10	0.06	0.84
8.94	1.10	12.21	7.21	88.08	3.04	0.06	0.87
8.96	1.12	12.40	6.81	84.52	3.01	0.06	0.89
8.98	1.14	12.61	6.52	82.23	2.98	0.06	0.90
9.00	1.15	12.74	6.38	81.27	2.97	0.06	0.91
9.02	1.18	13.13	6.18	81.14	2.95	0.07	0.94
9.04	1.25	13.88	5.91	82.02	2.92	0.07	0.99
9.06	1.35	15.10	5.50	83.10	2.88	0.07	1.08
9.08	1.48	16.61	5.02	83.36	2.83	0.08	1.20
9.10	1.58	17.84	4.74	84.57	2.79	0.08	1.29
9.12	1.63	18.48	4.71	87.10	2.79	0.08	1.33
9.14	1.63	18.48	4.95	91.46	2.82	0.08	1.33
9.16	1.60	18.11	5.32	96.34	2.86	0.08	1.30
9.18	1.56	17.66	5.75	101.55	2.91	0.07	1.26
9.20	1.53	17.22	6.17	106.31	2.95	0.07	1.23
9.22	1.53	17.20	6.35	109.30	2.96	0.07	1.23
9.24	1.55	17.33	6.41	111.04	2.97	0.07	1.24
9.26	1.55	17.32	6.53	113.03	2.98	0.07	1.24
9.28	1.52	16.99	6.76	114.81	3.00	0.07	1.21
9.30	1.50	16.59	7.01	116.29	3.02	0.07	1.18
9.32	1.48	16.32	7.17	117.06	3.04	0.07	1.17
9.34	1.48	16.29	7.27	118.37	3.05	0.07	1.16
9.36	1.48	16.28	7.36	119.88	3.05	0.07	1.16
9.38	1.48	16.22	7.41	120.19	3.06	0.07	1.16
9.40	1.45	15.81	7.57	119.75	3.07	0.07	1.13
9.42	1.41	15.33	7.75	118.84	3.09	0.07	1.10
9.44	1.36	14.65	8.09	118.50	3.11	0.07	1.05
9.46	1.32	14.08	8.38	118.03	3.14	0.07	1.01
9.48	1.28	13.59	8.64	117.38	3.16	0.07	0.97
9.50	1.27	13.43	8.70	116.79	3.16	0.07	0.96
9.52	1.26	13.34	8.73	116.36	3.16	0.07	0.95
9.54	1.27	13.37	8.65	115.55	3.16	0.07	0.95
9.56	1.26	13.28	8.58	113.88	3.15	0.07	0.95
9.58	1.26	13.14	8.53	112.04	3.15	0.07	0.94
9.60	1.24	12.88	8.58	110.49	3.15	0.07	0.92

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.62	1.22	12.65	8.63	109.25	3.15	0.07	0.90
9.64	1.21	12.45	8.66	107.84	3.16	0.06	0.89
9.66	1.19	12.24	8.69	106.38	3.16	0.06	0.87
9.68	1.18	12.06	8.72	105.14	3.16	0.06	0.86
9.70	1.17	11.97	8.69	103.97	3.16	0.06	0.85
9.72	1.18	12.08	8.49	102.58	3.14	0.06	0.86
9.74	1.22	12.52	8.05	100.85	3.11	0.06	0.89
9.76	1.29	13.26	7.43	98.57	3.06	0.07	0.95
9.78	1.35	13.94	6.92	96.40	3.02	0.07	1.00
9.80	1.40	14.51	6.48	94.04	2.98	0.07	1.04
9.82	1.42	14.73	6.39	94.18	2.97	0.07	1.05
9.84	1.43	14.84	6.48	96.14	2.98	0.07	1.06
9.86	1.43	14.74	6.80	100.20	3.00	0.07	1.05
9.88	1.41	14.57	7.17	104.50	3.04	0.07	1.04
9.90	1.40	14.36	7.55	108.45	3.07	0.07	1.03
9.92	1.38	14.13	7.92	111.99	3.10	0.07	1.01
9.94	1.37	13.96	8.17	114.05	3.12	0.07	1.00
9.96	1.35	13.63	8.41	114.67	3.14	0.07	0.97
9.98	1.33	13.45	8.49	114.19	3.14	0.07	0.96
10.00	1.32	13.23	8.56	113.29	3.15	0.07	0.95
10.02	1.31	13.19	8.56	112.86	3.15	0.07	0.94
10.04	1.31	13.15	8.52	112.00	3.15	0.07	0.94
10.06	1.33	13.29	8.35	110.98	3.13	0.07	0.95
10.08	1.35	13.47	8.15	109.74	3.12	0.07	0.96
10.10	1.36	13.60	8.00	108.88	3.11	0.07	0.97
10.12	1.36	13.58	7.99	108.44	3.10	0.07	0.97
10.14	1.36	13.49	8.04	108.53	3.11	0.07	0.96
10.16	1.36	13.46	8.09	108.86	3.11	0.07	0.96
10.18	1.38	13.68	7.98	109.18	3.10	0.07	0.98
10.20	1.40	13.87	7.92	109.88	3.10	0.07	0.99
10.22	1.40	13.90	7.98	110.96	3.10	0.07	0.99
10.24	1.38	13.58	8.25	112.04	3.13	0.07	0.97
10.26	1.35	13.27	8.43	111.92	3.14	0.07	0.95
10.28	1.31	12.80	8.69	111.21	3.16	0.07	0.91
10.30	1.29	12.50	8.79	109.85	3.17	0.07	0.89
10.32	1.26	12.16	8.95	108.85	3.18	0.07	0.87
10.34	1.25	12.02	8.93	107.37	3.18	0.06	0.86
10.36	1.24	11.81	8.96	105.77	3.18	0.06	0.84
10.38	1.23	11.74	8.85	103.97	3.17	0.06	0.84
10.40	1.24	11.78	8.72	102.72	3.16	0.06	0.84
10.42	1.26	11.95	8.51	101.77	3.15	0.06	0.85
10.44	1.27	12.11	8.35	101.18	3.13	0.06	0.87
10.46	1.29	12.29	8.21	100.82	3.12	0.07	0.88
10.48	1.30	12.42	8.16	101.30	3.12	0.07	0.89
10.50	1.31	12.48	8.18	102.10	3.12	0.07	0.89
10.52	1.30	12.37	8.34	103.10	3.13	0.07	0.88
10.54	1.30	12.26	8.48	103.95	3.14	0.07	0.88
10.56	1.30	12.30	8.53	104.92	3.15	0.07	0.88

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
10.58	1.34	12.66	8.33	105.47	3.13	0.07	0.90
10.60	1.39	13.21	7.98	105.44	3.10	0.07	0.94
10.62	1.43	13.57	7.73	104.92	3.08	0.07	0.97
10.64	1.44	13.72	7.68	105.28	3.08	0.07	0.98
10.66	1.44	13.64	7.79	106.31	3.09	0.07	0.97
10.68	1.44	13.62	7.91	107.77	3.10	0.07	0.97
10.70	1.46	13.83	7.83	108.22	3.09	0.07	0.99
10.72	1.52	14.41	7.48	107.76	3.06	0.07	1.03
10.74	1.58	15.07	7.15	107.70	3.04	0.07	1.08
10.76	1.63	15.58	6.98	108.67	3.02	0.07	1.11
10.78	1.42	13.27	7.53	99.92	3.07	0.07	0.95
10.80	1.47	13.82	7.29	100.77	3.05	0.06	0.99
10.82	1.52	14.35	7.14	102.46	3.03	0.07	1.02
10.84	1.79	17.14	6.78	116.27	3.00	0.07	1.22
10.86	1.77	16.90	7.15	120.78	3.04	0.07	1.21
10.88	1.72	16.35	7.58	123.98	3.07	0.07	1.17
10.90	1.66	15.71	7.94	124.73	3.10	0.07	1.12
10.92	1.60	15.03	8.30	124.75	3.13	0.07	1.07
10.94	1.56	14.50	8.64	125.32	3.16	0.07	1.04
10.96	1.52	14.09	8.99	126.60	3.18	0.07	1.01
10.98	1.49	13.78	9.28	127.86	3.20	0.07	0.98
11.00	1.48	13.61	9.40	127.99	3.21	0.07	0.97
11.02	1.48	13.54	9.39	127.19	3.21	0.07	0.97
11.04	1.47	13.43	9.36	125.80	3.21	0.07	0.96
11.06	1.45	13.16	9.43	124.10	3.21	0.07	0.94
11.08	1.43	12.91	9.45	122.00	3.21	0.07	0.92
11.10	1.42	12.80	9.36	119.73	3.21	0.07	0.91
11.12	1.43	12.85	9.15	117.66	3.19	0.07	0.92
11.14	1.41	12.68	9.18	116.47	3.20	0.07	0.91
11.16	1.38	12.35	9.38	115.86	3.21	0.07	0.88
11.18	1.34	11.85	9.69	114.88	3.23	0.07	0.85
11.20	1.30	11.44	9.92	113.49	3.25	0.06	0.82
11.22	1.28	11.23	9.95	111.72	3.25	0.06	0.80
11.24	1.28	11.14	9.91	110.38	3.25	0.06	0.80
11.26	1.28	11.15	9.79	109.12	3.24	0.06	0.80
11.28	1.29	11.22	9.61	107.87	3.23	0.06	0.80
11.30	1.31	11.46	9.29	106.50	3.20	0.06	0.82
11.32	1.36	11.86	8.86	105.16	3.17	0.07	0.85
11.34	1.39	12.18	8.54	104.05	3.15	0.07	0.87
11.36	1.42	12.45	8.30	103.38	3.13	0.07	0.89
11.38	1.45	12.74	8.10	103.15	3.11	0.07	0.91
11.40	1.47	12.99	7.96	103.36	3.10	0.07	0.93
11.42	1.46	12.85	8.12	104.29	3.12	0.07	0.92
11.44	1.43	12.52	8.40	105.15	3.14	0.07	0.89
11.46	1.38	11.94	8.85	105.71	3.17	0.07	0.85
11.48	1.36	11.68	9.00	105.12	3.18	0.06	0.83
11.50	1.34	11.47	9.03	103.57	3.18	0.06	0.82
11.52	1.35	11.59	8.76	101.63	3.16	0.07	0.83

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
11.54	1.40	12.04	8.27	99.57	3.13	0.07	0.86
11.56	1.46	12.68	7.71	97.78	3.08	0.07	0.91
11.58	1.54	13.40	7.16	95.98	3.04	0.07	0.96
11.60	1.57	13.68	6.96	95.24	3.02	0.07	0.98
11.62	1.56	13.60	7.01	95.39	3.02	0.07	0.97
11.64	1.53	13.22	7.30	96.52	3.05	0.07	0.94
11.66	1.49	12.85	7.61	97.81	3.07	0.07	0.92
11.68	1.45	12.40	8.03	99.62	3.11	0.07	0.89
11.70	1.43	12.13	8.29	100.52	3.13	0.07	0.87
11.72	1.40	11.85	8.51	100.76	3.15	0.07	0.85
11.74	1.39	11.70	8.54	99.88	3.15	0.07	0.84
11.76	1.36	11.41	8.73	99.58	3.16	0.07	0.81
11.78	1.33	11.12	8.87	98.61	3.17	0.06	0.79
11.80	1.33	11.11	8.86	98.40	3.17	0.06	0.79
11.82	1.34	11.17	8.74	97.65	3.16	0.07	0.80
11.84	1.35	11.26	8.69	97.93	3.16	0.06	0.80
11.86	1.35	11.22	8.66	97.21	3.16	0.06	0.80
11.88	1.36	11.28	8.50	95.89	3.14	0.06	0.81
11.90	1.37	11.33	8.30	93.96	3.13	0.07	0.81
11.92	1.37	11.29	8.18	92.36	3.12	0.06	0.81
11.94	1.35	11.11	8.21	91.24	3.12	0.06	0.79
11.96	1.34	11.00	8.17	89.85	3.12	0.06	0.79
11.98	1.32	10.80	8.21	88.63	3.12	0.06	0.77
12.00	1.28	10.39	8.50	88.37	3.14	0.06	0.74
12.02	1.20	9.61	9.31	89.51	3.20	0.06	0.69
12.04	1.12	8.78	10.25	89.94	3.27	0.06	0.63
12.06	1.06	8.15	11.01	89.73	3.32	0.06	0.58
12.08	1.02	7.76	11.47	88.95	3.35	0.06	0.55
12.10	0.98	7.42	11.96	88.74	3.38	0.06	0.53
12.13	0.97	7.25	12.18	88.34	3.39	0.06	0.52
12.14	0.96	7.11	12.26	87.15	3.40	0.06	0.51
12.17	0.94	6.90	12.35	85.25	3.40	0.06	0.49
12.18	0.90	6.50	12.79	83.17	3.43	0.06	0.46
12.20	0.86	6.15	13.21	81.27	3.45	0.06	0.44
12.22	0.84	5.93	13.40	79.50	3.46	0.06	0.42
12.24	0.83	5.83	13.32	77.62	3.46	0.06	0.42
12.26	0.83	5.86	13.02	76.32	3.44	0.06	0.42
12.29	0.86	6.06	12.47	75.53	3.41	0.06	0.43
12.30	0.89	6.36	11.90	75.73	3.37	0.06	0.45
12.32	0.93	6.78	11.20	75.97	3.33	0.06	0.48
12.34	0.97	7.13	10.58	75.48	3.29	0.06	0.51
12.36	0.99	7.28	10.19	74.21	3.27	0.06	0.52
12.38	0.98	7.15	10.19	72.92	3.27	0.06	0.51
12.40	0.96	6.97	10.28	71.65	3.27	0.06	0.50
12.42	0.95	6.84	10.30	70.50	3.27	0.06	0.49
12.44	0.93	6.71	10.29	69.02	3.27	0.06	0.48
12.46	0.90	6.33	10.78	68.22	3.30	0.06	0.45
12.48	0.84	5.79	11.75	67.97	3.36	0.06	0.41

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
12.50	0.77	5.13	13.10	67.28	3.45	0.06	0.37
12.52	0.73	4.75	13.83	65.68	3.49	0.06	0.34
12.54	0.70	4.47	14.10	63.05	3.50	0.06	0.32
12.56	0.70	4.41	13.73	60.53	3.48	0.06	0.31
12.58	0.69	4.35	13.46	58.59	3.47	0.06	0.31
12.60	0.70	4.47	12.80	57.26	3.43	0.06	0.32
12.62	0.72	4.61	12.10	55.83	3.39	0.06	0.33
12.64	0.72	4.57	11.92	54.45	3.38	0.06	0.33
12.66	0.70	4.43	11.96	53.01	3.38	0.06	0.32
12.68	0.69	4.29	12.09	51.89	3.39	0.06	0.31
12.70	0.69	4.28	11.85	50.72	3.37	0.06	0.31
12.72	0.70	4.36	11.41	49.78	3.34	0.06	0.31
12.74	0.73	4.60	10.69	49.20	3.30	0.06	0.33
12.76	0.77	5.03	9.72	48.89	3.23	0.06	0.36
12.78	0.84	5.64	8.84	49.83	3.17	0.06	0.40
12.80	0.88	6.02	8.59	51.75	3.15	0.06	0.43
12.82	0.91	6.25	8.67	54.19	3.16	0.06	0.45
12.84	0.91	6.25	8.90	55.66	3.17	0.06	0.45
12.86	0.91	6.22	9.17	57.05	3.19	0.06	0.44
12.88	0.90	6.16	9.44	58.19	3.21	0.06	0.44
12.90	0.89	6.08	9.81	59.64	3.24	0.06	0.43
12.92	0.90	6.10	9.98	60.85	3.25	0.06	0.44
12.94	0.90	6.12	10.15	62.07	3.26	0.06	0.44
12.96	0.91	6.23	10.10	62.94	3.26	0.06	0.45
12.98	0.92	6.30	10.12	63.77	3.26	0.06	0.45
13.00	0.92	6.30	10.21	64.31	3.27	0.06	0.45
13.02	0.92	6.26	10.34	64.77	3.28	0.06	0.45
13.04	0.92	6.19	10.46	64.77	3.28	0.06	0.44
13.06	0.91	6.13	10.57	64.80	3.29	0.06	0.44
13.08	0.88	5.87	11.06	64.86	3.32	0.06	0.42
13.10	0.85	5.56	11.66	64.77	3.36	0.06	0.40
13.12	0.81	5.19	12.38	64.30	3.40	0.06	0.37
13.14	0.78	4.93	12.87	63.43	3.43	0.06	0.35
13.16	0.76	4.73	13.11	62.00	3.45	0.06	0.34
13.19	0.74	4.58	13.18	60.31	3.45	0.06	0.33
13.20	0.72	4.40	13.32	58.56	3.46	0.06	0.31
13.22	0.70	4.18	13.58	56.75	3.47	0.06	0.30
13.24	0.68	4.00	13.68	54.76	3.48	0.06	0.29
13.26	0.68	3.96	13.30	52.61	3.46	0.06	0.28
13.28	0.69	4.03	12.59	50.74	3.42	0.06	0.29
13.30	0.69	4.09	12.06	49.30	3.38	0.06	0.29
13.32	0.71	4.17	11.57	48.27	3.35	0.06	0.30
13.34	0.74	4.51	10.59	47.73	3.29	0.06	0.32
13.36	0.81	5.06	9.34	47.22	3.21	0.06	0.36
13.38	0.89	5.82	8.08	47.03	3.11	0.06	0.42
13.40	0.97	6.52	7.38	48.12	3.06	0.06	0.47
13.42	1.05	7.19	7.01	50.38	3.02	0.06	0.51
13.44	1.11	7.75	6.94	53.76	3.02	0.06	0.55

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
13.46	1.14	7.99	7.18	57.37	3.04	0.06	0.57
13.48	1.13	7.90	7.81	61.73	3.09	0.06	0.56
13.50	1.08	7.42	8.90	66.02	3.17	0.06	0.53
13.52	1.03	6.93	9.97	69.16	3.25	0.06	0.50
13.54	1.01	6.77	10.43	70.62	3.28	0.06	0.48
13.56	1.03	6.89	10.28	70.87	3.27	0.06	0.49
13.58	1.05	7.06	10.01	70.64	3.25	0.06	0.50
13.60	1.05	7.07	9.91	70.05	3.25	0.06	0.50
13.62	1.05	7.07	9.74	68.83	3.23	0.06	0.50
13.64	1.06	7.14	9.41	67.16	3.21	0.06	0.51
13.66	1.07	7.26	9.09	66.04	3.19	0.06	0.52
13.68	1.09	7.38	8.98	66.26	3.18	0.06	0.53
13.70	1.10	7.46	9.13	68.15	3.19	0.06	0.53
13.72	1.11	7.54	9.34	70.43	3.21	0.06	0.54
13.74	1.11	7.55	9.63	72.72	3.23	0.06	0.54
13.76	1.11	7.55	9.88	74.55	3.24	0.06	0.54
13.78	1.12	7.57	10.10	76.43	3.26	0.06	0.54
13.80	1.13	7.63	10.24	78.16	3.27	0.06	0.55
13.82	1.14	7.72	10.29	79.43	3.27	0.06	0.55
13.84	1.16	7.86	10.18	79.98	3.26	0.06	0.56
13.86	1.18	8.01	10.02	80.27	3.25	0.06	0.57
13.88	1.19	8.13	9.90	80.53	3.25	0.06	0.58
13.90	1.20	8.16	9.88	80.69	3.24	0.06	0.58
13.92	1.19	8.09	9.95	80.52	3.25	0.06	0.58
13.94	1.19	8.03	9.97	80.09	3.25	0.06	0.57
13.96	1.18	8.00	9.94	79.46	3.25	0.06	0.57
13.98	1.19	8.09	9.71	78.54	3.23	0.06	0.58
14.00	1.23	8.39	9.22	77.40	3.20	0.06	0.60
14.02	1.27	8.72	8.78	76.57	3.17	0.06	0.62
14.04	1.31	9.04	8.45	76.40	3.14	0.06	0.65
14.06	1.34	9.28	8.26	76.71	3.13	0.06	0.66
14.08	1.37	9.50	8.16	77.56	3.12	0.06	0.68
14.10	1.38	9.56	8.30	79.39	3.13	0.06	0.68
14.12	1.39	9.64	8.48	81.78	3.14	0.06	0.69
14.14	1.41	9.78	8.61	84.17	3.15	0.06	0.70
14.16	1.44	10.00	8.61	86.05	3.15	0.06	0.71
14.18	1.45	10.06	8.74	87.96	3.16	0.06	0.72
14.20	1.44	10.02	8.95	89.77	3.18	0.06	0.72
14.22	1.45	10.05	9.05	90.97	3.19	0.06	0.72
14.24	1.45	10.04	9.11	91.47	3.19	0.06	0.72
14.26	1.45	10.06	9.12	91.80	3.19	0.06	0.72
14.28	1.45	10.05	9.12	91.68	3.19	0.06	0.72
14.30	1.46	10.09	9.06	91.44	3.19	0.06	0.72
14.32	1.47	10.12	8.95	90.56	3.18	0.06	0.72
14.34	1.46	10.06	8.94	89.98	3.18	0.06	0.72
14.36	1.45	9.92	9.05	89.74	3.19	0.06	0.71
14.38	1.42	9.67	9.29	89.85	3.20	0.06	0.69
14.40	1.40	9.54	9.42	89.86	3.21	0.06	0.68

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
14.42	1.40	9.46	9.49	89.70	3.22	0.06	0.68
14.44	1.40	9.45	9.47	89.48	3.22	0.06	0.67
14.46	1.38	9.33	9.59	89.43	3.22	0.06	0.67
14.48	1.37	9.21	9.67	89.11	3.23	0.06	0.66
14.50	1.38	9.25	9.56	88.43	3.22	0.06	0.66
14.52	1.39	9.29	9.43	87.62	3.21	0.06	0.66
14.54	1.39	9.33	9.37	87.44	3.21	0.06	0.67
14.56	1.39	9.28	9.44	87.60	3.21	0.06	0.66
14.58	1.38	9.21	9.56	88.05	3.22	0.06	0.66
14.60	1.38	9.17	9.60	87.99	3.22	0.06	0.65
14.62	1.37	9.11	9.63	87.76	3.23	0.06	0.65
14.64	1.38	9.18	9.54	87.55	3.22	0.06	0.66
14.66	1.39	9.25	9.45	87.47	3.21	0.06	0.66
14.68	1.39	9.19	9.53	87.59	3.22	0.06	0.66
14.70	1.37	8.99	9.76	87.75	3.24	0.06	0.64
14.72	1.34	8.79	10.02	88.06	3.25	0.06	0.63
14.74	1.35	8.80	10.07	88.63	3.26	0.06	0.63
14.76	1.14	7.08	10.92	77.37	3.31	0.06	0.51
14.78	1.20	7.58	10.14	76.82	3.26	0.06	0.54
14.80	1.26	8.06	9.41	75.88	3.21	0.06	0.58
14.82	1.58	10.59	8.10	85.82	3.11	0.07	0.76
14.84	1.66	11.27	7.50	84.45	3.06	0.07	0.80
14.86	1.78	12.20	6.83	83.33	3.01	0.07	0.87
14.88	1.88	12.96	6.38	82.76	2.97	0.07	0.93
14.90	1.94	13.47	6.24	84.02	2.95	0.07	0.96
14.92	1.98	13.76	6.21	85.48	2.95	0.07	0.98
14.94	2.08	14.56	6.02	87.63	2.93	0.07	1.04
14.96	2.13	14.95	6.05	90.40	2.93	0.07	1.07
14.98	2.17	15.17	6.17	93.69	2.95	0.07	1.08
15.00	2.09	14.51	6.69	97.05	2.99	0.07	1.04
15.02	2.03	14.01	7.16	100.26	3.04	0.07	1.00
15.04	1.91	13.08	7.89	103.20	3.10	0.07	0.93
15.06	1.80	12.15	8.72	105.92	3.16	0.07	0.87
15.08	1.68	11.17	9.66	107.89	3.23	0.07	0.80
15.10	1.60	10.53	10.36	109.02	3.28	0.07	0.75
15.12	1.54	10.09	10.85	109.49	3.31	0.06	0.72
15.14	1.50	9.73	11.23	109.23	3.33	0.06	0.69
15.16	1.47	9.50	11.41	108.35	3.34	0.06	0.68
15.18	1.48	9.50	11.26	106.88	3.33	0.06	0.68
15.20	1.50	9.66	10.81	104.49	3.31	0.06	0.69
15.22	1.53	9.89	10.28	101.74	3.27	0.06	0.71
15.24	1.57	10.17	9.68	98.40	3.23	0.06	0.73
15.26	1.60	10.40	9.13	94.97	3.19	0.07	0.74
15.28	1.61	10.48	8.79	92.17	3.17	0.07	0.75
15.30	1.59	10.32	8.79	90.65	3.17	0.07	0.74
15.32	1.56	10.04	8.99	90.28	3.18	0.06	0.72
15.34	1.54	9.88	9.11	90.03	3.19	0.06	0.71
15.36	1.52	9.72	9.28	90.22	3.20	0.06	0.69

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
15.38	1.50	9.56	9.45	90.32	3.21	0.06	0.68
15.40	1.45	9.13	9.90	90.37	3.25	0.06	0.65
15.42	1.37	8.53	10.46	89.22	3.28	0.06	0.61
15.44	1.28	7.78	11.18	86.95	3.33	0.06	0.56
15.46	1.20	7.19	11.69	83.99	3.36	0.06	0.51
15.48	1.14	6.70	12.14	81.38	3.39	0.06	0.48
15.50	1.09	6.30	12.60	79.32	3.42	0.06	0.45
15.52	1.03	5.85	13.19	77.12	3.45	0.06	0.42
15.54	0.99	5.46	13.64	74.55	3.48	0.06	0.39
15.56	0.94	5.13	13.98	71.73	3.49	0.06	0.37
15.58	0.91	4.85	14.29	69.29	3.51	0.06	0.35
15.60	0.89	4.73	14.19	67.07	3.51	0.06	0.34
15.62	0.90	4.79	13.54	64.83	3.47	0.06	0.34
15.64	0.94	5.07	12.29	62.36	3.40	0.06	0.36
15.66	1.00	5.53	10.88	60.23	3.31	0.06	0.40
15.68	1.08	6.14	9.58	58.87	3.22	0.06	0.44
15.70	1.18	6.87	8.45	58.03	3.14	0.06	0.49
15.72	1.27	7.52	7.64	57.49	3.08	0.06	0.54
15.74	1.34	8.03	7.17	57.57	3.04	0.06	0.57
15.76	1.21	7.08	8.04	56.92	3.11	0.06	0.51
15.78	1.20	6.99	8.46	59.17	3.14	0.06	0.50
15.80	1.18	6.84	9.01	61.64	3.18	0.06	0.49
15.82	1.31	7.82	8.53	66.64	3.15	0.06	0.56
15.85	1.29	7.62	9.22	70.26	3.20	0.06	0.54
15.86	1.25	7.35	9.99	73.43	3.25	0.06	0.53
15.88	1.23	7.12	10.49	74.71	3.29	0.06	0.51
15.90	1.21	6.96	10.65	74.16	3.30	0.06	0.50
15.92	1.19	6.86	10.57	72.50	3.29	0.06	0.49
15.94	1.18	6.71	10.54	70.73	3.29	0.06	0.48
15.96	1.17	6.67	10.27	68.54	3.27	0.06	0.48
15.98	1.18	6.70	9.93	66.53	3.25	0.06	0.48
16.00	1.22	7.03	9.27	65.13	3.20	0.06	0.50
16.02	1.28	7.47	8.68	64.85	3.16	0.06	0.53
16.04	1.35	7.96	8.17	65.01	3.12	0.06	0.57
16.06	1.38	8.20	7.96	65.21	3.10	0.06	0.59
16.08	1.38	8.17	8.05	65.76	3.11	0.06	0.58
16.10	1.33	7.80	8.59	67.04	3.15	0.06	0.56
16.12	1.26	7.23	9.54	68.99	3.22	0.06	0.52
16.14	1.17	6.58	10.70	70.45	3.30	0.06	0.47
16.16	1.11	6.14	11.60	71.19	3.36	0.06	0.44
16.18	1.09	5.97	12.02	71.76	3.38	0.06	0.43
16.20	1.10	6.04	11.90	71.89	3.37	0.06	0.43
16.22	1.11	6.12	11.58	70.91	3.35	0.06	0.44
16.24	1.11	6.05	11.33	68.46	3.34	0.06	0.43
16.26	1.09	5.92	10.99	64.98	3.32	0.06	0.42
16.28	1.09	5.90	10.48	61.85	3.28	0.06	0.42
16.30	1.14	6.26	9.46	59.27	3.22	0.06	0.45
16.32	1.24	6.97	8.28	57.71	3.13	0.06	0.50

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
16.34	1.36	7.88	7.25	57.15	3.04	0.06	0.56
16.36	1.45	8.49	6.85	58.16	3.01	0.06	0.61
16.38	1.47	8.63	6.97	60.13	3.02	0.06	0.62
16.40	1.42	8.28	7.48	61.93	3.06	0.06	0.59
16.42	1.35	7.74	8.16	63.14	3.12	0.06	0.55
16.44	1.26	7.11	9.10	64.69	3.19	0.06	0.51
16.46	1.19	6.56	10.18	66.79	3.26	0.06	0.47
16.48	1.14	6.21	10.96	68.09	3.32	0.06	0.44
16.50	1.13	6.07	11.27	68.43	3.34	0.06	0.43
16.52	1.13	6.07	11.17	67.82	3.33	0.06	0.43
16.54	1.12	6.03	11.10	66.89	3.32	0.06	0.43
16.56	1.13	6.08	10.75	65.33	3.30	0.06	0.43
16.58	1.14	6.16	10.23	63.04	3.27	0.06	0.44
16.60	1.16	6.28	9.63	60.49	3.23	0.06	0.45
16.62	1.16	6.28	9.37	58.83	3.21	0.06	0.45
16.64	1.16	6.23	9.28	57.82	3.20	0.06	0.45
16.66	1.14	6.13	9.31	57.11	3.20	0.06	0.44
16.68	1.14	6.11	9.15	55.89	3.19	0.06	0.44
16.70	1.15	6.16	8.89	54.80	3.17	0.06	0.44
16.72	1.20	6.52	8.27	53.95	3.13	0.06	0.47
16.74	1.28	7.05	7.58	53.48	3.07	0.06	0.50
16.76	1.40	7.93	7.02	55.68	3.02	0.06	0.57
16.79	1.49	8.55	6.86	58.71	3.01	0.06	0.61
16.80	1.51	8.72	7.18	62.65	3.04	0.06	0.62
16.82	1.48	8.47	7.57	64.07	3.07	0.06	0.60
16.84	1.44	8.20	7.89	64.70	3.10	0.06	0.59
16.86	1.45	8.23	8.03	66.07	3.11	0.06	0.59

Abbreviations

q_t:	Total cone resistance
K_c:	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c:	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

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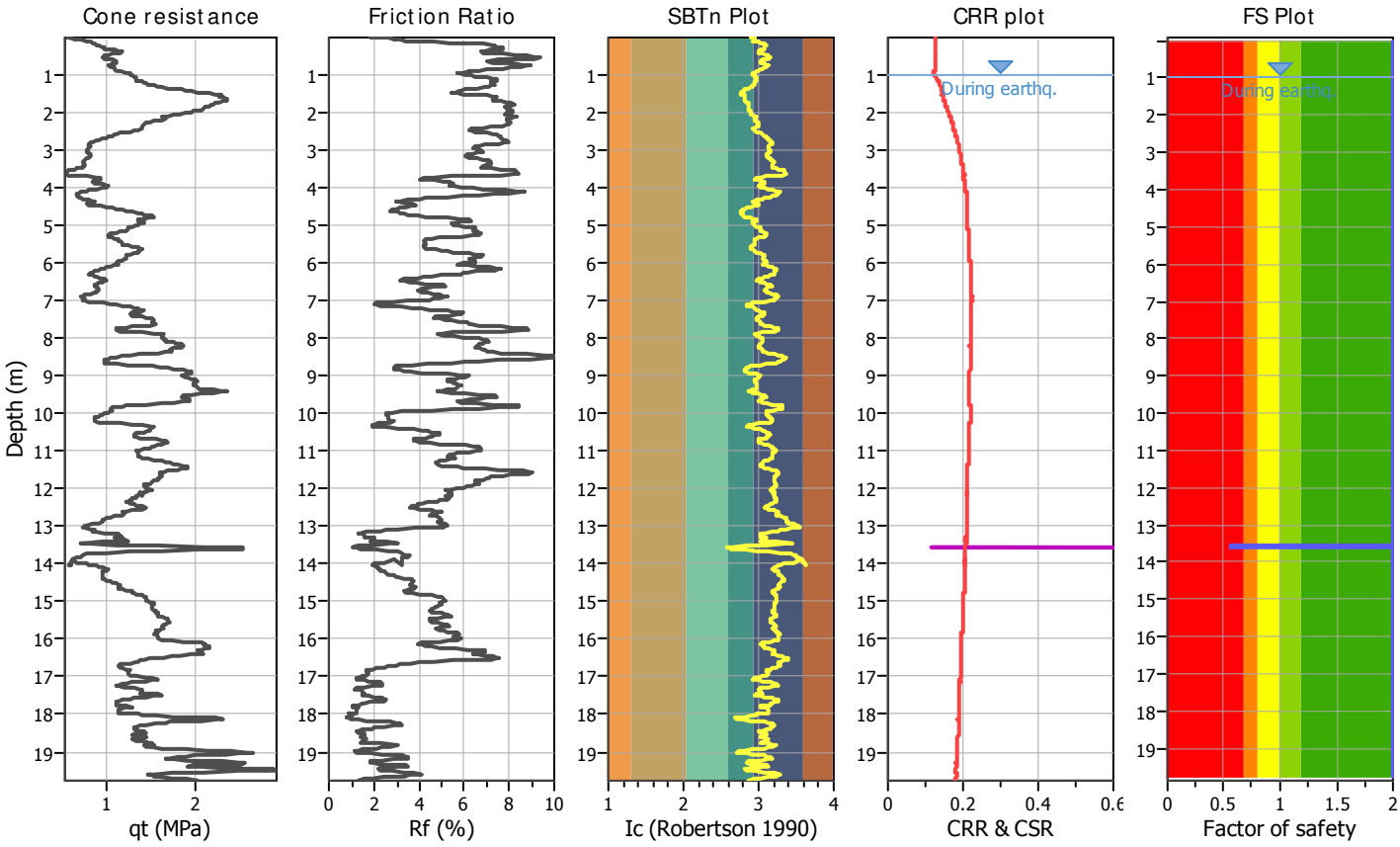
LIQUEFACTION ANALYSIS REPORT

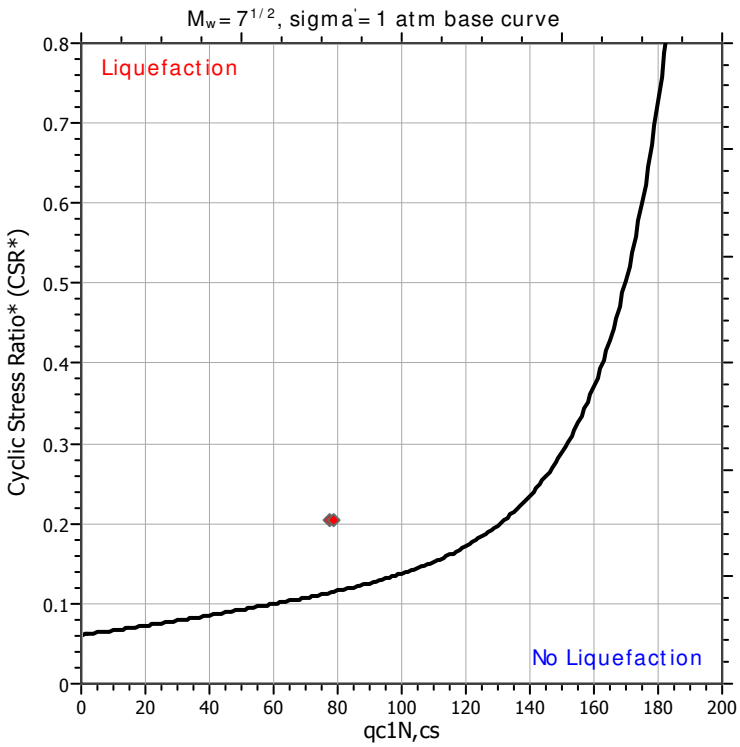
Project title : Location :

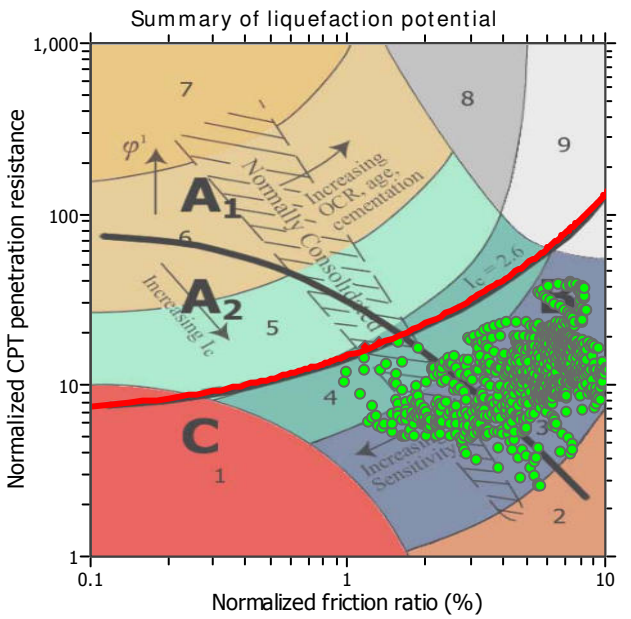
CPT file : CPTu-03_Biancolina

Input parameters and analysis data

Analysis method:	B&I (2014)	G.W.T. (in-situ):	2.20 m	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.00 m	Fill height:	N/A	Limit depth applied:	No
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	N/A
Earthquake magnitude M_w:	6.14	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.23	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		

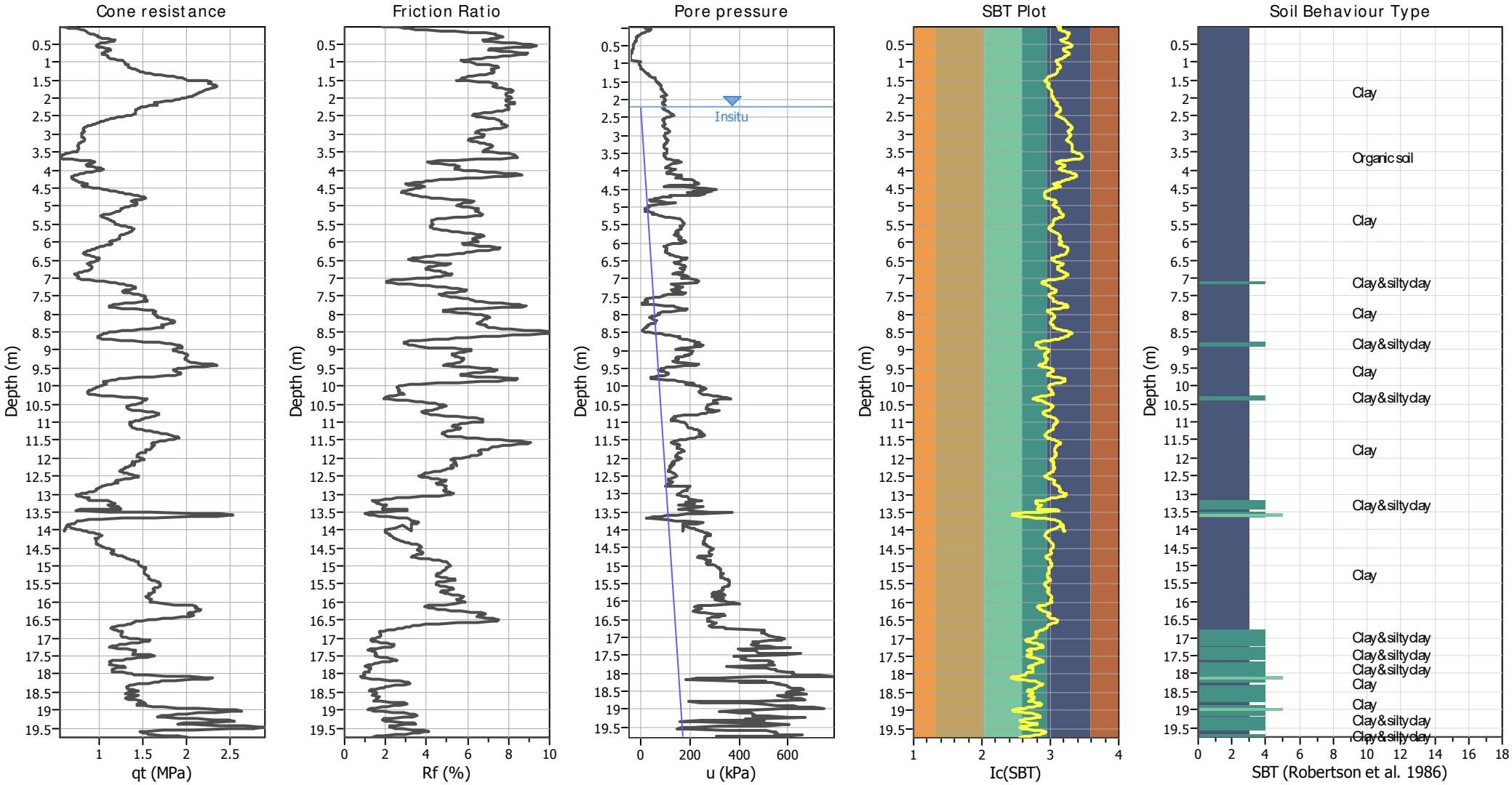






Zone A_1: Cyclic liquefaction likely depending on size and duration of cyclic loading
Zone A_2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



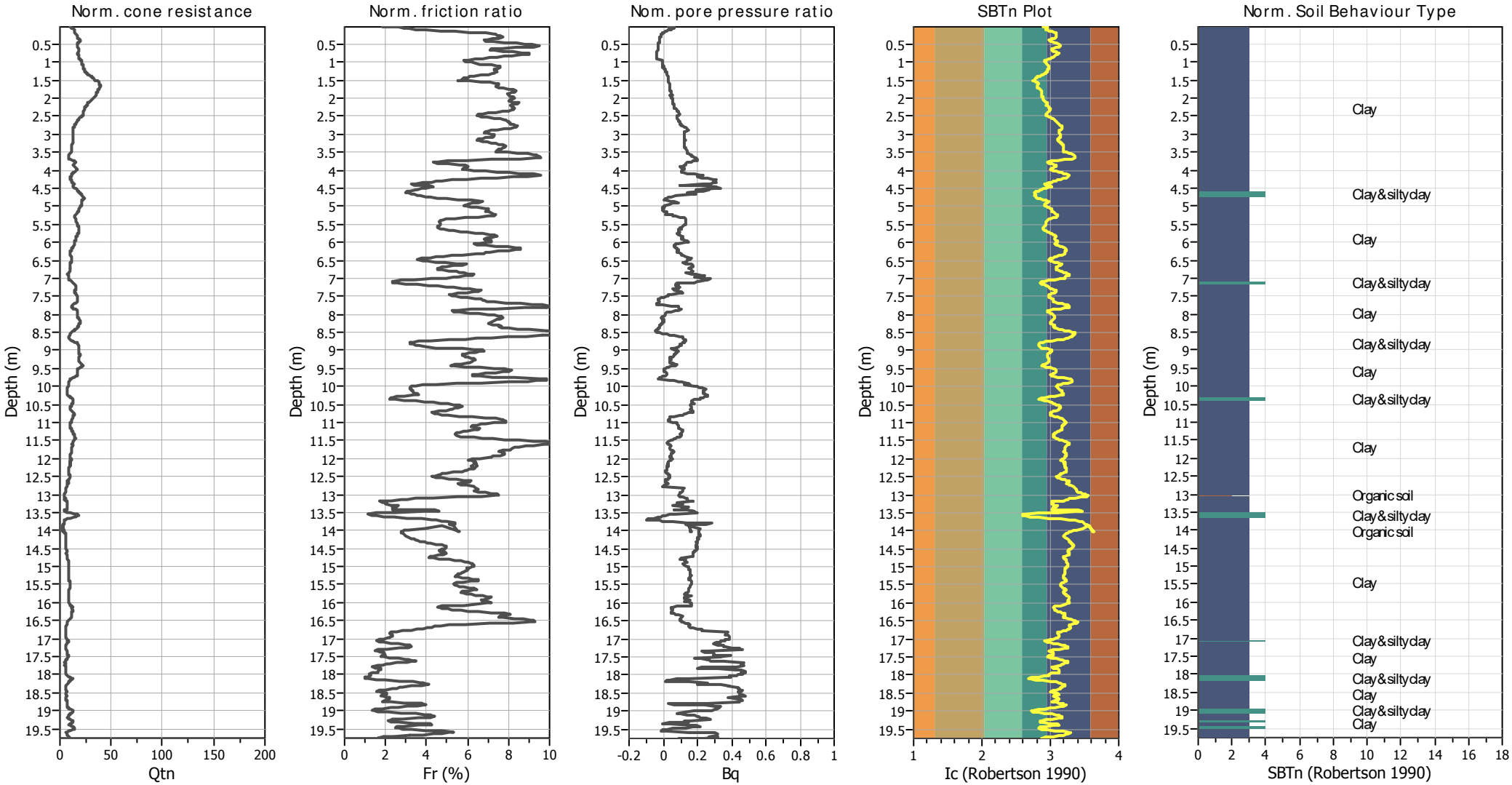
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	1.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.23	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.20 m	Fill height:	N/A	Limit depth:	N/A

SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

CPT basic interpretation plots (normalized)



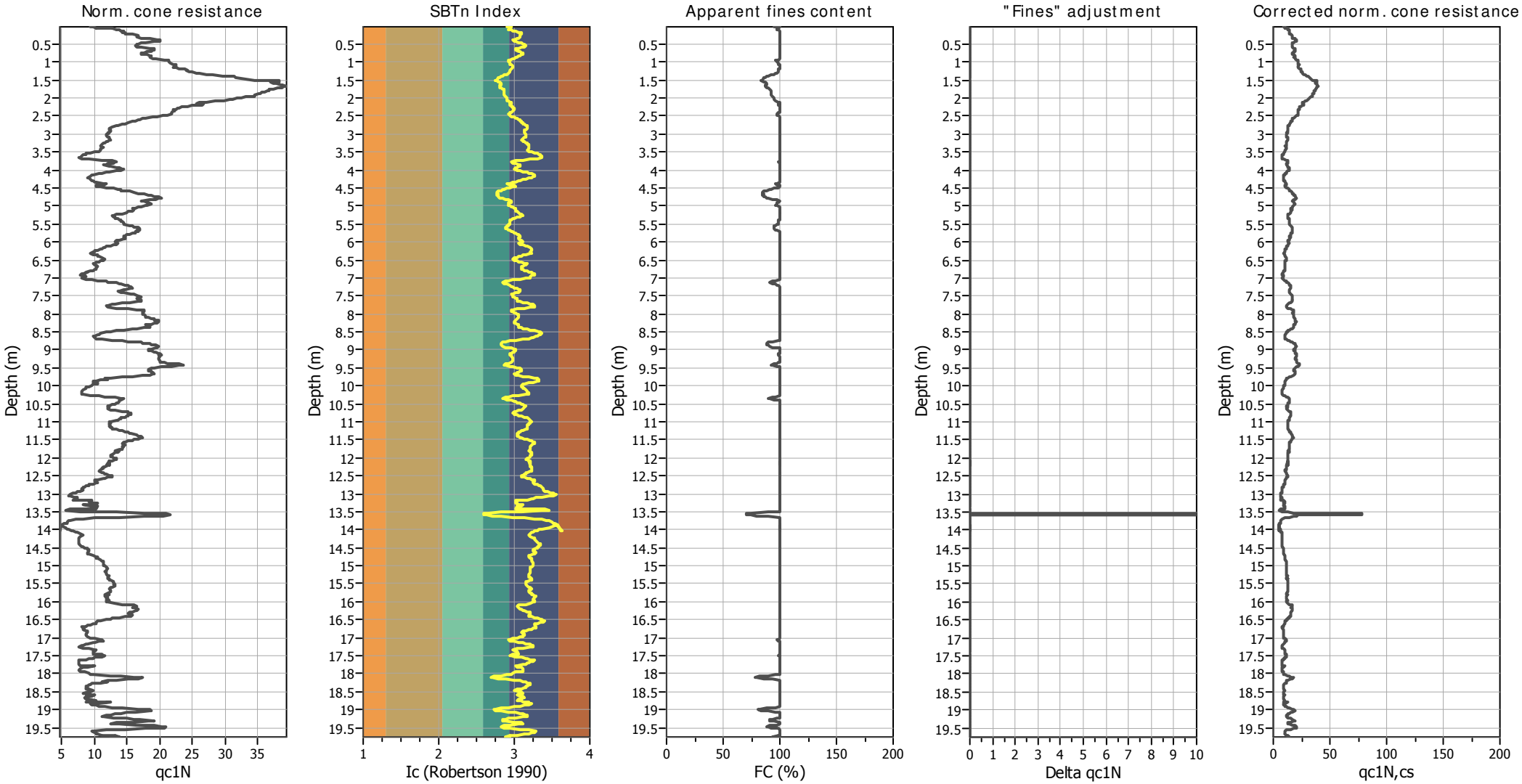
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	1.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.23	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.20 m	Fill height:	N/A	Limit depth:	N/A

SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

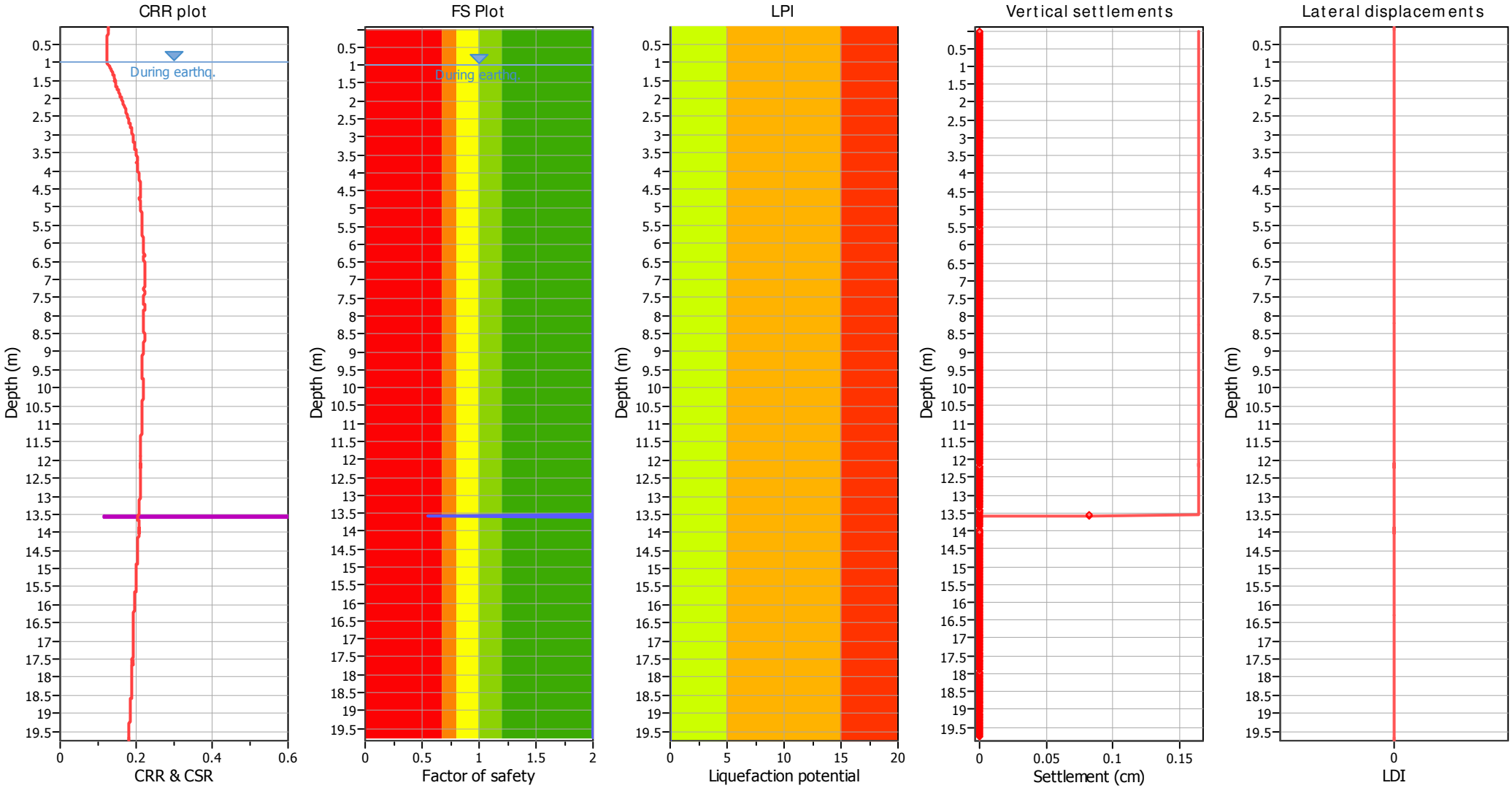
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	1.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.23	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.20 m	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	1.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.23	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.20 m	Fill height:	N/A	Limit depth:	N/A

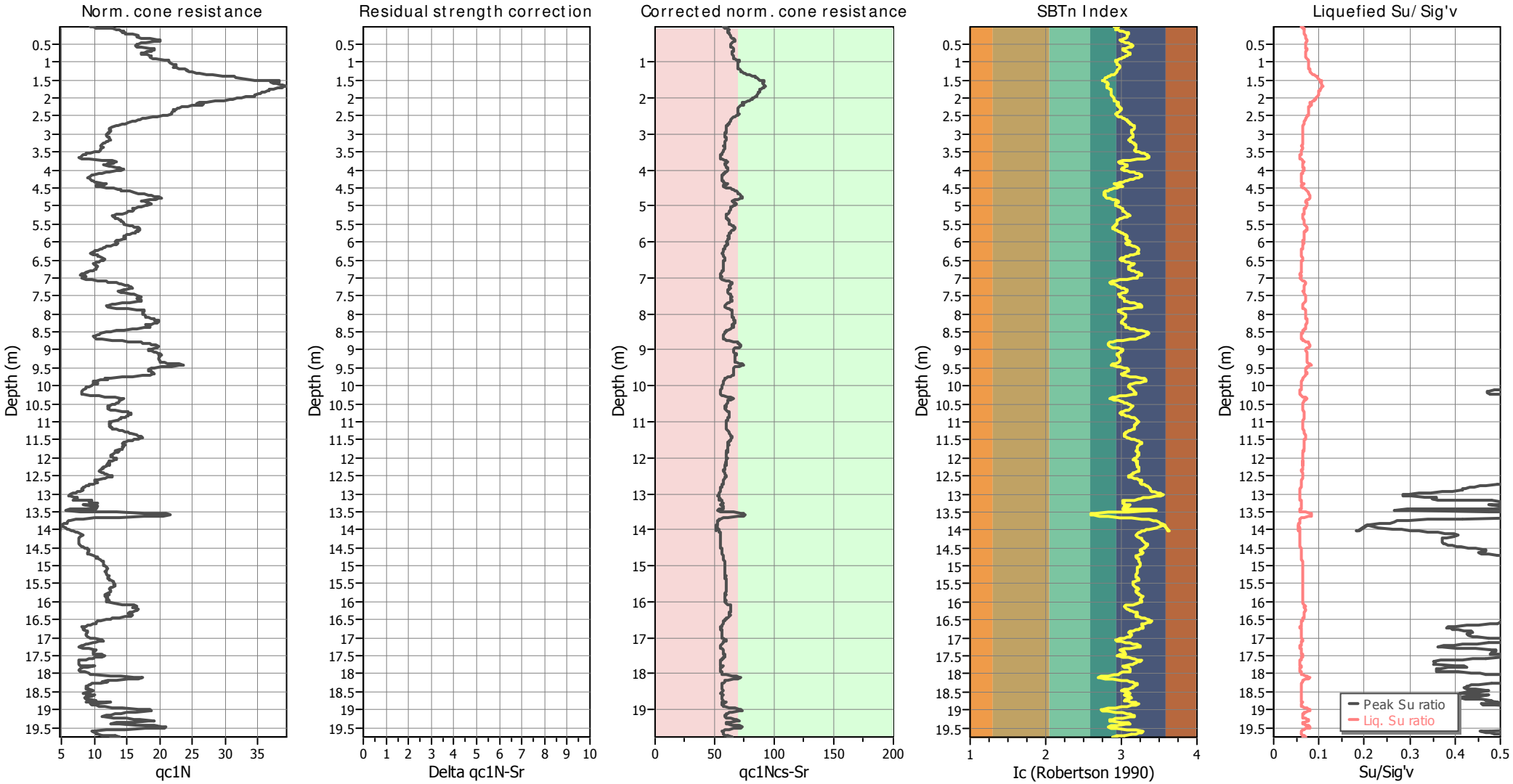
F.S. color scheme

- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

LPI color scheme

- Very high risk
- High risk
- Low risk

Check for strength loss plots (Idriss & Boulanger (2008))



Input parameters and analysis data

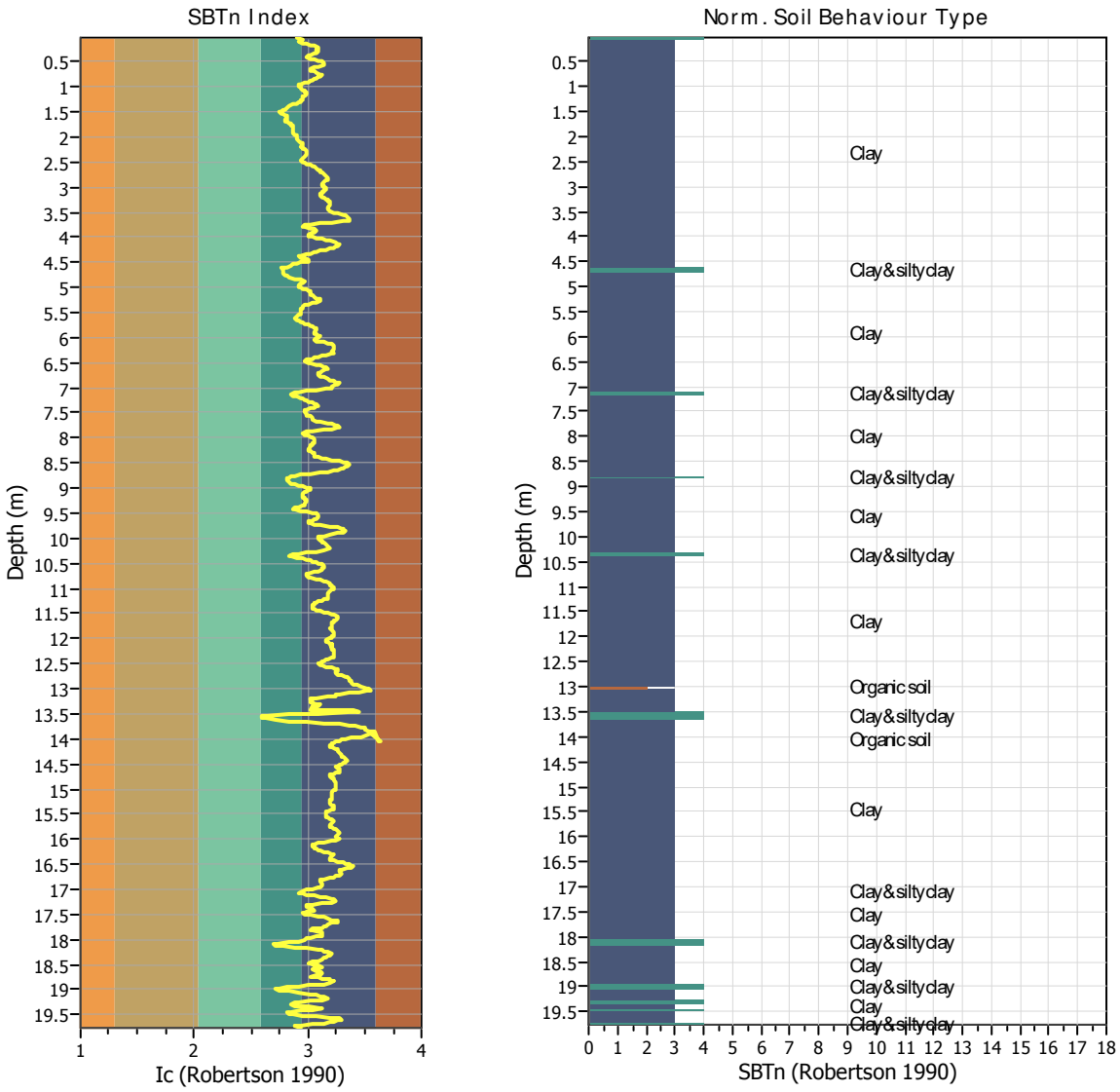
Analysis method:	B&I (2014)	Depth to GWT (erthq.):	1.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.23	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.20 m	Fill height:	N/A	Limit depth:	N/A

TRANSITION LAYER DETECTION ALGORITHM REPORT
Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vise-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between $1.80 < I_c < 3.0$) and a rate of change of I_c. Transitions typically occur when the rate of change of I_c is fast (i.e. delta I_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties		General statistics	
I_c minimum check value:	1.70	Total points in CPT file:	987
I_c maximum check value:	3.00	Total points excluded:	0
I_c change ratio value:	0.0100	Exclusion percentage:	0.00%
Minimum number of points in layer:	4	Number of layers detected:	0

:: Field input data ::

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
1	0.02	0.56	9.05	16.92	51.69	15.49
2	0.04	0.58	13.85	40.31	55.61	15.95
3	0.06	0.61	19.20	41.54	55.07	16.21
4	0.08	0.75	23.69	37.48	54.18	16.47
5	0.10	0.79	25.67	34.52	53.70	16.71
6	0.12	0.82	33.17	24.43	55.42	16.92
7	0.14	0.83	39.29	18.46	57.65	17.14
8	0.16	0.86	45.16	13.29	60.18	17.32
9	0.18	0.85	52.85	3.32	62.36	17.50
10	0.20	0.88	60.54	-1.91	64.67	17.64
11	0.22	0.88	65.96	-4.92	65.14	17.75
12	0.24	0.94	69.42	-8.49	64.49	17.83
13	0.26	0.99	71.07	-11.75	63.72	17.89
14	0.28	0.99	75.14	-14.34	63.68	17.94
15	0.30	0.99	76.75	-16.31	64.28	17.96
16	0.32	0.98	75.77	-17.91	64.04	17.97
17	0.34	1.02	76.54	-18.95	62.55	18.00
18	0.36	1.11	79.05	-19.38	60.52	18.04
19	0.38	1.16	80.21	-19.69	58.66	18.08
20	0.40	1.19	80.26	-20.74	57.62	18.09
21	0.42	1.20	79.37	-22.65	57.95	18.09
22	0.44	1.14	80.88	-25.05	59.72	18.09
23	0.46	1.07	82.62	-27.14	62.52	18.10
24	0.48	1.02	85.03	-28.49	65.04	18.10
25	0.50	1.00	86.55	-29.23	66.87	18.12
26	0.52	0.98	89.12	-30.34	68.15	18.14
27	0.54	0.98	91.50	-30.95	69.07	18.17
28	0.56	0.98	92.69	-31.82	69.04	18.17
29	0.58	0.99	89.72	-31.38	68.04	18.16
30	0.60	1.02	86.87	-31.32	65.07	18.12
31	0.62	1.11	80.47	-33.05	62.00	18.09
32	0.64	1.14	78.30	-33.78	59.79	18.06
33	0.66	1.14	78.94	-35.14	59.46	18.06
34	0.68	1.13	80.10	-36.37	60.33	18.09
35	0.70	1.11	84.27	-37.42	61.86	18.12
36	0.72	1.08	87.64	-38.15	63.75	18.15
37	0.74	1.05	89.15	-39.08	65.56	18.17
38	0.76	1.03	91.65	-39.51	66.86	18.19
39	0.78	1.02	93.71	-39.75	66.52	18.20
40	0.80	1.08	91.02	-39.45	65.11	18.20
41	0.82	1.11	88.14	-39.45	63.19	18.17
42	0.84	1.11	84.97	-39.32	62.21	18.13
43	0.86	1.10	81.80	-39.75	61.22	18.08
44	0.88	1.11	76.22	-40.43	60.01	18.03
45	0.90	1.13	73.47	-40.74	58.60	18.00
46	0.92	1.16	74.59	-39.94	56.64	17.99
47	0.95	1.23	71.53	-2.15	54.73	17.99
48	0.96	1.28	71.18	-2.40	53.27	18.00

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
49	0.98	1.28	73.26	-3.14	53.44	18.04
50	1.00	1.28	78.97	-3.63	54.16	18.09
51	1.02	1.29	81.43	-3.51	54.72	18.15
52	1.05	1.31	83.96	-2.95	55.01	18.20
53	1.06	1.32	88.58	-2.03	55.46	18.26
54	1.08	1.34	94.37	-0.55	56.33	18.32
55	1.10	1.33	98.76	0.80	56.95	18.37
56	1.12	1.34	99.63	-0.06	57.53	18.38
57	1.14	1.32	99.21	-0.18	57.57	18.39
58	1.16	1.34	100.04	5.42	57.31	18.40
59	1.18	1.37	101.29	10.03	56.42	18.42
60	1.20	1.42	101.51	13.72	55.45	18.44
61	1.22	1.45	102.15	16.68	55.16	18.46
62	1.24	1.44	106.08	20.37	55.19	18.49
63	1.26	1.46	107.52	21.48	55.20	18.51
64	1.28	1.49	108.86	29.78	54.58	18.54
65	1.30	1.53	110.53	32.25	53.98	18.56
66	1.32	1.55	112.06	37.60	53.15	18.59
67	1.34	1.62	113.24	38.52	52.00	18.60
68	1.36	1.68	111.31	42.52	50.29	18.62
69	1.38	1.76	110.83	50.22	48.40	18.63
70	1.40	1.87	111.85	57.05	47.01	18.65
71	1.44	1.89	111.82	58.03	46.27	18.66
72	1.44	1.89	111.82	58.03	45.17	18.68
73	1.51	2.06	113.38	62.83	44.25	18.69
74	1.51	2.06	113.38	62.83	43.34	18.71
75	1.51	2.06	113.60	63.38	43.30	18.81
76	1.52	2.29	138.36	72.74	43.73	18.92
77	1.54	2.28	148.67	73.60	44.92	19.06
78	1.56	2.21	160.33	73.17	46.24	19.12
79	1.58	2.24	165.09	76.18	47.14	19.17
80	1.60	2.26	168.42	77.78	47.13	19.20
81	1.62	2.29	172.00	81.42	47.02	19.22
82	1.64	2.31	172.26	82.71	46.56	19.23
83	1.66	2.35	169.72	84.06	46.32	19.22
84	1.68	2.32	169.10	83.20	46.27	19.22
85	1.70	2.32	171.63	83.94	46.92	19.23
86	1.72	2.27	176.56	85.05	47.67	19.25
87	1.74	2.24	177.67	87.08	48.65	19.26
88	1.76	2.19	179.84	88.49	49.32	19.27
89	1.78	2.19	182.08	91.88	49.80	19.27
90	1.81	2.17	181.21	94.95	49.96	19.26
91	1.82	2.15	177.93	96.74	49.94	19.24
92	1.84	2.13	171.84	99.02	49.85	19.21
93	1.86	2.11	168.66	101.35	49.65	19.18
94	1.88	2.10	164.94	104.31	49.72	19.15
95	1.90	2.06	162.43	105.72	49.93	19.14
96	1.92	2.06	166.10	83.20	50.04	19.13

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
97	1.94	2.07	162.68	95.57	50.51	19.13
98	1.97	1.99	164.09	96.43	51.08	19.12
99	1.98	1.96	164.44	96.55	51.77	19.10
100	2.00	1.93	156.75	100.31	52.02	19.07
101	2.02	1.89	153.47	100.86	51.96	19.02
102	2.04	1.87	148.63	101.66	52.08	18.98
103	2.06	1.82	142.80	96.92	52.47	18.93
104	2.08	1.74	138.66	93.17	53.31	18.88
105	2.10	1.66	134.53	89.60	54.64	18.84
106	2.13	1.60	135.00	87.57	55.95	18.82
107	2.14	1.57	136.51	89.91	55.89	18.82
108	2.16	1.66	132.59	100.06	55.27	18.81
109	2.18	1.65	131.15	102.40	54.68	18.79
110	2.20	1.60	129.77	97.11	55.06	18.76
111	2.22	1.56	124.22	92.31	55.77	18.72
112	2.24	1.51	121.66	91.38	56.44	18.67
113	2.26	1.46	118.70	93.23	57.25	18.64
114	2.28	1.44	117.64	96.86	57.72	18.62
115	2.30	1.43	116.01	103.45	57.92	18.60
116	2.32	1.41	114.05	109.11	58.11	18.58
117	2.34	1.39	113.28	112.92	57.98	18.55
118	2.36	1.40	109.49	118.09	57.69	18.53
119	2.38	1.39	106.41	121.54	56.88	18.48
120	2.40	1.39	100.68	124.92	56.15	18.43
121	2.42	1.38	95.58	129.42	55.21	18.37
122	2.45	1.38	91.80	133.60	54.35	18.32
123	2.46	1.38	87.95	133.11	53.89	18.27
124	2.48	1.35	85.13	119.32	54.19	18.23
125	2.50	1.30	83.71	105.85	55.09	18.18
126	2.52	1.25	81.21	99.08	56.39	18.15
127	2.54	1.21	81.12	93.91	58.07	18.12
128	2.56	1.14	81.66	91.51	60.07	18.11
129	2.58	1.10	82.52	92.49	61.73	18.10
130	2.60	1.08	81.50	95.08	62.74	18.09
131	2.62	1.06	80.82	96.62	63.46	18.07
132	2.64	1.03	79.76	98.03	64.18	18.04
133	2.66	1.01	78.00	97.91	65.09	18.01
134	2.68	0.97	76.43	98.22	65.64	17.98
135	2.70	0.96	74.57	98.46	66.31	17.94
136	2.72	0.94	73.48	97.91	66.95	17.91
137	2.74	0.91	71.81	88.86	68.19	17.88
138	2.76	0.87	70.98	93.05	69.29	17.84
139	2.78	0.86	68.96	96.86	70.38	17.80
140	2.80	0.82	66.75	101.17	70.87	17.76
141	2.82	0.81	64.54	106.65	71.30	17.71
142	2.84	0.79	62.04	112.55	70.99	17.66
143	2.86	0.79	59.44	114.46	70.37	17.60
144	2.88	0.79	56.40	115.88	69.10	17.56

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
145	2.90	0.81	55.13	119.32	68.20	17.53
146	2.92	0.80	54.14	110.28	67.33	17.50
147	2.94	0.81	51.93	103.20	67.45	17.47
148	2.97	0.79	51.96	102.22	67.44	17.46
149	2.98	0.79	52.15	101.17	68.21	17.46
150	3.00	0.78	53.15	97.54	68.99	17.47
151	3.02	0.76	53.82	96.06	69.66	17.48
152	3.04	0.78	54.36	98.40	69.70	17.49
153	3.07	0.79	54.43	101.78	69.18	17.50
154	3.08	0.79	54.17	103.14	68.33	17.49
155	3.10	0.81	52.92	103.94	67.55	17.48
156	3.12	0.81	51.54	105.91	66.85	17.46
157	3.14	0.81	51.22	108.31	66.05	17.44
158	3.16	0.83	50.51	109.91	65.75	17.43
159	3.18	0.81	50.10	106.52	65.94	17.43
160	3.21	0.80	51.25	105.35	67.18	17.43
161	3.22	0.78	51.66	100.55	68.43	17.44
162	3.24	0.77	52.24	98.83	69.55	17.44
163	3.26	0.76	52.50	98.46	70.67	17.45
164	3.28	0.74	53.52	98.03	71.46	17.46
165	3.30	0.74	54.26	97.42	72.27	17.47
166	3.32	0.73	54.03	94.89	72.85	17.47
167	3.34	0.72	54.48	94.95	72.91	17.48
168	3.36	0.75	55.02	98.03	72.42	17.49
169	3.38	0.76	54.89	102.58	71.98	17.49
170	3.40	0.74	54.25	104.98	71.78	17.48
171	3.42	0.74	53.00	106.46	71.72	17.44
172	3.44	0.74	50.78	108.68	71.57	17.41
173	3.48	0.73	50.59	108.86	72.03	17.38
174	3.49	0.70	49.60	104.06	73.13	17.37
175	3.50	0.68	49.85	101.91	75.50	17.34
176	3.52	0.63	49.85	97.85	78.65	17.32
177	3.54	0.59	50.04	96.86	81.70	17.30
178	3.56	0.58	49.78	97.72	83.65	17.27
179	3.58	0.56	47.67	97.78	84.80	17.24
180	3.60	0.55	47.63	98.34	85.69	17.21
181	3.62	0.54	46.54	99.82	86.57	17.19
182	3.64	0.52	46.25	102.89	87.22	17.17
183	3.66	0.52	46.35	107.45	86.27	17.16
184	3.68	0.56	44.87	118.95	82.36	17.17
185	3.70	0.62	43.91	133.54	74.16	17.19
186	3.72	0.77	42.91	156.06	65.97	17.22
187	3.74	0.88	41.66	159.69	59.46	17.22
188	3.76	0.93	39.32	163.69	56.29	17.20
189	3.78	0.93	37.88	140.06	55.32	17.16
190	3.80	0.91	37.97	131.51	56.93	17.17
191	3.82	0.85	41.05	121.48	59.64	17.21
192	3.84	0.82	43.87	119.57	62.80	17.26

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
193	3.86	0.80	45.56	113.11	63.72	17.33
194	3.88	0.86	48.55	106.71	63.75	17.39
195	3.90	0.88	50.79	101.91	62.44	17.48
196	3.92	0.94	53.80	114.71	61.07	17.54
197	3.94	0.99	54.22	132.62	59.39	17.59
198	3.96	1.02	55.37	139.57	58.52	17.63
199	3.98	1.03	57.49	126.95	58.98	17.66
200	4.00	1.00	59.05	117.60	60.76	17.70
201	4.02	0.96	62.13	111.63	63.98	17.71
202	4.04	0.87	62.61	105.23	67.14	17.70
203	4.06	0.84	62.16	105.05	70.27	17.69
204	4.08	0.80	63.76	126.77	72.73	17.70
205	4.10	0.76	66.00	150.52	75.95	17.70
206	4.12	0.70	66.35	165.78	78.26	17.67
207	4.14	0.68	61.45	167.94	79.31	17.60
208	4.16	0.67	57.09	154.71	78.14	17.49
209	4.18	0.67	50.33	140.92	77.02	17.37
210	4.20	0.64	45.17	157.72	75.06	17.23
211	4.22	0.65	41.07	180.00	72.54	17.11
212	4.25	0.67	36.39	206.28	69.39	17.01
213	4.26	0.67	33.60	218.03	66.18	16.90
214	4.28	0.69	30.55	220.18	63.82	16.83
215	4.30	0.71	29.85	217.05	61.89	16.80
216	4.32	0.72	29.88	233.48	60.37	16.77
217	4.34	0.74	27.99	236.74	57.51	16.74
218	4.36	0.82	26.48	237.60	54.24	16.70
219	4.38	0.86	25.45	209.78	52.83	16.69
220	4.40	0.82	26.22	116.25	54.11	16.69
221	4.42	0.79	27.66	94.95	57.05	16.74
222	4.44	0.75	29.72	178.77	58.94	16.80
223	4.47	0.76	31.83	248.80	59.30	16.89
224	4.48	0.80	33.69	261.85	57.49	16.97
225	4.50	0.88	34.42	310.03	54.59	17.03
226	4.52	0.96	34.49	299.14	51.95	17.06
227	4.54	1.00	34.52	212.06	50.02	17.08
228	4.56	1.04	34.49	287.32	49.16	17.09
229	4.59	1.04	34.39	268.80	47.24	17.08
230	4.60	1.15	32.28	263.45	45.58	17.08
231	4.62	1.20	33.05	187.94	44.35	17.12
232	4.64	1.21	35.99	219.38	44.57	17.22
233	4.66	1.25	40.54	259.02	44.86	17.34
234	4.68	1.32	44.10	234.77	44.69	17.44
235	4.70	1.38	45.51	121.29	44.55	17.53
236	4.72	1.42	49.58	121.78	44.92	17.63
237	4.74	1.45	55.31	86.34	45.40	17.75
238	4.76	1.51	60.25	69.11	45.85	17.85
239	4.78	1.54	63.96	59.57	46.82	17.96
240	4.80	1.52	72.36	48.12	48.44	18.06

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
241	4.82	1.49	77.13	35.94	51.03	18.14
242	4.84	1.41	83.21	42.58	53.96	18.19
243	4.86	1.31	86.03	85.42	56.15	18.23
244	4.88	1.34	87.89	106.28	56.46	18.24
245	4.90	1.39	86.16	140.92	55.41	18.24
246	4.92	1.40	84.05	96.43	54.01	18.22
247	4.94	1.45	81.07	79.94	53.51	18.17
248	4.97	1.40	76.74	33.78	53.26	18.13
249	4.98	1.38	75.49	30.83	53.59	18.09
250	5.00	1.37	74.94	38.46	54.28	18.08
251	5.02	1.33	76.22	35.45	55.59	18.09
252	5.04	1.29	78.78	19.32	57.30	18.11
253	5.07	1.27	80.61	21.11	59.13	18.13
254	5.08	1.23	82.91	32.74	59.91	18.14
255	5.10	1.24	82.01	28.25	60.05	18.13
256	5.12	1.26	79.42	20.98	59.79	18.11
257	5.14	1.23	78.68	31.75	60.14	18.09
258	5.16	1.19	78.04	53.35	60.99	18.07
259	5.18	1.17	76.94	48.74	62.32	18.04
260	5.21	1.11	75.12	46.77	63.68	18.00
261	5.22	1.06	72.74	66.34	65.08	17.95
262	5.24	1.04	71.49	79.26	65.79	17.91
263	5.26	1.01	68.64	82.03	66.17	17.86
264	5.28	0.99	65.72	99.51	65.52	17.80
265	5.30	1.01	61.30	121.35	63.78	17.73
266	5.32	1.02	55.53	151.38	61.37	17.65
267	5.34	1.04	52.77	159.45	59.02	17.58
268	5.36	1.07	49.79	165.97	57.15	17.53
269	5.38	1.10	48.25	168.74	55.90	17.51
270	5.40	1.10	48.70	169.05	55.20	17.51
271	5.42	1.12	48.76	174.65	54.93	17.51
272	5.44	1.13	48.96	174.34	54.72	17.54
273	5.46	1.15	51.07	176.43	54.60	17.56
274	5.52	1.16	51.42	173.29	54.72	17.58
275	5.52	1.16	51.42	173.29	54.74	17.59
276	5.52	1.15	51.68	173.23	54.03	17.61
277	5.54	1.23	52.70	160.25	53.27	17.64
278	5.56	1.27	54.56	166.34	52.28	17.69
279	5.58	1.30	56.00	168.37	51.66	17.73
280	5.60	1.35	56.96	162.15	51.41	17.77
281	5.62	1.36	60.23	166.71	51.51	17.83
282	5.64	1.37	63.15	153.54	52.09	17.88
283	5.66	1.37	64.81	146.03	53.21	17.93
284	5.68	1.33	68.98	149.97	54.17	17.97
285	5.70	1.35	71.25	144.31	55.61	18.02
286	5.72	1.32	74.74	154.09	56.71	18.07
287	5.74	1.31	78.56	148.74	58.48	18.12
288	5.76	1.28	81.95	135.32	60.03	18.15

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
289	5.78	1.25	83.33	135.57	61.61	18.16
290	5.80	1.22	83.62	150.03	62.78	18.17
291	5.82	1.20	84.61	160.00	63.75	18.17
292	5.84	1.18	84.10	162.22	63.73	18.14
293	5.86	1.19	78.60	166.15	63.27	18.11
294	5.88	1.21	78.76	153.60	62.54	18.08
295	5.90	1.20	77.23	156.80	62.26	18.06
296	5.92	1.19	74.50	158.89	62.73	18.03
297	5.94	1.14	74.34	175.38	63.77	18.01
298	5.96	1.10	73.92	183.69	65.19	17.99
299	5.98	1.08	73.25	185.97	65.94	17.97
300	6.01	1.08	71.55	168.00	65.14	17.93
301	6.02	1.12	66.84	131.75	63.80	17.89
302	6.04	1.13	64.60	113.97	62.94	17.85
303	6.07	1.11	65.56	110.89	63.95	17.85
304	6.08	1.07	67.06	100.98	66.00	17.86
305	6.10	1.03	68.73	94.83	68.77	17.88
306	6.12	0.98	71.45	98.15	71.31	17.90
307	6.14	0.96	74.08	103.14	73.41	17.92
308	6.16	0.94	74.04	106.89	74.58	17.92
309	6.18	0.93	72.06	106.40	75.13	17.87
310	6.20	0.90	67.67	109.54	75.37	17.80
311	6.22	0.87	62.79	108.62	75.38	17.70
312	6.24	0.84	56.90	103.63	74.70	17.59
313	6.26	0.84	51.80	99.02	74.18	17.49
314	6.28	0.81	49.11	102.58	74.45	17.41
315	6.30	0.77	48.08	112.86	74.78	17.35
316	6.32	0.79	45.84	118.28	73.47	17.30
317	6.34	0.83	42.35	121.11	70.10	17.25
318	6.36	0.87	39.91	129.72	67.02	17.20
319	6.38	0.89	38.89	144.18	64.86	17.15
320	6.40	0.89	36.93	149.17	62.69	17.12
321	6.42	0.94	35.20	171.08	60.67	17.07
322	6.44	0.95	33.54	187.38	58.06	17.01
323	6.46	0.98	30.40	182.40	56.87	16.97
324	6.48	0.98	31.62	167.45	56.75	16.96
325	6.50	0.95	32.61	164.62	58.55	17.00
326	6.52	0.92	34.66	163.45	60.55	17.04
327	6.54	0.91	35.69	146.34	63.06	17.09
328	6.56	0.87	38.16	136.37	65.81	17.15
329	6.58	0.85	42.10	141.23	68.65	17.23
330	6.60	0.84	44.79	151.88	70.45	17.30
331	6.62	0.84	45.78	169.66	70.90	17.32
332	6.64	0.84	45.34	179.08	69.82	17.30
333	6.66	0.87	41.01	182.95	67.86	17.25
334	6.69	0.89	39.44	180.49	66.06	17.19
335	6.70	0.89	38.52	175.45	64.99	17.14
336	6.72	0.89	36.08	160.86	64.81	17.11

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
337	6.74	0.87	36.15	171.51	64.72	17.07
338	6.76	0.87	35.76	178.09	64.98	17.07
339	6.78	0.87	35.73	170.40	66.29	17.10
340	6.80	0.84	39.29	170.03	68.45	17.12
341	6.82	0.80	39.16	169.35	71.37	17.12
342	6.84	0.75	37.26	150.65	73.09	17.09
343	6.86	0.76	37.52	129.29	75.12	17.05
344	6.88	0.71	37.39	147.94	77.06	17.05
345	6.90	0.69	38.39	163.26	79.05	17.04
346	6.92	0.68	37.88	182.52	78.34	17.05
347	6.94	0.72	37.43	198.09	76.12	17.04
348	6.96	0.75	36.63	197.48	74.40	17.01
349	6.98	0.72	33.58	166.09	74.03	16.94
350	7.00	0.70	31.85	195.69	73.57	16.81
351	7.02	0.69	26.85	222.28	69.74	16.67
352	7.04	0.76	22.14	226.77	63.60	16.51
353	7.06	0.84	20.00	237.42	57.61	16.42
354	7.08	0.90	19.68	226.28	53.26	16.45
355	7.10	1.03	21.98	229.72	50.86	16.53
356	7.12	1.06	22.85	231.02	49.05	16.67
357	7.14	1.18	25.67	138.15	49.09	16.83
358	7.16	1.21	31.85	126.77	50.45	17.09
359	7.18	1.23	40.98	151.14	52.57	17.34
360	7.20	1.29	49.15	151.63	54.24	17.56
361	7.22	1.34	55.72	141.05	55.20	17.73
362	7.24	1.36	61.59	173.35	56.39	17.87
363	7.26	1.38	69.92	152.86	57.51	17.99
364	7.28	1.40	74.79	163.02	58.88	18.08
365	7.30	1.38	77.89	122.83	60.65	18.12
366	7.32	1.30	79.11	135.51	62.47	18.12
367	7.34	1.28	77.83	128.98	64.12	18.09
368	7.36	1.23	75.39	158.46	64.48	18.04
369	7.38	1.22	71.29	171.32	63.90	18.00
370	7.40	1.25	68.76	184.80	62.30	17.96
371	7.42	1.29	67.22	173.42	59.81	17.94
372	7.44	1.39	65.29	112.68	57.77	17.94
373	7.46	1.43	65.58	91.69	56.41	17.98
374	7.48	1.48	71.35	92.37	56.59	18.03
375	7.50	1.47	74.58	77.72	56.57	18.11
376	7.52	1.55	77.72	56.86	57.33	18.17
377	7.54	1.53	84.00	31.20	58.18	18.24
378	7.56	1.51	88.29	22.15	60.07	18.30
379	7.58	1.48	91.46	16.18	60.99	18.34
380	7.60	1.52	93.70	17.17	61.17	18.37
381	7.62	1.56	96.10	15.69	60.98	18.41
382	7.64	1.56	98.82	27.20	61.46	18.43
383	7.66	1.52	100.20	19.88	63.46	18.43
384	7.68	1.39	98.72	10.83	66.59	18.41

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
385	7.70	1.29	99.75	6.52	70.63	18.38
386	7.72	1.20	99.04	8.18	73.98	18.35
387	7.74	1.15	99.36	51.57	76.64	18.33
388	7.76	1.10	98.56	99.82	78.26	18.32
389	7.78	1.08	98.88	138.46	79.00	18.31
390	7.80	1.09	98.23	141.48	78.42	18.29
391	7.82	1.10	93.10	149.85	74.46	18.23
392	7.84	1.23	80.53	169.60	68.39	18.17
393	7.86	1.38	77.20	190.71	61.78	18.13
394	7.88	1.52	76.50	186.34	57.59	18.15
395	7.90	1.61	77.17	161.11	55.56	18.18
396	7.92	1.63	79.00	123.94	55.50	18.21
397	7.94	1.61	82.55	90.28	56.72	18.27
398	7.96	1.60	89.86	78.09	58.59	18.35
399	7.98	1.60	97.96	71.02	60.03	18.43
400	8.00	1.61	102.35	77.91	61.37	18.51
401	8.02	1.62	111.19	71.63	61.91	18.57
402	8.04	1.65	113.34	57.48	62.54	18.62
403	8.06	1.65	116.00	45.85	62.82	18.65
404	8.08	1.65	118.11	38.83	62.92	18.68
405	8.10	1.70	120.96	39.57	62.40	18.70
406	8.12	1.74	121.31	49.05	61.39	18.72
407	8.15	1.79	122.27	59.88	60.75	18.74
408	8.16	1.79	122.43	63.14	59.93	18.75
409	8.18	1.86	123.87	58.28	59.57	18.76
410	8.20	1.86	124.79	59.51	59.05	18.77
411	8.22	1.87	123.61	58.52	59.06	18.76
412	8.24	1.84	121.23	58.15	59.02	18.73
413	8.26	1.80	115.11	41.72	59.55	18.70
414	8.28	1.76	115.39	33.78	60.93	18.68
415	8.30	1.68	119.49	30.83	62.17	18.68
416	8.32	1.70	119.49	28.68	62.57	18.70
417	8.34	1.75	119.84	26.34	62.07	18.70
418	8.36	1.75	120.00	22.83	62.67	18.71
419	8.38	1.66	122.75	19.14	64.52	18.70
420	8.40	1.57	120.64	12.80	67.05	18.68
421	8.42	1.50	119.10	9.97	70.32	18.65
422	8.44	1.37	120.76	6.03	74.32	18.63
423	8.46	1.26	122.78	6.15	79.01	18.60
424	8.48	1.17	119.73	20.68	82.72	18.57
425	8.50	1.12	118.71	37.85	85.67	18.51
426	8.52	1.04	112.68	61.23	86.89	18.44
427	8.54	1.04	103.87	81.29	86.59	18.33
428	8.56	1.02	91.63	99.75	84.82	18.22
429	8.58	1.00	84.10	119.08	83.51	18.08
430	8.60	0.95	73.59	143.69	82.20	17.95
431	8.62	0.94	66.02	158.58	80.21	17.79
432	8.64	0.95	57.21	157.54	77.64	17.67

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
433	8.66	0.96	53.88	156.74	75.11	17.58
434	8.68	0.98	52.06	169.42	71.84	17.55
435	8.70	1.07	50.04	191.32	66.51	17.51
436	8.72	1.21	45.55	206.95	59.90	17.48
437	8.74	1.36	43.06	216.62	54.62	17.47
438	8.76	1.46	44.31	222.03	51.25	17.52
439	8.78	1.56	46.65	239.51	49.39	17.59
440	8.80	1.65	48.61	243.75	48.45	17.67
441	8.82	1.69	52.36	236.98	47.32	17.73
442	8.84	1.80	52.29	220.00	47.44	17.83
443	8.86	1.80	60.94	253.23	47.19	17.92
444	8.88	1.88	64.05	240.55	47.54	18.02
445	8.90	1.93	66.94	232.86	48.63	18.15
446	8.93	1.91	82.09	183.75	50.81	18.29
447	8.94	1.89	92.57	167.38	53.48	18.43
448	8.96	1.89	99.46	143.82	55.99	18.54
449	8.98	1.82	109.65	179.26	58.07	18.61
450	9.00	1.79	113.46	208.00	59.83	18.66
451	9.02	1.79	115.92	213.11	59.99	18.67
452	9.04	1.83	113.52	210.15	59.12	18.67
453	9.06	1.88	110.41	208.25	57.98	18.65
454	9.08	1.89	109.00	200.06	56.82	18.64
455	9.10	1.94	106.69	206.22	55.85	18.62
456	9.12	1.97	104.51	178.09	55.08	18.62
457	9.14	1.98	106.30	192.86	55.01	18.62
458	9.16	1.96	107.26	188.12	55.39	18.64
459	9.18	1.97	109.95	171.88	55.75	18.65
460	9.20	1.97	108.38	145.97	56.24	18.66
461	9.22	1.95	112.03	144.12	56.86	18.68
462	9.24	1.95	116.03	155.20	57.49	18.71
463	9.26	1.95	116.99	152.37	57.52	18.72
464	9.28	1.97	114.90	146.22	57.24	18.72
465	9.30	1.98	114.39	137.17	56.93	18.71
466	9.32	1.99	115.28	133.11	56.87	18.72
467	9.34	1.99	115.92	145.35	56.22	18.71
468	9.36	2.05	112.14	173.60	55.45	18.73
469	9.38	2.11	117.33	222.15	53.45	18.75
470	9.40	2.28	115.24	238.71	51.51	18.76
471	9.42	2.36	111.36	223.26	50.31	18.76
472	9.44	2.29	113.22	178.52	51.21	18.76
473	9.46	2.18	118.47	137.54	54.15	18.79
474	9.48	2.04	126.10	109.29	57.83	18.82
475	9.50	1.91	130.61	94.89	61.10	18.85
476	9.52	1.88	134.87	85.35	63.50	18.87
477	9.54	1.83	137.59	83.63	64.60	18.88
478	9.56	1.83	137.27	74.15	65.13	18.89
479	9.58	1.84	137.20	85.97	64.56	18.88
480	9.60	1.87	132.97	95.88	63.67	18.85

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
481	9.62	1.88	127.65	108.18	62.21	18.81
482	9.64	1.91	121.56	111.94	60.71	18.76
483	9.66	1.93	114.54	104.62	59.39	18.70
484	9.68	1.91	107.72	110.40	58.89	18.64
485	9.70	1.86	105.41	94.03	59.72	18.59
486	9.72	1.76	103.64	69.17	62.11	18.55
487	9.74	1.61	103.19	54.34	66.37	18.52
488	9.76	1.44	105.85	43.26	72.29	18.49
489	9.78	1.27	107.42	49.23	78.64	18.46
490	9.80	1.17	107.42	44.37	81.36	18.42
491	9.82	1.22	98.72	109.72	82.59	18.35
492	9.84	1.12	93.24	133.60	82.21	18.24
493	9.86	1.05	82.13	154.40	83.40	18.08
494	9.88	0.99	68.70	164.98	81.99	17.89
495	9.90	0.99	58.38	196.12	77.58	17.69
496	9.92	1.06	48.20	212.37	72.59	17.50
497	9.95	1.06	41.02	219.26	68.39	17.27
498	9.96	1.01	31.57	185.78	66.54	17.07
499	9.98	0.98	29.64	229.60	65.30	16.89
500	10.00	0.97	26.86	241.66	65.04	16.78
501	10.02	0.93	24.52	242.40	65.44	16.70
502	10.04	0.90	24.84	256.06	66.16	16.66
503	10.06	0.90	24.71	268.06	67.03	16.65
504	10.08	0.88	24.23	259.82	67.97	16.64
505	10.10	0.85	24.85	253.29	68.89	16.60
506	10.12	0.84	22.70	245.66	70.10	16.58
507	10.14	0.82	23.41	241.91	70.49	16.54
508	10.16	0.82	22.77	239.38	70.84	16.54
509	10.18	0.83	22.93	241.17	71.28	16.57
510	10.20	0.82	24.89	243.20	71.98	16.62
511	10.22	0.82	25.69	254.52	72.22	16.66
512	10.24	0.85	25.85	271.88	68.98	16.68
513	10.26	0.96	24.25	297.91	63.07	16.69
514	10.28	1.11	24.09	310.71	57.80	16.75
515	10.30	1.20	26.88	336.92	53.32	16.83
516	10.32	1.35	26.88	348.55	50.51	16.94
517	10.34	1.45	29.13	364.31	48.29	17.02
518	10.36	1.51	31.12	326.83	49.43	17.19
519	10.38	1.46	39.58	303.26	52.34	17.37
520	10.40	1.43	47.11	296.31	55.73	17.55
521	10.42	1.44	51.53	295.75	57.87	17.68
522	10.44	1.45	56.11	296.37	59.55	17.78
523	10.46	1.42	61.53	316.37	61.39	17.86
524	10.48	1.40	64.29	294.52	63.23	17.92
525	10.50	1.38	66.27	278.58	65.03	17.93
526	10.52	1.32	65.79	273.72	66.95	17.94
527	10.54	1.28	66.92	270.34	68.60	17.92
528	10.56	1.25	65.73	269.48	69.13	17.89

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
529	10.58	1.25	61.47	268.18	68.35	17.85
530	10.60	1.28	59.74	266.58	67.71	17.81
531	10.62	1.26	60.06	264.68	67.21	17.80
532	10.64	1.27	59.42	271.38	66.74	17.80
533	10.66	1.31	58.90	279.82	65.01	17.80
534	10.68	1.38	58.42	300.62	61.98	17.81
535	10.70	1.51	57.52	320.00	59.21	17.84
536	10.72	1.58	60.31	294.83	57.88	17.91
537	10.74	1.60	65.73	272.49	57.81	17.98
538	10.76	1.64	68.13	269.11	58.18	18.04
539	10.78	1.65	69.54	248.55	59.06	18.08
540	10.80	1.60	73.89	230.28	60.61	18.14
541	10.82	1.60	79.33	175.08	63.12	18.22
542	10.84	1.58	88.65	143.75	65.57	18.32
543	10.86	1.55	95.32	137.35	68.33	18.39
544	10.88	1.50	99.55	140.37	70.44	18.43
545	10.90	1.48	100.80	132.68	71.93	18.44
546	10.92	1.46	100.12	128.80	72.65	18.43
547	10.94	1.44	98.26	124.98	73.33	18.42
548	10.96	1.42	97.91	122.46	74.38	18.38
549	10.98	1.33	92.59	148.92	75.35	18.33
550	11.00	1.31	88.96	165.54	75.49	18.26
551	11.02	1.31	83.07	180.43	74.40	18.20
552	11.04	1.33	79.89	183.94	73.18	18.14
553	11.06	1.32	76.78	183.32	72.33	18.10
554	11.08	1.32	74.57	187.08	71.79	18.07
555	11.10	1.32	72.52	189.85	71.02	18.03
556	11.13	1.33	70.66	187.20	70.83	18.03
557	11.14	1.33	72.83	188.06	70.95	18.05
558	11.17	1.34	76.23	195.14	71.34	18.10
559	11.18	1.37	79.53	208.49	71.49	18.14
560	11.20	1.37	80.94	217.66	70.60	18.17
561	11.22	1.43	79.97	229.72	69.02	18.18
562	11.24	1.50	79.65	237.60	66.92	18.19
563	11.26	1.54	80.26	242.71	65.38	18.21
564	11.28	1.58	80.58	245.35	64.07	18.22
565	11.30	1.63	79.71	249.23	62.91	18.23
566	11.32	1.67	80.70	235.38	62.17	18.26
567	11.34	1.69	84.87	252.31	61.46	18.31
568	11.36	1.77	87.75	258.28	60.97	18.37
569	11.39	1.81	91.53	250.52	60.93	18.44
570	11.40	1.84	100.60	240.00	61.56	18.53
571	11.42	1.86	107.26	228.06	62.66	18.62
572	11.44	1.88	115.56	220.18	63.73	18.69
573	11.46	1.87	120.94	203.14	65.58	18.76
574	11.48	1.81	128.72	183.26	68.04	18.81
575	11.50	1.75	135.93	161.78	70.78	18.86
576	11.52	1.73	142.18	141.91	73.37	18.90

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
577	11.54	1.66	146.15	136.00	75.63	18.92
578	11.56	1.62	148.36	126.71	77.58	18.92
579	11.58	1.58	146.88	125.60	78.65	18.91
580	11.60	1.56	143.61	134.03	78.43	18.88
581	11.62	1.59	138.00	151.32	77.10	18.83
582	11.64	1.61	130.09	159.63	75.76	18.78
583	11.66	1.58	123.97	154.40	74.93	18.72
584	11.68	1.56	118.93	147.88	74.28	18.67
585	11.70	1.59	114.99	147.32	73.84	18.64
586	11.72	1.57	113.51	149.97	73.45	18.61
587	11.75	1.56	112.45	155.20	73.71	18.58
588	11.76	1.53	107.58	172.49	73.42	18.55
589	11.78	1.53	104.25	170.89	73.51	18.47
590	11.80	1.45	94.24	177.60	73.06	18.45
591	11.82	1.53	101.61	173.42	73.54	18.44
592	11.84	1.49	102.89	162.15	74.04	18.46
593	11.86	1.45	100.04	152.55	74.99	18.43
594	11.88	1.43	95.11	151.08	75.78	18.38
595	11.91	1.38	93.02	150.52	75.54	18.34
596	11.92	1.41	89.92	148.80	75.27	18.30
597	11.94	1.40	87.38	145.29	74.63	18.28
598	11.96	1.40	87.45	143.38	74.49	18.27
599	11.98	1.41	88.12	156.06	73.93	18.26
600	12.00	1.43	84.72	164.12	71.93	18.23
601	12.02	1.49	77.80	158.40	70.26	18.19
602	12.04	1.49	78.35	151.88	69.43	18.16
603	12.06	1.46	78.41	146.52	70.37	18.15
604	12.08	1.42	77.35	137.72	71.68	18.14
605	12.10	1.38	77.06	133.85	72.64	18.12
606	12.20	1.38	76.33	133.85	73.38	18.11
607	12.20	1.38	76.33	133.85	73.45	18.10
608	12.11	1.36	75.43	133.35	73.26	18.06
609	12.20	1.33	70.53	125.42	73.32	18.03
610	12.22	1.34	69.41	127.63	73.71	17.99
611	12.24	1.30	70.05	119.88	74.58	17.98
612	12.26	1.27	69.50	118.95	75.64	17.96
613	12.28	1.27	68.32	123.63	75.51	17.93
614	12.30	1.28	65.08	121.54	75.11	17.89
615	12.32	1.24	61.75	118.52	74.94	17.84
616	12.34	1.22	60.34	114.95	75.43	17.78
617	12.36	1.20	58.26	112.74	75.34	17.74
618	12.38	1.20	55.18	112.18	73.45	17.68
619	12.40	1.27	51.21	123.51	71.19	17.65
620	12.42	1.30	51.85	130.52	69.31	17.64
621	12.44	1.32	53.01	134.03	68.77	17.66
622	12.46	1.33	53.33	140.43	67.63	17.67
623	12.48	1.39	51.95	144.18	65.97	17.67
624	12.50	1.43	51.63	147.45	64.64	17.68

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
625	12.52	1.45	53.55	146.95	65.54	17.73
626	12.55	1.38	57.97	138.09	67.75	17.76
627	12.56	1.33	58.52	133.54	70.43	17.78
628	12.58	1.29	57.82	118.95	73.29	17.77
629	12.60	1.20	60.03	112.62	76.17	17.76
630	12.62	1.16	59.23	110.83	78.55	17.75
631	12.64	1.15	58.75	118.46	78.61	17.73
632	12.66	1.17	56.99	127.20	77.29	17.70
633	12.68	1.20	54.68	129.66	76.27	17.67
634	12.70	1.17	53.05	125.66	76.54	17.62
635	12.72	1.12	51.00	115.69	78.62	17.58
636	12.74	1.06	50.93	108.68	81.23	17.56
637	12.76	1.04	52.95	104.86	83.87	17.55
638	12.78	0.99	51.22	101.97	84.91	17.52
639	12.80	0.98	48.60	201.17	85.99	17.48
640	12.83	0.95	49.08	192.80	86.54	17.45
641	12.84	0.94	48.32	187.75	87.97	17.45
642	12.86	0.92	48.83	187.45	88.17	17.43
643	12.88	0.94	47.52	192.25	87.76	17.41
644	12.90	0.94	45.69	189.17	87.87	17.38
645	12.92	0.90	45.37	179.02	89.82	17.35
646	12.94	0.85	45.43	168.18	93.16	17.33
647	12.96	0.82	45.24	164.31	96.52	17.28
648	12.98	0.77	41.91	159.14	100.00	17.22
649	13.00	0.72	40.30	154.34	100.00	17.13
650	13.02	0.71	37.42	150.71	100.00	17.05
651	13.04	0.70	35.08	155.20	100.00	16.94
652	13.06	0.72	30.05	169.72	94.44	16.81
653	13.08	0.81	25.21	187.51	86.25	16.65
654	13.10	0.84	21.72	196.49	79.66	16.51
655	13.12	0.86	20.09	197.48	77.15	16.38
656	13.14	0.82	17.72	193.29	76.00	16.21
657	13.16	0.79	13.90	207.63	71.62	16.05
658	13.18	0.93	13.13	236.86	64.06	16.00
659	13.20	1.11	14.16	250.95	59.55	16.13
660	13.22	1.13	17.14	183.20	59.77	16.29
661	13.24	1.06	19.48	180.92	61.08	16.39
662	13.26	1.12	18.49	208.68	59.93	16.41
663	13.28	1.21	17.98	220.49	59.48	16.45
664	13.30	1.12	20.73	160.37	63.07	16.53
665	13.32	0.98	23.52	156.25	66.46	16.61
666	13.34	1.09	23.23	236.62	64.69	16.64
667	13.36	1.23	21.76	252.43	61.40	16.68
668	13.41	1.20	24.29	213.54	60.24	16.70
669	13.41	1.20	24.29	213.54	67.13	16.71
670	13.42	0.84	25.00	155.69	76.54	16.65
671	13.44	0.72	24.36	187.51	90.43	16.53
672	13.46	0.67	21.55	200.62	94.95	16.44

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
673	13.48	0.67	21.10	204.55	86.85	16.45
674	13.50	0.92	22.70	283.32	65.36	16.55
675	13.52	1.57	20.17	372.55	48.13	16.64
676	13.54	2.06	19.08	242.46	37.76	16.79
677	13.56	2.44	24.66	186.71	34.72	17.01
678	13.58	2.52	30.36	150.28	35.03	17.27
679	13.60	2.54	36.35	105.17	37.15	17.45
680	13.62	2.41	40.29	80.37	41.02	17.56
681	13.64	2.07	43.50	54.46	47.66	17.59
682	13.66	1.62	44.91	30.71	57.34	17.48
683	13.68	1.18	38.21	23.94	68.73	17.27
684	13.70	0.98	31.80	36.12	79.13	17.00
685	13.72	0.85	27.90	99.88	86.23	16.78
686	13.74	0.75	24.76	109.85	91.92	16.66
687	13.76	0.72	25.91	141.48	95.86	16.58
688	13.78	0.69	24.34	182.15	98.49	16.66
689	13.80	0.70	30.27	254.15	98.43	16.64
690	13.83	0.69	24.76	232.55	100.00	16.59
691	13.84	0.64	21.65	172.62	100.00	16.41
692	13.86	0.60	20.31	175.32	100.00	16.29
693	14.03	0.56	19.57	173.23	100.00	16.23
694	14.03	0.56	19.57	173.23	100.00	16.21
695	14.03	0.56	19.28	172.92	100.00	16.20
696	13.88	0.56	19.28	172.92	100.00	16.15
697	13.96	0.66	15.92	209.91	95.98	16.09
698	13.98	0.71	15.31	220.18	87.42	16.03
699	14.00	0.73	15.41	225.29	83.64	16.05
700	14.02	0.77	15.85	233.42	81.16	16.10
701	14.04	0.80	16.62	242.46	78.95	16.17
702	14.06	0.84	18.00	250.58	77.16	16.26
703	14.08	0.88	19.16	260.43	75.51	16.37
704	14.10	0.92	20.85	269.54	74.51	16.47
705	14.12	0.94	22.42	275.26	73.35	16.55
706	14.14	0.98	22.81	282.95	72.66	16.59
707	14.16	0.98	22.94	283.63	72.86	16.60
708	14.18	0.95	23.10	268.49	74.38	16.61
709	14.21	0.92	23.74	263.94	76.54	16.61
710	14.22	0.90	23.87	263.32	77.52	16.62
711	14.24	0.91	23.64	262.34	78.20	16.63
712	14.26	0.90	24.44	261.48	78.29	16.65
713	14.28	0.91	25.02	261.54	78.80	16.69
714	14.30	0.92	26.17	258.83	79.61	16.74
715	14.32	0.91	28.06	257.48	80.59	16.80
716	14.37	0.92	28.99	259.26	81.50	16.84
717	14.37	0.92	28.99	259.26	82.20	16.89
718	14.38	0.92	32.26	255.82	83.31	16.97
719	14.40	0.92	34.86	257.42	84.29	17.05
720	14.42	0.94	36.36	265.35	84.53	17.11

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
721	14.44	0.95	37.29	267.14	83.90	17.16
722	14.46	0.98	38.51	270.28	83.18	17.20
723	14.48	1.00	39.50	277.97	82.35	17.24
724	14.50	1.02	40.59	285.05	80.97	17.27
725	14.52	1.07	41.04	292.31	79.31	17.30
726	14.54	1.09	40.84	293.97	77.72	17.32
727	14.56	1.11	41.58	290.58	77.19	17.34
728	14.58	1.12	42.67	284.80	77.69	17.36
729	14.60	1.10	43.79	279.75	78.84	17.39
730	14.62	1.08	44.33	276.55	79.68	17.39
731	14.64	1.09	43.82	275.69	79.88	17.38
732	14.66	1.08	42.92	278.58	79.03	17.37
733	14.68	1.11	42.63	283.63	76.81	17.36
734	14.70	1.18	41.03	291.14	74.65	17.36
735	14.72	1.20	41.93	286.40	72.72	17.37
736	14.74	1.24	42.50	239.26	71.90	17.40
737	14.76	1.27	43.08	232.31	72.25	17.47
738	14.78	1.26	49.20	230.28	73.45	17.57
739	14.80	1.27	54.60	266.34	74.84	17.70
740	14.82	1.32	59.79	261.78	75.60	17.80
741	14.84	1.33	63.54	265.35	75.81	17.90
742	14.86	1.38	69.37	282.89	76.11	17.98
743	14.88	1.39	71.67	284.06	76.16	18.03
744	14.90	1.39	72.54	269.60	76.60	18.06
745	14.92	1.38	73.95	264.06	76.73	18.07
746	14.94	1.39	72.95	268.00	76.84	18.07
747	14.96	1.40	73.91	271.75	76.96	18.09
748	14.98	1.39	75.99	296.92	76.92	18.10
749	15.00	1.42	76.25	306.22	76.30	18.12
750	15.02	1.45	75.12	308.98	75.25	18.12
751	15.04	1.46	75.63	314.71	74.30	18.12
752	15.06	1.49	75.70	316.98	74.24	18.14
753	15.08	1.47	77.33	322.03	74.34	18.13
754	15.10	1.45	75.21	323.45	74.55	18.11
755	15.12	1.45	72.23	323.82	74.30	18.09
756	15.14	1.45	72.17	323.75	74.20	18.07
757	15.16	1.44	71.65	323.88	74.09	18.06
758	15.18	1.45	70.46	327.51	73.77	18.04
759	15.20	1.46	68.96	327.32	73.26	18.03
760	15.22	1.46	68.96	328.86	72.87	18.02
761	15.24	1.47	69.43	335.69	72.49	18.03
762	15.26	1.49	68.95	330.15	71.98	18.04
763	15.28	1.51	70.17	326.89	72.14	18.07
764	15.30	1.50	74.52	325.60	73.03	18.12
765	15.32	1.50	79.01	326.83	74.21	18.17
766	15.34	1.49	79.52	327.08	74.81	18.21
767	15.36	1.52	83.40	336.00	75.39	18.25
768	15.38	1.51	87.27	341.48	75.63	18.29

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
769	15.40	1.53	87.69	353.05	75.23	18.30
770	15.42	1.56	84.67	357.35	73.55	18.27
771	15.44	1.60	79.86	361.97	71.54	18.22
772	15.46	1.61	75.67	362.03	70.16	18.18
773	15.48	1.61	74.86	363.08	69.53	18.16
774	15.50	1.62	75.05	362.09	69.44	18.16
775	15.52	1.63	75.63	359.63	69.65	18.17
776	15.54	1.62	77.33	355.57	69.79	18.19
777	15.56	1.65	79.06	358.28	70.39	18.23
778	15.58	1.64	83.25	354.77	71.33	18.27
779	15.60	1.60	85.27	343.20	72.84	18.29
780	15.62	1.57	85.97	331.38	74.29	18.30
781	15.64	1.55	86.90	333.66	75.05	18.30
782	15.66	1.54	85.68	331.26	74.83	18.27
783	15.68	1.56	80.75	334.77	73.72	18.24
784	15.70	1.58	77.80	330.83	72.53	18.19
785	15.72	1.58	76.42	325.54	72.21	18.18
786	15.74	1.57	77.35	307.14	72.94	18.17
787	15.76	1.52	77.38	295.57	74.16	18.18
788	15.78	1.51	79.33	292.18	75.61	18.19
789	15.80	1.47	80.32	336.37	76.18	18.24
790	15.82	1.55	88.85	341.72	77.70	18.29
791	15.84	1.46	89.75	304.18	78.55	18.32
792	15.86	1.47	88.88	291.57	79.65	18.32
793	15.88	1.49	89.20	293.85	78.92	18.32
794	15.90	1.52	89.07	307.69	78.56	18.32
795	15.92	1.49	88.91	336.00	77.68	18.32
796	15.94	1.54	86.89	327.63	77.12	18.31
797	15.96	1.55	86.02	299.88	77.26	18.31
798	15.98	1.49	89.67	323.08	78.42	18.34
799	16.00	1.49	93.61	342.58	79.09	18.37
800	16.02	1.54	93.90	355.26	77.27	18.40
801	16.04	1.66	94.06	378.89	73.43	18.42
802	16.07	1.80	92.04	400.00	69.20	18.43
803	16.08	1.92	89.03	372.86	65.32	18.41
804	16.10	2.03	84.96	286.65	62.47	18.38
805	16.12	2.09	81.30	239.14	61.07	18.35
806	16.14	2.06	81.49	220.37	61.41	18.35
807	16.16	2.01	86.01	224.12	62.33	18.40
808	16.18	2.07	91.23	234.58	62.98	18.47
809	16.20	2.12	97.35	247.02	63.57	18.56
810	16.22	2.11	106.00	237.66	64.77	18.64
811	16.24	2.11	113.56	223.32	66.26	18.71
812	16.26	2.08	115.67	216.12	68.43	18.78
813	16.28	2.03	129.22	215.14	70.95	18.84
814	16.30	1.97	137.46	242.03	73.53	18.91
815	16.32	1.94	139.92	262.28	74.59	18.93
816	16.34	1.97	140.30	299.02	74.22	18.95

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
817	16.36	2.02	140.33	336.68	73.20	18.94
818	16.38	2.02	136.42	341.72	72.45	18.91
819	16.40	1.99	129.76	328.80	72.94	18.86
820	16.42	1.88	126.04	318.40	74.82	18.82
821	16.44	1.77	125.84	288.31	78.48	18.79
822	16.46	1.64	128.05	277.60	81.60	18.76
823	16.48	1.60	122.57	272.98	84.30	18.71
824	16.50	1.52	117.54	270.52	86.22	18.65
825	16.52	1.42	113.18	270.22	88.45	18.56
826	16.54	1.35	102.80	274.15	89.52	18.45
827	16.56	1.33	91.97	281.72	87.97	18.29
828	16.58	1.32	76.01	303.75	84.60	18.11
829	16.60	1.32	62.29	307.26	81.10	17.88
830	16.62	1.27	51.46	297.85	78.98	17.67
831	16.64	1.23	46.34	288.25	78.73	17.49
832	16.66	1.16	41.02	284.12	79.10	17.34
833	16.68	1.12	35.99	280.31	80.17	17.20
834	16.70	1.06	34.13	288.55	80.14	17.09
835	16.72	1.07	31.38	310.52	79.63	17.02
836	16.74	1.08	30.48	336.68	77.23	16.96
837	16.76	1.11	28.18	347.57	75.63	16.89
838	16.78	1.09	26.32	344.98	72.03	16.77
839	16.80	1.14	21.22	491.94	69.25	16.68
840	16.82	1.16	22.08	500.37	66.18	16.60
841	16.84	1.18	21.15	499.88	65.78	16.61
842	16.86	1.17	21.25	496.06	66.21	16.60
843	16.88	1.14	22.05	491.20	66.90	16.62
844	16.90	1.15	22.24	500.37	67.64	16.64
845	16.92	1.14	22.34	506.77	67.34	16.63
846	16.94	1.15	21.77	514.83	66.94	16.62
847	16.96	1.16	21.38	518.71	65.91	16.60
848	16.98	1.18	21.06	527.82	64.38	16.59
849	17.00	1.23	20.45	550.22	61.69	16.56
850	17.02	1.31	19.04	560.00	57.80	16.53
851	17.04	1.44	18.47	586.34	54.92	16.54
852	17.06	1.47	19.78	573.11	53.54	16.59
853	17.08	1.49	20.94	570.65	55.04	16.69
854	17.10	1.41	23.50	527.45	58.09	16.78
855	17.12	1.33	26.07	481.78	61.90	16.86
856	17.14	1.30	27.09	455.20	66.69	16.94
857	17.16	1.18	31.10	468.12	70.11	16.98
858	17.18	1.16	30.20	478.46	73.60	16.97
859	17.20	1.09	27.70	457.78	75.12	16.91
860	17.22	1.05	27.67	449.54	77.05	16.84
861	17.24	1.01	26.17	473.85	77.13	16.75
862	17.26	1.01	22.20	521.66	73.73	16.60
863	17.28	1.09	18.13	550.40	67.20	16.44
864	17.30	1.20	16.14	608.80	60.87	16.31

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
865	17.32	1.32	14.99	425.48	57.73	16.31
866	17.34	1.34	17.14	393.72	57.74	16.40
867	17.36	1.33	19.86	415.51	59.63	16.54
868	17.38	1.30	21.59	466.83	61.14	16.61
869	17.44	1.29	21.33	479.14	61.90	16.64
870	17.44	1.29	21.33	479.14	60.86	16.68
871	17.44	1.38	23.13	622.83	58.78	16.74
872	17.46	1.48	24.06	652.18	56.72	16.81
873	17.48	1.51	23.93	587.88	55.29	16.83
874	17.50	1.54	23.71	589.23	56.26	16.85
875	17.52	1.48	25.92	378.58	60.20	16.96
876	17.54	1.34	32.55	398.89	64.64	17.03
877	17.56	1.31	30.37	423.26	69.07	17.07
878	17.58	1.22	31.21	415.45	71.44	17.04
879	17.63	1.16	31.46	410.03	74.12	17.04
880	17.63	1.16	31.46	410.03	77.06	16.99
881	17.64	1.01	28.39	447.51	78.01	16.88
882	17.66	1.01	24.51	521.35	77.56	16.70
883	17.68	1.02	19.86	535.20	73.96	16.52
884	17.70	1.03	17.56	526.95	71.74	16.35
885	17.72	1.00	16.27	520.37	70.36	16.25
886	17.74	1.02	15.28	532.18	68.96	16.14
887	17.76	1.02	12.97	537.97	66.94	16.04
888	17.78	1.04	12.46	544.06	61.08	15.98
889	17.80	1.35	12.09	374.22	60.30	16.08
890	17.82	1.19	16.03	351.63	60.94	16.18
891	17.84	1.10	15.97	438.09	65.88	16.22
892	17.86	1.05	14.69	507.20	67.06	16.14
893	17.88	1.04	13.47	532.12	67.23	16.07
894	17.90	1.02	13.53	550.03	66.91	16.03
895	17.95	1.04	13.57	551.88	66.89	16.04
896	17.95	1.04	13.57	551.88	64.08	16.01
897	17.96	1.15	12.00	596.18	60.42	15.98
898	17.98	1.23	11.93	618.52	57.37	15.97
899	18.00	1.23	12.57	617.23	56.66	16.06
900	18.02	1.27	14.59	619.63	56.50	16.17
901	18.04	1.33	15.30	629.60	52.72	16.31
902	18.06	1.66	16.52	728.43	47.65	16.41
903	18.08	1.87	16.64	780.18	42.17	16.48
904	18.10	2.14	16.20	459.14	40.00	16.66
905	18.12	2.33	23.34	321.42	40.97	16.92
906	18.14	2.24	30.04	231.69	45.18	17.20
907	18.16	2.02	35.45	192.98	51.10	17.35
908	18.18	1.80	39.52	181.85	58.28	17.51
909	18.20	1.63	48.88	365.54	64.41	17.61
910	18.22	1.52	50.54	509.78	67.08	17.68
911	18.24	1.62	50.41	440.25	68.89	17.68
912	18.26	1.47	49.90	404.18	71.10	17.65

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
913	18.28	1.31	48.30	531.75	74.42	17.54
914	18.30	1.26	40.93	565.42	74.49	17.35
915	18.32	1.24	30.26	547.88	72.55	17.13
916	18.34	1.20	28.65	588.43	70.62	16.94
917	18.36	1.19	26.09	593.23	69.75	16.87
918	18.38	1.22	25.13	603.45	69.06	16.80
919	18.40	1.18	23.88	594.77	67.91	16.70
920	18.42	1.18	20.22	615.02	65.17	16.55
921	18.44	1.25	16.12	647.51	61.29	16.42
922	18.46	1.33	17.08	662.77	58.93	16.42
923	18.48	1.34	19.26	652.55	59.66	16.50
924	18.50	1.28	20.03	638.77	62.24	16.57
925	18.52	1.21	21.09	606.22	65.36	16.57
926	18.54	1.14	20.25	593.35	66.78	16.54
927	18.56	1.17	19.00	626.58	64.80	16.51
928	18.58	1.30	19.10	674.95	61.51	16.52
929	18.60	1.36	19.68	671.45	60.85	16.61
930	18.62	1.31	22.85	569.78	63.73	16.68
931	18.64	1.19	23.71	554.58	66.72	16.67
932	18.66	1.18	20.51	583.69	67.97	16.61
933	18.68	1.17	19.84	601.23	66.85	16.56
934	18.70	1.20	20.77	627.14	65.80	16.60
935	18.72	1.27	22.08	652.86	63.05	16.66
936	18.74	1.41	22.37	667.26	60.53	16.65
937	18.76	1.36	18.84	658.03	64.68	16.86
938	18.78	1.21	35.46	467.63	67.21	17.22
939	18.80	1.70	48.98	193.72	71.96	17.51
940	18.82	1.44	48.62	242.83	71.91	17.57
941	18.84	1.30	42.57	429.66	74.96	17.46
942	18.86	1.31	38.37	500.12	72.39	17.33
943	18.89	1.41	35.39	554.89	68.36	17.27
944	18.90	1.48	34.59	575.02	63.40	17.22
945	18.92	1.60	31.19	622.03	58.84	17.16
946	18.94	1.73	28.34	646.89	53.16	17.10
947	18.96	1.96	26.99	703.75	47.28	17.08
948	18.98	2.29	26.16	746.22	42.85	17.14
949	19.00	2.51	30.10	579.08	41.67	17.33
950	19.02	2.56	39.46	452.68	42.97	17.53
951	19.04	2.53	43.43	432.31	47.87	17.76
952	19.07	2.21	57.30	322.40	53.40	17.91
953	19.08	2.04	63.00	345.97	59.85	18.02
954	19.10	1.91	65.44	402.95	63.70	18.05
955	19.13	1.80	64.89	449.17	66.73	18.04
956	19.14	1.71	65.15	458.77	69.04	17.99
957	19.16	1.62	60.05	454.46	71.01	17.92
958	19.18	1.55	56.91	453.66	70.90	17.81
959	19.20	1.57	50.15	516.74	67.06	17.71
960	19.22	1.77	44.22	600.74	59.79	17.60

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
961	19.24	2.04	39.25	665.35	53.67	17.56
962	19.26	2.21	40.63	471.63	50.70	17.62
963	19.28	2.31	47.55	424.37	48.52	17.73
964	19.31	2.62	49.09	503.20	48.68	17.86
965	19.32	2.50	55.33	246.28	51.43	17.99
966	19.34	2.20	67.15	157.23	58.72	18.08
967	19.36	1.84	69.78	234.40	65.75	18.10
968	19.38	1.72	66.22	412.74	67.29	18.05
969	19.40	1.91	61.90	506.28	61.81	18.02
970	19.42	2.27	58.66	604.06	54.38	18.03
971	19.44	2.63	58.85	579.20	49.33	18.06
972	19.46	2.78	60.90	507.32	47.34	18.14
973	19.48	2.87	67.27	314.34	47.75	18.23
974	19.50	2.83	71.82	211.20	50.29	18.26
975	19.52	2.46	69.61	166.95	55.10	18.22
976	19.54	2.05	67.24	147.26	63.49	18.14
977	19.56	1.64	69.67	194.22	72.87	18.02
978	19.58	1.38	61.12	348.55	79.65	17.91
979	19.60	1.35	56.57	509.66	80.35	17.80
980	19.62	1.40	54.80	535.94	77.87	17.75
981	19.64	1.44	52.82	550.52	75.43	17.69
982	19.66	1.44	46.92	547.20	72.66	17.58
983	19.68	1.46	40.00	555.75	68.19	17.41
984	19.70	1.57	32.47	545.29	60.93	17.25
985	19.72	1.83	28.88	658.89	54.56	17.11
986	19.74	1.92	26.31	577.29	50.82	17.05
987	19.76	1.74	30.29	307.38	54.81	17.10

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (m)
q_c:	Measured cone resistance (MPa)
f_s:	Sleeve friction resistance (kPa)
u:	Pore pressure (kPa)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (kN/m^3)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1	0.02	0.31	0.00	0.31	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
2	0.04	0.63	0.00	0.63	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
3	0.06	0.95	0.00	0.95	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
4	0.08	1.28	0.00	1.28	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
5	0.10	1.62	0.00	1.62	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
6	0.12	1.96	0.00	1.96	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
7	0.14	2.30	0.00	2.30	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
8	0.16	2.64	0.00	2.64	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
9	0.18	2.99	0.00	2.99	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
10	0.20	3.35	0.00	3.35	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
11	0.22	3.70	0.00	3.70	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
12	0.24	4.06	0.00	4.06	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
13	0.26	4.42	0.00	4.42	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
14	0.28	4.78	0.00	4.78	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
15	0.30	5.13	0.00	5.13	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
16	0.32	5.49	0.00	5.49	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
17	0.34	5.85	0.00	5.85	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
18	0.36	6.22	0.00	6.22	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
19	0.38	6.58	0.00	6.58	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
20	0.40	6.94	0.00	6.94	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
21	0.42	7.30	0.00	7.30	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
22	0.44	7.66	0.00	7.66	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
23	0.46	8.02	0.00	8.02	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
24	0.48	8.39	0.00	8.39	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
25	0.50	8.75	0.00	8.75	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
26	0.52	9.11	0.00	9.11	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
27	0.54	9.47	0.00	9.47	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
28	0.56	9.84	0.00	9.84	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
29	0.58	10.20	0.00	10.20	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
30	0.60	10.56	0.00	10.56	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
31	0.62	10.93	0.00	10.93	1.00	0.149	1.43	0.105	1.10	1.00	2.000	No
32	0.64	11.29	0.00	11.29	1.00	0.149	1.43	0.105	1.10	1.00	2.000	No
33	0.66	11.65	0.00	11.65	1.00	0.149	1.43	0.105	1.10	1.00	2.000	No
34	0.68	12.01	0.00	12.01	1.00	0.149	1.43	0.105	1.10	1.00	2.000	No
35	0.70	12.37	0.00	12.37	1.00	0.149	1.43	0.105	1.10	1.00	2.000	No
36	0.72	12.74	0.00	12.74	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
37	0.74	13.10	0.00	13.10	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
38	0.76	13.46	0.00	13.46	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
39	0.78	13.83	0.00	13.83	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
40	0.80	14.19	0.00	14.19	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
41	0.82	14.55	0.00	14.55	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
42	0.84	14.92	0.00	14.92	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
43	0.86	15.28	0.00	15.28	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
44	0.88	15.64	0.00	15.64	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
45	0.90	16.00	0.00	16.00	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
46	0.92	16.36	0.00	16.36	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
47	0.95	16.90	0.00	16.90	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
48	0.96	17.08	0.00	17.08	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
49	0.98	17.44	0.00	17.44	0.99	0.149	1.43	0.104	1.10	1.00	2.000	No
50	1.00	17.80	0.00	17.80	0.99	0.149	1.43	0.104	1.10	1.00	2.000	No
51	1.02	18.16	0.20	17.97	0.99	0.150	1.43	0.105	1.10	1.00	0.124	No
52	1.05	18.71	0.49	18.22	0.99	0.153	1.43	0.107	1.10	1.00	0.126	No
53	1.06	18.89	0.59	18.30	0.99	0.153	1.43	0.107	1.10	1.00	0.127	No
54	1.08	19.26	0.78	18.47	0.99	0.155	1.43	0.108	1.10	1.00	0.128	No
55	1.10	19.63	0.98	18.64	0.99	0.156	1.43	0.109	1.10	1.00	0.129	No
56	1.12	19.99	1.18	18.82	0.99	0.158	1.43	0.110	1.10	1.00	0.130	No
57	1.14	20.36	1.37	18.99	0.99	0.159	1.43	0.111	1.10	1.00	0.131	No
58	1.16	20.73	1.57	19.16	0.99	0.160	1.43	0.112	1.10	1.00	0.132	No
59	1.18	21.10	1.77	19.33	0.99	0.162	1.43	0.113	1.10	1.00	0.133	No
60	1.20	21.47	1.96	19.50	0.99	0.163	1.43	0.114	1.10	1.00	0.134	No
61	1.22	21.84	2.16	19.68	0.99	0.164	1.43	0.115	1.10	1.00	0.135	No
62	1.24	22.21	2.35	19.85	0.99	0.166	1.43	0.116	1.10	1.00	0.136	No
63	1.26	22.58	2.55	20.03	0.99	0.167	1.43	0.117	1.10	1.00	0.137	No
64	1.28	22.95	2.75	20.20	0.99	0.168	1.43	0.118	1.10	1.00	0.138	No
65	1.30	23.32	2.94	20.37	0.99	0.169	1.43	0.119	1.10	1.00	0.139	No
66	1.32	23.69	3.14	20.55	0.99	0.171	1.43	0.119	1.10	1.00	0.140	No
67	1.34	24.06	3.34	20.73	0.99	0.172	1.43	0.120	1.10	1.00	0.140	No
68	1.36	24.43	3.53	20.90	0.99	0.173	1.43	0.121	1.10	1.00	0.141	No
69	1.38	24.81	3.73	21.08	0.99	0.174	1.43	0.122	1.10	1.00	0.141	No
70	1.40	25.18	3.92	21.26	0.99	0.175	1.43	0.123	1.10	1.00	0.142	No
71	1.44	25.93	4.32	21.61	0.99	0.177	1.43	0.124	1.10	1.00	0.143	No
72	1.44	25.93	4.32	21.61	0.99	0.177	1.43	0.124	1.10	1.00	0.143	No
73	1.51	27.23	5.00	22.23	0.99	0.181	1.43	0.126	1.10	1.00	0.145	No
74	1.51	27.23	5.00	22.23	0.99	0.181	1.43	0.126	1.10	1.00	0.145	No
75	1.51	27.23	5.00	22.23	0.99	0.181	1.43	0.126	1.10	1.00	0.145	No
76	1.52	27.42	5.10	22.32	0.99	0.181	1.43	0.127	1.10	1.00	0.144	No
77	1.54	27.80	5.30	22.51	0.99	0.182	1.43	0.128	1.10	1.00	0.144	No
78	1.56	28.19	5.49	22.69	0.99	0.183	1.43	0.128	1.10	1.00	0.146	No
79	1.58	28.57	5.69	22.88	0.99	0.184	1.43	0.129	1.10	1.00	0.146	No
80	1.60	28.95	5.89	23.07	0.99	0.185	1.43	0.129	1.10	1.00	0.147	No
81	1.62	29.34	6.08	23.26	0.99	0.186	1.43	0.130	1.10	1.00	0.147	No
82	1.64	29.72	6.28	23.45	0.98	0.187	1.43	0.131	1.10	1.00	0.148	No
83	1.66	30.11	6.47	23.63	0.98	0.187	1.43	0.131	1.10	1.00	0.148	No
84	1.68	30.49	6.67	23.82	0.98	0.188	1.43	0.132	1.10	1.00	0.149	No
85	1.70	30.88	6.87	24.01	0.98	0.189	1.43	0.132	1.10	1.00	0.149	No
86	1.72	31.26	7.06	24.20	0.98	0.190	1.43	0.133	1.10	1.00	0.150	No
87	1.74	31.65	7.26	24.39	0.98	0.191	1.43	0.133	1.10	1.00	0.151	No
88	1.76	32.03	7.46	24.58	0.98	0.191	1.43	0.134	1.10	1.00	0.152	No
89	1.78	32.42	7.65	24.77	0.98	0.192	1.43	0.135	1.10	1.00	0.153	No
90	1.81	33.00	7.95	25.05	0.98	0.193	1.43	0.135	1.10	1.00	0.154	No
91	1.82	33.19	8.04	25.14	0.98	0.194	1.43	0.136	1.10	1.00	0.154	No
92	1.84	33.57	8.24	25.33	0.98	0.194	1.43	0.136	1.10	1.00	0.155	No
93	1.86	33.96	8.44	25.52	0.98	0.195	1.43	0.137	1.10	1.00	0.156	No
94	1.88	34.34	8.63	25.71	0.98	0.196	1.43	0.137	1.10	1.00	0.156	No
95	1.90	34.72	8.83	25.89	0.98	0.197	1.43	0.138	1.10	1.00	0.157	No
96	1.92	35.10	9.03	26.08	0.98	0.197	1.43	0.138	1.10	1.00	0.158	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
97	1.94	35.49	9.22	26.27	0.98	0.198	1.43	0.139	1.10	1.00	0.158	No
98	1.97	36.06	9.52	26.55	0.98	0.199	1.43	0.139	1.10	1.00	0.160	No
99	1.98	36.25	9.61	26.64	0.98	0.199	1.43	0.139	1.10	1.00	0.160	No
100	2.00	36.63	9.81	26.82	0.98	0.200	1.43	0.140	1.10	1.00	0.161	No
101	2.02	37.01	10.01	27.01	0.98	0.200	1.43	0.140	1.10	1.00	0.162	No
102	2.04	37.39	10.20	27.19	0.98	0.201	1.43	0.141	1.10	1.00	0.163	No
103	2.06	37.77	10.40	27.37	0.98	0.202	1.43	0.141	1.10	1.00	0.164	No
104	2.08	38.15	10.59	27.56	0.98	0.202	1.43	0.142	1.10	1.00	0.165	No
105	2.10	38.53	10.79	27.74	0.98	0.203	1.43	0.142	1.10	1.00	0.166	No
106	2.13	39.09	11.09	28.01	0.98	0.204	1.43	0.143	1.10	1.00	0.167	No
107	2.14	39.28	11.18	28.10	0.98	0.204	1.43	0.143	1.10	1.00	0.167	No
108	2.16	39.66	11.38	28.28	0.98	0.205	1.43	0.143	1.10	1.00	0.167	No
109	2.18	40.03	11.58	28.46	0.98	0.205	1.43	0.144	1.10	1.00	0.168	No
110	2.20	40.41	11.77	28.63	0.98	0.206	1.43	0.144	1.10	1.00	0.169	No
111	2.22	40.78	11.97	28.81	0.98	0.206	1.43	0.144	1.10	1.00	0.169	No
112	2.24	41.15	12.16	28.99	0.97	0.207	1.43	0.145	1.10	1.00	0.170	No
113	2.26	41.53	12.36	29.17	0.97	0.207	1.43	0.145	1.10	1.00	0.171	No
114	2.28	41.90	12.56	29.34	0.97	0.208	1.43	0.146	1.10	1.00	0.171	No
115	2.30	42.27	12.75	29.52	0.97	0.208	1.43	0.146	1.10	1.00	0.172	No
116	2.32	42.64	12.95	29.69	0.97	0.209	1.43	0.146	1.10	1.00	0.172	No
117	2.34	43.01	13.15	29.87	0.97	0.210	1.43	0.147	1.10	1.00	0.173	No
118	2.36	43.38	13.34	30.04	0.97	0.210	1.43	0.147	1.10	1.00	0.173	No
119	2.38	43.75	13.54	30.22	0.97	0.211	1.43	0.147	1.10	1.00	0.174	No
120	2.40	44.12	13.73	30.39	0.97	0.211	1.43	0.148	1.10	1.00	0.174	No
121	2.42	44.49	13.93	30.56	0.97	0.212	1.43	0.148	1.10	1.00	0.175	No
122	2.45	45.04	14.22	30.82	0.97	0.212	1.43	0.149	1.10	1.00	0.175	No
123	2.46	45.22	14.32	30.90	0.97	0.212	1.43	0.149	1.10	1.00	0.176	No
124	2.48	45.59	14.52	31.07	0.97	0.213	1.43	0.149	1.10	1.00	0.176	No
125	2.50	45.95	14.72	31.24	0.97	0.213	1.43	0.149	1.10	1.00	0.177	No
126	2.52	46.31	14.91	31.40	0.97	0.214	1.43	0.150	1.10	1.00	0.178	No
127	2.54	46.68	15.11	31.57	0.97	0.214	1.43	0.150	1.10	1.00	0.178	No
128	2.56	47.04	15.30	31.73	0.97	0.215	1.43	0.150	1.10	1.00	0.179	No
129	2.58	47.40	15.50	31.90	0.97	0.215	1.43	0.151	1.10	1.00	0.180	No
130	2.60	47.76	15.70	32.07	0.97	0.216	1.43	0.151	1.10	1.00	0.180	No
131	2.62	48.12	15.89	32.23	0.97	0.216	1.43	0.151	1.10	1.00	0.181	No
132	2.64	48.48	16.09	32.40	0.97	0.217	1.43	0.152	1.10	1.00	0.181	No
133	2.66	48.84	16.28	32.56	0.97	0.217	1.43	0.152	1.10	1.00	0.182	No
134	2.68	49.20	16.48	32.72	0.97	0.217	1.43	0.152	1.10	1.00	0.182	No
135	2.70	49.56	16.68	32.89	0.97	0.218	1.43	0.152	1.10	1.00	0.183	No
136	2.72	49.92	16.87	33.05	0.97	0.218	1.43	0.153	1.10	1.00	0.184	No
137	2.74	50.28	17.07	33.21	0.97	0.219	1.43	0.153	1.10	1.00	0.184	No
138	2.76	50.64	17.27	33.37	0.97	0.219	1.43	0.153	1.09	1.00	0.185	No
139	2.78	50.99	17.46	33.53	0.97	0.220	1.43	0.154	1.09	1.00	0.185	No
140	2.80	51.35	17.66	33.69	0.97	0.220	1.43	0.154	1.09	1.00	0.186	No
141	2.82	51.70	17.85	33.85	0.96	0.220	1.43	0.154	1.09	1.00	0.187	No
142	2.84	52.05	18.05	34.00	0.96	0.221	1.43	0.154	1.09	1.00	0.187	No
143	2.86	52.41	18.25	34.16	0.96	0.221	1.43	0.155	1.09	1.00	0.188	No
144	2.88	52.76	18.44	34.31	0.96	0.222	1.43	0.155	1.09	1.00	0.188	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
145	2.90	53.11	18.64	34.47	0.96	0.222	1.43	0.155	1.09	1.00	0.188	No
146	2.92	53.46	18.84	34.62	0.96	0.222	1.43	0.156	1.09	1.00	0.189	No
147	2.94	53.81	19.03	34.78	0.96	0.223	1.43	0.156	1.09	1.00	0.189	No
148	2.97	54.33	19.33	35.01	0.96	0.223	1.43	0.156	1.09	1.00	0.190	No
149	2.98	54.51	19.42	35.08	0.96	0.223	1.43	0.156	1.09	1.00	0.190	No
150	3.00	54.85	19.62	35.23	0.96	0.224	1.43	0.157	1.09	1.00	0.191	No
151	3.02	55.20	19.82	35.39	0.96	0.224	1.43	0.157	1.09	1.00	0.191	No
152	3.04	55.55	20.01	35.54	0.96	0.225	1.43	0.157	1.09	1.00	0.191	No
153	3.07	56.08	20.31	35.77	0.96	0.225	1.43	0.158	1.09	1.00	0.192	No
154	3.08	56.25	20.40	35.85	0.96	0.225	1.43	0.158	1.09	1.00	0.192	No
155	3.10	56.60	20.60	36.00	0.96	0.226	1.43	0.158	1.09	1.00	0.192	No
156	3.12	56.95	20.80	36.16	0.96	0.226	1.43	0.158	1.09	1.00	0.193	No
157	3.14	57.30	20.99	36.31	0.96	0.226	1.43	0.158	1.09	1.00	0.193	No
158	3.16	57.65	21.19	36.46	0.96	0.227	1.43	0.159	1.09	1.00	0.193	No
159	3.18	58.00	21.39	36.61	0.96	0.227	1.43	0.159	1.09	1.00	0.194	No
160	3.21	58.52	21.68	36.84	0.96	0.227	1.43	0.159	1.08	1.00	0.194	No
161	3.22	58.70	21.78	36.92	0.96	0.228	1.43	0.159	1.08	1.00	0.195	No
162	3.24	59.05	21.97	37.07	0.96	0.228	1.43	0.160	1.08	1.00	0.195	No
163	3.26	59.39	22.17	37.22	0.96	0.228	1.43	0.160	1.08	1.00	0.195	No
164	3.28	59.74	22.37	37.38	0.96	0.229	1.43	0.160	1.08	1.00	0.196	No
165	3.30	60.09	22.56	37.53	0.96	0.229	1.43	0.160	1.08	1.00	0.196	No
166	3.32	60.44	22.76	37.68	0.96	0.229	1.43	0.160	1.08	1.00	0.197	No
167	3.34	60.79	22.96	37.84	0.96	0.229	1.43	0.161	1.08	1.00	0.197	No
168	3.36	61.14	23.15	37.99	0.95	0.230	1.43	0.161	1.08	1.00	0.197	No
169	3.38	61.49	23.35	38.14	0.95	0.230	1.43	0.161	1.08	1.00	0.197	No
170	3.40	61.84	23.54	38.30	0.95	0.230	1.43	0.161	1.08	1.00	0.198	No
171	3.42	62.19	23.74	38.45	0.95	0.231	1.43	0.161	1.08	1.00	0.198	No
172	3.44	62.54	23.94	38.60	0.95	0.231	1.43	0.162	1.08	1.00	0.198	No
173	3.48	63.23	24.33	38.91	0.95	0.231	1.43	0.162	1.08	1.00	0.199	No
174	3.49	63.41	24.43	38.98	0.95	0.232	1.43	0.162	1.08	1.00	0.199	No
175	3.50	63.58	24.53	39.06	0.95	0.232	1.43	0.162	1.08	1.00	0.200	No
176	3.52	63.93	24.72	39.21	0.95	0.232	1.43	0.162	1.08	1.00	0.200	No
177	3.54	64.27	24.92	39.36	0.95	0.232	1.43	0.163	1.08	1.00	0.201	No
178	3.56	64.62	25.11	39.51	0.95	0.233	1.43	0.163	1.08	1.00	0.201	No
179	3.58	64.96	25.31	39.65	0.95	0.233	1.43	0.163	1.08	1.00	0.202	No
180	3.60	65.31	25.51	39.80	0.95	0.233	1.43	0.163	1.08	1.00	0.202	No
181	3.62	65.65	25.70	39.95	0.95	0.233	1.43	0.163	1.07	1.00	0.202	No
182	3.64	66.00	25.90	40.10	0.95	0.234	1.43	0.164	1.07	1.00	0.203	No
183	3.66	66.34	26.09	40.24	0.95	0.234	1.43	0.164	1.07	1.00	0.203	No
184	3.68	66.68	26.29	40.39	0.95	0.234	1.43	0.164	1.07	1.00	0.203	No
185	3.70	67.03	26.49	40.54	0.95	0.234	1.43	0.164	1.07	1.00	0.203	No
186	3.72	67.37	26.68	40.69	0.95	0.235	1.43	0.164	1.08	1.00	0.202	No
187	3.74	67.71	26.88	40.83	0.95	0.235	1.43	0.164	1.08	1.00	0.202	No
188	3.76	68.06	27.08	40.98	0.95	0.235	1.43	0.165	1.08	1.00	0.202	No
189	3.78	68.40	27.27	41.13	0.95	0.235	1.43	0.165	1.08	1.00	0.202	No
190	3.80	68.74	27.47	41.28	0.95	0.236	1.43	0.165	1.08	1.00	0.203	No
191	3.82	69.09	27.66	41.42	0.95	0.236	1.43	0.165	1.07	1.00	0.203	No
192	3.84	69.43	27.86	41.57	0.95	0.236	1.43	0.165	1.07	1.00	0.204	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
193	3.86	69.78	28.06	41.72	0.95	0.236	1.43	0.165	1.07	1.00	0.204	No
194	3.88	70.13	28.25	41.88	0.94	0.237	1.43	0.166	1.07	1.00	0.204	No
195	3.90	70.48	28.45	42.03	0.94	0.237	1.43	0.166	1.07	1.00	0.204	No
196	3.92	70.83	28.65	42.18	0.94	0.237	1.43	0.166	1.07	1.00	0.204	No
197	3.94	71.18	28.84	42.34	0.94	0.237	1.43	0.166	1.07	1.00	0.204	No
198	3.96	71.53	29.04	42.50	0.94	0.237	1.43	0.166	1.07	1.00	0.204	No
199	3.98	71.89	29.23	42.65	0.94	0.238	1.43	0.166	1.07	1.00	0.204	No
200	4.00	72.24	29.43	42.81	0.94	0.238	1.43	0.166	1.07	1.00	0.204	No
201	4.02	72.59	29.63	42.97	0.94	0.238	1.43	0.167	1.07	1.00	0.205	No
202	4.04	72.95	29.82	43.13	0.94	0.238	1.43	0.167	1.07	1.00	0.206	No
203	4.06	73.30	30.02	43.28	0.94	0.238	1.43	0.167	1.07	1.00	0.206	No
204	4.08	73.66	30.21	43.44	0.94	0.239	1.43	0.167	1.07	1.00	0.207	No
205	4.10	74.01	30.41	43.60	0.94	0.239	1.43	0.167	1.07	1.00	0.207	No
206	4.12	74.36	30.61	43.76	0.94	0.239	1.43	0.167	1.07	1.00	0.208	No
207	4.14	74.72	30.80	43.91	0.94	0.239	1.43	0.167	1.07	1.00	0.208	No
208	4.16	75.07	31.00	44.07	0.94	0.239	1.43	0.167	1.07	1.00	0.208	No
209	4.18	75.41	31.20	44.22	0.94	0.239	1.43	0.168	1.07	1.00	0.209	No
210	4.20	75.76	31.39	44.37	0.94	0.240	1.43	0.168	1.07	1.00	0.209	No
211	4.22	76.10	31.59	44.51	0.94	0.240	1.43	0.168	1.07	1.00	0.209	No
212	4.25	76.61	31.88	44.73	0.94	0.240	1.43	0.168	1.07	1.00	0.209	No
213	4.26	76.78	31.98	44.80	0.94	0.240	1.43	0.168	1.07	1.00	0.210	No
214	4.28	77.12	32.18	44.94	0.94	0.240	1.43	0.168	1.07	1.00	0.210	No
215	4.30	77.45	32.37	45.08	0.94	0.241	1.43	0.168	1.07	1.00	0.210	No
216	4.32	77.79	32.57	45.22	0.94	0.241	1.43	0.169	1.07	1.00	0.210	No
217	4.34	78.12	32.77	45.36	0.94	0.241	1.43	0.169	1.07	1.00	0.210	No
218	4.36	78.46	32.96	45.49	0.94	0.241	1.43	0.169	1.07	1.00	0.210	No
219	4.38	78.79	33.16	45.63	0.93	0.241	1.43	0.169	1.07	1.00	0.210	No
220	4.40	79.12	33.35	45.77	0.93	0.242	1.43	0.169	1.07	1.00	0.210	No
221	4.42	79.46	33.55	45.91	0.93	0.242	1.43	0.169	1.07	1.00	0.211	No
222	4.44	79.79	33.75	46.05	0.93	0.242	1.43	0.169	1.06	1.00	0.211	No
223	4.47	80.30	34.04	46.26	0.93	0.242	1.43	0.170	1.06	1.00	0.211	No
224	4.48	80.47	34.14	46.33	0.93	0.242	1.43	0.170	1.06	1.00	0.211	No
225	4.50	80.81	34.34	46.48	0.93	0.242	1.43	0.170	1.07	1.00	0.211	No
226	4.52	81.15	34.53	46.62	0.93	0.243	1.43	0.170	1.07	1.00	0.211	No
227	4.54	81.49	34.73	46.77	0.93	0.243	1.43	0.170	1.07	1.00	0.211	No
228	4.56	81.84	34.92	46.91	0.93	0.243	1.43	0.170	1.07	1.00	0.211	No
229	4.59	82.35	35.22	47.13	0.93	0.243	1.43	0.170	1.06	1.00	0.211	No
230	4.60	82.52	35.32	47.20	0.93	0.243	1.43	0.170	1.07	1.00	0.211	No
231	4.62	82.86	35.51	47.35	0.93	0.243	1.43	0.170	1.07	1.00	0.210	No
232	4.64	83.21	35.71	47.50	0.93	0.243	1.43	0.170	1.07	1.00	0.211	No
233	4.66	83.55	35.90	47.65	0.93	0.244	1.43	0.171	1.07	1.00	0.211	No
234	4.68	83.90	36.10	47.80	0.93	0.244	1.43	0.171	1.07	1.00	0.210	No
235	4.70	84.25	36.30	47.96	0.93	0.244	1.43	0.171	1.07	1.00	0.210	No
236	4.72	84.60	36.49	48.11	0.93	0.244	1.43	0.171	1.07	1.00	0.210	No
237	4.74	84.96	36.69	48.27	0.93	0.244	1.43	0.171	1.07	1.00	0.210	No
238	4.76	85.32	36.89	48.43	0.93	0.244	1.43	0.171	1.07	1.00	0.209	No
239	4.78	85.68	37.08	48.59	0.93	0.244	1.43	0.171	1.07	1.00	0.209	No
240	4.80	86.04	37.28	48.76	0.93	0.244	1.43	0.171	1.07	1.00	0.210	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
241	4.82	86.40	37.47	48.93	0.93	0.244	1.43	0.171	1.07	1.00	0.210	No
242	4.84	86.76	37.67	49.09	0.93	0.245	1.43	0.171	1.06	1.00	0.210	No
243	4.86	87.13	37.87	49.26	0.93	0.245	1.43	0.171	1.06	1.00	0.211	No
244	4.88	87.49	38.06	49.43	0.92	0.245	1.43	0.171	1.06	1.00	0.211	No
245	4.90	87.86	38.26	49.60	0.92	0.245	1.43	0.171	1.06	1.00	0.211	No
246	4.92	88.22	38.46	49.77	0.92	0.245	1.43	0.171	1.06	1.00	0.211	No
247	4.94	88.59	38.65	49.93	0.92	0.245	1.43	0.171	1.06	1.00	0.211	No
248	4.97	89.13	38.95	50.18	0.92	0.245	1.43	0.172	1.06	1.00	0.211	No
249	4.98	89.31	39.04	50.27	0.92	0.245	1.43	0.172	1.06	1.00	0.212	No
250	5.00	89.67	39.24	50.43	0.92	0.245	1.43	0.172	1.06	1.00	0.212	No
251	5.02	90.03	39.44	50.60	0.92	0.245	1.43	0.172	1.06	1.00	0.212	No
252	5.04	90.40	39.63	50.76	0.92	0.245	1.43	0.172	1.06	1.00	0.212	No
253	5.07	90.94	39.93	51.01	0.92	0.245	1.43	0.172	1.06	1.00	0.213	No
254	5.08	91.12	40.02	51.10	0.92	0.245	1.43	0.172	1.06	1.00	0.213	No
255	5.10	91.48	40.22	51.26	0.92	0.245	1.43	0.172	1.06	1.00	0.213	No
256	5.12	91.85	40.42	51.43	0.92	0.246	1.43	0.172	1.06	1.00	0.213	No
257	5.14	92.21	40.61	51.60	0.92	0.246	1.43	0.172	1.06	1.00	0.214	No
258	5.16	92.57	40.81	51.76	0.92	0.246	1.43	0.172	1.06	1.00	0.214	No
259	5.18	92.93	41.01	51.93	0.92	0.246	1.43	0.172	1.06	1.00	0.214	No
260	5.21	93.47	41.30	52.17	0.92	0.246	1.43	0.172	1.06	1.00	0.215	No
261	5.22	93.65	41.40	52.25	0.92	0.246	1.43	0.172	1.06	1.00	0.215	No
262	5.24	94.01	41.59	52.41	0.92	0.246	1.43	0.172	1.06	1.00	0.215	No
263	5.26	94.37	41.79	52.58	0.92	0.246	1.43	0.172	1.06	1.00	0.216	No
264	5.28	94.72	41.99	52.74	0.92	0.246	1.43	0.172	1.06	1.00	0.216	No
265	5.30	95.08	42.18	52.89	0.92	0.246	1.43	0.172	1.05	1.00	0.216	No
266	5.32	95.43	42.38	53.05	0.92	0.246	1.43	0.172	1.05	1.00	0.216	No
267	5.34	95.78	42.58	53.21	0.92	0.246	1.43	0.172	1.05	1.00	0.216	No
268	5.36	96.13	42.77	53.36	0.91	0.246	1.43	0.172	1.05	1.00	0.216	No
269	5.38	96.48	42.97	53.51	0.91	0.246	1.43	0.172	1.05	1.00	0.216	No
270	5.40	96.83	43.16	53.67	0.91	0.246	1.43	0.173	1.05	1.00	0.216	No
271	5.42	97.18	43.36	53.82	0.91	0.247	1.43	0.173	1.05	1.00	0.216	No
272	5.44	97.53	43.56	53.98	0.91	0.247	1.43	0.173	1.05	1.00	0.216	No
273	5.46	97.88	43.75	54.13	0.91	0.247	1.43	0.173	1.05	1.00	0.216	No
274	5.52	98.94	44.34	54.60	0.91	0.247	1.43	0.173	1.05	1.00	0.216	No
275	5.52	98.94	44.34	54.60	0.91	0.247	1.43	0.173	1.05	1.00	0.216	No
276	5.52	98.94	44.34	54.60	0.91	0.247	1.43	0.173	1.05	1.00	0.216	No
277	5.54	99.29	44.54	54.75	0.91	0.247	1.43	0.173	1.05	1.00	0.216	No
278	5.56	99.65	44.73	54.91	0.91	0.247	1.43	0.173	1.05	1.00	0.216	No
279	5.58	100.00	44.93	55.07	0.91	0.247	1.43	0.173	1.05	1.00	0.216	No
280	5.60	100.36	45.13	55.23	0.91	0.247	1.43	0.173	1.05	1.00	0.216	No
281	5.62	100.71	45.32	55.39	0.91	0.247	1.43	0.173	1.05	1.00	0.216	No
282	5.64	101.07	45.52	55.55	0.91	0.247	1.43	0.173	1.05	1.00	0.216	No
283	5.66	101.43	45.71	55.71	0.91	0.247	1.43	0.173	1.05	1.00	0.216	No
284	5.68	101.79	45.91	55.88	0.91	0.247	1.43	0.173	1.05	1.00	0.216	No
285	5.70	102.15	46.11	56.04	0.91	0.247	1.43	0.173	1.05	1.00	0.216	No
286	5.72	102.51	46.30	56.21	0.91	0.247	1.43	0.173	1.05	1.00	0.216	No
287	5.74	102.87	46.50	56.37	0.91	0.247	1.43	0.173	1.05	1.00	0.216	No
288	5.76	103.23	46.70	56.54	0.91	0.247	1.43	0.173	1.05	1.00	0.217	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
289	5.78	103.60	46.89	56.71	0.91	0.247	1.43	0.173	1.05	1.00	0.217	No
290	5.80	103.96	47.09	56.87	0.91	0.247	1.43	0.173	1.05	1.00	0.217	No
291	5.82	104.32	47.28	57.04	0.90	0.247	1.43	0.173	1.05	1.00	0.217	No
292	5.84	104.69	47.48	57.21	0.90	0.247	1.43	0.173	1.05	1.00	0.218	No
293	5.86	105.05	47.68	57.37	0.90	0.247	1.43	0.173	1.05	1.00	0.218	No
294	5.88	105.41	47.87	57.54	0.90	0.247	1.43	0.173	1.05	1.00	0.218	No
295	5.90	105.77	48.07	57.70	0.90	0.247	1.43	0.173	1.05	1.00	0.218	No
296	5.92	106.13	48.27	57.87	0.90	0.247	1.43	0.173	1.05	1.00	0.218	No
297	5.94	106.49	48.46	58.03	0.90	0.247	1.43	0.173	1.05	1.00	0.218	No
298	5.96	106.85	48.66	58.20	0.90	0.247	1.43	0.173	1.05	1.00	0.218	No
299	5.98	107.21	48.85	58.36	0.90	0.248	1.43	0.173	1.05	1.00	0.219	No
300	6.01	107.75	49.15	58.60	0.90	0.248	1.43	0.173	1.05	1.00	0.219	No
301	6.02	107.93	49.25	58.68	0.90	0.248	1.43	0.173	1.05	1.00	0.219	No
302	6.04	108.29	49.44	58.84	0.90	0.248	1.43	0.173	1.05	1.00	0.219	No
303	6.07	108.82	49.74	59.09	0.90	0.248	1.43	0.173	1.05	1.00	0.219	No
304	6.08	109.00	49.83	59.17	0.90	0.248	1.43	0.173	1.05	1.00	0.219	No
305	6.10	109.36	50.03	59.33	0.90	0.248	1.43	0.173	1.05	1.00	0.219	No
306	6.12	109.72	50.23	59.49	0.90	0.248	1.43	0.173	1.04	1.00	0.220	No
307	6.14	110.07	50.42	59.65	0.90	0.248	1.43	0.173	1.04	1.00	0.220	No
308	6.16	110.43	50.62	59.81	0.90	0.248	1.43	0.173	1.04	1.00	0.220	No
309	6.18	110.79	50.82	59.97	0.90	0.248	1.43	0.173	1.04	1.00	0.220	No
310	6.20	111.15	51.01	60.13	0.90	0.248	1.43	0.173	1.04	1.00	0.220	No
311	6.22	111.50	51.21	60.29	0.90	0.248	1.43	0.173	1.04	1.00	0.221	No
312	6.24	111.85	51.40	60.45	0.90	0.248	1.43	0.173	1.04	1.00	0.221	No
313	6.26	112.20	51.60	60.60	0.89	0.248	1.43	0.173	1.04	1.00	0.221	No
314	6.28	112.55	51.80	60.75	0.89	0.248	1.43	0.173	1.04	1.00	0.221	No
315	6.30	112.90	51.99	60.90	0.89	0.248	1.43	0.173	1.04	1.00	0.221	No
316	6.32	113.24	52.19	61.05	0.89	0.248	1.43	0.173	1.04	1.00	0.221	No
317	6.34	113.59	52.39	61.20	0.89	0.248	1.43	0.173	1.04	1.00	0.221	No
318	6.36	113.93	52.58	61.35	0.89	0.248	1.43	0.173	1.04	1.00	0.221	No
319	6.38	114.28	52.78	61.50	0.89	0.248	1.43	0.174	1.04	1.00	0.221	No
320	6.40	114.62	52.97	61.64	0.89	0.248	1.43	0.174	1.04	1.00	0.221	No
321	6.42	114.96	53.17	61.79	0.89	0.248	1.43	0.174	1.04	1.00	0.221	No
322	6.44	115.30	53.37	61.93	0.89	0.248	1.43	0.174	1.04	1.00	0.221	No
323	6.46	115.64	53.56	62.08	0.89	0.248	1.43	0.174	1.04	1.00	0.221	No
324	6.48	115.98	53.76	62.22	0.89	0.248	1.43	0.174	1.04	1.00	0.221	No
325	6.50	116.32	53.96	62.36	0.89	0.248	1.43	0.174	1.04	1.00	0.221	No
326	6.52	116.66	54.15	62.51	0.89	0.248	1.43	0.174	1.04	1.00	0.221	No
327	6.54	117.00	54.35	62.65	0.89	0.248	1.43	0.174	1.04	1.00	0.222	No
328	6.56	117.34	54.54	62.80	0.89	0.248	1.43	0.174	1.04	1.00	0.222	No
329	6.58	117.69	54.74	62.95	0.89	0.248	1.43	0.174	1.04	1.00	0.222	No
330	6.60	118.03	54.94	63.10	0.89	0.248	1.43	0.174	1.04	1.00	0.222	No
331	6.62	118.38	55.13	63.25	0.89	0.248	1.43	0.174	1.04	1.00	0.222	No
332	6.64	118.73	55.33	63.40	0.89	0.248	1.43	0.174	1.04	1.00	0.222	No
333	6.66	119.07	55.52	63.55	0.89	0.248	1.43	0.174	1.04	1.00	0.222	No
334	6.69	119.59	55.82	63.77	0.89	0.248	1.43	0.174	1.04	1.00	0.222	No
335	6.70	119.76	55.92	63.84	0.89	0.248	1.43	0.174	1.04	1.00	0.222	No
336	6.72	120.10	56.11	63.99	0.88	0.248	1.43	0.174	1.04	1.00	0.222	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
337	6.74	120.44	56.31	64.13	0.88	0.248	1.43	0.174	1.04	1.00	0.222	No
338	6.76	120.78	56.51	64.28	0.88	0.248	1.43	0.174	1.04	1.00	0.222	No
339	6.78	121.12	56.70	64.42	0.88	0.248	1.43	0.174	1.04	1.00	0.222	No
340	6.80	121.47	56.90	64.57	0.88	0.248	1.43	0.174	1.04	1.00	0.223	No
341	6.82	121.81	57.09	64.72	0.88	0.248	1.43	0.174	1.04	1.00	0.223	No
342	6.84	122.15	57.29	64.86	0.88	0.248	1.43	0.174	1.04	1.00	0.223	No
343	6.86	122.49	57.49	65.01	0.88	0.248	1.43	0.174	1.04	1.00	0.223	No
344	6.88	122.83	57.68	65.15	0.88	0.248	1.43	0.174	1.04	1.00	0.223	No
345	6.90	123.17	57.88	65.30	0.88	0.248	1.43	0.174	1.04	1.00	0.224	No
346	6.92	123.52	58.08	65.44	0.88	0.248	1.43	0.174	1.04	1.00	0.224	No
347	6.94	123.86	58.27	65.58	0.88	0.248	1.43	0.174	1.04	1.00	0.224	No
348	6.96	124.20	58.47	65.73	0.88	0.248	1.43	0.174	1.03	1.00	0.223	No
349	6.98	124.54	58.66	65.87	0.88	0.248	1.43	0.174	1.03	1.00	0.224	No
350	7.00	124.87	58.86	66.01	0.88	0.248	1.43	0.174	1.03	1.00	0.224	No
351	7.02	125.20	59.06	66.15	0.88	0.248	1.43	0.174	1.03	1.00	0.224	No
352	7.04	125.54	59.25	66.28	0.88	0.248	1.43	0.174	1.03	1.00	0.224	No
353	7.06	125.86	59.45	66.41	0.88	0.248	1.43	0.174	1.03	1.00	0.223	No
354	7.08	126.19	59.64	66.55	0.88	0.248	1.43	0.174	1.03	1.00	0.223	No
355	7.10	126.52	59.84	66.68	0.88	0.249	1.43	0.174	1.03	1.00	0.223	No
356	7.12	126.86	60.04	66.82	0.88	0.249	1.43	0.174	1.03	1.00	0.223	No
357	7.14	127.19	60.23	66.96	0.88	0.249	1.43	0.174	1.03	1.00	0.222	No
358	7.16	127.54	60.43	67.11	0.87	0.249	1.43	0.174	1.03	1.00	0.222	No
359	7.18	127.88	60.63	67.26	0.87	0.249	1.43	0.174	1.03	1.00	0.222	No
360	7.20	128.23	60.82	67.41	0.87	0.248	1.43	0.174	1.04	1.00	0.221	No
361	7.22	128.59	61.02	67.57	0.87	0.248	1.43	0.174	1.04	1.00	0.221	No
362	7.24	128.95	61.21	67.73	0.87	0.248	1.43	0.174	1.03	1.00	0.221	No
363	7.26	129.30	61.41	67.89	0.87	0.248	1.43	0.174	1.03	1.00	0.221	No
364	7.28	129.67	61.61	68.06	0.87	0.248	1.43	0.174	1.03	1.00	0.221	No
365	7.30	130.03	61.80	68.23	0.87	0.248	1.43	0.174	1.03	1.00	0.221	No
366	7.32	130.39	62.00	68.39	0.87	0.248	1.43	0.174	1.03	1.00	0.221	No
367	7.34	130.75	62.20	68.56	0.87	0.248	1.43	0.174	1.03	1.00	0.222	No
368	7.36	131.11	62.39	68.72	0.87	0.248	1.43	0.174	1.03	1.00	0.222	No
369	7.38	131.47	62.59	68.89	0.87	0.248	1.43	0.174	1.03	1.00	0.222	No
370	7.40	131.83	62.78	69.05	0.87	0.248	1.43	0.174	1.03	1.00	0.222	No
371	7.42	132.19	62.98	69.21	0.87	0.248	1.43	0.174	1.03	1.00	0.222	No
372	7.44	132.55	63.18	69.37	0.87	0.248	1.43	0.174	1.03	1.00	0.221	No
373	7.46	132.91	63.37	69.54	0.87	0.248	1.43	0.174	1.03	1.00	0.221	No
374	7.48	133.27	63.57	69.70	0.87	0.248	1.43	0.174	1.03	1.00	0.221	No
375	7.50	133.63	63.77	69.87	0.87	0.248	1.43	0.174	1.03	1.00	0.221	No
376	7.52	134.00	63.96	70.03	0.87	0.248	1.43	0.173	1.03	1.00	0.220	No
377	7.54	134.36	64.16	70.20	0.87	0.248	1.43	0.173	1.03	1.00	0.220	No
378	7.56	134.73	64.35	70.37	0.87	0.248	1.43	0.173	1.03	1.00	0.220	No
379	7.58	135.09	64.55	70.54	0.87	0.248	1.43	0.173	1.03	1.00	0.221	No
380	7.60	135.46	64.75	70.71	0.86	0.248	1.43	0.173	1.03	1.00	0.220	No
381	7.62	135.83	64.94	70.89	0.86	0.248	1.43	0.173	1.03	1.00	0.220	No
382	7.64	136.20	65.14	71.06	0.86	0.247	1.43	0.173	1.03	1.00	0.220	No
383	7.66	136.57	65.33	71.23	0.86	0.247	1.43	0.173	1.03	1.00	0.220	No
384	7.68	136.93	65.53	71.40	0.86	0.247	1.43	0.173	1.03	1.00	0.221	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
385	7.70	137.30	65.73	71.58	0.86	0.247	1.43	0.173	1.03	1.00	0.222	No
386	7.72	137.67	65.92	71.75	0.86	0.247	1.43	0.173	1.03	1.00	0.222	No
387	7.74	138.04	66.12	71.92	0.86	0.247	1.43	0.173	1.03	1.00	0.222	No
388	7.76	138.40	66.32	72.09	0.86	0.247	1.43	0.173	1.03	1.00	0.223	No
389	7.78	138.77	66.51	72.26	0.86	0.247	1.43	0.173	1.03	1.00	0.223	No
390	7.80	139.13	66.71	72.43	0.86	0.247	1.43	0.173	1.03	1.00	0.223	No
391	7.82	139.50	66.90	72.59	0.86	0.247	1.43	0.173	1.03	1.00	0.222	No
392	7.84	139.86	67.10	72.76	0.86	0.247	1.43	0.173	1.03	1.00	0.222	No
393	7.86	140.23	67.30	72.93	0.86	0.247	1.43	0.173	1.03	1.00	0.221	No
394	7.88	140.59	67.49	73.10	0.86	0.247	1.43	0.173	1.03	1.00	0.220	No
395	7.90	140.95	67.69	73.26	0.86	0.247	1.43	0.173	1.03	1.00	0.220	No
396	7.92	141.32	67.89	73.43	0.86	0.247	1.43	0.173	1.03	1.00	0.220	No
397	7.94	141.68	68.08	73.60	0.86	0.247	1.43	0.173	1.03	1.00	0.220	No
398	7.96	142.05	68.28	73.77	0.86	0.246	1.43	0.173	1.03	1.00	0.220	No
399	7.98	142.42	68.47	73.94	0.86	0.246	1.43	0.172	1.03	1.00	0.220	No
400	8.00	142.79	68.67	74.12	0.86	0.246	1.43	0.172	1.03	1.00	0.220	No
401	8.02	143.16	68.87	74.29	0.85	0.246	1.43	0.172	1.03	1.00	0.220	No
402	8.04	143.53	69.06	74.47	0.85	0.246	1.43	0.172	1.03	1.00	0.220	No
403	8.06	143.90	69.26	74.65	0.85	0.246	1.43	0.172	1.03	1.00	0.220	No
404	8.08	144.28	69.45	74.82	0.85	0.246	1.43	0.172	1.03	1.00	0.220	No
405	8.10	144.65	69.65	75.00	0.85	0.246	1.43	0.172	1.03	1.00	0.219	No
406	8.12	145.03	69.85	75.18	0.85	0.246	1.43	0.172	1.03	1.00	0.219	No
407	8.15	145.59	70.14	75.45	0.85	0.246	1.43	0.172	1.03	1.00	0.219	No
408	8.16	145.78	70.24	75.54	0.85	0.246	1.43	0.172	1.03	1.00	0.219	No
409	8.18	146.15	70.44	75.72	0.85	0.246	1.43	0.172	1.03	1.00	0.218	No
410	8.20	146.53	70.63	75.89	0.85	0.245	1.43	0.172	1.03	1.00	0.218	No
411	8.22	146.90	70.83	76.07	0.85	0.245	1.43	0.172	1.03	1.00	0.218	No
412	8.24	147.28	71.02	76.25	0.85	0.245	1.43	0.172	1.03	1.00	0.218	No
413	8.26	147.65	71.22	76.43	0.85	0.245	1.43	0.172	1.03	1.00	0.219	No
414	8.28	148.02	71.42	76.61	0.85	0.245	1.43	0.172	1.03	1.00	0.219	No
415	8.30	148.40	71.61	76.78	0.85	0.245	1.43	0.172	1.02	1.00	0.219	No
416	8.32	148.77	71.81	76.96	0.85	0.245	1.43	0.171	1.02	1.00	0.219	No
417	8.34	149.15	72.01	77.14	0.85	0.245	1.43	0.171	1.02	1.00	0.219	No
418	8.36	149.52	72.20	77.32	0.85	0.245	1.43	0.171	1.02	1.00	0.219	No
419	8.38	149.89	72.40	77.50	0.85	0.245	1.43	0.171	1.02	1.00	0.219	No
420	8.40	150.27	72.59	77.67	0.85	0.245	1.43	0.171	1.02	1.00	0.220	No
421	8.42	150.64	72.79	77.85	0.85	0.245	1.43	0.171	1.02	1.00	0.220	No
422	8.44	151.01	72.99	78.03	0.84	0.244	1.43	0.171	1.02	1.00	0.221	No
423	8.46	151.38	73.18	78.20	0.84	0.244	1.43	0.171	1.02	1.00	0.221	No
424	8.48	151.76	73.38	78.38	0.84	0.244	1.43	0.171	1.02	1.00	0.221	No
425	8.50	152.13	73.58	78.55	0.84	0.244	1.43	0.171	1.02	1.00	0.222	No
426	8.52	152.50	73.77	78.72	0.84	0.244	1.43	0.171	1.02	1.00	0.222	No
427	8.54	152.86	73.97	78.89	0.84	0.244	1.43	0.171	1.02	1.00	0.222	No
428	8.56	153.23	74.16	79.06	0.84	0.244	1.43	0.171	1.02	1.00	0.222	No
429	8.58	153.59	74.36	79.23	0.84	0.244	1.43	0.171	1.02	1.00	0.222	No
430	8.60	153.95	74.56	79.39	0.84	0.244	1.43	0.171	1.02	1.00	0.222	No
431	8.62	154.30	74.75	79.55	0.84	0.244	1.43	0.171	1.02	1.00	0.222	No
432	8.64	154.66	74.95	79.71	0.84	0.244	1.43	0.171	1.02	1.00	0.222	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
433	8.66	155.01	75.14	79.86	0.84	0.244	1.43	0.171	1.02	1.00	0.222	No
434	8.68	155.36	75.34	80.02	0.84	0.244	1.43	0.171	1.02	1.00	0.222	No
435	8.70	155.71	75.54	80.17	0.84	0.244	1.43	0.170	1.02	1.00	0.222	No
436	8.72	156.06	75.73	80.33	0.84	0.243	1.43	0.170	1.02	1.00	0.221	No
437	8.74	156.41	75.93	80.48	0.84	0.243	1.43	0.170	1.02	1.00	0.220	No
438	8.76	156.76	76.13	80.63	0.84	0.243	1.43	0.170	1.02	1.00	0.220	No
439	8.78	157.11	76.32	80.79	0.84	0.243	1.43	0.170	1.02	1.00	0.220	No
440	8.80	157.46	76.52	80.95	0.84	0.243	1.43	0.170	1.02	1.00	0.219	No
441	8.82	157.82	76.71	81.10	0.84	0.243	1.43	0.170	1.02	1.00	0.219	No
442	8.84	158.17	76.91	81.26	0.84	0.243	1.43	0.170	1.02	1.00	0.219	No
443	8.86	158.53	77.11	81.43	0.83	0.243	1.43	0.170	1.02	1.00	0.219	No
444	8.88	158.89	77.30	81.59	0.83	0.243	1.43	0.170	1.02	1.00	0.218	No
445	8.90	159.26	77.50	81.76	0.83	0.243	1.43	0.170	1.02	1.00	0.218	No
446	8.93	159.81	77.79	82.01	0.83	0.243	1.43	0.170	1.02	1.00	0.218	No
447	8.94	159.99	77.89	82.10	0.83	0.243	1.43	0.170	1.02	1.00	0.218	No
448	8.96	160.36	78.09	82.27	0.83	0.243	1.43	0.170	1.02	1.00	0.218	No
449	8.98	160.73	78.28	82.45	0.83	0.243	1.43	0.170	1.02	1.00	0.218	No
450	9.00	161.11	78.48	82.63	0.83	0.242	1.43	0.170	1.02	1.00	0.218	No
451	9.02	161.48	78.68	82.80	0.83	0.242	1.43	0.170	1.02	1.00	0.218	No
452	9.04	161.85	78.87	82.98	0.83	0.242	1.43	0.170	1.02	1.00	0.218	No
453	9.06	162.23	79.07	83.16	0.83	0.242	1.43	0.169	1.02	1.00	0.217	No
454	9.08	162.60	79.26	83.33	0.83	0.242	1.43	0.169	1.02	1.00	0.217	No
455	9.10	162.97	79.46	83.51	0.83	0.242	1.43	0.169	1.02	1.00	0.217	No
456	9.12	163.34	79.66	83.69	0.83	0.242	1.43	0.169	1.02	1.00	0.217	No
457	9.14	163.72	79.85	83.86	0.83	0.242	1.43	0.169	1.02	1.00	0.217	No
458	9.16	164.09	80.05	84.04	0.83	0.242	1.43	0.169	1.02	1.00	0.217	No
459	9.18	164.46	80.25	84.22	0.83	0.242	1.43	0.169	1.02	1.00	0.217	No
460	9.20	164.83	80.44	84.39	0.83	0.241	1.43	0.169	1.02	1.00	0.217	No
461	9.22	165.21	80.64	84.57	0.83	0.241	1.43	0.169	1.02	1.00	0.217	No
462	9.24	165.58	80.83	84.75	0.83	0.241	1.43	0.169	1.02	1.00	0.217	No
463	9.26	165.96	81.03	84.93	0.83	0.241	1.43	0.169	1.02	1.00	0.217	No
464	9.28	166.33	81.23	85.10	0.83	0.241	1.43	0.169	1.02	1.00	0.217	No
465	9.30	166.71	81.42	85.28	0.82	0.241	1.43	0.169	1.02	1.00	0.217	No
466	9.32	167.08	81.62	85.46	0.82	0.241	1.43	0.169	1.02	1.00	0.216	No
467	9.34	167.45	81.82	85.64	0.82	0.241	1.43	0.169	1.02	1.00	0.216	No
468	9.36	167.83	82.01	85.82	0.82	0.241	1.43	0.168	1.02	1.00	0.216	No
469	9.38	168.20	82.21	86.00	0.82	0.241	1.43	0.168	1.02	1.00	0.216	No
470	9.40	168.58	82.40	86.17	0.82	0.240	1.43	0.168	1.02	1.00	0.215	No
471	9.42	168.95	82.60	86.35	0.82	0.240	1.43	0.168	1.02	1.00	0.215	No
472	9.44	169.33	82.80	86.53	0.82	0.240	1.43	0.168	1.01	1.00	0.215	No
473	9.46	169.70	82.99	86.71	0.82	0.240	1.43	0.168	1.01	1.00	0.215	No
474	9.48	170.08	83.19	86.89	0.82	0.240	1.43	0.168	1.01	1.00	0.216	No
475	9.50	170.46	83.39	87.07	0.82	0.240	1.43	0.168	1.01	1.00	0.216	No
476	9.52	170.84	83.58	87.25	0.82	0.240	1.43	0.168	1.01	1.00	0.217	No
477	9.54	171.21	83.78	87.44	0.82	0.240	1.43	0.168	1.01	1.00	0.217	No
478	9.56	171.59	83.97	87.62	0.82	0.240	1.43	0.168	1.01	1.00	0.217	No
479	9.58	171.97	84.17	87.80	0.82	0.239	1.43	0.168	1.01	1.00	0.217	No
480	9.60	172.35	84.37	87.98	0.82	0.239	1.43	0.168	1.01	1.00	0.216	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
481	9.62	172.72	84.56	88.16	0.82	0.239	1.43	0.167	1.01	1.00	0.216	No
482	9.64	173.10	84.76	88.34	0.82	0.239	1.43	0.167	1.01	1.00	0.216	No
483	9.66	173.47	84.95	88.52	0.82	0.239	1.43	0.167	1.01	1.00	0.216	No
484	9.68	173.84	85.15	88.69	0.82	0.239	1.43	0.167	1.01	1.00	0.216	No
485	9.70	174.22	85.35	88.87	0.81	0.239	1.43	0.167	1.01	1.00	0.216	No
486	9.72	174.59	85.54	89.04	0.81	0.239	1.43	0.167	1.01	1.00	0.217	No
487	9.74	174.96	85.74	89.22	0.81	0.239	1.43	0.167	1.01	1.00	0.217	No
488	9.76	175.33	85.94	89.39	0.81	0.239	1.43	0.167	1.01	1.00	0.218	No
489	9.78	175.70	86.13	89.56	0.81	0.238	1.43	0.167	1.01	1.00	0.218	No
490	9.80	176.06	86.33	89.74	0.81	0.238	1.43	0.167	1.01	1.00	0.219	No
491	9.82	176.43	86.52	89.91	0.81	0.238	1.43	0.167	1.01	1.00	0.219	No
492	9.84	176.80	86.72	90.08	0.81	0.238	1.43	0.167	1.01	1.00	0.219	No
493	9.86	177.16	86.92	90.24	0.81	0.238	1.43	0.167	1.01	1.00	0.219	No
494	9.88	177.51	87.11	90.40	0.81	0.238	1.43	0.167	1.01	1.00	0.219	No
495	9.90	177.87	87.31	90.56	0.81	0.238	1.43	0.167	1.01	1.00	0.219	No
496	9.92	178.22	87.51	90.71	0.81	0.238	1.43	0.166	1.01	1.00	0.219	No
497	9.95	178.74	87.80	90.94	0.81	0.238	1.43	0.166	1.01	1.00	0.219	No
498	9.96	178.91	87.90	91.01	0.81	0.238	1.43	0.166	1.01	1.00	0.219	No
499	9.98	179.25	88.09	91.15	0.81	0.238	1.43	0.166	1.01	1.00	0.219	No
500	10.00	179.58	88.29	91.29	0.81	0.238	1.43	0.166	1.01	1.00	0.219	No
501	10.02	179.91	88.49	91.43	0.81	0.238	1.43	0.166	1.01	1.00	0.219	No
502	10.04	180.25	88.68	91.57	0.81	0.237	1.43	0.166	1.01	1.00	0.219	No
503	10.06	180.58	88.88	91.70	0.81	0.237	1.43	0.166	1.01	1.00	0.219	No
504	10.08	180.91	89.07	91.84	0.81	0.237	1.43	0.166	1.01	1.00	0.219	No
505	10.10	181.25	89.27	91.98	0.81	0.237	1.43	0.166	1.01	1.00	0.219	No
506	10.12	181.58	89.47	92.11	0.80	0.237	1.43	0.166	1.01	1.00	0.219	No
507	10.14	181.91	89.66	92.25	0.80	0.237	1.43	0.166	1.01	1.00	0.219	No
508	10.16	182.24	89.86	92.38	0.80	0.237	1.43	0.166	1.01	1.00	0.219	No
509	10.18	182.57	90.06	92.52	0.80	0.237	1.43	0.166	1.01	1.00	0.219	No
510	10.20	182.90	90.25	92.65	0.80	0.237	1.43	0.166	1.01	1.00	0.219	No
511	10.22	183.24	90.45	92.79	0.80	0.237	1.43	0.166	1.01	1.00	0.219	No
512	10.24	183.57	90.64	92.93	0.80	0.237	1.43	0.166	1.01	1.00	0.219	No
513	10.26	183.90	90.84	93.06	0.80	0.237	1.43	0.166	1.01	1.00	0.219	No
514	10.28	184.24	91.04	93.20	0.80	0.237	1.43	0.166	1.01	1.00	0.218	No
515	10.30	184.58	91.23	93.34	0.80	0.237	1.43	0.166	1.01	1.00	0.218	No
516	10.32	184.91	91.43	93.48	0.80	0.237	1.43	0.166	1.01	1.00	0.218	No
517	10.34	185.25	91.63	93.63	0.80	0.237	1.43	0.166	1.01	1.00	0.217	No
518	10.36	185.60	91.82	93.78	0.80	0.236	1.43	0.166	1.01	1.00	0.217	No
519	10.38	185.95	92.02	93.93	0.80	0.236	1.43	0.165	1.01	1.00	0.217	No
520	10.40	186.30	92.21	94.08	0.80	0.236	1.43	0.165	1.01	1.00	0.217	No
521	10.42	186.65	92.41	94.24	0.80	0.236	1.43	0.165	1.01	1.00	0.217	No
522	10.44	187.01	92.61	94.40	0.80	0.236	1.43	0.165	1.01	1.00	0.217	No
523	10.46	187.36	92.80	94.56	0.80	0.236	1.43	0.165	1.01	1.00	0.217	No
524	10.48	187.72	93.00	94.72	0.80	0.236	1.43	0.165	1.01	1.00	0.217	No
525	10.50	188.08	93.19	94.89	0.80	0.236	1.43	0.165	1.01	1.00	0.217	No
526	10.52	188.44	93.39	95.05	0.80	0.236	1.43	0.165	1.01	1.00	0.217	No
527	10.54	188.80	93.59	95.21	0.79	0.236	1.43	0.165	1.01	1.00	0.217	No
528	10.56	189.15	93.78	95.37	0.79	0.236	1.43	0.165	1.01	1.00	0.217	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
529	10.58	189.51	93.98	95.53	0.79	0.235	1.43	0.165	1.00	1.00	0.217	No
530	10.60	189.87	94.18	95.69	0.79	0.235	1.43	0.165	1.00	1.00	0.217	No
531	10.62	190.22	94.37	95.85	0.79	0.235	1.43	0.165	1.00	1.00	0.217	No
532	10.64	190.58	94.57	96.01	0.79	0.235	1.43	0.165	1.00	1.00	0.217	No
533	10.66	190.94	94.76	96.17	0.79	0.235	1.43	0.165	1.00	1.00	0.217	No
534	10.68	191.29	94.96	96.33	0.79	0.235	1.43	0.164	1.00	1.00	0.216	No
535	10.70	191.65	95.16	96.49	0.79	0.235	1.43	0.164	1.00	1.00	0.216	No
536	10.72	192.01	95.35	96.65	0.79	0.235	1.43	0.164	1.00	1.00	0.216	No
537	10.74	192.37	95.55	96.82	0.79	0.235	1.43	0.164	1.00	1.00	0.215	No
538	10.76	192.73	95.75	96.98	0.79	0.235	1.43	0.164	1.00	1.00	0.215	No
539	10.78	193.09	95.94	97.15	0.79	0.234	1.43	0.164	1.00	1.00	0.215	No
540	10.80	193.45	96.14	97.31	0.79	0.234	1.43	0.164	1.00	1.00	0.215	No
541	10.82	193.82	96.33	97.48	0.79	0.234	1.43	0.164	1.00	1.00	0.215	No
542	10.84	194.18	96.53	97.65	0.79	0.234	1.43	0.164	1.00	1.00	0.215	No
543	10.86	194.55	96.73	97.82	0.79	0.234	1.43	0.164	1.00	1.00	0.215	No
544	10.88	194.92	96.92	98.00	0.79	0.234	1.43	0.164	1.00	1.00	0.215	No
545	10.90	195.29	97.12	98.17	0.79	0.234	1.43	0.164	1.00	1.00	0.215	No
546	10.92	195.66	97.32	98.34	0.79	0.234	1.43	0.164	1.00	1.00	0.215	No
547	10.94	196.03	97.51	98.51	0.79	0.234	1.43	0.164	1.00	1.00	0.215	No
548	10.96	196.39	97.71	98.69	0.78	0.234	1.43	0.163	1.00	1.00	0.215	No
549	10.98	196.76	97.90	98.86	0.78	0.233	1.43	0.163	1.00	1.00	0.216	No
550	11.00	197.12	98.10	99.02	0.78	0.233	1.43	0.163	1.00	1.00	0.216	No
551	11.02	197.49	98.30	99.19	0.78	0.233	1.43	0.163	1.00	1.00	0.216	No
552	11.04	197.85	98.49	99.36	0.78	0.233	1.43	0.163	1.00	1.00	0.215	No
553	11.06	198.21	98.69	99.52	0.78	0.233	1.43	0.163	1.00	1.00	0.215	No
554	11.08	198.57	98.88	99.69	0.78	0.233	1.43	0.163	1.00	1.00	0.215	No
555	11.10	198.94	99.08	99.85	0.78	0.233	1.43	0.163	1.00	1.00	0.215	No
556	11.13	199.48	99.38	100.10	0.78	0.233	1.43	0.163	1.00	1.00	0.215	No
557	11.14	199.66	99.47	100.18	0.78	0.233	1.43	0.163	1.00	1.00	0.215	No
558	11.17	200.20	99.77	100.43	0.78	0.232	1.43	0.163	1.00	1.00	0.215	No
559	11.18	200.38	99.87	100.52	0.78	0.232	1.43	0.163	1.00	1.00	0.215	No
560	11.20	200.74	100.06	100.68	0.78	0.232	1.43	0.163	1.00	1.00	0.215	No
561	11.22	201.11	100.26	100.85	0.78	0.232	1.43	0.162	1.00	1.00	0.215	No
562	11.24	201.47	100.45	101.02	0.78	0.232	1.43	0.162	1.00	1.00	0.214	No
563	11.26	201.84	100.65	101.19	0.78	0.232	1.43	0.162	1.00	1.00	0.214	No
564	11.28	202.20	100.85	101.35	0.78	0.232	1.43	0.162	1.00	1.00	0.214	No
565	11.30	202.56	101.04	101.52	0.78	0.232	1.43	0.162	1.00	1.00	0.214	No
566	11.32	202.93	101.24	101.69	0.78	0.232	1.43	0.162	1.00	1.00	0.213	No
567	11.34	203.30	101.44	101.86	0.78	0.231	1.43	0.162	1.00	1.00	0.213	No
568	11.36	203.66	101.63	102.03	0.78	0.231	1.43	0.162	1.00	1.00	0.213	No
569	11.39	204.22	101.93	102.29	0.77	0.231	1.43	0.162	1.00	1.00	0.213	No
570	11.40	204.40	102.02	102.38	0.77	0.231	1.43	0.162	1.00	1.00	0.212	No
571	11.42	204.77	102.22	102.55	0.77	0.231	1.43	0.162	1.00	1.00	0.212	No
572	11.44	205.15	102.42	102.73	0.77	0.231	1.43	0.162	1.00	1.00	0.212	No
573	11.46	205.52	102.61	102.91	0.77	0.231	1.43	0.162	1.00	1.00	0.212	No
574	11.48	205.90	102.81	103.09	0.77	0.231	1.43	0.161	1.00	1.00	0.212	No
575	11.50	206.28	103.01	103.27	0.77	0.231	1.43	0.161	1.00	1.00	0.212	No
576	11.52	206.65	103.20	103.45	0.77	0.230	1.43	0.161	1.00	1.00	0.212	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
577	11.54	207.03	103.40	103.64	0.77	0.230	1.43	0.161	1.00	1.00	0.213	No
578	11.56	207.41	103.59	103.82	0.77	0.230	1.43	0.161	1.00	1.00	0.213	No
579	11.58	207.79	103.79	104.00	0.77	0.230	1.43	0.161	1.00	1.00	0.213	No
580	11.60	208.17	103.99	104.18	0.77	0.230	1.43	0.161	1.00	1.00	0.213	No
581	11.62	208.54	104.18	104.36	0.77	0.230	1.43	0.161	1.00	1.00	0.213	No
582	11.64	208.92	104.38	104.54	0.77	0.230	1.43	0.161	1.00	1.00	0.212	No
583	11.66	209.29	104.57	104.72	0.77	0.230	1.43	0.161	1.00	1.00	0.212	No
584	11.68	209.67	104.77	104.90	0.77	0.229	1.43	0.161	1.00	1.00	0.212	No
585	11.70	210.04	104.97	105.07	0.77	0.229	1.43	0.160	1.00	1.00	0.212	No
586	11.72	210.41	105.16	105.25	0.77	0.229	1.43	0.160	1.00	1.00	0.212	No
587	11.75	210.97	105.46	105.51	0.77	0.229	1.43	0.160	1.00	1.00	0.212	No
588	11.76	211.16	105.56	105.60	0.77	0.229	1.43	0.160	1.00	1.00	0.212	No
589	11.78	211.52	105.75	105.77	0.77	0.229	1.43	0.160	1.00	1.00	0.212	No
590	11.80	211.89	105.95	105.95	0.76	0.229	1.43	0.160	1.00	1.00	0.212	No
591	11.82	212.26	106.14	106.12	0.76	0.229	1.43	0.160	1.00	1.00	0.212	No
592	11.84	212.63	106.34	106.29	0.76	0.228	1.43	0.160	1.00	1.00	0.212	No
593	11.86	213.00	106.54	106.46	0.76	0.228	1.43	0.160	1.00	1.00	0.212	No
594	11.88	213.37	106.73	106.64	0.76	0.228	1.43	0.160	1.00	1.00	0.212	No
595	11.91	213.92	107.03	106.89	0.76	0.228	1.43	0.160	1.00	1.00	0.212	No
596	11.92	214.10	107.13	106.98	0.76	0.228	1.43	0.160	1.00	1.00	0.212	No
597	11.94	214.47	107.32	107.15	0.76	0.228	1.43	0.160	1.00	1.00	0.212	No
598	11.96	214.83	107.52	107.31	0.76	0.228	1.43	0.159	1.00	1.00	0.212	No
599	11.98	215.20	107.71	107.48	0.76	0.228	1.43	0.159	1.00	1.00	0.212	No
600	12.00	215.56	107.91	107.65	0.76	0.228	1.43	0.159	0.99	1.00	0.212	No
601	12.02	215.93	108.11	107.82	0.76	0.227	1.43	0.159	0.99	1.00	0.211	No
602	12.04	216.29	108.30	107.99	0.76	0.227	1.43	0.159	0.99	1.00	0.211	No
603	12.06	216.65	108.50	108.15	0.76	0.227	1.43	0.159	0.99	1.00	0.211	No
604	12.08	217.01	108.69	108.32	0.76	0.227	1.43	0.159	0.99	1.00	0.211	No
605	12.10	217.38	108.89	108.49	0.76	0.227	1.43	0.159	0.99	1.00	0.211	No
606	12.20	219.19	109.87	109.32	0.76	0.226	1.43	0.158	0.99	1.00	0.211	No
607	12.20	219.19	109.87	109.32	0.76	0.226	1.43	0.158	0.99	1.00	0.211	No
608	12.11	217.56	108.99	108.57	0.76	0.227	1.43	0.159	0.99	1.00	0.211	No
609	12.20	219.18	109.87	109.31	0.76	0.226	1.43	0.158	0.99	1.00	0.211	No
610	12.22	219.54	110.07	109.48	0.75	0.226	1.43	0.158	0.99	1.00	0.211	No
611	12.24	219.90	110.26	109.64	0.75	0.226	1.43	0.158	0.99	1.00	0.211	No
612	12.26	220.26	110.46	109.80	0.75	0.226	1.43	0.158	0.99	1.00	0.211	No
613	12.28	220.62	110.66	109.96	0.75	0.226	1.43	0.158	0.99	1.00	0.211	No
614	12.30	220.98	110.85	110.13	0.75	0.226	1.43	0.158	0.99	1.00	0.211	No
615	12.32	221.34	111.05	110.29	0.75	0.226	1.43	0.158	0.99	1.00	0.211	No
616	12.34	221.69	111.25	110.45	0.75	0.226	1.43	0.158	0.99	1.00	0.211	No
617	12.36	222.05	111.44	110.60	0.75	0.226	1.43	0.158	0.99	1.00	0.211	No
618	12.38	222.40	111.64	110.76	0.75	0.225	1.43	0.158	0.99	1.00	0.211	No
619	12.40	222.75	111.83	110.92	0.75	0.225	1.43	0.158	0.99	1.00	0.211	No
620	12.42	223.11	112.03	111.08	0.75	0.225	1.43	0.158	0.99	1.00	0.210	No
621	12.44	223.46	112.23	111.23	0.75	0.225	1.43	0.158	0.99	1.00	0.210	No
622	12.46	223.81	112.42	111.39	0.75	0.225	1.43	0.158	0.99	1.00	0.210	No
623	12.48	224.17	112.62	111.55	0.75	0.225	1.43	0.157	0.99	1.00	0.210	No
624	12.50	224.52	112.82	111.70	0.75	0.225	1.43	0.157	0.99	1.00	0.210	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
625	12.52	224.87	113.01	111.86	0.75	0.225	1.43	0.157	0.99	1.00	0.210	No
626	12.55	225.41	113.31	112.10	0.75	0.225	1.43	0.157	0.99	1.00	0.210	No
627	12.56	225.58	113.40	112.18	0.75	0.225	1.43	0.157	0.99	1.00	0.210	No
628	12.58	225.94	113.60	112.34	0.75	0.224	1.43	0.157	0.99	1.00	0.210	No
629	12.60	226.30	113.80	112.50	0.75	0.224	1.43	0.157	0.99	1.00	0.210	No
630	12.62	226.65	113.99	112.66	0.75	0.224	1.43	0.157	0.99	1.00	0.210	No
631	12.64	227.01	114.19	112.82	0.74	0.224	1.43	0.157	0.99	1.00	0.210	No
632	12.66	227.36	114.38	112.97	0.74	0.224	1.43	0.157	0.99	1.00	0.210	No
633	12.68	227.71	114.58	113.13	0.74	0.224	1.43	0.157	0.99	1.00	0.210	No
634	12.70	228.07	114.78	113.29	0.74	0.224	1.43	0.157	0.99	1.00	0.210	No
635	12.72	228.42	114.97	113.44	0.74	0.224	1.43	0.157	0.99	1.00	0.210	No
636	12.74	228.77	115.17	113.60	0.74	0.224	1.43	0.156	0.99	1.00	0.210	No
637	12.76	229.12	115.37	113.75	0.74	0.223	1.43	0.156	0.99	1.00	0.210	No
638	12.78	229.47	115.56	113.91	0.74	0.223	1.43	0.156	0.99	1.00	0.210	No
639	12.80	229.82	115.76	114.06	0.74	0.223	1.43	0.156	0.99	1.00	0.210	No
640	12.83	230.34	116.05	114.29	0.74	0.223	1.43	0.156	0.99	1.00	0.210	No
641	12.84	230.52	116.15	114.37	0.74	0.223	1.43	0.156	0.99	1.00	0.210	No
642	12.86	230.87	116.35	114.52	0.74	0.223	1.43	0.156	0.99	1.00	0.210	No
643	12.88	231.21	116.54	114.67	0.74	0.223	1.43	0.156	0.99	1.00	0.210	No
644	12.90	231.56	116.74	114.82	0.74	0.223	1.43	0.156	0.99	1.00	0.210	No
645	12.92	231.91	116.94	114.97	0.74	0.223	1.43	0.156	0.99	1.00	0.210	No
646	12.94	232.26	117.13	115.12	0.74	0.223	1.43	0.156	0.99	1.00	0.210	No
647	12.96	232.60	117.33	115.27	0.74	0.222	1.43	0.156	0.99	1.00	0.210	No
648	12.98	232.95	117.52	115.42	0.74	0.222	1.43	0.156	0.99	1.00	0.210	No
649	13.00	233.29	117.72	115.57	0.74	0.222	1.43	0.156	0.99	1.00	0.210	No
650	13.02	233.63	117.92	115.71	0.74	0.222	1.43	0.156	0.99	1.00	0.210	No
651	13.04	233.97	118.11	115.85	0.74	0.222	1.43	0.155	0.99	1.00	0.210	No
652	13.06	234.30	118.31	115.99	0.74	0.222	1.43	0.155	0.99	1.00	0.210	No
653	13.08	234.64	118.50	116.13	0.73	0.222	1.43	0.155	0.99	1.00	0.209	No
654	13.10	234.97	118.70	116.27	0.73	0.222	1.43	0.155	0.99	1.00	0.209	No
655	13.12	235.29	118.90	116.40	0.73	0.222	1.43	0.155	0.99	1.00	0.209	No
656	13.14	235.62	119.09	116.52	0.73	0.222	1.43	0.155	0.99	1.00	0.209	No
657	13.16	235.94	119.29	116.65	0.73	0.222	1.43	0.155	0.99	1.00	0.209	No
658	13.18	236.26	119.49	116.77	0.73	0.222	1.43	0.155	0.99	1.00	0.209	No
659	13.20	236.58	119.68	116.90	0.73	0.221	1.43	0.155	0.99	1.00	0.208	No
660	13.22	236.91	119.88	117.03	0.73	0.221	1.43	0.155	0.99	1.00	0.208	No
661	13.24	237.24	120.07	117.16	0.73	0.221	1.43	0.155	0.99	1.00	0.208	No
662	13.26	237.56	120.27	117.29	0.73	0.221	1.43	0.155	0.99	1.00	0.208	No
663	13.28	237.89	120.47	117.43	0.73	0.221	1.43	0.155	0.99	1.00	0.208	No
664	13.30	238.22	120.66	117.56	0.73	0.221	1.43	0.155	0.99	1.00	0.208	No
665	13.32	238.56	120.86	117.70	0.73	0.221	1.43	0.155	0.99	1.00	0.208	No
666	13.34	238.89	121.06	117.83	0.73	0.221	1.43	0.155	0.99	1.00	0.208	No
667	13.36	239.22	121.25	117.97	0.73	0.221	1.43	0.155	0.99	1.00	0.208	No
668	13.41	240.06	121.74	118.31	0.73	0.221	1.43	0.154	0.99	1.00	0.208	No
669	13.41	240.06	121.74	118.31	0.73	0.221	1.43	0.154	0.99	1.00	0.208	No
670	13.42	240.22	121.84	118.38	0.73	0.220	1.43	0.154	0.99	1.00	0.208	No
671	13.44	240.55	122.04	118.52	0.73	0.220	1.43	0.154	0.99	1.00	0.209	No
672	13.46	240.88	122.23	118.65	0.73	0.220	1.43	0.154	0.99	1.00	0.209	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
673	13.48	241.21	122.43	118.78	0.73	0.220	1.43	0.154	0.99	1.00	0.208	No
674	13.50	241.54	122.63	118.92	0.72	0.220	1.43	0.154	0.99	1.00	0.208	No
675	13.52	241.88	122.82	119.05	0.72	0.220	1.43	0.154	0.99	1.00	0.206	No
676	13.54	242.21	123.02	119.19	0.72	0.220	1.43	0.154	0.99	1.00	0.205	No
677	13.56	242.55	123.21	119.34	0.72	0.220	1.43	0.154	0.99	1.00	0.204	No
678	13.58	242.90	123.41	119.49	0.72	0.220	1.43	0.154	0.99	1.00	0.204	No
679	13.60	243.25	123.61	119.64	0.72	0.220	1.43	0.154	0.98	1.00	0.204	No
680	13.62	243.60	123.80	119.79	0.72	0.220	1.43	0.154	0.98	1.00	0.204	No
681	13.64	243.95	124.00	119.95	0.72	0.219	1.43	0.154	0.99	1.00	0.205	No
682	13.66	244.30	124.19	120.10	0.72	0.219	1.43	0.154	0.99	1.00	0.206	No
683	13.68	244.64	124.39	120.25	0.72	0.219	1.43	0.153	0.99	1.00	0.207	No
684	13.70	244.98	124.59	120.40	0.72	0.219	1.43	0.153	0.99	1.00	0.207	No
685	13.72	245.32	124.78	120.54	0.72	0.219	1.43	0.153	0.99	1.00	0.207	No
686	13.74	245.65	124.98	120.67	0.72	0.219	1.43	0.153	0.99	1.00	0.207	No
687	13.76	245.98	125.18	120.81	0.72	0.219	1.43	0.153	0.99	1.00	0.207	No
688	13.78	246.32	125.37	120.95	0.72	0.219	1.43	0.153	0.99	1.00	0.207	No
689	13.80	246.65	125.57	121.08	0.72	0.219	1.43	0.153	0.99	1.00	0.207	No
690	13.83	247.15	125.86	121.29	0.72	0.219	1.43	0.153	0.99	1.00	0.207	No
691	13.84	247.31	125.96	121.35	0.72	0.218	1.43	0.153	0.99	1.00	0.207	No
692	13.86	247.64	126.16	121.48	0.72	0.218	1.43	0.153	0.99	1.00	0.207	No
693	14.03	250.40	127.82	122.57	0.71	0.218	1.43	0.152	0.99	1.00	0.207	No
694	14.03	250.40	127.82	122.57	0.71	0.218	1.43	0.152	0.99	1.00	0.207	No
695	14.03	250.40	127.82	122.57	0.71	0.218	1.43	0.152	0.99	1.00	0.207	No
696	13.88	247.97	126.35	121.62	0.72	0.218	1.43	0.153	0.99	1.00	0.207	No
697	13.96	249.26	127.14	122.12	0.71	0.218	1.43	0.153	0.99	1.00	0.207	No
698	13.98	249.58	127.33	122.25	0.71	0.218	1.43	0.153	0.99	1.00	0.207	No
699	14.00	249.90	127.53	122.37	0.71	0.218	1.43	0.152	0.99	1.00	0.207	No
700	14.02	250.23	127.73	122.50	0.71	0.218	1.43	0.152	0.99	1.00	0.206	No
701	14.04	250.55	127.92	122.63	0.71	0.218	1.43	0.152	0.98	1.00	0.206	No
702	14.06	250.87	128.12	122.76	0.71	0.218	1.43	0.152	0.98	1.00	0.206	No
703	14.08	251.20	128.31	122.89	0.71	0.217	1.43	0.152	0.98	1.00	0.206	No
704	14.10	251.53	128.51	123.02	0.71	0.217	1.43	0.152	0.98	1.00	0.206	No
705	14.12	251.86	128.71	123.15	0.71	0.217	1.43	0.152	0.98	1.00	0.206	No
706	14.14	252.19	128.90	123.29	0.71	0.217	1.43	0.152	0.98	1.00	0.206	No
707	14.16	252.53	129.10	123.43	0.71	0.217	1.43	0.152	0.98	1.00	0.206	No
708	14.18	252.86	129.30	123.56	0.71	0.217	1.43	0.152	0.98	1.00	0.206	No
709	14.21	253.36	129.59	123.77	0.71	0.217	1.43	0.152	0.98	1.00	0.206	No
710	14.22	253.52	129.69	123.83	0.71	0.217	1.43	0.152	0.98	1.00	0.206	No
711	14.24	253.86	129.88	123.97	0.71	0.217	1.43	0.152	0.98	1.00	0.205	No
712	14.26	254.19	130.08	124.11	0.71	0.217	1.43	0.152	0.98	1.00	0.205	No
713	14.28	254.52	130.28	124.24	0.71	0.217	1.43	0.152	0.98	1.00	0.205	No
714	14.30	254.86	130.47	124.38	0.71	0.216	1.43	0.152	0.98	1.00	0.205	No
715	14.32	255.19	130.67	124.52	0.71	0.216	1.43	0.151	0.98	1.00	0.205	No
716	14.37	256.03	131.16	124.87	0.71	0.216	1.43	0.151	0.98	1.00	0.205	No
717	14.37	256.03	131.16	124.87	0.71	0.216	1.43	0.151	0.98	1.00	0.205	No
718	14.38	256.20	131.26	124.95	0.70	0.216	1.43	0.151	0.98	1.00	0.205	No
719	14.40	256.55	131.45	125.09	0.70	0.216	1.43	0.151	0.98	1.00	0.205	No
720	14.42	256.89	131.65	125.24	0.70	0.216	1.43	0.151	0.98	1.00	0.205	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
721	14.44	257.23	131.85	125.38	0.70	0.216	1.43	0.151	0.98	1.00	0.205	No
722	14.46	257.57	132.04	125.53	0.70	0.216	1.43	0.151	0.98	1.00	0.204	No
723	14.48	257.92	132.24	125.68	0.70	0.216	1.43	0.151	0.98	1.00	0.204	No
724	14.50	258.26	132.44	125.83	0.70	0.215	1.43	0.151	0.98	1.00	0.204	No
725	14.52	258.61	132.63	125.98	0.70	0.215	1.43	0.151	0.98	1.00	0.204	No
726	14.54	258.96	132.83	126.13	0.70	0.215	1.43	0.151	0.98	1.00	0.204	No
727	14.56	259.30	133.02	126.28	0.70	0.215	1.43	0.151	0.98	1.00	0.204	No
728	14.58	259.65	133.22	126.43	0.70	0.215	1.43	0.151	0.98	1.00	0.204	No
729	14.60	260.00	133.42	126.58	0.70	0.215	1.43	0.150	0.98	1.00	0.204	No
730	14.62	260.35	133.61	126.73	0.70	0.215	1.43	0.150	0.98	1.00	0.204	No
731	14.64	260.69	133.81	126.89	0.70	0.215	1.43	0.150	0.98	1.00	0.204	No
732	14.66	261.04	134.00	127.04	0.70	0.215	1.43	0.150	0.98	1.00	0.203	No
733	14.68	261.39	134.20	127.19	0.70	0.214	1.43	0.150	0.98	1.00	0.203	No
734	14.70	261.74	134.40	127.34	0.70	0.214	1.43	0.150	0.98	1.00	0.203	No
735	14.72	262.08	134.59	127.49	0.70	0.214	1.43	0.150	0.98	1.00	0.203	No
736	14.74	262.43	134.79	127.64	0.70	0.214	1.43	0.150	0.98	1.00	0.203	No
737	14.76	262.78	134.99	127.80	0.70	0.214	1.43	0.150	0.98	1.00	0.203	No
738	14.78	263.13	135.18	127.95	0.70	0.214	1.43	0.150	0.98	1.00	0.203	No
739	14.80	263.49	135.38	128.11	0.70	0.214	1.43	0.150	0.98	1.00	0.202	No
740	14.82	263.84	135.57	128.27	0.69	0.214	1.43	0.150	0.98	1.00	0.202	No
741	14.84	264.20	135.77	128.43	0.69	0.214	1.43	0.150	0.98	1.00	0.202	No
742	14.86	264.56	135.97	128.59	0.69	0.213	1.43	0.149	0.98	1.00	0.202	No
743	14.88	264.92	136.16	128.76	0.69	0.213	1.43	0.149	0.98	1.00	0.202	No
744	14.90	265.28	136.36	128.92	0.69	0.213	1.43	0.149	0.98	1.00	0.202	No
745	14.92	265.64	136.56	129.09	0.69	0.213	1.43	0.149	0.98	1.00	0.202	No
746	14.94	266.00	136.75	129.25	0.69	0.213	1.43	0.149	0.98	1.00	0.202	No
747	14.96	266.37	136.95	129.42	0.69	0.213	1.43	0.149	0.98	1.00	0.202	No
748	14.98	266.73	137.14	129.58	0.69	0.213	1.43	0.149	0.98	1.00	0.201	No
749	15.00	267.09	137.34	129.75	0.69	0.213	1.43	0.149	0.98	1.00	0.201	No
750	15.02	267.45	137.54	129.92	0.69	0.213	1.43	0.149	0.98	1.00	0.201	No
751	15.04	267.82	137.73	130.08	0.69	0.212	1.43	0.149	0.98	1.00	0.201	No
752	15.06	268.18	137.93	130.25	0.69	0.212	1.43	0.149	0.98	1.00	0.201	No
753	15.08	268.54	138.12	130.42	0.69	0.212	1.43	0.148	0.98	1.00	0.201	No
754	15.10	268.90	138.32	130.58	0.69	0.212	1.43	0.148	0.98	1.00	0.201	No
755	15.12	269.26	138.52	130.75	0.69	0.212	1.43	0.148	0.98	1.00	0.201	No
756	15.14	269.63	138.71	130.91	0.69	0.212	1.43	0.148	0.98	1.00	0.201	No
757	15.16	269.99	138.91	131.08	0.69	0.212	1.43	0.148	0.98	1.00	0.201	No
758	15.18	270.35	139.11	131.24	0.69	0.212	1.43	0.148	0.98	1.00	0.200	No
759	15.20	270.71	139.30	131.41	0.69	0.211	1.43	0.148	0.98	1.00	0.200	No
760	15.22	271.07	139.50	131.57	0.69	0.211	1.43	0.148	0.98	1.00	0.200	No
761	15.24	271.43	139.69	131.74	0.69	0.211	1.43	0.148	0.98	1.00	0.200	No
762	15.26	271.79	139.89	131.90	0.69	0.211	1.43	0.148	0.98	1.00	0.200	No
763	15.28	272.15	140.09	132.06	0.68	0.211	1.43	0.148	0.98	1.00	0.200	No
764	15.30	272.51	140.28	132.23	0.68	0.211	1.43	0.148	0.98	1.00	0.200	No
765	15.32	272.88	140.48	132.40	0.68	0.211	1.43	0.147	0.98	1.00	0.200	No
766	15.34	273.24	140.68	132.57	0.68	0.211	1.43	0.147	0.98	1.00	0.200	No
767	15.36	273.61	140.87	132.74	0.68	0.210	1.43	0.147	0.98	1.00	0.199	No
768	15.38	273.97	141.07	132.90	0.68	0.210	1.43	0.147	0.98	1.00	0.199	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
769	15.40	274.34	141.26	133.07	0.68	0.210	1.43	0.147	0.98	1.00	0.199	No
770	15.42	274.70	141.46	133.24	0.68	0.210	1.43	0.147	0.98	1.00	0.199	No
771	15.44	275.07	141.66	133.41	0.68	0.210	1.43	0.147	0.98	1.00	0.199	No
772	15.46	275.43	141.85	133.58	0.68	0.210	1.43	0.147	0.98	1.00	0.199	No
773	15.48	275.80	142.05	133.75	0.68	0.210	1.43	0.147	0.98	1.00	0.199	No
774	15.50	276.16	142.25	133.91	0.68	0.210	1.43	0.147	0.98	1.00	0.199	No
775	15.52	276.52	142.44	134.08	0.68	0.210	1.43	0.147	0.98	1.00	0.198	No
776	15.54	276.89	142.64	134.25	0.68	0.209	1.43	0.147	0.98	1.00	0.198	No
777	15.56	277.25	142.83	134.42	0.68	0.209	1.43	0.146	0.98	1.00	0.198	No
778	15.58	277.62	143.03	134.59	0.68	0.209	1.43	0.146	0.98	1.00	0.198	No
779	15.60	277.98	143.23	134.76	0.68	0.209	1.43	0.146	0.98	1.00	0.198	No
780	15.62	278.35	143.42	134.93	0.68	0.209	1.43	0.146	0.98	1.00	0.198	No
781	15.64	278.71	143.62	135.10	0.68	0.209	1.43	0.146	0.98	1.00	0.198	No
782	15.66	279.08	143.81	135.26	0.68	0.209	1.43	0.146	0.98	1.00	0.198	No
783	15.68	279.44	144.01	135.43	0.68	0.209	1.43	0.146	0.98	1.00	0.198	No
784	15.70	279.81	144.21	135.60	0.68	0.208	1.43	0.146	0.98	1.00	0.198	No
785	15.72	280.17	144.40	135.77	0.68	0.208	1.43	0.146	0.98	1.00	0.198	No
786	15.74	280.53	144.60	135.94	0.67	0.208	1.43	0.146	0.98	1.00	0.198	No
787	15.76	280.90	144.80	136.10	0.67	0.208	1.43	0.146	0.98	1.00	0.198	No
788	15.78	281.26	144.99	136.27	0.67	0.208	1.43	0.146	0.98	1.00	0.198	No
789	15.80	281.63	145.19	136.44	0.67	0.208	1.43	0.145	0.98	1.00	0.198	No
790	15.82	281.99	145.38	136.61	0.67	0.208	1.43	0.145	0.97	1.00	0.197	No
791	15.84	282.36	145.58	136.78	0.67	0.208	1.43	0.145	0.97	1.00	0.197	No
792	15.86	282.73	145.78	136.95	0.67	0.207	1.43	0.145	0.97	1.00	0.197	No
793	15.88	283.09	145.97	137.12	0.67	0.207	1.43	0.145	0.97	1.00	0.197	No
794	15.90	283.46	146.17	137.29	0.67	0.207	1.43	0.145	0.97	1.00	0.197	No
795	15.92	283.82	146.37	137.46	0.67	0.207	1.43	0.145	0.97	1.00	0.197	No
796	15.94	284.19	146.56	137.63	0.67	0.207	1.43	0.145	0.97	1.00	0.197	No
797	15.96	284.56	146.76	137.80	0.67	0.207	1.43	0.145	0.97	1.00	0.197	No
798	15.98	284.92	146.95	137.97	0.67	0.207	1.43	0.145	0.97	1.00	0.197	No
799	16.00	285.29	147.15	138.14	0.67	0.207	1.43	0.145	0.97	1.00	0.197	No
800	16.02	285.66	147.35	138.31	0.67	0.206	1.43	0.145	0.97	1.00	0.196	No
801	16.04	286.03	147.54	138.48	0.67	0.206	1.43	0.144	0.97	1.00	0.196	No
802	16.07	286.58	147.84	138.74	0.67	0.206	1.43	0.144	0.97	1.00	0.196	No
803	16.08	286.76	147.93	138.83	0.67	0.206	1.43	0.144	0.97	1.00	0.195	No
804	16.10	287.13	148.13	139.00	0.67	0.206	1.43	0.144	0.97	1.00	0.195	No
805	16.12	287.50	148.33	139.17	0.67	0.206	1.43	0.144	0.97	1.00	0.195	No
806	16.14	287.87	148.52	139.34	0.67	0.206	1.43	0.144	0.97	1.00	0.195	No
807	16.16	288.23	148.72	139.51	0.67	0.206	1.43	0.144	0.97	1.00	0.195	No
808	16.18	288.60	148.92	139.69	0.67	0.205	1.43	0.144	0.97	1.00	0.194	No
809	16.20	288.97	149.11	139.86	0.66	0.205	1.43	0.144	0.97	1.00	0.194	No
810	16.22	289.35	149.31	140.04	0.66	0.205	1.43	0.144	0.97	1.00	0.194	No
811	16.24	289.72	149.50	140.22	0.66	0.205	1.43	0.144	0.97	1.00	0.194	No
812	16.26	290.10	149.70	140.40	0.66	0.205	1.43	0.143	0.97	1.00	0.194	No
813	16.28	290.47	149.90	140.58	0.66	0.205	1.43	0.143	0.97	1.00	0.194	No
814	16.30	290.85	150.09	140.76	0.66	0.205	1.43	0.143	0.97	1.00	0.194	No
815	16.32	291.23	150.29	140.94	0.66	0.205	1.43	0.143	0.97	1.00	0.194	No
816	16.34	291.61	150.49	141.12	0.66	0.204	1.43	0.143	0.97	1.00	0.194	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
817	16.36	291.99	150.68	141.31	0.66	0.204	1.43	0.143	0.97	1.00	0.194	No
818	16.38	292.37	150.88	141.49	0.66	0.204	1.43	0.143	0.97	1.00	0.194	No
819	16.40	292.74	151.07	141.67	0.66	0.204	1.43	0.143	0.97	1.00	0.194	No
820	16.42	293.12	151.27	141.85	0.66	0.204	1.43	0.143	0.97	1.00	0.194	No
821	16.44	293.50	151.47	142.03	0.66	0.204	1.43	0.143	0.97	1.00	0.194	No
822	16.46	293.87	151.66	142.21	0.66	0.204	1.43	0.143	0.97	1.00	0.194	No
823	16.48	294.25	151.86	142.39	0.66	0.204	1.43	0.142	0.97	1.00	0.194	No
824	16.50	294.62	152.06	142.56	0.66	0.203	1.43	0.142	0.97	1.00	0.194	No
825	16.52	294.99	152.25	142.74	0.66	0.203	1.43	0.142	0.97	1.00	0.194	No
826	16.54	295.36	152.45	142.91	0.66	0.203	1.43	0.142	0.97	1.00	0.194	No
827	16.56	295.72	152.64	143.08	0.66	0.203	1.43	0.142	0.97	1.00	0.194	No
828	16.58	296.09	152.84	143.25	0.66	0.203	1.43	0.142	0.97	1.00	0.194	No
829	16.60	296.44	153.04	143.41	0.66	0.203	1.43	0.142	0.97	1.00	0.194	No
830	16.62	296.80	153.23	143.57	0.66	0.203	1.43	0.142	0.97	1.00	0.194	No
831	16.64	297.15	153.43	143.72	0.66	0.203	1.43	0.142	0.97	1.00	0.194	No
832	16.66	297.49	153.62	143.87	0.66	0.203	1.43	0.142	0.97	1.00	0.194	No
833	16.68	297.84	153.82	144.02	0.65	0.202	1.43	0.142	0.97	1.00	0.194	No
834	16.70	298.18	154.02	144.16	0.65	0.202	1.43	0.142	0.97	1.00	0.194	No
835	16.72	298.52	154.21	144.31	0.65	0.202	1.43	0.142	0.97	1.00	0.194	No
836	16.74	298.86	154.41	144.45	0.65	0.202	1.43	0.141	0.97	1.00	0.194	No
837	16.76	299.20	154.61	144.59	0.65	0.202	1.43	0.141	0.97	1.00	0.194	No
838	16.78	299.53	154.80	144.73	0.65	0.202	1.43	0.141	0.97	1.00	0.194	No
839	16.80	299.87	155.00	144.87	0.65	0.202	1.43	0.141	0.97	1.00	0.194	No
840	16.82	300.20	155.19	145.00	0.65	0.202	1.43	0.141	0.97	1.00	0.193	No
841	16.84	300.53	155.39	145.14	0.65	0.202	1.43	0.141	0.97	1.00	0.193	No
842	16.86	300.86	155.59	145.28	0.65	0.202	1.43	0.141	0.97	1.00	0.193	No
843	16.88	301.20	155.78	145.41	0.65	0.201	1.43	0.141	0.97	1.00	0.193	No
844	16.90	301.53	155.98	145.55	0.65	0.201	1.43	0.141	0.97	1.00	0.193	No
845	16.92	301.86	156.18	145.69	0.65	0.201	1.43	0.141	0.97	1.00	0.193	No
846	16.94	302.19	156.37	145.82	0.65	0.201	1.43	0.141	0.97	1.00	0.193	No
847	16.96	302.53	156.57	145.96	0.65	0.201	1.43	0.141	0.97	1.00	0.193	No
848	16.98	302.86	156.76	146.09	0.65	0.201	1.43	0.141	0.97	1.00	0.193	No
849	17.00	303.19	156.96	146.23	0.65	0.201	1.43	0.141	0.97	1.00	0.193	No
850	17.02	303.52	157.16	146.36	0.65	0.201	1.43	0.141	0.97	1.00	0.192	No
851	17.04	303.85	157.35	146.50	0.65	0.201	1.43	0.140	0.97	1.00	0.192	No
852	17.06	304.18	157.55	146.63	0.65	0.201	1.43	0.140	0.97	1.00	0.192	No
853	17.08	304.52	157.74	146.77	0.65	0.201	1.43	0.140	0.97	1.00	0.192	No
854	17.10	304.85	157.94	146.91	0.65	0.200	1.43	0.140	0.97	1.00	0.192	No
855	17.12	305.19	158.14	147.05	0.65	0.200	1.43	0.140	0.97	1.00	0.192	No
856	17.14	305.53	158.33	147.19	0.65	0.200	1.43	0.140	0.97	1.00	0.192	No
857	17.16	305.87	158.53	147.34	0.64	0.200	1.43	0.140	0.97	1.00	0.192	No
858	17.18	306.21	158.73	147.48	0.64	0.200	1.43	0.140	0.97	1.00	0.192	No
859	17.20	306.54	158.92	147.62	0.64	0.200	1.43	0.140	0.97	1.00	0.192	No
860	17.22	306.88	159.12	147.76	0.64	0.200	1.43	0.140	0.97	1.00	0.192	No
861	17.24	307.22	159.31	147.90	0.64	0.200	1.43	0.140	0.97	1.00	0.192	No
862	17.26	307.55	159.51	148.04	0.64	0.200	1.43	0.140	0.97	1.00	0.192	No
863	17.28	307.88	159.71	148.17	0.64	0.200	1.43	0.140	0.97	1.00	0.192	No
864	17.30	308.20	159.90	148.30	0.64	0.199	1.43	0.140	0.97	1.00	0.192	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
865	17.32	308.53	160.10	148.43	0.64	0.199	1.43	0.140	0.97	1.00	0.191	No
866	17.34	308.86	160.30	148.56	0.64	0.199	1.43	0.139	0.97	1.00	0.191	No
867	17.36	309.19	160.49	148.70	0.64	0.199	1.43	0.139	0.97	1.00	0.191	No
868	17.38	309.52	160.69	148.83	0.64	0.199	1.43	0.139	0.97	1.00	0.191	No
869	17.44	310.52	161.28	149.24	0.64	0.199	1.43	0.139	0.97	1.00	0.191	No
870	17.44	310.52	161.28	149.24	0.64	0.199	1.43	0.139	0.97	1.00	0.191	No
871	17.44	310.52	161.28	149.24	0.64	0.199	1.43	0.139	0.97	1.00	0.191	No
872	17.46	310.85	161.47	149.38	0.64	0.199	1.43	0.139	0.97	1.00	0.190	No
873	17.48	311.19	161.67	149.52	0.64	0.199	1.43	0.139	0.97	1.00	0.190	No
874	17.50	311.53	161.87	149.66	0.64	0.199	1.43	0.139	0.97	1.00	0.190	No
875	17.52	311.87	162.06	149.81	0.64	0.198	1.43	0.139	0.97	1.00	0.190	No
876	17.54	312.21	162.26	149.95	0.64	0.198	1.43	0.139	0.97	1.00	0.190	No
877	17.56	312.55	162.45	150.10	0.64	0.198	1.43	0.139	0.97	1.00	0.190	No
878	17.58	312.89	162.65	150.24	0.64	0.198	1.43	0.139	0.97	1.00	0.190	No
879	17.63	313.74	163.14	150.60	0.64	0.198	1.43	0.139	0.97	1.00	0.190	No
880	17.63	313.74	163.14	150.60	0.64	0.198	1.43	0.139	0.97	1.00	0.190	No
881	17.64	313.91	163.24	150.67	0.64	0.198	1.43	0.138	0.97	1.00	0.191	No
882	17.66	314.24	163.43	150.81	0.63	0.198	1.43	0.138	0.97	1.00	0.190	No
883	17.68	314.58	163.63	150.94	0.63	0.198	1.43	0.138	0.97	1.00	0.190	No
884	17.70	314.90	163.83	151.08	0.63	0.198	1.43	0.138	0.97	1.00	0.190	No
885	17.72	315.23	164.02	151.20	0.63	0.197	1.43	0.138	0.97	1.00	0.190	No
886	17.74	315.55	164.22	151.33	0.63	0.197	1.43	0.138	0.97	1.00	0.190	No
887	17.76	315.87	164.42	151.46	0.63	0.197	1.43	0.138	0.97	1.00	0.190	No
888	17.78	316.19	164.61	151.58	0.63	0.197	1.43	0.138	0.97	1.00	0.190	No
889	17.80	316.51	164.81	151.70	0.63	0.197	1.43	0.138	0.97	1.00	0.189	No
890	17.82	316.84	165.00	151.83	0.63	0.197	1.43	0.138	0.97	1.00	0.190	No
891	17.84	317.16	165.20	151.96	0.63	0.197	1.43	0.138	0.97	1.00	0.190	No
892	17.86	317.48	165.40	152.09	0.63	0.197	1.43	0.138	0.97	1.00	0.190	No
893	17.88	317.80	165.59	152.21	0.63	0.197	1.43	0.138	0.97	1.00	0.190	No
894	17.90	318.12	165.79	152.34	0.63	0.197	1.43	0.138	0.97	1.00	0.190	No
895	17.95	318.93	166.28	152.65	0.63	0.196	1.43	0.138	0.97	1.00	0.189	No
896	17.95	318.93	166.28	152.65	0.63	0.196	1.43	0.138	0.97	1.00	0.189	No
897	17.96	319.09	166.38	152.71	0.63	0.196	1.43	0.137	0.97	1.00	0.189	No
898	17.98	319.41	166.57	152.83	0.63	0.196	1.43	0.137	0.97	1.00	0.189	No
899	18.00	319.73	166.77	152.96	0.63	0.196	1.43	0.137	0.97	1.00	0.189	No
900	18.02	320.05	166.97	153.08	0.63	0.196	1.43	0.137	0.97	1.00	0.189	No
901	18.04	320.38	167.16	153.21	0.63	0.196	1.43	0.137	0.97	1.00	0.189	No
902	18.06	320.70	167.36	153.35	0.63	0.196	1.43	0.137	0.97	1.00	0.188	No
903	18.08	321.03	167.55	153.48	0.63	0.196	1.43	0.137	0.97	1.00	0.188	No
904	18.10	321.37	167.75	153.62	0.63	0.196	1.43	0.137	0.96	1.00	0.187	No
905	18.12	321.71	167.95	153.76	0.63	0.196	1.43	0.137	0.96	1.00	0.187	No
906	18.14	322.05	168.14	153.91	0.63	0.196	1.43	0.137	0.96	1.00	0.187	No
907	18.16	322.40	168.34	154.06	0.62	0.195	1.43	0.137	0.96	1.00	0.187	No
908	18.18	322.75	168.54	154.21	0.62	0.195	1.43	0.137	0.96	1.00	0.187	No
909	18.20	323.10	168.73	154.37	0.62	0.195	1.43	0.137	0.96	1.00	0.188	No
910	18.22	323.45	168.93	154.52	0.62	0.195	1.43	0.137	0.96	1.00	0.188	No
911	18.24	323.81	169.12	154.68	0.62	0.195	1.43	0.137	0.96	1.00	0.187	No
912	18.26	324.16	169.32	154.84	0.62	0.195	1.43	0.136	0.96	1.00	0.188	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
913	18.28	324.51	169.52	154.99	0.62	0.195	1.43	0.136	0.97	1.00	0.188	No
914	18.30	324.86	169.71	155.14	0.62	0.195	1.43	0.136	0.97	1.00	0.188	No
915	18.32	325.20	169.91	155.29	0.62	0.195	1.43	0.136	0.97	1.00	0.188	No
916	18.34	325.54	170.11	155.43	0.62	0.195	1.43	0.136	0.97	1.00	0.188	No
917	18.36	325.88	170.30	155.57	0.62	0.194	1.43	0.136	0.97	1.00	0.188	No
918	18.38	326.21	170.50	155.71	0.62	0.194	1.43	0.136	0.97	1.00	0.187	No
919	18.40	326.55	170.69	155.85	0.62	0.194	1.43	0.136	0.97	1.00	0.187	No
920	18.42	326.88	170.89	155.99	0.62	0.194	1.43	0.136	0.97	1.00	0.187	No
921	18.44	327.21	171.09	156.12	0.62	0.194	1.43	0.136	0.96	1.00	0.187	No
922	18.46	327.53	171.28	156.25	0.62	0.194	1.43	0.136	0.96	1.00	0.187	No
923	18.48	327.86	171.48	156.39	0.62	0.194	1.43	0.136	0.96	1.00	0.187	No
924	18.50	328.20	171.68	156.52	0.62	0.194	1.43	0.136	0.96	1.00	0.187	No
925	18.52	328.53	171.87	156.66	0.62	0.194	1.43	0.136	0.96	1.00	0.187	No
926	18.54	328.86	172.07	156.79	0.62	0.194	1.43	0.136	0.96	1.00	0.187	No
927	18.56	329.19	172.26	156.92	0.62	0.194	1.43	0.135	0.96	1.00	0.187	No
928	18.58	329.52	172.46	157.06	0.62	0.193	1.43	0.135	0.96	1.00	0.187	No
929	18.60	329.85	172.66	157.19	0.62	0.193	1.43	0.135	0.96	1.00	0.186	No
930	18.62	330.18	172.85	157.33	0.62	0.193	1.43	0.135	0.96	1.00	0.186	No
931	18.64	330.52	173.05	157.47	0.62	0.193	1.43	0.135	0.96	1.00	0.187	No
932	18.66	330.85	173.24	157.60	0.62	0.193	1.43	0.135	0.96	1.00	0.186	No
933	18.68	331.18	173.44	157.74	0.61	0.193	1.43	0.135	0.96	1.00	0.186	No
934	18.70	331.51	173.64	157.88	0.61	0.193	1.43	0.135	0.96	1.00	0.186	No
935	18.72	331.85	173.83	158.01	0.61	0.193	1.43	0.135	0.96	1.00	0.186	No
936	18.74	332.18	174.03	158.15	0.61	0.193	1.43	0.135	0.96	1.00	0.186	No
937	18.76	332.52	174.23	158.29	0.61	0.193	1.43	0.135	0.96	1.00	0.186	No
938	18.78	332.86	174.42	158.44	0.61	0.193	1.43	0.135	0.96	1.00	0.186	No
939	18.80	333.21	174.62	158.59	0.61	0.192	1.43	0.135	0.96	1.00	0.185	No
940	18.82	333.56	174.81	158.75	0.61	0.192	1.43	0.135	0.96	1.00	0.185	No
941	18.84	333.91	175.01	158.90	0.61	0.192	1.43	0.135	0.96	1.00	0.186	No
942	18.86	334.26	175.21	159.05	0.61	0.192	1.43	0.134	0.96	1.00	0.185	No
943	18.89	334.78	175.50	159.27	0.61	0.192	1.43	0.134	0.96	1.00	0.185	No
944	18.90	334.95	175.60	159.35	0.61	0.192	1.43	0.134	0.96	1.00	0.185	No
945	18.92	335.29	175.80	159.50	0.61	0.192	1.43	0.134	0.96	1.00	0.185	No
946	18.94	335.63	175.99	159.64	0.61	0.192	1.43	0.134	0.96	1.00	0.185	No
947	18.96	335.97	176.19	159.79	0.61	0.192	1.43	0.134	0.96	1.00	0.184	No
948	18.98	336.32	176.38	159.93	0.61	0.192	1.43	0.134	0.96	1.00	0.184	No
949	19.00	336.66	176.58	160.08	0.61	0.191	1.43	0.134	0.96	1.00	0.183	No
950	19.02	337.01	176.78	160.24	0.61	0.191	1.43	0.134	0.96	1.00	0.183	No
951	19.04	337.37	176.97	160.40	0.61	0.191	1.43	0.134	0.96	1.00	0.183	No
952	19.07	337.91	177.27	160.64	0.61	0.191	1.43	0.134	0.96	1.00	0.183	No
953	19.08	338.09	177.36	160.72	0.61	0.191	1.43	0.134	0.96	1.00	0.183	No
954	19.10	338.45	177.56	160.89	0.61	0.191	1.43	0.134	0.96	1.00	0.184	No
955	19.13	338.99	177.86	161.13	0.61	0.191	1.43	0.134	0.96	1.00	0.184	No
956	19.14	339.17	177.95	161.22	0.61	0.191	1.43	0.133	0.96	1.00	0.184	No
957	19.16	339.53	178.15	161.38	0.61	0.191	1.43	0.133	0.96	1.00	0.184	No
958	19.18	339.88	178.35	161.54	0.61	0.190	1.43	0.133	0.96	1.00	0.184	No
959	19.20	340.24	178.54	161.70	0.61	0.190	1.43	0.133	0.96	1.00	0.184	No
960	19.22	340.59	178.74	161.85	0.60	0.190	1.43	0.133	0.96	1.00	0.183	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
961	19.24	340.94	178.93	162.01	0.60	0.190	1.43	0.133	0.96	1.00	0.183	No
962	19.26	341.29	179.13	162.16	0.60	0.190	1.43	0.133	0.96	1.00	0.182	No
963	19.28	341.65	179.33	162.32	0.60	0.190	1.43	0.133	0.96	1.00	0.182	No
964	19.31	342.18	179.62	162.56	0.60	0.190	1.43	0.133	0.96	1.00	0.181	No
965	19.32	342.36	179.72	162.65	0.60	0.190	1.43	0.133	0.96	1.00	0.182	No
966	19.34	342.73	179.92	162.81	0.60	0.190	1.43	0.133	0.96	1.00	0.182	No
967	19.36	343.09	180.11	162.98	0.60	0.190	1.43	0.133	0.96	1.00	0.183	No
968	19.38	343.45	180.31	163.14	0.60	0.189	1.43	0.133	0.96	1.00	0.183	No
969	19.40	343.81	180.50	163.31	0.60	0.189	1.43	0.133	0.96	1.00	0.182	No
970	19.42	344.17	180.70	163.47	0.60	0.189	1.43	0.132	0.96	1.00	0.182	No
971	19.44	344.53	180.90	163.63	0.60	0.189	1.43	0.132	0.96	1.00	0.181	No
972	19.46	344.89	181.09	163.80	0.60	0.189	1.43	0.132	0.96	1.00	0.181	No
973	19.48	345.26	181.29	163.97	0.60	0.189	1.43	0.132	0.96	1.00	0.180	No
974	19.50	345.62	181.49	164.14	0.60	0.189	1.43	0.132	0.96	1.00	0.180	No
975	19.52	345.99	181.68	164.31	0.60	0.189	1.43	0.132	0.96	1.00	0.181	No
976	19.54	346.35	181.88	164.47	0.60	0.189	1.43	0.132	0.96	1.00	0.181	No
977	19.56	346.71	182.07	164.64	0.60	0.188	1.43	0.132	0.96	1.00	0.182	No
978	19.58	347.07	182.27	164.80	0.60	0.188	1.43	0.132	0.96	1.00	0.182	No
979	19.60	347.43	182.47	164.96	0.60	0.188	1.43	0.132	0.96	1.00	0.182	No
980	19.62	347.78	182.66	165.12	0.60	0.188	1.43	0.132	0.96	1.00	0.182	No
981	19.64	348.13	182.86	165.28	0.60	0.188	1.43	0.132	0.96	1.00	0.182	No
982	19.66	348.49	183.05	165.43	0.60	0.188	1.43	0.132	0.96	1.00	0.182	No
983	19.68	348.83	183.25	165.58	0.60	0.188	1.43	0.131	0.96	1.00	0.182	No
984	19.70	349.18	183.45	165.73	0.60	0.188	1.43	0.131	0.96	1.00	0.182	No
985	19.72	349.52	183.64	165.88	0.60	0.188	1.43	0.131	0.96	1.00	0.181	No
986	19.74	349.86	183.84	166.02	0.60	0.188	1.43	0.131	0.96	1.00	0.181	No
987	19.76	350.20	184.04	166.17	0.59	0.187	1.43	0.131	0.96	1.00	0.181	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (m)
σ_v: Total overburden pressure at test point (kPa)
u_0: Water pressure at test point (kPa)
σ_v': Effective overburden pressure based on GWT during earthquake (kPa)
r_d: Nonlinear shear mass factor
CSR: Cyclic Stress Ratio
MSF: Magnitude Scaling Factor
CSR_{eq}: CSR adjusted for M=7.5
K_σ: Effective overburden stress factor
CSR^*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1	0.02	0.57	94.61	2.90	0.59	1.70	9.40	0.00	9.40	4.000	No	Yes	2.00
2	0.04	0.60	99.53	2.96	0.58	1.70	9.75	0.00	9.75	4.000	No	Yes	2.00
3	0.06	0.66	98.87	2.95	0.58	1.70	10.26	0.00	10.26	4.000	No	Yes	2.00
4	0.08	0.73	97.76	2.93	0.57	1.70	12.64	0.00	12.64	4.000	No	Yes	2.00
5	0.10	0.80	97.16	2.93	0.57	1.70	13.30	0.00	13.30	4.000	No	Yes	2.00
6	0.12	0.82	99.29	2.95	0.57	1.70	13.81	0.00	13.81	4.000	No	Yes	2.00
7	0.14	0.84	100.00	2.99	0.57	1.70	14.00	0.00	14.00	4.000	No	Yes	2.00
8	0.16	0.85	100.00	3.02	0.57	1.70	14.43	0.00	14.43	4.000	No	Yes	2.00
9	0.18	0.86	100.00	3.06	0.57	1.70	14.29	0.00	14.29	4.000	No	Yes	2.00
10	0.20	0.87	100.00	3.09	0.56	1.70	14.74	0.00	14.74	4.000	No	Yes	2.00
11	0.22	0.90	100.00	3.10	0.56	1.70	14.72	0.00	14.72	4.000	No	Yes	2.00
12	0.24	0.93	100.00	3.09	0.56	1.70	15.73	0.00	15.73	4.000	No	Yes	2.00
13	0.26	0.97	100.00	3.08	0.56	1.70	16.61	0.00	16.61	4.000	No	Yes	2.00
14	0.28	0.99	100.00	3.08	0.56	1.70	16.60	0.00	16.60	4.000	No	Yes	2.00
15	0.30	0.98	100.00	3.08	0.56	1.70	16.61	0.00	16.61	4.000	No	Yes	2.00
16	0.32	0.99	100.00	3.08	0.56	1.70	16.47	0.00	16.47	4.000	No	Yes	2.00
17	0.34	1.03	100.00	3.06	0.56	1.70	17.06	0.00	17.06	4.000	No	Yes	2.00
18	0.36	1.09	100.00	3.03	0.55	1.70	18.61	0.00	18.61	4.000	No	Yes	2.00
19	0.38	1.15	100.00	3.00	0.55	1.70	19.51	0.00	19.51	4.000	No	Yes	2.00
20	0.40	1.18	100.00	2.99	0.55	1.70	20.01	0.00	20.01	4.000	No	Yes	2.00
21	0.42	1.17	100.00	2.99	0.55	1.70	20.14	0.00	20.14	4.000	No	Yes	2.00
22	0.44	1.13	100.00	3.02	0.55	1.70	19.15	0.00	19.15	4.000	No	Yes	2.00
23	0.46	1.07	100.00	3.06	0.55	1.70	17.87	0.00	17.87	4.000	No	Yes	2.00
24	0.48	1.02	100.00	3.09	0.56	1.70	17.18	0.00	17.18	4.000	No	Yes	2.00
25	0.50	1.00	100.00	3.12	0.56	1.70	16.76	0.00	16.76	4.000	No	Yes	2.00
26	0.52	0.98	100.00	3.14	0.56	1.70	16.46	0.00	16.46	4.000	No	Yes	2.00
27	0.54	0.97	100.00	3.15	0.56	1.70	16.41	0.00	16.41	4.000	No	Yes	2.00
28	0.56	0.97	100.00	3.15	0.56	1.70	16.36	0.00	16.36	4.000	No	Yes	2.00
29	0.58	0.99	100.00	3.13	0.56	1.70	16.56	0.00	16.56	4.000	No	Yes	2.00
30	0.60	1.03	100.00	3.09	0.56	1.70	17.09	0.00	17.09	4.000	No	Yes	2.00
31	0.62	1.08	100.00	3.05	0.55	1.70	18.54	0.00	18.54	4.000	No	Yes	2.00
32	0.64	1.12	100.00	3.02	0.55	1.70	19.11	0.00	19.11	4.000	No	Yes	2.00
33	0.66	1.13	100.00	3.01	0.55	1.70	19.11	0.00	19.11	4.000	No	Yes	2.00
34	0.68	1.12	100.00	3.03	0.55	1.70	18.97	0.00	18.97	4.000	No	Yes	2.00
35	0.70	1.10	100.00	3.05	0.55	1.70	18.65	0.00	18.65	4.000	No	Yes	2.00
36	0.72	1.07	100.00	3.08	0.55	1.70	18.09	0.00	18.09	4.000	No	Yes	2.00
37	0.74	1.04	100.00	3.10	0.55	1.70	17.58	0.00	17.58	4.000	No	Yes	2.00
38	0.76	1.03	100.00	3.12	0.56	1.70	17.25	0.00	17.25	4.000	No	Yes	2.00
39	0.78	1.04	100.00	3.11	0.56	1.70	17.19	0.00	17.19	4.000	No	Yes	2.00
40	0.80	1.06	100.00	3.09	0.55	1.70	18.15	0.00	18.15	4.000	No	Yes	2.00
41	0.82	1.09	100.00	3.07	0.55	1.70	18.59	0.00	18.59	4.000	No	Yes	2.00
42	0.84	1.10	100.00	3.05	0.55	1.70	18.68	0.00	18.68	4.000	No	Yes	2.00
43	0.86	1.10	100.00	3.04	0.55	1.70	18.46	0.00	18.46	4.000	No	Yes	2.00
44	0.88	1.11	100.00	3.02	0.55	1.70	18.59	0.00	18.59	4.000	No	Yes	2.00
45	0.90	1.13	100.00	3.00	0.55	1.70	18.99	0.00	18.99	4.000	No	Yes	2.00
46	0.92	1.17	100.00	2.97	0.55	1.70	19.50	0.00	19.50	4.000	No	Yes	2.00
47	0.95	1.22	98.44	2.94	0.54	1.70	20.63	0.00	20.63	4.000	No	Yes	2.00
48	0.96	1.26	96.62	2.92	0.54	1.70	21.42	0.00	21.42	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
49	0.98	1.28	96.83	2.92	0.54	1.70	21.50	0.00	21.50	4.000	No	Yes	2.00
50	1.00	1.28	97.73	2.93	0.54	1.70	21.41	0.00	21.41	4.000	No	Yes	2.00
51	1.02	1.29	98.43	2.94	0.54	1.70	21.64	0.00	21.64	4.000	No	Yes	2.00
52	1.05	1.31	98.79	2.95	0.54	1.70	21.99	0.00	21.99	4.000	No	Yes	2.00
53	1.06	1.32	99.35	2.95	0.54	1.70	22.18	0.00	22.18	4.000	No	Yes	2.00
54	1.08	1.33	100.00	2.97	0.54	1.70	22.49	0.00	22.49	4.000	No	Yes	2.00
55	1.10	1.34	100.00	2.98	0.54	1.70	22.33	0.00	22.33	4.000	No	Yes	2.00
56	1.12	1.33	100.00	2.99	0.54	1.70	22.43	0.00	22.43	4.000	No	Yes	2.00
57	1.14	1.33	100.00	2.99	0.54	1.70	22.11	0.00	22.11	4.000	No	Yes	2.00
58	1.16	1.34	100.00	2.98	0.54	1.70	22.41	0.00	22.41	4.000	No	Yes	2.00
59	1.18	1.38	100.00	2.97	0.54	1.70	23.03	0.00	23.03	4.000	No	Yes	2.00
60	1.20	1.42	99.33	2.95	0.53	1.70	23.80	0.00	23.80	4.000	No	Yes	2.00
61	1.22	1.44	98.97	2.95	0.53	1.70	24.30	0.00	24.30	4.000	No	Yes	2.00
62	1.24	1.45	99.01	2.95	0.53	1.70	24.08	0.00	24.08	4.000	No	Yes	2.00
63	1.26	1.47	99.02	2.95	0.53	1.70	24.42	0.00	24.42	4.000	No	Yes	2.00
64	1.28	1.50	98.26	2.94	0.53	1.70	25.03	0.00	25.03	4.000	No	Yes	2.00
65	1.30	1.53	97.52	2.93	0.53	1.70	25.71	0.00	25.71	4.000	No	Yes	2.00
66	1.32	1.58	96.47	2.92	0.53	1.70	26.04	0.00	26.04	4.000	No	Yes	2.00
67	1.34	1.62	95.00	2.90	0.52	1.70	27.16	0.00	27.16	4.000	No	Yes	2.00
68	1.36	1.70	92.78	2.87	0.52	1.70	28.16	0.00	28.16	4.000	No	Yes	2.00
69	1.38	1.78	90.28	2.84	0.52	1.70	29.59	0.00	29.59	4.000	No	Yes	2.00
70	1.40	1.85	88.39	2.82	0.51	1.70	31.33	0.00	31.33	4.000	No	Yes	2.00
71	1.44	1.89	87.39	2.80	0.51	1.70	31.64	0.00	31.64	4.000	No	Yes	2.00
72	1.44	1.96	85.85	2.79	0.51	1.70	31.64	0.00	31.64	4.000	No	Yes	2.00
73	1.51	2.01	84.56	2.77	0.50	1.70	34.51	0.00	34.51	4.000	No	Yes	2.00
74	1.51	2.07	83.25	2.75	0.50	1.70	34.51	0.00	34.51	4.000	No	Yes	2.00
75	1.51	2.15	83.20	2.75	0.50	1.70	34.59	0.00	34.59	4.000	No	Yes	2.00
76	1.52	2.22	83.81	2.76	0.49	1.70	38.36	0.00	38.36	4.000	No	Yes	2.00
77	1.54	2.27	85.51	2.78	0.49	1.70	38.25	0.00	38.25	4.000	No	Yes	2.00
78	1.56	2.26	87.34	2.80	0.50	1.70	37.08	0.00	37.08	4.000	No	Yes	2.00
79	1.58	2.25	88.58	2.82	0.49	1.70	37.56	0.00	37.56	4.000	No	Yes	2.00
80	1.60	2.28	88.57	2.82	0.49	1.70	37.84	0.00	37.84	4.000	No	Yes	2.00
81	1.62	2.30	88.41	2.82	0.49	1.70	38.48	0.00	38.48	4.000	No	Yes	2.00
82	1.64	2.34	87.78	2.81	0.49	1.70	38.76	0.00	38.76	4.000	No	Yes	2.00
83	1.66	2.34	87.45	2.81	0.49	1.70	39.47	0.00	39.47	4.000	No	Yes	2.00
84	1.68	2.35	87.38	2.80	0.49	1.70	38.92	0.00	38.92	4.000	No	Yes	2.00
85	1.70	2.32	88.28	2.82	0.49	1.70	38.88	0.00	38.88	4.000	No	Yes	2.00
86	1.72	2.29	89.30	2.83	0.49	1.70	38.17	0.00	38.17	4.000	No	Yes	2.00
87	1.74	2.25	90.61	2.85	0.49	1.70	37.54	0.00	37.54	4.000	No	Yes	2.00
88	1.76	2.22	91.50	2.86	0.50	1.70	36.79	0.00	36.79	4.000	No	Yes	2.00
89	1.78	2.20	92.15	2.86	0.50	1.70	36.75	0.00	36.75	4.000	No	Yes	2.00
90	1.81	2.19	92.36	2.87	0.50	1.70	36.47	0.00	36.47	4.000	No	Yes	2.00
91	1.82	2.17	92.32	2.87	0.50	1.70	36.12	0.00	36.12	4.000	No	Yes	2.00
92	1.84	2.15	92.21	2.87	0.50	1.70	35.72	0.00	35.72	4.000	No	Yes	2.00
93	1.86	2.13	91.95	2.86	0.50	1.70	35.37	0.00	35.37	4.000	No	Yes	2.00
94	1.88	2.11	92.04	2.86	0.50	1.70	35.25	0.00	35.25	4.000	No	Yes	2.00
95	1.90	2.09	92.32	2.87	0.50	1.70	34.50	0.00	34.50	4.000	No	Yes	2.00
96	1.92	2.08	92.46	2.87	0.50	1.70	34.58	0.00	34.58	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
97	1.94	2.06	93.08	2.88	0.50	1.69	34.59	0.00	34.59	4.000	No	Yes	2.00
98	1.97	2.03	93.82	2.89	0.51	1.69	33.18	0.00	33.18	4.000	No	Yes	2.00
99	1.98	1.98	94.71	2.90	0.51	1.69	32.56	0.00	32.56	4.000	No	Yes	2.00
100	2.00	1.94	95.02	2.90	0.51	1.68	31.93	0.00	31.93	4.000	No	Yes	2.00
101	2.02	1.91	94.96	2.90	0.51	1.67	31.20	0.00	31.20	4.000	No	Yes	2.00
102	2.04	1.88	95.10	2.90	0.51	1.67	30.68	0.00	30.68	4.000	No	Yes	2.00
103	2.06	1.83	95.61	2.91	0.51	1.66	29.88	0.00	29.88	4.000	No	Yes	2.00
104	2.08	1.76	96.67	2.92	0.52	1.66	28.52	0.00	28.52	4.000	No	Yes	2.00
105	2.10	1.69	98.33	2.94	0.52	1.66	27.22	0.00	27.22	4.000	No	Yes	2.00
106	2.13	1.63	99.94	2.96	0.53	1.65	26.12	0.00	26.12	4.000	No	Yes	2.00
107	2.14	1.63	99.87	2.96	0.53	1.65	25.55	0.00	25.55	4.000	No	Yes	2.00
108	2.16	1.65	99.12	2.95	0.52	1.63	26.75	0.00	26.75	4.000	No	Yes	2.00
109	2.18	1.66	98.39	2.94	0.52	1.63	26.55	0.00	26.55	4.000	No	Yes	2.00
110	2.20	1.62	98.85	2.95	0.53	1.62	25.64	0.00	25.64	4.000	No	Yes	2.00
111	2.22	1.58	99.73	2.96	0.53	1.62	25.03	0.00	25.03	4.000	No	Yes	2.00
112	2.24	1.53	100.00	2.97	0.53	1.62	24.23	0.00	24.23	4.000	No	Yes	2.00
113	2.26	1.49	100.00	2.98	0.53	1.62	23.35	0.00	23.35	4.000	No	Yes	2.00
114	2.28	1.46	100.00	2.99	0.54	1.62	22.97	0.00	22.97	4.000	No	Yes	2.00
115	2.30	1.44	100.00	2.99	0.54	1.62	22.79	0.00	22.79	4.000	No	Yes	2.00
116	2.32	1.43	100.00	2.99	0.54	1.62	22.45	0.00	22.45	4.000	No	Yes	2.00
117	2.34	1.42	100.00	2.99	0.54	1.61	22.10	0.00	22.10	4.000	No	Yes	2.00
118	2.36	1.41	100.00	2.99	0.54	1.61	22.21	0.00	22.21	4.000	No	Yes	2.00
119	2.38	1.42	100.00	2.98	0.54	1.61	22.01	0.00	22.01	4.000	No	Yes	2.00
120	2.40	1.41	100.00	2.96	0.54	1.60	21.95	0.00	21.95	4.000	No	Yes	2.00
121	2.42	1.41	99.04	2.95	0.54	1.60	21.79	0.00	21.79	4.000	No	Yes	2.00
122	2.45	1.41	97.98	2.94	0.54	1.60	21.78	0.00	21.78	4.000	No	Yes	2.00
123	2.46	1.40	97.39	2.93	0.54	1.60	21.78	0.00	21.78	4.000	No	Yes	2.00
124	2.48	1.37	97.77	2.93	0.54	1.59	21.27	0.00	21.27	4.000	No	Yes	2.00
125	2.50	1.32	98.89	2.95	0.54	1.59	20.41	0.00	20.41	4.000	No	Yes	2.00
126	2.52	1.27	100.00	2.97	0.55	1.59	19.70	0.00	19.70	4.000	No	Yes	2.00
127	2.54	1.22	100.00	2.99	0.55	1.59	18.99	0.00	18.99	4.000	No	Yes	2.00
128	2.56	1.17	100.00	3.02	0.55	1.60	17.93	0.00	17.93	4.000	No	Yes	2.00
129	2.58	1.12	100.00	3.05	0.56	1.60	17.29	0.00	17.29	4.000	No	Yes	2.00
130	2.60	1.10	100.00	3.06	0.56	1.59	17.01	0.00	17.01	4.000	No	Yes	2.00
131	2.62	1.08	100.00	3.07	0.56	1.59	16.62	0.00	16.62	4.000	No	Yes	2.00
132	2.64	1.05	100.00	3.08	0.56	1.59	16.16	0.00	16.16	4.000	No	Yes	2.00
133	2.66	1.02	100.00	3.09	0.56	1.59	15.85	0.00	15.85	4.000	No	Yes	2.00
134	2.68	1.00	100.00	3.10	0.56	1.59	15.22	0.00	15.22	4.000	No	Yes	2.00
135	2.70	0.98	100.00	3.11	0.56	1.59	15.08	0.00	15.08	4.000	No	Yes	2.00
136	2.72	0.96	100.00	3.12	0.56	1.58	14.73	0.00	14.73	4.000	No	Yes	2.00
137	2.74	0.93	100.00	3.14	0.57	1.58	14.18	0.00	14.18	4.000	No	Yes	2.00
138	2.76	0.90	100.00	3.15	0.57	1.58	13.62	0.00	13.62	4.000	No	Yes	2.00
139	2.78	0.87	100.00	3.17	0.57	1.58	13.35	0.00	13.35	4.000	No	Yes	2.00
140	2.80	0.85	100.00	3.17	0.57	1.58	12.76	0.00	12.76	4.000	No	Yes	2.00
141	2.82	0.83	100.00	3.18	0.57	1.58	12.59	0.00	12.59	4.000	No	Yes	2.00
142	2.84	0.82	100.00	3.17	0.57	1.58	12.32	0.00	12.32	4.000	No	Yes	2.00
143	2.86	0.81	100.00	3.17	0.57	1.57	12.26	0.00	12.26	4.000	No	Yes	2.00
144	2.88	0.82	100.00	3.15	0.57	1.57	12.24	0.00	12.24	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
145	2.90	0.82	100.00	3.14	0.57	1.57	12.55	0.00	12.55	4.000	No	Yes	2.00
146	2.92	0.83	100.00	3.13	0.57	1.56	12.39	0.00	12.39	4.000	No	Yes	2.00
147	2.94	0.82	100.00	3.13	0.57	1.56	12.44	0.00	12.44	4.000	No	Yes	2.00
148	2.97	0.82	100.00	3.13	0.57	1.56	12.13	0.00	12.13	4.000	No	Yes	2.00
149	2.98	0.81	100.00	3.14	0.57	1.56	12.18	0.00	12.18	4.000	No	Yes	2.00
150	3.00	0.80	100.00	3.15	0.57	1.55	11.95	0.00	11.95	4.000	No	Yes	2.00
151	3.02	0.79	100.00	3.16	0.58	1.55	11.72	0.00	11.72	4.000	No	Yes	2.00
152	3.04	0.80	100.00	3.16	0.58	1.55	11.87	0.00	11.87	4.000	No	Yes	2.00
153	3.07	0.80	100.00	3.15	0.57	1.54	11.97	0.00	11.97	4.000	No	Yes	2.00
154	3.08	0.82	100.00	3.14	0.57	1.54	12.06	0.00	12.06	4.000	No	Yes	2.00
155	3.10	0.82	100.00	3.13	0.57	1.54	12.27	0.00	12.27	4.000	No	Yes	2.00
156	3.12	0.83	100.00	3.12	0.57	1.54	12.21	0.00	12.21	4.000	No	Yes	2.00
157	3.14	0.84	100.00	3.11	0.57	1.53	12.22	0.00	12.22	4.000	No	Yes	2.00
158	3.16	0.84	100.00	3.10	0.57	1.53	12.57	0.00	12.57	4.000	No	Yes	2.00
159	3.18	0.84	100.00	3.11	0.57	1.53	12.24	0.00	12.24	4.000	No	Yes	2.00
160	3.21	0.82	100.00	3.12	0.57	1.52	12.03	0.00	12.03	4.000	No	Yes	2.00
161	3.22	0.80	100.00	3.14	0.58	1.52	11.75	0.00	11.75	4.000	No	Yes	2.00
162	3.24	0.79	100.00	3.16	0.58	1.52	11.52	0.00	11.52	4.000	No	Yes	2.00
163	3.26	0.77	100.00	3.17	0.58	1.52	11.36	0.00	11.36	4.000	No	Yes	2.00
164	3.28	0.77	100.00	3.18	0.58	1.52	11.13	0.00	11.13	4.000	No	Yes	2.00
165	3.30	0.76	100.00	3.19	0.58	1.52	11.13	0.00	11.13	4.000	No	Yes	2.00
166	3.32	0.75	100.00	3.20	0.58	1.51	10.94	0.00	10.94	4.000	No	Yes	2.00
167	3.34	0.75	100.00	3.20	0.58	1.51	10.81	0.00	10.81	4.000	No	Yes	2.00
168	3.36	0.76	100.00	3.19	0.58	1.51	11.12	0.00	11.12	4.000	No	Yes	2.00
169	3.38	0.77	100.00	3.19	0.58	1.50	11.26	0.00	11.26	4.000	No	Yes	2.00
170	3.40	0.77	100.00	3.18	0.58	1.50	11.00	0.00	11.00	4.000	No	Yes	2.00
171	3.42	0.76	100.00	3.18	0.58	1.50	11.00	0.00	11.00	4.000	No	Yes	2.00
172	3.44	0.76	100.00	3.18	0.58	1.50	10.88	0.00	10.88	4.000	No	Yes	2.00
173	3.48	0.74	100.00	3.19	0.58	1.49	10.70	0.00	10.70	4.000	No	Yes	2.00
174	3.49	0.73	100.00	3.20	0.58	1.49	10.38	0.00	10.38	4.000	No	Yes	2.00
175	3.50	0.69	100.00	3.23	0.58	1.49	10.10	0.00	10.10	4.000	No	Yes	2.00
176	3.52	0.66	100.00	3.27	0.59	1.49	9.27	0.00	9.27	4.000	No	Yes	2.00
177	3.54	0.62	100.00	3.31	0.59	1.49	8.74	0.00	8.74	4.000	No	Yes	2.00
178	3.56	0.60	100.00	3.33	0.59	1.49	8.58	0.00	8.58	4.000	No	Yes	2.00
179	3.58	0.58	100.00	3.34	0.59	1.49	8.20	0.00	8.20	4.000	No	Yes	2.00
180	3.60	0.57	100.00	3.35	0.59	1.49	8.04	0.00	8.04	4.000	No	Yes	2.00
181	3.62	0.56	100.00	3.36	0.59	1.49	7.95	0.00	7.95	4.000	No	Yes	2.00
182	3.64	0.55	100.00	3.37	0.59	1.49	7.70	0.00	7.70	4.000	No	Yes	2.00
183	3.66	0.56	100.00	3.36	0.59	1.48	7.65	0.00	7.65	4.000	No	Yes	2.00
184	3.68	0.59	100.00	3.32	0.59	1.48	8.13	0.00	8.13	4.000	No	Yes	2.00
185	3.70	0.68	100.00	3.21	0.59	1.47	9.04	0.00	9.04	4.000	No	Yes	2.00
186	3.72	0.79	100.00	3.11	0.58	1.46	11.15	0.00	11.15	4.000	No	Yes	2.00
187	3.74	0.89	100.00	3.01	0.57	1.46	12.62	0.00	12.62	4.000	No	Yes	2.00
188	3.76	0.94	100.00	2.97	0.57	1.45	13.27	0.00	13.27	4.000	No	Yes	2.00
189	3.78	0.95	99.17	2.95	0.57	1.45	13.25	0.00	13.25	4.000	No	Yes	2.00
190	3.80	0.92	100.00	2.98	0.57	1.45	13.03	0.00	13.03	4.000	No	Yes	2.00
191	3.82	0.89	100.00	3.02	0.57	1.45	12.13	0.00	12.13	4.000	No	Yes	2.00
192	3.84	0.85	100.00	3.06	0.58	1.45	11.75	0.00	11.75	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
193	3.86	0.85	100.00	3.08	0.58	1.45	11.47	0.00	11.47	4.000	No	Yes	2.00
194	3.88	0.87	100.00	3.08	0.57	1.44	12.27	0.00	12.27	4.000	No	Yes	2.00
195	3.90	0.92	100.00	3.06	0.57	1.44	12.48	0.00	12.48	4.000	No	Yes	2.00
196	3.92	0.96	100.00	3.04	0.57	1.43	13.32	0.00	13.32	4.000	No	Yes	2.00
197	3.94	1.01	100.00	3.01	0.57	1.43	13.90	0.00	13.90	4.000	No	Yes	2.00
198	3.96	1.04	100.00	3.00	0.57	1.42	14.32	0.00	14.32	4.000	No	Yes	2.00
199	3.98	1.04	100.00	3.01	0.57	1.42	14.45	0.00	14.45	4.000	No	Yes	2.00
200	4.00	1.02	100.00	3.03	0.57	1.42	13.98	0.00	13.98	4.000	No	Yes	2.00
201	4.02	0.96	100.00	3.08	0.57	1.42	13.39	0.00	13.39	4.000	No	Yes	2.00
202	4.04	0.91	100.00	3.12	0.57	1.42	12.16	0.00	12.16	4.000	No	Yes	2.00
203	4.06	0.86	100.00	3.16	0.58	1.42	11.75	0.00	11.75	4.000	No	Yes	2.00
204	4.08	0.82	100.00	3.20	0.58	1.42	11.19	0.00	11.19	4.000	No	Yes	2.00
205	4.10	0.78	100.00	3.24	0.58	1.42	10.62	0.00	10.62	4.000	No	Yes	2.00
206	4.12	0.75	100.00	3.27	0.58	1.42	9.86	0.00	9.86	4.000	No	Yes	2.00
207	4.14	0.72	100.00	3.28	0.58	1.42	9.55	0.00	9.55	4.000	No	Yes	2.00
208	4.16	0.71	100.00	3.26	0.58	1.42	9.41	0.00	9.41	4.000	No	Yes	2.00
209	4.18	0.69	100.00	3.25	0.58	1.41	9.39	0.00	9.39	4.000	No	Yes	2.00
210	4.20	0.68	100.00	3.23	0.59	1.41	8.92	0.00	8.92	4.000	No	Yes	2.00
211	4.22	0.69	100.00	3.19	0.59	1.41	9.02	0.00	9.02	4.000	No	Yes	2.00
212	4.25	0.70	100.00	3.15	0.59	1.41	9.25	0.00	9.25	4.000	No	Yes	2.00
213	4.26	0.72	100.00	3.11	0.58	1.41	9.30	0.00	9.30	4.000	No	Yes	2.00
214	4.28	0.73	100.00	3.08	0.58	1.40	9.57	0.00	9.57	4.000	No	Yes	2.00
215	4.30	0.75	100.00	3.05	0.58	1.40	9.83	0.00	9.83	4.000	No	Yes	2.00
216	4.32	0.77	100.00	3.03	0.58	1.40	9.97	0.00	9.97	4.000	No	Yes	2.00
217	4.34	0.81	100.00	2.99	0.58	1.40	10.14	0.00	10.14	4.000	No	Yes	2.00
218	4.36	0.85	97.83	2.94	0.58	1.39	11.25	0.00	11.25	4.000	No	Yes	2.00
219	4.38	0.87	96.07	2.91	0.58	1.39	11.80	0.00	11.80	4.000	No	Yes	2.00
220	4.40	0.85	97.67	2.93	0.58	1.39	11.28	0.00	11.28	4.000	No	Yes	2.00
221	4.42	0.81	100.00	2.98	0.58	1.39	10.76	0.00	10.76	4.000	No	Yes	2.00
222	4.44	0.80	100.00	3.01	0.58	1.39	10.28	0.00	10.28	4.000	No	Yes	2.00
223	4.47	0.82	100.00	3.01	0.58	1.38	10.35	0.00	10.35	4.000	No	Yes	2.00
224	4.48	0.87	100.00	2.99	0.58	1.38	10.87	0.00	10.87	4.000	No	Yes	2.00
225	4.50	0.93	98.28	2.94	0.58	1.38	11.88	0.00	11.88	4.000	No	Yes	2.00
226	4.52	1.00	94.93	2.90	0.57	1.37	12.94	0.00	12.94	4.000	No	Yes	2.00
227	4.54	1.05	92.44	2.87	0.57	1.37	13.54	0.00	13.54	4.000	No	Yes	2.00
228	4.56	1.08	91.30	2.85	0.57	1.36	14.01	0.00	14.01	4.000	No	Yes	2.00
229	4.59	1.13	88.71	2.82	0.57	1.36	13.99	0.00	13.99	4.000	No	Yes	2.00
230	4.60	1.18	86.42	2.79	0.57	1.36	15.35	0.00	15.35	4.000	No	Yes	2.00
231	4.62	1.23	84.70	2.77	0.56	1.35	16.09	0.00	16.09	4.000	No	Yes	2.00
232	4.64	1.26	85.00	2.77	0.56	1.35	16.10	0.00	16.10	4.000	No	Yes	2.00
233	4.66	1.31	85.41	2.78	0.56	1.35	16.62	0.00	16.62	4.000	No	Yes	2.00
234	4.68	1.36	85.18	2.78	0.56	1.35	17.53	0.00	17.53	4.000	No	Yes	2.00
235	4.70	1.40	84.97	2.77	0.56	1.34	18.23	0.00	18.23	4.000	No	Yes	2.00
236	4.72	1.44	85.50	2.78	0.55	1.34	18.71	0.00	18.71	4.000	No	Yes	2.00
237	4.74	1.48	86.17	2.79	0.55	1.34	19.13	0.00	19.13	4.000	No	Yes	2.00
238	4.76	1.52	86.80	2.80	0.55	1.33	19.85	0.00	19.85	4.000	No	Yes	2.00
239	4.78	1.54	88.14	2.81	0.55	1.33	20.23	0.00	20.23	4.000	No	Yes	2.00
240	4.80	1.53	90.33	2.84	0.55	1.33	19.95	0.00	19.95	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
241	4.82	1.48	93.75	2.88	0.55	1.32	19.46	0.00	19.46	4.000	No	Yes	2.00
242	4.84	1.41	97.49	2.93	0.55	1.32	18.50	0.00	18.50	4.000	No	Yes	2.00
243	4.86	1.37	100.00	2.96	0.56	1.33	17.09	0.00	17.09	4.000	No	Yes	2.00
244	4.88	1.37	100.00	2.97	0.55	1.32	17.54	0.00	17.54	4.000	No	Yes	2.00
245	4.90	1.40	99.28	2.95	0.55	1.32	18.14	0.00	18.14	4.000	No	Yes	2.00
246	4.92	1.43	97.55	2.93	0.55	1.32	18.18	0.00	18.18	4.000	No	Yes	2.00
247	4.94	1.43	96.92	2.92	0.55	1.31	18.77	0.00	18.77	4.000	No	Yes	2.00
248	4.97	1.42	96.61	2.92	0.55	1.31	18.16	0.00	18.16	4.000	No	Yes	2.00
249	4.98	1.39	97.03	2.93	0.55	1.31	17.85	0.00	17.85	4.000	No	Yes	2.00
250	5.00	1.37	97.88	2.94	0.55	1.31	17.75	0.00	17.75	4.000	No	Yes	2.00
251	5.02	1.34	99.51	2.96	0.56	1.31	17.22	0.00	17.22	4.000	No	Yes	2.00
252	5.04	1.30	100.00	2.98	0.56	1.31	16.62	0.00	16.62	4.000	No	Yes	2.00
253	5.07	1.27	100.00	3.01	0.56	1.31	16.38	0.00	16.38	4.000	No	Yes	2.00
254	5.08	1.25	100.00	3.02	0.56	1.31	15.88	0.00	15.88	4.000	No	Yes	2.00
255	5.10	1.25	100.00	3.02	0.56	1.30	16.02	0.00	16.02	4.000	No	Yes	2.00
256	5.12	1.25	100.00	3.02	0.56	1.30	16.14	0.00	16.14	4.000	No	Yes	2.00
257	5.14	1.23	100.00	3.02	0.56	1.30	15.79	0.00	15.79	4.000	No	Yes	2.00
258	5.16	1.21	100.00	3.04	0.56	1.30	15.26	0.00	15.26	4.000	No	Yes	2.00
259	5.18	1.17	100.00	3.06	0.56	1.30	15.02	0.00	15.02	4.000	No	Yes	2.00
260	5.21	1.12	100.00	3.07	0.57	1.30	14.16	0.00	14.16	4.000	No	Yes	2.00
261	5.22	1.08	100.00	3.09	0.57	1.30	13.59	0.00	13.59	4.000	No	Yes	2.00
262	5.24	1.05	100.00	3.10	0.57	1.30	13.27	0.00	13.27	4.000	No	Yes	2.00
263	5.26	1.03	100.00	3.11	0.57	1.30	12.98	0.00	12.98	4.000	No	Yes	2.00
264	5.28	1.02	100.00	3.10	0.57	1.29	12.63	0.00	12.63	4.000	No	Yes	2.00
265	5.30	1.03	100.00	3.08	0.57	1.29	12.84	0.00	12.84	4.000	No	Yes	2.00
266	5.32	1.05	100.00	3.04	0.57	1.29	13.05	0.00	13.05	4.000	No	Yes	2.00
267	5.34	1.08	100.00	3.01	0.57	1.29	13.26	0.00	13.26	4.000	No	Yes	2.00
268	5.36	1.10	100.00	2.98	0.57	1.29	13.58	0.00	13.58	4.000	No	Yes	2.00
269	5.38	1.12	99.88	2.96	0.57	1.28	13.91	0.00	13.91	4.000	No	Yes	2.00
270	5.40	1.14	99.02	2.95	0.57	1.28	13.95	0.00	13.95	4.000	No	Yes	2.00
271	5.42	1.15	98.69	2.95	0.57	1.28	14.13	0.00	14.13	4.000	No	Yes	2.00
272	5.44	1.17	98.43	2.94	0.57	1.28	14.25	0.00	14.25	4.000	No	Yes	2.00
273	5.46	1.18	98.28	2.94	0.57	1.28	14.43	0.00	14.43	4.000	No	Yes	2.00
274	5.52	1.19	98.43	2.94	0.57	1.27	14.54	0.00	14.54	4.000	No	Yes	2.00
275	5.52	1.19	98.46	2.94	0.57	1.27	14.54	0.00	14.54	4.000	No	Yes	2.00
276	5.52	1.22	97.58	2.93	0.57	1.27	14.43	0.00	14.43	4.000	No	Yes	2.00
277	5.54	1.25	96.62	2.92	0.56	1.27	15.44	0.00	15.44	4.000	No	Yes	2.00
278	5.56	1.30	95.36	2.90	0.56	1.26	15.83	0.00	15.83	4.000	No	Yes	2.00
279	5.58	1.34	94.57	2.89	0.56	1.26	16.15	0.00	16.15	4.000	No	Yes	2.00
280	5.60	1.37	94.25	2.89	0.56	1.26	16.73	0.00	16.73	4.000	No	Yes	2.00
281	5.62	1.39	94.37	2.89	0.56	1.26	16.85	0.00	16.85	4.000	No	Yes	2.00
282	5.64	1.40	95.12	2.90	0.56	1.26	16.94	0.00	16.94	4.000	No	Yes	2.00
283	5.66	1.39	96.54	2.92	0.56	1.25	16.94	0.00	16.94	4.000	No	Yes	2.00
284	5.68	1.38	97.74	2.93	0.56	1.25	16.46	0.00	16.46	4.000	No	Yes	2.00
285	5.70	1.36	99.53	2.96	0.56	1.25	16.66	0.00	16.66	4.000	No	Yes	2.00
286	5.72	1.36	100.00	2.97	0.56	1.25	16.27	0.00	16.27	4.000	No	Yes	2.00
287	5.74	1.33	100.00	3.00	0.56	1.25	16.16	0.00	16.16	4.000	No	Yes	2.00
288	5.76	1.31	100.00	3.02	0.56	1.25	15.74	0.00	15.74	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
289	5.78	1.28	100.00	3.05	0.56	1.25	15.44	0.00	15.44	4.000	No	Yes	2.00
290	5.80	1.26	100.00	3.06	0.56	1.25	14.99	0.00	14.99	4.000	No	Yes	2.00
291	5.82	1.23	100.00	3.08	0.56	1.24	14.77	0.00	14.77	4.000	No	Yes	2.00
292	5.84	1.22	100.00	3.08	0.57	1.24	14.52	0.00	14.52	4.000	No	Yes	2.00
293	5.86	1.23	100.00	3.07	0.56	1.24	14.57	0.00	14.57	4.000	No	Yes	2.00
294	5.88	1.23	100.00	3.06	0.56	1.24	14.76	0.00	14.76	4.000	No	Yes	2.00
295	5.90	1.23	100.00	3.05	0.56	1.24	14.65	0.00	14.65	4.000	No	Yes	2.00
296	5.92	1.21	100.00	3.06	0.57	1.24	14.52	0.00	14.52	4.000	No	Yes	2.00
297	5.94	1.18	100.00	3.08	0.57	1.24	13.91	0.00	13.91	4.000	No	Yes	2.00
298	5.96	1.14	100.00	3.10	0.57	1.23	13.39	0.00	13.39	4.000	No	Yes	2.00
299	5.98	1.12	100.00	3.11	0.57	1.23	13.14	0.00	13.14	4.000	No	Yes	2.00
300	6.01	1.13	100.00	3.10	0.57	1.23	13.09	0.00	13.09	4.000	No	Yes	2.00
301	6.02	1.14	100.00	3.08	0.57	1.23	13.63	0.00	13.63	4.000	No	Yes	2.00
302	6.04	1.15	100.00	3.06	0.57	1.23	13.69	0.00	13.69	4.000	No	Yes	2.00
303	6.07	1.12	100.00	3.08	0.57	1.23	13.44	0.00	13.44	4.000	No	Yes	2.00
304	6.08	1.09	100.00	3.11	0.57	1.23	12.90	0.00	12.90	4.000	No	Yes	2.00
305	6.10	1.04	100.00	3.14	0.57	1.23	12.41	0.00	12.41	4.000	No	Yes	2.00
306	6.12	1.01	100.00	3.18	0.58	1.22	11.87	0.00	11.87	4.000	No	Yes	2.00
307	6.14	0.98	100.00	3.21	0.58	1.22	11.62	0.00	11.62	4.000	No	Yes	2.00
308	6.16	0.96	100.00	3.22	0.58	1.22	11.36	0.00	11.36	4.000	No	Yes	2.00
309	6.18	0.94	100.00	3.23	0.58	1.22	11.14	0.00	11.14	4.000	No	Yes	2.00
310	6.20	0.92	100.00	3.23	0.58	1.22	10.85	0.00	10.85	4.000	No	Yes	2.00
311	6.22	0.89	100.00	3.23	0.58	1.22	10.47	0.00	10.47	4.000	No	Yes	2.00
312	6.24	0.87	100.00	3.22	0.58	1.22	10.12	0.00	10.12	4.000	No	Yes	2.00
313	6.26	0.85	100.00	3.22	0.58	1.22	10.14	0.00	10.14	4.000	No	Yes	2.00
314	6.28	0.83	100.00	3.22	0.58	1.22	9.76	0.00	9.76	4.000	No	Yes	2.00
315	6.30	0.81	100.00	3.22	0.59	1.21	9.28	0.00	9.28	4.000	No	Yes	2.00
316	6.32	0.82	100.00	3.21	0.58	1.21	9.46	0.00	9.46	4.000	No	Yes	2.00
317	6.34	0.85	100.00	3.16	0.58	1.21	9.86	0.00	9.86	4.000	No	Yes	2.00
318	6.36	0.89	100.00	3.12	0.58	1.21	10.37	0.00	10.37	4.000	No	Yes	2.00
319	6.38	0.91	100.00	3.09	0.58	1.21	10.55	0.00	10.55	4.000	No	Yes	2.00
320	6.40	0.94	100.00	3.06	0.58	1.21	10.59	0.00	10.59	4.000	No	Yes	2.00
321	6.42	0.96	100.00	3.03	0.58	1.20	11.18	0.00	11.18	4.000	No	Yes	2.00
322	6.44	0.99	100.00	2.99	0.58	1.20	11.22	0.00	11.22	4.000	No	Yes	2.00
323	6.46	1.01	100.00	2.98	0.58	1.20	11.60	0.00	11.60	4.000	No	Yes	2.00
324	6.48	1.01	100.00	2.97	0.58	1.20	11.62	0.00	11.62	4.000	No	Yes	2.00
325	6.50	0.98	100.00	3.00	0.58	1.20	11.25	0.00	11.25	4.000	No	Yes	2.00
326	6.52	0.96	100.00	3.03	0.58	1.20	10.86	0.00	10.86	4.000	No	Yes	2.00
327	6.54	0.93	100.00	3.07	0.58	1.20	10.75	0.00	10.75	4.000	No	Yes	2.00
328	6.56	0.90	100.00	3.10	0.58	1.20	10.28	0.00	10.28	4.000	No	Yes	2.00
329	6.58	0.88	100.00	3.14	0.58	1.19	9.97	0.00	9.97	4.000	No	Yes	2.00
330	6.60	0.87	100.00	3.17	0.58	1.19	9.93	0.00	9.93	4.000	No	Yes	2.00
331	6.62	0.88	100.00	3.17	0.58	1.19	9.87	0.00	9.87	4.000	No	Yes	2.00
332	6.64	0.89	100.00	3.16	0.58	1.19	9.92	0.00	9.92	4.000	No	Yes	2.00
333	6.66	0.90	100.00	3.13	0.58	1.19	10.15	0.00	10.15	4.000	No	Yes	2.00
334	6.69	0.92	100.00	3.11	0.58	1.19	10.41	0.00	10.41	4.000	No	Yes	2.00
335	6.70	0.92	100.00	3.09	0.58	1.19	10.38	0.00	10.38	4.000	No	Yes	2.00
336	6.72	0.92	100.00	3.09	0.58	1.18	10.35	0.00	10.35	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
337	6.74	0.91	100.00	3.09	0.58	1.18	10.20	0.00	10.20	4.000	No	Yes	2.00
338	6.76	0.91	100.00	3.09	0.58	1.18	10.14	0.00	10.14	4.000	No	Yes	2.00
339	6.78	0.89	100.00	3.11	0.58	1.18	10.13	0.00	10.13	4.000	No	Yes	2.00
340	6.80	0.87	100.00	3.14	0.58	1.18	9.75	0.00	9.75	4.000	No	Yes	2.00
341	6.82	0.83	100.00	3.18	0.59	1.18	9.26	0.00	9.26	4.000	No	Yes	2.00
342	6.84	0.80	100.00	3.20	0.59	1.18	8.74	0.00	8.74	4.000	No	Yes	2.00
343	6.86	0.77	100.00	3.23	0.59	1.18	8.82	0.00	8.82	4.000	No	Yes	2.00
344	6.88	0.75	100.00	3.25	0.59	1.18	8.19	0.00	8.19	4.000	No	Yes	2.00
345	6.90	0.72	100.00	3.28	0.59	1.18	7.95	0.00	7.95	4.000	No	Yes	2.00
346	6.92	0.73	100.00	3.27	0.59	1.17	7.89	0.00	7.89	4.000	No	Yes	2.00
347	6.94	0.76	100.00	3.24	0.59	1.17	8.38	0.00	8.38	4.000	No	Yes	2.00
348	6.96	0.77	100.00	3.22	0.59	1.17	8.69	0.00	8.69	4.000	No	Yes	2.00
349	6.98	0.76	100.00	3.21	0.59	1.17	8.34	0.00	8.34	4.000	No	Yes	2.00
350	7.00	0.74	100.00	3.21	0.59	1.17	8.06	0.00	8.06	4.000	No	Yes	2.00
351	7.02	0.76	100.00	3.16	0.59	1.17	7.92	0.00	7.92	4.000	No	Yes	2.00
352	7.04	0.81	100.00	3.07	0.59	1.17	8.76	0.00	8.76	4.000	No	Yes	2.00
353	7.06	0.88	100.00	2.99	0.58	1.16	9.60	0.00	9.60	4.000	No	Yes	2.00
354	7.08	0.97	96.61	2.92	0.58	1.16	10.37	0.00	10.37	4.000	No	Yes	2.00
355	7.10	1.04	93.53	2.88	0.58	1.16	11.76	0.00	11.76	4.000	No	Yes	2.00
356	7.12	1.13	91.15	2.85	0.58	1.16	12.14	0.00	12.14	4.000	No	Yes	2.00
357	7.14	1.18	91.21	2.85	0.57	1.16	13.40	0.00	13.40	4.000	No	Yes	2.00
358	7.16	1.23	93.00	2.87	0.57	1.15	13.80	0.00	13.80	4.000	No	Yes	2.00
359	7.18	1.27	95.73	2.91	0.57	1.15	14.02	0.00	14.02	4.000	No	Yes	2.00
360	7.20	1.32	97.84	2.94	0.57	1.15	14.64	0.00	14.64	4.000	No	Yes	2.00
361	7.22	1.36	99.03	2.95	0.56	1.15	15.14	0.00	15.14	4.000	No	Yes	2.00
362	7.24	1.39	100.00	2.97	0.56	1.15	15.39	0.00	15.39	4.000	No	Yes	2.00
363	7.26	1.41	100.00	2.99	0.56	1.14	15.63	0.00	15.63	4.000	No	Yes	2.00
364	7.28	1.42	100.00	3.01	0.56	1.14	15.82	0.00	15.82	4.000	No	Yes	2.00
365	7.30	1.39	100.00	3.03	0.56	1.14	15.59	0.00	15.59	4.000	No	Yes	2.00
366	7.32	1.35	100.00	3.06	0.56	1.14	14.68	0.00	14.68	4.000	No	Yes	2.00
367	7.34	1.30	100.00	3.08	0.57	1.14	14.40	0.00	14.40	4.000	No	Yes	2.00
368	7.36	1.27	100.00	3.09	0.57	1.14	13.80	0.00	13.80	4.000	No	Yes	2.00
369	7.38	1.27	100.00	3.08	0.57	1.14	13.68	0.00	13.68	4.000	No	Yes	2.00
370	7.40	1.29	100.00	3.06	0.57	1.14	14.05	0.00	14.05	4.000	No	Yes	2.00
371	7.42	1.35	100.00	3.02	0.57	1.14	14.50	0.00	14.50	4.000	No	Yes	2.00
372	7.44	1.40	100.00	2.99	0.56	1.13	15.59	0.00	15.59	4.000	No	Yes	2.00
373	7.46	1.46	100.00	2.97	0.56	1.13	15.99	0.00	15.99	4.000	No	Yes	2.00
374	7.48	1.48	100.00	2.97	0.56	1.13	16.53	0.00	16.53	4.000	No	Yes	2.00
375	7.50	1.52	100.00	2.97	0.56	1.13	16.40	0.00	16.40	4.000	No	Yes	2.00
376	7.52	1.53	100.00	2.98	0.56	1.13	17.25	0.00	17.25	4.000	No	Yes	2.00
377	7.54	1.54	100.00	3.00	0.56	1.13	16.99	0.00	16.99	4.000	No	Yes	2.00
378	7.56	1.51	100.00	3.02	0.56	1.12	16.79	0.00	16.79	4.000	No	Yes	2.00
379	7.58	1.51	100.00	3.04	0.56	1.12	16.42	0.00	16.42	4.000	No	Yes	2.00
380	7.60	1.52	100.00	3.04	0.56	1.12	16.81	0.00	16.81	4.000	No	Yes	2.00
381	7.62	1.55	100.00	3.04	0.56	1.12	17.23	0.00	17.23	4.000	No	Yes	2.00
382	7.64	1.55	100.00	3.04	0.56	1.12	17.17	0.00	17.17	4.000	No	Yes	2.00
383	7.66	1.49	100.00	3.07	0.56	1.12	16.79	0.00	16.79	4.000	No	Yes	2.00
384	7.68	1.40	100.00	3.12	0.56	1.12	15.33	0.00	15.33	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
385	7.70	1.30	100.00	3.17	0.57	1.12	14.25	0.00	14.25	4.000	No	Yes	2.00
386	7.72	1.22	100.00	3.21	0.57	1.12	13.25	0.00	13.25	4.000	No	Yes	2.00
387	7.74	1.16	100.00	3.25	0.57	1.12	12.69	0.00	12.69	4.000	No	Yes	2.00
388	7.76	1.13	100.00	3.27	0.57	1.11	12.11	0.00	12.11	4.000	No	Yes	2.00
389	7.78	1.12	100.00	3.28	0.58	1.11	11.89	0.00	11.89	4.000	No	Yes	2.00
390	7.80	1.12	100.00	3.27	0.57	1.11	11.96	0.00	11.96	4.000	No	Yes	2.00
391	7.82	1.17	100.00	3.22	0.57	1.11	12.09	0.00	12.09	4.000	No	Yes	2.00
392	7.84	1.27	100.00	3.14	0.57	1.11	13.43	0.00	13.43	4.000	No	Yes	2.00
393	7.86	1.41	100.00	3.05	0.56	1.11	15.05	0.00	15.05	4.000	No	Yes	2.00
394	7.88	1.54	100.00	2.99	0.56	1.10	16.58	0.00	16.58	4.000	No	Yes	2.00
395	7.90	1.62	99.47	2.96	0.55	1.10	17.50	0.00	17.50	4.000	No	Yes	2.00
396	7.92	1.64	99.40	2.95	0.55	1.10	17.71	0.00	17.71	4.000	No	Yes	2.00
397	7.94	1.63	100.00	2.97	0.55	1.10	17.44	0.00	17.44	4.000	No	Yes	2.00
398	7.96	1.62	100.00	3.00	0.55	1.10	17.39	0.00	17.39	4.000	No	Yes	2.00
399	7.98	1.62	100.00	3.02	0.56	1.10	17.29	0.00	17.29	4.000	No	Yes	2.00
400	8.00	1.62	100.00	3.04	0.55	1.10	17.42	0.00	17.42	4.000	No	Yes	2.00
401	8.02	1.64	100.00	3.05	0.55	1.09	17.52	0.00	17.52	4.000	No	Yes	2.00
402	8.04	1.65	100.00	3.06	0.55	1.09	17.82	0.00	17.82	4.000	No	Yes	2.00
403	8.06	1.66	100.00	3.06	0.55	1.09	17.75	0.00	17.75	4.000	No	Yes	2.00
404	8.08	1.67	100.00	3.06	0.55	1.09	17.75	0.00	17.75	4.000	No	Yes	2.00
405	8.10	1.70	100.00	3.06	0.55	1.09	18.27	0.00	18.27	4.000	No	Yes	2.00
406	8.12	1.75	100.00	3.04	0.55	1.09	18.69	0.00	18.69	4.000	No	Yes	2.00
407	8.15	1.78	100.00	3.03	0.55	1.09	19.17	0.00	19.17	4.000	No	Yes	2.00
408	8.16	1.82	100.00	3.02	0.55	1.09	19.13	0.00	19.13	4.000	No	Yes	2.00
409	8.18	1.84	100.00	3.02	0.55	1.08	19.85	0.00	19.85	4.000	No	Yes	2.00
410	8.20	1.87	100.00	3.01	0.55	1.08	19.82	0.00	19.82	4.000	No	Yes	2.00
411	8.22	1.87	100.00	3.01	0.55	1.08	19.91	0.00	19.91	4.000	No	Yes	2.00
412	8.24	1.85	100.00	3.01	0.55	1.08	19.65	0.00	19.65	4.000	No	Yes	2.00
413	8.26	1.81	100.00	3.02	0.55	1.08	19.20	0.00	19.20	4.000	No	Yes	2.00
414	8.28	1.76	100.00	3.04	0.55	1.08	18.70	0.00	18.70	4.000	No	Yes	2.00
415	8.30	1.72	100.00	3.05	0.55	1.08	17.90	0.00	17.90	4.000	No	Yes	2.00
416	8.32	1.72	100.00	3.06	0.55	1.08	18.07	0.00	18.07	4.000	No	Yes	2.00
417	8.34	1.74	100.00	3.05	0.55	1.07	18.56	0.00	18.56	4.000	No	Yes	2.00
418	8.36	1.73	100.00	3.06	0.55	1.07	18.53	0.00	18.53	4.000	No	Yes	2.00
419	8.38	1.66	100.00	3.09	0.55	1.07	17.62	0.00	17.62	4.000	No	Yes	2.00
420	8.40	1.58	100.00	3.12	0.56	1.07	16.58	0.00	16.58	4.000	No	Yes	2.00
421	8.42	1.48	100.00	3.17	0.56	1.07	15.89	0.00	15.89	4.000	No	Yes	2.00
422	8.44	1.38	100.00	3.22	0.57	1.07	14.43	0.00	14.43	4.000	No	Yes	2.00
423	8.46	1.27	100.00	3.28	0.57	1.07	13.33	0.00	13.33	4.000	No	Yes	2.00
424	8.48	1.19	100.00	3.32	0.57	1.07	12.39	0.00	12.39	4.000	No	Yes	2.00
425	8.50	1.12	100.00	3.35	0.58	1.07	11.81	0.00	11.81	4.000	No	Yes	2.00
426	8.52	1.08	100.00	3.37	0.58	1.07	11.01	0.00	11.01	4.000	No	Yes	2.00
427	8.54	1.05	100.00	3.36	0.58	1.07	10.92	0.00	10.92	4.000	No	Yes	2.00
428	8.56	1.04	100.00	3.34	0.58	1.07	10.68	0.00	10.68	4.000	No	Yes	2.00
429	8.58	1.01	100.00	3.33	0.58	1.06	10.52	0.00	10.52	4.000	No	Yes	2.00
430	8.60	0.99	100.00	3.31	0.58	1.06	10.00	0.00	10.00	4.000	No	Yes	2.00
431	8.62	0.98	100.00	3.29	0.58	1.06	9.89	0.00	9.89	4.000	No	Yes	2.00
432	8.64	0.98	100.00	3.26	0.58	1.06	9.92	0.00	9.92	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
433	8.66	1.00	100.00	3.23	0.58	1.06	10.06	0.00	10.06	4.000	No	Yes	2.00
434	8.68	1.04	100.00	3.19	0.58	1.06	10.25	0.00	10.25	4.000	No	Yes	2.00
435	8.70	1.12	100.00	3.11	0.58	1.06	11.16	0.00	11.16	4.000	No	Yes	2.00
436	8.72	1.26	100.00	3.02	0.57	1.06	12.62	0.00	12.62	4.000	No	Yes	2.00
437	8.74	1.39	98.31	2.94	0.57	1.05	14.20	0.00	14.20	4.000	No	Yes	2.00
438	8.76	1.51	94.04	2.89	0.56	1.05	15.17	0.00	15.17	4.000	No	Yes	2.00
439	8.78	1.60	91.61	2.86	0.56	1.05	16.23	0.00	16.23	4.000	No	Yes	2.00
440	8.80	1.68	90.35	2.84	0.56	1.05	17.10	0.00	17.10	4.000	No	Yes	2.00
441	8.82	1.76	88.83	2.82	0.56	1.05	17.46	0.00	17.46	4.000	No	Yes	2.00
442	8.84	1.81	88.98	2.82	0.55	1.05	18.59	0.00	18.59	4.000	No	Yes	2.00
443	8.86	1.87	88.65	2.82	0.55	1.05	18.62	0.00	18.62	4.000	No	Yes	2.00
444	8.88	1.92	89.13	2.83	0.55	1.05	19.38	0.00	19.38	4.000	No	Yes	2.00
445	8.90	1.95	90.59	2.84	0.55	1.04	19.94	0.00	19.94	4.000	No	Yes	2.00
446	8.93	1.95	93.46	2.88	0.55	1.04	19.69	0.00	19.69	4.000	No	Yes	2.00
447	8.94	1.93	96.89	2.92	0.55	1.04	19.47	0.00	19.47	4.000	No	Yes	2.00
448	8.96	1.90	100.00	2.96	0.55	1.04	19.47	0.00	19.47	4.000	No	Yes	2.00
449	8.98	1.87	100.00	2.99	0.55	1.04	18.73	0.00	18.73	4.000	No	Yes	2.00
450	9.00	1.84	100.00	3.02	0.55	1.04	18.37	0.00	18.37	4.000	No	Yes	2.00
451	9.02	1.85	100.00	3.02	0.55	1.04	18.37	0.00	18.37	4.000	No	Yes	2.00
452	9.04	1.88	100.00	3.01	0.55	1.04	18.75	0.00	18.75	4.000	No	Yes	2.00
453	9.06	1.91	100.00	2.99	0.55	1.04	19.23	0.00	19.23	4.000	No	Yes	2.00
454	9.08	1.94	100.00	2.97	0.55	1.04	19.34	0.00	19.34	4.000	No	Yes	2.00
455	9.10	1.97	99.83	2.96	0.55	1.03	19.77	0.00	19.77	4.000	No	Yes	2.00
456	9.12	2.00	98.87	2.95	0.55	1.03	20.12	0.00	20.12	4.000	No	Yes	2.00
457	9.14	2.01	98.80	2.95	0.55	1.03	20.22	0.00	20.22	4.000	No	Yes	2.00
458	9.16	2.01	99.26	2.95	0.55	1.03	19.95	0.00	19.95	4.000	No	Yes	2.00
459	9.18	2.00	99.70	2.96	0.55	1.03	20.06	0.00	20.06	4.000	No	Yes	2.00
460	9.20	1.99	100.00	2.97	0.55	1.03	19.99	0.00	19.99	4.000	No	Yes	2.00
461	9.22	1.98	100.00	2.98	0.55	1.03	19.74	0.00	19.74	4.000	No	Yes	2.00
462	9.24	1.98	100.00	2.99	0.55	1.03	19.74	0.00	19.74	4.000	No	Yes	2.00
463	9.26	1.99	100.00	2.99	0.55	1.03	19.78	0.00	19.78	4.000	No	Yes	2.00
464	9.28	2.00	100.00	2.98	0.55	1.02	19.92	0.00	19.92	4.000	No	Yes	2.00
465	9.30	2.01	100.00	2.98	0.55	1.02	20.04	0.00	20.04	4.000	No	Yes	2.00
466	9.32	2.02	100.00	2.98	0.55	1.02	20.12	0.00	20.12	4.000	No	Yes	2.00
467	9.34	2.04	100.00	2.97	0.55	1.02	20.10	0.00	20.10	4.000	No	Yes	2.00
468	9.36	2.09	99.33	2.95	0.54	1.02	20.68	0.00	20.68	4.000	No	Yes	2.00
469	9.38	2.19	96.84	2.92	0.54	1.02	21.22	0.00	21.22	4.000	No	Yes	2.00
470	9.40	2.29	94.37	2.89	0.54	1.02	22.87	0.00	22.87	4.000	No	Yes	2.00
471	9.42	2.35	92.82	2.87	0.54	1.02	23.66	0.00	23.66	4.000	No	Yes	2.00
472	9.44	2.31	93.99	2.89	0.54	1.02	23.00	0.00	23.00	4.000	No	Yes	2.00
473	9.46	2.20	97.72	2.93	0.54	1.02	21.81	0.00	21.81	4.000	No	Yes	2.00
474	9.48	2.06	100.00	2.99	0.54	1.01	20.40	0.00	20.40	4.000	No	Yes	2.00
475	9.50	1.96	100.00	3.04	0.55	1.01	19.12	0.00	19.12	4.000	No	Yes	2.00
476	9.52	1.89	100.00	3.07	0.55	1.01	18.74	0.00	18.74	4.000	No	Yes	2.00
477	9.54	1.86	100.00	3.09	0.55	1.01	18.27	0.00	18.27	4.000	No	Yes	2.00
478	9.56	1.85	100.00	3.10	0.55	1.01	18.29	0.00	18.29	4.000	No	Yes	2.00
479	9.58	1.86	100.00	3.09	0.55	1.01	18.29	0.00	18.29	4.000	No	Yes	2.00
480	9.60	1.88	100.00	3.07	0.55	1.01	18.61	0.00	18.61	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
481	9.62	1.91	100.00	3.05	0.55	1.01	18.66	0.00	18.66	4.000	No	Yes	2.00
482	9.64	1.93	100.00	3.03	0.55	1.01	18.97	0.00	18.97	4.000	No	Yes	2.00
483	9.66	1.94	100.00	3.01	0.55	1.01	19.20	0.00	19.20	4.000	No	Yes	2.00
484	9.68	1.92	100.00	3.01	0.55	1.00	18.89	0.00	18.89	4.000	No	Yes	2.00
485	9.70	1.86	100.00	3.02	0.55	1.00	18.43	0.00	18.43	4.000	No	Yes	2.00
486	9.72	1.76	100.00	3.05	0.55	1.00	17.45	0.00	17.45	4.000	No	Yes	2.00
487	9.74	1.62	100.00	3.11	0.56	1.00	15.94	0.00	15.94	4.000	No	Yes	2.00
488	9.76	1.45	100.00	3.19	0.57	1.00	14.21	0.00	14.21	4.000	No	Yes	2.00
489	9.78	1.30	100.00	3.27	0.57	1.00	12.57	0.00	12.57	4.000	No	Yes	2.00
490	9.80	1.24	100.00	3.30	0.58	1.00	11.56	0.00	11.56	4.000	No	Yes	2.00
491	9.82	1.19	100.00	3.32	0.57	1.00	12.00	0.00	12.00	4.000	No	Yes	2.00
492	9.84	1.16	100.00	3.31	0.58	1.00	11.01	0.00	11.01	4.000	No	Yes	2.00
493	9.86	1.08	100.00	3.33	0.58	1.00	10.34	0.00	10.34	4.000	No	Yes	2.00
494	9.88	1.05	100.00	3.31	0.58	1.00	9.76	0.00	9.76	4.000	No	Yes	2.00
495	9.90	1.05	100.00	3.26	0.58	0.99	9.75	0.00	9.75	4.000	No	Yes	2.00
496	9.92	1.08	100.00	3.19	0.58	0.99	10.42	0.00	10.42	4.000	No	Yes	2.00
497	9.95	1.09	100.00	3.14	0.58	0.99	10.37	0.00	10.37	4.000	No	Yes	2.00
498	9.96	1.06	100.00	3.11	0.58	0.99	9.90	0.00	9.90	4.000	No	Yes	2.00
499	9.98	1.03	100.00	3.10	0.58	0.99	9.62	0.00	9.62	4.000	No	Yes	2.00
500	10.00	1.01	100.00	3.09	0.58	0.99	9.48	0.00	9.48	4.000	No	Yes	2.00
501	10.02	0.98	100.00	3.10	0.59	0.99	9.11	0.00	9.11	4.000	No	Yes	2.00
502	10.04	0.96	100.00	3.11	0.59	0.99	8.77	0.00	8.77	4.000	No	Yes	2.00
503	10.06	0.95	100.00	3.12	0.59	0.99	8.79	0.00	8.79	4.000	No	Yes	2.00
504	10.08	0.93	100.00	3.13	0.59	0.99	8.61	0.00	8.61	4.000	No	Yes	2.00
505	10.10	0.91	100.00	3.15	0.59	0.99	8.31	0.00	8.31	4.000	No	Yes	2.00
506	10.12	0.89	100.00	3.16	0.59	0.99	8.16	0.00	8.16	4.000	No	Yes	2.00
507	10.14	0.87	100.00	3.17	0.59	0.98	8.00	0.00	8.00	4.000	No	Yes	2.00
508	10.16	0.87	100.00	3.17	0.59	0.98	7.93	0.00	7.93	4.000	No	Yes	2.00
509	10.18	0.87	100.00	3.18	0.59	0.98	8.05	0.00	8.05	4.000	No	Yes	2.00
510	10.20	0.87	100.00	3.19	0.59	0.98	7.98	0.00	7.98	4.000	No	Yes	2.00
511	10.22	0.88	100.00	3.19	0.59	0.98	7.93	0.00	7.93	4.000	No	Yes	2.00
512	10.24	0.93	100.00	3.15	0.59	0.98	8.20	0.00	8.20	4.000	No	Yes	2.00
513	10.26	1.03	100.00	3.07	0.59	0.98	9.29	0.00	9.29	4.000	No	Yes	2.00
514	10.28	1.15	100.00	2.99	0.58	0.98	10.75	0.00	10.75	4.000	No	Yes	2.00
515	10.30	1.29	96.68	2.92	0.58	0.98	11.59	0.00	11.59	4.000	No	Yes	2.00
516	10.32	1.40	93.07	2.88	0.57	0.98	13.04	0.00	13.04	4.000	No	Yes	2.00
517	10.34	1.51	90.14	2.84	0.57	0.98	14.02	0.00	14.02	4.000	No	Yes	2.00
518	10.36	1.54	91.65	2.86	0.57	0.98	14.58	0.00	14.58	4.000	No	Yes	2.00
519	10.38	1.53	95.44	2.91	0.57	0.98	14.05	0.00	14.05	4.000	No	Yes	2.00
520	10.40	1.50	99.68	2.96	0.57	0.98	13.77	0.00	13.77	4.000	No	Yes	2.00
521	10.42	1.50	100.00	2.99	0.57	0.97	13.88	0.00	13.88	4.000	No	Yes	2.00
522	10.44	1.50	100.00	3.02	0.57	0.97	13.89	0.00	13.89	4.000	No	Yes	2.00
523	10.46	1.48	100.00	3.04	0.57	0.97	13.65	0.00	13.65	4.000	No	Yes	2.00
524	10.48	1.46	100.00	3.07	0.57	0.97	13.44	0.00	13.44	4.000	No	Yes	2.00
525	10.50	1.42	100.00	3.09	0.57	0.97	13.23	0.00	13.23	4.000	No	Yes	2.00
526	10.52	1.38	100.00	3.12	0.57	0.97	12.61	0.00	12.61	4.000	No	Yes	2.00
527	10.54	1.34	100.00	3.14	0.57	0.97	12.20	0.00	12.20	4.000	No	Yes	2.00
528	10.56	1.31	100.00	3.15	0.57	0.97	11.99	0.00	11.99	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
529	10.58	1.31	100.00	3.14	0.57	0.97	11.93	0.00	11.93	4.000	No	Yes	2.00
530	10.60	1.32	100.00	3.13	0.57	0.97	12.21	0.00	12.21	4.000	No	Yes	2.00
531	10.62	1.32	100.00	3.12	0.57	0.97	12.02	0.00	12.02	4.000	No	Yes	2.00
532	10.64	1.34	100.00	3.12	0.57	0.97	12.12	0.00	12.12	4.000	No	Yes	2.00
533	10.66	1.38	100.00	3.09	0.57	0.96	12.47	0.00	12.47	4.000	No	Yes	2.00
534	10.68	1.46	100.00	3.05	0.57	0.96	13.13	0.00	13.13	4.000	No	Yes	2.00
535	10.70	1.55	100.00	3.01	0.57	0.96	14.32	0.00	14.32	4.000	No	Yes	2.00
536	10.72	1.62	100.00	2.99	0.56	0.96	15.05	0.00	15.05	4.000	No	Yes	2.00
537	10.74	1.66	100.00	2.99	0.56	0.96	15.19	0.00	15.19	4.000	No	Yes	2.00
538	10.76	1.68	100.00	3.00	0.56	0.96	15.53	0.00	15.53	4.000	No	Yes	2.00
539	10.78	1.68	100.00	3.01	0.56	0.96	15.63	0.00	15.63	4.000	No	Yes	2.00
540	10.80	1.66	100.00	3.03	0.56	0.96	15.12	0.00	15.12	4.000	No	Yes	2.00
541	10.82	1.63	100.00	3.07	0.56	0.96	15.14	0.00	15.14	4.000	No	Yes	2.00
542	10.84	1.61	100.00	3.10	0.56	0.96	14.94	0.00	14.94	4.000	No	Yes	2.00
543	10.86	1.57	100.00	3.14	0.56	0.96	14.62	0.00	14.62	4.000	No	Yes	2.00
544	10.88	1.54	100.00	3.17	0.57	0.96	14.13	0.00	14.13	4.000	No	Yes	2.00
545	10.90	1.51	100.00	3.19	0.57	0.95	13.96	0.00	13.96	4.000	No	Yes	2.00
546	10.92	1.49	100.00	3.20	0.57	0.95	13.72	0.00	13.72	4.000	No	Yes	2.00
547	10.94	1.46	100.00	3.20	0.57	0.95	13.53	0.00	13.53	4.000	No	Yes	2.00
548	10.96	1.42	100.00	3.22	0.57	0.95	13.31	0.00	13.31	4.000	No	Yes	2.00
549	10.98	1.38	100.00	3.23	0.57	0.95	12.49	0.00	12.49	4.000	No	Yes	2.00
550	11.00	1.35	100.00	3.23	0.57	0.95	12.26	0.00	12.26	4.000	No	Yes	2.00
551	11.02	1.35	100.00	3.22	0.57	0.95	12.28	0.00	12.28	4.000	No	Yes	2.00
552	11.04	1.35	100.00	3.20	0.57	0.95	12.42	0.00	12.42	4.000	No	Yes	2.00
553	11.06	1.36	100.00	3.19	0.57	0.95	12.32	0.00	12.32	4.000	No	Yes	2.00
554	11.08	1.36	100.00	3.18	0.57	0.95	12.32	0.00	12.32	4.000	No	Yes	2.00
555	11.10	1.36	100.00	3.17	0.57	0.95	12.31	0.00	12.31	4.000	No	Yes	2.00
556	11.13	1.36	100.00	3.17	0.57	0.94	12.44	0.00	12.44	4.000	No	Yes	2.00
557	11.14	1.37	100.00	3.17	0.57	0.94	12.36	0.00	12.36	4.000	No	Yes	2.00
558	11.17	1.38	100.00	3.18	0.57	0.94	12.45	0.00	12.45	4.000	No	Yes	2.00
559	11.18	1.40	100.00	3.18	0.57	0.94	12.74	0.00	12.74	4.000	No	Yes	2.00
560	11.20	1.43	100.00	3.17	0.57	0.94	12.71	0.00	12.71	4.000	No	Yes	2.00
561	11.22	1.48	100.00	3.15	0.57	0.94	13.29	0.00	13.29	4.000	No	Yes	2.00
562	11.24	1.54	100.00	3.12	0.57	0.94	13.90	0.00	13.90	4.000	No	Yes	2.00
563	11.26	1.59	100.00	3.10	0.57	0.94	14.31	0.00	14.31	4.000	No	Yes	2.00
564	11.28	1.63	100.00	3.08	0.56	0.94	14.62	0.00	14.62	4.000	No	Yes	2.00
565	11.30	1.67	100.00	3.06	0.56	0.94	15.06	0.00	15.06	4.000	No	Yes	2.00
566	11.32	1.71	100.00	3.05	0.56	0.94	15.44	0.00	15.44	4.000	No	Yes	2.00
567	11.34	1.76	100.00	3.04	0.56	0.94	15.66	0.00	15.66	4.000	No	Yes	2.00
568	11.36	1.81	100.00	3.04	0.56	0.94	16.39	0.00	16.39	4.000	No	Yes	2.00
569	11.39	1.86	100.00	3.04	0.56	0.94	16.76	0.00	16.76	4.000	No	Yes	2.00
570	11.40	1.89	100.00	3.04	0.56	0.94	16.97	0.00	16.97	4.000	No	Yes	2.00
571	11.42	1.91	100.00	3.06	0.56	0.94	17.19	0.00	17.19	4.000	No	Yes	2.00
572	11.44	1.91	100.00	3.08	0.56	0.93	17.32	0.00	17.32	4.000	No	Yes	2.00
573	11.46	1.89	100.00	3.10	0.56	0.93	17.24	0.00	17.24	4.000	No	Yes	2.00
574	11.48	1.85	100.00	3.13	0.56	0.93	16.65	0.00	16.65	4.000	No	Yes	2.00
575	11.50	1.79	100.00	3.17	0.56	0.93	16.10	0.00	16.10	4.000	No	Yes	2.00
576	11.52	1.74	100.00	3.20	0.56	0.93	15.85	0.00	15.85	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
577	11.54	1.69	100.00	3.23	0.56	0.93	15.24	0.00	15.24	4.000	No	Yes	2.00
578	11.56	1.65	100.00	3.26	0.56	0.93	14.81	0.00	14.81	4.000	No	Yes	2.00
579	11.58	1.61	100.00	3.27	0.57	0.93	14.49	0.00	14.49	4.000	No	Yes	2.00
580	11.60	1.60	100.00	3.27	0.57	0.93	14.29	0.00	14.29	4.000	No	Yes	2.00
581	11.62	1.62	100.00	3.25	0.57	0.93	14.49	0.00	14.49	4.000	No	Yes	2.00
582	11.64	1.62	100.00	3.23	0.56	0.93	14.71	0.00	14.71	4.000	No	Yes	2.00
583	11.66	1.62	100.00	3.22	0.57	0.92	14.41	0.00	14.41	4.000	No	Yes	2.00
584	11.68	1.61	100.00	3.22	0.57	0.92	14.24	0.00	14.24	4.000	No	Yes	2.00
585	11.70	1.60	100.00	3.21	0.57	0.92	14.50	0.00	14.50	4.000	No	Yes	2.00
586	11.72	1.60	100.00	3.21	0.57	0.92	14.24	0.00	14.24	4.000	No	Yes	2.00
587	11.75	1.58	100.00	3.21	0.57	0.92	14.19	0.00	14.19	4.000	No	Yes	2.00
588	11.76	1.57	100.00	3.21	0.57	0.92	13.87	0.00	13.87	4.000	No	Yes	2.00
589	11.78	1.54	100.00	3.21	0.57	0.92	13.92	0.00	13.92	4.000	No	Yes	2.00
590	11.80	1.54	100.00	3.20	0.57	0.92	13.09	0.00	13.09	4.000	No	Yes	2.00
591	11.82	1.52	100.00	3.21	0.57	0.92	13.88	0.00	13.88	4.000	No	Yes	2.00
592	11.84	1.52	100.00	3.21	0.57	0.92	13.50	0.00	13.50	4.000	No	Yes	2.00
593	11.86	1.49	100.00	3.23	0.57	0.92	13.09	0.00	13.09	4.000	No	Yes	2.00
594	11.88	1.45	100.00	3.24	0.57	0.91	12.88	0.00	12.88	4.000	No	Yes	2.00
595	11.91	1.44	100.00	3.23	0.57	0.91	12.43	0.00	12.43	4.000	No	Yes	2.00
596	11.92	1.43	100.00	3.23	0.57	0.91	12.73	0.00	12.73	4.000	No	Yes	2.00
597	11.94	1.43	100.00	3.22	0.57	0.91	12.63	0.00	12.63	4.000	No	Yes	2.00
598	11.96	1.43	100.00	3.22	0.57	0.91	12.58	0.00	12.58	4.000	No	Yes	2.00
599	11.98	1.44	100.00	3.21	0.57	0.91	12.71	0.00	12.71	4.000	No	Yes	2.00
600	12.00	1.48	100.00	3.19	0.57	0.91	12.83	0.00	12.83	4.000	No	Yes	2.00
601	12.02	1.50	100.00	3.16	0.57	0.91	13.39	0.00	13.39	4.000	No	Yes	2.00
602	12.04	1.51	100.00	3.15	0.57	0.91	13.34	0.00	13.34	4.000	No	Yes	2.00
603	12.06	1.48	100.00	3.17	0.57	0.91	13.07	0.00	13.07	4.000	No	Yes	2.00
604	12.08	1.45	100.00	3.18	0.57	0.91	12.70	0.00	12.70	4.000	No	Yes	2.00
605	12.10	1.42	100.00	3.20	0.57	0.91	12.35	0.00	12.35	4.000	No	Yes	2.00
606	12.20	1.40	100.00	3.20	0.57	0.90	12.26	0.00	12.26	4.000	No	Yes	2.00
607	12.20	1.40	100.00	3.21	0.57	0.90	12.26	0.00	12.26	4.000	No	Yes	2.00
608	12.11	1.38	100.00	3.20	0.57	0.91	12.19	0.00	12.19	4.000	No	Yes	2.00
609	12.20	1.37	100.00	3.20	0.58	0.90	11.87	0.00	11.87	4.000	No	Yes	2.00
610	12.22	1.35	100.00	3.21	0.57	0.90	11.93	0.00	11.93	4.000	No	Yes	2.00
611	12.24	1.33	100.00	3.22	0.58	0.90	11.58	0.00	11.58	4.000	No	Yes	2.00
612	12.26	1.30	100.00	3.23	0.58	0.90	11.28	0.00	11.28	4.000	No	Yes	2.00
613	12.28	1.30	100.00	3.23	0.58	0.90	11.23	0.00	11.23	4.000	No	Yes	2.00
614	12.30	1.29	100.00	3.23	0.58	0.90	11.35	0.00	11.35	4.000	No	Yes	2.00
615	12.32	1.27	100.00	3.22	0.58	0.90	11.03	0.00	11.03	4.000	No	Yes	2.00
616	12.34	1.25	100.00	3.23	0.58	0.90	10.83	0.00	10.83	4.000	No	Yes	2.00
617	12.36	1.23	100.00	3.23	0.58	0.90	10.64	0.00	10.64	4.000	No	Yes	2.00
618	12.38	1.25	100.00	3.21	0.58	0.90	10.65	0.00	10.65	4.000	No	Yes	2.00
619	12.40	1.28	100.00	3.18	0.58	0.90	11.25	0.00	11.25	4.000	No	Yes	2.00
620	12.42	1.32	100.00	3.15	0.58	0.89	11.47	0.00	11.47	4.000	No	Yes	2.00
621	12.44	1.34	100.00	3.14	0.58	0.89	11.61	0.00	11.61	4.000	No	Yes	2.00
622	12.46	1.37	100.00	3.13	0.58	0.89	11.75	0.00	11.75	4.000	No	Yes	2.00
623	12.48	1.41	100.00	3.11	0.57	0.89	12.23	0.00	12.23	4.000	No	Yes	2.00
624	12.50	1.45	100.00	3.09	0.57	0.89	12.64	0.00	12.64	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
625	12.52	1.45	100.00	3.10	0.57	0.89	12.73	0.00	12.73	4.000	No	Yes	2.00
626	12.55	1.41	100.00	3.13	0.57	0.89	12.10	0.00	12.10	4.000	No	Yes	2.00
627	12.56	1.36	100.00	3.17	0.58	0.89	11.68	0.00	11.68	4.000	No	Yes	2.00
628	12.58	1.30	100.00	3.20	0.58	0.89	11.29	0.00	11.29	4.000	No	Yes	2.00
629	12.60	1.24	100.00	3.24	0.58	0.89	10.52	0.00	10.52	4.000	No	Yes	2.00
630	12.62	1.19	100.00	3.27	0.58	0.89	10.12	0.00	10.12	4.000	No	Yes	2.00
631	12.64	1.19	100.00	3.27	0.58	0.89	10.09	0.00	10.09	4.000	No	Yes	2.00
632	12.66	1.20	100.00	3.25	0.58	0.89	10.28	0.00	10.28	4.000	No	Yes	2.00
633	12.68	1.21	100.00	3.24	0.58	0.89	10.48	0.00	10.48	4.000	No	Yes	2.00
634	12.70	1.19	100.00	3.24	0.58	0.88	10.25	0.00	10.25	4.000	No	Yes	2.00
635	12.72	1.14	100.00	3.27	0.58	0.88	9.75	0.00	9.75	4.000	No	Yes	2.00
636	12.74	1.09	100.00	3.30	0.59	0.88	9.23	0.00	9.23	4.000	No	Yes	2.00
637	12.76	1.05	100.00	3.33	0.59	0.88	9.06	0.00	9.06	4.000	No	Yes	2.00
638	12.78	1.03	100.00	3.35	0.59	0.88	8.65	0.00	8.65	4.000	No	Yes	2.00
639	12.80	1.01	100.00	3.36	0.59	0.88	8.51	0.00	8.51	4.000	No	Yes	2.00
640	12.83	0.99	100.00	3.36	0.59	0.88	8.25	0.00	8.25	4.000	No	Yes	2.00
641	12.84	0.98	100.00	3.38	0.59	0.88	8.13	0.00	8.13	4.000	No	Yes	2.00
642	12.86	0.97	100.00	3.38	0.59	0.88	8.01	0.00	8.01	4.000	No	Yes	2.00
643	12.88	0.97	100.00	3.38	0.59	0.88	8.10	0.00	8.10	4.000	No	Yes	2.00
644	12.90	0.96	100.00	3.38	0.59	0.88	8.13	0.00	8.13	4.000	No	Yes	2.00
645	12.92	0.93	100.00	3.40	0.59	0.88	7.78	0.00	7.78	4.000	No	Yes	2.00
646	12.94	0.89	100.00	3.44	0.59	0.88	7.35	0.00	7.35	4.000	No	Yes	2.00
647	12.96	0.85	100.00	3.47	0.59	0.87	7.08	0.00	7.08	4.000	No	Yes	2.00
648	12.98	0.80	100.00	3.51	0.60	0.87	6.65	0.00	6.65	4.000	No	Yes	2.00
649	13.00	0.77	100.00	3.54	0.60	0.87	6.18	0.00	6.18	4.000	No	Yes	2.00
650	13.02	0.74	100.00	3.55	0.60	0.87	6.14	0.00	6.14	4.000	No	Yes	2.00
651	13.04	0.74	100.00	3.52	0.60	0.87	6.03	0.00	6.03	4.000	No	Yes	2.00
652	13.06	0.78	100.00	3.45	0.60	0.87	6.23	0.00	6.23	4.000	No	Yes	2.00
653	13.08	0.83	100.00	3.36	0.59	0.87	6.95	0.00	6.95	4.000	No	Yes	2.00
654	13.10	0.88	100.00	3.28	0.59	0.87	7.25	0.00	7.25	4.000	No	Yes	2.00
655	13.12	0.88	100.00	3.25	0.59	0.87	7.38	0.00	7.38	4.000	No	Yes	2.00
656	13.14	0.86	100.00	3.24	0.59	0.87	7.04	0.00	7.04	4.000	No	Yes	2.00
657	13.16	0.89	100.00	3.18	0.60	0.87	6.76	0.00	6.76	4.000	No	Yes	2.00
658	13.18	0.99	100.00	3.08	0.59	0.87	8.00	0.00	8.00	4.000	No	Yes	2.00
659	13.20	1.10	100.00	3.02	0.58	0.87	9.55	0.00	9.55	4.000	No	Yes	2.00
660	13.22	1.14	100.00	3.02	0.58	0.87	9.66	0.00	9.66	4.000	No	Yes	2.00
661	13.24	1.14	100.00	3.04	0.59	0.87	9.08	0.00	9.08	4.000	No	Yes	2.00
662	13.26	1.17	100.00	3.02	0.58	0.87	9.58	0.00	9.58	4.000	No	Yes	2.00
663	13.28	1.19	100.00	3.01	0.58	0.87	10.40	0.00	10.40	4.000	No	Yes	2.00
664	13.30	1.14	100.00	3.07	0.58	0.87	9.59	0.00	9.59	4.000	No	Yes	2.00
665	13.32	1.10	100.00	3.11	0.59	0.87	8.34	0.00	8.34	4.000	No	Yes	2.00
666	13.34	1.14	100.00	3.09	0.59	0.87	9.28	0.00	9.28	4.000	No	Yes	2.00
667	13.36	1.22	100.00	3.04	0.58	0.87	10.50	0.00	10.50	4.000	No	Yes	2.00
668	13.41	1.25	100.00	3.03	0.58	0.86	10.24	0.00	10.24	4.000	No	Yes	2.00
669	13.41	1.12	100.00	3.12	0.58	0.86	10.24	0.00	10.24	4.000	No	Yes	2.00
670	13.42	0.96	100.00	3.24	0.59	0.86	7.12	0.00	7.12	4.000	No	Yes	2.00
671	13.44	0.78	100.00	3.41	0.60	0.86	6.13	0.00	6.13	4.000	No	Yes	2.00
672	13.46	0.73	100.00	3.46	0.60	0.86	5.67	0.00	5.67	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
673	13.48	0.80	100.00	3.37	0.60	0.86	5.67	0.00	5.67	4.000	No	Yes	2.00
674	13.50	1.11	100.00	3.10	0.59	0.86	7.84	0.00	7.84	4.000	No	Yes	2.00
675	13.52	1.58	89.92	2.84	0.57	0.86	13.36	0.00	13.36	4.000	No	Yes	2.00
676	13.54	2.07	74.86	2.65	0.56	0.87	17.57	0.00	17.57	4.000	No	Yes	2.00
677	13.56	2.38	69.96	2.59	0.55	0.87	20.88	56.69	77.57	0.114	No	No	0.56
678	13.58	2.53	70.46	2.59	0.55	0.87	21.61	56.99	78.60	0.115	No	No	0.56
679	13.60	2.51	73.89	2.64	0.55	0.87	21.71	0.00	21.71	4.000	No	Yes	2.00
680	13.62	2.35	79.84	2.71	0.55	0.87	20.60	0.00	20.60	4.000	No	Yes	2.00
681	13.64	2.04	89.28	2.83	0.56	0.86	17.62	0.00	17.62	4.000	No	Yes	2.00
682	13.66	1.63	100.00	2.98	0.57	0.86	13.74	0.00	13.74	4.000	No	Yes	2.00
683	13.68	1.27	100.00	3.14	0.58	0.86	10.02	0.00	10.02	4.000	No	Yes	2.00
684	13.70	1.01	100.00	3.28	0.59	0.86	8.23	0.00	8.23	4.000	No	Yes	2.00
685	13.72	0.88	100.00	3.36	0.59	0.85	7.14	0.00	7.14	4.000	No	Yes	2.00
686	13.74	0.80	100.00	3.42	0.60	0.85	6.34	0.00	6.34	4.000	No	Yes	2.00
687	13.76	0.75	100.00	3.47	0.60	0.85	6.02	0.00	6.02	4.000	No	Yes	2.00
688	13.78	0.74	100.00	3.50	0.60	0.85	5.80	0.00	5.80	4.000	No	Yes	2.00
689	13.80	0.74	100.00	3.49	0.60	0.85	5.88	0.00	5.88	4.000	No	Yes	2.00
690	13.83	0.72	100.00	3.51	0.60	0.85	5.81	0.00	5.81	4.000	No	Yes	2.00
691	13.84	0.68	100.00	3.53	0.60	0.85	5.36	0.00	5.36	4.000	No	Yes	2.00
692	13.86	0.63	100.00	3.58	0.60	0.85	4.99	0.00	4.99	4.000	No	Yes	2.00
693	14.03	0.61	100.00	3.62	0.60	0.84	4.67	0.00	4.67	4.000	No	Yes	2.00
694	14.03	0.60	100.00	3.64	0.60	0.84	4.67	0.00	4.67	4.000	No	Yes	2.00
695	14.03	0.60	100.00	3.64	0.60	0.84	4.69	0.00	4.69	4.000	No	Yes	2.00
696	13.88	0.63	100.00	3.56	0.60	0.85	4.71	0.00	4.71	4.000	No	Yes	2.00
697	13.96	0.68	100.00	3.47	0.60	0.85	5.50	0.00	5.50	4.000	No	Yes	2.00
698	13.98	0.74	100.00	3.37	0.60	0.85	5.89	0.00	5.89	4.000	No	Yes	2.00
699	14.00	0.78	100.00	3.33	0.60	0.85	6.12	0.00	6.12	4.000	No	Yes	2.00
700	14.02	0.81	100.00	3.30	0.60	0.85	6.41	0.00	6.41	4.000	No	Yes	2.00
701	14.04	0.85	100.00	3.27	0.60	0.85	6.68	0.00	6.68	4.000	No	Yes	2.00
702	14.06	0.89	100.00	3.25	0.59	0.85	7.03	0.00	7.03	4.000	No	Yes	2.00
703	14.08	0.93	100.00	3.23	0.59	0.84	7.32	0.00	7.32	4.000	No	Yes	2.00
704	14.10	0.97	100.00	3.22	0.59	0.84	7.69	0.00	7.69	4.000	No	Yes	2.00
705	14.12	1.00	100.00	3.20	0.59	0.84	7.86	0.00	7.86	4.000	No	Yes	2.00
706	14.14	1.02	100.00	3.20	0.59	0.84	8.15	0.00	8.15	4.000	No	Yes	2.00
707	14.16	1.02	100.00	3.20	0.59	0.84	8.18	0.00	8.18	4.000	No	Yes	2.00
708	14.18	1.00	100.00	3.22	0.59	0.84	7.87	0.00	7.87	4.000	No	Yes	2.00
709	14.21	0.98	100.00	3.24	0.59	0.84	7.66	0.00	7.66	4.000	No	Yes	2.00
710	14.22	0.96	100.00	3.26	0.59	0.84	7.49	0.00	7.49	4.000	No	Yes	2.00
711	14.24	0.96	100.00	3.27	0.59	0.84	7.56	0.00	7.56	4.000	No	Yes	2.00
712	14.26	0.96	100.00	3.27	0.59	0.84	7.50	0.00	7.50	4.000	No	Yes	2.00
713	14.28	0.96	100.00	3.27	0.59	0.84	7.57	0.00	7.57	4.000	No	Yes	2.00
714	14.30	0.97	100.00	3.28	0.59	0.84	7.62	0.00	7.62	4.000	No	Yes	2.00
715	14.32	0.97	100.00	3.29	0.59	0.84	7.54	0.00	7.54	4.000	No	Yes	2.00
716	14.37	0.97	100.00	3.31	0.59	0.84	7.57	0.00	7.57	4.000	No	Yes	2.00
717	14.37	0.97	100.00	3.31	0.59	0.84	7.57	0.00	7.57	4.000	No	Yes	2.00
718	14.38	0.97	100.00	3.33	0.59	0.84	7.62	0.00	7.62	4.000	No	Yes	2.00
719	14.40	0.98	100.00	3.34	0.59	0.84	7.64	0.00	7.64	4.000	No	Yes	2.00
720	14.42	0.99	100.00	3.34	0.59	0.84	7.77	0.00	7.77	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
721	14.44	1.01	100.00	3.33	0.59	0.84	7.88	0.00	7.88	4.000	No	Yes	2.00
722	14.46	1.03	100.00	3.33	0.59	0.84	8.10	0.00	8.10	4.000	No	Yes	2.00
723	14.48	1.06	100.00	3.32	0.59	0.84	8.23	0.00	8.23	4.000	No	Yes	2.00
724	14.50	1.09	100.00	3.30	0.59	0.84	8.40	0.00	8.40	4.000	No	Yes	2.00
725	14.52	1.12	100.00	3.28	0.59	0.84	8.80	0.00	8.80	4.000	No	Yes	2.00
726	14.54	1.15	100.00	3.26	0.59	0.83	9.01	0.00	9.01	4.000	No	Yes	2.00
727	14.56	1.17	100.00	3.25	0.59	0.83	9.17	0.00	9.17	4.000	No	Yes	2.00
728	14.58	1.17	100.00	3.26	0.59	0.83	9.19	0.00	9.19	4.000	No	Yes	2.00
729	14.60	1.15	100.00	3.27	0.59	0.83	9.02	0.00	9.02	4.000	No	Yes	2.00
730	14.62	1.14	100.00	3.28	0.59	0.83	8.88	0.00	8.88	4.000	No	Yes	2.00
731	14.64	1.14	100.00	3.29	0.59	0.83	8.91	0.00	8.91	4.000	No	Yes	2.00
732	14.66	1.15	100.00	3.28	0.59	0.83	8.88	0.00	8.88	4.000	No	Yes	2.00
733	14.68	1.18	100.00	3.25	0.59	0.83	9.13	0.00	9.13	4.000	No	Yes	2.00
734	14.70	1.22	100.00	3.22	0.58	0.83	9.70	0.00	9.70	4.000	No	Yes	2.00
735	14.72	1.26	100.00	3.20	0.58	0.83	9.85	0.00	9.85	4.000	No	Yes	2.00
736	14.74	1.29	100.00	3.19	0.58	0.83	10.19	0.00	10.19	4.000	No	Yes	2.00
737	14.76	1.31	100.00	3.19	0.58	0.83	10.42	0.00	10.42	4.000	No	Yes	2.00
738	14.78	1.32	100.00	3.21	0.58	0.83	10.35	0.00	10.35	4.000	No	Yes	2.00
739	14.80	1.34	100.00	3.22	0.58	0.83	10.43	0.00	10.43	4.000	No	Yes	2.00
740	14.82	1.36	100.00	3.23	0.58	0.83	10.81	0.00	10.81	4.000	No	Yes	2.00
741	14.84	1.39	100.00	3.24	0.58	0.83	10.84	0.00	10.84	4.000	No	Yes	2.00
742	14.86	1.42	100.00	3.24	0.58	0.83	11.24	0.00	11.24	4.000	No	Yes	2.00
743	14.88	1.44	100.00	3.24	0.58	0.83	11.35	0.00	11.35	4.000	No	Yes	2.00
744	14.90	1.44	100.00	3.25	0.58	0.83	11.36	0.00	11.36	4.000	No	Yes	2.00
745	14.92	1.44	100.00	3.25	0.58	0.83	11.29	0.00	11.29	4.000	No	Yes	2.00
746	14.94	1.45	100.00	3.25	0.58	0.83	11.37	0.00	11.37	4.000	No	Yes	2.00
747	14.96	1.45	100.00	3.25	0.58	0.83	11.38	0.00	11.38	4.000	No	Yes	2.00
748	14.98	1.46	100.00	3.25	0.58	0.83	11.29	0.00	11.29	4.000	No	Yes	2.00
749	15.00	1.48	100.00	3.24	0.58	0.82	11.53	0.00	11.53	4.000	No	Yes	2.00
750	15.02	1.50	100.00	3.23	0.58	0.82	11.77	0.00	11.77	4.000	No	Yes	2.00
751	15.04	1.53	100.00	3.22	0.58	0.82	11.89	0.00	11.89	4.000	No	Yes	2.00
752	15.06	1.54	100.00	3.22	0.57	0.82	12.10	0.00	12.10	4.000	No	Yes	2.00
753	15.08	1.53	100.00	3.22	0.57	0.82	11.93	0.00	11.93	4.000	No	Yes	2.00
754	15.10	1.52	100.00	3.22	0.58	0.82	11.80	0.00	11.80	4.000	No	Yes	2.00
755	15.12	1.52	100.00	3.22	0.58	0.82	11.74	0.00	11.74	4.000	No	Yes	2.00
756	15.14	1.51	100.00	3.22	0.58	0.82	11.77	0.00	11.77	4.000	No	Yes	2.00
757	15.16	1.51	100.00	3.21	0.58	0.82	11.64	0.00	11.64	4.000	No	Yes	2.00
758	15.18	1.51	100.00	3.21	0.58	0.82	11.70	0.00	11.70	4.000	No	Yes	2.00
759	15.20	1.52	100.00	3.20	0.58	0.82	11.77	0.00	11.77	4.000	No	Yes	2.00
760	15.22	1.53	100.00	3.20	0.58	0.82	11.80	0.00	11.80	4.000	No	Yes	2.00
761	15.24	1.54	100.00	3.19	0.58	0.82	11.88	0.00	11.88	4.000	No	Yes	2.00
762	15.26	1.56	100.00	3.19	0.57	0.82	12.02	0.00	12.02	4.000	No	Yes	2.00
763	15.28	1.57	100.00	3.19	0.57	0.82	12.22	0.00	12.22	4.000	No	Yes	2.00
764	15.30	1.57	100.00	3.20	0.57	0.82	12.13	0.00	12.13	4.000	No	Yes	2.00
765	15.32	1.56	100.00	3.22	0.57	0.82	12.08	0.00	12.08	4.000	No	Yes	2.00
766	15.34	1.57	100.00	3.22	0.57	0.82	12.01	0.00	12.01	4.000	No	Yes	2.00
767	15.36	1.57	100.00	3.23	0.57	0.82	12.25	0.00	12.25	4.000	No	Yes	2.00
768	15.38	1.59	100.00	3.23	0.57	0.82	12.16	0.00	12.16	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
769	15.40	1.60	100.00	3.23	0.57	0.81	12.28	0.00	12.28	4.000	No	Yes	2.00
770	15.42	1.63	100.00	3.21	0.57	0.81	12.55	0.00	12.55	4.000	No	Yes	2.00
771	15.44	1.66	100.00	3.18	0.57	0.81	12.85	0.00	12.85	4.000	No	Yes	2.00
772	15.46	1.68	100.00	3.16	0.57	0.81	12.97	0.00	12.97	4.000	No	Yes	2.00
773	15.48	1.69	100.00	3.15	0.57	0.81	12.94	0.00	12.94	4.000	No	Yes	2.00
774	15.50	1.69	100.00	3.15	0.57	0.81	13.00	0.00	13.00	4.000	No	Yes	2.00
775	15.52	1.69	100.00	3.16	0.57	0.81	13.05	0.00	13.05	4.000	No	Yes	2.00
776	15.54	1.70	100.00	3.16	0.57	0.81	12.96	0.00	12.96	4.000	No	Yes	2.00
777	15.56	1.70	100.00	3.17	0.57	0.81	13.18	0.00	13.18	4.000	No	Yes	2.00
778	15.58	1.70	100.00	3.18	0.57	0.81	13.11	0.00	13.11	4.000	No	Yes	2.00
779	15.60	1.67	100.00	3.20	0.57	0.81	12.79	0.00	12.79	4.000	No	Yes	2.00
780	15.62	1.64	100.00	3.22	0.57	0.81	12.54	0.00	12.54	4.000	No	Yes	2.00
781	15.64	1.62	100.00	3.23	0.57	0.81	12.34	0.00	12.34	4.000	No	Yes	2.00
782	15.66	1.62	100.00	3.22	0.57	0.81	12.31	0.00	12.31	4.000	No	Yes	2.00
783	15.68	1.63	100.00	3.21	0.57	0.81	12.39	0.00	12.39	4.000	No	Yes	2.00
784	15.70	1.64	100.00	3.19	0.57	0.81	12.57	0.00	12.57	4.000	No	Yes	2.00
785	15.72	1.64	100.00	3.19	0.57	0.81	12.58	0.00	12.58	4.000	No	Yes	2.00
786	15.74	1.62	100.00	3.20	0.57	0.81	12.46	0.00	12.46	4.000	No	Yes	2.00
787	15.76	1.59	100.00	3.21	0.57	0.80	12.10	0.00	12.10	4.000	No	Yes	2.00
788	15.78	1.56	100.00	3.23	0.57	0.80	12.00	0.00	12.00	4.000	No	Yes	2.00
789	15.80	1.58	100.00	3.24	0.58	0.80	11.64	0.00	11.64	4.000	No	Yes	2.00
790	15.82	1.56	100.00	3.26	0.57	0.80	12.32	0.00	12.32	4.000	No	Yes	2.00
791	15.84	1.56	100.00	3.27	0.58	0.80	11.60	0.00	11.60	4.000	No	Yes	2.00
792	15.86	1.53	100.00	3.28	0.58	0.80	11.65	0.00	11.65	4.000	No	Yes	2.00
793	15.88	1.55	100.00	3.27	0.58	0.80	11.75	0.00	11.75	4.000	No	Yes	2.00
794	15.90	1.56	100.00	3.27	0.57	0.80	12.00	0.00	12.00	4.000	No	Yes	2.00
795	15.92	1.58	100.00	3.26	0.58	0.80	11.80	0.00	11.80	4.000	No	Yes	2.00
796	15.94	1.59	100.00	3.25	0.57	0.80	12.13	0.00	12.13	4.000	No	Yes	2.00
797	15.96	1.59	100.00	3.25	0.57	0.80	12.21	0.00	12.21	4.000	No	Yes	2.00
798	15.98	1.57	100.00	3.27	0.58	0.80	11.78	0.00	11.78	4.000	No	Yes	2.00
799	16.00	1.58	100.00	3.28	0.58	0.80	11.73	0.00	11.73	4.000	No	Yes	2.00
800	16.02	1.63	100.00	3.25	0.57	0.80	12.11	0.00	12.11	4.000	No	Yes	2.00
801	16.04	1.74	100.00	3.21	0.57	0.80	13.08	0.00	13.08	4.000	No	Yes	2.00
802	16.07	1.87	100.00	3.15	0.57	0.80	14.22	0.00	14.22	4.000	No	Yes	2.00
803	16.08	1.99	100.00	3.10	0.56	0.80	15.12	0.00	15.12	4.000	No	Yes	2.00
804	16.10	2.07	100.00	3.06	0.56	0.80	16.04	0.00	16.04	4.000	No	Yes	2.00
805	16.12	2.11	100.00	3.04	0.56	0.80	16.48	0.00	16.48	4.000	No	Yes	2.00
806	16.14	2.10	100.00	3.04	0.56	0.80	16.24	0.00	16.24	4.000	No	Yes	2.00
807	16.16	2.09	100.00	3.06	0.56	0.80	15.88	0.00	15.88	4.000	No	Yes	2.00
808	16.18	2.11	100.00	3.07	0.56	0.80	16.30	0.00	16.30	4.000	No	Yes	2.00
809	16.20	2.15	100.00	3.07	0.56	0.80	16.69	0.00	16.69	4.000	No	Yes	2.00
810	16.22	2.16	100.00	3.09	0.56	0.80	16.66	0.00	16.66	4.000	No	Yes	2.00
811	16.24	2.15	100.00	3.11	0.56	0.80	16.58	0.00	16.58	4.000	No	Yes	2.00
812	16.26	2.12	100.00	3.14	0.56	0.80	16.38	0.00	16.38	4.000	No	Yes	2.00
813	16.28	2.07	100.00	3.17	0.56	0.80	15.93	0.00	15.93	4.000	No	Yes	2.00
814	16.30	2.03	100.00	3.21	0.56	0.79	15.48	0.00	15.48	4.000	No	Yes	2.00
815	16.32	2.01	100.00	3.22	0.56	0.79	15.22	0.00	15.22	4.000	No	Yes	2.00
816	16.34	2.03	100.00	3.22	0.56	0.79	15.41	0.00	15.41	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
817	16.36	2.07	100.00	3.20	0.56	0.79	15.78	0.00	15.78	4.000	No	Yes	2.00
818	16.38	2.07	100.00	3.19	0.56	0.79	15.82	0.00	15.82	4.000	No	Yes	2.00
819	16.40	2.03	100.00	3.20	0.56	0.79	15.52	0.00	15.52	4.000	No	Yes	2.00
820	16.42	1.94	100.00	3.22	0.56	0.79	14.68	0.00	14.68	4.000	No	Yes	2.00
821	16.44	1.82	100.00	3.27	0.57	0.79	13.82	0.00	13.82	4.000	No	Yes	2.00
822	16.46	1.73	100.00	3.31	0.57	0.79	12.71	0.00	12.71	4.000	No	Yes	2.00
823	16.48	1.64	100.00	3.34	0.57	0.79	12.43	0.00	12.43	4.000	No	Yes	2.00
824	16.50	1.57	100.00	3.36	0.58	0.78	11.79	0.00	11.79	4.000	No	Yes	2.00
825	16.52	1.49	100.00	3.39	0.58	0.78	11.00	0.00	11.00	4.000	No	Yes	2.00
826	16.54	1.42	100.00	3.40	0.58	0.78	10.45	0.00	10.45	4.000	No	Yes	2.00
827	16.56	1.39	100.00	3.38	0.58	0.78	10.24	0.00	10.24	4.000	No	Yes	2.00
828	16.58	1.38	100.00	3.34	0.58	0.78	10.17	0.00	10.17	4.000	No	Yes	2.00
829	16.60	1.37	100.00	3.30	0.58	0.78	10.18	0.00	10.18	4.000	No	Yes	2.00
830	16.62	1.33	100.00	3.27	0.58	0.78	9.80	0.00	9.80	4.000	No	Yes	2.00
831	16.64	1.28	100.00	3.27	0.58	0.78	9.45	0.00	9.45	4.000	No	Yes	2.00
832	16.66	1.23	100.00	3.28	0.59	0.78	8.93	0.00	8.93	4.000	No	Yes	2.00
833	16.68	1.17	100.00	3.29	0.59	0.78	8.58	0.00	8.58	4.000	No	Yes	2.00
834	16.70	1.14	100.00	3.29	0.59	0.78	8.11	0.00	8.11	4.000	No	Yes	2.00
835	16.72	1.13	100.00	3.28	0.59	0.78	8.18	0.00	8.18	4.000	No	Yes	2.00
836	16.74	1.15	100.00	3.25	0.59	0.77	8.27	0.00	8.27	4.000	No	Yes	2.00
837	16.76	1.16	100.00	3.23	0.59	0.77	8.48	0.00	8.48	4.000	No	Yes	2.00
838	16.78	1.19	100.00	3.19	0.59	0.77	8.34	0.00	8.34	4.000	No	Yes	2.00
839	16.80	1.22	100.00	3.15	0.59	0.77	8.69	0.00	8.69	4.000	No	Yes	2.00
840	16.82	1.26	100.00	3.11	0.59	0.77	8.87	0.00	8.87	4.000	No	Yes	2.00
841	16.84	1.27	100.00	3.10	0.59	0.77	9.00	0.00	9.00	4.000	No	Yes	2.00
842	16.86	1.26	100.00	3.11	0.59	0.77	8.90	0.00	8.90	4.000	No	Yes	2.00
843	16.88	1.25	100.00	3.12	0.59	0.77	8.66	0.00	8.66	4.000	No	Yes	2.00
844	16.90	1.24	100.00	3.13	0.59	0.77	8.79	0.00	8.79	4.000	No	Yes	2.00
845	16.92	1.25	100.00	3.13	0.59	0.77	8.66	0.00	8.66	4.000	No	Yes	2.00
846	16.94	1.25	100.00	3.12	0.59	0.77	8.75	0.00	8.75	4.000	No	Yes	2.00
847	16.96	1.27	100.00	3.11	0.59	0.77	8.86	0.00	8.86	4.000	No	Yes	2.00
848	16.98	1.30	100.00	3.08	0.59	0.77	9.00	0.00	9.00	4.000	No	Yes	2.00
849	17.00	1.35	100.00	3.05	0.58	0.77	9.34	0.00	9.34	4.000	No	Yes	2.00
850	17.02	1.44	100.00	2.99	0.58	0.77	9.99	0.00	9.99	4.000	No	Yes	2.00
851	17.04	1.52	98.68	2.95	0.58	0.77	10.96	0.00	10.96	4.000	No	Yes	2.00
852	17.06	1.58	96.96	2.92	0.58	0.77	11.23	0.00	11.23	4.000	No	Yes	2.00
853	17.08	1.57	98.83	2.95	0.58	0.77	11.37	0.00	11.37	4.000	No	Yes	2.00
854	17.10	1.52	100.00	2.99	0.58	0.77	10.75	0.00	10.75	4.000	No	Yes	2.00
855	17.12	1.44	100.00	3.05	0.58	0.77	10.11	0.00	10.11	4.000	No	Yes	2.00
856	17.14	1.36	100.00	3.12	0.58	0.77	9.85	0.00	9.85	4.000	No	Yes	2.00
857	17.16	1.30	100.00	3.16	0.59	0.77	8.91	0.00	8.91	4.000	No	Yes	2.00
858	17.18	1.23	100.00	3.21	0.59	0.77	8.74	0.00	8.74	4.000	No	Yes	2.00
859	17.20	1.19	100.00	3.23	0.59	0.77	8.24	0.00	8.24	4.000	No	Yes	2.00
860	17.22	1.14	100.00	3.25	0.59	0.76	7.95	0.00	7.95	4.000	No	Yes	2.00
861	17.24	1.12	100.00	3.25	0.59	0.76	7.59	0.00	7.59	4.000	No	Yes	2.00
862	17.26	1.14	100.00	3.21	0.59	0.76	7.61	0.00	7.61	4.000	No	Yes	2.00
863	17.28	1.21	100.00	3.12	0.59	0.76	8.19	0.00	8.19	4.000	No	Yes	2.00
864	17.30	1.31	100.00	3.03	0.59	0.76	9.07	0.00	9.07	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
865	17.32	1.38	100.00	2.99	0.58	0.77	9.99	0.00	9.99	4.000	No	Yes	2.00
866	17.34	1.41	100.00	2.99	0.58	0.77	10.15	0.00	10.15	4.000	No	Yes	2.00
867	17.36	1.41	100.00	3.02	0.58	0.77	10.02	0.00	10.02	4.000	No	Yes	2.00
868	17.38	1.40	100.00	3.04	0.58	0.76	9.80	0.00	9.80	4.000	No	Yes	2.00
869	17.44	1.39	100.00	3.05	0.58	0.76	9.71	0.00	9.71	4.000	No	Yes	2.00
870	17.44	1.42	100.00	3.03	0.58	0.76	9.71	0.00	9.71	4.000	No	Yes	2.00
871	17.44	1.50	100.00	3.00	0.58	0.76	10.40	0.00	10.40	4.000	No	Yes	2.00
872	17.46	1.58	100.00	2.97	0.58	0.76	11.19	0.00	11.19	4.000	No	Yes	2.00
873	17.48	1.63	99.13	2.95	0.58	0.76	11.42	0.00	11.42	4.000	No	Yes	2.00
874	17.50	1.62	100.00	2.97	0.58	0.76	11.65	0.00	11.65	4.000	No	Yes	2.00
875	17.52	1.54	100.00	3.03	0.58	0.76	11.14	0.00	11.14	4.000	No	Yes	2.00
876	17.54	1.45	100.00	3.09	0.58	0.76	10.05	0.00	10.05	4.000	No	Yes	2.00
877	17.56	1.37	100.00	3.15	0.58	0.76	9.83	0.00	9.83	4.000	No	Yes	2.00
878	17.58	1.31	100.00	3.18	0.59	0.76	9.11	0.00	9.11	4.000	No	Yes	2.00
879	17.63	1.26	100.00	3.21	0.59	0.76	8.70	0.00	8.70	4.000	No	Yes	2.00
880	17.63	1.20	100.00	3.25	0.59	0.76	8.70	0.00	8.70	4.000	No	Yes	2.00
881	17.64	1.15	100.00	3.26	0.59	0.76	7.52	0.00	7.52	4.000	No	Yes	2.00
882	17.66	1.11	100.00	3.26	0.59	0.76	7.55	0.00	7.55	4.000	No	Yes	2.00
883	17.68	1.13	100.00	3.21	0.59	0.76	7.63	0.00	7.63	4.000	No	Yes	2.00
884	17.70	1.13	100.00	3.18	0.59	0.76	7.68	0.00	7.68	4.000	No	Yes	2.00
885	17.72	1.12	100.00	3.17	0.59	0.75	7.48	0.00	7.48	4.000	No	Yes	2.00
886	17.74	1.12	100.00	3.15	0.59	0.75	7.62	0.00	7.62	4.000	No	Yes	2.00
887	17.76	1.14	100.00	3.12	0.59	0.75	7.62	0.00	7.62	4.000	No	Yes	2.00
888	17.78	1.24	100.00	3.04	0.59	0.75	7.74	0.00	7.74	4.000	No	Yes	2.00
889	17.80	1.28	100.00	3.03	0.58	0.76	10.10	0.00	10.10	4.000	No	Yes	2.00
890	17.82	1.29	100.00	3.04	0.59	0.75	8.88	0.00	8.88	4.000	No	Yes	2.00
891	17.84	1.20	100.00	3.11	0.59	0.75	8.17	0.00	8.17	4.000	No	Yes	2.00
892	17.86	1.16	100.00	3.12	0.59	0.75	7.82	0.00	7.82	4.000	No	Yes	2.00
893	17.88	1.14	100.00	3.12	0.59	0.75	7.69	0.00	7.69	4.000	No	Yes	2.00
894	17.90	1.14	100.00	3.12	0.59	0.75	7.57	0.00	7.57	4.000	No	Yes	2.00
895	17.95	1.14	100.00	3.12	0.59	0.75	7.72	0.00	7.72	4.000	No	Yes	2.00
896	17.95	1.19	100.00	3.08	0.59	0.75	7.72	0.00	7.72	4.000	No	Yes	2.00
897	17.96	1.26	100.00	3.03	0.59	0.75	8.50	0.00	8.50	4.000	No	Yes	2.00
898	17.98	1.33	100.00	2.98	0.59	0.75	9.16	0.00	9.16	4.000	No	Yes	2.00
899	18.00	1.37	100.00	2.97	0.59	0.75	9.14	0.00	9.14	4.000	No	Yes	2.00
900	18.02	1.40	100.00	2.97	0.58	0.75	9.44	0.00	9.44	4.000	No	Yes	2.00
901	18.04	1.55	95.92	2.91	0.58	0.75	9.91	0.00	9.91	4.000	No	Yes	2.00
902	18.06	1.77	89.28	2.83	0.58	0.75	12.39	0.00	12.39	4.000	No	Yes	2.00
903	18.08	2.02	81.54	2.73	0.57	0.76	13.95	0.00	13.95	4.000	No	Yes	2.00
904	18.10	2.22	78.32	2.69	0.57	0.76	16.01	0.00	16.01	4.000	No	Yes	2.00
905	18.12	2.30	79.78	2.71	0.56	0.76	17.44	0.00	17.44	4.000	No	Yes	2.00
906	18.14	2.25	85.86	2.79	0.56	0.76	16.81	0.00	16.81	4.000	No	Yes	2.00
907	18.16	2.06	93.85	2.89	0.56	0.76	15.06	0.00	15.06	4.000	No	Yes	2.00
908	18.18	1.86	100.00	3.00	0.57	0.76	13.38	0.00	13.38	4.000	No	Yes	2.00
909	18.20	1.72	100.00	3.09	0.57	0.75	12.08	0.00	12.08	4.000	No	Yes	2.00
910	18.22	1.68	100.00	3.12	0.58	0.75	11.24	0.00	11.24	4.000	No	Yes	2.00
911	18.24	1.63	100.00	3.15	0.57	0.75	12.05	0.00	12.05	4.000	No	Yes	2.00
912	18.26	1.56	100.00	3.18	0.58	0.75	10.90	0.00	10.90	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
913	18.28	1.45	100.00	3.22	0.58	0.75	9.65	0.00	9.65	4.000	No	Yes	2.00
914	18.30	1.38	100.00	3.22	0.59	0.75	9.25	0.00	9.25	4.000	No	Yes	2.00
915	18.32	1.35	100.00	3.19	0.59	0.75	9.13	0.00	9.13	4.000	No	Yes	2.00
916	18.34	1.33	100.00	3.17	0.59	0.75	8.86	0.00	8.86	4.000	No	Yes	2.00
917	18.36	1.32	100.00	3.16	0.59	0.74	8.75	0.00	8.75	4.000	No	Yes	2.00
918	18.38	1.32	100.00	3.15	0.59	0.74	8.95	0.00	8.95	4.000	No	Yes	2.00
919	18.40	1.31	100.00	3.13	0.59	0.74	8.69	0.00	8.69	4.000	No	Yes	2.00
920	18.42	1.33	100.00	3.10	0.59	0.74	8.62	0.00	8.62	4.000	No	Yes	2.00
921	18.44	1.38	100.00	3.04	0.59	0.74	9.16	0.00	9.16	4.000	No	Yes	2.00
922	18.46	1.44	100.00	3.01	0.58	0.74	9.74	0.00	9.74	4.000	No	Yes	2.00
923	18.48	1.44	100.00	3.02	0.58	0.74	9.84	0.00	9.84	4.000	No	Yes	2.00
924	18.50	1.40	100.00	3.05	0.58	0.74	9.36	0.00	9.36	4.000	No	Yes	2.00
925	18.52	1.33	100.00	3.10	0.59	0.74	8.88	0.00	8.88	4.000	No	Yes	2.00
926	18.54	1.29	100.00	3.12	0.59	0.74	8.35	0.00	8.35	4.000	No	Yes	2.00
927	18.56	1.33	100.00	3.09	0.59	0.74	8.52	0.00	8.52	4.000	No	Yes	2.00
928	18.58	1.41	100.00	3.04	0.58	0.74	9.53	0.00	9.53	4.000	No	Yes	2.00
929	18.60	1.45	100.00	3.03	0.58	0.74	9.98	0.00	9.98	4.000	No	Yes	2.00
930	18.62	1.41	100.00	3.08	0.58	0.74	9.57	0.00	9.57	4.000	No	Yes	2.00
931	18.64	1.34	100.00	3.12	0.59	0.74	8.66	0.00	8.66	4.000	No	Yes	2.00
932	18.66	1.29	100.00	3.13	0.59	0.74	8.61	0.00	8.61	4.000	No	Yes	2.00
933	18.68	1.30	100.00	3.12	0.59	0.74	8.53	0.00	8.53	4.000	No	Yes	2.00
934	18.70	1.34	100.00	3.10	0.59	0.74	8.74	0.00	8.74	4.000	No	Yes	2.00
935	18.72	1.42	100.00	3.07	0.59	0.74	9.24	0.00	9.24	4.000	No	Yes	2.00
936	18.74	1.48	100.00	3.03	0.58	0.74	10.29	0.00	10.29	4.000	No	Yes	2.00
937	18.76	1.45	100.00	3.09	0.58	0.74	9.95	0.00	9.95	4.000	No	Yes	2.00
938	18.78	1.51	100.00	3.12	0.59	0.74	8.79	0.00	8.79	4.000	No	Yes	2.00
939	18.80	1.51	100.00	3.19	0.57	0.74	12.44	0.00	12.44	4.000	No	Yes	2.00
940	18.82	1.54	100.00	3.19	0.58	0.74	10.48	0.00	10.48	4.000	No	Yes	2.00
941	18.84	1.43	100.00	3.22	0.58	0.74	9.44	0.00	9.44	4.000	No	Yes	2.00
942	18.86	1.44	100.00	3.19	0.58	0.74	9.51	0.00	9.51	4.000	No	Yes	2.00
943	18.89	1.51	100.00	3.14	0.58	0.74	10.29	0.00	10.29	4.000	No	Yes	2.00
944	18.90	1.61	100.00	3.07	0.58	0.74	10.77	0.00	10.77	4.000	No	Yes	2.00
945	18.92	1.73	100.00	3.01	0.58	0.74	11.69	0.00	11.69	4.000	No	Yes	2.00
946	18.94	1.89	96.48	2.92	0.57	0.74	12.61	0.00	12.61	4.000	No	Yes	2.00
947	18.96	2.13	88.77	2.82	0.57	0.74	14.34	0.00	14.34	4.000	No	Yes	2.00
948	18.98	2.39	82.54	2.74	0.56	0.74	16.78	0.00	16.78	4.000	No	Yes	2.00
949	19.00	2.57	80.81	2.72	0.56	0.75	18.46	0.00	18.46	4.000	No	Yes	2.00
950	19.02	2.63	82.71	2.75	0.55	0.75	18.83	0.00	18.83	4.000	No	Yes	2.00
951	19.04	2.51	89.56	2.83	0.55	0.75	18.59	0.00	18.59	4.000	No	Yes	2.00
952	19.07	2.33	96.79	2.92	0.56	0.74	16.18	0.00	16.18	4.000	No	Yes	2.00
953	19.08	2.13	100.00	3.02	0.56	0.74	14.92	0.00	14.92	4.000	No	Yes	2.00
954	19.10	2.00	100.00	3.08	0.57	0.74	13.96	0.00	13.96	4.000	No	Yes	2.00
955	19.13	1.90	100.00	3.12	0.57	0.74	13.12	0.00	13.12	4.000	No	Yes	2.00
956	19.14	1.80	100.00	3.15	0.57	0.74	12.45	0.00	12.45	4.000	No	Yes	2.00
957	19.16	1.72	100.00	3.17	0.58	0.73	11.74	0.00	11.74	4.000	No	Yes	2.00
958	19.18	1.67	100.00	3.17	0.58	0.73	11.19	0.00	11.19	4.000	No	Yes	2.00
959	19.20	1.73	100.00	3.12	0.58	0.73	11.35	0.00	11.35	4.000	No	Yes	2.00
960	19.22	1.91	100.00	3.02	0.57	0.74	12.84	0.00	12.84	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
961	19.24	2.12	97.12	2.93	0.56	0.74	14.83	0.00	14.83	4.000	No	Yes	2.00
962	19.26	2.29	93.32	2.88	0.56	0.74	16.10	0.00	16.10	4.000	No	Yes	2.00
963	19.28	2.47	90.45	2.84	0.56	0.74	16.84	0.00	16.84	4.000	No	Yes	2.00
964	19.31	2.55	90.66	2.85	0.55	0.74	19.17	0.00	19.17	4.000	No	Yes	2.00
965	19.32	2.50	94.27	2.89	0.55	0.74	18.24	0.00	18.24	4.000	No	Yes	2.00
966	19.34	2.22	100.00	3.00	0.56	0.74	15.99	0.00	15.99	4.000	No	Yes	2.00
967	19.36	1.97	100.00	3.10	0.57	0.73	13.29	0.00	13.29	4.000	No	Yes	2.00
968	19.38	1.90	100.00	3.12	0.57	0.73	12.43	0.00	12.43	4.000	No	Yes	2.00
969	19.40	2.07	100.00	3.05	0.57	0.73	13.83	0.00	13.83	4.000	No	Yes	2.00
970	19.42	2.38	98.02	2.94	0.56	0.74	16.47	0.00	16.47	4.000	No	Yes	2.00
971	19.44	2.67	91.53	2.86	0.55	0.74	19.17	0.00	19.17	4.000	No	Yes	2.00
972	19.46	2.85	88.85	2.82	0.55	0.74	20.29	0.00	20.29	4.000	No	Yes	2.00
973	19.48	2.90	89.40	2.83	0.55	0.74	20.99	0.00	20.99	4.000	No	Yes	2.00
974	19.50	2.77	92.79	2.87	0.55	0.74	20.68	0.00	20.68	4.000	No	Yes	2.00
975	19.52	2.48	98.91	2.95	0.55	0.74	17.91	0.00	17.91	4.000	No	Yes	2.00
976	19.54	2.08	100.00	3.07	0.56	0.73	14.78	0.00	14.78	4.000	No	Yes	2.00
977	19.56	1.73	100.00	3.20	0.58	0.73	11.73	0.00	11.73	4.000	No	Yes	2.00
978	19.58	1.53	100.00	3.28	0.58	0.72	9.85	0.00	9.85	4.000	No	Yes	2.00
979	19.60	1.47	100.00	3.29	0.58	0.72	9.65	0.00	9.65	4.000	No	Yes	2.00
980	19.62	1.51	100.00	3.26	0.58	0.72	10.00	0.00	10.00	4.000	No	Yes	2.00
981	19.64	1.54	100.00	3.23	0.58	0.72	10.28	0.00	10.28	4.000	No	Yes	2.00
982	19.66	1.56	100.00	3.20	0.58	0.72	10.24	0.00	10.24	4.000	No	Yes	2.00
983	19.68	1.60	100.00	3.14	0.58	0.72	10.42	0.00	10.42	4.000	No	Yes	2.00
984	19.70	1.74	100.00	3.04	0.58	0.72	11.22	0.00	11.22	4.000	No	Yes	2.00
985	19.72	1.89	98.24	2.94	0.57	0.73	13.11	0.00	13.11	4.000	No	Yes	2.00
986	19.74	2.01	93.48	2.88	0.57	0.73	13.77	0.00	13.77	4.000	No	Yes	2.00
987	19.76	1.88	98.55	2.94	0.57	0.72	12.44	0.00	12.44	4.000	No	Yes	2.00

Abbreviations

Depth: Depth from free surface, at which CPT was performed (m)
q_t: Total cone resistance
FC: Fines content (%)
I_c: Soil behavior type index
m: Stress exponent
C_N: Overburden correction factor
q_{c1N}: Normalized and adjusted cone resistance
Δq_{c1N}: Cone resistance correction factor due to fines
$q_{c1N,cs}$: Normalized and adjusted cone resistance
$CRR_{7.5}$: Cyclic resistance ratio for M_w=7.5
FS: Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
0.02	2.00	0.00	9.99	0.02	0.00	0.04	2.00	0.00	9.98	0.02	0.00
0.06	2.00	0.00	9.97	0.02	0.00	0.08	2.00	0.00	9.96	0.02	0.00
0.10	2.00	0.00	9.95	0.02	0.00	0.12	2.00	0.00	9.94	0.02	0.00
0.14	2.00	0.00	9.93	0.02	0.00	0.16	2.00	0.00	9.92	0.02	0.00
0.18	2.00	0.00	9.91	0.02	0.00	0.20	2.00	0.00	9.90	0.02	0.00
0.22	2.00	0.00	9.89	0.02	0.00	0.24	2.00	0.00	9.88	0.02	0.00
0.26	2.00	0.00	9.87	0.02	0.00	0.28	2.00	0.00	9.86	0.02	0.00
0.30	2.00	0.00	9.85	0.02	0.00	0.32	2.00	0.00	9.84	0.02	0.00
0.34	2.00	0.00	9.83	0.02	0.00	0.36	2.00	0.00	9.82	0.02	0.00
0.38	2.00	0.00	9.81	0.02	0.00	0.40	2.00	0.00	9.80	0.02	0.00
0.42	2.00	0.00	9.79	0.02	0.00	0.44	2.00	0.00	9.78	0.02	0.00
0.46	2.00	0.00	9.77	0.02	0.00	0.48	2.00	0.00	9.76	0.02	0.00
0.50	2.00	0.00	9.75	0.02	0.00	0.52	2.00	0.00	9.74	0.02	0.00
0.54	2.00	0.00	9.73	0.02	0.00	0.56	2.00	0.00	9.72	0.02	0.00
0.58	2.00	0.00	9.71	0.02	0.00	0.60	2.00	0.00	9.70	0.02	0.00
0.62	2.00	0.00	9.69	0.02	0.00	0.64	2.00	0.00	9.68	0.02	0.00
0.66	2.00	0.00	9.67	0.02	0.00	0.68	2.00	0.00	9.66	0.02	0.00
0.70	2.00	0.00	9.65	0.02	0.00	0.72	2.00	0.00	9.64	0.02	0.00
0.74	2.00	0.00	9.63	0.02	0.00	0.76	2.00	0.00	9.62	0.02	0.00
0.78	2.00	0.00	9.61	0.02	0.00	0.80	2.00	0.00	9.60	0.02	0.00
0.82	2.00	0.00	9.59	0.02	0.00	0.84	2.00	0.00	9.58	0.02	0.00
0.86	2.00	0.00	9.57	0.02	0.00	0.88	2.00	0.00	9.56	0.02	0.00
0.90	2.00	0.00	9.55	0.02	0.00	0.92	2.00	0.00	9.54	0.02	0.00
0.95	2.00	0.00	9.53	0.03	0.00	0.96	2.00	0.00	9.52	0.01	0.00
0.98	2.00	0.00	9.51	0.02	0.00	1.00	2.00	0.00	9.50	0.02	0.00
1.02	2.00	0.00	9.49	0.02	0.00	1.05	2.00	0.00	9.48	0.03	0.00
1.06	2.00	0.00	9.47	0.01	0.00	1.08	2.00	0.00	9.46	0.02	0.00
1.10	2.00	0.00	9.45	0.02	0.00	1.12	2.00	0.00	9.44	0.02	0.00
1.14	2.00	0.00	9.43	0.02	0.00	1.16	2.00	0.00	9.42	0.02	0.00
1.18	2.00	0.00	9.41	0.02	0.00	1.20	2.00	0.00	9.40	0.02	0.00
1.22	2.00	0.00	9.39	0.02	0.00	1.24	2.00	0.00	9.38	0.02	0.00
1.26	2.00	0.00	9.37	0.02	0.00	1.28	2.00	0.00	9.36	0.02	0.00
1.30	2.00	0.00	9.35	0.02	0.00	1.32	2.00	0.00	9.34	0.02	0.00
1.34	2.00	0.00	9.33	0.02	0.00	1.36	2.00	0.00	9.32	0.02	0.00
1.38	2.00	0.00	9.31	0.02	0.00	1.40	2.00	0.00	9.30	0.02	0.00
1.44	2.00	0.00	9.28	0.04	0.00	1.44	2.00	0.00	9.28	0.00	0.00
1.51	2.00	0.00	9.24	0.07	0.00	1.51	2.00	0.00	9.24	0.00	0.00
1.51	2.00	0.00	9.24	0.00	0.00	1.52	2.00	0.00	9.24	0.01	0.00
1.54	2.00	0.00	9.23	0.02	0.00	1.56	2.00	0.00	9.22	0.02	0.00
1.58	2.00	0.00	9.21	0.02	0.00	1.60	2.00	0.00	9.20	0.02	0.00
1.62	2.00	0.00	9.19	0.02	0.00	1.64	2.00	0.00	9.18	0.02	0.00
1.66	2.00	0.00	9.17	0.02	0.00	1.68	2.00	0.00	9.16	0.02	0.00
1.70	2.00	0.00	9.15	0.02	0.00	1.72	2.00	0.00	9.14	0.02	0.00
1.74	2.00	0.00	9.13	0.02	0.00	1.76	2.00	0.00	9.12	0.02	0.00
1.78	2.00	0.00	9.11	0.02	0.00	1.81	2.00	0.00	9.10	0.03	0.00
1.82	2.00	0.00	9.09	0.01	0.00	1.84	2.00	0.00	9.08	0.02	0.00
1.86	2.00	0.00	9.07	0.02	0.00	1.88	2.00	0.00	9.06	0.02	0.00
1.90	2.00	0.00	9.05	0.02	0.00	1.92	2.00	0.00	9.04	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
1.94	2.00	0.00	9.03	0.02	0.00	1.97	2.00	0.00	9.02	0.03	0.00
1.98	2.00	0.00	9.01	0.01	0.00	2.00	2.00	0.00	9.00	0.02	0.00
2.02	2.00	0.00	8.99	0.02	0.00	2.04	2.00	0.00	8.98	0.02	0.00
2.06	2.00	0.00	8.97	0.02	0.00	2.08	2.00	0.00	8.96	0.02	0.00
2.10	2.00	0.00	8.95	0.02	0.00	2.13	2.00	0.00	8.94	0.03	0.00
2.14	2.00	0.00	8.93	0.01	0.00	2.16	2.00	0.00	8.92	0.02	0.00
2.18	2.00	0.00	8.91	0.02	0.00	2.20	2.00	0.00	8.90	0.02	0.00
2.22	2.00	0.00	8.89	0.02	0.00	2.24	2.00	0.00	8.88	0.02	0.00
2.26	2.00	0.00	8.87	0.02	0.00	2.28	2.00	0.00	8.86	0.02	0.00
2.30	2.00	0.00	8.85	0.02	0.00	2.32	2.00	0.00	8.84	0.02	0.00
2.34	2.00	0.00	8.83	0.02	0.00	2.36	2.00	0.00	8.82	0.02	0.00
2.38	2.00	0.00	8.81	0.02	0.00	2.40	2.00	0.00	8.80	0.02	0.00
2.42	2.00	0.00	8.79	0.02	0.00	2.45	2.00	0.00	8.78	0.03	0.00
2.46	2.00	0.00	8.77	0.01	0.00	2.48	2.00	0.00	8.76	0.02	0.00
2.50	2.00	0.00	8.75	0.02	0.00	2.52	2.00	0.00	8.74	0.02	0.00
2.54	2.00	0.00	8.73	0.02	0.00	2.56	2.00	0.00	8.72	0.02	0.00
2.58	2.00	0.00	8.71	0.02	0.00	2.60	2.00	0.00	8.70	0.02	0.00
2.62	2.00	0.00	8.69	0.02	0.00	2.64	2.00	0.00	8.68	0.02	0.00
2.66	2.00	0.00	8.67	0.02	0.00	2.68	2.00	0.00	8.66	0.02	0.00
2.70	2.00	0.00	8.65	0.02	0.00	2.72	2.00	0.00	8.64	0.02	0.00
2.74	2.00	0.00	8.63	0.02	0.00	2.76	2.00	0.00	8.62	0.02	0.00
2.78	2.00	0.00	8.61	0.02	0.00	2.80	2.00	0.00	8.60	0.02	0.00
2.82	2.00	0.00	8.59	0.02	0.00	2.84	2.00	0.00	8.58	0.02	0.00
2.86	2.00	0.00	8.57	0.02	0.00	2.88	2.00	0.00	8.56	0.02	0.00
2.90	2.00	0.00	8.55	0.02	0.00	2.92	2.00	0.00	8.54	0.02	0.00
2.94	2.00	0.00	8.53	0.02	0.00	2.97	2.00	0.00	8.52	0.03	0.00
2.98	2.00	0.00	8.51	0.01	0.00	3.00	2.00	0.00	8.50	0.02	0.00
3.02	2.00	0.00	8.49	0.02	0.00	3.04	2.00	0.00	8.48	0.02	0.00
3.07	2.00	0.00	8.47	0.03	0.00	3.08	2.00	0.00	8.46	0.01	0.00
3.10	2.00	0.00	8.45	0.02	0.00	3.12	2.00	0.00	8.44	0.02	0.00
3.14	2.00	0.00	8.43	0.02	0.00	3.16	2.00	0.00	8.42	0.02	0.00
3.18	2.00	0.00	8.41	0.02	0.00	3.21	2.00	0.00	8.40	0.03	0.00
3.22	2.00	0.00	8.39	0.01	0.00	3.24	2.00	0.00	8.38	0.02	0.00
3.26	2.00	0.00	8.37	0.02	0.00	3.28	2.00	0.00	8.36	0.02	0.00
3.30	2.00	0.00	8.35	0.02	0.00	3.32	2.00	0.00	8.34	0.02	0.00
3.34	2.00	0.00	8.33	0.02	0.00	3.36	2.00	0.00	8.32	0.02	0.00
3.38	2.00	0.00	8.31	0.02	0.00	3.40	2.00	0.00	8.30	0.02	0.00
3.42	2.00	0.00	8.29	0.02	0.00	3.44	2.00	0.00	8.28	0.02	0.00
3.48	2.00	0.00	8.26	0.04	0.00	3.49	2.00	0.00	8.26	0.01	0.00
3.50	2.00	0.00	8.25	0.01	0.00	3.52	2.00	0.00	8.24	0.02	0.00
3.54	2.00	0.00	8.23	0.02	0.00	3.56	2.00	0.00	8.22	0.02	0.00
3.58	2.00	0.00	8.21	0.02	0.00	3.60	2.00	0.00	8.20	0.02	0.00
3.62	2.00	0.00	8.19	0.02	0.00	3.64	2.00	0.00	8.18	0.02	0.00
3.66	2.00	0.00	8.17	0.02	0.00	3.68	2.00	0.00	8.16	0.02	0.00
3.70	2.00	0.00	8.15	0.02	0.00	3.72	2.00	0.00	8.14	0.02	0.00
3.74	2.00	0.00	8.13	0.02	0.00	3.76	2.00	0.00	8.12	0.02	0.00
3.78	2.00	0.00	8.11	0.02	0.00	3.80	2.00	0.00	8.10	0.02	0.00
3.82	2.00	0.00	8.09	0.02	0.00	3.84	2.00	0.00	8.08	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
3.86	2.00	0.00	8.07	0.02	0.00	3.88	2.00	0.00	8.06	0.02	0.00
3.90	2.00	0.00	8.05	0.02	0.00	3.92	2.00	0.00	8.04	0.02	0.00
3.94	2.00	0.00	8.03	0.02	0.00	3.96	2.00	0.00	8.02	0.02	0.00
3.98	2.00	0.00	8.01	0.02	0.00	4.00	2.00	0.00	8.00	0.02	0.00
4.02	2.00	0.00	7.99	0.02	0.00	4.04	2.00	0.00	7.98	0.02	0.00
4.06	2.00	0.00	7.97	0.02	0.00	4.08	2.00	0.00	7.96	0.02	0.00
4.10	2.00	0.00	7.95	0.02	0.00	4.12	2.00	0.00	7.94	0.02	0.00
4.14	2.00	0.00	7.93	0.02	0.00	4.16	2.00	0.00	7.92	0.02	0.00
4.18	2.00	0.00	7.91	0.02	0.00	4.20	2.00	0.00	7.90	0.02	0.00
4.22	2.00	0.00	7.89	0.02	0.00	4.25	2.00	0.00	7.88	0.03	0.00
4.26	2.00	0.00	7.87	0.01	0.00	4.28	2.00	0.00	7.86	0.02	0.00
4.30	2.00	0.00	7.85	0.02	0.00	4.32	2.00	0.00	7.84	0.02	0.00
4.34	2.00	0.00	7.83	0.02	0.00	4.36	2.00	0.00	7.82	0.02	0.00
4.38	2.00	0.00	7.81	0.02	0.00	4.40	2.00	0.00	7.80	0.02	0.00
4.42	2.00	0.00	7.79	0.02	0.00	4.44	2.00	0.00	7.78	0.02	0.00
4.47	2.00	0.00	7.77	0.03	0.00	4.48	2.00	0.00	7.76	0.01	0.00
4.50	2.00	0.00	7.75	0.02	0.00	4.52	2.00	0.00	7.74	0.02	0.00
4.54	2.00	0.00	7.73	0.02	0.00	4.56	2.00	0.00	7.72	0.02	0.00
4.59	2.00	0.00	7.71	0.03	0.00	4.60	2.00	0.00	7.70	0.01	0.00
4.62	2.00	0.00	7.69	0.02	0.00	4.64	2.00	0.00	7.68	0.02	0.00
4.66	2.00	0.00	7.67	0.02	0.00	4.68	2.00	0.00	7.66	0.02	0.00
4.70	2.00	0.00	7.65	0.02	0.00	4.72	2.00	0.00	7.64	0.02	0.00
4.74	2.00	0.00	7.63	0.02	0.00	4.76	2.00	0.00	7.62	0.02	0.00
4.78	2.00	0.00	7.61	0.02	0.00	4.80	2.00	0.00	7.60	0.02	0.00
4.82	2.00	0.00	7.59	0.02	0.00	4.84	2.00	0.00	7.58	0.02	0.00
4.86	2.00	0.00	7.57	0.02	0.00	4.88	2.00	0.00	7.56	0.02	0.00
4.90	2.00	0.00	7.55	0.02	0.00	4.92	2.00	0.00	7.54	0.02	0.00
4.94	2.00	0.00	7.53	0.02	0.00	4.97	2.00	0.00	7.52	0.03	0.00
4.98	2.00	0.00	7.51	0.01	0.00	5.00	2.00	0.00	7.50	0.02	0.00
5.02	2.00	0.00	7.49	0.02	0.00	5.04	2.00	0.00	7.48	0.02	0.00
5.07	2.00	0.00	7.47	0.03	0.00	5.08	2.00	0.00	7.46	0.01	0.00
5.10	2.00	0.00	7.45	0.02	0.00	5.12	2.00	0.00	7.44	0.02	0.00
5.14	2.00	0.00	7.43	0.02	0.00	5.16	2.00	0.00	7.42	0.02	0.00
5.18	2.00	0.00	7.41	0.02	0.00	5.21	2.00	0.00	7.40	0.03	0.00
5.22	2.00	0.00	7.39	0.01	0.00	5.24	2.00	0.00	7.38	0.02	0.00
5.26	2.00	0.00	7.37	0.02	0.00	5.28	2.00	0.00	7.36	0.02	0.00
5.30	2.00	0.00	7.35	0.02	0.00	5.32	2.00	0.00	7.34	0.02	0.00
5.34	2.00	0.00	7.33	0.02	0.00	5.36	2.00	0.00	7.32	0.02	0.00
5.38	2.00	0.00	7.31	0.02	0.00	5.40	2.00	0.00	7.30	0.02	0.00
5.42	2.00	0.00	7.29	0.02	0.00	5.44	2.00	0.00	7.28	0.02	0.00
5.46	2.00	0.00	7.27	0.02	0.00	5.52	2.00	0.00	7.24	0.06	0.00
5.52	2.00	0.00	7.24	0.00	0.00	5.52	2.00	0.00	7.24	0.00	0.00
5.54	2.00	0.00	7.23	0.02	0.00	5.56	2.00	0.00	7.22	0.02	0.00
5.58	2.00	0.00	7.21	0.02	0.00	5.60	2.00	0.00	7.20	0.02	0.00
5.62	2.00	0.00	7.19	0.02	0.00	5.64	2.00	0.00	7.18	0.02	0.00
5.66	2.00	0.00	7.17	0.02	0.00	5.68	2.00	0.00	7.16	0.02	0.00
5.70	2.00	0.00	7.15	0.02	0.00	5.72	2.00	0.00	7.14	0.02	0.00
5.74	2.00	0.00	7.13	0.02	0.00	5.76	2.00	0.00	7.12	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
5.78	2.00	0.00	7.11	0.02	0.00	5.80	2.00	0.00	7.10	0.02	0.00
5.82	2.00	0.00	7.09	0.02	0.00	5.84	2.00	0.00	7.08	0.02	0.00
5.86	2.00	0.00	7.07	0.02	0.00	5.88	2.00	0.00	7.06	0.02	0.00
5.90	2.00	0.00	7.05	0.02	0.00	5.92	2.00	0.00	7.04	0.02	0.00
5.94	2.00	0.00	7.03	0.02	0.00	5.96	2.00	0.00	7.02	0.02	0.00
5.98	2.00	0.00	7.01	0.02	0.00	6.01	2.00	0.00	7.00	0.03	0.00
6.02	2.00	0.00	6.99	0.01	0.00	6.04	2.00	0.00	6.98	0.02	0.00
6.07	2.00	0.00	6.97	0.03	0.00	6.08	2.00	0.00	6.96	0.01	0.00
6.10	2.00	0.00	6.95	0.02	0.00	6.12	2.00	0.00	6.94	0.02	0.00
6.14	2.00	0.00	6.93	0.02	0.00	6.16	2.00	0.00	6.92	0.02	0.00
6.18	2.00	0.00	6.91	0.02	0.00	6.20	2.00	0.00	6.90	0.02	0.00
6.22	2.00	0.00	6.89	0.02	0.00	6.24	2.00	0.00	6.88	0.02	0.00
6.26	2.00	0.00	6.87	0.02	0.00	6.28	2.00	0.00	6.86	0.02	0.00
6.30	2.00	0.00	6.85	0.02	0.00	6.32	2.00	0.00	6.84	0.02	0.00
6.34	2.00	0.00	6.83	0.02	0.00	6.36	2.00	0.00	6.82	0.02	0.00
6.38	2.00	0.00	6.81	0.02	0.00	6.40	2.00	0.00	6.80	0.02	0.00
6.42	2.00	0.00	6.79	0.02	0.00	6.44	2.00	0.00	6.78	0.02	0.00
6.46	2.00	0.00	6.77	0.02	0.00	6.48	2.00	0.00	6.76	0.02	0.00
6.50	2.00	0.00	6.75	0.02	0.00	6.52	2.00	0.00	6.74	0.02	0.00
6.54	2.00	0.00	6.73	0.02	0.00	6.56	2.00	0.00	6.72	0.02	0.00
6.58	2.00	0.00	6.71	0.02	0.00	6.60	2.00	0.00	6.70	0.02	0.00
6.62	2.00	0.00	6.69	0.02	0.00	6.64	2.00	0.00	6.68	0.02	0.00
6.66	2.00	0.00	6.67	0.02	0.00	6.69	2.00	0.00	6.66	0.03	0.00
6.70	2.00	0.00	6.65	0.01	0.00	6.72	2.00	0.00	6.64	0.02	0.00
6.74	2.00	0.00	6.63	0.02	0.00	6.76	2.00	0.00	6.62	0.02	0.00
6.78	2.00	0.00	6.61	0.02	0.00	6.80	2.00	0.00	6.60	0.02	0.00
6.82	2.00	0.00	6.59	0.02	0.00	6.84	2.00	0.00	6.58	0.02	0.00
6.86	2.00	0.00	6.57	0.02	0.00	6.88	2.00	0.00	6.56	0.02	0.00
6.90	2.00	0.00	6.55	0.02	0.00	6.92	2.00	0.00	6.54	0.02	0.00
6.94	2.00	0.00	6.53	0.02	0.00	6.96	2.00	0.00	6.52	0.02	0.00
6.98	2.00	0.00	6.51	0.02	0.00	7.00	2.00	0.00	6.50	0.02	0.00
7.02	2.00	0.00	6.49	0.02	0.00	7.04	2.00	0.00	6.48	0.02	0.00
7.06	2.00	0.00	6.47	0.02	0.00	7.08	2.00	0.00	6.46	0.02	0.00
7.10	2.00	0.00	6.45	0.02	0.00	7.12	2.00	0.00	6.44	0.02	0.00
7.14	2.00	0.00	6.43	0.02	0.00	7.16	2.00	0.00	6.42	0.02	0.00
7.18	2.00	0.00	6.41	0.02	0.00	7.20	2.00	0.00	6.40	0.02	0.00
7.22	2.00	0.00	6.39	0.02	0.00	7.24	2.00	0.00	6.38	0.02	0.00
7.26	2.00	0.00	6.37	0.02	0.00	7.28	2.00	0.00	6.36	0.02	0.00
7.30	2.00	0.00	6.35	0.02	0.00	7.32	2.00	0.00	6.34	0.02	0.00
7.34	2.00	0.00	6.33	0.02	0.00	7.36	2.00	0.00	6.32	0.02	0.00
7.38	2.00	0.00	6.31	0.02	0.00	7.40	2.00	0.00	6.30	0.02	0.00
7.42	2.00	0.00	6.29	0.02	0.00	7.44	2.00	0.00	6.28	0.02	0.00
7.46	2.00	0.00	6.27	0.02	0.00	7.48	2.00	0.00	6.26	0.02	0.00
7.50	2.00	0.00	6.25	0.02	0.00	7.52	2.00	0.00	6.24	0.02	0.00
7.54	2.00	0.00	6.23	0.02	0.00	7.56	2.00	0.00	6.22	0.02	0.00
7.58	2.00	0.00	6.21	0.02	0.00	7.60	2.00	0.00	6.20	0.02	0.00
7.62	2.00	0.00	6.19	0.02	0.00	7.64	2.00	0.00	6.18	0.02	0.00
7.66	2.00	0.00	6.17	0.02	0.00	7.68	2.00	0.00	6.16	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
7.70	2.00	0.00	6.15	0.02	0.00	7.72	2.00	0.00	6.14	0.02	0.00
7.74	2.00	0.00	6.13	0.02	0.00	7.76	2.00	0.00	6.12	0.02	0.00
7.78	2.00	0.00	6.11	0.02	0.00	7.80	2.00	0.00	6.10	0.02	0.00
7.82	2.00	0.00	6.09	0.02	0.00	7.84	2.00	0.00	6.08	0.02	0.00
7.86	2.00	0.00	6.07	0.02	0.00	7.88	2.00	0.00	6.06	0.02	0.00
7.90	2.00	0.00	6.05	0.02	0.00	7.92	2.00	0.00	6.04	0.02	0.00
7.94	2.00	0.00	6.03	0.02	0.00	7.96	2.00	0.00	6.02	0.02	0.00
7.98	2.00	0.00	6.01	0.02	0.00	8.00	2.00	0.00	6.00	0.02	0.00
8.02	2.00	0.00	5.99	0.02	0.00	8.04	2.00	0.00	5.98	0.02	0.00
8.06	2.00	0.00	5.97	0.02	0.00	8.08	2.00	0.00	5.96	0.02	0.00
8.10	2.00	0.00	5.95	0.02	0.00	8.12	2.00	0.00	5.94	0.02	0.00
8.15	2.00	0.00	5.93	0.03	0.00	8.16	2.00	0.00	5.92	0.01	0.00
8.18	2.00	0.00	5.91	0.02	0.00	8.20	2.00	0.00	5.90	0.02	0.00
8.22	2.00	0.00	5.89	0.02	0.00	8.24	2.00	0.00	5.88	0.02	0.00
8.26	2.00	0.00	5.87	0.02	0.00	8.28	2.00	0.00	5.86	0.02	0.00
8.30	2.00	0.00	5.85	0.02	0.00	8.32	2.00	0.00	5.84	0.02	0.00
8.34	2.00	0.00	5.83	0.02	0.00	8.36	2.00	0.00	5.82	0.02	0.00
8.38	2.00	0.00	5.81	0.02	0.00	8.40	2.00	0.00	5.80	0.02	0.00
8.42	2.00	0.00	5.79	0.02	0.00	8.44	2.00	0.00	5.78	0.02	0.00
8.46	2.00	0.00	5.77	0.02	0.00	8.48	2.00	0.00	5.76	0.02	0.00
8.50	2.00	0.00	5.75	0.02	0.00	8.52	2.00	0.00	5.74	0.02	0.00
8.54	2.00	0.00	5.73	0.02	0.00	8.56	2.00	0.00	5.72	0.02	0.00
8.58	2.00	0.00	5.71	0.02	0.00	8.60	2.00	0.00	5.70	0.02	0.00
8.62	2.00	0.00	5.69	0.02	0.00	8.64	2.00	0.00	5.68	0.02	0.00
8.66	2.00	0.00	5.67	0.02	0.00	8.68	2.00	0.00	5.66	0.02	0.00
8.70	2.00	0.00	5.65	0.02	0.00	8.72	2.00	0.00	5.64	0.02	0.00
8.74	2.00	0.00	5.63	0.02	0.00	8.76	2.00	0.00	5.62	0.02	0.00
8.78	2.00	0.00	5.61	0.02	0.00	8.80	2.00	0.00	5.60	0.02	0.00
8.82	2.00	0.00	5.59	0.02	0.00	8.84	2.00	0.00	5.58	0.02	0.00
8.86	2.00	0.00	5.57	0.02	0.00	8.88	2.00	0.00	5.56	0.02	0.00
8.90	2.00	0.00	5.55	0.02	0.00	8.93	2.00	0.00	5.54	0.03	0.00
8.94	2.00	0.00	5.53	0.01	0.00	8.96	2.00	0.00	5.52	0.02	0.00
8.98	2.00	0.00	5.51	0.02	0.00	9.00	2.00	0.00	5.50	0.02	0.00
9.02	2.00	0.00	5.49	0.02	0.00	9.04	2.00	0.00	5.48	0.02	0.00
9.06	2.00	0.00	5.47	0.02	0.00	9.08	2.00	0.00	5.46	0.02	0.00
9.10	2.00	0.00	5.45	0.02	0.00	9.12	2.00	0.00	5.44	0.02	0.00
9.14	2.00	0.00	5.43	0.02	0.00	9.16	2.00	0.00	5.42	0.02	0.00
9.18	2.00	0.00	5.41	0.02	0.00	9.20	2.00	0.00	5.40	0.02	0.00
9.22	2.00	0.00	5.39	0.02	0.00	9.24	2.00	0.00	5.38	0.02	0.00
9.26	2.00	0.00	5.37	0.02	0.00	9.28	2.00	0.00	5.36	0.02	0.00
9.30	2.00	0.00	5.35	0.02	0.00	9.32	2.00	0.00	5.34	0.02	0.00
9.34	2.00	0.00	5.33	0.02	0.00	9.36	2.00	0.00	5.32	0.02	0.00
9.38	2.00	0.00	5.31	0.02	0.00	9.40	2.00	0.00	5.30	0.02	0.00
9.42	2.00	0.00	5.29	0.02	0.00	9.44	2.00	0.00	5.28	0.02	0.00
9.46	2.00	0.00	5.27	0.02	0.00	9.48	2.00	0.00	5.26	0.02	0.00
9.50	2.00	0.00	5.25	0.02	0.00	9.52	2.00	0.00	5.24	0.02	0.00
9.54	2.00	0.00	5.23	0.02	0.00	9.56	2.00	0.00	5.22	0.02	0.00
9.58	2.00	0.00	5.21	0.02	0.00	9.60	2.00	0.00	5.20	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
9.62	2.00	0.00	5.19	0.02	0.00	9.64	2.00	0.00	5.18	0.02	0.00
9.66	2.00	0.00	5.17	0.02	0.00	9.68	2.00	0.00	5.16	0.02	0.00
9.70	2.00	0.00	5.15	0.02	0.00	9.72	2.00	0.00	5.14	0.02	0.00
9.74	2.00	0.00	5.13	0.02	0.00	9.76	2.00	0.00	5.12	0.02	0.00
9.78	2.00	0.00	5.11	0.02	0.00	9.80	2.00	0.00	5.10	0.02	0.00
9.82	2.00	0.00	5.09	0.02	0.00	9.84	2.00	0.00	5.08	0.02	0.00
9.86	2.00	0.00	5.07	0.02	0.00	9.88	2.00	0.00	5.06	0.02	0.00
9.90	2.00	0.00	5.05	0.02	0.00	9.92	2.00	0.00	5.04	0.02	0.00
9.95	2.00	0.00	5.03	0.03	0.00	9.96	2.00	0.00	5.02	0.01	0.00
9.98	2.00	0.00	5.01	0.02	0.00	10.00	2.00	0.00	5.00	0.02	0.00
10.02	2.00	0.00	4.99	0.02	0.00	10.04	2.00	0.00	4.98	0.02	0.00
10.06	2.00	0.00	4.97	0.02	0.00	10.08	2.00	0.00	4.96	0.02	0.00
10.10	2.00	0.00	4.95	0.02	0.00	10.12	2.00	0.00	4.94	0.02	0.00
10.14	2.00	0.00	4.93	0.02	0.00	10.16	2.00	0.00	4.92	0.02	0.00
10.18	2.00	0.00	4.91	0.02	0.00	10.20	2.00	0.00	4.90	0.02	0.00
10.22	2.00	0.00	4.89	0.02	0.00	10.24	2.00	0.00	4.88	0.02	0.00
10.26	2.00	0.00	4.87	0.02	0.00	10.28	2.00	0.00	4.86	0.02	0.00
10.30	2.00	0.00	4.85	0.02	0.00	10.32	2.00	0.00	4.84	0.02	0.00
10.34	2.00	0.00	4.83	0.02	0.00	10.36	2.00	0.00	4.82	0.02	0.00
10.38	2.00	0.00	4.81	0.02	0.00	10.40	2.00	0.00	4.80	0.02	0.00
10.42	2.00	0.00	4.79	0.02	0.00	10.44	2.00	0.00	4.78	0.02	0.00
10.46	2.00	0.00	4.77	0.02	0.00	10.48	2.00	0.00	4.76	0.02	0.00
10.50	2.00	0.00	4.75	0.02	0.00	10.52	2.00	0.00	4.74	0.02	0.00
10.54	2.00	0.00	4.73	0.02	0.00	10.56	2.00	0.00	4.72	0.02	0.00
10.58	2.00	0.00	4.71	0.02	0.00	10.60	2.00	0.00	4.70	0.02	0.00
10.62	2.00	0.00	4.69	0.02	0.00	10.64	2.00	0.00	4.68	0.02	0.00
10.66	2.00	0.00	4.67	0.02	0.00	10.68	2.00	0.00	4.66	0.02	0.00
10.70	2.00	0.00	4.65	0.02	0.00	10.72	2.00	0.00	4.64	0.02	0.00
10.74	2.00	0.00	4.63	0.02	0.00	10.76	2.00	0.00	4.62	0.02	0.00
10.78	2.00	0.00	4.61	0.02	0.00	10.80	2.00	0.00	4.60	0.02	0.00
10.82	2.00	0.00	4.59	0.02	0.00	10.84	2.00	0.00	4.58	0.02	0.00
10.86	2.00	0.00	4.57	0.02	0.00	10.88	2.00	0.00	4.56	0.02	0.00
10.90	2.00	0.00	4.55	0.02	0.00	10.92	2.00	0.00	4.54	0.02	0.00
10.94	2.00	0.00	4.53	0.02	0.00	10.96	2.00	0.00	4.52	0.02	0.00
10.98	2.00	0.00	4.51	0.02	0.00	11.00	2.00	0.00	4.50	0.02	0.00
11.02	2.00	0.00	4.49	0.02	0.00	11.04	2.00	0.00	4.48	0.02	0.00
11.06	2.00	0.00	4.47	0.02	0.00	11.08	2.00	0.00	4.46	0.02	0.00
11.10	2.00	0.00	4.45	0.02	0.00	11.13	2.00	0.00	4.43	0.03	0.00
11.14	2.00	0.00	4.43	0.01	0.00	11.17	2.00	0.00	4.42	0.03	0.00
11.18	2.00	0.00	4.41	0.01	0.00	11.20	2.00	0.00	4.40	0.02	0.00
11.22	2.00	0.00	4.39	0.02	0.00	11.24	2.00	0.00	4.38	0.02	0.00
11.26	2.00	0.00	4.37	0.02	0.00	11.28	2.00	0.00	4.36	0.02	0.00
11.30	2.00	0.00	4.35	0.02	0.00	11.32	2.00	0.00	4.34	0.02	0.00
11.34	2.00	0.00	4.33	0.02	0.00	11.36	2.00	0.00	4.32	0.02	0.00
11.39	2.00	0.00	4.31	0.03	0.00	11.40	2.00	0.00	4.30	0.01	0.00
11.42	2.00	0.00	4.29	0.02	0.00	11.44	2.00	0.00	4.28	0.02	0.00
11.46	2.00	0.00	4.27	0.02	0.00	11.48	2.00	0.00	4.26	0.02	0.00
11.50	2.00	0.00	4.25	0.02	0.00	11.52	2.00	0.00	4.24	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
11.54	2.00	0.00	4.23	0.02	0.00	11.56	2.00	0.00	4.22	0.02	0.00
11.58	2.00	0.00	4.21	0.02	0.00	11.60	2.00	0.00	4.20	0.02	0.00
11.62	2.00	0.00	4.19	0.02	0.00	11.64	2.00	0.00	4.18	0.02	0.00
11.66	2.00	0.00	4.17	0.02	0.00	11.68	2.00	0.00	4.16	0.02	0.00
11.70	2.00	0.00	4.15	0.02	0.00	11.72	2.00	0.00	4.14	0.02	0.00
11.75	2.00	0.00	4.13	0.03	0.00	11.76	2.00	0.00	4.12	0.01	0.00
11.78	2.00	0.00	4.11	0.02	0.00	11.80	2.00	0.00	4.10	0.02	0.00
11.82	2.00	0.00	4.09	0.02	0.00	11.84	2.00	0.00	4.08	0.02	0.00
11.86	2.00	0.00	4.07	0.02	0.00	11.88	2.00	0.00	4.06	0.02	0.00
11.91	2.00	0.00	4.05	0.03	0.00	11.92	2.00	0.00	4.04	0.01	0.00
11.94	2.00	0.00	4.03	0.02	0.00	11.96	2.00	0.00	4.02	0.02	0.00
11.98	2.00	0.00	4.01	0.02	0.00	12.00	2.00	0.00	4.00	0.02	0.00
12.02	2.00	0.00	3.99	0.02	0.00	12.04	2.00	0.00	3.98	0.02	0.00
12.06	2.00	0.00	3.97	0.02	0.00	12.08	2.00	0.00	3.96	0.02	0.00
12.10	2.00	0.00	3.95	0.02	0.00	12.20	2.00	0.00	3.90	0.10	0.00
12.20	2.00	0.00	3.90	0.00	0.00	12.11	2.00	0.00	3.95	0.09	0.00
12.20	2.00	0.00	3.90	0.09	0.00	12.22	2.00	0.00	3.89	0.02	0.00
12.24	2.00	0.00	3.88	0.02	0.00	12.26	2.00	0.00	3.87	0.02	0.00
12.28	2.00	0.00	3.86	0.02	0.00	12.30	2.00	0.00	3.85	0.02	0.00
12.32	2.00	0.00	3.84	0.02	0.00	12.34	2.00	0.00	3.83	0.02	0.00
12.36	2.00	0.00	3.82	0.02	0.00	12.38	2.00	0.00	3.81	0.02	0.00
12.40	2.00	0.00	3.80	0.02	0.00	12.42	2.00	0.00	3.79	0.02	0.00
12.44	2.00	0.00	3.78	0.02	0.00	12.46	2.00	0.00	3.77	0.02	0.00
12.48	2.00	0.00	3.76	0.02	0.00	12.50	2.00	0.00	3.75	0.02	0.00
12.52	2.00	0.00	3.74	0.02	0.00	12.55	2.00	0.00	3.73	0.03	0.00
12.56	2.00	0.00	3.72	0.01	0.00	12.58	2.00	0.00	3.71	0.02	0.00
12.60	2.00	0.00	3.70	0.02	0.00	12.62	2.00	0.00	3.69	0.02	0.00
12.64	2.00	0.00	3.68	0.02	0.00	12.66	2.00	0.00	3.67	0.02	0.00
12.68	2.00	0.00	3.66	0.02	0.00	12.70	2.00	0.00	3.65	0.02	0.00
12.72	2.00	0.00	3.64	0.02	0.00	12.74	2.00	0.00	3.63	0.02	0.00
12.76	2.00	0.00	3.62	0.02	0.00	12.78	2.00	0.00	3.61	0.02	0.00
12.80	2.00	0.00	3.60	0.02	0.00	12.83	2.00	0.00	3.59	0.03	0.00
12.84	2.00	0.00	3.58	0.01	0.00	12.86	2.00	0.00	3.57	0.02	0.00
12.88	2.00	0.00	3.56	0.02	0.00	12.90	2.00	0.00	3.55	0.02	0.00
12.92	2.00	0.00	3.54	0.02	0.00	12.94	2.00	0.00	3.53	0.02	0.00
12.96	2.00	0.00	3.52	0.02	0.00	12.98	2.00	0.00	3.51	0.02	0.00
13.00	2.00	0.00	3.50	0.02	0.00	13.02	2.00	0.00	3.49	0.02	0.00
13.04	2.00	0.00	3.48	0.02	0.00	13.06	2.00	0.00	3.47	0.02	0.00
13.08	2.00	0.00	3.46	0.02	0.00	13.10	2.00	0.00	3.45	0.02	0.00
13.12	2.00	0.00	3.44	0.02	0.00	13.14	2.00	0.00	3.43	0.02	0.00
13.16	2.00	0.00	3.42	0.02	0.00	13.18	2.00	0.00	3.41	0.02	0.00
13.20	2.00	0.00	3.40	0.02	0.00	13.22	2.00	0.00	3.39	0.02	0.00
13.24	2.00	0.00	3.38	0.02	0.00	13.26	2.00	0.00	3.37	0.02	0.00
13.28	2.00	0.00	3.36	0.02	0.00	13.30	2.00	0.00	3.35	0.02	0.00
13.32	2.00	0.00	3.34	0.02	0.00	13.34	2.00	0.00	3.33	0.02	0.00
13.36	2.00	0.00	3.32	0.02	0.00	13.41	2.00	0.00	3.30	0.05	0.00
13.41	2.00	0.00	3.30	0.00	0.00	13.42	2.00	0.00	3.29	0.01	0.00
13.44	2.00	0.00	3.28	0.02	0.00	13.46	2.00	0.00	3.27	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
13.48	2.00	0.00	3.26	0.02	0.00	13.50	2.00	0.00	3.25	0.02	0.00
13.52	2.00	0.00	3.24	0.02	0.00	13.54	2.00	0.00	3.23	0.02	0.00
13.56	0.56	0.44	3.22	0.02	0.03	13.58	0.56	0.44	3.21	0.02	0.03
13.60	2.00	0.00	3.20	0.02	0.00	13.62	2.00	0.00	3.19	0.02	0.00
13.64	2.00	0.00	3.18	0.02	0.00	13.66	2.00	0.00	3.17	0.02	0.00
13.68	2.00	0.00	3.16	0.02	0.00	13.70	2.00	0.00	3.15	0.02	0.00
13.72	2.00	0.00	3.14	0.02	0.00	13.74	2.00	0.00	3.13	0.02	0.00
13.76	2.00	0.00	3.12	0.02	0.00	13.78	2.00	0.00	3.11	0.02	0.00
13.80	2.00	0.00	3.10	0.02	0.00	13.83	2.00	0.00	3.09	0.03	0.00
13.84	2.00	0.00	3.08	0.01	0.00	13.86	2.00	0.00	3.07	0.02	0.00
14.03	2.00	0.00	2.99	0.17	0.00	14.03	2.00	0.00	2.99	0.00	0.00
14.03	2.00	0.00	2.99	0.00	0.00	13.88	2.00	0.00	3.06	0.15	0.00
13.96	2.00	0.00	3.02	0.08	0.00	13.98	2.00	0.00	3.01	0.02	0.00
14.00	2.00	0.00	3.00	0.02	0.00	14.02	2.00	0.00	2.99	0.02	0.00
14.04	2.00	0.00	2.98	0.02	0.00	14.06	2.00	0.00	2.97	0.02	0.00
14.08	2.00	0.00	2.96	0.02	0.00	14.10	2.00	0.00	2.95	0.02	0.00
14.12	2.00	0.00	2.94	0.02	0.00	14.14	2.00	0.00	2.93	0.02	0.00
14.16	2.00	0.00	2.92	0.02	0.00	14.18	2.00	0.00	2.91	0.02	0.00
14.21	2.00	0.00	2.90	0.03	0.00	14.22	2.00	0.00	2.89	0.01	0.00
14.24	2.00	0.00	2.88	0.02	0.00	14.26	2.00	0.00	2.87	0.02	0.00
14.28	2.00	0.00	2.86	0.02	0.00	14.30	2.00	0.00	2.85	0.02	0.00
14.32	2.00	0.00	2.84	0.02	0.00	14.37	2.00	0.00	2.82	0.05	0.00
14.37	2.00	0.00	2.82	0.00	0.00	14.38	2.00	0.00	2.81	0.01	0.00
14.40	2.00	0.00	2.80	0.02	0.00	14.42	2.00	0.00	2.79	0.02	0.00
14.44	2.00	0.00	2.78	0.02	0.00	14.46	2.00	0.00	2.77	0.02	0.00
14.48	2.00	0.00	2.76	0.02	0.00	14.50	2.00	0.00	2.75	0.02	0.00
14.52	2.00	0.00	2.74	0.02	0.00	14.54	2.00	0.00	2.73	0.02	0.00
14.56	2.00	0.00	2.72	0.02	0.00	14.58	2.00	0.00	2.71	0.02	0.00
14.60	2.00	0.00	2.70	0.02	0.00	14.62	2.00	0.00	2.69	0.02	0.00
14.64	2.00	0.00	2.68	0.02	0.00	14.66	2.00	0.00	2.67	0.02	0.00
14.68	2.00	0.00	2.66	0.02	0.00	14.70	2.00	0.00	2.65	0.02	0.00
14.72	2.00	0.00	2.64	0.02	0.00	14.74	2.00	0.00	2.63	0.02	0.00
14.76	2.00	0.00	2.62	0.02	0.00	14.78	2.00	0.00	2.61	0.02	0.00
14.80	2.00	0.00	2.60	0.02	0.00	14.82	2.00	0.00	2.59	0.02	0.00
14.84	2.00	0.00	2.58	0.02	0.00	14.86	2.00	0.00	2.57	0.02	0.00
14.88	2.00	0.00	2.56	0.02	0.00	14.90	2.00	0.00	2.55	0.02	0.00
14.92	2.00	0.00	2.54	0.02	0.00	14.94	2.00	0.00	2.53	0.02	0.00
14.96	2.00	0.00	2.52	0.02	0.00	14.98	2.00	0.00	2.51	0.02	0.00
15.00	2.00	0.00	2.50	0.02	0.00	15.02	2.00	0.00	2.49	0.02	0.00
15.04	2.00	0.00	2.48	0.02	0.00	15.06	2.00	0.00	2.47	0.02	0.00
15.08	2.00	0.00	2.46	0.02	0.00	15.10	2.00	0.00	2.45	0.02	0.00
15.12	2.00	0.00	2.44	0.02	0.00	15.14	2.00	0.00	2.43	0.02	0.00
15.16	2.00	0.00	2.42	0.02	0.00	15.18	2.00	0.00	2.41	0.02	0.00
15.20	2.00	0.00	2.40	0.02	0.00	15.22	2.00	0.00	2.39	0.02	0.00
15.24	2.00	0.00	2.38	0.02	0.00	15.26	2.00	0.00	2.37	0.02	0.00
15.28	2.00	0.00	2.36	0.02	0.00	15.30	2.00	0.00	2.35	0.02	0.00
15.32	2.00	0.00	2.34	0.02	0.00	15.34	2.00	0.00	2.33	0.02	0.00
15.36	2.00	0.00	2.32	0.02	0.00	15.38	2.00	0.00	2.31	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
15.40	2.00	0.00	2.30	0.02	0.00	15.42	2.00	0.00	2.29	0.02	0.00
15.44	2.00	0.00	2.28	0.02	0.00	15.46	2.00	0.00	2.27	0.02	0.00
15.48	2.00	0.00	2.26	0.02	0.00	15.50	2.00	0.00	2.25	0.02	0.00
15.52	2.00	0.00	2.24	0.02	0.00	15.54	2.00	0.00	2.23	0.02	0.00
15.56	2.00	0.00	2.22	0.02	0.00	15.58	2.00	0.00	2.21	0.02	0.00
15.60	2.00	0.00	2.20	0.02	0.00	15.62	2.00	0.00	2.19	0.02	0.00
15.64	2.00	0.00	2.18	0.02	0.00	15.66	2.00	0.00	2.17	0.02	0.00
15.68	2.00	0.00	2.16	0.02	0.00	15.70	2.00	0.00	2.15	0.02	0.00
15.72	2.00	0.00	2.14	0.02	0.00	15.74	2.00	0.00	2.13	0.02	0.00
15.76	2.00	0.00	2.12	0.02	0.00	15.78	2.00	0.00	2.11	0.02	0.00
15.80	2.00	0.00	2.10	0.02	0.00	15.82	2.00	0.00	2.09	0.02	0.00
15.84	2.00	0.00	2.08	0.02	0.00	15.86	2.00	0.00	2.07	0.02	0.00
15.88	2.00	0.00	2.06	0.02	0.00	15.90	2.00	0.00	2.05	0.02	0.00
15.92	2.00	0.00	2.04	0.02	0.00	15.94	2.00	0.00	2.03	0.02	0.00
15.96	2.00	0.00	2.02	0.02	0.00	15.98	2.00	0.00	2.01	0.02	0.00
16.00	2.00	0.00	2.00	0.02	0.00	16.02	2.00	0.00	1.99	0.02	0.00
16.04	2.00	0.00	1.98	0.02	0.00	16.07	2.00	0.00	1.97	0.03	0.00
16.08	2.00	0.00	1.96	0.01	0.00	16.10	2.00	0.00	1.95	0.02	0.00
16.12	2.00	0.00	1.94	0.02	0.00	16.14	2.00	0.00	1.93	0.02	0.00
16.16	2.00	0.00	1.92	0.02	0.00	16.18	2.00	0.00	1.91	0.02	0.00
16.20	2.00	0.00	1.90	0.02	0.00	16.22	2.00	0.00	1.89	0.02	0.00
16.24	2.00	0.00	1.88	0.02	0.00	16.26	2.00	0.00	1.87	0.02	0.00
16.28	2.00	0.00	1.86	0.02	0.00	16.30	2.00	0.00	1.85	0.02	0.00
16.32	2.00	0.00	1.84	0.02	0.00	16.34	2.00	0.00	1.83	0.02	0.00
16.36	2.00	0.00	1.82	0.02	0.00	16.38	2.00	0.00	1.81	0.02	0.00
16.40	2.00	0.00	1.80	0.02	0.00	16.42	2.00	0.00	1.79	0.02	0.00
16.44	2.00	0.00	1.78	0.02	0.00	16.46	2.00	0.00	1.77	0.02	0.00
16.48	2.00	0.00	1.76	0.02	0.00	16.50	2.00	0.00	1.75	0.02	0.00
16.52	2.00	0.00	1.74	0.02	0.00	16.54	2.00	0.00	1.73	0.02	0.00
16.56	2.00	0.00	1.72	0.02	0.00	16.58	2.00	0.00	1.71	0.02	0.00
16.60	2.00	0.00	1.70	0.02	0.00	16.62	2.00	0.00	1.69	0.02	0.00
16.64	2.00	0.00	1.68	0.02	0.00	16.66	2.00	0.00	1.67	0.02	0.00
16.68	2.00	0.00	1.66	0.02	0.00	16.70	2.00	0.00	1.65	0.02	0.00
16.72	2.00	0.00	1.64	0.02	0.00	16.74	2.00	0.00	1.63	0.02	0.00
16.76	2.00	0.00	1.62	0.02	0.00	16.78	2.00	0.00	1.61	0.02	0.00
16.80	2.00	0.00	1.60	0.02	0.00	16.82	2.00	0.00	1.59	0.02	0.00
16.84	2.00	0.00	1.58	0.02	0.00	16.86	2.00	0.00	1.57	0.02	0.00
16.88	2.00	0.00	1.56	0.02	0.00	16.90	2.00	0.00	1.55	0.02	0.00
16.92	2.00	0.00	1.54	0.02	0.00	16.94	2.00	0.00	1.53	0.02	0.00
16.96	2.00	0.00	1.52	0.02	0.00	16.98	2.00	0.00	1.51	0.02	0.00
17.00	2.00	0.00	1.50	0.02	0.00	17.02	2.00	0.00	1.49	0.02	0.00
17.04	2.00	0.00	1.48	0.02	0.00	17.06	2.00	0.00	1.47	0.02	0.00
17.08	2.00	0.00	1.46	0.02	0.00	17.10	2.00	0.00	1.45	0.02	0.00
17.12	2.00	0.00	1.44	0.02	0.00	17.14	2.00	0.00	1.43	0.02	0.00
17.16	2.00	0.00	1.42	0.02	0.00	17.18	2.00	0.00	1.41	0.02	0.00
17.20	2.00	0.00	1.40	0.02	0.00	17.22	2.00	0.00	1.39	0.02	0.00
17.24	2.00	0.00	1.38	0.02	0.00	17.26	2.00	0.00	1.37	0.02	0.00
17.28	2.00	0.00	1.36	0.02	0.00	17.30	2.00	0.00	1.35	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
17.32	2.00	0.00	1.34	0.02	0.00	17.34	2.00	0.00	1.33	0.02	0.00
17.36	2.00	0.00	1.32	0.02	0.00	17.38	2.00	0.00	1.31	0.02	0.00
17.44	2.00	0.00	1.28	0.06	0.00	17.44	2.00	0.00	1.28	0.00	0.00
17.44	2.00	0.00	1.28	0.00	0.00	17.46	2.00	0.00	1.27	0.02	0.00
17.48	2.00	0.00	1.26	0.02	0.00	17.50	2.00	0.00	1.25	0.02	0.00
17.52	2.00	0.00	1.24	0.02	0.00	17.54	2.00	0.00	1.23	0.02	0.00
17.56	2.00	0.00	1.22	0.02	0.00	17.58	2.00	0.00	1.21	0.02	0.00
17.63	2.00	0.00	1.19	0.05	0.00	17.63	2.00	0.00	1.19	0.00	0.00
17.64	2.00	0.00	1.18	0.01	0.00	17.66	2.00	0.00	1.17	0.02	0.00
17.68	2.00	0.00	1.16	0.02	0.00	17.70	2.00	0.00	1.15	0.02	0.00
17.72	2.00	0.00	1.14	0.02	0.00	17.74	2.00	0.00	1.13	0.02	0.00
17.76	2.00	0.00	1.12	0.02	0.00	17.78	2.00	0.00	1.11	0.02	0.00
17.80	2.00	0.00	1.10	0.02	0.00	17.82	2.00	0.00	1.09	0.02	0.00
17.84	2.00	0.00	1.08	0.02	0.00	17.86	2.00	0.00	1.07	0.02	0.00
17.88	2.00	0.00	1.06	0.02	0.00	17.90	2.00	0.00	1.05	0.02	0.00
17.95	2.00	0.00	1.02	0.05	0.00	17.95	2.00	0.00	1.02	0.00	0.00
17.96	2.00	0.00	1.02	0.01	0.00	17.98	2.00	0.00	1.01	0.02	0.00
18.00	2.00	0.00	1.00	0.02	0.00	18.02	2.00	0.00	0.99	0.02	0.00
18.04	2.00	0.00	0.98	0.02	0.00	18.06	2.00	0.00	0.97	0.02	0.00
18.08	2.00	0.00	0.96	0.02	0.00	18.10	2.00	0.00	0.95	0.02	0.00
18.12	2.00	0.00	0.94	0.02	0.00	18.14	2.00	0.00	0.93	0.02	0.00
18.16	2.00	0.00	0.92	0.02	0.00	18.18	2.00	0.00	0.91	0.02	0.00
18.20	2.00	0.00	0.90	0.02	0.00	18.22	2.00	0.00	0.89	0.02	0.00
18.24	2.00	0.00	0.88	0.02	0.00	18.26	2.00	0.00	0.87	0.02	0.00
18.28	2.00	0.00	0.86	0.02	0.00	18.30	2.00	0.00	0.85	0.02	0.00
18.32	2.00	0.00	0.84	0.02	0.00	18.34	2.00	0.00	0.83	0.02	0.00
18.36	2.00	0.00	0.82	0.02	0.00	18.38	2.00	0.00	0.81	0.02	0.00
18.40	2.00	0.00	0.80	0.02	0.00	18.42	2.00	0.00	0.79	0.02	0.00
18.44	2.00	0.00	0.78	0.02	0.00	18.46	2.00	0.00	0.77	0.02	0.00
18.48	2.00	0.00	0.76	0.02	0.00	18.50	2.00	0.00	0.75	0.02	0.00
18.52	2.00	0.00	0.74	0.02	0.00	18.54	2.00	0.00	0.73	0.02	0.00
18.56	2.00	0.00	0.72	0.02	0.00	18.58	2.00	0.00	0.71	0.02	0.00
18.60	2.00	0.00	0.70	0.02	0.00	18.62	2.00	0.00	0.69	0.02	0.00
18.64	2.00	0.00	0.68	0.02	0.00	18.66	2.00	0.00	0.67	0.02	0.00
18.68	2.00	0.00	0.66	0.02	0.00	18.70	2.00	0.00	0.65	0.02	0.00
18.72	2.00	0.00	0.64	0.02	0.00	18.74	2.00	0.00	0.63	0.02	0.00
18.76	2.00	0.00	0.62	0.02	0.00	18.78	2.00	0.00	0.61	0.02	0.00
18.80	2.00	0.00	0.60	0.02	0.00	18.82	2.00	0.00	0.59	0.02	0.00
18.84	2.00	0.00	0.58	0.02	0.00	18.86	2.00	0.00	0.57	0.02	0.00
18.89	2.00	0.00	0.56	0.03	0.00	18.90	2.00	0.00	0.55	0.01	0.00
18.92	2.00	0.00	0.54	0.02	0.00	18.94	2.00	0.00	0.53	0.02	0.00
18.96	2.00	0.00	0.52	0.02	0.00	18.98	2.00	0.00	0.51	0.02	0.00
19.00	2.00	0.00	0.50	0.02	0.00	19.02	2.00	0.00	0.49	0.02	0.00
19.04	2.00	0.00	0.48	0.02	0.00	19.07	2.00	0.00	0.47	0.03	0.00
19.08	2.00	0.00	0.46	0.01	0.00	19.10	2.00	0.00	0.45	0.02	0.00
19.13	2.00	0.00	0.44	0.03	0.00	19.14	2.00	0.00	0.43	0.01	0.00
19.16	2.00	0.00	0.42	0.02	0.00	19.18	2.00	0.00	0.41	0.02	0.00
19.20	2.00	0.00	0.40	0.02	0.00	19.22	2.00	0.00	0.39	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
19.24	2.00	0.00	0.38	0.02	0.00	19.26	2.00	0.00	0.37	0.02	0.00
19.28	2.00	0.00	0.36	0.02	0.00	19.31	2.00	0.00	0.35	0.03	0.00
19.32	2.00	0.00	0.34	0.01	0.00	19.34	2.00	0.00	0.33	0.02	0.00
19.36	2.00	0.00	0.32	0.02	0.00	19.38	2.00	0.00	0.31	0.02	0.00
19.40	2.00	0.00	0.30	0.02	0.00	19.42	2.00	0.00	0.29	0.02	0.00
19.44	2.00	0.00	0.28	0.02	0.00	19.46	2.00	0.00	0.27	0.02	0.00
19.48	2.00	0.00	0.26	0.02	0.00	19.50	2.00	0.00	0.25	0.02	0.00
19.52	2.00	0.00	0.24	0.02	0.00	19.54	2.00	0.00	0.23	0.02	0.00
19.56	2.00	0.00	0.22	0.02	0.00	19.58	2.00	0.00	0.21	0.02	0.00
19.60	2.00	0.00	0.20	0.02	0.00	19.62	2.00	0.00	0.19	0.02	0.00
19.64	2.00	0.00	0.18	0.02	0.00	19.66	2.00	0.00	0.17	0.02	0.00
19.68	2.00	0.00	0.16	0.02	0.00	19.70	2.00	0.00	0.15	0.02	0.00
19.72	2.00	0.00	0.14	0.02	0.00	19.74	2.00	0.00	0.13	0.02	0.00
19.76	2.00	0.00	0.12	0.02	0.00						

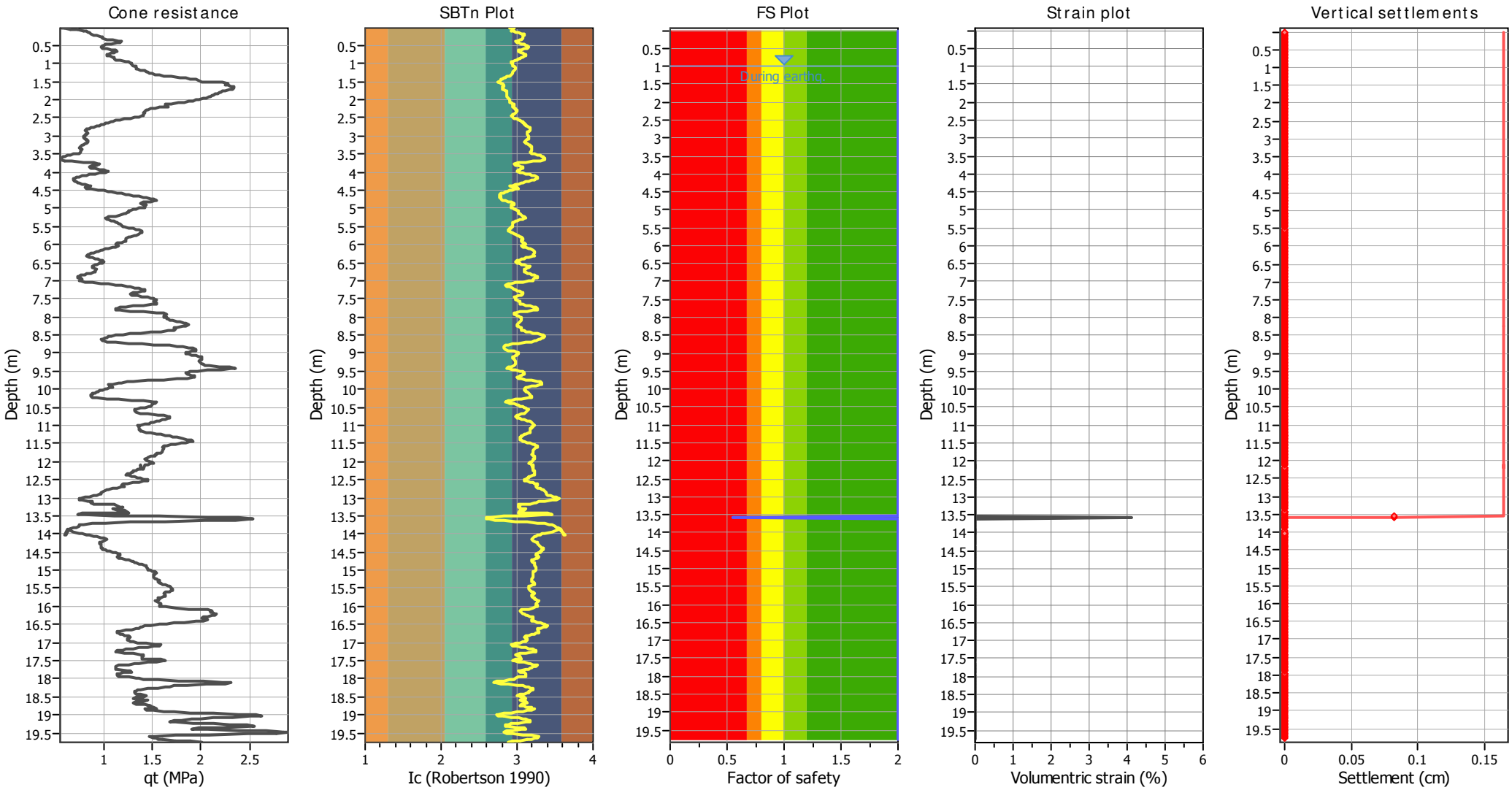
Overall liquefaction potential: 0.06

LPI = 0.00 - Liquefaction risk very low
LPI between 0.00 and 5.00 - Liquefaction risk low
LPI between 5.00 and 15.00 - Liquefaction risk high
LPI > 15.00 - Liquefaction risk very high

Abbreviations

FS: Calculated factor of safety for test point
F_L: 1 - FS
w_z: Function value of the extend of soil liquefaction according to depth
d_z: Layer thickness (m)
LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

q_t:	Total cone resistance (cone resistance q_c corrected for pore water effects)
I_c:	Soil Behaviour Type Index
FS:	Calculated Factor of Safety against liquefaction
Volumentric strain:	Post-liquefaction volumentric strain

:: Post-earthquake settlement due to soil liquefaction ::

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
1.00	21.41	2.00	0.00	1.00	0.00	1.02	21.64	2.00	0.00	1.00	0.00
1.05	21.99	2.00	0.00	1.00	0.00	1.06	22.18	2.00	0.00	1.00	0.00
1.08	22.49	2.00	0.00	1.00	0.00	1.10	22.33	2.00	0.00	1.00	0.00
1.12	22.43	2.00	0.00	1.00	0.00	1.14	22.11	2.00	0.00	1.00	0.00
1.16	22.41	2.00	0.00	1.00	0.00	1.18	23.03	2.00	0.00	1.00	0.00
1.20	23.80	2.00	0.00	1.00	0.00	1.22	24.30	2.00	0.00	1.00	0.00
1.24	24.08	2.00	0.00	1.00	0.00	1.26	24.42	2.00	0.00	1.00	0.00
1.28	25.03	2.00	0.00	1.00	0.00	1.30	25.71	2.00	0.00	1.00	0.00
1.32	26.04	2.00	0.00	1.00	0.00	1.34	27.16	2.00	0.00	1.00	0.00
1.36	28.16	2.00	0.00	1.00	0.00	1.38	29.59	2.00	0.00	1.00	0.00
1.40	31.33	2.00	0.00	1.00	0.00	1.44	31.64	2.00	0.00	1.00	0.00
1.44	31.64	2.00	0.00	1.00	0.00	1.51	34.51	2.00	0.00	1.00	0.00
1.51	34.51	2.00	0.00	1.00	0.00	1.51	34.59	2.00	0.00	1.00	0.00
1.52	38.36	2.00	0.00	1.00	0.00	1.54	38.25	2.00	0.00	1.00	0.00
1.56	37.08	2.00	0.00	1.00	0.00	1.58	37.56	2.00	0.00	1.00	0.00
1.60	37.84	2.00	0.00	1.00	0.00	1.62	38.48	2.00	0.00	1.00	0.00
1.64	38.76	2.00	0.00	1.00	0.00	1.66	39.47	2.00	0.00	1.00	0.00
1.68	38.92	2.00	0.00	1.00	0.00	1.70	38.88	2.00	0.00	1.00	0.00
1.72	38.17	2.00	0.00	1.00	0.00	1.74	37.54	2.00	0.00	1.00	0.00
1.76	36.79	2.00	0.00	1.00	0.00	1.78	36.75	2.00	0.00	1.00	0.00
1.81	36.47	2.00	0.00	1.00	0.00	1.82	36.12	2.00	0.00	1.00	0.00
1.84	35.72	2.00	0.00	1.00	0.00	1.86	35.37	2.00	0.00	1.00	0.00
1.88	35.25	2.00	0.00	1.00	0.00	1.90	34.50	2.00	0.00	1.00	0.00
1.92	34.58	2.00	0.00	1.00	0.00	1.94	34.59	2.00	0.00	1.00	0.00
1.97	33.18	2.00	0.00	1.00	0.00	1.98	32.56	2.00	0.00	1.00	0.00
2.00	31.93	2.00	0.00	1.00	0.00	2.02	31.20	2.00	0.00	1.00	0.00
2.04	30.68	2.00	0.00	1.00	0.00	2.06	29.88	2.00	0.00	1.00	0.00
2.08	28.52	2.00	0.00	1.00	0.00	2.10	27.22	2.00	0.00	1.00	0.00
2.13	26.12	2.00	0.00	1.00	0.00	2.14	25.55	2.00	0.00	1.00	0.00
2.16	26.75	2.00	0.00	1.00	0.00	2.18	26.55	2.00	0.00	1.00	0.00
2.20	25.64	2.00	0.00	1.00	0.00	2.22	25.03	2.00	0.00	1.00	0.00
2.24	24.23	2.00	0.00	1.00	0.00	2.26	23.35	2.00	0.00	1.00	0.00
2.28	22.97	2.00	0.00	1.00	0.00	2.30	22.79	2.00	0.00	1.00	0.00
2.32	22.45	2.00	0.00	1.00	0.00	2.34	22.10	2.00	0.00	1.00	0.00
2.36	22.21	2.00	0.00	1.00	0.00	2.38	22.01	2.00	0.00	1.00	0.00
2.40	21.95	2.00	0.00	1.00	0.00	2.42	21.79	2.00	0.00	1.00	0.00
2.45	21.78	2.00	0.00	1.00	0.00	2.46	21.78	2.00	0.00	1.00	0.00
2.48	21.27	2.00	0.00	1.00	0.00	2.50	20.41	2.00	0.00	1.00	0.00
2.52	19.70	2.00	0.00	1.00	0.00	2.54	18.99	2.00	0.00	1.00	0.00
2.56	17.93	2.00	0.00	1.00	0.00	2.58	17.29	2.00	0.00	1.00	0.00
2.60	17.01	2.00	0.00	1.00	0.00	2.62	16.62	2.00	0.00	1.00	0.00
2.64	16.16	2.00	0.00	1.00	0.00	2.66	15.85	2.00	0.00	1.00	0.00
2.68	15.22	2.00	0.00	1.00	0.00	2.70	15.08	2.00	0.00	1.00	0.00
2.72	14.73	2.00	0.00	1.00	0.00	2.74	14.18	2.00	0.00	1.00	0.00
2.76	13.62	2.00	0.00	1.00	0.00	2.78	13.35	2.00	0.00	1.00	0.00
2.80	12.76	2.00	0.00	1.00	0.00	2.82	12.59	2.00	0.00	1.00	0.00
2.84	12.32	2.00	0.00	1.00	0.00	2.86	12.26	2.00	0.00	1.00	0.00
2.88	12.24	2.00	0.00	1.00	0.00	2.90	12.55	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
2.92	12.39	2.00	0.00	1.00	0.00	2.94	12.44	2.00	0.00	1.00	0.00
2.97	12.13	2.00	0.00	1.00	0.00	2.98	12.18	2.00	0.00	1.00	0.00
3.00	11.95	2.00	0.00	1.00	0.00	3.02	11.72	2.00	0.00	1.00	0.00
3.04	11.87	2.00	0.00	1.00	0.00	3.07	11.97	2.00	0.00	1.00	0.00
3.08	12.06	2.00	0.00	1.00	0.00	3.10	12.27	2.00	0.00	1.00	0.00
3.12	12.21	2.00	0.00	1.00	0.00	3.14	12.22	2.00	0.00	1.00	0.00
3.16	12.57	2.00	0.00	1.00	0.00	3.18	12.24	2.00	0.00	1.00	0.00
3.21	12.03	2.00	0.00	1.00	0.00	3.22	11.75	2.00	0.00	1.00	0.00
3.24	11.52	2.00	0.00	1.00	0.00	3.26	11.36	2.00	0.00	1.00	0.00
3.28	11.13	2.00	0.00	1.00	0.00	3.30	11.13	2.00	0.00	1.00	0.00
3.32	10.94	2.00	0.00	1.00	0.00	3.34	10.81	2.00	0.00	1.00	0.00
3.36	11.12	2.00	0.00	1.00	0.00	3.38	11.26	2.00	0.00	1.00	0.00
3.40	11.00	2.00	0.00	1.00	0.00	3.42	11.00	2.00	0.00	1.00	0.00
3.44	10.88	2.00	0.00	1.00	0.00	3.48	10.70	2.00	0.00	1.00	0.00
3.49	10.38	2.00	0.00	1.00	0.00	3.50	10.10	2.00	0.00	1.00	0.00
3.52	9.27	2.00	0.00	1.00	0.00	3.54	8.74	2.00	0.00	1.00	0.00
3.56	8.58	2.00	0.00	1.00	0.00	3.58	8.20	2.00	0.00	1.00	0.00
3.60	8.04	2.00	0.00	1.00	0.00	3.62	7.95	2.00	0.00	1.00	0.00
3.64	7.70	2.00	0.00	1.00	0.00	3.66	7.65	2.00	0.00	1.00	0.00
3.68	8.13	2.00	0.00	1.00	0.00	3.70	9.04	2.00	0.00	1.00	0.00
3.72	11.15	2.00	0.00	1.00	0.00	3.74	12.62	2.00	0.00	1.00	0.00
3.76	13.27	2.00	0.00	1.00	0.00	3.78	13.25	2.00	0.00	1.00	0.00
3.80	13.03	2.00	0.00	1.00	0.00	3.82	12.13	2.00	0.00	1.00	0.00
3.84	11.75	2.00	0.00	1.00	0.00	3.86	11.47	2.00	0.00	1.00	0.00
3.88	12.27	2.00	0.00	1.00	0.00	3.90	12.48	2.00	0.00	1.00	0.00
3.92	13.32	2.00	0.00	1.00	0.00	3.94	13.90	2.00	0.00	1.00	0.00
3.96	14.32	2.00	0.00	1.00	0.00	3.98	14.45	2.00	0.00	1.00	0.00
4.00	13.98	2.00	0.00	1.00	0.00	4.02	13.39	2.00	0.00	1.00	0.00
4.04	12.16	2.00	0.00	1.00	0.00	4.06	11.75	2.00	0.00	1.00	0.00
4.08	11.19	2.00	0.00	1.00	0.00	4.10	10.62	2.00	0.00	1.00	0.00
4.12	9.86	2.00	0.00	1.00	0.00	4.14	9.55	2.00	0.00	1.00	0.00
4.16	9.41	2.00	0.00	1.00	0.00	4.18	9.39	2.00	0.00	1.00	0.00
4.20	8.92	2.00	0.00	1.00	0.00	4.22	9.02	2.00	0.00	1.00	0.00
4.25	9.25	2.00	0.00	1.00	0.00	4.26	9.30	2.00	0.00	1.00	0.00
4.28	9.57	2.00	0.00	1.00	0.00	4.30	9.83	2.00	0.00	1.00	0.00
4.32	9.97	2.00	0.00	1.00	0.00	4.34	10.14	2.00	0.00	1.00	0.00
4.36	11.25	2.00	0.00	1.00	0.00	4.38	11.80	2.00	0.00	1.00	0.00
4.40	11.28	2.00	0.00	1.00	0.00	4.42	10.76	2.00	0.00	1.00	0.00
4.44	10.28	2.00	0.00	1.00	0.00	4.47	10.35	2.00	0.00	1.00	0.00
4.48	10.87	2.00	0.00	1.00	0.00	4.50	11.88	2.00	0.00	1.00	0.00
4.52	12.94	2.00	0.00	1.00	0.00	4.54	13.54	2.00	0.00	1.00	0.00
4.56	14.01	2.00	0.00	1.00	0.00	4.59	13.99	2.00	0.00	1.00	0.00
4.60	15.35	2.00	0.00	1.00	0.00	4.62	16.09	2.00	0.00	1.00	0.00
4.64	16.10	2.00	0.00	1.00	0.00	4.66	16.62	2.00	0.00	1.00	0.00
4.68	17.53	2.00	0.00	1.00	0.00	4.70	18.23	2.00	0.00	1.00	0.00
4.72	18.71	2.00	0.00	1.00	0.00	4.74	19.13	2.00	0.00	1.00	0.00
4.76	19.85	2.00	0.00	1.00	0.00	4.78	20.23	2.00	0.00	1.00	0.00
4.80	19.95	2.00	0.00	1.00	0.00	4.82	19.46	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
4.84	18.50	2.00	0.00	1.00	0.00	4.86	17.09	2.00	0.00	1.00	0.00
4.88	17.54	2.00	0.00	1.00	0.00	4.90	18.14	2.00	0.00	1.00	0.00
4.92	18.18	2.00	0.00	1.00	0.00	4.94	18.77	2.00	0.00	1.00	0.00
4.97	18.16	2.00	0.00	1.00	0.00	4.98	17.85	2.00	0.00	1.00	0.00
5.00	17.75	2.00	0.00	1.00	0.00	5.02	17.22	2.00	0.00	1.00	0.00
5.04	16.62	2.00	0.00	1.00	0.00	5.07	16.38	2.00	0.00	1.00	0.00
5.08	15.88	2.00	0.00	1.00	0.00	5.10	16.02	2.00	0.00	1.00	0.00
5.12	16.14	2.00	0.00	1.00	0.00	5.14	15.79	2.00	0.00	1.00	0.00
5.16	15.26	2.00	0.00	1.00	0.00	5.18	15.02	2.00	0.00	1.00	0.00
5.21	14.16	2.00	0.00	1.00	0.00	5.22	13.59	2.00	0.00	1.00	0.00
5.24	13.27	2.00	0.00	1.00	0.00	5.26	12.98	2.00	0.00	1.00	0.00
5.28	12.63	2.00	0.00	1.00	0.00	5.30	12.84	2.00	0.00	1.00	0.00
5.32	13.05	2.00	0.00	1.00	0.00	5.34	13.26	2.00	0.00	1.00	0.00
5.36	13.58	2.00	0.00	1.00	0.00	5.38	13.91	2.00	0.00	1.00	0.00
5.40	13.95	2.00	0.00	1.00	0.00	5.42	14.13	2.00	0.00	1.00	0.00
5.44	14.25	2.00	0.00	1.00	0.00	5.46	14.43	2.00	0.00	1.00	0.00
5.52	14.54	2.00	0.00	1.00	0.00	5.52	14.54	2.00	0.00	1.00	0.00
5.52	14.43	2.00	0.00	1.00	0.00	5.54	15.44	2.00	0.00	1.00	0.00
5.56	15.83	2.00	0.00	1.00	0.00	5.58	16.15	2.00	0.00	1.00	0.00
5.60	16.73	2.00	0.00	1.00	0.00	5.62	16.85	2.00	0.00	1.00	0.00
5.64	16.94	2.00	0.00	1.00	0.00	5.66	16.94	2.00	0.00	1.00	0.00
5.68	16.46	2.00	0.00	1.00	0.00	5.70	16.66	2.00	0.00	1.00	0.00
5.72	16.27	2.00	0.00	1.00	0.00	5.74	16.16	2.00	0.00	1.00	0.00
5.76	15.74	2.00	0.00	1.00	0.00	5.78	15.44	2.00	0.00	1.00	0.00
5.80	14.99	2.00	0.00	1.00	0.00	5.82	14.77	2.00	0.00	1.00	0.00
5.84	14.52	2.00	0.00	1.00	0.00	5.86	14.57	2.00	0.00	1.00	0.00
5.88	14.76	2.00	0.00	1.00	0.00	5.90	14.65	2.00	0.00	1.00	0.00
5.92	14.52	2.00	0.00	1.00	0.00	5.94	13.91	2.00	0.00	1.00	0.00
5.96	13.39	2.00	0.00	1.00	0.00	5.98	13.14	2.00	0.00	1.00	0.00
6.01	13.09	2.00	0.00	1.00	0.00	6.02	13.63	2.00	0.00	1.00	0.00
6.04	13.69	2.00	0.00	1.00	0.00	6.07	13.44	2.00	0.00	1.00	0.00
6.08	12.90	2.00	0.00	1.00	0.00	6.10	12.41	2.00	0.00	1.00	0.00
6.12	11.87	2.00	0.00	1.00	0.00	6.14	11.62	2.00	0.00	1.00	0.00
6.16	11.36	2.00	0.00	1.00	0.00	6.18	11.14	2.00	0.00	1.00	0.00
6.20	10.85	2.00	0.00	1.00	0.00	6.22	10.47	2.00	0.00	1.00	0.00
6.24	10.12	2.00	0.00	1.00	0.00	6.26	10.14	2.00	0.00	1.00	0.00
6.28	9.76	2.00	0.00	1.00	0.00	6.30	9.28	2.00	0.00	1.00	0.00
6.32	9.46	2.00	0.00	1.00	0.00	6.34	9.86	2.00	0.00	1.00	0.00
6.36	10.37	2.00	0.00	1.00	0.00	6.38	10.55	2.00	0.00	1.00	0.00
6.40	10.59	2.00	0.00	1.00	0.00	6.42	11.18	2.00	0.00	1.00	0.00
6.44	11.22	2.00	0.00	1.00	0.00	6.46	11.60	2.00	0.00	1.00	0.00
6.48	11.62	2.00	0.00	1.00	0.00	6.50	11.25	2.00	0.00	1.00	0.00
6.52	10.86	2.00	0.00	1.00	0.00	6.54	10.75	2.00	0.00	1.00	0.00
6.56	10.28	2.00	0.00	1.00	0.00	6.58	9.97	2.00	0.00	1.00	0.00
6.60	9.93	2.00	0.00	1.00	0.00	6.62	9.87	2.00	0.00	1.00	0.00
6.64	9.92	2.00	0.00	1.00	0.00	6.66	10.15	2.00	0.00	1.00	0.00
6.69	10.41	2.00	0.00	1.00	0.00	6.70	10.38	2.00	0.00	1.00	0.00
6.72	10.35	2.00	0.00	1.00	0.00	6.74	10.20	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
6.76	10.14	2.00	0.00	1.00	0.00	6.78	10.13	2.00	0.00	1.00	0.00
6.80	9.75	2.00	0.00	1.00	0.00	6.82	9.26	2.00	0.00	1.00	0.00
6.84	8.74	2.00	0.00	1.00	0.00	6.86	8.82	2.00	0.00	1.00	0.00
6.88	8.19	2.00	0.00	1.00	0.00	6.90	7.95	2.00	0.00	1.00	0.00
6.92	7.89	2.00	0.00	1.00	0.00	6.94	8.38	2.00	0.00	1.00	0.00
6.96	8.69	2.00	0.00	1.00	0.00	6.98	8.34	2.00	0.00	1.00	0.00
7.00	8.06	2.00	0.00	1.00	0.00	7.02	7.92	2.00	0.00	1.00	0.00
7.04	8.76	2.00	0.00	1.00	0.00	7.06	9.60	2.00	0.00	1.00	0.00
7.08	10.37	2.00	0.00	1.00	0.00	7.10	11.76	2.00	0.00	1.00	0.00
7.12	12.14	2.00	0.00	1.00	0.00	7.14	13.40	2.00	0.00	1.00	0.00
7.16	13.80	2.00	0.00	1.00	0.00	7.18	14.02	2.00	0.00	1.00	0.00
7.20	14.64	2.00	0.00	1.00	0.00	7.22	15.14	2.00	0.00	1.00	0.00
7.24	15.39	2.00	0.00	1.00	0.00	7.26	15.63	2.00	0.00	1.00	0.00
7.28	15.82	2.00	0.00	1.00	0.00	7.30	15.59	2.00	0.00	1.00	0.00
7.32	14.68	2.00	0.00	1.00	0.00	7.34	14.40	2.00	0.00	1.00	0.00
7.36	13.80	2.00	0.00	1.00	0.00	7.38	13.68	2.00	0.00	1.00	0.00
7.40	14.05	2.00	0.00	1.00	0.00	7.42	14.50	2.00	0.00	1.00	0.00
7.44	15.59	2.00	0.00	1.00	0.00	7.46	15.99	2.00	0.00	1.00	0.00
7.48	16.53	2.00	0.00	1.00	0.00	7.50	16.40	2.00	0.00	1.00	0.00
7.52	17.25	2.00	0.00	1.00	0.00	7.54	16.99	2.00	0.00	1.00	0.00
7.56	16.79	2.00	0.00	1.00	0.00	7.58	16.42	2.00	0.00	1.00	0.00
7.60	16.81	2.00	0.00	1.00	0.00	7.62	17.23	2.00	0.00	1.00	0.00
7.64	17.17	2.00	0.00	1.00	0.00	7.66	16.79	2.00	0.00	1.00	0.00
7.68	15.33	2.00	0.00	1.00	0.00	7.70	14.25	2.00	0.00	1.00	0.00
7.72	13.25	2.00	0.00	1.00	0.00	7.74	12.69	2.00	0.00	1.00	0.00
7.76	12.11	2.00	0.00	1.00	0.00	7.78	11.89	2.00	0.00	1.00	0.00
7.80	11.96	2.00	0.00	1.00	0.00	7.82	12.09	2.00	0.00	1.00	0.00
7.84	13.43	2.00	0.00	1.00	0.00	7.86	15.05	2.00	0.00	1.00	0.00
7.88	16.58	2.00	0.00	1.00	0.00	7.90	17.50	2.00	0.00	1.00	0.00
7.92	17.71	2.00	0.00	1.00	0.00	7.94	17.44	2.00	0.00	1.00	0.00
7.96	17.39	2.00	0.00	1.00	0.00	7.98	17.29	2.00	0.00	1.00	0.00
8.00	17.42	2.00	0.00	1.00	0.00	8.02	17.52	2.00	0.00	1.00	0.00
8.04	17.82	2.00	0.00	1.00	0.00	8.06	17.75	2.00	0.00	1.00	0.00
8.08	17.75	2.00	0.00	1.00	0.00	8.10	18.27	2.00	0.00	1.00	0.00
8.12	18.69	2.00	0.00	1.00	0.00	8.15	19.17	2.00	0.00	1.00	0.00
8.16	19.13	2.00	0.00	1.00	0.00	8.18	19.85	2.00	0.00	1.00	0.00
8.20	19.82	2.00	0.00	1.00	0.00	8.22	19.91	2.00	0.00	1.00	0.00
8.24	19.65	2.00	0.00	1.00	0.00	8.26	19.20	2.00	0.00	1.00	0.00
8.28	18.70	2.00	0.00	1.00	0.00	8.30	17.90	2.00	0.00	1.00	0.00
8.32	18.07	2.00	0.00	1.00	0.00	8.34	18.56	2.00	0.00	1.00	0.00
8.36	18.53	2.00	0.00	1.00	0.00	8.38	17.62	2.00	0.00	1.00	0.00
8.40	16.58	2.00	0.00	1.00	0.00	8.42	15.89	2.00	0.00	1.00	0.00
8.44	14.43	2.00	0.00	1.00	0.00	8.46	13.33	2.00	0.00	1.00	0.00
8.48	12.39	2.00	0.00	1.00	0.00	8.50	11.81	2.00	0.00	1.00	0.00
8.52	11.01	2.00	0.00	1.00	0.00	8.54	10.92	2.00	0.00	1.00	0.00
8.56	10.68	2.00	0.00	1.00	0.00	8.58	10.52	2.00	0.00	1.00	0.00
8.60	10.00	2.00	0.00	1.00	0.00	8.62	9.89	2.00	0.00	1.00	0.00
8.64	9.92	2.00	0.00	1.00	0.00	8.66	10.06	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
8.68	10.25	2.00	0.00	1.00	0.00	8.70	11.16	2.00	0.00	1.00	0.00
8.72	12.62	2.00	0.00	1.00	0.00	8.74	14.20	2.00	0.00	1.00	0.00
8.76	15.17	2.00	0.00	1.00	0.00	8.78	16.23	2.00	0.00	1.00	0.00
8.80	17.10	2.00	0.00	1.00	0.00	8.82	17.46	2.00	0.00	1.00	0.00
8.84	18.59	2.00	0.00	1.00	0.00	8.86	18.62	2.00	0.00	1.00	0.00
8.88	19.38	2.00	0.00	1.00	0.00	8.90	19.94	2.00	0.00	1.00	0.00
8.93	19.69	2.00	0.00	1.00	0.00	8.94	19.47	2.00	0.00	1.00	0.00
8.96	19.47	2.00	0.00	1.00	0.00	8.98	18.73	2.00	0.00	1.00	0.00
9.00	18.37	2.00	0.00	1.00	0.00	9.02	18.37	2.00	0.00	1.00	0.00
9.04	18.75	2.00	0.00	1.00	0.00	9.06	19.23	2.00	0.00	1.00	0.00
9.08	19.34	2.00	0.00	1.00	0.00	9.10	19.77	2.00	0.00	1.00	0.00
9.12	20.12	2.00	0.00	1.00	0.00	9.14	20.22	2.00	0.00	1.00	0.00
9.16	19.95	2.00	0.00	1.00	0.00	9.18	20.06	2.00	0.00	1.00	0.00
9.20	19.99	2.00	0.00	1.00	0.00	9.22	19.74	2.00	0.00	1.00	0.00
9.24	19.74	2.00	0.00	1.00	0.00	9.26	19.78	2.00	0.00	1.00	0.00
9.28	19.92	2.00	0.00	1.00	0.00	9.30	20.04	2.00	0.00	1.00	0.00
9.32	20.12	2.00	0.00	1.00	0.00	9.34	20.10	2.00	0.00	1.00	0.00
9.36	20.68	2.00	0.00	1.00	0.00	9.38	21.22	2.00	0.00	1.00	0.00
9.40	22.87	2.00	0.00	1.00	0.00	9.42	23.66	2.00	0.00	1.00	0.00
9.44	23.00	2.00	0.00	1.00	0.00	9.46	21.81	2.00	0.00	1.00	0.00
9.48	20.40	2.00	0.00	1.00	0.00	9.50	19.12	2.00	0.00	1.00	0.00
9.52	18.74	2.00	0.00	1.00	0.00	9.54	18.27	2.00	0.00	1.00	0.00
9.56	18.29	2.00	0.00	1.00	0.00	9.58	18.29	2.00	0.00	1.00	0.00
9.60	18.61	2.00	0.00	1.00	0.00	9.62	18.66	2.00	0.00	1.00	0.00
9.64	18.97	2.00	0.00	1.00	0.00	9.66	19.20	2.00	0.00	1.00	0.00
9.68	18.89	2.00	0.00	1.00	0.00	9.70	18.43	2.00	0.00	1.00	0.00
9.72	17.45	2.00	0.00	1.00	0.00	9.74	15.94	2.00	0.00	1.00	0.00
9.76	14.21	2.00	0.00	1.00	0.00	9.78	12.57	2.00	0.00	1.00	0.00
9.80	11.56	2.00	0.00	1.00	0.00	9.82	12.00	2.00	0.00	1.00	0.00
9.84	11.01	2.00	0.00	1.00	0.00	9.86	10.34	2.00	0.00	1.00	0.00
9.88	9.76	2.00	0.00	1.00	0.00	9.90	9.75	2.00	0.00	1.00	0.00
9.92	10.42	2.00	0.00	1.00	0.00	9.95	10.37	2.00	0.00	1.00	0.00
9.96	9.90	2.00	0.00	1.00	0.00	9.98	9.62	2.00	0.00	1.00	0.00
10.00	9.48	2.00	0.00	1.00	0.00	10.02	9.11	2.00	0.00	1.00	0.00
10.04	8.77	2.00	0.00	1.00	0.00	10.06	8.79	2.00	0.00	1.00	0.00
10.08	8.61	2.00	0.00	1.00	0.00	10.10	8.31	2.00	0.00	1.00	0.00
10.12	8.16	2.00	0.00	1.00	0.00	10.14	8.00	2.00	0.00	1.00	0.00
10.16	7.93	2.00	0.00	1.00	0.00	10.18	8.05	2.00	0.00	1.00	0.00
10.20	7.98	2.00	0.00	1.00	0.00	10.22	7.93	2.00	0.00	1.00	0.00
10.24	8.20	2.00	0.00	1.00	0.00	10.26	9.29	2.00	0.00	1.00	0.00
10.28	10.75	2.00	0.00	1.00	0.00	10.30	11.59	2.00	0.00	1.00	0.00
10.32	13.04	2.00	0.00	1.00	0.00	10.34	14.02	2.00	0.00	1.00	0.00
10.36	14.58	2.00	0.00	1.00	0.00	10.38	14.05	2.00	0.00	1.00	0.00
10.40	13.77	2.00	0.00	1.00	0.00	10.42	13.88	2.00	0.00	1.00	0.00
10.44	13.89	2.00	0.00	1.00	0.00	10.46	13.65	2.00	0.00	1.00	0.00
10.48	13.44	2.00	0.00	1.00	0.00	10.50	13.23	2.00	0.00	1.00	0.00
10.52	12.61	2.00	0.00	1.00	0.00	10.54	12.20	2.00	0.00	1.00	0.00
10.56	11.99	2.00	0.00	1.00	0.00	10.58	11.93	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
10.60	12.21	2.00	0.00	1.00	0.00	10.62	12.02	2.00	0.00	1.00	0.00
10.64	12.12	2.00	0.00	1.00	0.00	10.66	12.47	2.00	0.00	1.00	0.00
10.68	13.13	2.00	0.00	1.00	0.00	10.70	14.32	2.00	0.00	1.00	0.00
10.72	15.05	2.00	0.00	1.00	0.00	10.74	15.19	2.00	0.00	1.00	0.00
10.76	15.53	2.00	0.00	1.00	0.00	10.78	15.63	2.00	0.00	1.00	0.00
10.80	15.12	2.00	0.00	1.00	0.00	10.82	15.14	2.00	0.00	1.00	0.00
10.84	14.94	2.00	0.00	1.00	0.00	10.86	14.62	2.00	0.00	1.00	0.00
10.88	14.13	2.00	0.00	1.00	0.00	10.90	13.96	2.00	0.00	1.00	0.00
10.92	13.72	2.00	0.00	1.00	0.00	10.94	13.53	2.00	0.00	1.00	0.00
10.96	13.31	2.00	0.00	1.00	0.00	10.98	12.49	2.00	0.00	1.00	0.00
11.00	12.26	2.00	0.00	1.00	0.00	11.02	12.28	2.00	0.00	1.00	0.00
11.04	12.42	2.00	0.00	1.00	0.00	11.06	12.32	2.00	0.00	1.00	0.00
11.08	12.32	2.00	0.00	1.00	0.00	11.10	12.31	2.00	0.00	1.00	0.00
11.13	12.44	2.00	0.00	1.00	0.00	11.14	12.36	2.00	0.00	1.00	0.00
11.17	12.45	2.00	0.00	1.00	0.00	11.18	12.74	2.00	0.00	1.00	0.00
11.20	12.71	2.00	0.00	1.00	0.00	11.22	13.29	2.00	0.00	1.00	0.00
11.24	13.90	2.00	0.00	1.00	0.00	11.26	14.31	2.00	0.00	1.00	0.00
11.28	14.62	2.00	0.00	1.00	0.00	11.30	15.06	2.00	0.00	1.00	0.00
11.32	15.44	2.00	0.00	1.00	0.00	11.34	15.66	2.00	0.00	1.00	0.00
11.36	16.39	2.00	0.00	1.00	0.00	11.39	16.76	2.00	0.00	1.00	0.00
11.40	16.97	2.00	0.00	1.00	0.00	11.42	17.19	2.00	0.00	1.00	0.00
11.44	17.32	2.00	0.00	1.00	0.00	11.46	17.24	2.00	0.00	1.00	0.00
11.48	16.65	2.00	0.00	1.00	0.00	11.50	16.10	2.00	0.00	1.00	0.00
11.52	15.85	2.00	0.00	1.00	0.00	11.54	15.24	2.00	0.00	1.00	0.00
11.56	14.81	2.00	0.00	1.00	0.00	11.58	14.49	2.00	0.00	1.00	0.00
11.60	14.29	2.00	0.00	1.00	0.00	11.62	14.49	2.00	0.00	1.00	0.00
11.64	14.71	2.00	0.00	1.00	0.00	11.66	14.41	2.00	0.00	1.00	0.00
11.68	14.24	2.00	0.00	1.00	0.00	11.70	14.50	2.00	0.00	1.00	0.00
11.72	14.24	2.00	0.00	1.00	0.00	11.75	14.19	2.00	0.00	1.00	0.00
11.76	13.87	2.00	0.00	1.00	0.00	11.78	13.92	2.00	0.00	1.00	0.00
11.80	13.09	2.00	0.00	1.00	0.00	11.82	13.88	2.00	0.00	1.00	0.00
11.84	13.50	2.00	0.00	1.00	0.00	11.86	13.09	2.00	0.00	1.00	0.00
11.88	12.88	2.00	0.00	1.00	0.00	11.91	12.43	2.00	0.00	1.00	0.00
11.92	12.73	2.00	0.00	1.00	0.00	11.94	12.63	2.00	0.00	1.00	0.00
11.96	12.58	2.00	0.00	1.00	0.00	11.98	12.71	2.00	0.00	1.00	0.00
12.00	12.83	2.00	0.00	1.00	0.00	12.02	13.39	2.00	0.00	1.00	0.00
12.04	13.34	2.00	0.00	1.00	0.00	12.06	13.07	2.00	0.00	1.00	0.00
12.08	12.70	2.00	0.00	1.00	0.00	12.10	12.35	2.00	0.00	1.00	0.00
12.20	12.26	2.00	0.00	1.00	0.00	12.20	12.26	2.00	0.00	1.00	0.00
12.11	12.19	2.00	0.00	1.00	0.00	12.20	11.87	2.00	0.00	1.00	0.00
12.22	11.93	2.00	0.00	1.00	0.00	12.24	11.58	2.00	0.00	1.00	0.00
12.26	11.28	2.00	0.00	1.00	0.00	12.28	11.23	2.00	0.00	1.00	0.00
12.30	11.35	2.00	0.00	1.00	0.00	12.32	11.03	2.00	0.00	1.00	0.00
12.34	10.83	2.00	0.00	1.00	0.00	12.36	10.64	2.00	0.00	1.00	0.00
12.38	10.65	2.00	0.00	1.00	0.00	12.40	11.25	2.00	0.00	1.00	0.00
12.42	11.47	2.00	0.00	1.00	0.00	12.44	11.61	2.00	0.00	1.00	0.00
12.46	11.75	2.00	0.00	1.00	0.00	12.48	12.23	2.00	0.00	1.00	0.00
12.50	12.64	2.00	0.00	1.00	0.00	12.52	12.73	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
12.55	12.10	2.00	0.00	1.00	0.00	12.56	11.68	2.00	0.00	1.00	0.00
12.58	11.29	2.00	0.00	1.00	0.00	12.60	10.52	2.00	0.00	1.00	0.00
12.62	10.12	2.00	0.00	1.00	0.00	12.64	10.09	2.00	0.00	1.00	0.00
12.66	10.28	2.00	0.00	1.00	0.00	12.68	10.48	2.00	0.00	1.00	0.00
12.70	10.25	2.00	0.00	1.00	0.00	12.72	9.75	2.00	0.00	1.00	0.00
12.74	9.23	2.00	0.00	1.00	0.00	12.76	9.06	2.00	0.00	1.00	0.00
12.78	8.65	2.00	0.00	1.00	0.00	12.80	8.51	2.00	0.00	1.00	0.00
12.83	8.25	2.00	0.00	1.00	0.00	12.84	8.13	2.00	0.00	1.00	0.00
12.86	8.01	2.00	0.00	1.00	0.00	12.88	8.10	2.00	0.00	1.00	0.00
12.90	8.13	2.00	0.00	1.00	0.00	12.92	7.78	2.00	0.00	1.00	0.00
12.94	7.35	2.00	0.00	1.00	0.00	12.96	7.08	2.00	0.00	1.00	0.00
12.98	6.65	2.00	0.00	1.00	0.00	13.00	6.18	2.00	0.00	1.00	0.00
13.02	6.14	2.00	0.00	1.00	0.00	13.04	6.03	2.00	0.00	1.00	0.00
13.06	6.23	2.00	0.00	1.00	0.00	13.08	6.95	2.00	0.00	1.00	0.00
13.10	7.25	2.00	0.00	1.00	0.00	13.12	7.38	2.00	0.00	1.00	0.00
13.14	7.04	2.00	0.00	1.00	0.00	13.16	6.76	2.00	0.00	1.00	0.00
13.18	8.00	2.00	0.00	1.00	0.00	13.20	9.55	2.00	0.00	1.00	0.00
13.22	9.66	2.00	0.00	1.00	0.00	13.24	9.08	2.00	0.00	1.00	0.00
13.26	9.58	2.00	0.00	1.00	0.00	13.28	10.40	2.00	0.00	1.00	0.00
13.30	9.59	2.00	0.00	1.00	0.00	13.32	8.34	2.00	0.00	1.00	0.00
13.34	9.28	2.00	0.00	1.00	0.00	13.36	10.50	2.00	0.00	1.00	0.00
13.41	10.24	2.00	0.00	1.00	0.00	13.41	10.24	2.00	0.00	1.00	0.00
13.42	7.12	2.00	0.00	1.00	0.00	13.44	6.13	2.00	0.00	1.00	0.00
13.46	5.67	2.00	0.00	1.00	0.00	13.48	5.67	2.00	0.00	1.00	0.00
13.50	7.84	2.00	0.00	1.00	0.00	13.52	13.36	2.00	0.00	1.00	0.00
13.54	17.57	2.00	0.00	1.00	0.00	13.56	77.57	0.56	4.13	1.00	0.08
13.58	78.60	0.56	4.08	1.00	0.08	13.60	21.71	2.00	0.00	1.00	0.00
13.62	20.60	2.00	0.00	1.00	0.00	13.64	17.62	2.00	0.00	1.00	0.00
13.66	13.74	2.00	0.00	1.00	0.00	13.68	10.02	2.00	0.00	1.00	0.00
13.70	8.23	2.00	0.00	1.00	0.00	13.72	7.14	2.00	0.00	1.00	0.00
13.74	6.34	2.00	0.00	1.00	0.00	13.76	6.02	2.00	0.00	1.00	0.00
13.78	5.80	2.00	0.00	1.00	0.00	13.80	5.88	2.00	0.00	1.00	0.00
13.83	5.81	2.00	0.00	1.00	0.00	13.84	5.36	2.00	0.00	1.00	0.00
13.86	4.99	2.00	0.00	1.00	0.00	14.03	4.67	2.00	0.00	1.00	0.00
14.03	4.67	2.00	0.00	1.00	0.00	14.03	4.69	2.00	0.00	1.00	0.00
13.88	4.71	2.00	0.00	1.00	0.00	13.96	5.50	2.00	0.00	1.00	0.00
13.98	5.89	2.00	0.00	1.00	0.00	14.00	6.12	2.00	0.00	1.00	0.00
14.02	6.41	2.00	0.00	1.00	0.00	14.04	6.68	2.00	0.00	1.00	0.00
14.06	7.03	2.00	0.00	1.00	0.00	14.08	7.32	2.00	0.00	1.00	0.00
14.10	7.69	2.00	0.00	1.00	0.00	14.12	7.86	2.00	0.00	1.00	0.00
14.14	8.15	2.00	0.00	1.00	0.00	14.16	8.18	2.00	0.00	1.00	0.00
14.18	7.87	2.00	0.00	1.00	0.00	14.21	7.66	2.00	0.00	1.00	0.00
14.22	7.49	2.00	0.00	1.00	0.00	14.24	7.56	2.00	0.00	1.00	0.00
14.26	7.50	2.00	0.00	1.00	0.00	14.28	7.57	2.00	0.00	1.00	0.00
14.30	7.62	2.00	0.00	1.00	0.00	14.32	7.54	2.00	0.00	1.00	0.00
14.37	7.57	2.00	0.00	1.00	0.00	14.37	7.57	2.00	0.00	1.00	0.00
14.38	7.62	2.00	0.00	1.00	0.00	14.40	7.64	2.00	0.00	1.00	0.00
14.42	7.77	2.00	0.00	1.00	0.00	14.44	7.88	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
14.46	8.10	2.00	0.00	1.00	0.00	14.48	8.23	2.00	0.00	1.00	0.00
14.50	8.40	2.00	0.00	1.00	0.00	14.52	8.80	2.00	0.00	1.00	0.00
14.54	9.01	2.00	0.00	1.00	0.00	14.56	9.17	2.00	0.00	1.00	0.00
14.58	9.19	2.00	0.00	1.00	0.00	14.60	9.02	2.00	0.00	1.00	0.00
14.62	8.88	2.00	0.00	1.00	0.00	14.64	8.91	2.00	0.00	1.00	0.00
14.66	8.88	2.00	0.00	1.00	0.00	14.68	9.13	2.00	0.00	1.00	0.00
14.70	9.70	2.00	0.00	1.00	0.00	14.72	9.85	2.00	0.00	1.00	0.00
14.74	10.19	2.00	0.00	1.00	0.00	14.76	10.42	2.00	0.00	1.00	0.00
14.78	10.35	2.00	0.00	1.00	0.00	14.80	10.43	2.00	0.00	1.00	0.00
14.82	10.81	2.00	0.00	1.00	0.00	14.84	10.84	2.00	0.00	1.00	0.00
14.86	11.24	2.00	0.00	1.00	0.00	14.88	11.35	2.00	0.00	1.00	0.00
14.90	11.36	2.00	0.00	1.00	0.00	14.92	11.29	2.00	0.00	1.00	0.00
14.94	11.37	2.00	0.00	1.00	0.00	14.96	11.38	2.00	0.00	1.00	0.00
14.98	11.29	2.00	0.00	1.00	0.00	15.00	11.53	2.00	0.00	1.00	0.00
15.02	11.77	2.00	0.00	1.00	0.00	15.04	11.89	2.00	0.00	1.00	0.00
15.06	12.10	2.00	0.00	1.00	0.00	15.08	11.93	2.00	0.00	1.00	0.00
15.10	11.80	2.00	0.00	1.00	0.00	15.12	11.74	2.00	0.00	1.00	0.00
15.14	11.77	2.00	0.00	1.00	0.00	15.16	11.64	2.00	0.00	1.00	0.00
15.18	11.70	2.00	0.00	1.00	0.00	15.20	11.77	2.00	0.00	1.00	0.00
15.22	11.80	2.00	0.00	1.00	0.00	15.24	11.88	2.00	0.00	1.00	0.00
15.26	12.02	2.00	0.00	1.00	0.00	15.28	12.22	2.00	0.00	1.00	0.00
15.30	12.13	2.00	0.00	1.00	0.00	15.32	12.08	2.00	0.00	1.00	0.00
15.34	12.01	2.00	0.00	1.00	0.00	15.36	12.25	2.00	0.00	1.00	0.00
15.38	12.16	2.00	0.00	1.00	0.00	15.40	12.28	2.00	0.00	1.00	0.00
15.42	12.55	2.00	0.00	1.00	0.00	15.44	12.85	2.00	0.00	1.00	0.00
15.46	12.97	2.00	0.00	1.00	0.00	15.48	12.94	2.00	0.00	1.00	0.00
15.50	13.00	2.00	0.00	1.00	0.00	15.52	13.05	2.00	0.00	1.00	0.00
15.54	12.96	2.00	0.00	1.00	0.00	15.56	13.18	2.00	0.00	1.00	0.00
15.58	13.11	2.00	0.00	1.00	0.00	15.60	12.79	2.00	0.00	1.00	0.00
15.62	12.54	2.00	0.00	1.00	0.00	15.64	12.34	2.00	0.00	1.00	0.00
15.66	12.31	2.00	0.00	1.00	0.00	15.68	12.39	2.00	0.00	1.00	0.00
15.70	12.57	2.00	0.00	1.00	0.00	15.72	12.58	2.00	0.00	1.00	0.00
15.74	12.46	2.00	0.00	1.00	0.00	15.76	12.10	2.00	0.00	1.00	0.00
15.78	12.00	2.00	0.00	1.00	0.00	15.80	11.64	2.00	0.00	1.00	0.00
15.82	12.32	2.00	0.00	1.00	0.00	15.84	11.60	2.00	0.00	1.00	0.00
15.86	11.65	2.00	0.00	1.00	0.00	15.88	11.75	2.00	0.00	1.00	0.00
15.90	12.00	2.00	0.00	1.00	0.00	15.92	11.80	2.00	0.00	1.00	0.00
15.94	12.13	2.00	0.00	1.00	0.00	15.96	12.21	2.00	0.00	1.00	0.00
15.98	11.78	2.00	0.00	1.00	0.00	16.00	11.73	2.00	0.00	1.00	0.00
16.02	12.11	2.00	0.00	1.00	0.00	16.04	13.08	2.00	0.00	1.00	0.00
16.07	14.22	2.00	0.00	1.00	0.00	16.08	15.12	2.00	0.00	1.00	0.00
16.10	16.04	2.00	0.00	1.00	0.00	16.12	16.48	2.00	0.00	1.00	0.00
16.14	16.24	2.00	0.00	1.00	0.00	16.16	15.88	2.00	0.00	1.00	0.00
16.18	16.30	2.00	0.00	1.00	0.00	16.20	16.69	2.00	0.00	1.00	0.00
16.22	16.66	2.00	0.00	1.00	0.00	16.24	16.58	2.00	0.00	1.00	0.00
16.26	16.38	2.00	0.00	1.00	0.00	16.28	15.93	2.00	0.00	1.00	0.00
16.30	15.48	2.00	0.00	1.00	0.00	16.32	15.22	2.00	0.00	1.00	0.00
16.34	15.41	2.00	0.00	1.00	0.00	16.36	15.78	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
16.38	15.82	2.00	0.00	1.00	0.00	16.40	15.52	2.00	0.00	1.00	0.00
16.42	14.68	2.00	0.00	1.00	0.00	16.44	13.82	2.00	0.00	1.00	0.00
16.46	12.71	2.00	0.00	1.00	0.00	16.48	12.43	2.00	0.00	1.00	0.00
16.50	11.79	2.00	0.00	1.00	0.00	16.52	11.00	2.00	0.00	1.00	0.00
16.54	10.45	2.00	0.00	1.00	0.00	16.56	10.24	2.00	0.00	1.00	0.00
16.58	10.17	2.00	0.00	1.00	0.00	16.60	10.18	2.00	0.00	1.00	0.00
16.62	9.80	2.00	0.00	1.00	0.00	16.64	9.45	2.00	0.00	1.00	0.00
16.66	8.93	2.00	0.00	1.00	0.00	16.68	8.58	2.00	0.00	1.00	0.00
16.70	8.11	2.00	0.00	1.00	0.00	16.72	8.18	2.00	0.00	1.00	0.00
16.74	8.27	2.00	0.00	1.00	0.00	16.76	8.48	2.00	0.00	1.00	0.00
16.78	8.34	2.00	0.00	1.00	0.00	16.80	8.69	2.00	0.00	1.00	0.00
16.82	8.87	2.00	0.00	1.00	0.00	16.84	9.00	2.00	0.00	1.00	0.00
16.86	8.90	2.00	0.00	1.00	0.00	16.88	8.66	2.00	0.00	1.00	0.00
16.90	8.79	2.00	0.00	1.00	0.00	16.92	8.66	2.00	0.00	1.00	0.00
16.94	8.75	2.00	0.00	1.00	0.00	16.96	8.86	2.00	0.00	1.00	0.00
16.98	9.00	2.00	0.00	1.00	0.00	17.00	9.34	2.00	0.00	1.00	0.00
17.02	9.99	2.00	0.00	1.00	0.00	17.04	10.96	2.00	0.00	1.00	0.00
17.06	11.23	2.00	0.00	1.00	0.00	17.08	11.37	2.00	0.00	1.00	0.00
17.10	10.75	2.00	0.00	1.00	0.00	17.12	10.11	2.00	0.00	1.00	0.00
17.14	9.85	2.00	0.00	1.00	0.00	17.16	8.91	2.00	0.00	1.00	0.00
17.18	8.74	2.00	0.00	1.00	0.00	17.20	8.24	2.00	0.00	1.00	0.00
17.22	7.95	2.00	0.00	1.00	0.00	17.24	7.59	2.00	0.00	1.00	0.00
17.26	7.61	2.00	0.00	1.00	0.00	17.28	8.19	2.00	0.00	1.00	0.00
17.30	9.07	2.00	0.00	1.00	0.00	17.32	9.99	2.00	0.00	1.00	0.00
17.34	10.15	2.00	0.00	1.00	0.00	17.36	10.02	2.00	0.00	1.00	0.00
17.38	9.80	2.00	0.00	1.00	0.00	17.44	9.71	2.00	0.00	1.00	0.00
17.44	9.71	2.00	0.00	1.00	0.00	17.44	10.40	2.00	0.00	1.00	0.00
17.46	11.19	2.00	0.00	1.00	0.00	17.48	11.42	2.00	0.00	1.00	0.00
17.50	11.65	2.00	0.00	1.00	0.00	17.52	11.14	2.00	0.00	1.00	0.00
17.54	10.05	2.00	0.00	1.00	0.00	17.56	9.83	2.00	0.00	1.00	0.00
17.58	9.11	2.00	0.00	1.00	0.00	17.63	8.70	2.00	0.00	1.00	0.00
17.63	8.70	2.00	0.00	1.00	0.00	17.64	7.52	2.00	0.00	1.00	0.00
17.66	7.55	2.00	0.00	1.00	0.00	17.68	7.63	2.00	0.00	1.00	0.00
17.70	7.68	2.00	0.00	1.00	0.00	17.72	7.48	2.00	0.00	1.00	0.00
17.74	7.62	2.00	0.00	1.00	0.00	17.76	7.62	2.00	0.00	1.00	0.00
17.78	7.74	2.00	0.00	1.00	0.00	17.80	10.10	2.00	0.00	1.00	0.00
17.82	8.88	2.00	0.00	1.00	0.00	17.84	8.17	2.00	0.00	1.00	0.00
17.86	7.82	2.00	0.00	1.00	0.00	17.88	7.69	2.00	0.00	1.00	0.00
17.90	7.57	2.00	0.00	1.00	0.00	17.95	7.72	2.00	0.00	1.00	0.00
17.95	7.72	2.00	0.00	1.00	0.00	17.96	8.50	2.00	0.00	1.00	0.00
17.98	9.16	2.00	0.00	1.00	0.00	18.00	9.14	2.00	0.00	1.00	0.00
18.02	9.44	2.00	0.00	1.00	0.00	18.04	9.91	2.00	0.00	1.00	0.00
18.06	12.39	2.00	0.00	1.00	0.00	18.08	13.95	2.00	0.00	1.00	0.00
18.10	16.01	2.00	0.00	1.00	0.00	18.12	17.44	2.00	0.00	1.00	0.00
18.14	16.81	2.00	0.00	1.00	0.00	18.16	15.06	2.00	0.00	1.00	0.00
18.18	13.38	2.00	0.00	1.00	0.00	18.20	12.08	2.00	0.00	1.00	0.00
18.22	11.24	2.00	0.00	1.00	0.00	18.24	12.05	2.00	0.00	1.00	0.00
18.26	10.90	2.00	0.00	1.00	0.00	18.28	9.65	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
18.30	9.25	2.00	0.00	1.00	0.00	18.32	9.13	2.00	0.00	1.00	0.00
18.34	8.86	2.00	0.00	1.00	0.00	18.36	8.75	2.00	0.00	1.00	0.00
18.38	8.95	2.00	0.00	1.00	0.00	18.40	8.69	2.00	0.00	1.00	0.00
18.42	8.62	2.00	0.00	1.00	0.00	18.44	9.16	2.00	0.00	1.00	0.00
18.46	9.74	2.00	0.00	1.00	0.00	18.48	9.84	2.00	0.00	1.00	0.00
18.50	9.36	2.00	0.00	1.00	0.00	18.52	8.88	2.00	0.00	1.00	0.00
18.54	8.35	2.00	0.00	1.00	0.00	18.56	8.52	2.00	0.00	1.00	0.00
18.58	9.53	2.00	0.00	1.00	0.00	18.60	9.98	2.00	0.00	1.00	0.00
18.62	9.57	2.00	0.00	1.00	0.00	18.64	8.66	2.00	0.00	1.00	0.00
18.66	8.61	2.00	0.00	1.00	0.00	18.68	8.53	2.00	0.00	1.00	0.00
18.70	8.74	2.00	0.00	1.00	0.00	18.72	9.24	2.00	0.00	1.00	0.00
18.74	10.29	2.00	0.00	1.00	0.00	18.76	9.95	2.00	0.00	1.00	0.00
18.78	8.79	2.00	0.00	1.00	0.00	18.80	12.44	2.00	0.00	1.00	0.00
18.82	10.48	2.00	0.00	1.00	0.00	18.84	9.44	2.00	0.00	1.00	0.00
18.86	9.51	2.00	0.00	1.00	0.00	18.89	10.29	2.00	0.00	1.00	0.00
18.90	10.77	2.00	0.00	1.00	0.00	18.92	11.69	2.00	0.00	1.00	0.00
18.94	12.61	2.00	0.00	1.00	0.00	18.96	14.34	2.00	0.00	1.00	0.00
18.98	16.78	2.00	0.00	1.00	0.00	19.00	18.46	2.00	0.00	1.00	0.00
19.02	18.83	2.00	0.00	1.00	0.00	19.04	18.59	2.00	0.00	1.00	0.00
19.07	16.18	2.00	0.00	1.00	0.00	19.08	14.92	2.00	0.00	1.00	0.00
19.10	13.96	2.00	0.00	1.00	0.00	19.13	13.12	2.00	0.00	1.00	0.00
19.14	12.45	2.00	0.00	1.00	0.00	19.16	11.74	2.00	0.00	1.00	0.00
19.18	11.19	2.00	0.00	1.00	0.00	19.20	11.35	2.00	0.00	1.00	0.00
19.22	12.84	2.00	0.00	1.00	0.00	19.24	14.83	2.00	0.00	1.00	0.00
19.26	16.10	2.00	0.00	1.00	0.00	19.28	16.84	2.00	0.00	1.00	0.00
19.31	19.17	2.00	0.00	1.00	0.00	19.32	18.24	2.00	0.00	1.00	0.00
19.34	15.99	2.00	0.00	1.00	0.00	19.36	13.29	2.00	0.00	1.00	0.00
19.38	12.43	2.00	0.00	1.00	0.00	19.40	13.83	2.00	0.00	1.00	0.00
19.42	16.47	2.00	0.00	1.00	0.00	19.44	19.17	2.00	0.00	1.00	0.00
19.46	20.29	2.00	0.00	1.00	0.00	19.48	20.99	2.00	0.00	1.00	0.00
19.50	20.68	2.00	0.00	1.00	0.00	19.52	17.91	2.00	0.00	1.00	0.00
19.54	14.78	2.00	0.00	1.00	0.00	19.56	11.73	2.00	0.00	1.00	0.00
19.58	9.85	2.00	0.00	1.00	0.00	19.60	9.65	2.00	0.00	1.00	0.00
19.62	10.00	2.00	0.00	1.00	0.00	19.64	10.28	2.00	0.00	1.00	0.00
19.66	10.24	2.00	0.00	1.00	0.00	19.68	10.42	2.00	0.00	1.00	0.00
19.70	11.22	2.00	0.00	1.00	0.00	19.72	13.11	2.00	0.00	1.00	0.00
19.74	13.77	2.00	0.00	1.00	0.00	19.76	12.44	2.00	0.00	1.00	0.00

Total estimated settlement: 0.16

Abbreviations

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumentric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

:: Strength loss calculation Idriss & Boulanger (2008) ::

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.02	0.57	9.72	5.65	54.93	2.90	0.06	131.81
0.04	0.60	10.18	6.27	63.87	2.96	0.06	68.00
0.06	0.66	11.15	6.19	68.97	2.95	0.06	49.14
0.08	0.73	12.34	6.04	74.56	2.93	0.07	40.41
0.10	0.80	13.51	5.97	80.63	2.93	0.07	35.11
0.12	0.82	13.94	6.24	87.04	2.95	0.07	29.96
0.14	0.84	14.29	6.61	94.43	2.99	0.07	26.13
0.16	0.85	14.43	7.03	101.34	3.02	0.07	22.92
0.18	0.86	14.65	7.39	108.27	3.06	0.07	20.55
0.20	0.87	14.72	7.79	114.59	3.09	0.07	18.47
0.22	0.90	15.18	7.87	119.46	3.10	0.07	17.23
0.24	0.93	15.80	7.76	122.54	3.09	0.07	16.35
0.26	0.97	16.42	7.63	125.17	3.08	0.07	15.62
0.28	0.99	16.70	7.62	127.21	3.08	0.07	14.69
0.30	0.98	16.64	7.72	128.46	3.08	0.07	13.61
0.32	0.99	16.78	7.68	128.86	3.08	0.07	12.83
0.34	1.03	17.45	7.43	129.56	3.06	0.07	12.52
0.36	1.09	18.47	7.08	130.80	3.03	0.07	12.48
0.38	1.15	19.45	6.77	131.76	3.00	0.07	12.43
0.40	1.18	19.96	6.60	131.79	2.99	0.07	12.09
0.42	1.17	19.83	6.66	131.99	2.99	0.07	11.41
0.44	1.13	19.09	6.95	132.68	3.02	0.07	10.47
0.46	1.07	18.08	7.42	134.15	3.06	0.07	9.47
0.48	1.02	17.26	7.85	135.49	3.09	0.07	8.65
0.50	1.00	16.77	8.17	136.99	3.12	0.07	8.05
0.52	0.98	16.50	8.39	138.48	3.14	0.07	7.61
0.54	0.97	16.36	8.55	139.91	3.15	0.07	7.25
0.56	0.97	16.39	8.55	140.06	3.15	0.07	7.00
0.58	0.99	16.61	8.37	139.04	3.13	0.07	6.84
0.60	1.03	17.34	7.86	136.23	3.09	0.07	6.90
0.62	1.08	18.19	7.33	133.40	3.05	0.07	7.00
0.64	1.12	18.86	6.96	131.30	3.02	0.07	7.02
0.66	1.13	19.00	6.91	131.19	3.01	0.07	6.85
0.68	1.12	18.83	7.05	132.80	3.03	0.07	6.59
0.70	1.10	18.48	7.31	135.08	3.05	0.07	6.28
0.72	1.07	18.00	7.63	137.36	3.08	0.07	5.94
0.74	1.04	17.52	7.94	139.11	3.10	0.07	5.62
0.76	1.03	17.21	8.17	140.52	3.12	0.07	5.37
0.78	1.04	17.39	8.11	141.02	3.11	0.07	5.29
0.80	1.06	17.84	7.86	140.28	3.09	0.07	5.28
0.82	1.09	18.34	7.53	138.18	3.07	0.07	5.29
0.84	1.10	18.44	7.37	135.83	3.05	0.07	5.19
0.86	1.10	18.43	7.20	132.71	3.04	0.07	5.07
0.88	1.11	18.52	7.00	129.63	3.02	0.07	4.98
0.90	1.13	18.87	6.76	127.62	3.00	0.07	4.96
0.92	1.17	19.60	6.44	126.22	2.97	0.07	5.03
0.95	1.22	20.45	6.13	125.40	2.94	0.08	5.09
0.96	1.26	21.16	5.90	124.83	2.92	0.08	5.21

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.98	1.28	21.42	5.93	126.91	2.92	0.08	5.16
1.00	1.28	21.49	6.04	129.79	2.93	0.08	5.07
1.02	1.29	21.65	6.13	132.72	2.94	0.08	5.01
1.05	1.31	21.90	6.18	135.28	2.95	0.08	4.92
1.06	1.32	22.19	6.25	138.67	2.95	0.08	4.93
1.08	1.33	22.30	6.39	142.50	2.97	0.08	4.87
1.10	1.34	22.38	6.49	145.30	2.98	0.08	4.79
1.12	1.33	22.25	6.59	146.53	2.99	0.08	4.67
1.14	1.33	22.27	6.59	146.85	2.99	0.08	4.60
1.16	1.34	22.48	6.55	147.23	2.98	0.08	4.56
1.18	1.38	23.06	6.41	147.72	2.97	0.08	4.59
1.20	1.42	23.71	6.25	148.12	2.95	0.08	4.64
1.22	1.44	24.07	6.20	149.24	2.95	0.08	4.63
1.24	1.45	24.28	6.21	150.69	2.95	0.08	4.59
1.26	1.47	24.53	6.21	152.28	2.95	0.08	4.57
1.28	1.50	25.09	6.11	153.25	2.94	0.08	4.59
1.30	1.53	25.65	6.01	154.22	2.93	0.08	4.62
1.32	1.58	26.37	5.88	155.09	2.92	0.08	4.68
1.34	1.62	27.20	5.70	155.03	2.90	0.09	4.75
1.36	1.70	28.41	5.43	154.32	2.87	0.09	4.89
1.38	1.78	29.83	5.14	153.44	2.84	0.09	5.05
1.40	1.85	31.02	4.93	153.08	2.82	0.10	5.18
1.44	1.89	31.71	4.83	153.03	2.80	0.10	5.14
1.44	1.96	32.80	4.66	152.94	2.79	0.10	5.31
1.51	2.01	33.75	4.53	152.90	2.77	0.10	5.21
1.51	2.07	34.75	4.40	152.89	2.75	0.10	5.36
1.51	2.15	36.06	4.39	158.45	2.75	0.10	5.56
1.52	2.22	37.33	4.46	166.31	2.76	0.11	5.72
1.54	2.27	38.18	4.63	176.67	2.78	0.11	5.77
1.56	2.26	37.90	4.82	182.73	2.80	0.10	5.65
1.58	2.25	37.76	4.95	187.08	2.82	0.10	5.55
1.60	2.28	38.24	4.95	189.39	2.82	0.10	5.55
1.62	2.30	38.65	4.94	190.75	2.82	0.11	5.53
1.64	2.34	39.20	4.87	190.79	2.81	0.11	5.54
1.66	2.34	39.34	4.83	190.11	2.81	0.11	5.49
1.68	2.35	39.37	4.82	189.97	2.80	0.11	5.43
1.70	2.32	38.93	4.92	191.61	2.82	0.11	5.30
1.72	2.29	38.46	5.03	193.60	2.83	0.10	5.17
1.74	2.25	37.75	5.18	195.60	2.85	0.10	5.01
1.76	2.22	37.28	5.28	196.92	2.86	0.10	4.89
1.78	2.20	36.92	5.36	197.78	2.86	0.10	4.78
1.81	2.19	36.69	5.38	197.47	2.87	0.10	4.67
1.82	2.17	36.35	5.38	195.48	2.87	0.10	4.60
1.84	2.15	35.98	5.36	193.00	2.87	0.10	4.50
1.86	2.13	35.68	5.34	190.37	2.86	0.10	4.42
1.88	2.11	35.27	5.34	188.52	2.86	0.10	4.32
1.90	2.09	34.98	5.38	188.08	2.87	0.10	4.23
1.92	2.08	34.79	5.39	187.67	2.87	0.10	4.16

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
1.94	2.06	34.42	5.47	188.15	2.88	0.10	4.07
1.97	2.03	33.84	5.56	187.99	2.89	0.10	3.94
1.98	1.98	33.02	5.66	187.00	2.90	0.09	3.83
2.00	1.94	32.43	5.70	184.91	2.90	0.09	3.72
2.02	1.91	31.91	5.69	181.67	2.90	0.09	3.62
2.04	1.88	31.31	5.71	178.81	2.90	0.09	3.52
2.06	1.83	30.45	5.77	175.80	2.91	0.09	3.39
2.08	1.76	29.29	5.91	172.98	2.92	0.09	3.23
2.10	1.69	28.04	6.12	171.55	2.94	0.08	3.06
2.13	1.63	27.06	6.33	171.28	2.96	0.08	2.91
2.14	1.63	27.04	6.32	170.85	2.96	0.08	2.89
2.16	1.65	27.32	6.22	169.93	2.95	0.08	2.89
2.18	1.66	27.49	6.12	168.37	2.94	0.08	2.89
2.20	1.62	26.94	6.18	166.58	2.95	0.08	2.80
2.22	1.58	26.12	6.30	164.57	2.96	0.08	2.70
2.24	1.53	25.31	6.41	162.17	2.97	0.08	2.61
2.26	1.49	24.58	6.54	160.76	2.98	0.08	2.52
2.28	1.46	24.10	6.62	159.50	2.99	0.08	2.46
2.30	1.44	23.83	6.65	158.45	2.99	0.08	2.42
2.32	1.43	23.57	6.68	157.45	2.99	0.08	2.39
2.34	1.42	23.41	6.66	155.93	2.99	0.08	2.36
2.36	1.41	23.31	6.61	154.12	2.99	0.08	2.34
2.38	1.42	23.31	6.48	151.07	2.98	0.08	2.33
2.40	1.41	23.21	6.36	147.65	2.96	0.08	2.31
2.42	1.41	23.18	6.21	143.95	2.95	0.08	2.30
2.45	1.41	23.17	6.07	140.66	2.94	0.08	2.29
2.46	1.40	23.00	6.00	137.94	2.93	0.08	2.26
2.48	1.37	22.48	6.04	135.90	2.93	0.08	2.21
2.50	1.32	21.69	6.19	134.26	2.95	0.07	2.12
2.52	1.27	20.84	6.40	133.34	2.97	0.07	2.03
2.54	1.22	19.91	6.68	132.92	2.99	0.07	1.93
2.56	1.17	19.03	7.01	133.33	3.02	0.07	1.84
2.58	1.12	18.31	7.29	133.42	3.05	0.07	1.76
2.60	1.10	17.86	7.46	133.17	3.06	0.07	1.71
2.62	1.08	17.47	7.58	132.40	3.07	0.07	1.67
2.64	1.05	17.06	7.70	131.42	3.08	0.07	1.62
2.66	1.02	16.56	7.86	130.17	3.09	0.07	1.57
2.68	1.00	16.18	7.95	128.72	3.10	0.07	1.53
2.70	0.98	15.79	8.07	127.42	3.11	0.07	1.49
2.72	0.96	15.41	8.18	126.08	3.12	0.07	1.44
2.74	0.93	14.88	8.40	124.94	3.14	0.07	1.39
2.76	0.90	14.38	8.59	123.53	3.15	0.07	1.34
2.78	0.87	13.88	8.78	121.94	3.17	0.07	1.29
2.80	0.85	13.53	8.87	120.02	3.17	0.06	1.25
2.82	0.83	13.18	8.95	117.95	3.18	0.06	1.21
2.84	0.82	13.03	8.89	115.86	3.17	0.06	1.20
2.86	0.81	12.93	8.78	113.53	3.17	0.06	1.18
2.88	0.82	13.04	8.56	111.60	3.15	0.06	1.19

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
2.90	0.82	13.11	8.40	110.07	3.14	0.06	1.19
2.92	0.83	13.19	8.25	108.77	3.13	0.06	1.19
2.94	0.82	13.03	8.27	107.75	3.13	0.06	1.18
2.97	0.82	12.96	8.27	107.12	3.13	0.06	1.16
2.98	0.81	12.79	8.40	107.42	3.14	0.06	1.15
3.00	0.80	12.64	8.54	107.92	3.15	0.06	1.13
3.02	0.79	12.54	8.66	108.53	3.16	0.06	1.12
3.04	0.80	12.57	8.66	108.93	3.16	0.06	1.12
3.07	0.80	12.73	8.57	109.11	3.15	0.06	1.12
3.08	0.82	12.91	8.42	108.76	3.14	0.06	1.14
3.10	0.82	13.02	8.29	107.93	3.13	0.06	1.15
3.12	0.83	13.11	8.16	107.06	3.12	0.06	1.15
3.14	0.84	13.25	8.03	106.36	3.11	0.06	1.16
3.16	0.84	13.28	7.97	105.92	3.10	0.06	1.16
3.18	0.84	13.23	8.01	105.91	3.11	0.06	1.15
3.21	0.82	12.91	8.22	106.17	3.12	0.06	1.12
3.22	0.80	12.64	8.44	106.72	3.14	0.06	1.09
3.24	0.79	12.39	8.64	106.98	3.16	0.06	1.07
3.26	0.77	12.16	8.83	107.42	3.17	0.06	1.04
3.28	0.77	12.03	8.98	107.94	3.18	0.06	1.03
3.30	0.76	11.87	9.12	108.29	3.19	0.06	1.01
3.32	0.75	11.76	9.22	108.49	3.20	0.06	1.00
3.34	0.75	11.78	9.23	108.72	3.20	0.06	1.00
3.36	0.76	11.93	9.15	109.07	3.19	0.06	1.01
3.38	0.77	12.03	9.07	109.07	3.19	0.06	1.01
3.40	0.77	12.01	9.03	108.47	3.18	0.06	1.01
3.42	0.76	11.88	9.02	107.19	3.18	0.06	0.99
3.44	0.76	11.79	8.99	106.05	3.18	0.06	0.98
3.48	0.74	11.56	9.08	104.89	3.19	0.06	0.96
3.49	0.73	11.26	9.27	104.41	3.20	0.06	0.93
3.50	0.69	10.69	9.70	103.74	3.23	0.06	0.88
3.52	0.66	10.05	10.27	103.23	3.27	0.06	0.83
3.54	0.62	9.46	10.83	102.50	3.31	0.06	0.78
3.56	0.60	9.05	11.19	101.31	3.33	0.06	0.74
3.58	0.58	8.79	11.41	100.24	3.34	0.06	0.72
3.60	0.57	8.55	11.57	98.96	3.35	0.06	0.70
3.62	0.56	8.37	11.74	98.26	3.36	0.06	0.68
3.64	0.55	8.23	11.86	97.67	3.37	0.06	0.67
3.66	0.56	8.33	11.68	97.38	3.36	0.06	0.67
3.68	0.59	8.91	10.95	97.60	3.32	0.06	0.72
3.70	0.68	10.38	9.46	98.14	3.21	0.06	0.83
3.72	0.79	12.24	8.01	98.08	3.11	0.06	0.98
3.74	0.89	14.00	6.91	96.71	3.01	0.06	1.12
3.76	0.94	14.85	6.38	94.82	2.97	0.07	1.18
3.78	0.95	15.01	6.23	93.43	2.95	0.07	1.19
3.80	0.92	14.51	6.49	94.15	2.98	0.06	1.15
3.82	0.89	13.89	6.94	96.36	3.02	0.06	1.10
3.84	0.85	13.25	7.47	98.96	3.06	0.06	1.04

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
3.86	0.85	13.31	7.62	101.48	3.08	0.06	1.05
3.88	0.87	13.60	7.63	103.79	3.08	0.06	1.07
3.90	0.92	14.38	7.41	106.53	3.06	0.06	1.12
3.92	0.96	15.11	7.17	108.38	3.04	0.07	1.18
3.94	1.01	15.93	6.89	109.82	3.01	0.07	1.24
3.96	1.04	16.44	6.75	110.95	3.00	0.07	1.27
3.98	1.04	16.48	6.83	112.46	3.01	0.07	1.27
4.00	1.02	16.08	7.12	114.53	3.03	0.07	1.24
4.02	0.96	15.12	7.67	115.97	3.08	0.07	1.16
4.04	0.91	14.20	8.21	116.63	3.12	0.06	1.09
4.06	0.86	13.32	8.76	116.71	3.16	0.06	1.02
4.08	0.82	12.75	9.20	117.30	3.20	0.06	0.97
4.10	0.78	12.05	9.78	117.87	3.24	0.06	0.91
4.12	0.75	11.44	10.20	116.67	3.27	0.06	0.87
4.14	0.72	10.95	10.39	113.83	3.28	0.06	0.83
4.16	0.71	10.74	10.18	109.32	3.26	0.06	0.81
4.18	0.69	10.48	9.98	104.49	3.25	0.06	0.79
4.20	0.68	10.36	9.62	99.63	3.23	0.06	0.78
4.22	0.69	10.39	9.17	95.25	3.19	0.06	0.78
4.25	0.70	10.63	8.61	91.49	3.15	0.06	0.79
4.26	0.72	10.91	8.05	87.82	3.11	0.06	0.81
4.28	0.73	11.18	7.64	85.40	3.08	0.06	0.83
4.30	0.75	11.48	7.31	83.99	3.05	0.06	0.85
4.32	0.77	11.76	7.06	82.97	3.03	0.06	0.87
4.34	0.81	12.39	6.58	81.56	2.99	0.06	0.91
4.36	0.85	13.14	6.05	79.56	2.94	0.06	0.96
4.38	0.87	13.50	5.83	78.71	2.91	0.07	0.99
4.40	0.85	13.15	6.03	79.31	2.93	0.06	0.96
4.42	0.81	12.48	6.51	81.24	2.98	0.06	0.91
4.44	0.80	12.26	6.82	83.59	3.01	0.06	0.89
4.47	0.82	12.50	6.88	86.01	3.01	0.06	0.91
4.48	0.87	13.35	6.58	87.83	2.99	0.06	0.97
4.50	0.93	14.52	6.11	88.71	2.94	0.06	1.05
4.52	1.00	15.59	5.69	88.73	2.90	0.07	1.12
4.54	1.05	16.35	5.39	88.17	2.87	0.07	1.19
4.56	1.08	16.69	5.26	87.80	2.85	0.07	1.21
4.59	1.13	17.36	4.97	86.26	2.82	0.07	1.27
4.60	1.18	18.03	4.72	85.14	2.79	0.08	1.33
4.62	1.23	18.75	4.54	85.22	2.77	0.08	1.39
4.64	1.26	19.27	4.58	88.18	2.77	0.08	1.42
4.66	1.31	19.93	4.62	92.02	2.78	0.08	1.47
4.68	1.36	20.69	4.59	95.03	2.78	0.08	1.53
4.70	1.40	21.38	4.57	97.78	2.77	0.08	1.58
4.72	1.44	21.90	4.63	101.34	2.78	0.08	1.61
4.74	1.48	22.54	4.70	105.87	2.79	0.08	1.66
4.76	1.52	23.13	4.76	110.14	2.80	0.08	1.70
4.78	1.54	23.48	4.91	115.24	2.81	0.08	1.72
4.80	1.53	23.38	5.15	120.41	2.84	0.08	1.70

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
4.82	1.48	22.79	5.55	126.43	2.88	0.08	1.64
4.84	1.41	21.78	6.01	130.86	2.93	0.07	1.56
4.86	1.37	21.03	6.36	133.79	2.96	0.07	1.50
4.88	1.37	20.96	6.41	134.39	2.97	0.07	1.50
4.90	1.40	21.41	6.24	133.60	2.95	0.07	1.53
4.92	1.43	21.85	6.02	131.45	2.93	0.07	1.56
4.94	1.43	21.68	5.94	128.70	2.92	0.07	1.55
4.97	1.42	21.39	5.90	126.16	2.92	0.07	1.53
4.98	1.39	20.94	5.95	124.58	2.93	0.07	1.50
5.00	1.37	20.55	6.06	124.51	2.94	0.07	1.47
5.02	1.34	19.99	6.27	125.37	2.96	0.07	1.43
5.04	1.30	19.37	6.55	126.82	2.98	0.07	1.38
5.07	1.27	18.74	6.85	128.39	3.01	0.07	1.34
5.08	1.25	18.50	6.98	129.15	3.02	0.07	1.32
5.10	1.25	18.37	7.00	128.68	3.02	0.07	1.31
5.12	1.25	18.31	6.96	127.43	3.02	0.07	1.31
5.14	1.23	17.99	7.02	126.26	3.02	0.07	1.28
5.16	1.21	17.52	7.16	125.46	3.04	0.07	1.25
5.18	1.17	16.84	7.39	124.36	3.06	0.07	1.20
5.21	1.12	16.11	7.62	122.69	3.07	0.07	1.15
5.22	1.08	15.41	7.86	121.09	3.09	0.07	1.10
5.24	1.05	14.93	7.98	119.17	3.10	0.07	1.07
5.26	1.03	14.55	8.05	117.11	3.11	0.06	1.04
5.28	1.02	14.40	7.93	114.25	3.10	0.06	1.03
5.30	1.03	14.48	7.63	110.57	3.08	0.06	1.03
5.32	1.05	14.78	7.22	106.81	3.04	0.06	1.06
5.34	1.08	15.12	6.83	103.28	3.01	0.07	1.08
5.36	1.10	15.47	6.52	100.91	2.98	0.07	1.10
5.38	1.12	15.74	6.32	99.48	2.96	0.07	1.12
5.40	1.14	15.95	6.21	99.00	2.95	0.07	1.14
5.42	1.15	16.08	6.16	99.09	2.95	0.07	1.15
5.44	1.17	16.26	6.13	99.70	2.94	0.07	1.16
5.46	1.18	16.43	6.11	100.38	2.94	0.07	1.17
5.52	1.19	16.45	6.13	100.81	2.94	0.07	1.17
5.52	1.19	16.46	6.13	101.00	2.94	0.07	1.18
5.52	1.22	16.83	6.02	101.31	2.93	0.07	1.20
5.54	1.25	17.28	5.90	101.97	2.92	0.07	1.24
5.56	1.30	17.92	5.74	102.88	2.90	0.07	1.29
5.58	1.34	18.39	5.65	103.84	2.89	0.07	1.32
5.60	1.37	18.77	5.61	105.26	2.89	0.07	1.35
5.62	1.39	19.06	5.62	107.16	2.89	0.07	1.37
5.64	1.40	19.14	5.71	109.34	2.90	0.07	1.37
5.66	1.39	18.99	5.89	111.86	2.92	0.07	1.36
5.68	1.38	18.88	6.04	114.07	2.93	0.07	1.35
5.70	1.36	18.59	6.27	116.66	2.96	0.07	1.33
5.72	1.36	18.45	6.45	119.05	2.97	0.07	1.32
5.74	1.33	18.04	6.74	121.67	3.00	0.07	1.29
5.76	1.31	17.66	7.00	123.67	3.02	0.07	1.26

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
5.78	1.28	17.17	7.27	124.74	3.05	0.07	1.23
5.80	1.26	16.78	7.46	125.20	3.06	0.07	1.20
5.82	1.23	16.41	7.63	125.19	3.08	0.07	1.17
5.84	1.22	16.24	7.63	123.84	3.08	0.07	1.16
5.86	1.23	16.21	7.55	122.32	3.07	0.07	1.16
5.88	1.23	16.24	7.42	120.53	3.06	0.07	1.16
5.90	1.23	16.19	7.38	119.40	3.05	0.07	1.16
5.92	1.21	15.85	7.46	118.15	3.06	0.07	1.13
5.94	1.18	15.35	7.63	117.15	3.08	0.07	1.10
5.96	1.14	14.80	7.88	116.61	3.10	0.07	1.06
5.98	1.12	14.45	8.01	115.73	3.11	0.07	1.03
6.01	1.13	14.46	7.87	113.82	3.10	0.06	1.03
6.02	1.14	14.62	7.64	111.63	3.08	0.07	1.04
6.04	1.15	14.68	7.49	110.00	3.06	0.07	1.05
6.07	1.12	14.33	7.66	109.83	3.08	0.07	1.02
6.08	1.09	13.81	8.02	110.70	3.11	0.06	0.99
6.10	1.04	13.15	8.50	111.79	3.14	0.06	0.94
6.12	1.01	12.64	8.95	113.08	3.18	0.06	0.90
6.14	0.98	12.22	9.32	113.91	3.21	0.06	0.87
6.16	0.96	11.93	9.53	113.71	3.22	0.06	0.85
6.18	0.94	11.62	9.63	111.91	3.23	0.06	0.83
6.20	0.92	11.26	9.68	108.93	3.23	0.06	0.80
6.22	0.89	10.84	9.68	104.93	3.23	0.06	0.77
6.24	0.87	10.54	9.56	100.74	3.22	0.06	0.75
6.26	0.85	10.25	9.46	96.96	3.22	0.06	0.73
6.28	0.83	9.92	9.51	94.32	3.22	0.06	0.71
6.30	0.81	9.66	9.57	92.44	3.22	0.06	0.69
6.32	0.82	9.70	9.33	90.57	3.21	0.06	0.69
6.34	0.85	10.13	8.73	88.48	3.16	0.06	0.72
6.36	0.89	10.56	8.19	86.55	3.12	0.06	0.75
6.38	0.91	10.86	7.82	84.91	3.09	0.06	0.78
6.40	0.94	11.20	7.45	83.42	3.06	0.06	0.80
6.42	0.96	11.49	7.11	81.63	3.03	0.06	0.82
6.44	0.99	11.89	6.67	79.36	2.99	0.06	0.85
6.46	1.01	12.04	6.48	78.03	2.98	0.06	0.86
6.48	1.01	12.02	6.46	77.64	2.97	0.06	0.86
6.50	0.98	11.71	6.76	79.08	3.00	0.06	0.84
6.52	0.96	11.34	7.09	80.39	3.03	0.06	0.81
6.54	0.93	10.93	7.51	82.09	3.07	0.06	0.78
6.56	0.90	10.55	7.98	84.26	3.10	0.06	0.75
6.58	0.88	10.23	8.48	86.78	3.14	0.06	0.73
6.60	0.87	10.10	8.80	88.81	3.17	0.06	0.72
6.62	0.88	10.10	8.88	89.63	3.17	0.06	0.72
6.64	0.89	10.20	8.68	88.56	3.16	0.06	0.73
6.66	0.90	10.40	8.34	86.78	3.13	0.06	0.74
6.69	0.92	10.55	8.03	84.72	3.11	0.06	0.75
6.70	0.92	10.61	7.84	83.20	3.09	0.06	0.76
6.72	0.92	10.51	7.81	82.08	3.09	0.06	0.75

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
6.74	0.91	10.41	7.80	81.13	3.09	0.06	0.74
6.76	0.91	10.32	7.84	80.93	3.09	0.06	0.74
6.78	0.89	10.14	8.07	81.79	3.11	0.06	0.72
6.80	0.87	9.78	8.44	82.61	3.14	0.06	0.70
6.82	0.83	9.23	8.96	82.69	3.18	0.06	0.66
6.84	0.80	8.83	9.27	81.84	3.20	0.06	0.63
6.86	0.77	8.40	9.63	80.91	3.23	0.06	0.60
6.88	0.75	8.10	9.98	80.88	3.25	0.06	0.58
6.90	0.72	7.79	10.35	80.58	3.28	0.06	0.56
6.92	0.73	7.89	10.22	80.65	3.27	0.06	0.56
6.94	0.76	8.19	9.81	80.41	3.24	0.06	0.59
6.96	0.77	8.34	9.50	79.25	3.22	0.06	0.60
6.98	0.76	8.21	9.43	77.43	3.21	0.06	0.59
7.00	0.74	7.93	9.35	74.16	3.21	0.06	0.57
7.02	0.76	8.13	8.67	70.51	3.16	0.06	0.58
7.04	0.81	8.74	7.60	66.45	3.07	0.06	0.62
7.06	0.88	9.65	6.60	63.67	2.99	0.06	0.69
7.08	0.97	10.76	5.90	63.47	2.92	0.06	0.77
7.10	1.04	11.66	5.52	64.36	2.88	0.07	0.84
7.12	1.13	12.67	5.24	66.42	2.85	0.07	0.91
7.14	1.18	13.34	5.25	70.00	2.85	0.07	0.96
7.16	1.23	13.99	5.46	76.33	2.87	0.07	1.00
7.18	1.27	14.50	5.79	83.91	2.91	0.07	1.04
7.20	1.32	15.01	6.05	90.85	2.94	0.07	1.07
7.22	1.36	15.52	6.21	96.37	2.95	0.07	1.11
7.24	1.39	15.88	6.40	101.65	2.97	0.07	1.13
7.26	1.41	16.14	6.58	106.24	2.99	0.07	1.15
7.28	1.42	16.15	6.81	110.01	3.01	0.07	1.15
7.30	1.39	15.77	7.11	112.02	3.03	0.07	1.13
7.32	1.35	15.19	7.41	112.57	3.06	0.07	1.08
7.34	1.30	14.53	7.69	111.81	3.08	0.07	1.04
7.36	1.27	14.17	7.75	109.91	3.09	0.07	1.01
7.38	1.27	14.07	7.66	107.74	3.08	0.07	1.01
7.40	1.29	14.33	7.38	105.80	3.06	0.07	1.02
7.42	1.35	14.98	6.96	104.31	3.02	0.07	1.07
7.44	1.40	15.61	6.63	103.41	2.99	0.07	1.11
7.46	1.46	16.28	6.40	104.23	2.97	0.07	1.16
7.48	1.48	16.53	6.43	106.32	2.97	0.07	1.18
7.50	1.52	16.95	6.43	109.01	2.97	0.07	1.21
7.52	1.53	17.06	6.55	111.78	2.98	0.07	1.22
7.54	1.54	17.14	6.69	114.71	3.00	0.07	1.22
7.56	1.51	16.78	7.01	117.58	3.02	0.07	1.20
7.58	1.51	16.68	7.16	119.50	3.04	0.07	1.19
7.60	1.52	16.82	7.19	120.99	3.04	0.07	1.20
7.62	1.55	17.09	7.16	122.37	3.04	0.07	1.22
7.64	1.55	17.07	7.24	123.56	3.04	0.07	1.22
7.66	1.49	16.34	7.58	123.89	3.07	0.07	1.17
7.68	1.40	15.24	8.12	123.71	3.12	0.07	1.09

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
7.70	1.30	13.91	8.83	122.82	3.17	0.07	0.99
7.72	1.22	12.97	9.43	122.22	3.21	0.07	0.93
7.74	1.16	12.24	9.91	121.28	3.25	0.06	0.87
7.76	1.13	11.84	10.20	120.74	3.27	0.06	0.85
7.78	1.12	11.63	10.34	120.21	3.28	0.06	0.83
7.80	1.12	11.65	10.23	119.18	3.27	0.06	0.83
7.82	1.17	12.23	9.51	116.28	3.22	0.06	0.87
7.84	1.27	13.37	8.43	112.78	3.14	0.07	0.96
7.86	1.41	15.02	7.30	109.59	3.05	0.07	1.07
7.88	1.54	16.48	6.60	108.71	2.99	0.07	1.18
7.90	1.62	17.38	6.27	108.87	2.96	0.07	1.24
7.92	1.64	17.59	6.26	110.08	2.95	0.07	1.26
7.94	1.63	17.47	6.45	112.76	2.97	0.07	1.25
7.96	1.62	17.26	6.76	116.68	3.00	0.07	1.23
7.98	1.62	17.22	7.00	120.58	3.02	0.07	1.23
8.00	1.62	17.25	7.23	124.62	3.04	0.07	1.23
8.02	1.64	17.41	7.32	127.41	3.05	0.07	1.24
8.04	1.65	17.49	7.42	129.80	3.06	0.07	1.25
8.06	1.66	17.52	7.47	130.94	3.06	0.07	1.25
8.08	1.67	17.65	7.49	132.19	3.06	0.07	1.26
8.10	1.70	17.98	7.40	133.04	3.06	0.07	1.28
8.12	1.75	18.49	7.23	133.67	3.04	0.07	1.32
8.15	1.78	18.78	7.12	133.74	3.03	0.07	1.34
8.16	1.82	19.21	6.98	134.12	3.02	0.07	1.37
8.18	1.84	19.41	6.92	134.43	3.02	0.07	1.39
8.20	1.87	19.67	6.84	134.49	3.01	0.07	1.41
8.22	1.87	19.58	6.84	133.89	3.01	0.07	1.40
8.24	1.85	19.32	6.83	132.04	3.01	0.07	1.38
8.26	1.81	18.85	6.92	130.45	3.02	0.07	1.35
8.28	1.76	18.18	7.15	130.02	3.04	0.07	1.30
8.30	1.72	17.75	7.36	130.66	3.05	0.07	1.27
8.32	1.72	17.68	7.43	131.32	3.06	0.07	1.26
8.34	1.74	17.88	7.34	131.29	3.05	0.07	1.28
8.36	1.73	17.69	7.45	131.72	3.06	0.07	1.26
8.38	1.66	16.96	7.76	131.63	3.09	0.07	1.21
8.40	1.58	15.99	8.20	131.11	3.12	0.07	1.14
8.42	1.48	14.84	8.77	130.17	3.17	0.07	1.06
8.44	1.38	13.67	9.49	129.65	3.22	0.07	0.98
8.46	1.27	12.43	10.34	128.48	3.28	0.07	0.89
8.48	1.19	11.51	11.02	126.92	3.32	0.06	0.82
8.50	1.12	10.73	11.57	124.14	3.35	0.06	0.77
8.52	1.08	10.24	11.80	120.87	3.37	0.06	0.73
8.54	1.05	9.88	11.74	116.06	3.36	0.06	0.71
8.56	1.04	9.75	11.41	111.22	3.34	0.06	0.70
8.58	1.01	9.46	11.17	105.63	3.33	0.06	0.68
8.60	0.99	9.21	10.93	100.66	3.31	0.06	0.66
8.62	0.98	9.02	10.56	95.27	3.29	0.06	0.64
8.64	0.98	9.05	10.09	91.25	3.26	0.06	0.65

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
8.66	1.00	9.17	9.63	88.31	3.23	0.06	0.66
8.68	1.04	9.62	9.04	86.98	3.19	0.06	0.69
8.70	1.12	10.54	8.11	85.41	3.11	0.06	0.75
8.72	1.26	11.94	6.98	83.32	3.02	0.06	0.85
8.74	1.39	13.35	6.12	81.62	2.94	0.07	0.95
8.76	1.51	14.61	5.58	81.55	2.89	0.07	1.04
8.78	1.60	15.61	5.29	82.67	2.86	0.07	1.12
8.80	1.68	16.40	5.15	84.48	2.84	0.08	1.17
8.82	1.76	17.18	4.98	85.60	2.82	0.08	1.23
8.84	1.81	17.70	5.00	88.51	2.82	0.08	1.27
8.86	1.87	18.36	4.96	91.09	2.82	0.08	1.31
8.88	1.92	18.82	5.01	94.38	2.83	0.08	1.35
8.90	1.95	19.14	5.18	99.10	2.84	0.08	1.37
8.93	1.95	19.10	5.51	105.27	2.88	0.08	1.36
8.94	1.93	18.88	5.93	112.01	2.92	0.08	1.35
8.96	1.90	18.52	6.34	117.35	2.96	0.07	1.32
8.98	1.87	18.15	6.68	121.17	2.99	0.07	1.30
9.00	1.84	17.80	6.97	124.03	3.02	0.07	1.27
9.02	1.85	17.82	6.99	124.60	3.02	0.07	1.27
9.04	1.88	18.09	6.85	123.94	3.01	0.07	1.29
9.06	1.91	18.40	6.66	122.57	2.99	0.07	1.31
9.08	1.94	18.73	6.47	121.19	2.97	0.07	1.34
9.10	1.97	19.00	6.31	119.95	2.96	0.07	1.36
9.12	2.00	19.28	6.19	119.29	2.95	0.07	1.38
9.14	2.01	19.31	6.18	119.28	2.95	0.07	1.38
9.16	2.01	19.26	6.24	120.18	2.95	0.07	1.38
9.18	2.00	19.13	6.30	120.48	2.96	0.07	1.37
9.20	1.99	19.02	6.38	121.25	2.97	0.07	1.36
9.22	1.98	18.88	6.48	122.25	2.98	0.07	1.35
9.24	1.98	18.79	6.58	123.67	2.99	0.07	1.34
9.26	1.99	18.84	6.59	124.06	2.99	0.07	1.35
9.28	2.00	18.91	6.54	123.65	2.98	0.07	1.35
9.30	2.01	18.99	6.49	123.23	2.98	0.07	1.36
9.32	2.02	19.03	6.48	123.29	2.98	0.07	1.36
9.34	2.04	19.26	6.37	122.75	2.97	0.07	1.38
9.36	2.09	19.67	6.25	122.92	2.95	0.07	1.41
9.38	2.19	20.66	5.93	122.46	2.92	0.08	1.48
9.40	2.29	21.68	5.62	121.90	2.89	0.08	1.55
9.42	2.35	22.23	5.44	120.86	2.87	0.08	1.59
9.44	2.31	21.79	5.58	121.49	2.89	0.08	1.56
9.46	2.20	20.59	6.04	124.32	2.93	0.08	1.47
9.48	2.06	19.20	6.64	127.42	2.99	0.07	1.37
9.50	1.96	18.11	7.18	130.04	3.04	0.07	1.29
9.52	1.89	17.36	7.59	131.69	3.07	0.07	1.24
9.54	1.86	17.05	7.78	132.56	3.09	0.07	1.22
9.56	1.85	16.88	7.87	132.76	3.10	0.07	1.21
9.58	1.86	16.99	7.77	131.96	3.09	0.07	1.21
9.60	1.88	17.12	7.62	130.38	3.07	0.07	1.22

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.62	1.91	17.35	7.37	127.83	3.05	0.07	1.24
9.64	1.93	17.53	7.11	124.73	3.03	0.07	1.25
9.66	1.94	17.60	6.89	121.30	3.01	0.07	1.26
9.68	1.92	17.39	6.81	118.44	3.01	0.07	1.24
9.70	1.86	16.76	6.95	116.47	3.02	0.07	1.20
9.72	1.76	15.72	7.35	115.57	3.05	0.07	1.12
9.74	1.62	14.27	8.08	115.29	3.11	0.07	1.02
9.76	1.45	12.61	9.12	115.05	3.19	0.07	0.90
9.78	1.30	11.13	10.27	114.36	3.27	0.06	0.80
9.80	1.24	10.43	10.77	112.37	3.30	0.06	0.75
9.82	1.19	9.96	11.00	109.52	3.32	0.06	0.71
9.84	1.16	9.62	10.93	105.09	3.31	0.06	0.69
9.86	1.08	8.90	11.15	99.19	3.33	0.06	0.64
9.88	1.05	8.51	10.89	92.67	3.31	0.06	0.61
9.90	1.05	8.57	10.08	86.37	3.26	0.06	0.61
9.92	1.08	8.80	9.18	80.77	3.19	0.06	0.63
9.95	1.09	8.83	8.43	74.48	3.14	0.06	0.63
9.96	1.06	8.58	8.11	69.56	3.11	0.06	0.61
9.98	1.03	8.29	7.90	65.47	3.10	0.06	0.59
10.00	1.01	8.06	7.85	63.27	3.09	0.06	0.58
10.02	0.98	7.79	7.92	61.68	3.10	0.06	0.56
10.04	0.96	7.57	8.04	60.90	3.11	0.06	0.54
10.06	0.95	7.41	8.20	60.71	3.12	0.06	0.53
10.08	0.93	7.25	8.36	60.60	3.13	0.06	0.52
10.10	0.91	7.02	8.52	59.82	3.15	0.06	0.50
10.12	0.89	6.80	8.73	59.40	3.16	0.06	0.49
10.14	0.87	6.66	8.80	58.63	3.17	0.06	0.48
10.16	0.87	6.62	8.87	58.64	3.17	0.06	0.47
10.18	0.87	6.60	8.94	59.06	3.18	0.06	0.47
10.20	0.87	6.61	9.07	59.92	3.19	0.06	0.47
10.22	0.88	6.67	9.11	60.81	3.19	0.06	0.48
10.24	0.93	7.13	8.54	60.90	3.15	0.06	0.51
10.26	1.03	8.09	7.51	60.78	3.07	0.06	0.58
10.28	1.15	9.23	6.63	61.23	2.99	0.06	0.66
10.30	1.29	10.49	5.91	61.97	2.92	0.07	0.75
10.32	1.40	11.59	5.47	63.33	2.88	0.07	0.83
10.34	1.51	12.56	5.13	64.38	2.84	0.07	0.90
10.36	1.54	12.84	5.30	68.06	2.86	0.07	0.92
10.38	1.53	12.70	5.75	73.06	2.91	0.07	0.91
10.40	1.50	12.44	6.29	78.30	2.96	0.07	0.89
10.42	1.50	12.38	6.64	82.20	2.99	0.07	0.88
10.44	1.50	12.34	6.92	85.41	3.02	0.07	0.88
10.46	1.48	12.19	7.23	88.11	3.04	0.07	0.87
10.48	1.46	11.95	7.54	90.13	3.07	0.07	0.85
10.50	1.42	11.58	7.85	90.86	3.09	0.07	0.83
10.52	1.38	11.15	8.18	91.19	3.12	0.06	0.80
10.54	1.34	10.73	8.47	90.85	3.14	0.06	0.77
10.56	1.31	10.49	8.56	89.84	3.15	0.06	0.75

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
10.58	1.31	10.49	8.43	88.37	3.14	0.06	0.75
10.60	1.32	10.49	8.31	87.18	3.13	0.06	0.75
10.62	1.32	10.54	8.23	86.73	3.12	0.06	0.75
10.64	1.34	10.62	8.15	86.53	3.12	0.06	0.76
10.66	1.38	10.99	7.85	86.25	3.09	0.06	0.79
10.68	1.46	11.73	7.33	85.94	3.05	0.07	0.84
10.70	1.55	12.56	6.86	86.22	3.01	0.07	0.90
10.72	1.62	13.20	6.64	87.70	2.99	0.07	0.94
10.74	1.66	13.55	6.63	89.84	2.99	0.07	0.97
10.76	1.68	13.69	6.69	91.66	3.00	0.07	0.98
10.78	1.68	13.63	6.84	93.24	3.01	0.07	0.97
10.80	1.66	13.44	7.10	95.37	3.03	0.07	0.96
10.82	1.63	13.14	7.52	98.86	3.07	0.07	0.94
10.84	1.61	12.91	7.94	102.55	3.10	0.07	0.92
10.86	1.57	12.56	8.42	105.78	3.14	0.07	0.90
10.88	1.54	12.23	8.79	107.51	3.17	0.07	0.87
10.90	1.51	11.92	9.06	108.02	3.19	0.07	0.85
10.92	1.49	11.71	9.19	107.61	3.20	0.07	0.84
10.94	1.46	11.49	9.31	106.93	3.20	0.07	0.82
10.96	1.42	11.10	9.50	105.39	3.22	0.07	0.79
10.98	1.38	10.70	9.67	103.54	3.23	0.06	0.76
11.00	1.35	10.40	9.70	100.86	3.23	0.06	0.74
11.02	1.35	10.39	9.50	98.73	3.22	0.06	0.74
11.04	1.35	10.41	9.28	96.65	3.20	0.06	0.74
11.06	1.36	10.42	9.13	95.14	3.19	0.06	0.74
11.08	1.36	10.38	9.03	93.76	3.18	0.06	0.74
11.10	1.36	10.41	8.90	92.64	3.17	0.06	0.74
11.13	1.36	10.41	8.86	92.24	3.17	0.06	0.74
11.14	1.37	10.46	8.88	92.90	3.17	0.06	0.75
11.17	1.38	10.55	8.95	94.43	3.18	0.06	0.75
11.18	1.40	10.68	8.98	95.89	3.18	0.06	0.76
11.20	1.43	10.95	8.82	96.63	3.17	0.06	0.78
11.22	1.48	11.33	8.54	96.78	3.15	0.07	0.81
11.24	1.54	11.84	8.18	96.81	3.12	0.07	0.85
11.26	1.59	12.26	7.91	96.98	3.10	0.07	0.88
11.28	1.63	12.62	7.68	97.01	3.08	0.07	0.90
11.30	1.67	12.97	7.49	97.09	3.06	0.07	0.93
11.32	1.71	13.29	7.36	97.83	3.05	0.07	0.95
11.34	1.76	13.70	7.24	99.22	3.04	0.07	0.98
11.36	1.81	14.12	7.16	101.08	3.04	0.07	1.01
11.39	1.86	14.50	7.15	103.69	3.04	0.07	1.04
11.40	1.89	14.73	7.26	106.92	3.04	0.07	1.05
11.42	1.91	14.87	7.44	110.73	3.06	0.07	1.06
11.44	1.91	14.92	7.63	113.82	3.08	0.07	1.07
11.46	1.89	14.71	7.94	116.91	3.10	0.07	1.05
11.48	1.85	14.29	8.37	119.62	3.13	0.07	1.02
11.50	1.79	13.81	8.85	122.25	3.17	0.07	0.99
11.52	1.74	13.33	9.32	124.17	3.20	0.07	0.95

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
11.54	1.69	12.89	9.72	125.33	3.23	0.07	0.92
11.56	1.65	12.45	10.08	125.42	3.26	0.07	0.89
11.58	1.61	12.14	10.27	124.70	3.27	0.07	0.87
11.60	1.60	12.04	10.23	123.23	3.27	0.07	0.86
11.62	1.62	12.12	9.99	121.12	3.25	0.07	0.87
11.64	1.62	12.16	9.75	118.53	3.23	0.07	0.87
11.66	1.62	12.07	9.60	115.83	3.22	0.07	0.86
11.68	1.61	11.99	9.48	113.63	3.22	0.07	0.86
11.70	1.60	11.92	9.40	112.05	3.21	0.07	0.85
11.72	1.60	11.90	9.33	111.05	3.21	0.07	0.85
11.75	1.58	11.70	9.38	109.75	3.21	0.07	0.84
11.76	1.57	11.62	9.32	108.32	3.21	0.07	0.83
11.78	1.54	11.28	9.34	105.35	3.21	0.07	0.81
11.80	1.54	11.27	9.26	104.39	3.20	0.06	0.81
11.82	1.52	11.13	9.35	104.02	3.21	0.07	0.79
11.84	1.52	11.10	9.44	104.79	3.21	0.07	0.79
11.86	1.49	10.77	9.61	103.51	3.23	0.06	0.77
11.88	1.45	10.43	9.75	101.69	3.24	0.06	0.74
11.91	1.44	10.30	9.71	99.97	3.23	0.06	0.74
11.92	1.43	10.22	9.66	98.70	3.23	0.06	0.73
11.94	1.43	10.25	9.54	97.81	3.22	0.06	0.73
11.96	1.43	10.24	9.52	97.46	3.22	0.06	0.73
11.98	1.44	10.30	9.42	97.04	3.21	0.06	0.74
12.00	1.48	10.56	9.06	95.63	3.19	0.06	0.75
12.02	1.50	10.74	8.76	94.09	3.16	0.07	0.77
12.04	1.51	10.79	8.62	93.01	3.15	0.07	0.77
12.06	1.48	10.56	8.78	92.76	3.17	0.06	0.75
12.08	1.45	10.24	9.01	92.29	3.18	0.06	0.73
12.10	1.42	9.99	9.19	91.73	3.20	0.06	0.71
12.20	1.40	9.78	9.32	91.15	3.20	0.06	0.70
12.20	1.40	9.74	9.33	90.85	3.21	0.06	0.70
12.11	1.38	9.69	9.30	90.08	3.20	0.06	0.69
12.20	1.37	9.52	9.31	88.56	3.20	0.06	0.68
12.22	1.35	9.32	9.38	87.45	3.21	0.06	0.67
12.24	1.33	9.13	9.53	87.07	3.22	0.06	0.65
12.26	1.30	8.91	9.73	86.64	3.23	0.06	0.64
12.28	1.30	8.83	9.70	85.69	3.23	0.06	0.63
12.30	1.29	8.75	9.63	84.23	3.23	0.06	0.62
12.32	1.27	8.61	9.60	82.68	3.22	0.06	0.62
12.34	1.25	8.38	9.69	81.22	3.23	0.06	0.60
12.36	1.23	8.26	9.67	79.88	3.23	0.06	0.59
12.38	1.25	8.39	9.33	78.25	3.21	0.06	0.60
12.40	1.28	8.65	8.93	77.17	3.18	0.06	0.62
12.42	1.32	8.94	8.60	76.88	3.15	0.06	0.64
12.44	1.34	9.10	8.50	77.34	3.14	0.06	0.65
12.46	1.37	9.33	8.30	77.43	3.13	0.06	0.67
12.48	1.41	9.64	8.01	77.23	3.11	0.06	0.69
12.50	1.45	9.94	7.78	77.33	3.09	0.06	0.71

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
12.52	1.45	9.89	7.94	78.48	3.10	0.06	0.71
12.55	1.41	9.57	8.32	79.65	3.13	0.06	0.68
12.56	1.36	9.12	8.79	80.21	3.17	0.06	0.65
12.58	1.30	8.62	9.30	80.20	3.20	0.06	0.62
12.60	1.24	8.13	9.82	79.86	3.24	0.06	0.58
12.62	1.19	7.76	10.25	79.60	3.27	0.06	0.55
12.64	1.19	7.69	10.27	78.94	3.27	0.06	0.55
12.66	1.20	7.80	10.02	78.23	3.25	0.06	0.56
12.68	1.21	7.85	9.84	77.20	3.24	0.06	0.56
12.70	1.19	7.67	9.89	75.89	3.24	0.06	0.55
12.72	1.14	7.28	10.27	74.73	3.27	0.06	0.52
12.74	1.09	6.90	10.75	74.21	3.30	0.06	0.49
12.76	1.05	6.56	11.24	73.71	3.33	0.06	0.47
12.78	1.03	6.39	11.43	72.99	3.35	0.06	0.46
12.80	1.01	6.18	11.63	71.93	3.36	0.06	0.44
12.83	0.99	6.06	11.73	71.15	3.36	0.06	0.43
12.84	0.98	5.91	12.00	70.88	3.38	0.06	0.42
12.86	0.97	5.85	12.04	70.47	3.38	0.06	0.42
12.88	0.97	5.85	11.96	69.97	3.38	0.06	0.42
12.90	0.96	5.77	11.98	69.18	3.38	0.06	0.41
12.92	0.93	5.53	12.35	68.29	3.40	0.06	0.39
12.94	0.89	5.19	12.98	67.43	3.44	0.06	0.37
12.96	0.85	4.84	13.63	65.90	3.47	0.06	0.35
12.98	0.80	4.47	14.30	63.96	3.51	0.06	0.32
13.00	0.77	4.18	14.77	61.67	3.54	0.06	0.30
13.02	0.74	3.98	15.02	59.83	3.55	0.06	0.28
13.04	0.74	4.00	14.50	58.05	3.52	0.06	0.29
13.06	0.78	4.26	13.23	56.41	3.45	0.06	0.30
13.08	0.83	4.65	11.68	54.31	3.36	0.06	0.33
13.10	0.88	5.01	10.46	52.39	3.28	0.06	0.36
13.12	0.88	5.04	10.00	50.35	3.25	0.06	0.36
13.14	0.86	4.89	9.79	47.87	3.24	0.06	0.35
13.16	0.89	5.09	9.00	45.83	3.18	0.06	0.36
13.18	0.99	5.87	7.68	45.09	3.08	0.06	0.42
13.20	1.10	6.72	6.92	46.54	3.02	0.06	0.48
13.22	1.14	7.01	6.96	48.80	3.02	0.06	0.50
13.24	1.14	7.00	7.18	50.20	3.04	0.06	0.50
13.26	1.17	7.23	6.98	50.51	3.02	0.06	0.52
13.28	1.19	7.37	6.91	50.92	3.01	0.06	0.53
13.30	1.14	6.97	7.51	52.36	3.07	0.06	0.50
13.32	1.10	6.64	8.10	53.75	3.11	0.06	0.47
13.34	1.14	6.95	7.79	54.17	3.09	0.06	0.50
13.36	1.22	7.55	7.23	54.55	3.04	0.06	0.54
13.41	1.25	7.80	7.04	54.86	3.03	0.06	0.56
13.41	1.12	6.75	8.21	55.42	3.12	0.06	0.48
13.42	0.96	5.50	9.89	54.43	3.24	0.06	0.39
13.44	0.78	4.13	12.47	51.49	3.41	0.06	0.30
13.46	0.73	3.72	13.32	49.54	3.46	0.06	0.27

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
13.48	0.80	4.27	11.79	50.41	3.37	0.06	0.31
13.50	1.11	6.65	7.91	52.56	3.10	0.06	0.47
13.52	1.58	10.20	5.10	52.07	2.84	0.07	0.73
13.54	2.07	14.28	3.64	51.90	2.65	0.08	1.00
13.56	2.38	16.73	3.25	54.35	2.59	0.08	0.60
13.58	2.53	17.88	3.29	58.76	2.59	0.08	0.61
13.60	2.51	17.65	3.56	62.75	2.64	0.08	1.23
13.62	2.35	16.26	4.07	66.25	2.71	0.08	1.15
13.64	2.04	13.67	5.03	68.80	2.83	0.08	0.98
13.66	1.63	10.51	6.55	68.88	2.98	0.07	0.75
13.68	1.27	7.73	8.49	65.65	3.14	0.06	0.55
13.70	1.01	5.81	10.36	60.22	3.28	0.06	0.42
13.72	0.88	4.76	11.68	55.60	3.36	0.06	0.34
13.74	0.80	4.16	12.75	53.01	3.42	0.06	0.30
13.76	0.75	3.80	13.50	51.30	3.47	0.06	0.27
13.78	0.74	3.73	14.00	52.24	3.50	0.06	0.27
13.80	0.74	3.71	13.99	51.93	3.49	0.06	0.27
13.83	0.72	3.57	14.27	50.92	3.51	0.06	0.25
13.84	0.68	3.27	14.64	47.80	3.53	0.06	0.23
13.86	0.63	2.90	15.64	45.33	3.58	0.06	0.21
14.03	0.61	2.66	16.47	43.79	3.62	0.06	0.19
14.03	0.60	2.58	16.76	43.21	3.64	0.06	0.18
14.03	0.60	2.58	16.71	43.17	3.64	0.06	0.18
13.88	0.63	2.88	15.15	43.67	3.56	0.06	0.21
13.96	0.68	3.24	13.52	43.79	3.47	0.06	0.23
13.98	0.74	3.68	11.90	43.81	3.37	0.06	0.26
14.00	0.78	3.96	11.19	44.32	3.33	0.06	0.28
14.02	0.81	4.20	10.73	45.10	3.30	0.06	0.30
14.04	0.85	4.48	10.33	46.26	3.27	0.06	0.32
14.06	0.89	4.76	10.00	47.58	3.25	0.06	0.34
14.08	0.93	5.06	9.70	49.14	3.23	0.06	0.36
14.10	0.97	5.32	9.52	50.62	3.22	0.06	0.38
14.12	1.00	5.57	9.31	51.84	3.20	0.06	0.40
14.14	1.02	5.72	9.19	52.52	3.20	0.06	0.41
14.16	1.02	5.71	9.23	52.68	3.20	0.06	0.41
14.18	1.00	5.55	9.50	52.76	3.22	0.06	0.40
14.21	0.98	5.33	9.89	52.73	3.24	0.06	0.38
14.22	0.96	5.24	10.07	52.75	3.26	0.06	0.37
14.24	0.96	5.19	10.19	52.84	3.27	0.06	0.37
14.26	0.96	5.21	10.21	53.14	3.27	0.06	0.37
14.28	0.96	5.22	10.30	53.76	3.27	0.06	0.37
14.30	0.97	5.23	10.45	54.62	3.28	0.06	0.37
14.32	0.97	5.22	10.63	55.52	3.29	0.06	0.37
14.37	0.97	5.19	10.80	56.06	3.31	0.06	0.37
14.37	0.97	5.22	10.93	57.03	3.31	0.06	0.37
14.38	0.97	5.24	11.13	58.30	3.33	0.06	0.37
14.40	0.98	5.29	11.31	59.89	3.34	0.06	0.38
14.42	0.99	5.37	11.36	61.00	3.34	0.06	0.38

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
14.44	1.01	5.51	11.24	61.92	3.33	0.06	0.39
14.46	1.03	5.65	11.11	62.72	3.33	0.06	0.40
14.48	1.06	5.80	10.95	63.57	3.32	0.06	0.41
14.50	1.09	6.01	10.70	64.34	3.30	0.06	0.43
14.52	1.12	6.24	10.39	64.87	3.28	0.06	0.45
14.54	1.15	6.46	10.10	65.31	3.26	0.06	0.46
14.56	1.17	6.57	10.01	65.71	3.25	0.06	0.47
14.58	1.17	6.56	10.10	66.25	3.26	0.06	0.47
14.60	1.15	6.46	10.31	66.63	3.27	0.06	0.46
14.62	1.14	6.38	10.46	66.71	3.28	0.06	0.46
14.64	1.14	6.33	10.50	66.46	3.29	0.06	0.45
14.66	1.15	6.40	10.34	66.20	3.28	0.06	0.46
14.68	1.18	6.63	9.94	65.91	3.25	0.06	0.47
14.70	1.22	6.91	9.55	65.97	3.22	0.06	0.49
14.72	1.26	7.19	9.20	66.16	3.20	0.06	0.51
14.74	1.29	7.36	9.05	66.67	3.19	0.06	0.53
14.76	1.31	7.48	9.12	68.15	3.19	0.06	0.53
14.78	1.32	7.55	9.33	70.46	3.21	0.06	0.54
14.80	1.34	7.67	9.58	73.53	3.22	0.06	0.55
14.82	1.36	7.83	9.72	76.07	3.23	0.06	0.56
14.84	1.39	8.06	9.76	78.67	3.24	0.06	0.58
14.86	1.42	8.22	9.81	80.67	3.24	0.06	0.59
14.88	1.44	8.37	9.82	82.16	3.24	0.06	0.60
14.90	1.44	8.37	9.90	82.81	3.25	0.06	0.60
14.92	1.44	8.36	9.92	82.96	3.25	0.06	0.60
14.94	1.45	8.36	9.94	83.13	3.25	0.06	0.60
14.96	1.45	8.37	9.96	83.40	3.25	0.06	0.60
14.98	1.46	8.43	9.96	83.91	3.25	0.06	0.60
15.00	1.48	8.55	9.84	84.17	3.24	0.06	0.61
15.02	1.50	8.73	9.66	84.24	3.23	0.06	0.62
15.04	1.53	8.89	9.48	84.26	3.22	0.06	0.63
15.06	1.54	8.93	9.47	84.58	3.22	0.06	0.64
15.08	1.53	8.90	9.49	84.46	3.22	0.06	0.64
15.10	1.52	8.80	9.53	83.81	3.22	0.06	0.63
15.12	1.52	8.75	9.48	82.95	3.22	0.06	0.62
15.14	1.51	8.70	9.47	82.33	3.22	0.06	0.62
15.16	1.51	8.68	9.45	82.01	3.21	0.06	0.62
15.18	1.51	8.68	9.39	81.47	3.21	0.06	0.62
15.20	1.52	8.72	9.30	81.05	3.20	0.06	0.62
15.22	1.53	8.77	9.23	80.89	3.20	0.06	0.63
15.24	1.54	8.83	9.16	80.90	3.19	0.06	0.63
15.26	1.56	8.95	9.07	81.13	3.19	0.06	0.64
15.28	1.57	9.01	9.10	81.93	3.19	0.06	0.64
15.30	1.57	9.02	9.25	83.44	3.20	0.06	0.64
15.32	1.56	8.95	9.47	84.74	3.22	0.06	0.64
15.34	1.57	8.98	9.58	86.01	3.22	0.06	0.64
15.36	1.57	9.00	9.68	87.17	3.23	0.06	0.64
15.38	1.59	9.09	9.72	88.34	3.23	0.06	0.65

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
15.40	1.60	9.18	9.65	88.56	3.23	0.06	0.66
15.42	1.63	9.37	9.35	87.64	3.21	0.06	0.67
15.44	1.66	9.57	8.99	86.00	3.18	0.06	0.68
15.46	1.68	9.67	8.74	84.55	3.16	0.06	0.69
15.48	1.69	9.71	8.63	83.80	3.15	0.06	0.69
15.50	1.69	9.72	8.62	83.76	3.15	0.06	0.69
15.52	1.69	9.72	8.65	84.10	3.16	0.06	0.69
15.54	1.70	9.76	8.68	84.69	3.16	0.06	0.70
15.56	1.70	9.77	8.79	85.79	3.17	0.07	0.70
15.58	1.70	9.70	8.95	86.88	3.18	0.07	0.69
15.60	1.67	9.51	9.22	87.69	3.20	0.06	0.68
15.62	1.64	9.28	9.48	87.99	3.22	0.06	0.66
15.64	1.62	9.14	9.62	87.88	3.23	0.06	0.65
15.66	1.62	9.09	9.58	87.07	3.22	0.06	0.65
15.68	1.63	9.15	9.38	85.80	3.21	0.06	0.65
15.70	1.64	9.22	9.17	84.47	3.19	0.06	0.66
15.72	1.64	9.21	9.11	83.93	3.19	0.06	0.66
15.74	1.62	9.06	9.24	83.72	3.20	0.06	0.65
15.76	1.59	8.88	9.46	83.96	3.21	0.06	0.63
15.78	1.56	8.66	9.72	84.16	3.23	0.06	0.62
15.80	1.58	8.73	9.82	85.80	3.24	0.06	0.62
15.82	1.56	8.62	10.10	87.07	3.26	0.06	0.62
15.84	1.56	8.60	10.25	88.14	3.27	0.06	0.61
15.86	1.53	8.41	10.46	87.93	3.28	0.06	0.60
15.88	1.55	8.52	10.32	87.93	3.27	0.06	0.61
15.90	1.56	8.58	10.26	87.96	3.27	0.06	0.61
15.92	1.58	8.69	10.10	87.74	3.26	0.06	0.62
15.94	1.59	8.74	9.99	87.34	3.25	0.06	0.62
15.96	1.59	8.72	10.02	87.39	3.25	0.06	0.62
15.98	1.57	8.61	10.23	88.12	3.27	0.06	0.62
16.00	1.58	8.61	10.35	89.09	3.28	0.06	0.61
16.02	1.63	8.98	10.02	90.03	3.25	0.06	0.64
16.04	1.74	9.69	9.33	90.41	3.21	0.06	0.69
16.07	1.87	10.52	8.58	90.19	3.15	0.07	0.75
16.08	1.99	11.29	7.90	89.18	3.10	0.07	0.81
16.10	2.07	11.83	7.41	87.67	3.06	0.07	0.84
16.12	2.11	12.06	7.18	86.52	3.04	0.07	0.86
16.14	2.10	11.98	7.23	86.63	3.04	0.07	0.86
16.16	2.09	11.92	7.39	88.06	3.06	0.07	0.85
16.18	2.11	12.05	7.50	90.35	3.07	0.07	0.86
16.20	2.15	12.26	7.60	93.16	3.07	0.07	0.88
16.22	2.16	12.32	7.80	96.16	3.09	0.07	0.88
16.24	2.15	12.22	8.06	98.49	3.11	0.07	0.87
16.26	2.12	12.00	8.44	101.29	3.14	0.07	0.86
16.28	2.07	11.70	8.89	103.96	3.17	0.07	0.84
16.30	2.03	11.40	9.35	106.50	3.21	0.07	0.81
16.32	2.01	11.28	9.54	107.60	3.22	0.07	0.81
16.34	2.03	11.40	9.47	107.95	3.22	0.07	0.81

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
16.36	2.07	11.59	9.29	107.65	3.20	0.07	0.83
16.38	2.07	11.63	9.15	106.44	3.19	0.07	0.83
16.40	2.03	11.31	9.24	104.54	3.20	0.07	0.81
16.42	1.94	10.74	9.58	102.84	3.22	0.07	0.77
16.44	1.82	9.94	10.24	101.84	3.27	0.07	0.71
16.46	1.73	9.31	10.81	100.64	3.31	0.06	0.66
16.48	1.64	8.74	11.32	98.88	3.34	0.06	0.62
16.50	1.57	8.26	11.67	96.47	3.36	0.06	0.59
16.52	1.49	7.72	12.09	93.31	3.39	0.06	0.55
16.54	1.42	7.29	12.29	89.64	3.40	0.06	0.52
16.56	1.39	7.07	12.00	84.91	3.38	0.06	0.51
16.58	1.38	7.01	11.37	79.72	3.34	0.06	0.50
16.60	1.37	6.89	10.72	73.91	3.30	0.06	0.49
16.62	1.33	6.68	10.33	69.06	3.27	0.06	0.48
16.64	1.28	6.33	10.29	65.08	3.27	0.06	0.45
16.66	1.23	5.98	10.35	61.90	3.28	0.06	0.43
16.68	1.17	5.61	10.55	59.15	3.29	0.06	0.40
16.70	1.14	5.41	10.55	57.01	3.29	0.06	0.39
16.72	1.13	5.34	10.45	55.82	3.28	0.06	0.38
16.74	1.15	5.47	10.01	54.73	3.25	0.06	0.39
16.76	1.16	5.52	9.72	53.69	3.23	0.06	0.39
16.78	1.19	5.70	9.08	51.74	3.19	0.06	0.41
16.80	1.22	5.87	8.58	50.38	3.15	0.06	0.42
16.82	1.26	6.11	8.05	49.19	3.11	0.06	0.44
16.84	1.27	6.17	7.98	49.21	3.10	0.06	0.44
16.86	1.26	6.10	8.05	49.15	3.11	0.06	0.44
16.88	1.25	6.04	8.17	49.39	3.12	0.06	0.43
16.90	1.24	5.98	8.30	49.62	3.13	0.06	0.43
16.92	1.25	6.01	8.25	49.55	3.13	0.06	0.43
16.94	1.25	6.03	8.18	49.32	3.12	0.06	0.43
16.96	1.27	6.13	8.00	49.03	3.11	0.06	0.44
16.98	1.30	6.30	7.74	48.75	3.08	0.06	0.45
17.00	1.35	6.62	7.28	48.22	3.05	0.06	0.47
17.02	1.44	7.18	6.63	47.59	2.99	0.06	0.51
17.04	1.52	7.70	6.16	47.43	2.95	0.06	0.55
17.06	1.58	8.07	5.94	47.96	2.92	0.07	0.58
17.08	1.57	7.99	6.18	49.37	2.95	0.06	0.57
17.10	1.52	7.64	6.68	51.02	2.99	0.06	0.55
17.12	1.44	7.18	7.31	52.49	3.05	0.06	0.51
17.14	1.36	6.65	8.14	54.08	3.12	0.06	0.47
17.16	1.30	6.27	8.74	54.77	3.16	0.06	0.45
17.18	1.23	5.83	9.36	54.53	3.21	0.06	0.42
17.20	1.19	5.55	9.63	53.50	3.23	0.06	0.40
17.22	1.14	5.24	9.98	52.25	3.25	0.06	0.37
17.24	1.12	5.09	10.00	50.84	3.25	0.06	0.36
17.26	1.14	5.19	9.38	48.70	3.21	0.06	0.37
17.28	1.21	5.65	8.23	46.45	3.12	0.06	0.40
17.30	1.31	6.25	7.14	44.63	3.03	0.06	0.45

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
17.32	1.38	6.71	6.62	44.43	2.99	0.06	0.48
17.34	1.41	6.88	6.62	45.57	2.99	0.06	0.49
17.36	1.41	6.84	6.93	47.47	3.02	0.06	0.49
17.38	1.40	6.76	7.19	48.59	3.04	0.06	0.48
17.44	1.39	6.69	7.32	48.92	3.05	0.06	0.48
17.44	1.42	6.92	7.14	49.39	3.03	0.06	0.49
17.44	1.50	7.39	6.79	50.20	3.00	0.06	0.53
17.46	1.58	7.89	6.45	50.92	2.97	0.06	0.56
17.48	1.63	8.21	6.22	51.06	2.95	0.06	0.59
17.50	1.62	8.08	6.38	51.53	2.97	0.06	0.58
17.52	1.54	7.63	7.03	53.60	3.03	0.06	0.54
17.54	1.45	7.06	7.78	54.97	3.09	0.06	0.50
17.56	1.37	6.53	8.55	55.85	3.15	0.06	0.47
17.58	1.31	6.17	8.97	55.34	3.18	0.06	0.44
17.63	1.26	5.85	9.45	55.25	3.21	0.06	0.42
17.63	1.20	5.43	9.98	54.23	3.25	0.06	0.39
17.64	1.15	5.16	10.16	52.45	3.26	0.06	0.37
17.66	1.11	4.92	10.07	49.60	3.26	0.06	0.35
17.68	1.13	5.00	9.42	47.09	3.21	0.06	0.36
17.70	1.13	4.98	9.03	44.91	3.18	0.06	0.36
17.72	1.12	4.97	8.78	43.62	3.17	0.06	0.35
17.74	1.12	4.95	8.53	42.26	3.15	0.06	0.35
17.76	1.14	5.03	8.18	41.13	3.12	0.06	0.36
17.78	1.24	5.63	7.18	40.39	3.04	0.06	0.40
17.80	1.28	5.89	7.05	41.49	3.03	0.06	0.42
17.82	1.29	5.96	7.15	42.63	3.04	0.06	0.43
17.84	1.20	5.40	8.00	43.15	3.11	0.06	0.39
17.86	1.16	5.15	8.20	42.21	3.12	0.06	0.37
17.88	1.14	5.03	8.23	41.37	3.12	0.06	0.36
17.90	1.14	5.02	8.17	41.00	3.12	0.06	0.36
17.95	1.14	5.02	8.17	41.01	3.12	0.06	0.36
17.95	1.19	5.29	7.69	40.68	3.08	0.06	0.38
17.96	1.26	5.71	7.07	40.32	3.03	0.06	0.41
17.98	1.33	6.11	6.56	40.09	2.98	0.06	0.44
18.00	1.37	6.37	6.44	41.02	2.97	0.06	0.45
18.02	1.40	6.57	6.42	42.15	2.97	0.06	0.47
18.04	1.55	7.48	5.81	43.48	2.91	0.06	0.53
18.06	1.77	8.75	5.03	44.02	2.83	0.07	0.62
18.08	2.02	10.44	4.23	44.18	2.73	0.07	0.74
18.10	2.22	11.70	3.93	46.04	2.69	0.08	0.82
18.12	2.30	12.19	4.07	49.58	2.71	0.08	0.86
18.14	2.25	11.64	4.66	54.29	2.79	0.08	0.83
18.16	2.06	10.47	5.56	58.20	2.89	0.07	0.75
18.18	1.86	9.27	6.71	62.22	3.00	0.07	0.66
18.20	1.72	8.38	7.74	64.92	3.09	0.06	0.60
18.22	1.68	8.13	8.21	66.74	3.12	0.06	0.58
18.24	1.63	7.83	8.52	66.74	3.15	0.06	0.56
18.26	1.56	7.42	8.91	66.07	3.18	0.06	0.53

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
18.28	1.45	6.72	9.51	63.89	3.22	0.06	0.48
18.30	1.38	6.31	9.52	60.03	3.22	0.06	0.45
18.32	1.35	6.12	9.17	56.09	3.19	0.06	0.44
18.34	1.33	5.99	8.83	52.88	3.17	0.06	0.43
18.36	1.32	5.96	8.67	51.70	3.16	0.06	0.43
18.38	1.32	5.91	8.55	50.56	3.15	0.06	0.42
18.40	1.31	5.88	8.35	49.13	3.13	0.06	0.42
18.42	1.33	5.95	7.87	46.88	3.10	0.06	0.43
18.44	1.38	6.26	7.21	45.14	3.04	0.06	0.45
18.46	1.44	6.59	6.82	44.94	3.01	0.06	0.47
18.48	1.44	6.64	6.94	46.05	3.02	0.06	0.47
18.50	1.40	6.38	7.37	47.05	3.05	0.06	0.46
18.52	1.33	5.96	7.91	47.12	3.10	0.06	0.43
18.54	1.29	5.73	8.15	46.72	3.12	0.06	0.41
18.56	1.33	5.93	7.81	46.29	3.09	0.06	0.42
18.58	1.41	6.39	7.25	46.30	3.04	0.06	0.46
18.60	1.45	6.64	7.14	47.40	3.03	0.06	0.47
18.62	1.41	6.36	7.63	48.49	3.08	0.06	0.45
18.64	1.34	5.96	8.14	48.49	3.12	0.06	0.43
18.66	1.29	5.69	8.36	47.56	3.13	0.06	0.41
18.68	1.30	5.74	8.16	46.83	3.12	0.06	0.41
18.70	1.34	5.93	7.98	47.33	3.10	0.06	0.42
18.72	1.42	6.42	7.51	48.18	3.07	0.06	0.46
18.74	1.48	6.74	7.08	47.77	3.03	0.06	0.48
18.76	1.45	6.55	7.79	51.01	3.09	0.06	0.47
18.78	1.51	6.92	8.23	56.94	3.12	0.06	0.49
18.80	1.51	6.89	9.06	62.49	3.19	0.06	0.49
18.82	1.54	7.05	9.06	63.81	3.19	0.06	0.50
18.84	1.43	6.40	9.60	61.41	3.22	0.06	0.46
18.86	1.44	6.46	9.14	59.09	3.19	0.06	0.46
18.89	1.51	6.86	8.43	57.82	3.14	0.06	0.49
18.90	1.61	7.48	7.57	56.63	3.07	0.06	0.53
18.92	1.73	8.12	6.80	55.23	3.01	0.06	0.58
18.94	1.89	9.10	5.88	53.50	2.92	0.07	0.65
18.96	2.13	10.46	4.98	52.05	2.82	0.07	0.75
18.98	2.39	12.06	4.33	52.24	2.74	0.08	0.85
19.00	2.57	13.18	4.16	54.89	2.72	0.08	0.93
19.02	2.63	13.45	4.35	58.47	2.75	0.08	0.95
19.04	2.51	12.63	5.06	63.93	2.83	0.08	0.90
19.07	2.33	11.56	5.92	68.46	2.92	0.07	0.83
19.08	2.13	10.36	6.97	72.23	3.02	0.07	0.74
19.10	2.00	9.62	7.62	73.29	3.08	0.07	0.69
19.13	1.90	9.01	8.14	73.39	3.12	0.07	0.64
19.14	1.80	8.46	8.55	72.31	3.15	0.06	0.60
19.16	1.72	7.96	8.90	70.78	3.17	0.06	0.57
19.18	1.67	7.69	8.88	68.26	3.17	0.06	0.55
19.20	1.73	8.03	8.20	65.85	3.12	0.06	0.57
19.22	1.91	9.05	6.96	62.97	3.02	0.06	0.65

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
19.24	2.12	10.25	5.96	61.09	2.93	0.07	0.73
19.26	2.29	11.20	5.50	61.56	2.88	0.07	0.80
19.28	2.47	12.24	5.16	63.19	2.84	0.08	0.87
19.31	2.55	12.68	5.19	65.78	2.85	0.08	0.91
19.32	2.50	12.36	5.61	69.32	2.89	0.08	0.88
19.34	2.22	10.75	6.78	72.92	3.00	0.07	0.77
19.36	1.97	9.32	7.97	74.34	3.10	0.07	0.67
19.38	1.90	8.90	8.24	73.36	3.12	0.06	0.64
19.40	2.07	9.85	7.30	71.90	3.05	0.07	0.70
19.42	2.38	11.63	6.08	70.65	2.94	0.07	0.83
19.44	2.67	13.26	5.29	70.09	2.86	0.08	0.95
19.46	2.85	14.28	4.98	71.19	2.82	0.08	1.02
19.48	2.90	14.51	5.05	73.21	2.83	0.08	1.04
19.50	2.77	13.77	5.43	74.80	2.87	0.08	0.98
19.52	2.48	12.13	6.19	75.12	2.95	0.07	0.87
19.54	2.08	9.85	7.59	74.72	3.07	0.07	0.70
19.56	1.73	7.86	9.23	72.52	3.20	0.06	0.56
19.58	1.53	6.68	10.46	69.81	3.28	0.06	0.48
19.60	1.47	6.36	10.58	67.28	3.29	0.06	0.45
19.62	1.51	6.54	10.13	66.27	3.26	0.06	0.47
19.64	1.54	6.71	9.69	64.95	3.23	0.06	0.48
19.66	1.56	6.82	9.19	62.65	3.20	0.06	0.49
19.68	1.60	7.05	8.40	59.23	3.14	0.06	0.50
19.70	1.74	7.83	7.15	55.98	3.04	0.06	0.56
19.72	1.89	8.69	6.11	53.07	2.94	0.07	0.62
19.74	2.01	9.35	5.51	51.57	2.88	0.07	0.67
19.76	1.88	8.60	6.15	52.86	2.94	0.07	0.61

Abbreviations

q_t:	Total cone resistance
K_c:	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c:	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

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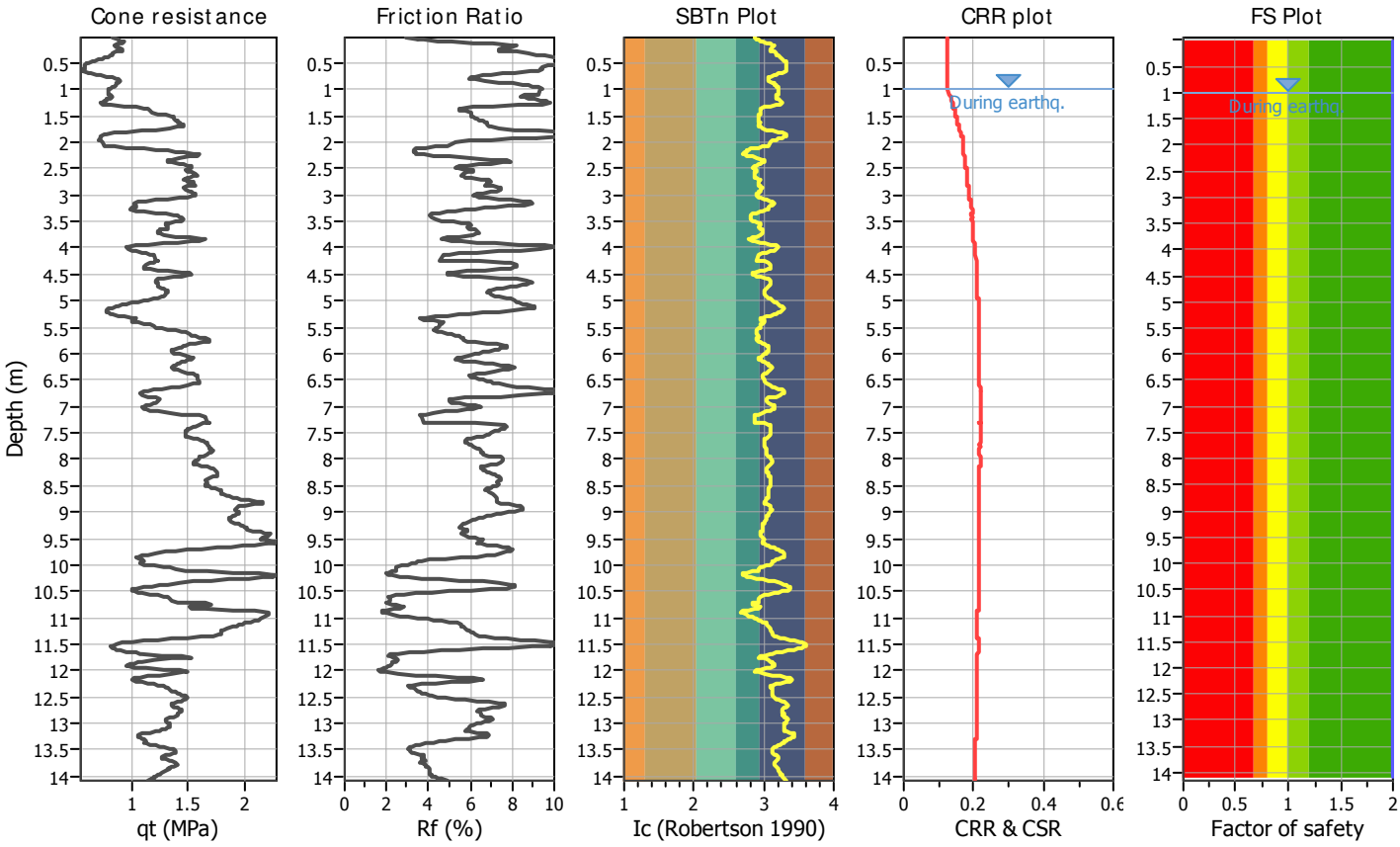
LIQUEFACTION ANALYSIS REPORT

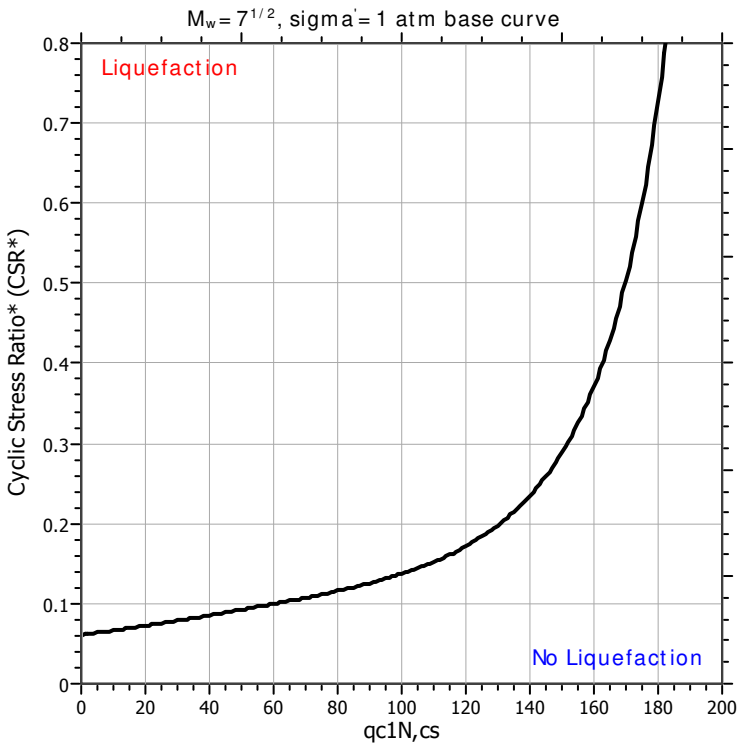
Project title : Location :

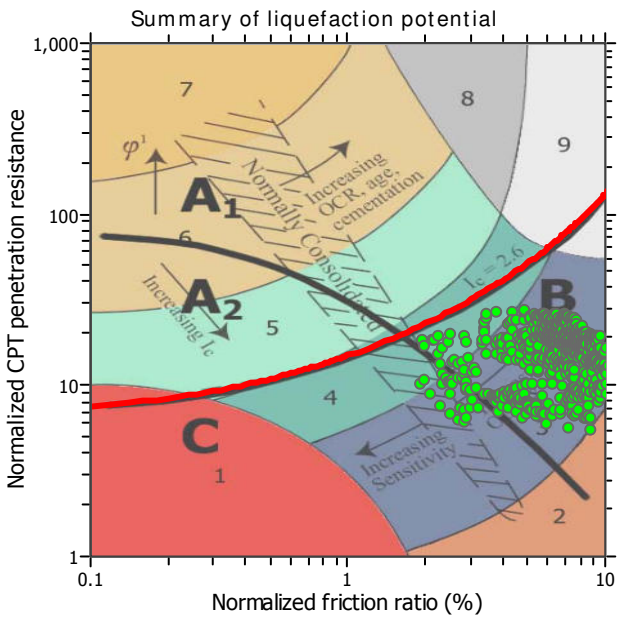
CPT file : CPTu-04_Biancolina

Input parameters and analysis data

Analysis method:	B&I (2014)	G.W.T. (in-situ):	2.20 m	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.00 m	Fill height:	N/A	Limit depth applied:	No
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	N/A
Earthquake magnitude M_w:	6.14	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.23	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		

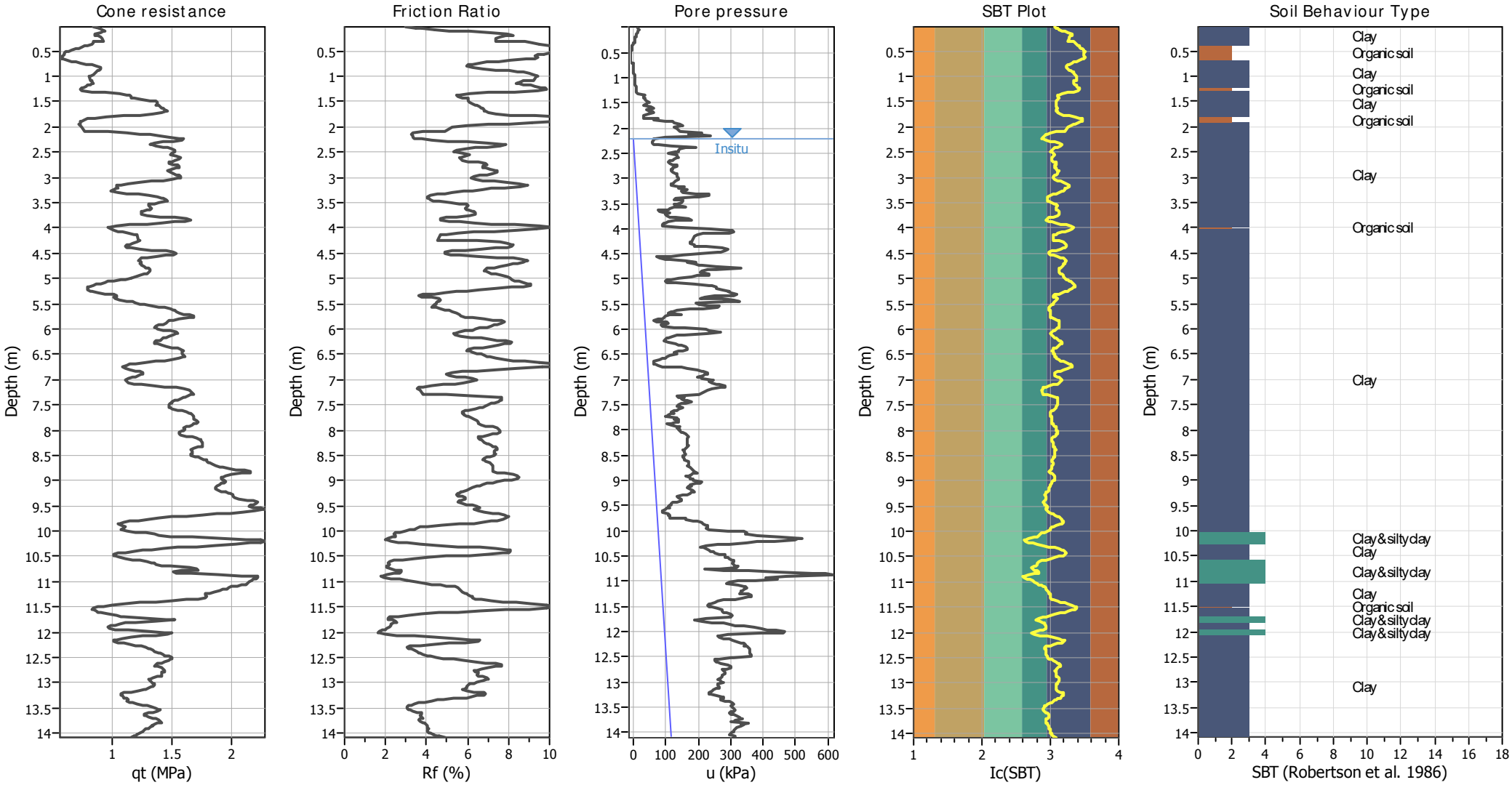






Zone A_1: Cyclic liquefaction likely depending on size and duration of cyclic loading
Zone A_2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



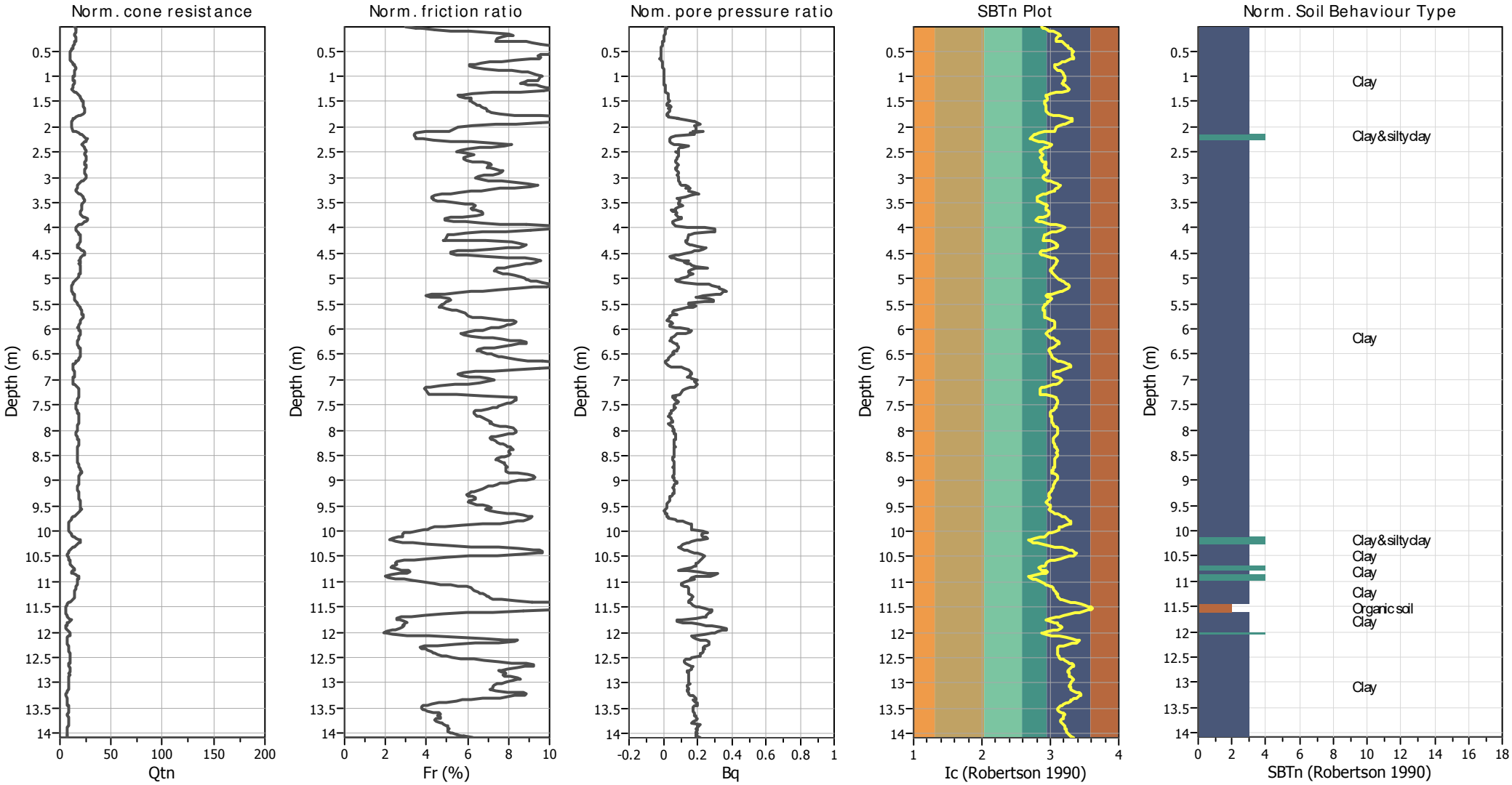
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	1.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.23	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.20 m	Fill height:	N/A	Limit depth:	N/A

SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

CPT basic interpretation plots (normalized)



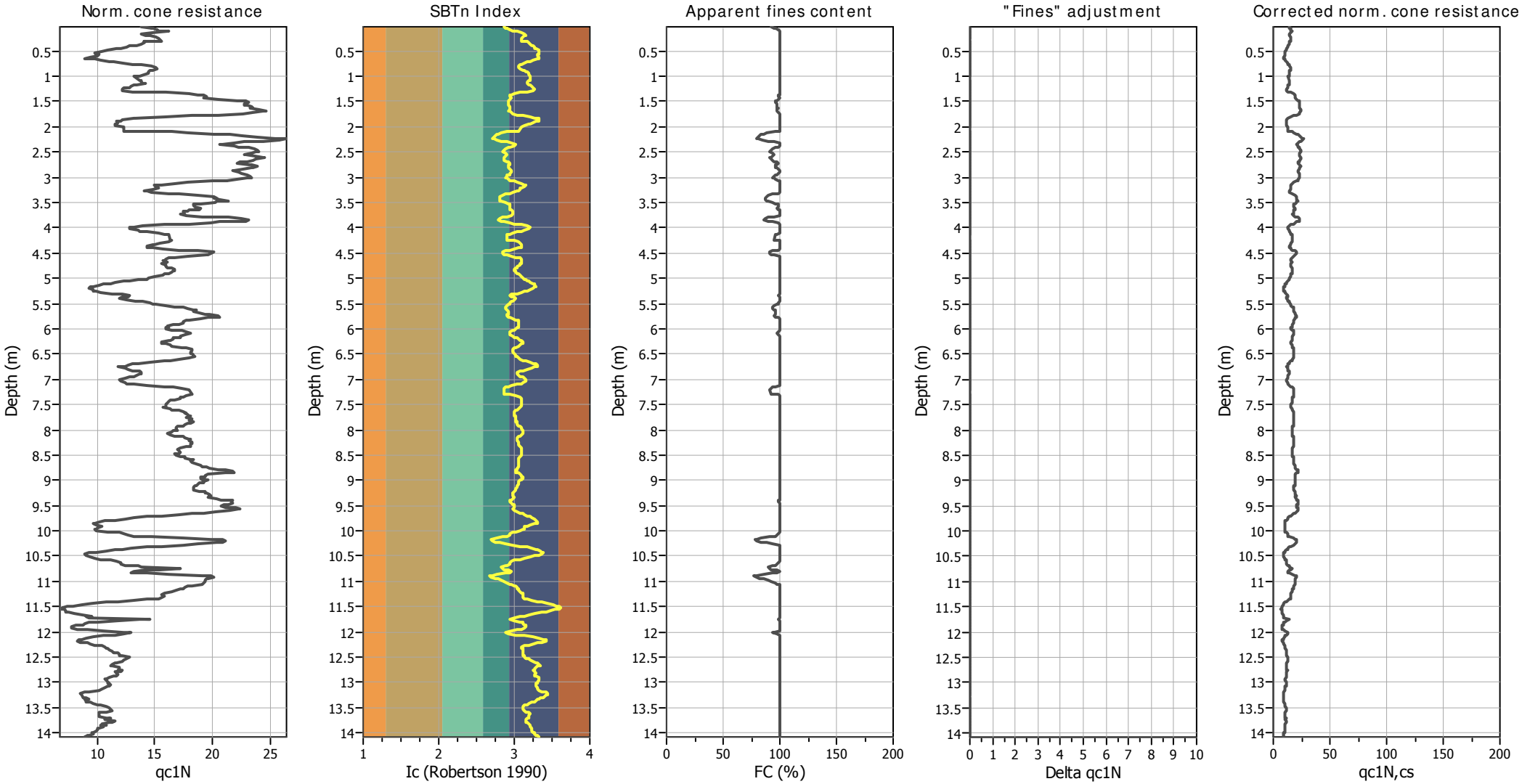
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	1.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.23	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.20 m	Fill height:	N/A	Limit depth:	N/A

SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

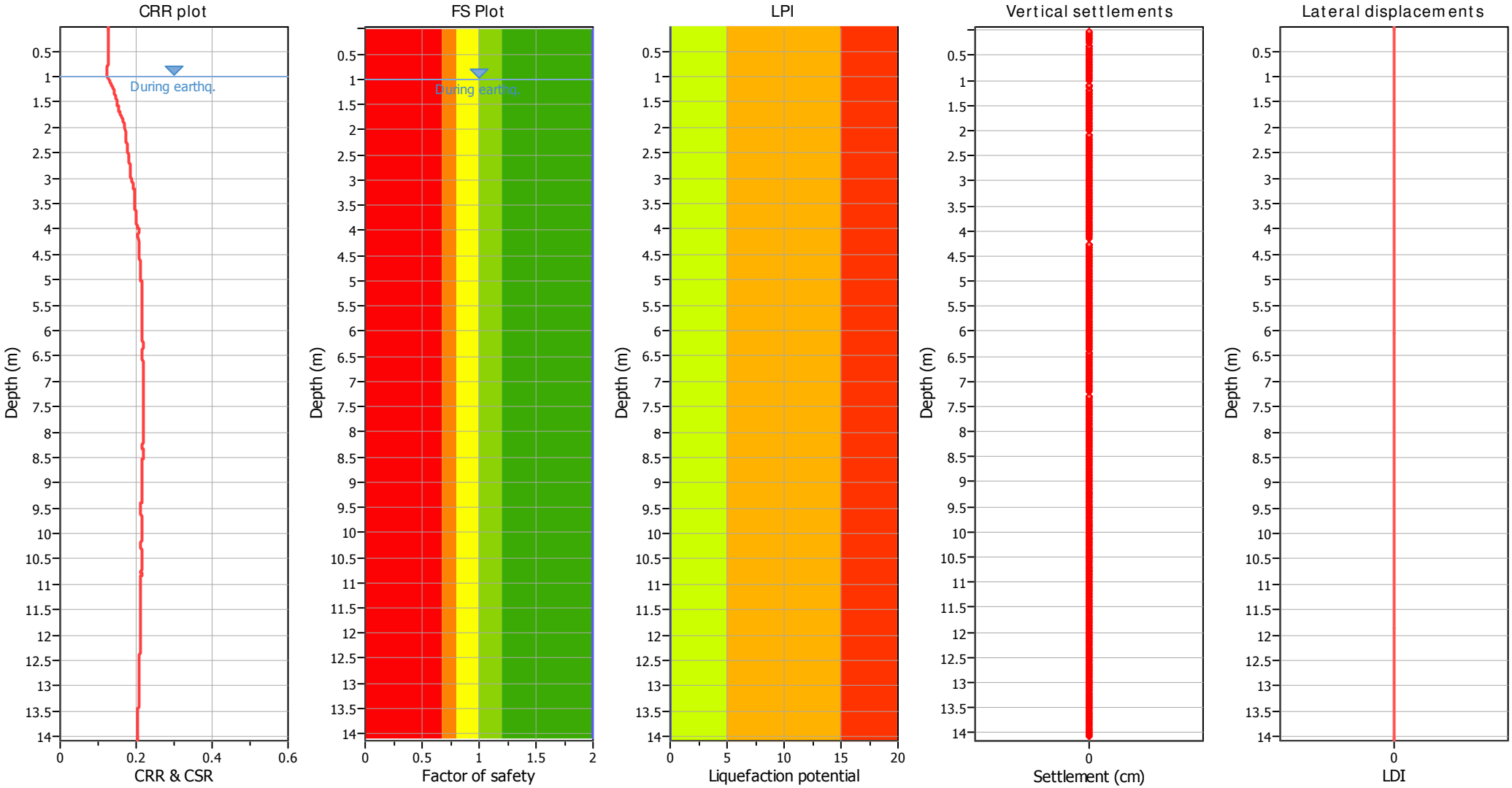
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	1.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.23	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.20 m	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	1.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.23	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.20 m	Fill height:	N/A	Limit depth:	N/A

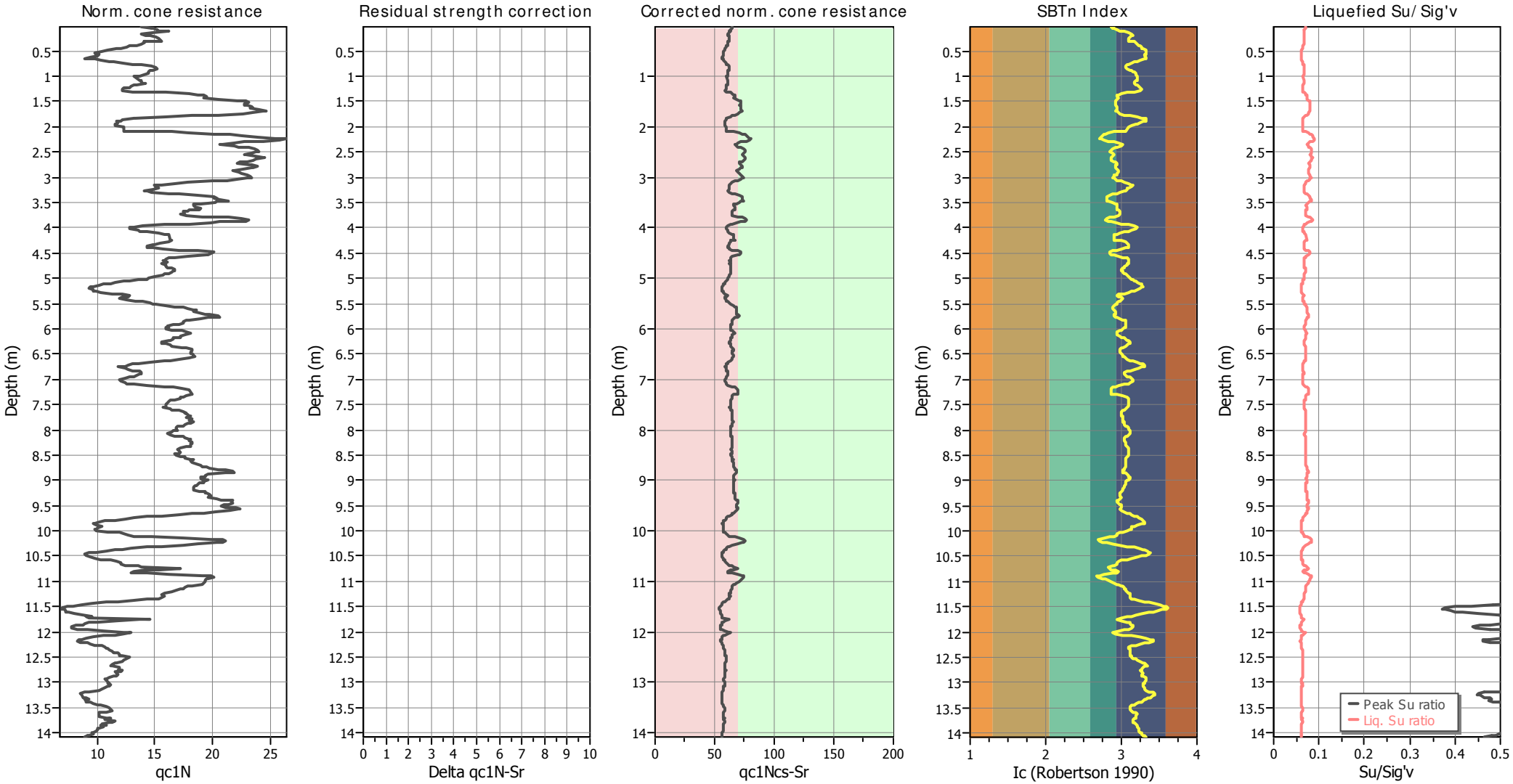
F.S. color scheme

- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

LPI color scheme

- Very high risk
- High risk
- Low risk

Check for strength loss plots (Idriss & Boulanger (2008))



Input parameters and analysis data

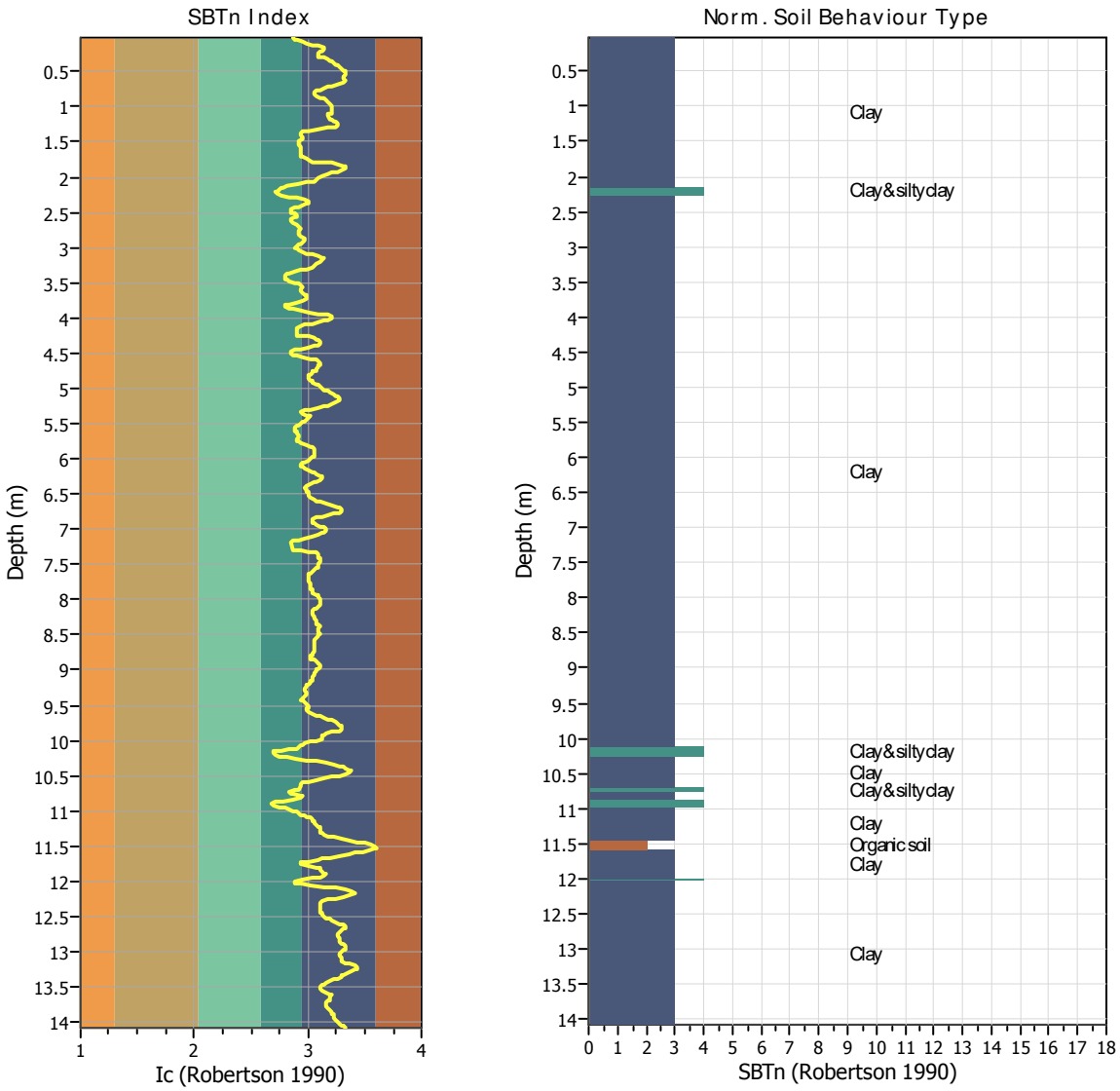
Analysis method:	B&I (2014)	Depth to GWT (erthq.):	1.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.23	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.20 m	Fill height:	N/A	Limit depth:	N/A

TRANSITION LAYER DETECTION ALGORITHM REPORT
Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vise-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between $1.80 < I_c < 3.0$) and a rate of change of I_c. Transitions typically occur when the rate of change of I_c is fast (i.e. delta I_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties		General statistics	
I_c minimum check value:	1.70	Total points in CPT file:	700
I_c maximum check value:	3.00	Total points excluded:	0
I_c change ratio value:	0.0100	Exclusion percentage:	0.00%
Minimum number of points in layer:	4	Number of layers detected:	0

:: Field input data ::

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
1	0.02	0.82	22.33	13.78	49.92	16.62
2	0.04	0.88	29.90	16.68	51.59	16.88
3	0.06	0.88	32.52	17.17	52.69	16.99
4	0.08	0.90	38.35	14.46	55.09	17.19
5	0.10	0.92	48.64	11.08	57.29	17.41
6	0.12	0.96	56.33	10.83	60.77	17.60
7	0.14	0.89	64.34	9.35	64.64	17.72
8	0.16	0.82	69.53	9.23	68.16	17.78
9	0.18	0.85	70.17	6.40	69.06	17.81
10	0.20	0.87	69.60	5.23	67.51	17.81
11	0.22	0.90	67.13	4.74	66.14	17.80
12	0.24	0.91	67.39	3.88	65.07	17.80
13	0.30	0.93	68.16	3.51	64.79	17.81
14	0.30	0.93	68.16	3.51	66.44	17.82
15	0.30	0.84	71.76	-0.37	68.48	17.84
16	0.32	0.84	73.82	-1.35	70.91	17.87
17	0.34	0.84	75.68	-2.65	71.97	17.90
18	0.36	0.82	78.63	-4.12	73.42	17.92
19	0.38	0.80	79.56	-5.05	75.33	17.93
20	0.40	0.76	79.08	-5.91	76.74	17.91
21	0.42	0.75	76.71	-6.83	78.16	17.87
22	0.44	0.72	75.08	-7.08	79.12	17.82
23	0.46	0.69	72.68	-6.77	80.90	17.78
24	0.48	0.65	71.02	-7.69	82.73	17.72
25	0.50	0.62	68.62	-8.25	83.56	17.65
26	0.52	0.62	62.31	-8.55	83.99	17.57
27	0.54	0.59	59.46	-8.43	83.27	17.50
28	0.56	0.59	57.47	-8.00	82.85	17.45
29	0.58	0.60	56.03	-8.80	81.92	17.42
30	0.60	0.59	54.53	-8.86	82.22	17.37
31	0.62	0.56	52.13	-9.05	83.76	17.33
32	0.64	0.53	51.55	-9.42	83.66	17.30
33	0.66	0.58	51.14	-8.92	81.69	17.30
34	0.68	0.61	50.34	-7.88	77.57	17.30
35	0.70	0.66	48.61	-4.62	74.36	17.30
36	0.72	0.68	47.65	-0.68	71.25	17.30
37	0.74	0.73	48.16	-0.86	68.50	17.32
38	0.76	0.78	48.23	-1.05	65.87	17.36
39	0.78	0.83	49.35	-0.98	63.55	17.41
40	0.80	0.88	51.33	-1.72	62.41	17.47
41	0.82	0.90	54.76	-2.34	62.43	17.56
42	0.84	0.91	60.38	0.06	64.02	17.66
43	0.87	0.88	65.47	0.37	66.29	17.75
44	0.88	0.87	70.47	0.74	68.44	17.82
45	0.90	0.86	73.06	1.05	69.93	17.87
46	0.92	0.86	75.95	1.66	70.77	17.90
47	0.94	0.86	76.72	2.15	71.67	17.92
48	0.96	0.84	77.39	2.34	72.70	17.92

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
49	0.99	0.81	76.91	2.46	74.08	17.90
50	1.00	0.79	76.07	2.95	74.19	17.88
51	1.09	0.82	73.79	3.51	73.89	17.87
52	1.09	0.82	73.79	3.51	72.88	17.86
53	1.09	0.82	73.44	3.57	72.70	17.86
54	1.09	0.82	73.44	3.57	72.03	17.83
55	1.11	0.82	68.40	5.42	71.59	17.81
56	1.13	0.83	69.93	6.09	70.90	17.80
57	1.14	0.84	70.41	6.28	71.55	17.81
58	1.17	0.80	71.31	6.40	72.47	17.81
59	1.18	0.79	71.24	6.71	74.22	17.81
60	1.20	0.77	72.26	7.14	75.21	17.81
61	1.22	0.77	72.84	7.57	76.65	17.81
62	1.24	0.73	72.80	7.69	77.59	17.80
63	1.26	0.72	71.71	8.12	78.36	17.78
64	1.28	0.72	70.55	8.25	76.75	17.76
65	1.30	0.78	68.08	9.17	71.26	17.77
66	1.32	0.95	65.96	13.42	64.33	17.78
67	1.34	1.07	64.16	34.71	58.76	17.79
68	1.36	1.11	62.04	32.00	55.78	17.79
69	1.38	1.15	61.40	31.57	54.63	17.79
70	1.40	1.16	63.41	31.51	54.67	17.82
71	1.42	1.15	66.58	33.85	55.58	17.88
72	1.44	1.15	70.94	34.03	55.98	17.95
73	1.46	1.22	75.20	41.17	55.06	18.03
74	1.48	1.32	78.40	48.31	53.75	18.11
75	1.50	1.36	82.78	45.60	52.98	18.18
76	1.52	1.38	84.96	40.00	53.19	18.21
77	1.54	1.35	84.86	33.05	53.58	18.22
78	1.56	1.35	86.17	32.92	53.98	18.24
79	1.58	1.37	89.37	54.34	54.05	18.28
80	1.60	1.40	92.18	60.31	54.11	18.32
81	1.62	1.40	94.04	51.32	54.39	18.34
82	1.64	1.39	95.73	40.37	54.46	18.37
83	1.66	1.43	98.07	48.31	54.26	18.40
84	1.68	1.47	99.99	58.46	53.97	18.43
85	1.70	1.46	101.26	60.31	54.36	18.43
86	1.72	1.40	98.98	46.22	55.33	18.41
87	1.74	1.35	96.80	31.26	57.63	18.38
88	1.78	1.22	99.26	29.60	61.43	18.36
89	1.78	1.09	102.08	29.85	66.99	18.33
90	1.80	0.95	102.55	30.34	73.41	18.27
91	1.82	0.79	95.80	73.97	78.58	18.21
92	1.84	0.79	97.73	60.68	82.57	18.14
93	1.86	0.72	94.36	96.80	83.29	18.10
94	1.88	0.71	86.70	120.25	83.02	17.99
95	1.90	0.70	75.33	127.02	80.40	17.85
96	1.92	0.70	65.75	141.29	77.47	17.69

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
97	1.94	0.70	58.22	150.28	74.48	17.53
98	1.96	0.69	49.95	147.08	71.81	17.37
99	1.98	0.68	42.64	124.98	67.97	17.20
100	2.00	0.73	37.35	136.37	64.92	17.09
101	2.08	0.73	37.03	141.23	62.99	17.04
102	2.08	0.73	37.03	141.23	62.87	17.04
103	2.08	0.73	37.03	141.23	57.86	17.06
104	2.10	0.98	35.62	212.49	52.78	17.12
105	2.12	1.07	37.51	170.89	47.30	17.20
106	2.14	1.20	39.75	193.78	45.16	17.32
107	2.16	1.28	43.56	236.49	43.74	17.43
108	2.18	1.35	46.44	97.85	42.70	17.52
109	2.20	1.45	47.69	68.98	41.90	17.61
110	2.22	1.55	53.23	64.55	41.04	17.72
111	2.24	1.62	57.72	61.29	41.93	17.87
112	2.26	1.59	67.97	57.05	44.19	18.00
113	2.28	1.50	75.85	57.66	48.08	18.13
114	2.30	1.39	83.98	58.89	52.25	18.23
115	2.32	1.35	95.13	62.15	56.35	18.33
116	2.34	1.28	102.43	77.35	59.22	18.41
117	2.36	1.26	107.01	114.95	59.45	18.44
118	2.38	1.35	103.23	193.91	57.98	18.44
119	2.40	1.38	99.32	161.97	55.29	18.41
120	2.42	1.44	93.64	143.88	53.07	18.35
121	2.44	1.48	86.59	137.23	51.02	18.30
122	2.46	1.50	84.22	138.52	49.44	18.24
123	2.48	1.51	79.38	129.72	48.89	18.21
124	2.50	1.50	80.24	108.49	49.19	18.21
125	2.52	1.47	84.75	128.12	50.77	18.26
126	2.54	1.44	92.53	132.06	52.03	18.31
127	2.56	1.45	92.79	135.57	52.03	18.33
128	2.58	1.50	88.52	136.55	50.65	18.32
129	2.60	1.56	87.49	133.23	49.45	18.32
130	2.62	1.57	89.09	124.68	49.29	18.32
131	2.64	1.52	88.28	121.85	49.67	18.30
132	2.66	1.50	85.72	110.77	50.44	18.29
133	2.68	1.47	88.28	109.17	51.79	18.32
134	2.70	1.44	96.83	112.12	53.64	18.38
135	2.72	1.42	102.62	121.97	54.49	18.45
136	2.74	1.49	104.73	134.09	54.34	18.49
137	2.76	1.51	106.17	136.31	53.40	18.51
138	2.78	1.55	104.89	122.52	53.12	18.51
139	2.81	1.53	104.44	122.95	53.00	18.51
140	2.82	1.52	104.86	116.68	53.70	18.51
141	2.84	1.47	105.91	116.25	54.89	18.51
142	2.86	1.42	108.41	117.85	56.08	18.52
143	2.88	1.42	108.64	121.66	56.47	18.53
144	2.90	1.46	109.72	129.29	56.07	18.54

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
145	2.92	1.48	110.62	132.43	55.15	18.55
146	2.94	1.51	107.80	132.25	54.08	18.52
147	2.96	1.52	101.52	134.52	52.75	18.48
148	2.98	1.54	97.67	137.91	51.69	18.44
149	3.00	1.55	95.81	138.89	51.26	18.41
150	3.02	1.52	95.04	137.72	51.70	18.39
151	3.04	1.47	94.62	131.45	53.03	18.39
152	3.06	1.41	96.86	129.97	55.06	18.38
153	3.08	1.32	96.95	126.40	58.26	18.36
154	3.10	1.17	97.17	121.29	61.70	18.32
155	3.12	1.10	95.63	117.54	65.32	18.28
156	3.14	1.03	93.80	117.85	67.68	18.24
157	3.16	0.98	92.61	139.69	68.74	18.20
158	3.18	0.99	88.99	157.11	67.86	18.15
159	3.20	1.02	81.87	137.05	65.66	18.06
160	3.22	1.01	73.35	166.40	63.83	17.96
161	3.24	0.99	67.55	152.98	63.15	17.84
162	3.26	0.93	61.97	149.48	62.34	17.73
163	3.28	0.95	55.94	151.20	60.78	17.64
164	3.30	0.98	53.70	190.65	57.48	17.61
165	3.32	1.09	55.20	231.26	54.67	17.64
166	3.34	1.15	55.62	230.77	51.31	17.67
167	3.36	1.26	53.73	202.22	48.45	17.69
168	3.38	1.37	54.49	187.02	46.65	17.73
169	3.40	1.39	58.34	129.05	46.31	17.77
170	3.42	1.37	58.78	126.09	46.45	17.81
171	3.44	1.41	59.33	149.97	46.17	17.85
172	3.46	1.47	62.98	151.02	46.71	17.90
173	3.48	1.40	67.30	148.43	48.01	17.97
174	3.50	1.39	71.44	134.34	50.67	18.03
175	3.52	1.30	75.82	124.25	52.94	18.07
176	3.54	1.27	78.58	139.38	54.85	18.10
177	3.56	1.26	78.96	158.95	55.30	18.11
178	3.58	1.28	78.03	126.58	54.79	18.11
179	3.60	1.32	78.38	110.40	54.26	18.11
180	3.63	1.31	77.84	108.25	54.69	18.10
181	3.64	1.25	77.74	75.45	55.56	18.09
182	3.66	1.24	77.96	82.22	56.81	18.09
183	3.68	1.22	79.34	100.55	57.21	18.09
184	3.70	1.21	78.67	110.28	57.37	18.10
185	3.72	1.23	78.67	99.63	57.61	18.10
186	3.74	1.20	79.98	101.42	57.32	18.10
187	3.76	1.24	78.37	110.89	55.85	18.10
188	3.78	1.34	77.12	129.66	51.96	18.10
189	3.80	1.52	73.89	170.34	48.28	18.12
190	3.82	1.60	74.66	177.72	45.95	18.15
191	3.84	1.65	78.54	127.88	45.64	18.19
192	3.86	1.63	79.72	106.52	47.66	18.24

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
193	3.88	1.47	87.09	100.43	50.43	18.26
194	3.90	1.41	88.92	93.23	54.55	18.28
195	3.92	1.27	90.84	90.46	58.97	18.29
196	3.94	1.12	96.41	88.74	65.06	18.29
197	3.96	0.99	99.45	89.60	70.79	18.29
198	3.98	0.93	100.64	144.49	73.98	18.26
199	4.00	0.91	95.86	235.26	74.13	18.23
200	4.02	0.91	92.95	295.38	71.86	18.18
201	4.04	0.96	86.22	304.25	68.70	18.10
202	4.07	0.98	75.87	309.78	64.77	18.00
203	4.08	1.02	68.33	294.71	60.65	17.88
204	4.10	1.10	61.06	214.83	57.03	17.79
205	4.12	1.14	57.95	196.37	54.22	17.72
206	4.14	1.17	55.64	186.22	52.65	17.70
207	4.26	1.19	55.61	179.69	51.91	17.69
208	4.26	1.19	55.61	179.69	51.72	17.69
209	4.26	1.19	55.77	176.49	51.77	17.69
210	4.26	1.19	55.77	176.49	54.99	17.90
211	4.26	1.20	88.92	174.15	58.30	18.09
212	4.28	1.18	91.90	173.66	62.12	18.26
213	4.30	1.13	93.95	175.82	63.87	18.26
214	4.32	1.09	93.63	188.06	65.16	18.25
215	4.34	1.08	91.06	188.98	65.82	18.23
216	4.36	1.05	90.00	225.11	65.81	18.20
217	4.38	1.05	88.94	273.60	64.94	18.18
218	4.40	1.09	86.06	290.15	62.67	18.16
219	4.42	1.16	82.02	293.17	59.01	18.14
220	4.44	1.27	78.49	284.43	54.71	18.11
221	4.46	1.39	74.10	267.26	50.64	18.10
222	4.48	1.51	73.56	259.88	48.67	18.10
223	4.50	1.49	74.64	205.60	48.54	18.12
224	4.52	1.46	77.01	152.92	49.66	18.15
225	4.54	1.46	80.34	116.49	52.12	18.19
226	4.56	1.34	87.04	71.82	55.82	18.26
227	4.58	1.25	96.97	81.17	60.25	18.33
228	4.60	1.21	101.90	98.03	63.39	18.39
229	4.62	1.20	106.93	112.80	64.96	18.43
230	4.64	1.19	109.72	158.95	65.74	18.46
231	4.66	1.18	110.00	192.92	65.53	18.46
232	4.68	1.21	107.54	167.26	65.06	18.45
233	4.70	1.20	104.23	189.85	64.57	18.41
234	4.72	1.18	101.41	202.40	63.98	18.38
235	4.74	1.20	98.62	212.74	63.16	18.35
236	4.76	1.21	96.28	255.14	61.74	18.32
237	4.78	1.22	91.97	330.65	60.67	18.30
238	4.80	1.25	91.78	255.45	59.45	18.28
239	4.82	1.28	89.38	230.40	58.95	18.27
240	4.84	1.27	89.25	209.66	58.84	18.27

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
241	4.86	1.27	90.37	206.34	59.25	18.27
242	4.88	1.26	90.66	206.65	59.87	18.28
243	4.90	1.24	92.48	231.75	60.72	18.29
244	4.92	1.22	94.21	232.37	61.81	18.30
245	4.94	1.20	94.47	195.69	63.40	18.30
246	4.96	1.15	95.62	179.88	65.00	18.29
247	4.98	1.11	93.06	138.28	66.44	18.26
248	5.01	1.10	91.45	115.20	67.66	18.21
249	5.02	1.04	86.23	101.05	68.92	18.15
250	5.04	0.99	82.96	99.02	70.76	18.08
251	5.06	0.95	81.58	101.91	72.84	18.04
252	5.08	0.89	80.81	130.83	74.57	18.01
253	5.10	0.87	80.23	190.15	76.50	17.99
254	5.12	0.81	79.01	233.35	77.94	17.95
255	5.14	0.79	76.74	240.18	79.28	17.88
256	5.16	0.75	69.50	253.78	79.63	17.79
257	5.18	0.73	64.08	257.29	78.86	17.67
258	5.20	0.72	57.25	254.52	76.59	17.56
259	5.22	0.74	51.87	275.26	73.87	17.45
260	5.24	0.75	48.28	294.77	70.99	17.37
261	5.26	0.77	45.08	291.94	68.58	17.31
262	5.28	0.80	43.48	300.06	64.77	17.27
263	5.30	0.88	41.10	317.60	60.53	17.24
264	5.32	0.95	38.51	309.78	56.35	17.19
265	5.34	1.01	36.07	249.85	54.65	17.17
266	5.36	1.00	38.19	220.18	55.65	17.22
267	5.38	0.95	43.06	208.06	58.20	17.31
268	5.40	0.94	46.78	274.83	59.73	17.41
269	5.42	0.99	49.73	309.60	59.02	17.49
270	5.44	1.06	51.49	328.86	57.48	17.56
271	5.46	1.11	52.96	286.34	56.05	17.61
272	5.48	1.16	53.67	193.35	55.27	17.64
273	5.50	1.18	54.53	199.88	54.63	17.67
274	5.52	1.20	55.56	232.12	53.54	17.70
275	5.54	1.28	56.75	266.09	52.34	17.75
276	5.56	1.34	59.44	259.14	51.18	17.82
277	5.58	1.41	62.68	216.06	51.10	17.91
278	5.60	1.44	69.60	175.20	51.34	18.00
279	5.62	1.48	74.05	134.28	51.79	18.08
280	5.64	1.50	76.04	119.94	52.45	18.15
281	5.66	1.49	81.33	116.31	52.96	18.20
282	5.68	1.53	85.11	109.05	53.31	18.28
283	5.70	1.58	90.14	149.23	53.13	18.33
284	5.72	1.61	92.25	114.03	52.64	18.39
285	5.74	1.68	94.78	96.31	52.37	18.42
286	5.76	1.69	97.31	95.38	53.07	18.46
287	5.78	1.61	102.40	90.58	54.87	18.50
288	5.80	1.56	105.99	73.91	57.71	18.52

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
289	5.82	1.47	109.38	63.69	59.96	18.55
290	5.84	1.45	112.65	69.91	61.81	18.57
291	5.86	1.44	115.53	101.91	62.34	18.58
292	5.88	1.44	113.00	108.00	62.45	18.55
293	5.90	1.40	105.41	89.23	62.31	18.49
294	5.92	1.36	100.02	85.48	62.76	18.42
295	5.94	1.32	98.52	89.05	62.75	18.37
296	5.97	1.33	94.19	124.12	62.34	18.32
297	5.98	1.32	87.52	155.14	61.22	18.28
298	6.00	1.32	87.39	223.45	60.32	18.26
299	6.02	1.36	88.80	231.75	58.90	18.28
300	6.04	1.45	89.44	263.02	57.04	18.28
301	6.06	1.48	83.89	267.14	55.22	18.26
302	6.08	1.51	82.58	226.46	54.25	18.23
303	6.10	1.51	81.68	157.91	54.27	18.21
304	6.12	1.47	79.08	134.52	55.17	18.20
305	6.14	1.44	83.02	122.71	56.70	18.23
306	6.16	1.44	89.65	105.54	58.91	18.30
307	6.18	1.39	96.41	102.40	60.74	18.36
308	6.20	1.39	99.10	98.46	62.51	18.41
309	6.22	1.37	103.27	93.91	63.77	18.45
310	6.24	1.36	108.10	93.17	65.61	18.49
311	6.26	1.31	111.27	108.98	66.77	18.51
312	6.28	1.31	109.96	129.91	66.76	18.51
313	6.30	1.35	107.46	138.83	65.53	18.49
314	6.32	1.38	105.28	146.77	64.11	18.48
315	6.34	1.40	103.64	159.88	62.34	18.46
316	6.36	1.47	100.28	164.98	60.42	18.44
317	6.38	1.51	96.91	167.38	58.19	18.42
318	6.41	1.56	93.58	163.45	57.07	18.40
319	6.42	1.55	94.15	154.34	56.59	18.40
320	6.44	1.56	95.82	140.49	57.16	18.42
321	6.46	1.55	98.64	127.02	57.81	18.45
322	6.48	1.55	101.61	128.62	58.47	18.48
323	6.50	1.56	104.72	132.12	59.01	18.52
324	6.52	1.57	109.33	111.38	59.41	18.56
325	6.54	1.58	111.00	102.89	59.78	18.59
326	6.56	1.59	113.14	97.85	60.46	18.60
327	6.58	1.55	114.55	90.65	61.96	18.61
328	6.60	1.47	116.67	81.48	64.15	18.61
329	6.62	1.41	116.86	63.88	66.52	18.61
330	6.64	1.37	118.46	60.25	69.66	18.61
331	6.66	1.26	123.23	61.11	73.31	18.60
332	6.68	1.17	123.17	64.12	77.31	18.60
333	6.70	1.12	124.45	66.58	79.85	18.58
334	6.72	1.10	122.84	77.11	81.15	18.55
335	6.74	1.07	118.23	91.20	80.96	18.46
336	6.76	1.02	99.06	148.43	79.00	18.36

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
337	6.78	1.07	94.58	164.31	75.37	18.23
338	6.81	1.11	84.20	197.60	71.51	18.15
339	6.82	1.13	76.96	212.74	67.28	18.05
340	6.84	1.19	68.88	217.17	64.05	17.95
341	6.87	1.21	64.62	227.88	61.65	17.88
342	6.88	1.21	61.93	228.86	60.72	17.82
343	6.90	1.20	59.85	220.31	60.90	17.80
344	6.92	1.18	62.16	214.58	62.05	17.82
345	6.94	1.15	64.98	198.22	64.01	17.86
346	6.96	1.13	68.73	206.22	66.29	17.91
347	6.98	1.09	71.26	212.43	68.52	17.93
348	7.00	1.05	72.25	242.77	69.93	17.94
349	7.02	1.05	71.74	244.43	70.13	17.93
350	7.04	1.06	68.76	231.69	68.85	17.90
351	7.06	1.09	65.62	244.18	67.27	17.86
352	7.08	1.10	63.83	256.80	64.58	17.81
353	7.10	1.17	59.24	265.11	61.10	17.77
354	7.12	1.27	55.94	283.75	56.51	17.74
355	7.15	1.41	54.82	282.95	52.87	17.74
356	7.16	1.48	54.41	270.46	50.50	17.77
357	7.18	1.55	56.46	243.88	49.46	17.82
358	7.20	1.61	60.30	226.52	49.29	17.90
359	7.30	1.64	65.21	202.15	49.61	17.96
360	7.30	1.64	65.21	202.15	49.97	18.00
361	7.30	1.63	66.26	196.68	54.60	18.26
362	7.32	1.59	117.31	134.03	59.28	18.49
363	7.34	1.58	121.25	136.86	63.75	18.68
364	7.36	1.55	123.20	155.08	64.36	18.69
365	7.38	1.56	120.96	145.91	64.86	18.68
366	7.40	1.51	118.65	154.83	65.24	18.64
367	7.42	1.47	114.90	164.49	65.65	18.61
368	7.44	1.47	112.62	179.02	65.77	18.57
369	7.46	1.45	109.67	161.23	65.50	18.54
370	7.48	1.46	106.21	146.46	65.33	18.51
371	7.50	1.44	103.84	139.88	64.95	18.48
372	7.52	1.45	100.92	134.40	64.57	18.45
373	7.54	1.45	98.20	138.40	64.38	18.42
374	7.56	1.43	98.23	150.71	63.62	18.40
375	7.58	1.48	95.34	139.08	62.68	18.39
376	7.60	1.51	93.00	132.37	60.96	18.37
377	7.62	1.56	92.04	125.85	59.71	18.37
378	7.64	1.60	92.81	116.74	58.82	18.39
379	7.66	1.62	94.70	123.63	58.63	18.41
380	7.68	1.62	95.94	115.08	58.62	18.43
381	7.70	1.64	96.42	107.45	58.65	18.45
382	7.72	1.66	98.95	102.95	58.84	18.48
383	7.74	1.66	103.41	99.57	59.23	18.50
384	7.76	1.63	100.97	133.11	59.56	18.52

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
385	7.78	1.68	106.39	126.83	60.09	18.55
386	7.80	1.66	111.48	140.18	60.21	18.60
387	7.83	1.70	111.67	139.26	60.53	18.62
388	7.84	1.69	112.80	128.92	60.38	18.62
389	7.86	1.68	111.38	115.75	60.68	18.61
390	7.88	1.66	109.37	104.06	61.12	18.60
391	7.90	1.64	110.45	115.14	61.76	18.60
392	7.93	1.62	112.02	134.58	63.08	18.62
393	7.94	1.57	117.11	142.03	64.34	18.64
394	7.96	1.57	119.58	135.20	65.46	18.67
395	7.98	1.57	120.76	143.51	65.66	18.68
396	8.00	1.58	121.15	136.92	65.96	18.68
397	8.02	1.55	120.79	144.92	66.17	18.67
398	8.04	1.54	118.81	145.72	66.60	18.65
399	8.06	1.51	114.93	150.34	66.52	18.62
400	8.08	1.51	112.65	159.45	65.99	18.59
401	8.10	1.53	109.44	166.52	64.87	18.57
402	8.12	1.57	107.68	170.09	63.26	18.56
403	8.14	1.65	108.48	169.23	62.15	18.58
404	8.16	1.66	110.37	166.58	61.42	18.61
405	8.18	1.70	113.63	167.69	61.34	18.64
406	8.20	1.71	115.39	164.37	61.43	18.66
407	8.22	1.70	117.22	164.86	61.65	18.68
408	8.24	1.72	119.68	165.11	61.86	18.70
409	8.26	1.73	121.03	164.92	62.18	18.72
410	8.28	1.71	123.40	165.42	62.62	18.75
411	8.30	1.72	126.89	167.26	63.04	18.76
412	8.32	1.73	127.11	171.32	63.46	18.77
413	8.34	1.69	126.24	165.29	64.22	18.76
414	8.36	1.64	125.67	159.69	65.09	18.74
415	8.38	1.62	123.77	158.03	65.60	18.72
416	8.40	1.62	121.21	154.22	65.44	18.71
417	8.43	1.64	120.92	156.92	65.17	18.70
418	8.44	1.64	121.66	156.98	65.03	18.71
419	8.46	1.64	121.75	155.14	65.43	18.71
420	8.48	1.61	122.01	160.25	65.68	18.70
421	8.50	1.62	121.04	157.42	65.47	18.70
422	8.52	1.65	119.63	153.29	64.48	18.69
423	8.54	1.69	118.48	153.91	63.71	18.69
424	8.56	1.69	118.38	155.45	62.74	18.69
425	8.58	1.75	117.99	155.02	62.26	18.71
426	8.60	1.77	120.97	157.35	62.15	18.73
427	8.62	1.75	124.53	168.68	62.50	18.76
428	8.64	1.77	126.23	171.51	63.00	18.78
429	8.66	1.77	129.65	171.94	62.94	18.81
430	8.68	1.80	130.90	170.28	62.81	18.83
431	8.70	1.84	134.27	168.06	62.56	18.87
432	8.72	1.86	138.27	167.51	62.33	18.90

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
433	8.74	1.89	140.22	174.71	62.02	18.92
434	8.76	1.92	140.49	181.05	61.46	18.96
435	8.78	2.00	148.21	179.32	60.70	19.00
436	8.80	2.07	151.93	182.52	59.94	19.05
437	8.82	2.13	156.35	190.28	59.48	19.09
438	8.84	2.14	160.26	197.85	60.01	19.12
439	8.86	2.06	162.09	184.00	61.97	19.12
440	8.88	1.92	165.26	180.00	64.10	19.12
441	8.90	1.90	164.52	171.45	65.48	19.11
442	8.92	1.91	162.15	160.25	65.85	19.10
443	8.94	1.87	162.98	173.17	66.08	19.09
444	8.96	1.87	162.27	175.94	66.13	19.08
445	8.98	1.88	157.66	182.83	65.10	19.06
446	9.00	1.93	150.86	183.88	64.12	19.02
447	9.02	1.90	146.89	208.62	63.06	18.97
448	9.05	1.90	138.94	206.65	62.77	18.92
449	9.06	1.87	133.90	191.14	62.16	18.86
450	9.08	1.85	126.37	173.05	61.90	18.81
451	9.10	1.85	123.97	179.32	61.51	18.77
452	9.12	1.83	119.67	171.32	61.26	18.73
453	9.14	1.82	116.40	164.37	60.79	18.70
454	9.16	1.83	112.62	175.75	60.44	18.67
455	9.18	1.83	112.75	176.00	59.60	18.66
456	9.21	1.88	109.99	185.42	58.67	18.65
457	9.22	1.93	108.97	186.22	57.86	18.65
458	9.24	1.93	111.56	179.38	57.43	18.66
459	9.26	1.95	111.27	176.80	57.14	18.66
460	9.28	1.97	108.80	164.80	56.63	18.66
461	9.30	1.99	109.31	152.43	56.77	18.67
462	9.32	1.98	114.76	135.69	57.55	18.71
463	9.34	1.97	120.37	137.17	57.94	18.76
464	9.36	2.04	121.81	148.18	57.56	18.78
465	9.38	2.08	121.71	149.11	56.02	18.80
466	9.40	2.19	120.27	149.23	55.27	18.81
467	9.42	2.18	123.76	133.35	54.82	18.83
468	9.44	2.20	125.88	121.17	55.64	18.86
469	9.47	2.16	129.88	115.63	56.56	18.88
470	9.48	2.12	132.96	114.28	57.85	18.91
471	9.50	2.10	137.35	110.40	58.77	18.95
472	9.53	2.14	144.75	107.94	58.75	19.00
473	9.54	2.24	147.47	113.60	57.96	19.03
474	9.56	2.28	145.20	101.23	57.15	19.03
475	9.58	2.26	142.76	97.54	57.20	19.01
476	9.60	2.19	140.23	88.25	58.60	18.99
477	9.62	2.07	143.72	90.65	60.78	18.97
478	9.64	1.96	142.92	88.43	63.57	18.96
479	9.66	1.85	143.94	108.37	65.96	18.92
480	9.68	1.74	136.99	111.82	68.67	18.86

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
481	9.70	1.59	130.07	108.37	71.34	18.76
482	9.72	1.46	119.72	110.89	74.22	18.65
483	9.74	1.36	110.49	110.83	76.15	18.52
484	9.76	1.28	99.04	159.02	77.96	18.39
485	9.79	1.18	91.83	160.00	79.38	18.24
486	9.80	1.10	80.29	181.97	80.75	18.10
487	9.82	1.05	72.76	197.17	81.46	17.96
488	9.85	1.00	67.38	211.02	80.97	17.83
489	9.86	1.00	58.92	216.06	78.70	17.69
490	9.88	1.02	50.18	223.08	74.40	17.54
491	9.90	1.07	44.28	227.75	70.32	17.40
492	9.92	1.08	40.15	226.58	68.25	17.30
493	9.94	1.04	38.64	226.95	67.80	17.22
494	9.96	1.02	36.21	226.09	67.85	17.14
495	9.98	1.01	33.71	233.05	66.97	17.09
496	10.00	1.03	33.74	292.37	64.18	17.06
497	10.02	1.13	31.98	341.23	60.31	17.06
498	10.04	1.23	31.70	348.00	56.77	17.06
499	10.06	1.28	31.83	343.32	55.01	17.11
500	10.08	1.32	34.62	351.26	54.26	17.18
501	10.11	1.37	36.35	382.28	52.68	17.29
502	10.12	1.53	39.55	450.95	48.51	17.38
503	10.14	1.82	39.11	519.57	43.81	17.47
504	10.16	2.06	41.00	504.86	40.52	17.57
505	10.18	2.18	45.58	496.49	40.00	17.72
506	10.20	2.20	53.15	433.35	41.17	17.85
507	10.22	2.17	58.15	383.08	43.28	17.98
508	10.24	2.12	64.52	350.58	46.71	18.10
509	10.26	1.96	75.36	294.28	51.10	18.21
510	10.28	1.83	82.98	259.75	57.35	18.34
511	10.30	1.64	96.63	223.94	63.48	18.42
512	10.32	1.51	101.83	206.22	70.26	18.47
513	10.34	1.36	107.05	214.52	75.33	18.48
514	10.36	1.28	106.38	224.18	79.54	18.45
515	10.38	1.21	102.85	232.31	82.07	18.39
516	10.40	1.14	95.80	237.66	84.44	18.29
517	10.42	1.05	87.60	246.52	86.71	18.18
518	10.44	0.98	81.06	252.18	88.21	18.05
519	10.46	0.95	72.41	266.09	87.15	17.89
520	10.48	0.95	59.24	280.18	84.08	17.72
521	10.50	0.95	51.49	282.46	78.89	17.52
522	10.52	1.00	42.16	284.18	73.84	17.35
523	10.54	1.04	36.52	290.03	68.47	17.18
524	10.56	1.09	32.68	294.65	63.41	17.07
525	10.58	1.18	29.63	305.97	59.10	16.98
526	10.60	1.23	27.49	307.32	55.78	16.93
527	10.62	1.28	27.75	308.74	54.47	16.93
528	10.64	1.29	28.84	303.88	54.45	16.97

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
529	10.66	1.28	30.25	308.00	54.34	17.00
530	10.70	1.33	29.80	311.63	52.79	17.02
531	10.70	1.44	29.13	321.05	50.90	17.05
532	10.72	1.48	30.79	319.08	48.04	17.21
533	10.75	1.83	39.83	264.31	48.85	17.39
534	10.76	1.64	45.09	218.77	50.11	17.51
535	10.78	1.51	42.40	279.02	53.87	17.49
536	10.80	1.41	41.79	354.09	55.52	17.45
537	10.82	1.39	41.89	432.86	54.39	17.42
538	10.84	1.53	38.97	550.22	50.50	17.41
539	10.86	1.74	37.37	591.45	44.75	17.42
540	10.88	2.05	38.36	614.58	40.99	17.45
541	10.90	2.13	38.01	469.42	39.43	17.52
542	10.92	2.15	42.04	413.97	40.54	17.62
543	10.94	2.10	49.25	406.52	42.82	17.79
544	10.96	2.09	58.06	445.11	45.52	17.95
545	10.98	2.08	66.27	378.40	47.74	18.10
546	11.00	2.09	72.58	320.62	50.21	18.24
547	11.02	2.06	84.50	296.74	52.49	18.37
548	11.06	2.06	93.15	287.51	54.23	18.45
549	11.06	2.06	93.15	287.51	56.22	18.53
550	11.08	1.97	105.00	321.60	57.96	18.58
551	11.10	1.92	106.32	342.65	60.19	18.63
552	11.12	1.90	110.54	344.18	61.09	18.64
553	11.14	1.89	109.97	351.32	61.62	18.64
554	11.16	1.87	106.86	341.85	62.09	18.62
555	11.18	1.82	106.92	337.60	62.82	18.61
556	11.20	1.79	106.53	332.98	64.07	18.59
557	11.23	1.73	106.27	332.12	65.05	18.58
558	11.24	1.72	106.21	329.17	65.93	18.58
559	11.26	1.70	107.74	355.14	66.22	18.60
560	11.28	1.72	110.27	365.05	66.44	18.62
561	11.30	1.73	111.93	365.05	66.69	18.63
562	11.32	1.70	111.35	353.29	67.24	18.62
563	11.34	1.67	109.40	334.15	68.70	18.60
564	11.36	1.57	108.08	312.98	71.49	18.56
565	11.38	1.43	107.44	279.69	75.86	18.52
566	11.40	1.30	106.02	261.42	80.93	18.46
567	11.42	1.19	102.98	248.98	86.81	18.40
568	11.44	1.05	100.54	237.48	93.06	18.34
569	11.46	0.95	99.16	232.06	100.00	18.27
570	11.48	0.87	95.18	230.22	100.00	18.19
571	11.50	0.82	89.99	231.20	100.00	18.10
572	11.52	0.78	81.60	240.31	100.00	17.99
573	11.54	0.75	74.42	258.09	100.00	17.86
574	11.56	0.79	65.70	271.63	100.00	17.73
575	11.58	0.81	56.25	274.95	97.42	17.57
576	11.60	0.81	47.82	274.46	91.99	17.39

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
577	11.62	0.84	40.10	279.57	86.22	17.23
578	11.64	0.90	36.03	288.80	79.13	17.10
579	11.66	0.98	31.93	301.78	72.28	16.99
580	11.68	1.05	27.90	306.52	67.84	16.84
581	11.70	1.00	23.44	296.92	64.46	16.68
582	11.72	1.04	20.94	300.68	58.38	16.87
583	11.74	1.62	36.40	223.75	54.81	17.08
584	11.76	1.53	35.98	194.65	54.45	17.26
585	11.78	1.30	34.19	189.23	58.95	17.14
586	11.80	1.12	30.09	208.62	63.56	16.97
587	11.82	1.04	26.05	240.18	65.95	16.80
588	11.84	1.00	23.84	278.22	66.53	16.68
589	11.87	0.98	22.91	294.71	67.70	16.61
590	11.88	0.91	22.40	312.12	69.22	16.54
591	11.90	0.87	21.02	341.17	70.14	16.47
592	11.92	0.87	19.74	373.66	68.69	16.43
593	11.94	0.93	19.58	394.52	65.54	16.45
594	11.96	1.03	21.15	414.34	61.02	16.55
595	11.98	1.19	22.82	440.06	55.54	16.66
596	12.00	1.38	22.98	467.32	51.47	16.75
597	12.02	1.45	24.55	460.55	50.68	16.86
598	12.04	1.39	28.24	396.18	53.90	17.00
599	12.06	1.30	34.10	290.46	60.04	17.18
600	12.08	1.19	41.02	266.03	68.04	17.38
601	12.10	1.09	51.41	260.92	76.19	17.55
602	12.12	1.02	58.49	265.05	83.51	17.69
603	12.14	0.97	64.80	276.86	88.56	17.78
604	12.16	0.94	67.88	295.08	91.38	17.82
605	12.18	0.93	66.60	306.46	90.98	17.80
606	12.20	0.97	62.27	317.97	87.31	17.75
607	12.22	1.04	56.12	332.00	82.12	17.65
608	12.24	1.07	48.81	341.78	76.94	17.53
609	12.26	1.11	44.49	343.94	71.71	17.40
610	12.28	1.19	37.73	341.60	67.81	17.31
611	12.30	1.21	37.76	350.46	65.59	17.29
612	12.32	1.23	40.48	356.25	65.66	17.34
613	12.34	1.24	42.72	356.92	66.18	17.42
614	12.36	1.26	45.64	358.58	66.30	17.48
615	12.38	1.29	47.11	360.62	66.64	17.55
616	12.40	1.29	50.41	359.20	66.40	17.61
617	12.42	1.35	52.04	357.78	66.52	17.67
618	12.44	1.35	54.09	360.80	66.64	17.73
619	12.46	1.36	58.19	363.14	67.27	17.80
620	12.48	1.39	61.75	365.23	67.34	17.88
621	12.51	1.46	64.99	310.15	68.22	17.97
622	12.52	1.43	72.42	302.28	69.69	18.07
623	12.54	1.43	79.59	265.78	72.20	18.16
624	12.56	1.41	83.95	251.38	74.36	18.24

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
625	12.58	1.40	90.68	251.57	77.08	18.31
626	12.60	1.34	96.67	256.18	79.75	18.37
627	12.62	1.33	101.96	258.22	82.42	18.42
628	12.64	1.30	105.83	270.40	83.78	18.45
629	12.66	1.29	103.97	291.69	84.17	18.44
630	12.68	1.30	101.63	298.71	82.44	18.42
631	12.70	1.37	98.27	301.48	80.66	18.41
632	12.72	1.37	97.43	299.38	78.91	18.36
633	12.75	1.35	88.85	285.97	78.05	18.34
634	12.76	1.41	91.77	275.26	77.43	18.31
635	12.78	1.39	91.57	277.66	78.03	18.33
636	12.80	1.34	92.57	282.52	78.94	18.33
637	12.82	1.35	93.18	283.75	79.31	18.32
638	12.84	1.36	91.09	280.43	78.94	18.32
639	12.86	1.36	90.64	274.52	79.29	18.31
640	12.88	1.33	92.66	273.78	80.82	18.32
641	12.90	1.28	94.33	271.94	82.75	18.32
642	12.92	1.25	92.53	268.49	84.13	18.30
643	12.94	1.23	89.93	261.60	84.01	18.27
644	12.96	1.26	87.66	262.95	83.01	18.24
645	12.98	1.28	86.44	271.14	81.68	18.22
646	13.01	1.28	83.81	273.91	80.99	18.20
647	13.02	1.28	82.59	277.91	80.04	18.17
648	13.04	1.31	80.44	261.23	79.78	18.16
649	13.06	1.29	80.50	259.63	79.67	18.14
650	13.08	1.27	78.97	258.77	80.26	18.11
651	13.10	1.24	76.21	263.38	80.93	18.08
652	13.12	1.21	75.05	264.49	81.14	18.04
653	13.14	1.22	71.79	253.48	81.53	18.01
654	13.16	1.19	70.92	247.94	83.64	17.99
655	13.18	1.09	74.03	240.74	87.38	17.98
656	13.20	1.04	74.76	231.45	91.79	17.98
657	13.23	1.00	73.96	234.34	93.28	17.96
658	13.24	1.02	71.91	236.62	93.13	17.93
659	13.26	1.02	70.63	253.29	91.34	17.89
660	13.29	1.03	65.63	273.97	88.54	17.82
661	13.30	1.07	58.77	278.03	84.89	17.73
662	13.32	1.09	53.39	280.00	82.70	17.63
663	13.34	1.05	51.30	266.95	81.27	17.55
664	13.36	1.07	47.39	268.86	80.48	17.48
665	13.38	1.06	44.28	283.51	77.89	17.40
666	13.40	1.11	41.95	297.17	75.43	17.35
667	13.42	1.14	40.73	303.94	72.67	17.33
668	13.44	1.19	40.34	309.78	70.56	17.32
669	13.46	1.22	39.70	302.52	68.63	17.33
670	13.48	1.27	40.09	300.55	67.23	17.36
671	13.50	1.31	42.33	303.14	66.42	17.41
672	13.52	1.33	43.58	310.34	66.48	17.46

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
673	13.54	1.32	45.03	311.38	66.57	17.48
674	13.56	1.34	45.09	311.63	67.76	17.52
675	13.58	1.29	48.13	308.31	69.94	17.55
676	13.60	1.21	49.80	300.55	72.39	17.56
677	13.62	1.20	48.04	296.86	73.31	17.53
678	13.64	1.21	45.61	302.22	72.81	17.49
679	13.66	1.21	45.64	307.63	72.86	17.51
680	13.68	1.21	49.64	317.35	72.64	17.57
681	13.70	1.28	52.02	327.38	71.70	17.63
682	13.72	1.33	52.31	331.88	70.44	17.61
683	13.74	1.27	46.09	336.86	69.32	17.62
684	13.76	1.38	52.46	312.55	69.44	17.64
685	13.78	1.36	54.83	308.31	70.05	17.71
686	13.80	1.32	54.93	300.68	71.43	17.68
687	13.82	1.25	50.06	354.28	72.33	17.68
688	13.85	1.29	55.15	331.14	73.46	17.67
689	13.86	1.23	54.80	339.69	73.56	17.69
690	13.88	1.27	52.23	329.72	74.36	17.66
691	13.90	1.22	52.52	317.78	74.70	17.64
692	13.92	1.20	52.84	317.78	75.50	17.63
693	13.94	1.21	51.14	315.20	75.71	17.61
694	13.96	1.19	50.12	309.97	76.03	17.59
695	13.98	1.17	50.66	307.08	77.12	17.58
696	14.00	1.15	51.11	305.54	77.90	17.59
697	14.02	1.16	51.30	299.69	79.15	17.61
698	14.04	1.13	53.93	296.49	80.25	17.62
699	14.06	1.11	53.99	301.05	81.57	17.64
700	14.08	1.08	57.19	311.75	83.96	17.68

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (m)
q_c:	Measured cone resistance (MPa)
f_s:	Sleeve friction resistance (kPa)
u:	Pore pressure (kPa)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (kN/m^3)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1	0.02	0.33	0.00	0.33	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
2	0.04	0.67	0.00	0.67	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
3	0.06	1.01	0.00	1.01	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
4	0.08	1.35	0.00	1.35	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
5	0.10	1.70	0.00	1.70	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
6	0.12	2.05	0.00	2.05	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
7	0.14	2.41	0.00	2.41	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
8	0.16	2.76	0.00	2.76	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
9	0.18	3.12	0.00	3.12	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
10	0.20	3.48	0.00	3.48	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
11	0.22	3.83	0.00	3.83	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
12	0.24	4.19	0.00	4.19	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
13	0.30	5.26	0.00	5.26	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
14	0.30	5.26	0.00	5.26	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
15	0.30	5.26	0.00	5.26	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
16	0.32	5.61	0.00	5.61	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
17	0.34	5.97	0.00	5.97	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
18	0.36	6.33	0.00	6.33	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
19	0.38	6.69	0.00	6.69	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
20	0.40	7.05	0.00	7.05	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
21	0.42	7.40	0.00	7.40	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
22	0.44	7.76	0.00	7.76	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
23	0.46	8.12	0.00	8.12	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
24	0.48	8.47	0.00	8.47	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
25	0.50	8.82	0.00	8.82	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
26	0.52	9.18	0.00	9.18	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
27	0.54	9.53	0.00	9.53	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
28	0.56	9.87	0.00	9.87	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
29	0.58	10.22	0.00	10.22	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
30	0.60	10.57	0.00	10.57	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
31	0.62	10.92	0.00	10.92	1.00	0.149	1.43	0.105	1.10	1.00	2.000	No
32	0.64	11.26	0.00	11.26	1.00	0.149	1.43	0.105	1.10	1.00	2.000	No
33	0.66	11.61	0.00	11.61	1.00	0.149	1.43	0.105	1.10	1.00	2.000	No
34	0.68	11.95	0.00	11.95	1.00	0.149	1.43	0.105	1.10	1.00	2.000	No
35	0.70	12.30	0.00	12.30	1.00	0.149	1.43	0.105	1.10	1.00	2.000	No
36	0.72	12.65	0.00	12.65	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
37	0.74	12.99	0.00	12.99	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
38	0.76	13.34	0.00	13.34	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
39	0.78	13.69	0.00	13.69	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
40	0.80	14.04	0.00	14.04	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
41	0.82	14.39	0.00	14.39	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
42	0.84	14.74	0.00	14.74	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
43	0.87	15.27	0.00	15.27	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
44	0.88	15.45	0.00	15.45	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
45	0.90	15.81	0.00	15.81	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
46	0.92	16.17	0.00	16.17	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
47	0.94	16.53	0.00	16.53	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
48	0.96	16.88	0.00	16.88	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
49	0.99	17.42	0.00	17.42	0.99	0.149	1.43	0.104	1.10	1.00	2.000	No
50	1.00	17.60	0.00	17.60	0.99	0.149	1.43	0.104	1.10	1.00	2.000	No
51	1.09	19.21	0.88	18.33	0.99	0.156	1.43	0.109	1.10	1.00	0.131	No
52	1.09	19.21	0.88	18.33	0.99	0.156	1.43	0.109	1.10	1.00	0.131	No
53	1.09	19.21	0.88	18.33	0.99	0.156	1.43	0.109	1.10	1.00	0.131	No
54	1.09	19.21	0.88	18.33	0.99	0.156	1.43	0.109	1.10	1.00	0.131	No
55	1.11	19.56	1.08	18.49	0.99	0.157	1.43	0.110	1.10	1.00	0.132	No
56	1.13	19.92	1.28	18.65	0.99	0.159	1.43	0.111	1.10	1.00	0.133	No
57	1.14	20.10	1.37	18.73	0.99	0.159	1.43	0.111	1.10	1.00	0.134	No
58	1.17	20.63	1.67	18.97	0.99	0.161	1.43	0.113	1.10	1.00	0.136	No
59	1.18	20.81	1.77	19.05	0.99	0.162	1.43	0.113	1.10	1.00	0.136	No
60	1.20	21.17	1.96	19.21	0.99	0.163	1.43	0.114	1.10	1.00	0.137	No
61	1.22	21.52	2.16	19.37	0.99	0.165	1.43	0.115	1.10	1.00	0.139	No
62	1.24	21.88	2.35	19.53	0.99	0.166	1.43	0.116	1.10	1.00	0.140	No
63	1.26	22.24	2.55	19.68	0.99	0.167	1.43	0.117	1.10	1.00	0.141	No
64	1.28	22.59	2.75	19.84	0.99	0.169	1.43	0.118	1.10	1.00	0.142	No
65	1.30	22.95	2.94	20.00	0.99	0.170	1.43	0.119	1.10	1.00	0.143	No
66	1.32	23.30	3.14	20.16	0.99	0.171	1.43	0.120	1.10	1.00	0.143	No
67	1.34	23.66	3.34	20.32	0.99	0.172	1.43	0.121	1.10	1.00	0.143	No
68	1.36	24.01	3.53	20.48	0.99	0.173	1.43	0.121	1.10	1.00	0.144	No
69	1.38	24.37	3.73	20.64	0.99	0.175	1.43	0.122	1.10	1.00	0.145	No
70	1.40	24.73	3.92	20.80	0.99	0.176	1.43	0.123	1.10	1.00	0.146	No
71	1.42	25.08	4.12	20.96	0.99	0.177	1.43	0.124	1.10	1.00	0.147	No
72	1.44	25.44	4.32	21.13	0.99	0.178	1.43	0.124	1.10	1.00	0.148	No
73	1.46	25.80	4.51	21.29	0.99	0.179	1.43	0.125	1.10	1.00	0.148	No
74	1.48	26.17	4.71	21.46	0.99	0.180	1.43	0.126	1.10	1.00	0.149	No
75	1.50	26.53	4.91	21.62	0.99	0.181	1.43	0.127	1.10	1.00	0.149	No
76	1.52	26.89	5.10	21.79	0.99	0.182	1.43	0.127	1.10	1.00	0.150	No
77	1.54	27.26	5.30	21.96	0.99	0.183	1.43	0.128	1.10	1.00	0.151	No
78	1.56	27.62	5.49	22.13	0.99	0.184	1.43	0.129	1.10	1.00	0.152	No
79	1.58	27.99	5.69	22.30	0.99	0.185	1.43	0.129	1.10	1.00	0.153	No
80	1.60	28.35	5.89	22.47	0.99	0.186	1.43	0.130	1.10	1.00	0.153	No
81	1.62	28.72	6.08	22.64	0.99	0.187	1.43	0.131	1.10	1.00	0.154	No
82	1.64	29.09	6.28	22.81	0.98	0.188	1.43	0.131	1.10	1.00	0.155	No
83	1.66	29.46	6.47	22.98	0.98	0.189	1.43	0.132	1.10	1.00	0.155	No
84	1.68	29.83	6.67	23.15	0.98	0.190	1.43	0.133	1.10	1.00	0.156	No
85	1.70	30.19	6.87	23.33	0.98	0.190	1.43	0.133	1.10	1.00	0.156	No
86	1.72	30.56	7.06	23.50	0.98	0.191	1.43	0.134	1.10	1.00	0.157	No
87	1.74	30.93	7.26	23.67	0.98	0.192	1.43	0.134	1.10	1.00	0.158	No
88	1.78	31.66	7.65	24.01	0.98	0.194	1.43	0.136	1.10	1.00	0.161	No
89	1.78	31.66	7.65	24.01	0.98	0.194	1.43	0.136	1.10	1.00	0.161	No
90	1.80	32.03	7.85	24.18	0.98	0.194	1.43	0.136	1.10	1.00	0.163	No
91	1.82	32.39	8.04	24.35	0.98	0.195	1.43	0.137	1.10	1.00	0.164	No
92	1.84	32.76	8.24	24.52	0.98	0.196	1.43	0.137	1.10	1.00	0.165	No
93	1.86	33.12	8.44	24.68	0.98	0.197	1.43	0.138	1.10	1.00	0.166	No
94	1.88	33.48	8.63	24.84	0.98	0.198	1.43	0.138	1.10	1.00	0.166	No
95	1.90	33.83	8.83	25.01	0.98	0.198	1.43	0.139	1.10	1.00	0.167	No
96	1.92	34.19	9.03	25.16	0.98	0.199	1.43	0.139	1.10	1.00	0.168	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
97	1.94	34.54	9.22	25.32	0.98	0.200	1.43	0.140	1.10	1.00	0.168	No
98	1.96	34.89	9.42	25.47	0.98	0.201	1.43	0.140	1.10	1.00	0.169	No
99	1.98	35.23	9.61	25.62	0.98	0.201	1.43	0.141	1.10	1.00	0.170	No
100	2.00	35.57	9.81	25.76	0.98	0.202	1.43	0.141	1.10	1.00	0.170	No
101	2.08	36.94	10.59	26.34	0.98	0.205	1.43	0.143	1.10	1.00	0.173	No
102	2.08	36.94	10.59	26.34	0.98	0.205	1.43	0.143	1.10	1.00	0.173	No
103	2.08	36.94	10.59	26.34	0.98	0.205	1.43	0.143	1.10	1.00	0.173	No
104	2.10	37.28	10.79	26.49	0.98	0.206	1.43	0.144	1.10	1.00	0.172	No
105	2.12	37.62	10.99	26.63	0.98	0.206	1.43	0.144	1.10	1.00	0.172	No
106	2.14	37.97	11.18	26.78	0.98	0.207	1.43	0.145	1.10	1.00	0.172	No
107	2.16	38.32	11.38	26.94	0.98	0.208	1.43	0.145	1.10	1.00	0.172	No
108	2.18	38.67	11.58	27.09	0.98	0.208	1.43	0.146	1.10	1.00	0.172	No
109	2.20	39.02	11.77	27.25	0.98	0.209	1.43	0.146	1.10	1.00	0.172	No
110	2.22	39.37	11.97	27.41	0.98	0.209	1.43	0.147	1.10	1.00	0.172	No
111	2.24	39.73	12.16	27.57	0.97	0.210	1.43	0.147	1.10	1.00	0.172	No
112	2.26	40.09	12.36	27.73	0.97	0.211	1.43	0.147	1.10	1.00	0.173	No
113	2.28	40.45	12.56	27.90	0.97	0.211	1.43	0.148	1.10	1.00	0.174	No
114	2.30	40.82	12.75	28.07	0.97	0.212	1.43	0.148	1.10	1.00	0.175	No
115	2.32	41.19	12.95	28.24	0.97	0.212	1.43	0.149	1.10	1.00	0.175	No
116	2.34	41.55	13.15	28.41	0.97	0.213	1.43	0.149	1.10	1.00	0.176	No
117	2.36	41.92	13.34	28.58	0.97	0.213	1.43	0.149	1.10	1.00	0.177	No
118	2.38	42.29	13.54	28.75	0.97	0.214	1.43	0.150	1.10	1.00	0.177	No
119	2.40	42.66	13.73	28.92	0.97	0.214	1.43	0.150	1.10	1.00	0.177	No
120	2.42	43.03	13.93	29.10	0.97	0.215	1.43	0.150	1.10	1.00	0.177	No
121	2.44	43.39	14.13	29.27	0.97	0.215	1.43	0.151	1.10	1.00	0.177	No
122	2.46	43.76	14.32	29.43	0.97	0.216	1.43	0.151	1.10	1.00	0.178	No
123	2.48	44.12	14.52	29.60	0.97	0.216	1.43	0.151	1.10	1.00	0.178	No
124	2.50	44.48	14.72	29.77	0.97	0.217	1.43	0.152	1.10	1.00	0.179	No
125	2.52	44.85	14.91	29.94	0.97	0.217	1.43	0.152	1.10	1.00	0.179	No
126	2.54	45.22	15.11	30.11	0.97	0.218	1.43	0.152	1.10	1.00	0.180	No
127	2.56	45.58	15.30	30.28	0.97	0.218	1.43	0.153	1.10	1.00	0.180	No
128	2.58	45.95	15.50	30.45	0.97	0.219	1.43	0.153	1.10	1.00	0.180	No
129	2.60	46.32	15.70	30.62	0.97	0.219	1.43	0.153	1.10	1.00	0.180	No
130	2.62	46.68	15.89	30.79	0.97	0.219	1.43	0.154	1.10	1.00	0.181	No
131	2.64	47.05	16.09	30.96	0.97	0.220	1.43	0.154	1.10	1.00	0.181	No
132	2.66	47.41	16.28	31.13	0.97	0.220	1.43	0.154	1.10	1.00	0.182	No
133	2.68	47.78	16.48	31.30	0.97	0.221	1.43	0.155	1.10	1.00	0.182	No
134	2.70	48.15	16.68	31.47	0.97	0.221	1.43	0.155	1.10	1.00	0.183	No
135	2.72	48.52	16.87	31.64	0.97	0.222	1.43	0.155	1.10	1.00	0.183	No
136	2.74	48.89	17.07	31.82	0.97	0.222	1.43	0.155	1.10	1.00	0.183	No
137	2.76	49.26	17.27	31.99	0.97	0.222	1.43	0.156	1.10	1.00	0.183	No
138	2.78	49.63	17.46	32.17	0.97	0.223	1.43	0.156	1.10	1.00	0.183	No
139	2.81	50.18	17.76	32.43	0.96	0.223	1.43	0.156	1.10	1.00	0.184	No
140	2.82	50.37	17.85	32.51	0.96	0.223	1.43	0.156	1.10	1.00	0.184	No
141	2.84	50.74	18.05	32.69	0.96	0.224	1.43	0.157	1.10	1.00	0.185	No
142	2.86	51.11	18.25	32.86	0.96	0.224	1.43	0.157	1.10	1.00	0.185	No
143	2.88	51.48	18.44	33.04	0.96	0.224	1.43	0.157	1.10	1.00	0.186	No
144	2.90	51.85	18.64	33.21	0.96	0.225	1.43	0.157	1.10	1.00	0.186	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
145	2.92	52.22	18.84	33.39	0.96	0.225	1.43	0.158	1.10	1.00	0.186	No
146	2.94	52.59	19.03	33.56	0.96	0.226	1.43	0.158	1.10	1.00	0.186	No
147	2.96	52.96	19.23	33.73	0.96	0.226	1.43	0.158	1.10	1.00	0.186	No
148	2.98	53.33	19.42	33.91	0.96	0.226	1.43	0.158	1.10	1.00	0.186	No
149	3.00	53.70	19.62	34.08	0.96	0.227	1.43	0.159	1.10	1.00	0.187	No
150	3.02	54.07	19.82	34.25	0.96	0.227	1.43	0.159	1.10	1.00	0.187	No
151	3.04	54.43	20.01	34.42	0.96	0.227	1.43	0.159	1.10	1.00	0.188	No
152	3.06	54.80	20.21	34.59	0.96	0.227	1.43	0.159	1.10	1.00	0.188	No
153	3.08	55.17	20.40	34.76	0.96	0.228	1.43	0.159	1.10	1.00	0.189	No
154	3.10	55.53	20.60	34.93	0.96	0.228	1.43	0.160	1.09	1.00	0.191	No
155	3.12	55.90	20.80	35.10	0.96	0.228	1.43	0.160	1.09	1.00	0.192	No
156	3.14	56.26	20.99	35.27	0.96	0.229	1.43	0.160	1.09	1.00	0.193	No
157	3.16	56.63	21.19	35.44	0.96	0.229	1.43	0.160	1.09	1.00	0.194	No
158	3.18	56.99	21.39	35.61	0.96	0.229	1.43	0.160	1.09	1.00	0.194	No
159	3.20	57.35	21.58	35.77	0.96	0.230	1.43	0.161	1.09	1.00	0.194	No
160	3.22	57.71	21.78	35.93	0.96	0.230	1.43	0.161	1.09	1.00	0.194	No
161	3.24	58.07	21.97	36.09	0.96	0.230	1.43	0.161	1.09	1.00	0.195	No
162	3.26	58.42	22.17	36.25	0.96	0.231	1.43	0.161	1.09	1.00	0.196	No
163	3.28	58.78	22.37	36.41	0.96	0.231	1.43	0.162	1.09	1.00	0.196	No
164	3.30	59.13	22.56	36.57	0.96	0.231	1.43	0.162	1.09	1.00	0.196	No
165	3.32	59.48	22.76	36.72	0.96	0.231	1.43	0.162	1.09	1.00	0.195	No
166	3.34	59.83	22.96	36.88	0.96	0.232	1.43	0.162	1.09	1.00	0.196	No
167	3.36	60.19	23.15	37.04	0.95	0.232	1.43	0.162	1.09	1.00	0.195	No
168	3.38	60.54	23.35	37.20	0.95	0.232	1.43	0.163	1.09	1.00	0.195	No
169	3.40	60.90	23.54	37.35	0.95	0.233	1.43	0.163	1.09	1.00	0.195	No
170	3.42	61.25	23.74	37.51	0.95	0.233	1.43	0.163	1.09	1.00	0.195	No
171	3.44	61.61	23.94	37.68	0.95	0.233	1.43	0.163	1.09	1.00	0.195	No
172	3.46	61.97	24.13	37.84	0.95	0.233	1.43	0.163	1.09	1.00	0.195	No
173	3.48	62.33	24.33	38.00	0.95	0.234	1.43	0.164	1.09	1.00	0.196	No
174	3.50	62.69	24.53	38.16	0.95	0.234	1.43	0.164	1.09	1.00	0.196	No
175	3.52	63.05	24.72	38.33	0.95	0.234	1.43	0.164	1.09	1.00	0.197	No
176	3.54	63.41	24.92	38.50	0.95	0.234	1.43	0.164	1.09	1.00	0.198	No
177	3.56	63.77	25.11	38.66	0.95	0.235	1.43	0.164	1.09	1.00	0.198	No
178	3.58	64.14	25.31	38.83	0.95	0.235	1.43	0.164	1.09	1.00	0.198	No
179	3.60	64.50	25.51	38.99	0.95	0.235	1.43	0.164	1.09	1.00	0.198	No
180	3.63	65.04	25.80	39.24	0.95	0.235	1.43	0.165	1.09	1.00	0.198	No
181	3.64	65.22	25.90	39.33	0.95	0.235	1.43	0.165	1.08	1.00	0.199	No
182	3.66	65.59	26.09	39.49	0.95	0.236	1.43	0.165	1.08	1.00	0.199	No
183	3.68	65.95	26.29	39.66	0.95	0.236	1.43	0.165	1.08	1.00	0.200	No
184	3.70	66.31	26.49	39.82	0.95	0.236	1.43	0.165	1.08	1.00	0.200	No
185	3.72	66.67	26.68	39.99	0.95	0.236	1.43	0.165	1.08	1.00	0.200	No
186	3.74	67.03	26.88	40.15	0.95	0.237	1.43	0.166	1.08	1.00	0.201	No
187	3.76	67.39	27.08	40.32	0.95	0.237	1.43	0.166	1.08	1.00	0.201	No
188	3.78	67.76	27.27	40.49	0.95	0.237	1.43	0.166	1.08	1.00	0.200	No
189	3.80	68.12	27.47	40.65	0.95	0.237	1.43	0.166	1.08	1.00	0.199	No
190	3.82	68.48	27.66	40.82	0.95	0.237	1.43	0.166	1.08	1.00	0.199	No
191	3.84	68.85	27.86	40.99	0.95	0.237	1.43	0.166	1.08	1.00	0.199	No
192	3.86	69.21	28.06	41.15	0.95	0.238	1.43	0.166	1.08	1.00	0.199	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
193	3.88	69.58	28.25	41.32	0.94	0.238	1.43	0.166	1.08	1.00	0.201	No
194	3.90	69.94	28.45	41.49	0.94	0.238	1.43	0.167	1.08	1.00	0.201	No
195	3.92	70.31	28.65	41.66	0.94	0.238	1.43	0.167	1.08	1.00	0.202	No
196	3.94	70.67	28.84	41.83	0.94	0.238	1.43	0.167	1.08	1.00	0.204	No
197	3.96	71.04	29.04	42.00	0.94	0.239	1.43	0.167	1.08	1.00	0.205	No
198	3.98	71.40	29.23	42.17	0.94	0.239	1.43	0.167	1.07	1.00	0.205	No
199	4.00	71.77	29.43	42.34	0.94	0.239	1.43	0.167	1.07	1.00	0.206	No
200	4.02	72.13	29.63	42.51	0.94	0.239	1.43	0.167	1.07	1.00	0.206	No
201	4.04	72.49	29.82	42.67	0.94	0.239	1.43	0.167	1.07	1.00	0.206	No
202	4.07	73.03	30.12	42.92	0.94	0.239	1.43	0.168	1.07	1.00	0.206	No
203	4.08	73.21	30.21	43.00	0.94	0.240	1.43	0.168	1.07	1.00	0.206	No
204	4.10	73.57	30.41	43.16	0.94	0.240	1.43	0.168	1.07	1.00	0.206	No
205	4.12	73.92	30.61	43.32	0.94	0.240	1.43	0.168	1.07	1.00	0.206	No
206	4.14	74.28	30.80	43.47	0.94	0.240	1.43	0.168	1.07	1.00	0.206	No
207	4.26	76.40	31.98	44.42	0.94	0.241	1.43	0.169	1.07	1.00	0.207	No
208	4.26	76.40	31.98	44.42	0.94	0.241	1.43	0.169	1.07	1.00	0.207	No
209	4.26	76.40	31.98	44.42	0.94	0.241	1.43	0.169	1.07	1.00	0.207	No
210	4.26	76.40	31.98	44.42	0.94	0.241	1.43	0.169	1.07	1.00	0.207	No
211	4.26	76.40	31.98	44.42	0.94	0.241	1.43	0.169	1.07	1.00	0.207	No
212	4.28	76.76	32.18	44.59	0.94	0.241	1.43	0.169	1.07	1.00	0.207	No
213	4.30	77.13	32.37	44.76	0.94	0.241	1.43	0.169	1.07	1.00	0.208	No
214	4.32	77.49	32.57	44.93	0.94	0.241	1.43	0.169	1.07	1.00	0.208	No
215	4.34	77.86	32.77	45.09	0.94	0.242	1.43	0.169	1.07	1.00	0.208	No
216	4.36	78.22	32.96	45.26	0.94	0.242	1.43	0.169	1.07	1.00	0.209	No
217	4.38	78.59	33.16	45.43	0.93	0.242	1.43	0.169	1.07	1.00	0.209	No
218	4.40	78.95	33.35	45.60	0.93	0.242	1.43	0.169	1.07	1.00	0.209	No
219	4.42	79.31	33.55	45.76	0.93	0.242	1.43	0.169	1.07	1.00	0.208	No
220	4.44	79.68	33.75	45.93	0.93	0.242	1.43	0.170	1.07	1.00	0.208	No
221	4.46	80.04	33.94	46.09	0.93	0.242	1.43	0.170	1.07	1.00	0.207	No
222	4.48	80.40	34.14	46.26	0.93	0.242	1.43	0.170	1.07	1.00	0.207	No
223	4.50	80.76	34.34	46.43	0.93	0.243	1.43	0.170	1.07	1.00	0.207	No
224	4.52	81.12	34.53	46.59	0.93	0.243	1.43	0.170	1.07	1.00	0.207	No
225	4.54	81.49	34.73	46.76	0.93	0.243	1.43	0.170	1.07	1.00	0.207	No
226	4.56	81.85	34.92	46.93	0.93	0.243	1.43	0.170	1.07	1.00	0.208	No
227	4.58	82.22	35.12	47.10	0.93	0.243	1.43	0.170	1.07	1.00	0.209	No
228	4.60	82.59	35.32	47.27	0.93	0.243	1.43	0.170	1.07	1.00	0.210	No
229	4.62	82.96	35.51	47.44	0.93	0.243	1.43	0.170	1.07	1.00	0.210	No
230	4.64	83.33	35.71	47.62	0.93	0.243	1.43	0.170	1.07	1.00	0.210	No
231	4.66	83.70	35.90	47.79	0.93	0.243	1.43	0.170	1.07	1.00	0.210	No
232	4.68	84.06	36.10	47.96	0.93	0.243	1.43	0.170	1.07	1.00	0.210	No
233	4.70	84.43	36.30	48.14	0.93	0.243	1.43	0.170	1.06	1.00	0.210	No
234	4.72	84.80	36.49	48.31	0.93	0.244	1.43	0.170	1.06	1.00	0.211	No
235	4.74	85.17	36.69	48.48	0.93	0.244	1.43	0.171	1.06	1.00	0.211	No
236	4.76	85.53	36.89	48.65	0.93	0.244	1.43	0.171	1.06	1.00	0.211	No
237	4.78	85.90	37.08	48.82	0.93	0.244	1.43	0.171	1.06	1.00	0.211	No
238	4.80	86.27	37.28	48.99	0.93	0.244	1.43	0.171	1.06	1.00	0.211	No
239	4.82	86.63	37.47	49.16	0.93	0.244	1.43	0.171	1.06	1.00	0.211	No
240	4.84	87.00	37.67	49.33	0.93	0.244	1.43	0.171	1.06	1.00	0.211	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
241	4.86	87.36	37.87	49.49	0.93	0.244	1.43	0.171	1.06	1.00	0.211	No
242	4.88	87.73	38.06	49.66	0.92	0.244	1.43	0.171	1.06	1.00	0.211	No
243	4.90	88.09	38.26	49.83	0.92	0.244	1.43	0.171	1.06	1.00	0.212	No
244	4.92	88.46	38.46	50.00	0.92	0.244	1.43	0.171	1.06	1.00	0.212	No
245	4.94	88.82	38.65	50.17	0.92	0.244	1.43	0.171	1.06	1.00	0.212	No
246	4.96	89.19	38.85	50.34	0.92	0.244	1.43	0.171	1.06	1.00	0.213	No
247	4.98	89.56	39.04	50.51	0.92	0.245	1.43	0.171	1.06	1.00	0.213	No
248	5.01	90.10	39.34	50.76	0.92	0.245	1.43	0.171	1.06	1.00	0.213	No
249	5.02	90.28	39.44	50.85	0.92	0.245	1.43	0.171	1.06	1.00	0.214	No
250	5.04	90.65	39.63	51.01	0.92	0.245	1.43	0.171	1.06	1.00	0.214	No
251	5.06	91.01	39.83	51.18	0.92	0.245	1.43	0.171	1.06	1.00	0.214	No
252	5.08	91.37	40.02	51.34	0.92	0.245	1.43	0.171	1.06	1.00	0.215	No
253	5.10	91.73	40.22	51.50	0.92	0.245	1.43	0.171	1.06	1.00	0.215	No
254	5.12	92.08	40.42	51.67	0.92	0.245	1.43	0.172	1.06	1.00	0.216	No
255	5.14	92.44	40.61	51.83	0.92	0.245	1.43	0.172	1.06	1.00	0.216	No
256	5.16	92.80	40.81	51.99	0.92	0.245	1.43	0.172	1.05	1.00	0.216	No
257	5.18	93.15	41.01	52.15	0.92	0.245	1.43	0.172	1.05	1.00	0.216	No
258	5.20	93.50	41.20	52.30	0.92	0.245	1.43	0.172	1.05	1.00	0.217	No
259	5.22	93.85	41.40	52.45	0.92	0.245	1.43	0.172	1.05	1.00	0.217	No
260	5.24	94.20	41.59	52.61	0.92	0.246	1.43	0.172	1.05	1.00	0.217	No
261	5.26	94.55	41.79	52.76	0.92	0.246	1.43	0.172	1.05	1.00	0.217	No
262	5.28	94.89	41.99	52.90	0.92	0.246	1.43	0.172	1.05	1.00	0.217	No
263	5.30	95.24	42.18	53.05	0.92	0.246	1.43	0.172	1.05	1.00	0.216	No
264	5.32	95.58	42.38	53.20	0.92	0.246	1.43	0.172	1.05	1.00	0.216	No
265	5.34	95.92	42.58	53.35	0.92	0.246	1.43	0.172	1.05	1.00	0.216	No
266	5.36	96.27	42.77	53.50	0.91	0.246	1.43	0.172	1.05	1.00	0.216	No
267	5.38	96.61	42.97	53.65	0.91	0.246	1.43	0.172	1.05	1.00	0.216	No
268	5.40	96.96	43.16	53.80	0.91	0.246	1.43	0.172	1.05	1.00	0.217	No
269	5.42	97.31	43.36	53.95	0.91	0.246	1.43	0.172	1.05	1.00	0.217	No
270	5.44	97.66	43.56	54.11	0.91	0.246	1.43	0.172	1.05	1.00	0.216	No
271	5.46	98.02	43.75	54.26	0.91	0.246	1.43	0.172	1.05	1.00	0.216	No
272	5.48	98.37	43.95	54.42	0.91	0.246	1.43	0.173	1.05	1.00	0.216	No
273	5.50	98.72	44.15	54.58	0.91	0.247	1.43	0.173	1.05	1.00	0.216	No
274	5.52	99.08	44.34	54.73	0.91	0.247	1.43	0.173	1.05	1.00	0.216	No
275	5.54	99.43	44.54	54.89	0.91	0.247	1.43	0.173	1.05	1.00	0.216	No
276	5.56	99.79	44.73	55.05	0.91	0.247	1.43	0.173	1.05	1.00	0.215	No
277	5.58	100.14	44.93	55.22	0.91	0.247	1.43	0.173	1.05	1.00	0.215	No
278	5.60	100.50	45.13	55.38	0.91	0.247	1.43	0.173	1.05	1.00	0.215	No
279	5.62	100.87	45.32	55.54	0.91	0.247	1.43	0.173	1.05	1.00	0.215	No
280	5.64	101.23	45.52	55.71	0.91	0.247	1.43	0.173	1.05	1.00	0.215	No
281	5.66	101.59	45.71	55.88	0.91	0.247	1.43	0.173	1.05	1.00	0.215	No
282	5.68	101.96	45.91	56.05	0.91	0.247	1.43	0.173	1.05	1.00	0.215	No
283	5.70	102.33	46.11	56.22	0.91	0.247	1.43	0.173	1.05	1.00	0.214	No
284	5.72	102.69	46.30	56.39	0.91	0.247	1.43	0.173	1.05	1.00	0.214	No
285	5.74	103.06	46.50	56.56	0.91	0.247	1.43	0.173	1.05	1.00	0.214	No
286	5.76	103.43	46.70	56.74	0.91	0.247	1.43	0.173	1.05	1.00	0.214	No
287	5.78	103.80	46.89	56.91	0.91	0.247	1.43	0.173	1.05	1.00	0.214	No
288	5.80	104.17	47.09	57.08	0.91	0.247	1.43	0.173	1.05	1.00	0.215	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
289	5.82	104.54	47.28	57.26	0.90	0.247	1.43	0.173	1.05	1.00	0.215	No
290	5.84	104.91	47.48	57.43	0.90	0.247	1.43	0.173	1.05	1.00	0.216	No
291	5.86	105.29	47.68	57.61	0.90	0.247	1.43	0.173	1.05	1.00	0.216	No
292	5.88	105.66	47.87	57.78	0.90	0.247	1.43	0.173	1.05	1.00	0.216	No
293	5.90	106.03	48.07	57.96	0.90	0.247	1.43	0.173	1.05	1.00	0.216	No
294	5.92	106.39	48.27	58.13	0.90	0.247	1.43	0.173	1.05	1.00	0.216	No
295	5.94	106.76	48.46	58.30	0.90	0.247	1.43	0.173	1.05	1.00	0.217	No
296	5.97	107.31	48.76	58.56	0.90	0.247	1.43	0.173	1.05	1.00	0.217	No
297	5.98	107.49	48.85	58.64	0.90	0.247	1.43	0.173	1.05	1.00	0.217	No
298	6.00	107.86	49.05	58.81	0.90	0.247	1.43	0.173	1.05	1.00	0.217	No
299	6.02	108.23	49.25	58.98	0.90	0.247	1.43	0.173	1.05	1.00	0.217	No
300	6.04	108.59	49.44	59.15	0.90	0.247	1.43	0.173	1.05	1.00	0.216	No
301	6.06	108.96	49.64	59.32	0.90	0.247	1.43	0.173	1.05	1.00	0.216	No
302	6.08	109.32	49.83	59.49	0.90	0.247	1.43	0.173	1.05	1.00	0.216	No
303	6.10	109.69	50.03	59.65	0.90	0.247	1.43	0.173	1.05	1.00	0.216	No
304	6.12	110.05	50.23	59.82	0.90	0.247	1.43	0.173	1.05	1.00	0.216	No
305	6.14	110.41	50.42	59.99	0.90	0.247	1.43	0.173	1.05	1.00	0.217	No
306	6.16	110.78	50.62	60.16	0.90	0.247	1.43	0.173	1.05	1.00	0.217	No
307	6.18	111.15	50.82	60.33	0.90	0.247	1.43	0.173	1.05	1.00	0.217	No
308	6.20	111.52	51.01	60.50	0.90	0.247	1.43	0.173	1.05	1.00	0.217	No
309	6.22	111.88	51.21	60.68	0.90	0.247	1.43	0.173	1.04	1.00	0.217	No
310	6.24	112.25	51.40	60.85	0.90	0.247	1.43	0.173	1.04	1.00	0.217	No
311	6.26	112.62	51.60	61.02	0.89	0.247	1.43	0.173	1.04	1.00	0.218	No
312	6.28	112.99	51.80	61.20	0.89	0.247	1.43	0.173	1.04	1.00	0.218	No
313	6.30	113.36	51.99	61.37	0.89	0.247	1.43	0.173	1.04	1.00	0.218	No
314	6.32	113.73	52.19	61.54	0.89	0.247	1.43	0.173	1.04	1.00	0.218	No
315	6.34	114.10	52.39	61.72	0.89	0.247	1.43	0.173	1.04	1.00	0.217	No
316	6.36	114.47	52.58	61.89	0.89	0.247	1.43	0.173	1.04	1.00	0.217	No
317	6.38	114.84	52.78	62.06	0.89	0.247	1.43	0.173	1.04	1.00	0.217	No
318	6.41	115.39	53.07	62.32	0.89	0.247	1.43	0.173	1.04	1.00	0.217	No
319	6.42	115.58	53.17	62.41	0.89	0.247	1.43	0.173	1.04	1.00	0.217	No
320	6.44	115.94	53.37	62.58	0.89	0.247	1.43	0.173	1.04	1.00	0.217	No
321	6.46	116.31	53.56	62.75	0.89	0.247	1.43	0.173	1.04	1.00	0.217	No
322	6.48	116.68	53.76	62.92	0.89	0.247	1.43	0.173	1.04	1.00	0.217	No
323	6.50	117.05	53.96	63.10	0.89	0.247	1.43	0.173	1.04	1.00	0.217	No
324	6.52	117.42	54.15	63.27	0.89	0.247	1.43	0.173	1.04	1.00	0.217	No
325	6.54	117.80	54.35	63.45	0.89	0.247	1.43	0.173	1.04	1.00	0.217	No
326	6.56	118.17	54.54	63.62	0.89	0.247	1.43	0.173	1.04	1.00	0.217	No
327	6.58	118.54	54.74	63.80	0.89	0.247	1.43	0.173	1.04	1.00	0.217	No
328	6.60	118.91	54.94	63.98	0.89	0.247	1.43	0.173	1.04	1.00	0.218	No
329	6.62	119.28	55.13	64.15	0.89	0.247	1.43	0.173	1.04	1.00	0.218	No
330	6.64	119.66	55.33	64.33	0.89	0.247	1.43	0.173	1.04	1.00	0.218	No
331	6.66	120.03	55.52	64.50	0.89	0.246	1.43	0.173	1.04	1.00	0.219	No
332	6.68	120.40	55.72	64.68	0.89	0.246	1.43	0.173	1.04	1.00	0.219	No
333	6.70	120.77	55.92	64.86	0.89	0.246	1.43	0.172	1.04	1.00	0.220	No
334	6.72	121.14	56.11	65.03	0.88	0.246	1.43	0.172	1.04	1.00	0.220	No
335	6.74	121.51	56.31	65.20	0.88	0.246	1.43	0.172	1.04	1.00	0.220	No
336	6.76	121.88	56.51	65.37	0.88	0.246	1.43	0.172	1.04	1.00	0.220	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
337	6.78	122.24	56.70	65.54	0.88	0.246	1.43	0.172	1.04	1.00	0.220	No
338	6.81	122.79	57.00	65.79	0.88	0.246	1.43	0.172	1.04	1.00	0.220	No
339	6.82	122.97	57.09	65.88	0.88	0.246	1.43	0.172	1.04	1.00	0.220	No
340	6.84	123.33	57.29	66.04	0.88	0.246	1.43	0.172	1.04	1.00	0.219	No
341	6.87	123.87	57.58	66.28	0.88	0.246	1.43	0.172	1.04	1.00	0.219	No
342	6.88	124.04	57.68	66.36	0.88	0.246	1.43	0.172	1.04	1.00	0.219	No
343	6.90	124.40	57.88	66.52	0.88	0.246	1.43	0.172	1.04	1.00	0.220	No
344	6.92	124.76	58.08	66.68	0.88	0.246	1.43	0.172	1.04	1.00	0.220	No
345	6.94	125.11	58.27	66.84	0.88	0.246	1.43	0.172	1.04	1.00	0.220	No
346	6.96	125.47	58.47	67.00	0.88	0.246	1.43	0.172	1.03	1.00	0.220	No
347	6.98	125.83	58.66	67.17	0.88	0.246	1.43	0.172	1.03	1.00	0.220	No
348	7.00	126.19	58.86	67.33	0.88	0.246	1.43	0.172	1.03	1.00	0.220	No
349	7.02	126.55	59.06	67.49	0.88	0.246	1.43	0.172	1.03	1.00	0.221	No
350	7.04	126.91	59.25	67.65	0.88	0.246	1.43	0.172	1.03	1.00	0.221	No
351	7.06	127.26	59.45	67.81	0.88	0.246	1.43	0.172	1.03	1.00	0.220	No
352	7.08	127.62	59.64	67.97	0.88	0.246	1.43	0.172	1.03	1.00	0.220	No
353	7.10	127.97	59.84	68.13	0.88	0.246	1.43	0.172	1.03	1.00	0.220	No
354	7.12	128.33	60.04	68.29	0.88	0.246	1.43	0.172	1.03	1.00	0.220	No
355	7.15	128.86	60.33	68.53	0.87	0.246	1.43	0.172	1.03	1.00	0.219	No
356	7.16	129.04	60.43	68.61	0.87	0.246	1.43	0.172	1.03	1.00	0.219	No
357	7.18	129.40	60.63	68.77	0.87	0.246	1.43	0.172	1.03	1.00	0.218	No
358	7.20	129.75	60.82	68.93	0.87	0.246	1.43	0.172	1.03	1.00	0.218	No
359	7.30	131.55	61.80	69.75	0.87	0.246	1.43	0.172	1.03	1.00	0.218	No
360	7.30	131.55	61.80	69.75	0.87	0.246	1.43	0.172	1.03	1.00	0.218	No
361	7.30	131.55	61.80	69.75	0.87	0.246	1.43	0.172	1.03	1.00	0.218	No
362	7.32	131.92	62.00	69.92	0.87	0.246	1.43	0.172	1.03	1.00	0.218	No
363	7.34	132.29	62.20	70.10	0.87	0.246	1.43	0.172	1.03	1.00	0.218	No
364	7.36	132.67	62.39	70.27	0.87	0.246	1.43	0.172	1.03	1.00	0.218	No
365	7.38	133.04	62.59	70.45	0.87	0.246	1.43	0.172	1.03	1.00	0.218	No
366	7.40	133.41	62.78	70.63	0.87	0.245	1.43	0.172	1.03	1.00	0.219	No
367	7.42	133.79	62.98	70.80	0.87	0.245	1.43	0.172	1.03	1.00	0.219	No
368	7.44	134.16	63.18	70.98	0.87	0.245	1.43	0.172	1.03	1.00	0.219	No
369	7.46	134.53	63.37	71.15	0.87	0.245	1.43	0.172	1.03	1.00	0.219	No
370	7.48	134.90	63.57	71.33	0.87	0.245	1.43	0.172	1.03	1.00	0.219	No
371	7.50	135.27	63.77	71.50	0.87	0.245	1.43	0.172	1.03	1.00	0.219	No
372	7.52	135.64	63.96	71.67	0.87	0.245	1.43	0.172	1.03	1.00	0.219	No
373	7.54	136.00	64.16	71.85	0.87	0.245	1.43	0.172	1.03	1.00	0.219	No
374	7.56	136.37	64.35	72.02	0.87	0.245	1.43	0.171	1.03	1.00	0.219	No
375	7.58	136.74	64.55	72.19	0.87	0.245	1.43	0.171	1.03	1.00	0.219	No
376	7.60	137.11	64.75	72.36	0.86	0.245	1.43	0.171	1.03	1.00	0.219	No
377	7.62	137.48	64.94	72.53	0.86	0.245	1.43	0.171	1.03	1.00	0.218	No
378	7.64	137.84	65.14	72.70	0.86	0.245	1.43	0.171	1.03	1.00	0.218	No
379	7.66	138.21	65.33	72.88	0.86	0.245	1.43	0.171	1.03	1.00	0.218	No
380	7.68	138.58	65.53	73.05	0.86	0.245	1.43	0.171	1.03	1.00	0.218	No
381	7.70	138.95	65.73	73.22	0.86	0.245	1.43	0.171	1.03	1.00	0.218	No
382	7.72	139.32	65.92	73.40	0.86	0.245	1.43	0.171	1.03	1.00	0.218	No
383	7.74	139.69	66.12	73.57	0.86	0.244	1.43	0.171	1.03	1.00	0.218	No
384	7.76	140.06	66.32	73.74	0.86	0.244	1.43	0.171	1.03	1.00	0.218	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
385	7.78	140.43	66.51	73.92	0.86	0.244	1.43	0.171	1.03	1.00	0.218	No
386	7.80	140.80	66.71	74.09	0.86	0.244	1.43	0.171	1.03	1.00	0.218	No
387	7.83	141.36	67.00	74.36	0.86	0.244	1.43	0.171	1.03	1.00	0.218	No
388	7.84	141.55	67.10	74.45	0.86	0.244	1.43	0.171	1.03	1.00	0.218	No
389	7.86	141.92	67.30	74.62	0.86	0.244	1.43	0.171	1.03	1.00	0.218	No
390	7.88	142.29	67.49	74.80	0.86	0.244	1.43	0.171	1.03	1.00	0.218	No
391	7.90	142.66	67.69	74.97	0.86	0.244	1.43	0.171	1.03	1.00	0.218	No
392	7.93	143.22	67.98	75.24	0.86	0.244	1.43	0.171	1.03	1.00	0.218	No
393	7.94	143.41	68.08	75.33	0.86	0.244	1.43	0.171	1.03	1.00	0.218	No
394	7.96	143.78	68.28	75.50	0.86	0.244	1.43	0.171	1.03	1.00	0.218	No
395	7.98	144.15	68.47	75.68	0.86	0.244	1.43	0.171	1.03	1.00	0.218	No
396	8.00	144.53	68.67	75.86	0.86	0.244	1.43	0.171	1.03	1.00	0.218	No
397	8.02	144.90	68.87	76.04	0.85	0.244	1.43	0.170	1.03	1.00	0.218	No
398	8.04	145.27	69.06	76.21	0.85	0.243	1.43	0.170	1.02	1.00	0.218	No
399	8.06	145.65	69.26	76.39	0.85	0.243	1.43	0.170	1.02	1.00	0.218	No
400	8.08	146.02	69.45	76.56	0.85	0.243	1.43	0.170	1.02	1.00	0.218	No
401	8.10	146.39	69.65	76.74	0.85	0.243	1.43	0.170	1.02	1.00	0.218	No
402	8.12	146.76	69.85	76.91	0.85	0.243	1.43	0.170	1.02	1.00	0.218	No
403	8.14	147.13	70.04	77.09	0.85	0.243	1.43	0.170	1.02	1.00	0.218	No
404	8.16	147.51	70.24	77.27	0.85	0.243	1.43	0.170	1.02	1.00	0.218	No
405	8.18	147.88	70.44	77.44	0.85	0.243	1.43	0.170	1.02	1.00	0.217	No
406	8.20	148.25	70.63	77.62	0.85	0.243	1.43	0.170	1.02	1.00	0.217	No
407	8.22	148.62	70.83	77.80	0.85	0.243	1.43	0.170	1.02	1.00	0.217	No
408	8.24	149.00	71.02	77.97	0.85	0.243	1.43	0.170	1.02	1.00	0.217	No
409	8.26	149.37	71.22	78.15	0.85	0.243	1.43	0.170	1.02	1.00	0.217	No
410	8.28	149.75	71.42	78.33	0.85	0.243	1.43	0.170	1.02	1.00	0.217	No
411	8.30	150.12	71.61	78.51	0.85	0.242	1.43	0.170	1.02	1.00	0.217	No
412	8.32	150.50	71.81	78.69	0.85	0.242	1.43	0.170	1.02	1.00	0.217	No
413	8.34	150.87	72.01	78.87	0.85	0.242	1.43	0.170	1.02	1.00	0.217	No
414	8.36	151.25	72.20	79.05	0.85	0.242	1.43	0.170	1.02	1.00	0.218	No
415	8.38	151.62	72.40	79.23	0.85	0.242	1.43	0.169	1.02	1.00	0.218	No
416	8.40	152.00	72.59	79.40	0.85	0.242	1.43	0.169	1.02	1.00	0.218	No
417	8.43	152.56	72.89	79.67	0.85	0.242	1.43	0.169	1.02	1.00	0.218	No
418	8.44	152.75	72.99	79.76	0.84	0.242	1.43	0.169	1.02	1.00	0.217	No
419	8.46	153.12	73.18	79.94	0.84	0.242	1.43	0.169	1.02	1.00	0.217	No
420	8.48	153.49	73.38	80.12	0.84	0.242	1.43	0.169	1.02	1.00	0.218	No
421	8.50	153.87	73.58	80.29	0.84	0.242	1.43	0.169	1.02	1.00	0.217	No
422	8.52	154.24	73.77	80.47	0.84	0.242	1.43	0.169	1.02	1.00	0.217	No
423	8.54	154.62	73.97	80.65	0.84	0.241	1.43	0.169	1.02	1.00	0.217	No
424	8.56	154.99	74.16	80.83	0.84	0.241	1.43	0.169	1.02	1.00	0.217	No
425	8.58	155.36	74.36	81.00	0.84	0.241	1.43	0.169	1.02	1.00	0.217	No
426	8.60	155.74	74.56	81.18	0.84	0.241	1.43	0.169	1.02	1.00	0.217	No
427	8.62	156.11	74.75	81.36	0.84	0.241	1.43	0.169	1.02	1.00	0.217	No
428	8.64	156.49	74.95	81.54	0.84	0.241	1.43	0.169	1.02	1.00	0.217	No
429	8.66	156.87	75.14	81.72	0.84	0.241	1.43	0.169	1.02	1.00	0.217	No
430	8.68	157.24	75.34	81.90	0.84	0.241	1.43	0.169	1.02	1.00	0.216	No
431	8.70	157.62	75.54	82.08	0.84	0.241	1.43	0.169	1.02	1.00	0.216	No
432	8.72	158.00	75.73	82.26	0.84	0.241	1.43	0.168	1.02	1.00	0.216	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
433	8.74	158.38	75.93	82.45	0.84	0.241	1.43	0.168	1.02	1.00	0.216	No
434	8.76	158.75	76.13	82.63	0.84	0.241	1.43	0.168	1.02	1.00	0.216	No
435	8.78	159.13	76.32	82.81	0.84	0.240	1.43	0.168	1.02	1.00	0.215	No
436	8.80	159.52	76.52	83.00	0.84	0.240	1.43	0.168	1.02	1.00	0.215	No
437	8.82	159.90	76.71	83.18	0.84	0.240	1.43	0.168	1.02	1.00	0.215	No
438	8.84	160.28	76.91	83.37	0.84	0.240	1.43	0.168	1.02	1.00	0.214	No
439	8.86	160.66	77.11	83.56	0.83	0.240	1.43	0.168	1.02	1.00	0.215	No
440	8.88	161.04	77.30	83.74	0.83	0.240	1.43	0.168	1.02	1.00	0.215	No
441	8.90	161.43	77.50	83.93	0.83	0.240	1.43	0.168	1.02	1.00	0.216	No
442	8.92	161.81	77.70	84.11	0.83	0.240	1.43	0.168	1.02	1.00	0.215	No
443	8.94	162.19	77.89	84.30	0.83	0.240	1.43	0.168	1.02	1.00	0.216	No
444	8.96	162.57	78.09	84.48	0.83	0.240	1.43	0.168	1.02	1.00	0.216	No
445	8.98	162.95	78.28	84.67	0.83	0.239	1.43	0.168	1.02	1.00	0.215	No
446	9.00	163.33	78.48	84.85	0.83	0.239	1.43	0.168	1.02	1.00	0.215	No
447	9.02	163.71	78.68	85.04	0.83	0.239	1.43	0.167	1.02	1.00	0.215	No
448	9.05	164.28	78.97	85.31	0.83	0.239	1.43	0.167	1.02	1.00	0.215	No
449	9.06	164.47	79.07	85.40	0.83	0.239	1.43	0.167	1.02	1.00	0.215	No
450	9.08	164.85	79.26	85.58	0.83	0.239	1.43	0.167	1.02	1.00	0.215	No
451	9.10	165.22	79.46	85.76	0.83	0.239	1.43	0.167	1.01	1.00	0.215	No
452	9.12	165.60	79.66	85.94	0.83	0.239	1.43	0.167	1.01	1.00	0.215	No
453	9.14	165.97	79.85	86.12	0.83	0.239	1.43	0.167	1.01	1.00	0.215	No
454	9.16	166.34	80.05	86.29	0.83	0.239	1.43	0.167	1.01	1.00	0.215	No
455	9.18	166.72	80.25	86.47	0.83	0.238	1.43	0.167	1.01	1.00	0.215	No
456	9.21	167.28	80.54	86.74	0.83	0.238	1.43	0.167	1.01	1.00	0.215	No
457	9.22	167.46	80.64	86.82	0.83	0.238	1.43	0.167	1.01	1.00	0.215	No
458	9.24	167.84	80.83	87.00	0.83	0.238	1.43	0.167	1.01	1.00	0.215	No
459	9.26	168.21	81.03	87.18	0.83	0.238	1.43	0.167	1.01	1.00	0.215	No
460	9.28	168.58	81.23	87.36	0.83	0.238	1.43	0.167	1.01	1.00	0.214	No
461	9.30	168.96	81.42	87.53	0.82	0.238	1.43	0.167	1.01	1.00	0.214	No
462	9.32	169.33	81.62	87.71	0.82	0.238	1.43	0.166	1.01	1.00	0.214	No
463	9.34	169.70	81.82	87.89	0.82	0.238	1.43	0.166	1.01	1.00	0.214	No
464	9.36	170.08	82.01	88.07	0.82	0.238	1.43	0.166	1.01	1.00	0.214	No
465	9.38	170.46	82.21	88.25	0.82	0.238	1.43	0.166	1.01	1.00	0.214	No
466	9.40	170.83	82.40	88.43	0.82	0.237	1.43	0.166	1.01	1.00	0.213	No
467	9.42	171.21	82.60	88.61	0.82	0.237	1.43	0.166	1.01	1.00	0.213	No
468	9.44	171.59	82.80	88.79	0.82	0.237	1.43	0.166	1.01	1.00	0.213	No
469	9.47	172.15	83.09	89.06	0.82	0.237	1.43	0.166	1.01	1.00	0.213	No
470	9.48	172.34	83.19	89.15	0.82	0.237	1.43	0.166	1.01	1.00	0.213	No
471	9.50	172.72	83.39	89.34	0.82	0.237	1.43	0.166	1.01	1.00	0.213	No
472	9.53	173.29	83.68	89.61	0.82	0.237	1.43	0.166	1.01	1.00	0.213	No
473	9.54	173.48	83.78	89.70	0.82	0.237	1.43	0.166	1.01	1.00	0.213	No
474	9.56	173.86	83.97	89.89	0.82	0.237	1.43	0.166	1.01	1.00	0.212	No
475	9.58	174.24	84.17	90.07	0.82	0.237	1.43	0.166	1.01	1.00	0.213	No
476	9.60	174.62	84.37	90.26	0.82	0.236	1.43	0.165	1.01	1.00	0.213	No
477	9.62	175.00	84.56	90.44	0.82	0.236	1.43	0.165	1.01	1.00	0.213	No
478	9.64	175.38	84.76	90.62	0.82	0.236	1.43	0.165	1.01	1.00	0.214	No
479	9.66	175.76	84.95	90.80	0.82	0.236	1.43	0.165	1.01	1.00	0.214	No
480	9.68	176.14	85.15	90.99	0.82	0.236	1.43	0.165	1.01	1.00	0.215	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
481	9.70	176.51	85.35	91.16	0.81	0.236	1.43	0.165	1.01	1.00	0.215	No
482	9.72	176.88	85.54	91.34	0.81	0.236	1.43	0.165	1.01	1.00	0.216	No
483	9.74	177.26	85.74	91.52	0.81	0.236	1.43	0.165	1.01	1.00	0.216	No
484	9.76	177.62	85.94	91.69	0.81	0.236	1.43	0.165	1.01	1.00	0.216	No
485	9.79	178.17	86.23	91.94	0.81	0.235	1.43	0.165	1.01	1.00	0.217	No
486	9.80	178.35	86.33	92.02	0.81	0.235	1.43	0.165	1.01	1.00	0.217	No
487	9.82	178.71	86.52	92.19	0.81	0.235	1.43	0.165	1.01	1.00	0.217	No
488	9.85	179.25	86.82	92.43	0.81	0.235	1.43	0.165	1.01	1.00	0.217	No
489	9.86	179.42	86.92	92.51	0.81	0.235	1.43	0.165	1.01	1.00	0.217	No
490	9.88	179.77	87.11	92.66	0.81	0.235	1.43	0.165	1.01	1.00	0.217	No
491	9.90	180.12	87.31	92.81	0.81	0.235	1.43	0.165	1.01	1.00	0.217	No
492	9.92	180.47	87.51	92.96	0.81	0.235	1.43	0.164	1.01	1.00	0.217	No
493	9.94	180.81	87.70	93.11	0.81	0.235	1.43	0.164	1.01	1.00	0.217	No
494	9.96	181.15	87.90	93.26	0.81	0.235	1.43	0.164	1.01	1.00	0.217	No
495	9.98	181.50	88.09	93.40	0.81	0.235	1.43	0.164	1.01	1.00	0.217	No
496	10.00	181.84	88.29	93.55	0.81	0.235	1.43	0.164	1.01	1.00	0.217	No
497	10.02	182.18	88.49	93.69	0.81	0.235	1.43	0.164	1.01	1.00	0.216	No
498	10.04	182.52	88.68	93.84	0.81	0.235	1.43	0.164	1.01	1.00	0.216	No
499	10.06	182.86	88.88	93.98	0.81	0.235	1.43	0.164	1.01	1.00	0.216	No
500	10.08	183.21	89.07	94.13	0.81	0.234	1.43	0.164	1.01	1.00	0.216	No
501	10.11	183.72	89.37	94.36	0.81	0.234	1.43	0.164	1.01	1.00	0.216	No
502	10.12	183.90	89.47	94.43	0.80	0.234	1.43	0.164	1.01	1.00	0.215	No
503	10.14	184.25	89.66	94.58	0.80	0.234	1.43	0.164	1.01	1.00	0.214	No
504	10.16	184.60	89.86	94.74	0.80	0.234	1.43	0.164	1.01	1.00	0.213	No
505	10.18	184.95	90.06	94.90	0.80	0.234	1.43	0.164	1.01	1.00	0.213	No
506	10.20	185.31	90.25	95.06	0.80	0.234	1.43	0.164	1.01	1.00	0.213	No
507	10.22	185.67	90.45	95.22	0.80	0.234	1.43	0.164	1.01	1.00	0.213	No
508	10.24	186.03	90.64	95.39	0.80	0.234	1.43	0.164	1.01	1.00	0.213	No
509	10.26	186.40	90.84	95.56	0.80	0.234	1.43	0.164	1.01	1.00	0.213	No
510	10.28	186.76	91.04	95.73	0.80	0.234	1.43	0.164	1.01	1.00	0.213	No
511	10.30	187.13	91.23	95.90	0.80	0.234	1.43	0.163	1.00	1.00	0.214	No
512	10.32	187.50	91.43	96.07	0.80	0.233	1.43	0.163	1.00	1.00	0.214	No
513	10.34	187.87	91.63	96.25	0.80	0.233	1.43	0.163	1.00	1.00	0.215	No
514	10.36	188.24	91.82	96.42	0.80	0.233	1.43	0.163	1.00	1.00	0.215	No
515	10.38	188.61	92.02	96.59	0.80	0.233	1.43	0.163	1.00	1.00	0.215	No
516	10.40	188.97	92.21	96.76	0.80	0.233	1.43	0.163	1.00	1.00	0.216	No
517	10.42	189.34	92.41	96.93	0.80	0.233	1.43	0.163	1.00	1.00	0.216	No
518	10.44	189.70	92.61	97.09	0.80	0.233	1.43	0.163	1.00	1.00	0.216	No
519	10.46	190.06	92.80	97.25	0.80	0.233	1.43	0.163	1.00	1.00	0.216	No
520	10.48	190.41	93.00	97.41	0.80	0.233	1.43	0.163	1.00	1.00	0.216	No
521	10.50	190.76	93.19	97.57	0.80	0.233	1.43	0.163	1.00	1.00	0.216	No
522	10.52	191.11	93.39	97.72	0.80	0.233	1.43	0.163	1.00	1.00	0.216	No
523	10.54	191.45	93.59	97.86	0.79	0.232	1.43	0.163	1.00	1.00	0.216	No
524	10.56	191.79	93.78	98.01	0.79	0.232	1.43	0.163	1.00	1.00	0.215	No
525	10.58	192.13	93.98	98.15	0.79	0.232	1.43	0.163	1.00	1.00	0.215	No
526	10.60	192.47	94.18	98.29	0.79	0.232	1.43	0.163	1.00	1.00	0.215	No
527	10.62	192.81	94.37	98.44	0.79	0.232	1.43	0.163	1.00	1.00	0.215	No
528	10.64	193.15	94.57	98.58	0.79	0.232	1.43	0.162	1.00	1.00	0.215	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
529	10.66	193.49	94.76	98.72	0.79	0.232	1.43	0.162	1.00	1.00	0.215	No
530	10.70	194.17	95.16	99.01	0.79	0.232	1.43	0.162	1.00	1.00	0.214	No
531	10.70	194.17	95.16	99.01	0.79	0.232	1.43	0.162	1.00	1.00	0.214	No
532	10.72	194.51	95.35	99.16	0.79	0.232	1.43	0.162	1.00	1.00	0.214	No
533	10.75	195.04	95.65	99.39	0.79	0.232	1.43	0.162	1.00	1.00	0.213	No
534	10.76	195.21	95.75	99.46	0.79	0.232	1.43	0.162	1.00	1.00	0.213	No
535	10.78	195.56	95.94	99.62	0.79	0.232	1.43	0.162	1.00	1.00	0.214	No
536	10.80	195.91	96.14	99.77	0.79	0.232	1.43	0.162	1.00	1.00	0.214	No
537	10.82	196.26	96.33	99.92	0.79	0.231	1.43	0.162	1.00	1.00	0.214	No
538	10.84	196.61	96.53	100.08	0.79	0.231	1.43	0.162	1.00	1.00	0.213	No
539	10.86	196.95	96.73	100.23	0.79	0.231	1.43	0.162	1.00	1.00	0.213	No
540	10.88	197.30	96.92	100.38	0.79	0.231	1.43	0.162	1.00	1.00	0.212	No
541	10.90	197.65	97.12	100.53	0.79	0.231	1.43	0.162	1.00	1.00	0.212	No
542	10.92	198.01	97.32	100.69	0.79	0.231	1.43	0.162	1.00	1.00	0.211	No
543	10.94	198.36	97.51	100.85	0.79	0.231	1.43	0.162	1.00	1.00	0.211	No
544	10.96	198.72	97.71	101.01	0.78	0.231	1.43	0.162	1.00	1.00	0.211	No
545	10.98	199.08	97.90	101.18	0.78	0.231	1.43	0.162	1.00	1.00	0.211	No
546	11.00	199.45	98.10	101.35	0.78	0.231	1.43	0.161	1.00	1.00	0.211	No
547	11.02	199.82	98.30	101.52	0.78	0.231	1.43	0.161	1.00	1.00	0.211	No
548	11.06	200.55	98.69	101.86	0.78	0.230	1.43	0.161	1.00	1.00	0.211	No
549	11.06	200.55	98.69	101.86	0.78	0.230	1.43	0.161	1.00	1.00	0.211	No
550	11.08	200.92	98.88	102.04	0.78	0.230	1.43	0.161	1.00	1.00	0.211	No
551	11.10	201.30	99.08	102.22	0.78	0.230	1.43	0.161	1.00	1.00	0.211	No
552	11.12	201.67	99.28	102.39	0.78	0.230	1.43	0.161	1.00	1.00	0.211	No
553	11.14	202.04	99.47	102.57	0.78	0.230	1.43	0.161	1.00	1.00	0.211	No
554	11.16	202.42	99.67	102.75	0.78	0.230	1.43	0.161	1.00	1.00	0.211	No
555	11.18	202.79	99.87	102.92	0.78	0.230	1.43	0.161	1.00	1.00	0.211	No
556	11.20	203.16	100.06	103.10	0.78	0.230	1.43	0.161	1.00	1.00	0.211	No
557	11.23	203.72	100.36	103.36	0.78	0.229	1.43	0.161	1.00	1.00	0.211	No
558	11.24	203.90	100.45	103.45	0.78	0.229	1.43	0.161	1.00	1.00	0.211	No
559	11.26	204.27	100.65	103.62	0.78	0.229	1.43	0.160	1.00	1.00	0.211	No
560	11.28	204.65	100.85	103.80	0.78	0.229	1.43	0.160	1.00	1.00	0.211	No
561	11.30	205.02	101.04	103.98	0.78	0.229	1.43	0.160	1.00	1.00	0.211	No
562	11.32	205.39	101.24	104.15	0.78	0.229	1.43	0.160	1.00	1.00	0.211	No
563	11.34	205.76	101.44	104.33	0.78	0.229	1.43	0.160	1.00	1.00	0.211	No
564	11.36	206.14	101.63	104.50	0.78	0.229	1.43	0.160	1.00	1.00	0.212	No
565	11.38	206.51	101.83	104.68	0.77	0.229	1.43	0.160	1.00	1.00	0.212	No
566	11.40	206.88	102.02	104.85	0.77	0.228	1.43	0.160	1.00	1.00	0.212	No
567	11.42	207.24	102.22	105.02	0.77	0.228	1.43	0.160	1.00	1.00	0.213	No
568	11.44	207.61	102.42	105.19	0.77	0.228	1.43	0.160	1.00	1.00	0.213	No
569	11.46	207.98	102.61	105.36	0.77	0.228	1.43	0.160	1.00	1.00	0.213	No
570	11.48	208.34	102.81	105.53	0.77	0.228	1.43	0.160	1.00	1.00	0.213	No
571	11.50	208.70	103.01	105.70	0.77	0.228	1.43	0.160	1.00	1.00	0.213	No
572	11.52	209.06	103.20	105.86	0.77	0.228	1.43	0.159	1.00	1.00	0.213	No
573	11.54	209.42	103.40	106.02	0.77	0.228	1.43	0.159	1.00	1.00	0.213	No
574	11.56	209.77	103.59	106.18	0.77	0.228	1.43	0.159	1.00	1.00	0.213	No
575	11.58	210.12	103.79	106.33	0.77	0.227	1.43	0.159	1.00	1.00	0.213	No
576	11.60	210.47	103.99	106.49	0.77	0.227	1.43	0.159	1.00	1.00	0.213	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
577	11.62	210.82	104.18	106.63	0.77	0.227	1.43	0.159	1.00	1.00	0.213	No
578	11.64	211.16	104.38	106.78	0.77	0.227	1.43	0.159	1.00	1.00	0.213	No
579	11.66	211.50	104.57	106.92	0.77	0.227	1.43	0.159	1.00	1.00	0.212	No
580	11.68	211.83	104.77	107.06	0.77	0.227	1.43	0.159	1.00	1.00	0.212	No
581	11.70	212.17	104.97	107.20	0.77	0.227	1.43	0.159	1.00	1.00	0.212	No
582	11.72	212.51	105.16	107.34	0.77	0.227	1.43	0.159	1.00	1.00	0.212	No
583	11.74	212.85	105.36	107.49	0.77	0.227	1.43	0.159	0.99	1.00	0.210	No
584	11.76	213.19	105.56	107.64	0.77	0.227	1.43	0.159	0.99	1.00	0.211	No
585	11.78	213.54	105.75	107.78	0.77	0.227	1.43	0.159	0.99	1.00	0.211	No
586	11.80	213.87	105.95	107.93	0.76	0.227	1.43	0.159	0.99	1.00	0.212	No
587	11.82	214.21	106.14	108.07	0.76	0.227	1.43	0.159	0.99	1.00	0.212	No
588	11.84	214.54	106.34	108.20	0.76	0.226	1.43	0.158	0.99	1.00	0.212	No
589	11.87	215.04	106.63	108.41	0.76	0.226	1.43	0.158	0.99	1.00	0.212	No
590	11.88	215.21	106.73	108.48	0.76	0.226	1.43	0.158	0.99	1.00	0.212	No
591	11.90	215.54	106.93	108.61	0.76	0.226	1.43	0.158	0.99	1.00	0.212	No
592	11.92	215.87	107.13	108.74	0.76	0.226	1.43	0.158	0.99	1.00	0.212	No
593	11.94	216.19	107.32	108.87	0.76	0.226	1.43	0.158	0.99	1.00	0.212	No
594	11.96	216.53	107.52	109.01	0.76	0.226	1.43	0.158	0.99	1.00	0.212	No
595	11.98	216.86	107.71	109.15	0.76	0.226	1.43	0.158	0.99	1.00	0.211	No
596	12.00	217.19	107.91	109.28	0.76	0.226	1.43	0.158	0.99	1.00	0.211	No
597	12.02	217.53	108.11	109.43	0.76	0.226	1.43	0.158	0.99	1.00	0.210	No
598	12.04	217.87	108.30	109.57	0.76	0.226	1.43	0.158	0.99	1.00	0.210	No
599	12.06	218.21	108.50	109.72	0.76	0.226	1.43	0.158	0.99	1.00	0.211	No
600	12.08	218.56	108.69	109.87	0.76	0.225	1.43	0.158	0.99	1.00	0.211	No
601	12.10	218.91	108.89	110.02	0.76	0.225	1.43	0.158	0.99	1.00	0.211	No
602	12.12	219.27	109.09	110.18	0.76	0.225	1.43	0.158	0.99	1.00	0.211	No
603	12.14	219.62	109.28	110.34	0.76	0.225	1.43	0.158	0.99	1.00	0.211	No
604	12.16	219.98	109.48	110.50	0.76	0.225	1.43	0.158	0.99	1.00	0.211	No
605	12.18	220.34	109.68	110.66	0.76	0.225	1.43	0.157	0.99	1.00	0.211	No
606	12.20	220.69	109.87	110.82	0.76	0.225	1.43	0.157	0.99	1.00	0.211	No
607	12.22	221.04	110.07	110.97	0.75	0.225	1.43	0.157	0.99	1.00	0.211	No
608	12.24	221.39	110.26	111.13	0.75	0.225	1.43	0.157	0.99	1.00	0.211	No
609	12.26	221.74	110.46	111.28	0.75	0.225	1.43	0.157	0.99	1.00	0.210	No
610	12.28	222.09	110.66	111.43	0.75	0.224	1.43	0.157	0.99	1.00	0.210	No
611	12.30	222.43	110.85	111.58	0.75	0.224	1.43	0.157	0.99	1.00	0.210	No
612	12.32	222.78	111.05	111.73	0.75	0.224	1.43	0.157	0.99	1.00	0.210	No
613	12.34	223.13	111.25	111.88	0.75	0.224	1.43	0.157	0.99	1.00	0.210	No
614	12.36	223.48	111.44	112.04	0.75	0.224	1.43	0.157	0.99	1.00	0.210	No
615	12.38	223.83	111.64	112.19	0.75	0.224	1.43	0.157	0.99	1.00	0.210	No
616	12.40	224.18	111.83	112.35	0.75	0.224	1.43	0.157	0.99	1.00	0.209	No
617	12.42	224.54	112.03	112.50	0.75	0.224	1.43	0.157	0.99	1.00	0.209	No
618	12.44	224.89	112.23	112.66	0.75	0.224	1.43	0.157	0.99	1.00	0.209	No
619	12.46	225.25	112.42	112.82	0.75	0.224	1.43	0.157	0.99	1.00	0.209	No
620	12.48	225.60	112.62	112.98	0.75	0.224	1.43	0.156	0.99	1.00	0.209	No
621	12.51	226.14	112.91	113.23	0.75	0.223	1.43	0.156	0.99	1.00	0.209	No
622	12.52	226.32	113.01	113.31	0.75	0.223	1.43	0.156	0.99	1.00	0.209	No
623	12.54	226.69	113.21	113.48	0.75	0.223	1.43	0.156	0.99	1.00	0.209	No
624	12.56	227.05	113.40	113.65	0.75	0.223	1.43	0.156	0.99	1.00	0.209	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
625	12.58	227.42	113.60	113.82	0.75	0.223	1.43	0.156	0.99	1.00	0.209	No
626	12.60	227.78	113.80	113.99	0.75	0.223	1.43	0.156	0.99	1.00	0.209	No
627	12.62	228.15	113.99	114.16	0.75	0.223	1.43	0.156	0.99	1.00	0.209	No
628	12.64	228.52	114.19	114.33	0.74	0.223	1.43	0.156	0.99	1.00	0.209	No
629	12.66	228.89	114.38	114.51	0.74	0.222	1.43	0.156	0.99	1.00	0.209	No
630	12.68	229.26	114.58	114.68	0.74	0.222	1.43	0.156	0.99	1.00	0.208	No
631	12.70	229.63	114.78	114.85	0.74	0.222	1.43	0.156	0.99	1.00	0.208	No
632	12.72	229.99	114.97	115.02	0.74	0.222	1.43	0.155	0.99	1.00	0.208	No
633	12.75	230.54	115.27	115.28	0.74	0.222	1.43	0.155	0.99	1.00	0.208	No
634	12.76	230.73	115.37	115.36	0.74	0.222	1.43	0.155	0.99	1.00	0.208	No
635	12.78	231.09	115.56	115.53	0.74	0.222	1.43	0.155	0.99	1.00	0.208	No
636	12.80	231.46	115.76	115.70	0.74	0.222	1.43	0.155	0.99	1.00	0.208	No
637	12.82	231.83	115.95	115.87	0.74	0.222	1.43	0.155	0.99	1.00	0.208	No
638	12.84	232.19	116.15	116.04	0.74	0.221	1.43	0.155	0.99	1.00	0.208	No
639	12.86	232.56	116.35	116.21	0.74	0.221	1.43	0.155	0.99	1.00	0.208	No
640	12.88	232.93	116.54	116.38	0.74	0.221	1.43	0.155	0.99	1.00	0.208	No
641	12.90	233.29	116.74	116.55	0.74	0.221	1.43	0.155	0.99	1.00	0.208	No
642	12.92	233.66	116.94	116.72	0.74	0.221	1.43	0.155	0.99	1.00	0.208	No
643	12.94	234.02	117.13	116.89	0.74	0.221	1.43	0.155	0.99	1.00	0.208	No
644	12.96	234.39	117.33	117.06	0.74	0.221	1.43	0.155	0.99	1.00	0.207	No
645	12.98	234.75	117.52	117.23	0.74	0.221	1.43	0.154	0.99	1.00	0.207	No
646	13.01	235.30	117.82	117.48	0.74	0.220	1.43	0.154	0.99	1.00	0.207	No
647	13.02	235.48	117.92	117.56	0.74	0.220	1.43	0.154	0.99	1.00	0.207	No
648	13.04	235.84	118.11	117.73	0.74	0.220	1.43	0.154	0.99	1.00	0.207	No
649	13.06	236.21	118.31	117.90	0.74	0.220	1.43	0.154	0.99	1.00	0.207	No
650	13.08	236.57	118.50	118.06	0.73	0.220	1.43	0.154	0.99	1.00	0.207	No
651	13.10	236.93	118.70	118.23	0.73	0.220	1.43	0.154	0.99	1.00	0.207	No
652	13.12	237.29	118.90	118.39	0.73	0.220	1.43	0.154	0.99	1.00	0.207	No
653	13.14	237.65	119.09	118.56	0.73	0.220	1.43	0.154	0.99	1.00	0.207	No
654	13.16	238.01	119.29	118.72	0.73	0.220	1.43	0.154	0.99	1.00	0.207	No
655	13.18	238.37	119.49	118.89	0.73	0.220	1.43	0.154	0.99	1.00	0.207	No
656	13.20	238.73	119.68	119.05	0.73	0.219	1.43	0.154	0.99	1.00	0.207	No
657	13.23	239.27	119.98	119.29	0.73	0.219	1.43	0.153	0.99	1.00	0.207	No
658	13.24	239.45	120.07	119.37	0.73	0.219	1.43	0.153	0.99	1.00	0.207	No
659	13.26	239.81	120.27	119.54	0.73	0.219	1.43	0.153	0.99	1.00	0.207	No
660	13.29	240.34	120.56	119.78	0.73	0.219	1.43	0.153	0.99	1.00	0.207	No
661	13.30	240.52	120.66	119.86	0.73	0.219	1.43	0.153	0.99	1.00	0.207	No
662	13.32	240.87	120.86	120.01	0.73	0.219	1.43	0.153	0.99	1.00	0.206	No
663	13.34	241.22	121.06	120.17	0.73	0.219	1.43	0.153	0.99	1.00	0.206	No
664	13.36	241.57	121.25	120.32	0.73	0.219	1.43	0.153	0.99	1.00	0.206	No
665	13.38	241.92	121.45	120.47	0.73	0.218	1.43	0.153	0.99	1.00	0.206	No
666	13.40	242.27	121.64	120.62	0.73	0.218	1.43	0.153	0.99	1.00	0.206	No
667	13.42	242.61	121.84	120.77	0.73	0.218	1.43	0.153	0.99	1.00	0.206	No
668	13.44	242.96	122.04	120.92	0.73	0.218	1.43	0.153	0.99	1.00	0.206	No
669	13.46	243.31	122.23	121.07	0.73	0.218	1.43	0.153	0.99	1.00	0.206	No
670	13.48	243.65	122.43	121.22	0.73	0.218	1.43	0.153	0.99	1.00	0.205	No
671	13.50	244.00	122.63	121.38	0.72	0.218	1.43	0.153	0.99	1.00	0.205	No
672	13.52	244.35	122.82	121.53	0.72	0.218	1.43	0.152	0.98	1.00	0.205	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
673	13.54	244.70	123.02	121.68	0.72	0.218	1.43	0.152	0.98	1.00	0.205	No
674	13.56	245.05	123.21	121.84	0.72	0.218	1.43	0.152	0.98	1.00	0.205	No
675	13.58	245.40	123.41	121.99	0.72	0.217	1.43	0.152	0.98	1.00	0.205	No
676	13.60	245.75	123.61	122.15	0.72	0.217	1.43	0.152	0.98	1.00	0.205	No
677	13.62	246.10	123.80	122.30	0.72	0.217	1.43	0.152	0.98	1.00	0.205	No
678	13.64	246.45	124.00	122.45	0.72	0.217	1.43	0.152	0.98	1.00	0.205	No
679	13.66	246.80	124.19	122.61	0.72	0.217	1.43	0.152	0.98	1.00	0.205	No
680	13.68	247.15	124.39	122.76	0.72	0.217	1.43	0.152	0.98	1.00	0.205	No
681	13.70	247.51	124.59	122.92	0.72	0.217	1.43	0.152	0.98	1.00	0.205	No
682	13.72	247.86	124.78	123.08	0.72	0.217	1.43	0.152	0.98	1.00	0.204	No
683	13.74	248.21	124.98	123.23	0.72	0.217	1.43	0.152	0.98	1.00	0.204	No
684	13.76	248.56	125.18	123.39	0.72	0.217	1.43	0.152	0.98	1.00	0.204	No
685	13.78	248.92	125.37	123.55	0.72	0.216	1.43	0.151	0.98	1.00	0.204	No
686	13.80	249.27	125.57	123.70	0.72	0.216	1.43	0.151	0.98	1.00	0.204	No
687	13.82	249.63	125.76	123.86	0.72	0.216	1.43	0.151	0.98	1.00	0.204	No
688	13.85	250.16	126.06	124.10	0.72	0.216	1.43	0.151	0.98	1.00	0.204	No
689	13.86	250.33	126.16	124.18	0.72	0.216	1.43	0.151	0.98	1.00	0.204	No
690	13.88	250.69	126.35	124.33	0.72	0.216	1.43	0.151	0.98	1.00	0.204	No
691	13.90	251.04	126.55	124.49	0.72	0.216	1.43	0.151	0.98	1.00	0.204	No
692	13.92	251.39	126.75	124.65	0.72	0.216	1.43	0.151	0.98	1.00	0.204	No
693	13.94	251.74	126.94	124.80	0.71	0.216	1.43	0.151	0.98	1.00	0.204	No
694	13.96	252.10	127.14	124.96	0.71	0.215	1.43	0.151	0.98	1.00	0.204	No
695	13.98	252.45	127.33	125.11	0.71	0.215	1.43	0.151	0.98	1.00	0.204	No
696	14.00	252.80	127.53	125.27	0.71	0.215	1.43	0.151	0.98	1.00	0.204	No
697	14.02	253.15	127.73	125.43	0.71	0.215	1.43	0.151	0.98	1.00	0.204	No
698	14.04	253.50	127.92	125.58	0.71	0.215	1.43	0.151	0.98	1.00	0.204	No
699	14.06	253.86	128.12	125.74	0.71	0.215	1.43	0.150	0.98	1.00	0.204	No
700	14.08	254.21	128.31	125.90	0.71	0.215	1.43	0.150	0.98	1.00	0.204	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (m)
σ_v: Total overburden pressure at test point (kPa)
u_0: Water pressure at test point (kPa)
σ_v': Effective overburden pressure based on GWT during earthquake (kPa)
r_d: Nonlinear shear mass factor
CSR: Cyclic Stress Ratio
MSF: Magnitude Scaling Factor
CSR_{eq}: CSR adjusted for M=7.5
K_σ: Effective overburden stress factor
CSR^*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1	0.02	0.84	92.31	2.87	0.57	1.70	13.75	0.00	13.75	4.000	No	Yes	2.00
2	0.04	0.88	94.47	2.89	0.57	1.70	14.69	0.00	14.69	4.000	No	Yes	2.00
3	0.06	0.89	95.88	2.91	0.57	1.70	14.85	0.00	14.85	4.000	No	Yes	2.00
4	0.08	0.90	98.89	2.95	0.56	1.70	15.13	0.00	15.13	4.000	No	Yes	2.00
5	0.10	0.93	100.00	2.98	0.56	1.70	15.38	0.00	15.38	4.000	No	Yes	2.00
6	0.12	0.92	100.00	3.03	0.56	1.70	16.16	0.00	16.16	4.000	No	Yes	2.00
7	0.14	0.89	100.00	3.09	0.56	1.70	14.87	0.00	14.87	4.000	No	Yes	2.00
8	0.16	0.85	100.00	3.14	0.57	1.70	13.82	0.00	13.82	4.000	No	Yes	2.00
9	0.18	0.85	100.00	3.15	0.57	1.70	14.22	0.00	14.22	4.000	No	Yes	2.00
10	0.20	0.87	100.00	3.13	0.56	1.70	14.59	0.00	14.59	4.000	No	Yes	2.00
11	0.22	0.89	100.00	3.11	0.56	1.70	15.08	0.00	15.08	4.000	No	Yes	2.00
12	0.24	0.91	100.00	3.09	0.56	1.70	15.30	0.00	15.30	4.000	No	Yes	2.00
13	0.30	0.92	100.00	3.09	0.56	1.70	15.55	0.00	15.55	4.000	No	Yes	2.00
14	0.30	0.90	100.00	3.11	0.56	1.70	15.55	0.00	15.55	4.000	No	Yes	2.00
15	0.30	0.87	100.00	3.14	0.57	1.70	14.09	0.00	14.09	4.000	No	Yes	2.00
16	0.32	0.84	100.00	3.17	0.57	1.70	14.15	0.00	14.15	4.000	No	Yes	2.00
17	0.34	0.83	100.00	3.19	0.57	1.70	14.05	0.00	14.05	4.000	No	Yes	2.00
18	0.36	0.82	100.00	3.21	0.57	1.70	13.80	0.00	13.80	4.000	No	Yes	2.00
19	0.38	0.79	100.00	3.23	0.57	1.70	13.42	0.00	13.42	4.000	No	Yes	2.00
20	0.40	0.77	100.00	3.25	0.57	1.70	12.77	0.00	12.77	4.000	No	Yes	2.00
21	0.42	0.74	100.00	3.26	0.57	1.70	12.55	0.00	12.55	4.000	No	Yes	2.00
22	0.44	0.72	100.00	3.28	0.57	1.70	12.02	0.00	12.02	4.000	No	Yes	2.00
23	0.46	0.68	100.00	3.30	0.58	1.70	11.61	0.00	11.61	4.000	No	Yes	2.00
24	0.48	0.65	100.00	3.32	0.58	1.70	10.92	0.00	10.92	4.000	No	Yes	2.00
25	0.50	0.63	100.00	3.33	0.58	1.70	10.38	0.00	10.38	4.000	No	Yes	2.00
26	0.52	0.61	100.00	3.33	0.58	1.70	10.36	0.00	10.36	4.000	No	Yes	2.00
27	0.54	0.60	100.00	3.33	0.58	1.70	9.82	0.00	9.82	4.000	No	Yes	2.00
28	0.56	0.59	100.00	3.32	0.58	1.70	9.96	0.00	9.96	4.000	No	Yes	2.00
29	0.58	0.60	100.00	3.31	0.58	1.70	10.12	0.00	10.12	4.000	No	Yes	2.00
30	0.60	0.58	100.00	3.31	0.58	1.70	9.97	0.00	9.97	4.000	No	Yes	2.00
31	0.62	0.56	100.00	3.33	0.58	1.70	9.36	0.00	9.36	4.000	No	Yes	2.00
32	0.64	0.56	100.00	3.33	0.59	1.70	8.94	0.00	8.94	4.000	No	Yes	2.00
33	0.66	0.57	100.00	3.31	0.58	1.70	9.76	0.00	9.76	4.000	No	Yes	2.00
34	0.68	0.62	100.00	3.26	0.58	1.70	10.28	0.00	10.28	4.000	No	Yes	2.00
35	0.70	0.65	100.00	3.22	0.58	1.70	11.06	0.00	11.06	4.000	No	Yes	2.00
36	0.72	0.69	100.00	3.18	0.58	1.70	11.46	0.00	11.46	4.000	No	Yes	2.00
37	0.74	0.73	100.00	3.14	0.57	1.70	12.21	0.00	12.21	4.000	No	Yes	2.00
38	0.76	0.78	100.00	3.11	0.57	1.70	13.11	0.00	13.11	4.000	No	Yes	2.00
39	0.78	0.83	100.00	3.07	0.57	1.70	13.85	0.00	13.85	4.000	No	Yes	2.00
40	0.80	0.87	100.00	3.06	0.56	1.70	14.72	0.00	14.72	4.000	No	Yes	2.00
41	0.82	0.89	100.00	3.06	0.56	1.70	15.07	0.00	15.07	4.000	No	Yes	2.00
42	0.84	0.90	100.00	3.08	0.56	1.70	15.24	0.00	15.24	4.000	No	Yes	2.00
43	0.87	0.89	100.00	3.11	0.56	1.70	14.81	0.00	14.81	4.000	No	Yes	2.00
44	0.88	0.87	100.00	3.14	0.57	1.70	14.57	0.00	14.57	4.000	No	Yes	2.00
45	0.90	0.86	100.00	3.16	0.57	1.70	14.49	0.00	14.49	4.000	No	Yes	2.00
46	0.92	0.86	100.00	3.17	0.57	1.70	14.44	0.00	14.44	4.000	No	Yes	2.00
47	0.94	0.85	100.00	3.18	0.57	1.70	14.40	0.00	14.40	4.000	No	Yes	2.00
48	0.96	0.84	100.00	3.20	0.57	1.70	14.07	0.00	14.07	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
49	0.99	0.81	100.00	3.21	0.57	1.70	13.64	0.00	13.64	4.000	No	Yes	2.00
50	1.00	0.81	100.00	3.22	0.57	1.70	13.20	0.00	13.20	4.000	No	Yes	2.00
51	1.09	0.81	100.00	3.21	0.57	1.70	13.69	0.00	13.69	4.000	No	Yes	2.00
52	1.09	0.82	100.00	3.20	0.57	1.70	13.69	0.00	13.69	4.000	No	Yes	2.00
53	1.09	0.82	100.00	3.20	0.57	1.70	13.81	0.00	13.81	4.000	No	Yes	2.00
54	1.09	0.82	100.00	3.19	0.57	1.70	13.81	0.00	13.81	4.000	No	Yes	2.00
55	1.11	0.82	100.00	3.18	0.57	1.70	13.78	0.00	13.78	4.000	No	Yes	2.00
56	1.13	0.83	100.00	3.17	0.57	1.70	13.87	0.00	13.87	4.000	No	Yes	2.00
57	1.14	0.83	100.00	3.18	0.57	1.70	14.14	0.00	14.14	4.000	No	Yes	2.00
58	1.17	0.81	100.00	3.19	0.57	1.70	13.49	0.00	13.49	4.000	No	Yes	2.00
59	1.18	0.79	100.00	3.22	0.57	1.70	13.24	0.00	13.24	4.000	No	Yes	2.00
60	1.20	0.78	100.00	3.23	0.57	1.70	12.87	0.00	12.87	4.000	No	Yes	2.00
61	1.22	0.76	100.00	3.25	0.57	1.70	12.85	0.00	12.85	4.000	No	Yes	2.00
62	1.24	0.74	100.00	3.26	0.57	1.70	12.28	0.00	12.28	4.000	No	Yes	2.00
63	1.26	0.73	100.00	3.27	0.57	1.70	12.15	0.00	12.15	4.000	No	Yes	2.00
64	1.28	0.74	100.00	3.25	0.57	1.70	12.13	0.00	12.13	4.000	No	Yes	2.00
65	1.30	0.82	100.00	3.18	0.57	1.70	13.08	0.00	13.08	4.000	No	Yes	2.00
66	1.32	0.94	100.00	3.08	0.56	1.70	15.99	0.00	15.99	4.000	No	Yes	2.00
67	1.34	1.05	100.00	3.00	0.55	1.70	17.95	0.00	17.95	4.000	No	Yes	2.00
68	1.36	1.12	99.74	2.96	0.55	1.70	18.67	0.00	18.67	4.000	No	Yes	2.00
69	1.38	1.15	98.32	2.94	0.55	1.70	19.24	0.00	19.24	4.000	No	Yes	2.00
70	1.40	1.16	98.37	2.94	0.55	1.70	19.49	0.00	19.49	4.000	No	Yes	2.00
71	1.42	1.16	99.50	2.96	0.55	1.70	19.27	0.00	19.27	4.000	No	Yes	2.00
72	1.44	1.18	99.98	2.96	0.55	1.70	19.25	0.00	19.25	4.000	No	Yes	2.00
73	1.46	1.24	98.86	2.95	0.54	1.70	20.48	0.00	20.48	4.000	No	Yes	2.00
74	1.48	1.31	97.22	2.93	0.54	1.70	22.15	0.00	22.15	4.000	No	Yes	2.00
75	1.50	1.36	96.26	2.92	0.54	1.70	22.88	0.00	22.88	4.000	No	Yes	2.00
76	1.52	1.37	96.52	2.92	0.54	1.70	23.09	0.00	23.09	4.000	No	Yes	2.00
77	1.54	1.37	97.01	2.93	0.54	1.70	22.72	0.00	22.72	4.000	No	Yes	2.00
78	1.56	1.37	97.51	2.93	0.54	1.70	22.70	0.00	22.70	4.000	No	Yes	2.00
79	1.58	1.38	97.60	2.93	0.54	1.70	22.95	0.00	22.95	4.000	No	Yes	2.00
80	1.60	1.40	97.68	2.93	0.53	1.70	23.44	0.00	23.44	4.000	No	Yes	2.00
81	1.62	1.41	98.02	2.94	0.53	1.70	23.53	0.00	23.53	4.000	No	Yes	2.00
82	1.64	1.42	98.11	2.94	0.54	1.70	23.31	0.00	23.31	4.000	No	Yes	2.00
83	1.66	1.44	97.86	2.94	0.53	1.70	24.07	0.00	24.07	4.000	No	Yes	2.00
84	1.68	1.46	97.50	2.93	0.53	1.70	24.60	0.00	24.60	4.000	No	Yes	2.00
85	1.70	1.45	97.99	2.94	0.53	1.70	24.46	0.00	24.46	4.000	No	Yes	2.00
86	1.72	1.41	99.18	2.95	0.53	1.70	23.48	0.00	23.48	4.000	No	Yes	2.00
87	1.74	1.33	100.00	2.99	0.54	1.70	22.63	0.00	22.63	4.000	No	Yes	2.00
88	1.78	1.22	100.00	3.04	0.54	1.70	20.51	0.00	20.51	4.000	No	Yes	2.00
89	1.78	1.09	100.00	3.12	0.55	1.70	18.21	0.00	18.21	4.000	No	Yes	2.00
90	1.80	0.95	100.00	3.21	0.56	1.70	15.99	0.00	15.99	4.000	No	Yes	2.00
91	1.82	0.85	100.00	3.27	0.57	1.70	13.24	0.00	13.24	4.000	No	Yes	2.00
92	1.84	0.78	100.00	3.32	0.57	1.70	13.21	0.00	13.21	4.000	No	Yes	2.00
93	1.86	0.76	100.00	3.33	0.57	1.70	12.15	0.00	12.15	4.000	No	Yes	2.00
94	1.88	0.74	100.00	3.32	0.57	1.70	11.99	0.00	11.99	4.000	No	Yes	2.00
95	1.90	0.73	100.00	3.29	0.58	1.70	11.71	0.00	11.71	4.000	No	Yes	2.00
96	1.92	0.73	100.00	3.26	0.58	1.70	11.78	0.00	11.78	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
97	1.94	0.72	100.00	3.22	0.58	1.70	11.69	0.00	11.69	4.000	No	Yes	2.00
98	1.96	0.72	100.00	3.18	0.58	1.70	11.53	0.00	11.53	4.000	No	Yes	2.00
99	1.98	0.73	100.00	3.13	0.58	1.70	11.48	0.00	11.48	4.000	No	Yes	2.00
100	2.00	0.74	100.00	3.09	0.57	1.70	12.25	0.00	12.25	4.000	No	Yes	2.00
101	2.08	0.76	100.00	3.07	0.57	1.70	12.29	0.00	12.29	4.000	No	Yes	2.00
102	2.08	0.76	100.00	3.06	0.57	1.70	12.29	0.00	12.29	4.000	No	Yes	2.00
103	2.08	0.85	100.00	2.99	0.57	1.70	12.29	0.00	12.29	4.000	No	Yes	2.00
104	2.10	0.96	95.99	2.91	0.56	1.70	16.43	0.00	16.43	4.000	No	Yes	2.00
105	2.12	1.12	88.79	2.82	0.56	1.70	17.87	0.00	17.87	4.000	No	Yes	2.00
106	2.14	1.22	85.83	2.79	0.55	1.70	20.10	0.00	20.10	4.000	No	Yes	2.00
107	2.16	1.31	83.83	2.76	0.54	1.70	21.54	0.00	21.54	4.000	No	Yes	2.00
108	2.18	1.39	82.33	2.74	0.54	1.69	22.46	0.00	22.46	4.000	No	Yes	2.00
109	2.20	1.47	81.15	2.73	0.54	1.67	23.91	0.00	23.91	4.000	No	Yes	2.00
110	2.22	1.55	79.88	2.71	0.53	1.66	25.38	0.00	25.38	4.000	No	Yes	2.00
111	2.24	1.60	81.20	2.73	0.53	1.65	26.41	0.00	26.41	4.000	No	Yes	2.00
112	2.26	1.58	84.47	2.77	0.53	1.65	25.83	0.00	25.83	4.000	No	Yes	2.00
113	2.28	1.51	89.85	2.84	0.53	1.65	24.45	0.00	24.45	4.000	No	Yes	2.00
114	2.30	1.43	95.32	2.90	0.54	1.65	22.72	0.00	22.72	4.000	No	Yes	2.00
115	2.32	1.35	100.00	2.97	0.54	1.65	21.92	0.00	21.92	4.000	No	Yes	2.00
116	2.34	1.31	100.00	3.01	0.54	1.65	20.81	0.00	20.81	4.000	No	Yes	2.00
117	2.36	1.32	100.00	3.01	0.54	1.65	20.58	0.00	20.58	4.000	No	Yes	2.00
118	2.38	1.36	100.00	2.99	0.54	1.64	21.84	0.00	21.84	4.000	No	Yes	2.00
119	2.40	1.42	99.13	2.95	0.54	1.63	22.24	0.00	22.24	4.000	No	Yes	2.00
120	2.42	1.46	96.37	2.92	0.54	1.63	23.11	0.00	23.11	4.000	No	Yes	2.00
121	2.44	1.50	93.74	2.88	0.53	1.62	23.65	0.00	23.65	4.000	No	Yes	2.00
122	2.46	1.52	91.68	2.86	0.53	1.62	23.91	0.00	23.91	4.000	No	Yes	2.00
123	2.48	1.53	90.94	2.85	0.53	1.61	24.03	0.00	24.03	4.000	No	Yes	2.00
124	2.50	1.52	91.33	2.85	0.54	1.61	23.78	0.00	23.78	4.000	No	Yes	2.00
125	2.52	1.49	93.41	2.88	0.54	1.61	23.35	0.00	23.35	4.000	No	Yes	2.00
126	2.54	1.48	95.04	2.90	0.54	1.61	22.79	0.00	22.79	4.000	No	Yes	2.00
127	2.56	1.49	95.05	2.90	0.54	1.60	22.92	0.00	22.92	4.000	No	Yes	2.00
128	2.58	1.53	93.26	2.88	0.54	1.60	23.63	0.00	23.63	4.000	No	Yes	2.00
129	2.60	1.57	91.68	2.86	0.53	1.59	24.43	0.00	24.43	4.000	No	Yes	2.00
130	2.62	1.57	91.47	2.86	0.53	1.59	24.54	0.00	24.54	4.000	No	Yes	2.00
131	2.64	1.55	91.97	2.86	0.53	1.59	23.81	0.00	23.81	4.000	No	Yes	2.00
132	2.66	1.52	92.98	2.87	0.54	1.58	23.46	0.00	23.46	4.000	No	Yes	2.00
133	2.68	1.49	94.74	2.90	0.54	1.58	23.00	0.00	23.00	4.000	No	Yes	2.00
134	2.70	1.47	97.08	2.93	0.54	1.58	22.41	0.00	22.41	4.000	No	Yes	2.00
135	2.72	1.48	98.15	2.94	0.54	1.58	22.16	0.00	22.16	4.000	No	Yes	2.00
136	2.74	1.50	97.96	2.94	0.54	1.57	23.16	0.00	23.16	4.000	No	Yes	2.00
137	2.76	1.54	96.78	2.92	0.53	1.57	23.41	0.00	23.41	4.000	No	Yes	2.00
138	2.78	1.55	96.42	2.92	0.53	1.56	23.83	0.00	23.83	4.000	No	Yes	2.00
139	2.81	1.56	96.28	2.92	0.53	1.56	23.50	0.00	23.50	4.000	No	Yes	2.00
140	2.82	1.53	97.16	2.93	0.53	1.56	23.41	0.00	23.41	4.000	No	Yes	2.00
141	2.84	1.50	98.65	2.95	0.54	1.56	22.64	0.00	22.64	4.000	No	Yes	2.00
142	2.86	1.46	100.00	2.96	0.54	1.56	21.88	0.00	21.88	4.000	No	Yes	2.00
143	2.88	1.46	100.00	2.97	0.54	1.55	21.79	0.00	21.79	4.000	No	Yes	2.00
144	2.90	1.48	100.00	2.96	0.54	1.55	22.25	0.00	22.25	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
145	2.92	1.51	98.97	2.95	0.54	1.54	22.54	0.00	22.54	4.000	No	Yes	2.00
146	2.94	1.53	97.64	2.93	0.54	1.54	23.00	0.00	23.00	4.000	No	Yes	2.00
147	2.96	1.55	95.96	2.91	0.54	1.54	23.05	0.00	23.05	4.000	No	Yes	2.00
148	2.98	1.56	94.60	2.90	0.54	1.53	23.29	0.00	23.29	4.000	No	Yes	2.00
149	3.00	1.56	94.05	2.89	0.54	1.53	23.37	0.00	23.37	4.000	No	Yes	2.00
150	3.02	1.54	94.62	2.90	0.54	1.53	22.95	0.00	22.95	4.000	No	Yes	2.00
151	3.04	1.49	96.32	2.92	0.54	1.53	22.11	0.00	22.11	4.000	No	Yes	2.00
152	3.06	1.42	98.86	2.95	0.54	1.53	21.21	0.00	21.21	4.000	No	Yes	2.00
153	3.08	1.33	100.00	3.00	0.55	1.53	19.95	0.00	19.95	4.000	No	Yes	2.00
154	3.10	1.22	100.00	3.05	0.55	1.54	17.80	0.00	17.80	4.000	No	Yes	2.00
155	3.12	1.13	100.00	3.10	0.56	1.54	16.73	0.00	16.73	4.000	No	Yes	2.00
156	3.14	1.06	100.00	3.13	0.56	1.54	15.61	0.00	15.61	4.000	No	Yes	2.00
157	3.16	1.03	100.00	3.14	0.56	1.54	14.95	0.00	14.95	4.000	No	Yes	2.00
158	3.18	1.03	100.00	3.13	0.56	1.53	15.04	0.00	15.04	4.000	No	Yes	2.00
159	3.20	1.04	100.00	3.10	0.56	1.53	15.37	0.00	15.37	4.000	No	Yes	2.00
160	3.22	1.04	100.00	3.08	0.56	1.53	15.29	0.00	15.29	4.000	No	Yes	2.00
161	3.24	1.01	100.00	3.07	0.56	1.53	14.84	0.00	14.84	4.000	No	Yes	2.00
162	3.26	0.99	100.00	3.06	0.57	1.53	14.03	0.00	14.03	4.000	No	Yes	2.00
163	3.28	0.99	100.00	3.03	0.57	1.52	14.30	0.00	14.30	4.000	No	Yes	2.00
164	3.30	1.04	100.00	2.99	0.56	1.52	14.67	0.00	14.67	4.000	No	Yes	2.00
165	3.32	1.12	98.37	2.94	0.56	1.51	16.24	0.00	16.24	4.000	No	Yes	2.00
166	3.34	1.21	94.12	2.89	0.56	1.51	17.05	0.00	17.05	4.000	No	Yes	2.00
167	3.36	1.30	90.36	2.84	0.55	1.50	18.69	0.00	18.69	4.000	No	Yes	2.00
168	3.38	1.38	87.90	2.81	0.55	1.49	20.11	0.00	20.11	4.000	No	Yes	2.00
169	3.40	1.41	87.44	2.81	0.55	1.49	20.40	0.00	20.40	4.000	No	Yes	2.00
170	3.42	1.42	87.63	2.81	0.55	1.48	20.13	0.00	20.13	4.000	No	Yes	2.00
171	3.44	1.45	87.25	2.80	0.55	1.48	20.65	0.00	20.65	4.000	No	Yes	2.00
172	3.46	1.46	87.98	2.81	0.54	1.47	21.39	0.00	21.39	4.000	No	Yes	2.00
173	3.48	1.45	89.76	2.83	0.55	1.48	20.36	0.00	20.36	4.000	No	Yes	2.00
174	3.50	1.39	93.29	2.88	0.55	1.47	20.18	0.00	20.18	4.000	No	Yes	2.00
175	3.52	1.35	96.20	2.92	0.55	1.47	18.95	0.00	18.95	4.000	No	Yes	2.00
176	3.54	1.30	98.59	2.94	0.55	1.47	18.39	0.00	18.39	4.000	No	Yes	2.00
177	3.56	1.30	99.15	2.95	0.55	1.47	18.28	0.00	18.28	4.000	No	Yes	2.00
178	3.58	1.31	98.52	2.94	0.55	1.47	18.51	0.00	18.51	4.000	No	Yes	2.00
179	3.60	1.33	97.86	2.94	0.55	1.46	19.03	0.00	19.03	4.000	No	Yes	2.00
180	3.63	1.31	98.39	2.94	0.55	1.46	18.91	0.00	18.91	4.000	No	Yes	2.00
181	3.64	1.28	99.47	2.96	0.55	1.46	17.98	0.00	17.98	4.000	No	Yes	2.00
182	3.66	1.25	100.00	2.97	0.55	1.46	17.84	0.00	17.84	4.000	No	Yes	2.00
183	3.68	1.24	100.00	2.98	0.55	1.46	17.48	0.00	17.48	4.000	No	Yes	2.00
184	3.70	1.24	100.00	2.98	0.55	1.45	17.41	0.00	17.41	4.000	No	Yes	2.00
185	3.72	1.24	100.00	2.99	0.55	1.45	17.60	0.00	17.60	4.000	No	Yes	2.00
186	3.74	1.24	100.00	2.98	0.56	1.45	17.18	0.00	17.18	4.000	No	Yes	2.00
187	3.76	1.28	99.83	2.96	0.55	1.45	17.66	0.00	17.66	4.000	No	Yes	2.00
188	3.78	1.39	94.96	2.90	0.55	1.44	19.07	0.00	19.07	4.000	No	Yes	2.00
189	3.80	1.52	90.12	2.84	0.54	1.43	21.42	0.00	21.42	4.000	No	Yes	2.00
190	3.82	1.62	86.95	2.80	0.54	1.43	22.54	0.00	22.54	4.000	No	Yes	2.00
191	3.84	1.65	86.51	2.79	0.54	1.42	23.13	0.00	23.13	4.000	No	Yes	2.00
192	3.86	1.61	89.28	2.83	0.54	1.42	22.83	0.00	22.83	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
193	3.88	1.52	92.97	2.87	0.55	1.42	20.67	0.00	20.67	4.000	No	Yes	2.00
194	3.90	1.41	98.22	2.94	0.55	1.42	19.80	0.00	19.80	4.000	No	Yes	2.00
195	3.92	1.29	100.00	3.01	0.55	1.42	17.92	0.00	17.92	4.000	No	Yes	2.00
196	3.94	1.15	100.00	3.09	0.56	1.43	15.84	0.00	15.84	4.000	No	Yes	2.00
197	3.96	1.04	100.00	3.17	0.57	1.43	13.99	0.00	13.99	4.000	No	Yes	2.00
198	3.98	0.97	100.00	3.21	0.57	1.43	13.17	0.00	13.17	4.000	No	Yes	2.00
199	4.00	0.96	100.00	3.21	0.57	1.43	12.79	0.00	12.79	4.000	No	Yes	2.00
200	4.02	0.98	100.00	3.19	0.57	1.43	12.86	0.00	12.86	4.000	No	Yes	2.00
201	4.04	1.01	100.00	3.14	0.57	1.42	13.49	0.00	13.49	4.000	No	Yes	2.00
202	4.07	1.05	100.00	3.09	0.57	1.42	13.68	0.00	13.68	4.000	No	Yes	2.00
203	4.08	1.09	100.00	3.03	0.57	1.42	14.29	0.00	14.29	4.000	No	Yes	2.00
204	4.10	1.13	100.00	2.98	0.56	1.41	15.26	0.00	15.26	4.000	No	Yes	2.00
205	4.12	1.17	97.81	2.94	0.56	1.41	15.78	0.00	15.78	4.000	No	Yes	2.00
206	4.14	1.20	95.84	2.91	0.56	1.40	16.16	0.00	16.16	4.000	No	Yes	2.00
207	4.26	1.22	94.89	2.90	0.56	1.39	16.32	0.00	16.32	4.000	No	Yes	2.00
208	4.26	1.22	94.64	2.90	0.56	1.39	16.32	0.00	16.32	4.000	No	Yes	2.00
209	4.26	1.22	94.71	2.90	0.56	1.39	16.29	0.00	16.29	4.000	No	Yes	2.00
210	4.26	1.23	98.77	2.95	0.56	1.39	16.28	0.00	16.28	4.000	No	Yes	2.00
211	4.26	1.22	100.00	3.00	0.56	1.39	16.46	0.00	16.46	4.000	No	Yes	2.00
212	4.28	1.20	100.00	3.05	0.56	1.39	16.17	0.00	16.17	4.000	No	Yes	2.00
213	4.30	1.17	100.00	3.08	0.56	1.39	15.45	0.00	15.45	4.000	No	Yes	2.00
214	4.32	1.14	100.00	3.10	0.56	1.39	14.95	0.00	14.95	4.000	No	Yes	2.00
215	4.34	1.11	100.00	3.10	0.56	1.39	14.76	0.00	14.76	4.000	No	Yes	2.00
216	4.36	1.11	100.00	3.10	0.57	1.38	14.36	0.00	14.36	4.000	No	Yes	2.00
217	4.38	1.12	100.00	3.09	0.57	1.38	14.33	0.00	14.33	4.000	No	Yes	2.00
218	4.40	1.16	100.00	3.06	0.56	1.38	14.85	0.00	14.85	4.000	No	Yes	2.00
219	4.42	1.23	100.00	3.01	0.56	1.37	15.66	0.00	15.66	4.000	No	Yes	2.00
220	4.44	1.33	98.42	2.94	0.56	1.37	17.14	0.00	17.14	4.000	No	Yes	2.00
221	4.46	1.44	93.25	2.88	0.55	1.36	18.71	0.00	18.71	4.000	No	Yes	2.00
222	4.48	1.51	90.64	2.85	0.55	1.36	20.17	0.00	20.17	4.000	No	Yes	2.00
223	4.50	1.53	90.47	2.84	0.55	1.36	19.91	0.00	19.91	4.000	No	Yes	2.00
224	4.52	1.50	91.97	2.86	0.55	1.35	19.56	0.00	19.56	4.000	No	Yes	2.00
225	4.54	1.45	95.16	2.90	0.55	1.35	19.52	0.00	19.52	4.000	No	Yes	2.00
226	4.56	1.37	99.79	2.96	0.55	1.35	17.87	0.00	17.87	4.000	No	Yes	2.00
227	4.58	1.28	100.00	3.03	0.56	1.35	16.71	0.00	16.71	4.000	No	Yes	2.00
228	4.60	1.24	100.00	3.07	0.56	1.35	16.19	0.00	16.19	4.000	No	Yes	2.00
229	4.62	1.22	100.00	3.09	0.56	1.35	15.95	0.00	15.95	4.000	No	Yes	2.00
230	4.64	1.22	100.00	3.10	0.56	1.35	15.82	0.00	15.82	4.000	No	Yes	2.00
231	4.66	1.23	100.00	3.10	0.56	1.35	15.73	0.00	15.73	4.000	No	Yes	2.00
232	4.68	1.23	100.00	3.09	0.56	1.34	16.06	0.00	16.06	4.000	No	Yes	2.00
233	4.70	1.23	100.00	3.09	0.56	1.34	15.84	0.00	15.84	4.000	No	Yes	2.00
234	4.72	1.23	100.00	3.08	0.56	1.34	15.60	0.00	15.60	4.000	No	Yes	2.00
235	4.74	1.24	100.00	3.07	0.56	1.34	15.90	0.00	15.90	4.000	No	Yes	2.00
236	4.76	1.26	100.00	3.05	0.56	1.34	15.93	0.00	15.93	4.000	No	Yes	2.00
237	4.78	1.28	100.00	3.03	0.56	1.33	16.03	0.00	16.03	4.000	No	Yes	2.00
238	4.80	1.30	100.00	3.01	0.56	1.33	16.40	0.00	16.40	4.000	No	Yes	2.00
239	4.82	1.31	100.00	3.01	0.56	1.33	16.77	0.00	16.77	4.000	No	Yes	2.00
240	4.84	1.32	100.00	3.01	0.56	1.33	16.68	0.00	16.68	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
241	4.86	1.31	100.00	3.01	0.56	1.32	16.54	0.00	16.54	4.000	No	Yes	2.00
242	4.88	1.30	100.00	3.02	0.56	1.32	16.48	0.00	16.48	4.000	No	Yes	2.00
243	4.90	1.29	100.00	3.03	0.56	1.32	16.22	0.00	16.22	4.000	No	Yes	2.00
244	4.92	1.27	100.00	3.05	0.56	1.32	15.86	0.00	15.86	4.000	No	Yes	2.00
245	4.94	1.23	100.00	3.07	0.56	1.32	15.66	0.00	15.66	4.000	No	Yes	2.00
246	4.96	1.19	100.00	3.09	0.56	1.32	14.98	0.00	14.98	4.000	No	Yes	2.00
247	4.98	1.15	100.00	3.11	0.57	1.32	14.47	0.00	14.47	4.000	No	Yes	2.00
248	5.01	1.11	100.00	3.13	0.57	1.31	14.31	0.00	14.31	4.000	No	Yes	2.00
249	5.02	1.06	100.00	3.15	0.57	1.31	13.49	0.00	13.49	4.000	No	Yes	2.00
250	5.04	1.01	100.00	3.17	0.57	1.31	12.79	0.00	12.79	4.000	No	Yes	2.00
251	5.06	0.96	100.00	3.20	0.57	1.31	12.26	0.00	12.26	4.000	No	Yes	2.00
252	5.08	0.93	100.00	3.22	0.58	1.31	11.56	0.00	11.56	4.000	No	Yes	2.00
253	5.10	0.89	100.00	3.24	0.58	1.31	11.21	0.00	11.21	4.000	No	Yes	2.00
254	5.12	0.87	100.00	3.26	0.58	1.31	10.54	0.00	10.54	4.000	No	Yes	2.00
255	5.14	0.83	100.00	3.28	0.58	1.31	10.17	0.00	10.17	4.000	No	Yes	2.00
256	5.16	0.80	100.00	3.28	0.58	1.31	9.64	0.00	9.64	4.000	No	Yes	2.00
257	5.18	0.78	100.00	3.27	0.58	1.31	9.39	0.00	9.39	4.000	No	Yes	2.00
258	5.20	0.78	100.00	3.25	0.58	1.31	9.31	0.00	9.31	4.000	No	Yes	2.00
259	5.22	0.79	100.00	3.21	0.58	1.30	9.59	0.00	9.59	4.000	No	Yes	2.00
260	5.24	0.81	100.00	3.17	0.58	1.30	9.61	0.00	9.61	4.000	No	Yes	2.00
261	5.26	0.83	100.00	3.14	0.58	1.30	9.86	0.00	9.86	4.000	No	Yes	2.00
262	5.28	0.88	100.00	3.09	0.58	1.30	10.22	0.00	10.22	4.000	No	Yes	2.00
263	5.30	0.94	100.00	3.03	0.58	1.29	11.29	0.00	11.29	4.000	No	Yes	2.00
264	5.32	1.01	100.00	2.97	0.57	1.29	12.12	0.00	12.12	4.000	No	Yes	2.00
265	5.34	1.04	98.34	2.94	0.57	1.29	12.80	0.00	12.80	4.000	No	Yes	2.00
266	5.36	1.03	99.58	2.96	0.57	1.29	12.64	0.00	12.64	4.000	No	Yes	2.00
267	5.38	1.01	100.00	3.00	0.57	1.29	12.11	0.00	12.11	4.000	No	Yes	2.00
268	5.40	1.01	100.00	3.02	0.57	1.28	11.92	0.00	11.92	4.000	No	Yes	2.00
269	5.42	1.06	100.00	3.01	0.57	1.28	12.49	0.00	12.49	4.000	No	Yes	2.00
270	5.44	1.11	100.00	2.98	0.57	1.28	13.34	0.00	13.34	4.000	No	Yes	2.00
271	5.46	1.16	100.00	2.96	0.57	1.27	13.96	0.00	13.96	4.000	No	Yes	2.00
272	5.48	1.20	99.11	2.95	0.57	1.27	14.59	0.00	14.59	4.000	No	Yes	2.00
273	5.50	1.22	98.32	2.94	0.56	1.27	14.80	0.00	14.80	4.000	No	Yes	2.00
274	5.52	1.27	96.96	2.92	0.56	1.27	15.07	0.00	15.07	4.000	No	Yes	2.00
275	5.54	1.32	95.44	2.91	0.56	1.26	15.98	0.00	15.98	4.000	No	Yes	2.00
276	5.56	1.39	93.95	2.89	0.56	1.26	16.68	0.00	16.68	4.000	No	Yes	2.00
277	5.58	1.44	93.84	2.89	0.56	1.26	17.46	0.00	17.46	4.000	No	Yes	2.00
278	5.60	1.48	94.15	2.89	0.55	1.26	17.86	0.00	17.86	4.000	No	Yes	2.00
279	5.62	1.50	94.74	2.90	0.55	1.25	18.35	0.00	18.35	4.000	No	Yes	2.00
280	5.64	1.52	95.58	2.91	0.55	1.25	18.55	0.00	18.55	4.000	No	Yes	2.00
281	5.66	1.53	96.22	2.92	0.55	1.25	18.36	0.00	18.36	4.000	No	Yes	2.00
282	5.68	1.56	96.66	2.92	0.55	1.25	18.84	0.00	18.84	4.000	No	Yes	2.00
283	5.70	1.60	96.44	2.92	0.55	1.24	19.40	0.00	19.40	4.000	No	Yes	2.00
284	5.72	1.65	95.82	2.91	0.55	1.24	19.69	0.00	19.69	4.000	No	Yes	2.00
285	5.74	1.68	95.48	2.91	0.55	1.24	20.53	0.00	20.53	4.000	No	Yes	2.00
286	5.76	1.68	96.37	2.92	0.54	1.24	20.64	0.00	20.64	4.000	No	Yes	2.00
287	5.78	1.64	98.62	2.95	0.55	1.24	19.64	0.00	19.64	4.000	No	Yes	2.00
288	5.80	1.56	100.00	2.99	0.55	1.24	19.00	0.00	19.00	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
289	5.82	1.51	100.00	3.02	0.55	1.24	17.97	0.00	17.97	4.000	No	Yes	2.00
290	5.84	1.47	100.00	3.05	0.55	1.24	17.72	0.00	17.72	4.000	No	Yes	2.00
291	5.86	1.46	100.00	3.06	0.55	1.23	17.50	0.00	17.50	4.000	No	Yes	2.00
292	5.88	1.45	100.00	3.06	0.55	1.23	17.52	0.00	17.52	4.000	No	Yes	2.00
293	5.90	1.42	100.00	3.06	0.56	1.23	17.05	0.00	17.05	4.000	No	Yes	2.00
294	5.92	1.38	100.00	3.06	0.56	1.23	16.57	0.00	16.57	4.000	No	Yes	2.00
295	5.94	1.36	100.00	3.06	0.56	1.23	16.04	0.00	16.04	4.000	No	Yes	2.00
296	5.97	1.35	100.00	3.06	0.56	1.23	16.14	0.00	16.14	4.000	No	Yes	2.00
297	5.98	1.36	100.00	3.04	0.56	1.23	15.92	0.00	15.92	4.000	No	Yes	2.00
298	6.00	1.37	100.00	3.03	0.56	1.22	15.98	0.00	15.98	4.000	No	Yes	2.00
299	6.02	1.42	100.00	3.01	0.56	1.22	16.42	0.00	16.42	4.000	No	Yes	2.00
300	6.04	1.48	100.00	2.98	0.55	1.22	17.38	0.00	17.38	4.000	No	Yes	2.00
301	6.06	1.53	99.05	2.95	0.55	1.22	17.71	0.00	17.71	4.000	No	Yes	2.00
302	6.08	1.54	97.85	2.94	0.55	1.21	18.10	0.00	18.10	4.000	No	Yes	2.00
303	6.10	1.53	97.87	2.94	0.55	1.21	18.13	0.00	18.13	4.000	No	Yes	2.00
304	6.12	1.50	98.99	2.95	0.55	1.21	17.54	0.00	17.54	4.000	No	Yes	2.00
305	6.14	1.47	100.00	2.97	0.56	1.21	17.27	0.00	17.27	4.000	No	Yes	2.00
306	6.16	1.45	100.00	3.01	0.56	1.21	17.15	0.00	17.15	4.000	No	Yes	2.00
307	6.18	1.43	100.00	3.03	0.56	1.21	16.58	0.00	16.58	4.000	No	Yes	2.00
308	6.20	1.40	100.00	3.06	0.56	1.21	16.61	0.00	16.61	4.000	No	Yes	2.00
309	6.22	1.39	100.00	3.08	0.56	1.21	16.33	0.00	16.33	4.000	No	Yes	2.00
310	6.24	1.37	100.00	3.10	0.56	1.20	16.14	0.00	16.14	4.000	No	Yes	2.00
311	6.26	1.35	100.00	3.12	0.56	1.20	15.57	0.00	15.57	4.000	No	Yes	2.00
312	6.28	1.35	100.00	3.12	0.56	1.20	15.57	0.00	15.57	4.000	No	Yes	2.00
313	6.30	1.37	100.00	3.10	0.56	1.20	16.01	0.00	16.01	4.000	No	Yes	2.00
314	6.32	1.41	100.00	3.08	0.56	1.20	16.28	0.00	16.28	4.000	No	Yes	2.00
315	6.34	1.45	100.00	3.06	0.56	1.20	16.50	0.00	16.50	4.000	No	Yes	2.00
316	6.36	1.49	100.00	3.03	0.56	1.19	17.29	0.00	17.29	4.000	No	Yes	2.00
317	6.38	1.54	100.00	3.00	0.55	1.19	17.72	0.00	17.72	4.000	No	Yes	2.00
318	6.41	1.57	100.00	2.98	0.55	1.19	18.28	0.00	18.28	4.000	No	Yes	2.00
319	6.42	1.59	100.00	2.97	0.55	1.19	18.21	0.00	18.21	4.000	No	Yes	2.00
320	6.44	1.58	100.00	2.98	0.55	1.19	18.26	0.00	18.26	4.000	No	Yes	2.00
321	6.46	1.58	100.00	2.99	0.55	1.18	18.10	0.00	18.10	4.000	No	Yes	2.00
322	6.48	1.58	100.00	3.00	0.55	1.18	18.09	0.00	18.09	4.000	No	Yes	2.00
323	6.50	1.59	100.00	3.01	0.55	1.18	18.20	0.00	18.20	4.000	No	Yes	2.00
324	6.52	1.60	100.00	3.01	0.55	1.18	18.34	0.00	18.34	4.000	No	Yes	2.00
325	6.54	1.60	100.00	3.02	0.55	1.18	18.39	0.00	18.39	4.000	No	Yes	2.00
326	6.56	1.59	100.00	3.03	0.55	1.18	18.47	0.00	18.47	4.000	No	Yes	2.00
327	6.58	1.56	100.00	3.05	0.55	1.18	17.96	0.00	17.96	4.000	No	Yes	2.00
328	6.60	1.49	100.00	3.08	0.56	1.18	17.10	0.00	17.10	4.000	No	Yes	2.00
329	6.62	1.43	100.00	3.11	0.56	1.17	16.37	0.00	16.37	4.000	No	Yes	2.00
330	6.64	1.36	100.00	3.16	0.56	1.17	15.84	0.00	15.84	4.000	No	Yes	2.00
331	6.66	1.28	100.00	3.20	0.57	1.17	14.55	0.00	14.55	4.000	No	Yes	2.00
332	6.68	1.20	100.00	3.25	0.57	1.17	13.56	0.00	13.56	4.000	No	Yes	2.00
333	6.70	1.14	100.00	3.29	0.57	1.17	13.00	0.00	13.00	4.000	No	Yes	2.00
334	6.72	1.11	100.00	3.30	0.57	1.17	12.68	0.00	12.68	4.000	No	Yes	2.00
335	6.74	1.08	100.00	3.30	0.57	1.17	12.39	0.00	12.39	4.000	No	Yes	2.00
336	6.76	1.08	100.00	3.28	0.58	1.17	11.76	0.00	11.76	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
337	6.78	1.10	100.00	3.23	0.57	1.17	12.36	0.00	12.36	4.000	No	Yes	2.00
338	6.81	1.14	100.00	3.18	0.57	1.17	12.72	0.00	12.72	4.000	No	Yes	2.00
339	6.82	1.19	100.00	3.12	0.57	1.16	13.03	0.00	13.03	4.000	No	Yes	2.00
340	6.84	1.22	100.00	3.08	0.57	1.16	13.68	0.00	13.68	4.000	No	Yes	2.00
341	6.87	1.25	100.00	3.05	0.57	1.16	13.79	0.00	13.79	4.000	No	Yes	2.00
342	6.88	1.25	100.00	3.03	0.57	1.16	13.81	0.00	13.81	4.000	No	Yes	2.00
343	6.90	1.24	100.00	3.04	0.57	1.16	13.67	0.00	13.67	4.000	No	Yes	2.00
344	6.92	1.22	100.00	3.05	0.57	1.16	13.44	0.00	13.44	4.000	No	Yes	2.00
345	6.94	1.19	100.00	3.08	0.57	1.16	13.16	0.00	13.16	4.000	No	Yes	2.00
346	6.96	1.16	100.00	3.11	0.57	1.15	12.83	0.00	12.83	4.000	No	Yes	2.00
347	6.98	1.13	100.00	3.14	0.57	1.15	12.37	0.00	12.37	4.000	No	Yes	2.00
348	7.00	1.11	100.00	3.16	0.57	1.15	11.93	0.00	11.93	4.000	No	Yes	2.00
349	7.02	1.10	100.00	3.16	0.57	1.15	11.94	0.00	11.94	4.000	No	Yes	2.00
350	7.04	1.11	100.00	3.15	0.57	1.15	12.01	0.00	12.01	4.000	No	Yes	2.00
351	7.06	1.13	100.00	3.12	0.57	1.15	12.36	0.00	12.36	4.000	No	Yes	2.00
352	7.08	1.17	100.00	3.09	0.57	1.15	12.48	0.00	12.48	4.000	No	Yes	2.00
353	7.10	1.23	100.00	3.04	0.57	1.14	13.23	0.00	13.23	4.000	No	Yes	2.00
354	7.12	1.34	100.00	2.97	0.57	1.14	14.32	0.00	14.32	4.000	No	Yes	2.00
355	7.15	1.44	96.12	2.91	0.56	1.14	15.82	0.00	15.82	4.000	No	Yes	2.00
356	7.16	1.53	93.06	2.88	0.56	1.14	16.59	0.00	16.59	4.000	No	Yes	2.00
357	7.18	1.59	91.70	2.86	0.56	1.14	17.36	0.00	17.36	4.000	No	Yes	2.00
358	7.20	1.64	91.46	2.86	0.55	1.13	18.02	0.00	18.02	4.000	No	Yes	2.00
359	7.30	1.67	91.90	2.86	0.55	1.13	18.28	0.00	18.28	4.000	No	Yes	2.00
360	7.30	1.68	92.36	2.87	0.55	1.13	18.28	0.00	18.28	4.000	No	Yes	2.00
361	7.30	1.66	98.28	2.94	0.55	1.13	18.20	0.00	18.20	4.000	No	Yes	2.00
362	7.32	1.63	100.00	3.01	0.55	1.13	17.71	0.00	17.71	4.000	No	Yes	2.00
363	7.34	1.60	100.00	3.08	0.55	1.13	17.51	0.00	17.51	4.000	No	Yes	2.00
364	7.36	1.59	100.00	3.08	0.56	1.12	17.25	0.00	17.25	4.000	No	Yes	2.00
365	7.38	1.57	100.00	3.09	0.56	1.12	17.25	0.00	17.25	4.000	No	Yes	2.00
366	7.40	1.55	100.00	3.10	0.56	1.12	16.77	0.00	16.77	4.000	No	Yes	2.00
367	7.42	1.52	100.00	3.10	0.56	1.12	16.31	0.00	16.31	4.000	No	Yes	2.00
368	7.44	1.50	100.00	3.10	0.56	1.12	16.23	0.00	16.23	4.000	No	Yes	2.00
369	7.46	1.49	100.00	3.10	0.56	1.12	16.06	0.00	16.06	4.000	No	Yes	2.00
370	7.48	1.48	100.00	3.10	0.56	1.12	16.06	0.00	16.06	4.000	No	Yes	2.00
371	7.50	1.48	100.00	3.09	0.56	1.12	15.91	0.00	15.91	4.000	No	Yes	2.00
372	7.52	1.47	100.00	3.09	0.56	1.11	15.91	0.00	15.91	4.000	No	Yes	2.00
373	7.54	1.47	100.00	3.08	0.56	1.11	15.91	0.00	15.91	4.000	No	Yes	2.00
374	7.56	1.48	100.00	3.07	0.56	1.11	15.68	0.00	15.68	4.000	No	Yes	2.00
375	7.58	1.50	100.00	3.06	0.56	1.11	16.26	0.00	16.26	4.000	No	Yes	2.00
376	7.60	1.54	100.00	3.04	0.56	1.11	16.50	0.00	16.50	4.000	No	Yes	2.00
377	7.62	1.58	100.00	3.02	0.56	1.11	17.08	0.00	17.08	4.000	No	Yes	2.00
378	7.64	1.62	100.00	3.00	0.55	1.11	17.49	0.00	17.49	4.000	No	Yes	2.00
379	7.66	1.64	100.00	3.00	0.55	1.10	17.67	0.00	17.67	4.000	No	Yes	2.00
380	7.68	1.65	100.00	3.00	0.55	1.10	17.64	0.00	17.64	4.000	No	Yes	2.00
381	7.70	1.66	100.00	3.00	0.55	1.10	17.82	0.00	17.82	4.000	No	Yes	2.00
382	7.72	1.67	100.00	3.01	0.55	1.10	18.02	0.00	18.02	4.000	No	Yes	2.00
383	7.74	1.67	100.00	3.01	0.55	1.10	18.05	0.00	18.05	4.000	No	Yes	2.00
384	7.76	1.68	100.00	3.02	0.55	1.10	17.67	0.00	17.67	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
385	7.78	1.68	100.00	3.02	0.55	1.10	18.16	0.00	18.16	4.000	No	Yes	2.00
386	7.80	1.70	100.00	3.03	0.55	1.10	17.95	0.00	17.95	4.000	No	Yes	2.00
387	7.83	1.71	100.00	3.03	0.55	1.09	18.32	0.00	18.32	4.000	No	Yes	2.00
388	7.84	1.72	100.00	3.03	0.55	1.09	18.28	0.00	18.28	4.000	No	Yes	2.00
389	7.86	1.70	100.00	3.03	0.55	1.09	18.13	0.00	18.13	4.000	No	Yes	2.00
390	7.88	1.68	100.00	3.04	0.55	1.09	17.88	0.00	17.88	4.000	No	Yes	2.00
391	7.90	1.66	100.00	3.05	0.55	1.09	17.63	0.00	17.63	4.000	No	Yes	2.00
392	7.93	1.64	100.00	3.07	0.55	1.09	17.40	0.00	17.40	4.000	No	Yes	2.00
393	7.94	1.61	100.00	3.08	0.56	1.09	16.90	0.00	16.90	4.000	No	Yes	2.00
394	7.96	1.60	100.00	3.10	0.56	1.09	16.81	0.00	16.81	4.000	No	Yes	2.00
395	7.98	1.60	100.00	3.10	0.56	1.09	16.78	0.00	16.78	4.000	No	Yes	2.00
396	8.00	1.60	100.00	3.11	0.56	1.08	16.96	0.00	16.96	4.000	No	Yes	2.00
397	8.02	1.59	100.00	3.11	0.56	1.08	16.56	0.00	16.56	4.000	No	Yes	2.00
398	8.04	1.56	100.00	3.12	0.56	1.08	16.44	0.00	16.44	4.000	No	Yes	2.00
399	8.06	1.55	100.00	3.11	0.56	1.08	16.11	0.00	16.11	4.000	No	Yes	2.00
400	8.08	1.55	100.00	3.11	0.56	1.08	16.11	0.00	16.11	4.000	No	Yes	2.00
401	8.10	1.57	100.00	3.09	0.56	1.08	16.33	0.00	16.33	4.000	No	Yes	2.00
402	8.12	1.62	100.00	3.07	0.56	1.08	16.73	0.00	16.73	4.000	No	Yes	2.00
403	8.14	1.66	100.00	3.05	0.55	1.08	17.49	0.00	17.49	4.000	No	Yes	2.00
404	8.16	1.70	100.00	3.04	0.55	1.07	17.62	0.00	17.62	4.000	No	Yes	2.00
405	8.18	1.72	100.00	3.04	0.55	1.07	17.99	0.00	17.99	4.000	No	Yes	2.00
406	8.20	1.74	100.00	3.04	0.55	1.07	18.09	0.00	18.09	4.000	No	Yes	2.00
407	8.22	1.74	100.00	3.05	0.55	1.07	18.01	0.00	18.01	4.000	No	Yes	2.00
408	8.24	1.75	100.00	3.05	0.55	1.07	18.16	0.00	18.16	4.000	No	Yes	2.00
409	8.26	1.75	100.00	3.05	0.55	1.07	18.23	0.00	18.23	4.000	No	Yes	2.00
410	8.28	1.76	100.00	3.06	0.55	1.07	18.05	0.00	18.05	4.000	No	Yes	2.00
411	8.30	1.75	100.00	3.07	0.55	1.07	18.13	0.00	18.13	4.000	No	Yes	2.00
412	8.32	1.75	100.00	3.07	0.55	1.06	18.13	0.00	18.13	4.000	No	Yes	2.00
413	8.34	1.72	100.00	3.08	0.55	1.06	17.75	0.00	17.75	4.000	No	Yes	2.00
414	8.36	1.68	100.00	3.09	0.56	1.06	17.21	0.00	17.21	4.000	No	Yes	2.00
415	8.38	1.66	100.00	3.10	0.56	1.06	16.99	0.00	16.99	4.000	No	Yes	2.00
416	8.40	1.66	100.00	3.10	0.56	1.06	16.92	0.00	16.92	4.000	No	Yes	2.00
417	8.43	1.66	100.00	3.10	0.56	1.06	17.09	0.00	17.09	4.000	No	Yes	2.00
418	8.44	1.67	100.00	3.09	0.56	1.06	17.18	0.00	17.18	4.000	No	Yes	2.00
419	8.46	1.66	100.00	3.10	0.56	1.06	17.08	0.00	17.08	4.000	No	Yes	2.00
420	8.48	1.65	100.00	3.10	0.56	1.06	16.74	0.00	16.74	4.000	No	Yes	2.00
421	8.50	1.66	100.00	3.10	0.56	1.05	16.88	0.00	16.88	4.000	No	Yes	2.00
422	8.52	1.69	100.00	3.09	0.56	1.05	17.17	0.00	17.17	4.000	No	Yes	2.00
423	8.54	1.71	100.00	3.08	0.55	1.05	17.59	0.00	17.59	4.000	No	Yes	2.00
424	8.56	1.74	100.00	3.06	0.55	1.05	17.56	0.00	17.56	4.000	No	Yes	2.00
425	8.58	1.77	100.00	3.05	0.55	1.05	18.15	0.00	18.15	4.000	No	Yes	2.00
426	8.60	1.79	100.00	3.05	0.55	1.05	18.30	0.00	18.30	4.000	No	Yes	2.00
427	8.62	1.79	100.00	3.06	0.55	1.05	18.08	0.00	18.08	4.000	No	Yes	2.00
428	8.64	1.80	100.00	3.07	0.55	1.05	18.25	0.00	18.25	4.000	No	Yes	2.00
429	8.66	1.81	100.00	3.06	0.55	1.05	18.25	0.00	18.25	4.000	No	Yes	2.00
430	8.68	1.84	100.00	3.06	0.55	1.04	18.57	0.00	18.57	4.000	No	Yes	2.00
431	8.70	1.87	100.00	3.06	0.55	1.04	18.93	0.00	18.93	4.000	No	Yes	2.00
432	8.72	1.90	100.00	3.06	0.55	1.04	19.12	0.00	19.12	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
433	8.74	1.93	100.00	3.05	0.55	1.04	19.43	0.00	19.43	4.000	No	Yes	2.00
434	8.76	1.97	100.00	3.04	0.55	1.04	19.70	0.00	19.70	4.000	No	Yes	2.00
435	8.78	2.03	100.00	3.03	0.54	1.04	20.45	0.00	20.45	4.000	No	Yes	2.00
436	8.80	2.10	100.00	3.02	0.54	1.04	21.17	0.00	21.17	4.000	No	Yes	2.00
437	8.82	2.15	100.00	3.01	0.54	1.04	21.75	0.00	21.75	4.000	No	Yes	2.00
438	8.84	2.15	100.00	3.02	0.54	1.03	21.85	0.00	21.85	4.000	No	Yes	2.00
439	8.86	2.08	100.00	3.05	0.54	1.03	21.06	0.00	21.06	4.000	No	Yes	2.00
440	8.88	2.00	100.00	3.08	0.55	1.03	19.58	0.00	19.58	4.000	No	Yes	2.00
441	8.90	1.94	100.00	3.10	0.55	1.03	19.34	0.00	19.34	4.000	No	Yes	2.00
442	8.92	1.93	100.00	3.11	0.55	1.03	19.40	0.00	19.40	4.000	No	Yes	2.00
443	8.94	1.92	100.00	3.11	0.55	1.03	19.02	0.00	19.02	4.000	No	Yes	2.00
444	8.96	1.91	100.00	3.11	0.55	1.03	18.94	0.00	18.94	4.000	No	Yes	2.00
445	8.98	1.93	100.00	3.09	0.55	1.03	19.05	0.00	19.05	4.000	No	Yes	2.00
446	9.00	1.94	100.00	3.08	0.55	1.03	19.55	0.00	19.55	4.000	No	Yes	2.00
447	9.02	1.95	100.00	3.07	0.55	1.03	19.19	0.00	19.19	4.000	No	Yes	2.00
448	9.05	1.93	100.00	3.06	0.55	1.02	19.19	0.00	19.19	4.000	No	Yes	2.00
449	9.06	1.91	100.00	3.05	0.55	1.02	18.89	0.00	18.89	4.000	No	Yes	2.00
450	9.08	1.89	100.00	3.05	0.55	1.02	18.68	0.00	18.68	4.000	No	Yes	2.00
451	9.10	1.88	100.00	3.04	0.55	1.02	18.61	0.00	18.61	4.000	No	Yes	2.00
452	9.12	1.87	100.00	3.04	0.55	1.02	18.46	0.00	18.46	4.000	No	Yes	2.00
453	9.14	1.86	100.00	3.03	0.55	1.02	18.32	0.00	18.32	4.000	No	Yes	2.00
454	9.16	1.86	100.00	3.03	0.55	1.02	18.39	0.00	18.39	4.000	No	Yes	2.00
455	9.18	1.88	100.00	3.02	0.55	1.02	18.40	0.00	18.40	4.000	No	Yes	2.00
456	9.21	1.92	100.00	3.00	0.55	1.02	18.83	0.00	18.83	4.000	No	Yes	2.00
457	9.22	1.95	100.00	2.99	0.55	1.02	19.29	0.00	19.29	4.000	No	Yes	2.00
458	9.24	1.97	100.00	2.98	0.55	1.01	19.32	0.00	19.32	4.000	No	Yes	2.00
459	9.26	1.99	100.00	2.98	0.55	1.01	19.53	0.00	19.53	4.000	No	Yes	2.00
460	9.28	2.01	100.00	2.97	0.55	1.01	19.72	0.00	19.72	4.000	No	Yes	2.00
461	9.30	2.01	100.00	2.97	0.55	1.01	19.88	0.00	19.88	4.000	No	Yes	2.00
462	9.32	2.01	100.00	2.99	0.55	1.01	19.70	0.00	19.70	4.000	No	Yes	2.00
463	9.34	2.02	100.00	2.99	0.55	1.01	19.63	0.00	19.63	4.000	No	Yes	2.00
464	9.36	2.06	100.00	2.99	0.54	1.01	20.31	0.00	20.31	4.000	No	Yes	2.00
465	9.38	2.14	100.00	2.96	0.54	1.01	20.71	0.00	20.71	4.000	No	Yes	2.00
466	9.40	2.18	99.12	2.95	0.54	1.01	21.78	0.00	21.78	4.000	No	Yes	2.00
467	9.42	2.22	98.55	2.94	0.54	1.01	21.60	0.00	21.60	4.000	No	Yes	2.00
468	9.44	2.20	99.57	2.96	0.54	1.00	21.79	0.00	21.79	4.000	No	Yes	2.00
469	9.47	2.18	100.00	2.97	0.54	1.00	21.34	0.00	21.34	4.000	No	Yes	2.00
470	9.48	2.15	100.00	2.99	0.54	1.00	21.00	0.00	21.00	4.000	No	Yes	2.00
471	9.50	2.14	100.00	3.00	0.54	1.00	20.75	0.00	20.75	4.000	No	Yes	2.00
472	9.53	2.18	100.00	3.00	0.54	1.00	21.09	0.00	21.09	4.000	No	Yes	2.00
473	9.54	2.24	100.00	2.99	0.54	1.00	22.05	0.00	22.05	4.000	No	Yes	2.00
474	9.56	2.28	100.00	2.98	0.54	1.00	22.42	0.00	22.42	4.000	No	Yes	2.00
475	9.58	2.26	100.00	2.98	0.54	1.00	22.21	0.00	22.21	4.000	No	Yes	2.00
476	9.60	2.19	100.00	3.00	0.54	1.00	21.51	0.00	21.51	4.000	No	Yes	2.00
477	9.62	2.09	100.00	3.03	0.54	1.00	20.29	0.00	20.29	4.000	No	Yes	2.00
478	9.64	1.98	100.00	3.07	0.55	0.99	19.22	0.00	19.22	4.000	No	Yes	2.00
479	9.66	1.87	100.00	3.11	0.55	0.99	18.17	0.00	18.17	4.000	No	Yes	2.00
480	9.68	1.75	100.00	3.14	0.56	0.99	17.06	0.00	17.06	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
481	9.70	1.62	100.00	3.18	0.56	0.99	15.59	0.00	15.59	4.000	No	Yes	2.00
482	9.72	1.49	100.00	3.22	0.57	0.99	14.31	0.00	14.31	4.000	No	Yes	2.00
483	9.74	1.39	100.00	3.24	0.57	0.99	13.24	0.00	13.24	4.000	No	Yes	2.00
484	9.76	1.30	100.00	3.26	0.57	0.99	12.44	0.00	12.44	4.000	No	Yes	2.00
485	9.79	1.22	100.00	3.28	0.58	0.99	11.53	0.00	11.53	4.000	No	Yes	2.00
486	9.80	1.14	100.00	3.30	0.58	0.99	10.66	0.00	10.66	4.000	No	Yes	2.00
487	9.82	1.09	100.00	3.30	0.58	0.99	10.17	0.00	10.17	4.000	No	Yes	2.00
488	9.85	1.06	100.00	3.30	0.58	0.98	9.73	0.00	9.73	4.000	No	Yes	2.00
489	9.86	1.05	100.00	3.27	0.58	0.98	9.66	0.00	9.66	4.000	No	Yes	2.00
490	9.88	1.07	100.00	3.22	0.58	0.98	9.88	0.00	9.88	4.000	No	Yes	2.00
491	9.90	1.10	100.00	3.17	0.58	0.98	10.37	0.00	10.37	4.000	No	Yes	2.00
492	9.92	1.11	100.00	3.14	0.58	0.98	10.43	0.00	10.43	4.000	No	Yes	2.00
493	9.94	1.09	100.00	3.13	0.58	0.98	10.06	0.00	10.06	4.000	No	Yes	2.00
494	9.96	1.07	100.00	3.13	0.58	0.98	9.88	0.00	9.88	4.000	No	Yes	2.00
495	9.98	1.07	100.00	3.12	0.58	0.98	9.76	0.00	9.76	4.000	No	Yes	2.00
496	10.00	1.11	100.00	3.08	0.58	0.98	9.96	0.00	9.96	4.000	No	Yes	2.00
497	10.02	1.20	100.00	3.03	0.58	0.98	10.88	0.00	10.88	4.000	No	Yes	2.00
498	10.04	1.28	100.00	2.97	0.58	0.98	11.88	0.00	11.88	4.000	No	Yes	2.00
499	10.06	1.35	98.79	2.95	0.57	0.98	12.28	0.00	12.28	4.000	No	Yes	2.00
500	10.08	1.39	97.86	2.94	0.57	0.98	12.69	0.00	12.69	4.000	No	Yes	2.00
501	10.11	1.48	95.87	2.91	0.57	0.97	13.13	0.00	13.13	4.000	No	Yes	2.00
502	10.12	1.66	90.43	2.84	0.57	0.97	14.67	0.00	14.67	4.000	No	Yes	2.00
503	10.14	1.90	83.93	2.76	0.56	0.97	17.49	0.00	17.49	4.000	No	Yes	2.00
504	10.16	2.12	79.10	2.70	0.55	0.97	19.79	0.00	19.79	4.000	No	Yes	2.00
505	10.18	2.24	78.32	2.69	0.55	0.97	20.87	0.00	20.87	4.000	No	Yes	2.00
506	10.20	2.27	80.07	2.71	0.55	0.97	21.13	0.00	21.13	4.000	No	Yes	2.00
507	10.22	2.24	83.17	2.75	0.55	0.97	20.83	0.00	20.83	4.000	No	Yes	2.00
508	10.24	2.15	87.98	2.81	0.55	0.97	20.32	0.00	20.32	4.000	No	Yes	2.00
509	10.26	2.03	93.85	2.89	0.55	0.97	18.75	0.00	18.75	4.000	No	Yes	2.00
510	10.28	1.86	100.00	2.98	0.55	0.97	17.43	0.00	17.43	4.000	No	Yes	2.00
511	10.30	1.70	100.00	3.07	0.56	0.97	15.60	0.00	15.60	4.000	No	Yes	2.00
512	10.32	1.54	100.00	3.16	0.57	0.97	14.36	0.00	14.36	4.000	No	Yes	2.00
513	10.34	1.43	100.00	3.23	0.57	0.96	12.91	0.00	12.91	4.000	No	Yes	2.00
514	10.36	1.33	100.00	3.28	0.57	0.96	12.20	0.00	12.20	4.000	No	Yes	2.00
515	10.38	1.26	100.00	3.31	0.58	0.96	11.48	0.00	11.48	4.000	No	Yes	2.00
516	10.40	1.18	100.00	3.34	0.58	0.96	10.77	0.00	10.77	4.000	No	Yes	2.00
517	10.42	1.10	100.00	3.37	0.58	0.96	9.95	0.00	9.95	4.000	No	Yes	2.00
518	10.44	1.04	100.00	3.38	0.59	0.96	9.28	0.00	9.28	4.000	No	Yes	2.00
519	10.46	1.01	100.00	3.37	0.59	0.96	8.94	0.00	8.94	4.000	No	Yes	2.00
520	10.48	1.01	100.00	3.34	0.59	0.96	9.00	0.00	9.00	4.000	No	Yes	2.00
521	10.50	1.03	100.00	3.27	0.59	0.96	9.01	0.00	9.01	4.000	No	Yes	2.00
522	10.52	1.06	100.00	3.21	0.58	0.96	9.42	0.00	9.42	4.000	No	Yes	2.00
523	10.54	1.10	100.00	3.14	0.58	0.96	9.81	0.00	9.81	4.000	No	Yes	2.00
524	10.56	1.16	100.00	3.07	0.58	0.95	10.24	0.00	10.24	4.000	No	Yes	2.00
525	10.58	1.23	100.00	3.01	0.58	0.95	11.12	0.00	11.12	4.000	No	Yes	2.00
526	10.60	1.29	99.74	2.96	0.58	0.95	11.61	0.00	11.61	4.000	No	Yes	2.00
527	10.62	1.33	98.13	2.94	0.57	0.95	12.04	0.00	12.04	4.000	No	Yes	2.00
528	10.64	1.34	98.09	2.94	0.57	0.95	12.08	0.00	12.08	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
529	10.66	1.36	97.96	2.94	0.57	0.95	12.05	0.00	12.05	4.000	No	Yes	2.00
530	10.70	1.41	96.01	2.91	0.57	0.95	12.43	0.00	12.43	4.000	No	Yes	2.00
531	10.70	1.48	93.58	2.88	0.57	0.95	13.50	0.00	13.50	4.000	No	Yes	2.00
532	10.72	1.64	89.80	2.83	0.57	0.95	13.87	0.00	13.87	4.000	No	Yes	2.00
533	10.75	1.70	90.88	2.85	0.56	0.95	17.16	0.00	17.16	4.000	No	Yes	2.00
534	10.76	1.71	92.56	2.87	0.56	0.95	15.32	0.00	15.32	4.000	No	Yes	2.00
535	10.78	1.58	97.38	2.93	0.57	0.95	14.16	0.00	14.16	4.000	No	Yes	2.00
536	10.80	1.51	99.42	2.96	0.57	0.95	13.20	0.00	13.20	4.000	No	Yes	2.00
537	10.82	1.53	98.02	2.94	0.57	0.95	12.93	0.00	12.93	4.000	No	Yes	2.00
538	10.84	1.66	93.07	2.88	0.57	0.95	14.30	0.00	14.30	4.000	No	Yes	2.00
539	10.86	1.89	85.26	2.78	0.56	0.95	16.19	0.00	16.19	4.000	No	Yes	2.00
540	10.88	2.08	79.80	2.71	0.55	0.95	19.08	0.00	19.08	4.000	No	Yes	2.00
541	10.90	2.21	77.45	2.68	0.55	0.94	19.88	0.00	19.88	4.000	No	Yes	2.00
542	10.92	2.22	79.13	2.70	0.55	0.94	20.05	0.00	20.05	4.000	No	Yes	2.00
543	10.94	2.20	82.50	2.74	0.55	0.94	19.59	0.00	19.59	4.000	No	Yes	2.00
544	10.96	2.18	86.34	2.79	0.55	0.94	19.47	0.00	19.47	4.000	No	Yes	2.00
545	10.98	2.16	89.39	2.83	0.55	0.94	19.36	0.00	19.36	4.000	No	Yes	2.00
546	11.00	2.14	92.69	2.87	0.55	0.94	19.40	0.00	19.40	4.000	No	Yes	2.00
547	11.02	2.13	95.63	2.91	0.55	0.94	19.16	0.00	19.16	4.000	No	Yes	2.00
548	11.06	2.12	97.82	2.94	0.55	0.94	19.04	0.00	19.04	4.000	No	Yes	2.00
549	11.06	2.08	100.00	2.97	0.55	0.94	19.05	0.00	19.05	4.000	No	Yes	2.00
550	11.08	2.05	100.00	2.99	0.55	0.94	18.19	0.00	18.19	4.000	No	Yes	2.00
551	11.10	2.00	100.00	3.03	0.55	0.94	17.80	0.00	17.80	4.000	No	Yes	2.00
552	11.12	1.97	100.00	3.04	0.55	0.94	17.54	0.00	17.54	4.000	No	Yes	2.00
553	11.14	1.95	100.00	3.05	0.55	0.94	17.43	0.00	17.43	4.000	No	Yes	2.00
554	11.16	1.93	100.00	3.05	0.56	0.93	17.23	0.00	17.23	4.000	No	Yes	2.00
555	11.18	1.89	100.00	3.06	0.56	0.93	16.77	0.00	16.77	4.000	No	Yes	2.00
556	11.20	1.84	100.00	3.08	0.56	0.93	16.42	0.00	16.42	4.000	No	Yes	2.00
557	11.23	1.81	100.00	3.09	0.56	0.93	15.87	0.00	15.87	4.000	No	Yes	2.00
558	11.24	1.78	100.00	3.11	0.56	0.93	15.77	0.00	15.77	4.000	No	Yes	2.00
559	11.26	1.78	100.00	3.11	0.56	0.93	15.57	0.00	15.57	4.000	No	Yes	2.00
560	11.28	1.79	100.00	3.11	0.56	0.93	15.79	0.00	15.79	4.000	No	Yes	2.00
561	11.30	1.79	100.00	3.12	0.56	0.93	15.85	0.00	15.85	4.000	No	Yes	2.00
562	11.32	1.77	100.00	3.12	0.56	0.93	15.57	0.00	15.57	4.000	No	Yes	2.00
563	11.34	1.71	100.00	3.14	0.56	0.93	15.27	0.00	15.27	4.000	No	Yes	2.00
564	11.36	1.62	100.00	3.18	0.57	0.93	14.36	0.00	14.36	4.000	No	Yes	2.00
565	11.38	1.49	100.00	3.24	0.57	0.92	13.06	0.00	13.06	4.000	No	Yes	2.00
566	11.40	1.36	100.00	3.30	0.58	0.92	11.84	0.00	11.84	4.000	No	Yes	2.00
567	11.42	1.23	100.00	3.37	0.58	0.92	10.83	0.00	10.83	4.000	No	Yes	2.00
568	11.44	1.11	100.00	3.44	0.58	0.92	9.48	0.00	9.48	4.000	No	Yes	2.00
569	11.46	1.00	100.00	3.51	0.59	0.92	8.62	0.00	8.62	4.000	No	Yes	2.00
570	11.48	0.93	100.00	3.56	0.59	0.92	7.84	0.00	7.84	4.000	No	Yes	2.00
571	11.50	0.87	100.00	3.59	0.59	0.92	7.43	0.00	7.43	4.000	No	Yes	2.00
572	11.52	0.83	100.00	3.61	0.59	0.92	7.05	0.00	7.05	4.000	No	Yes	2.00
573	11.54	0.82	100.00	3.59	0.60	0.91	6.75	0.00	6.75	4.000	No	Yes	2.00
574	11.56	0.84	100.00	3.54	0.59	0.91	7.09	0.00	7.09	4.000	No	Yes	2.00
575	11.58	0.86	100.00	3.48	0.59	0.91	7.30	0.00	7.30	4.000	No	Yes	2.00
576	11.60	0.87	100.00	3.43	0.59	0.91	7.28	0.00	7.28	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
577	11.62	0.90	100.00	3.36	0.59	0.91	7.53	0.00	7.53	4.000	No	Yes	2.00
578	11.64	0.96	100.00	3.28	0.59	0.91	8.05	0.00	8.05	4.000	No	Yes	2.00
579	11.66	1.04	100.00	3.19	0.59	0.91	8.81	0.00	8.81	4.000	No	Yes	2.00
580	11.68	1.07	100.00	3.13	0.58	0.91	9.46	0.00	9.46	4.000	No	Yes	2.00
581	11.70	1.09	100.00	3.09	0.59	0.91	8.97	0.00	8.97	4.000	No	Yes	2.00
582	11.72	1.27	100.00	3.00	0.58	0.91	9.32	0.00	9.32	4.000	No	Yes	2.00
583	11.74	1.44	98.55	2.94	0.57	0.91	14.58	0.00	14.58	4.000	No	Yes	2.00
584	11.76	1.52	98.09	2.94	0.57	0.91	13.72	0.00	13.72	4.000	No	Yes	2.00
585	11.78	1.36	100.00	3.01	0.58	0.91	11.69	0.00	11.69	4.000	No	Yes	2.00
586	11.80	1.20	100.00	3.07	0.58	0.91	10.03	0.00	10.03	4.000	No	Yes	2.00
587	11.82	1.10	100.00	3.11	0.59	0.91	9.27	0.00	9.27	4.000	No	Yes	2.00
588	11.84	1.06	100.00	3.11	0.59	0.91	8.93	0.00	8.93	4.000	No	Yes	2.00
589	11.87	1.02	100.00	3.13	0.59	0.90	8.71	0.00	8.71	4.000	No	Yes	2.00
590	11.88	0.98	100.00	3.15	0.59	0.90	8.13	0.00	8.13	4.000	No	Yes	2.00
591	11.90	0.95	100.00	3.16	0.59	0.90	7.75	0.00	7.75	4.000	No	Yes	2.00
592	11.92	0.97	100.00	3.14	0.59	0.90	7.79	0.00	7.79	4.000	No	Yes	2.00
593	11.94	1.02	100.00	3.10	0.59	0.90	8.28	0.00	8.28	4.000	No	Yes	2.00
594	11.96	1.13	100.00	3.04	0.59	0.90	9.13	0.00	9.13	4.000	No	Yes	2.00
595	11.98	1.29	99.45	2.96	0.58	0.90	10.58	0.00	10.58	4.000	No	Yes	2.00
596	12.00	1.43	94.32	2.89	0.57	0.90	12.32	0.00	12.32	4.000	No	Yes	2.00
597	12.02	1.49	93.30	2.88	0.57	0.90	12.93	0.00	12.93	4.000	No	Yes	2.00
598	12.04	1.46	97.41	2.93	0.57	0.90	12.33	0.00	12.33	4.000	No	Yes	2.00
599	12.06	1.36	100.00	3.02	0.58	0.90	11.55	0.00	11.55	4.000	No	Yes	2.00
600	12.08	1.25	100.00	3.13	0.58	0.90	10.58	0.00	10.58	4.000	No	Yes	2.00
601	12.10	1.15	100.00	3.24	0.58	0.90	9.63	0.00	9.63	4.000	No	Yes	2.00
602	12.12	1.08	100.00	3.33	0.59	0.90	9.00	0.00	9.00	4.000	No	Yes	2.00
603	12.14	1.03	100.00	3.39	0.59	0.90	8.60	0.00	8.60	4.000	No	Yes	2.00
604	12.16	1.01	100.00	3.42	0.59	0.90	8.33	0.00	8.33	4.000	No	Yes	2.00
605	12.18	1.01	100.00	3.41	0.59	0.89	8.22	0.00	8.22	4.000	No	Yes	2.00
606	12.20	1.04	100.00	3.37	0.59	0.89	8.56	0.00	8.56	4.000	No	Yes	2.00
607	12.22	1.09	100.00	3.31	0.59	0.89	9.13	0.00	9.13	4.000	No	Yes	2.00
608	12.24	1.14	100.00	3.25	0.58	0.89	9.39	0.00	9.39	4.000	No	Yes	2.00
609	12.26	1.19	100.00	3.18	0.58	0.89	9.82	0.00	9.82	4.000	No	Yes	2.00
610	12.28	1.24	100.00	3.13	0.58	0.89	10.46	0.00	10.46	4.000	No	Yes	2.00
611	12.30	1.28	100.00	3.10	0.58	0.89	10.66	0.00	10.66	4.000	No	Yes	2.00
612	12.32	1.30	100.00	3.10	0.58	0.89	10.80	0.00	10.80	4.000	No	Yes	2.00
613	12.34	1.31	100.00	3.11	0.58	0.89	10.89	0.00	10.89	4.000	No	Yes	2.00
614	12.36	1.33	100.00	3.11	0.58	0.89	11.07	0.00	11.07	4.000	No	Yes	2.00
615	12.38	1.35	100.00	3.12	0.58	0.89	11.33	0.00	11.33	4.000	No	Yes	2.00
616	12.40	1.38	100.00	3.11	0.58	0.89	11.36	0.00	11.36	4.000	No	Yes	2.00
617	12.42	1.40	100.00	3.11	0.58	0.89	11.81	0.00	11.81	4.000	No	Yes	2.00
618	12.44	1.43	100.00	3.12	0.58	0.89	11.86	0.00	11.86	4.000	No	Yes	2.00
619	12.46	1.44	100.00	3.12	0.57	0.89	11.93	0.00	11.93	4.000	No	Yes	2.00
620	12.48	1.47	100.00	3.13	0.57	0.89	12.15	0.00	12.15	4.000	No	Yes	2.00
621	12.51	1.49	100.00	3.14	0.57	0.89	12.76	0.00	12.76	4.000	No	Yes	2.00
622	12.52	1.50	100.00	3.16	0.57	0.89	12.50	0.00	12.50	4.000	No	Yes	2.00
623	12.54	1.48	100.00	3.19	0.57	0.89	12.51	0.00	12.51	4.000	No	Yes	2.00
624	12.56	1.47	100.00	3.22	0.57	0.88	12.33	0.00	12.33	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
625	12.58	1.43	100.00	3.25	0.57	0.88	12.22	0.00	12.22	4.000	No	Yes	2.00
626	12.60	1.41	100.00	3.28	0.58	0.88	11.69	0.00	11.69	4.000	No	Yes	2.00
627	12.62	1.38	100.00	3.32	0.58	0.88	11.57	0.00	11.57	4.000	No	Yes	2.00
628	12.64	1.36	100.00	3.33	0.58	0.88	11.31	0.00	11.31	4.000	No	Yes	2.00
629	12.66	1.35	100.00	3.34	0.58	0.88	11.17	0.00	11.17	4.000	No	Yes	2.00
630	12.68	1.38	100.00	3.32	0.58	0.88	11.26	0.00	11.26	4.000	No	Yes	2.00
631	12.70	1.41	100.00	3.30	0.57	0.88	11.91	0.00	11.91	4.000	No	Yes	2.00
632	12.72	1.43	100.00	3.27	0.57	0.88	11.92	0.00	11.92	4.000	No	Yes	2.00
633	12.75	1.44	100.00	3.26	0.58	0.88	11.73	0.00	11.73	4.000	No	Yes	2.00
634	12.76	1.44	100.00	3.26	0.57	0.88	12.18	0.00	12.18	4.000	No	Yes	2.00
635	12.78	1.43	100.00	3.26	0.57	0.88	12.03	0.00	12.03	4.000	No	Yes	2.00
636	12.80	1.42	100.00	3.27	0.58	0.88	11.57	0.00	11.57	4.000	No	Yes	2.00
637	12.82	1.41	100.00	3.28	0.58	0.88	11.68	0.00	11.68	4.000	No	Yes	2.00
638	12.84	1.41	100.00	3.27	0.58	0.87	11.77	0.00	11.77	4.000	No	Yes	2.00
639	12.86	1.41	100.00	3.28	0.58	0.87	11.72	0.00	11.72	4.000	No	Yes	2.00
640	12.88	1.38	100.00	3.30	0.58	0.87	11.46	0.00	11.46	4.000	No	Yes	2.00
641	12.90	1.34	100.00	3.32	0.58	0.87	11.04	0.00	11.04	4.000	No	Yes	2.00
642	12.92	1.31	100.00	3.34	0.58	0.87	10.72	0.00	10.72	4.000	No	Yes	2.00
643	12.94	1.30	100.00	3.33	0.58	0.87	10.61	0.00	10.61	4.000	No	Yes	2.00
644	12.96	1.31	100.00	3.32	0.58	0.87	10.81	0.00	10.81	4.000	No	Yes	2.00
645	12.98	1.33	100.00	3.31	0.58	0.87	10.96	0.00	10.96	4.000	No	Yes	2.00
646	13.01	1.33	100.00	3.30	0.58	0.87	11.01	0.00	11.01	4.000	No	Yes	2.00
647	13.02	1.34	100.00	3.29	0.58	0.87	10.94	0.00	10.94	4.000	No	Yes	2.00
648	13.04	1.34	100.00	3.28	0.58	0.87	11.19	0.00	11.19	4.000	No	Yes	2.00
649	13.06	1.34	100.00	3.28	0.58	0.87	11.02	0.00	11.02	4.000	No	Yes	2.00
650	13.08	1.32	100.00	3.29	0.58	0.87	10.85	0.00	10.85	4.000	No	Yes	2.00
651	13.10	1.29	100.00	3.30	0.58	0.87	10.63	0.00	10.63	4.000	No	Yes	2.00
652	13.12	1.28	100.00	3.30	0.58	0.86	10.36	0.00	10.36	4.000	No	Yes	2.00
653	13.14	1.26	100.00	3.31	0.58	0.86	10.37	0.00	10.37	4.000	No	Yes	2.00
654	13.16	1.22	100.00	3.33	0.58	0.86	10.17	0.00	10.17	4.000	No	Yes	2.00
655	13.18	1.16	100.00	3.37	0.59	0.86	9.30	0.00	9.30	4.000	No	Yes	2.00
656	13.20	1.09	100.00	3.42	0.59	0.86	8.83	0.00	8.83	4.000	No	Yes	2.00
657	13.23	1.07	100.00	3.44	0.59	0.86	8.49	0.00	8.49	4.000	No	Yes	2.00
658	13.24	1.06	100.00	3.44	0.59	0.86	8.65	0.00	8.65	4.000	No	Yes	2.00
659	13.26	1.08	100.00	3.42	0.59	0.86	8.66	0.00	8.66	4.000	No	Yes	2.00
660	13.29	1.10	100.00	3.39	0.59	0.86	8.75	0.00	8.75	4.000	No	Yes	2.00
661	13.30	1.12	100.00	3.35	0.59	0.86	9.08	0.00	9.08	4.000	No	Yes	2.00
662	13.32	1.13	100.00	3.32	0.59	0.86	9.23	0.00	9.23	4.000	No	Yes	2.00
663	13.34	1.12	100.00	3.30	0.59	0.86	8.90	0.00	8.90	4.000	No	Yes	2.00
664	13.36	1.12	100.00	3.29	0.59	0.86	9.03	0.00	9.03	4.000	No	Yes	2.00
665	13.38	1.14	100.00	3.26	0.59	0.86	8.98	0.00	8.98	4.000	No	Yes	2.00
666	13.40	1.17	100.00	3.23	0.58	0.86	9.38	0.00	9.38	4.000	No	Yes	2.00
667	13.42	1.21	100.00	3.20	0.58	0.85	9.65	0.00	9.65	4.000	No	Yes	2.00
668	13.44	1.25	100.00	3.17	0.58	0.85	10.03	0.00	10.03	4.000	No	Yes	2.00
669	13.46	1.29	100.00	3.14	0.58	0.85	10.32	0.00	10.32	4.000	No	Yes	2.00
670	13.48	1.33	100.00	3.12	0.58	0.85	10.72	0.00	10.72	4.000	No	Yes	2.00
671	13.50	1.37	100.00	3.11	0.58	0.85	11.07	0.00	11.07	4.000	No	Yes	2.00
672	13.52	1.38	100.00	3.11	0.58	0.85	11.19	0.00	11.19	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
673	13.54	1.39	100.00	3.11	0.58	0.85	11.13	0.00	11.13	4.000	No	Yes	2.00
674	13.56	1.38	100.00	3.13	0.58	0.85	11.26	0.00	11.26	4.000	No	Yes	2.00
675	13.58	1.34	100.00	3.16	0.58	0.85	10.84	0.00	10.84	4.000	No	Yes	2.00
676	13.60	1.30	100.00	3.19	0.58	0.85	10.19	0.00	10.19	4.000	No	Yes	2.00
677	13.62	1.27	100.00	3.20	0.58	0.85	10.09	0.00	10.09	4.000	No	Yes	2.00
678	13.64	1.27	100.00	3.20	0.58	0.85	10.14	0.00	10.14	4.000	No	Yes	2.00
679	13.66	1.27	100.00	3.20	0.58	0.85	10.14	0.00	10.14	4.000	No	Yes	2.00
680	13.68	1.30	100.00	3.20	0.58	0.85	10.15	0.00	10.15	4.000	No	Yes	2.00
681	13.70	1.34	100.00	3.18	0.58	0.85	10.73	0.00	10.73	4.000	No	Yes	2.00
682	13.72	1.36	100.00	3.17	0.58	0.85	11.16	0.00	11.16	4.000	No	Yes	2.00
683	13.74	1.39	100.00	3.15	0.58	0.85	10.60	0.00	10.60	4.000	No	Yes	2.00
684	13.76	1.40	100.00	3.15	0.58	0.85	11.49	0.00	11.49	4.000	No	Yes	2.00
685	13.78	1.41	100.00	3.16	0.58	0.85	11.33	0.00	11.33	4.000	No	Yes	2.00
686	13.80	1.37	100.00	3.18	0.58	0.85	10.98	0.00	10.98	4.000	No	Yes	2.00
687	13.82	1.35	100.00	3.19	0.58	0.84	10.39	0.00	10.39	4.000	No	Yes	2.00
688	13.85	1.33	100.00	3.21	0.58	0.84	10.77	0.00	10.77	4.000	No	Yes	2.00
689	13.86	1.33	100.00	3.21	0.58	0.84	10.27	0.00	10.27	4.000	No	Yes	2.00
690	13.88	1.31	100.00	3.22	0.58	0.84	10.52	0.00	10.52	4.000	No	Yes	2.00
691	13.90	1.29	100.00	3.22	0.58	0.84	10.16	0.00	10.16	4.000	No	Yes	2.00
692	13.92	1.28	100.00	3.23	0.58	0.84	9.99	0.00	9.99	4.000	No	Yes	2.00
693	13.94	1.27	100.00	3.23	0.58	0.84	10.04	0.00	10.04	4.000	No	Yes	2.00
694	13.96	1.25	100.00	3.24	0.58	0.84	9.90	0.00	9.90	4.000	No	Yes	2.00
695	13.98	1.23	100.00	3.25	0.58	0.84	9.69	0.00	9.69	4.000	No	Yes	2.00
696	14.00	1.22	100.00	3.26	0.58	0.84	9.50	0.00	9.50	4.000	No	Yes	2.00
697	14.02	1.21	100.00	3.28	0.58	0.84	9.61	0.00	9.61	4.000	No	Yes	2.00
698	14.04	1.19	100.00	3.29	0.58	0.84	9.33	0.00	9.33	4.000	No	Yes	2.00
699	14.06	1.18	100.00	3.31	0.59	0.84	9.18	0.00	9.18	4.000	No	Yes	2.00
700	14.08	1.15	100.00	3.33	0.59	0.84	8.90	0.00	8.90	4.000	No	Yes	2.00

Abbreviations

Depth: Depth from free surface, at which CPT was performed (m)
q_t: Total cone resistance
FC: Fines content (%)
I_c: Soil behavior type index
m: Stress exponent
C_N: Overburden correction factor
q_{c1N}: Normalized and adjusted cone resistance
Δq_{c1N}: Cone resistance correction factor due to fines
$q_{c1N,cs}$: Normalized and adjusted cone resistance
$CRR_{7.5}$: Cyclic resistance ratio for M_w=7.5
FS: Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
0.02	2.00	0.00	9.99	0.02	0.00	0.04	2.00	0.00	9.98	0.02	0.00
0.06	2.00	0.00	9.97	0.02	0.00	0.08	2.00	0.00	9.96	0.02	0.00
0.10	2.00	0.00	9.95	0.02	0.00	0.12	2.00	0.00	9.94	0.02	0.00
0.14	2.00	0.00	9.93	0.02	0.00	0.16	2.00	0.00	9.92	0.02	0.00
0.18	2.00	0.00	9.91	0.02	0.00	0.20	2.00	0.00	9.90	0.02	0.00
0.22	2.00	0.00	9.89	0.02	0.00	0.24	2.00	0.00	9.88	0.02	0.00
0.30	2.00	0.00	9.85	0.06	0.00	0.30	2.00	0.00	9.85	0.00	0.00
0.30	2.00	0.00	9.85	0.00	0.00	0.32	2.00	0.00	9.84	0.02	0.00
0.34	2.00	0.00	9.83	0.02	0.00	0.36	2.00	0.00	9.82	0.02	0.00
0.38	2.00	0.00	9.81	0.02	0.00	0.40	2.00	0.00	9.80	0.02	0.00
0.42	2.00	0.00	9.79	0.02	0.00	0.44	2.00	0.00	9.78	0.02	0.00
0.46	2.00	0.00	9.77	0.02	0.00	0.48	2.00	0.00	9.76	0.02	0.00
0.50	2.00	0.00	9.75	0.02	0.00	0.52	2.00	0.00	9.74	0.02	0.00
0.54	2.00	0.00	9.73	0.02	0.00	0.56	2.00	0.00	9.72	0.02	0.00
0.58	2.00	0.00	9.71	0.02	0.00	0.60	2.00	0.00	9.70	0.02	0.00
0.62	2.00	0.00	9.69	0.02	0.00	0.64	2.00	0.00	9.68	0.02	0.00
0.66	2.00	0.00	9.67	0.02	0.00	0.68	2.00	0.00	9.66	0.02	0.00
0.70	2.00	0.00	9.65	0.02	0.00	0.72	2.00	0.00	9.64	0.02	0.00
0.74	2.00	0.00	9.63	0.02	0.00	0.76	2.00	0.00	9.62	0.02	0.00
0.78	2.00	0.00	9.61	0.02	0.00	0.80	2.00	0.00	9.60	0.02	0.00
0.82	2.00	0.00	9.59	0.02	0.00	0.84	2.00	0.00	9.58	0.02	0.00
0.87	2.00	0.00	9.57	0.03	0.00	0.88	2.00	0.00	9.56	0.01	0.00
0.90	2.00	0.00	9.55	0.02	0.00	0.92	2.00	0.00	9.54	0.02	0.00
0.94	2.00	0.00	9.53	0.02	0.00	0.96	2.00	0.00	9.52	0.02	0.00
0.99	2.00	0.00	9.51	0.03	0.00	1.00	2.00	0.00	9.50	0.01	0.00
1.09	2.00	0.00	9.46	0.09	0.00	1.09	2.00	0.00	9.46	0.00	0.00
1.09	2.00	0.00	9.46	0.00	0.00	1.09	2.00	0.00	9.46	0.00	0.00
1.11	2.00	0.00	9.45	0.02	0.00	1.13	2.00	0.00	9.44	0.02	0.00
1.14	2.00	0.00	9.43	0.01	0.00	1.17	2.00	0.00	9.41	0.03	0.00
1.18	2.00	0.00	9.41	0.01	0.00	1.20	2.00	0.00	9.40	0.02	0.00
1.22	2.00	0.00	9.39	0.02	0.00	1.24	2.00	0.00	9.38	0.02	0.00
1.26	2.00	0.00	9.37	0.02	0.00	1.28	2.00	0.00	9.36	0.02	0.00
1.30	2.00	0.00	9.35	0.02	0.00	1.32	2.00	0.00	9.34	0.02	0.00
1.34	2.00	0.00	9.33	0.02	0.00	1.36	2.00	0.00	9.32	0.02	0.00
1.38	2.00	0.00	9.31	0.02	0.00	1.40	2.00	0.00	9.30	0.02	0.00
1.42	2.00	0.00	9.29	0.02	0.00	1.44	2.00	0.00	9.28	0.02	0.00
1.46	2.00	0.00	9.27	0.02	0.00	1.48	2.00	0.00	9.26	0.02	0.00
1.50	2.00	0.00	9.25	0.02	0.00	1.52	2.00	0.00	9.24	0.02	0.00
1.54	2.00	0.00	9.23	0.02	0.00	1.56	2.00	0.00	9.22	0.02	0.00
1.58	2.00	0.00	9.21	0.02	0.00	1.60	2.00	0.00	9.20	0.02	0.00
1.62	2.00	0.00	9.19	0.02	0.00	1.64	2.00	0.00	9.18	0.02	0.00
1.66	2.00	0.00	9.17	0.02	0.00	1.68	2.00	0.00	9.16	0.02	0.00
1.70	2.00	0.00	9.15	0.02	0.00	1.72	2.00	0.00	9.14	0.02	0.00
1.74	2.00	0.00	9.13	0.02	0.00	1.78	2.00	0.00	9.11	0.04	0.00
1.78	2.00	0.00	9.11	0.00	0.00	1.80	2.00	0.00	9.10	0.02	0.00
1.82	2.00	0.00	9.09	0.02	0.00	1.84	2.00	0.00	9.08	0.02	0.00
1.86	2.00	0.00	9.07	0.02	0.00	1.88	2.00	0.00	9.06	0.02	0.00
1.90	2.00	0.00	9.05	0.02	0.00	1.92	2.00	0.00	9.04	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
1.94	2.00	0.00	9.03	0.02	0.00	1.96	2.00	0.00	9.02	0.02	0.00
1.98	2.00	0.00	9.01	0.02	0.00	2.00	2.00	0.00	9.00	0.02	0.00
2.08	2.00	0.00	8.96	0.08	0.00	2.08	2.00	0.00	8.96	0.00	0.00
2.08	2.00	0.00	8.96	0.00	0.00	2.10	2.00	0.00	8.95	0.02	0.00
2.12	2.00	0.00	8.94	0.02	0.00	2.14	2.00	0.00	8.93	0.02	0.00
2.16	2.00	0.00	8.92	0.02	0.00	2.18	2.00	0.00	8.91	0.02	0.00
2.20	2.00	0.00	8.90	0.02	0.00	2.22	2.00	0.00	8.89	0.02	0.00
2.24	2.00	0.00	8.88	0.02	0.00	2.26	2.00	0.00	8.87	0.02	0.00
2.28	2.00	0.00	8.86	0.02	0.00	2.30	2.00	0.00	8.85	0.02	0.00
2.32	2.00	0.00	8.84	0.02	0.00	2.34	2.00	0.00	8.83	0.02	0.00
2.36	2.00	0.00	8.82	0.02	0.00	2.38	2.00	0.00	8.81	0.02	0.00
2.40	2.00	0.00	8.80	0.02	0.00	2.42	2.00	0.00	8.79	0.02	0.00
2.44	2.00	0.00	8.78	0.02	0.00	2.46	2.00	0.00	8.77	0.02	0.00
2.48	2.00	0.00	8.76	0.02	0.00	2.50	2.00	0.00	8.75	0.02	0.00
2.52	2.00	0.00	8.74	0.02	0.00	2.54	2.00	0.00	8.73	0.02	0.00
2.56	2.00	0.00	8.72	0.02	0.00	2.58	2.00	0.00	8.71	0.02	0.00
2.60	2.00	0.00	8.70	0.02	0.00	2.62	2.00	0.00	8.69	0.02	0.00
2.64	2.00	0.00	8.68	0.02	0.00	2.66	2.00	0.00	8.67	0.02	0.00
2.68	2.00	0.00	8.66	0.02	0.00	2.70	2.00	0.00	8.65	0.02	0.00
2.72	2.00	0.00	8.64	0.02	0.00	2.74	2.00	0.00	8.63	0.02	0.00
2.76	2.00	0.00	8.62	0.02	0.00	2.78	2.00	0.00	8.61	0.02	0.00
2.81	2.00	0.00	8.60	0.03	0.00	2.82	2.00	0.00	8.59	0.01	0.00
2.84	2.00	0.00	8.58	0.02	0.00	2.86	2.00	0.00	8.57	0.02	0.00
2.88	2.00	0.00	8.56	0.02	0.00	2.90	2.00	0.00	8.55	0.02	0.00
2.92	2.00	0.00	8.54	0.02	0.00	2.94	2.00	0.00	8.53	0.02	0.00
2.96	2.00	0.00	8.52	0.02	0.00	2.98	2.00	0.00	8.51	0.02	0.00
3.00	2.00	0.00	8.50	0.02	0.00	3.02	2.00	0.00	8.49	0.02	0.00
3.04	2.00	0.00	8.48	0.02	0.00	3.06	2.00	0.00	8.47	0.02	0.00
3.08	2.00	0.00	8.46	0.02	0.00	3.10	2.00	0.00	8.45	0.02	0.00
3.12	2.00	0.00	8.44	0.02	0.00	3.14	2.00	0.00	8.43	0.02	0.00
3.16	2.00	0.00	8.42	0.02	0.00	3.18	2.00	0.00	8.41	0.02	0.00
3.20	2.00	0.00	8.40	0.02	0.00	3.22	2.00	0.00	8.39	0.02	0.00
3.24	2.00	0.00	8.38	0.02	0.00	3.26	2.00	0.00	8.37	0.02	0.00
3.28	2.00	0.00	8.36	0.02	0.00	3.30	2.00	0.00	8.35	0.02	0.00
3.32	2.00	0.00	8.34	0.02	0.00	3.34	2.00	0.00	8.33	0.02	0.00
3.36	2.00	0.00	8.32	0.02	0.00	3.38	2.00	0.00	8.31	0.02	0.00
3.40	2.00	0.00	8.30	0.02	0.00	3.42	2.00	0.00	8.29	0.02	0.00
3.44	2.00	0.00	8.28	0.02	0.00	3.46	2.00	0.00	8.27	0.02	0.00
3.48	2.00	0.00	8.26	0.02	0.00	3.50	2.00	0.00	8.25	0.02	0.00
3.52	2.00	0.00	8.24	0.02	0.00	3.54	2.00	0.00	8.23	0.02	0.00
3.56	2.00	0.00	8.22	0.02	0.00	3.58	2.00	0.00	8.21	0.02	0.00
3.60	2.00	0.00	8.20	0.02	0.00	3.63	2.00	0.00	8.19	0.03	0.00
3.64	2.00	0.00	8.18	0.01	0.00	3.66	2.00	0.00	8.17	0.02	0.00
3.68	2.00	0.00	8.16	0.02	0.00	3.70	2.00	0.00	8.15	0.02	0.00
3.72	2.00	0.00	8.14	0.02	0.00	3.74	2.00	0.00	8.13	0.02	0.00
3.76	2.00	0.00	8.12	0.02	0.00	3.78	2.00	0.00	8.11	0.02	0.00
3.80	2.00	0.00	8.10	0.02	0.00	3.82	2.00	0.00	8.09	0.02	0.00
3.84	2.00	0.00	8.08	0.02	0.00	3.86	2.00	0.00	8.07	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
3.88	2.00	0.00	8.06	0.02	0.00	3.90	2.00	0.00	8.05	0.02	0.00
3.92	2.00	0.00	8.04	0.02	0.00	3.94	2.00	0.00	8.03	0.02	0.00
3.96	2.00	0.00	8.02	0.02	0.00	3.98	2.00	0.00	8.01	0.02	0.00
4.00	2.00	0.00	8.00	0.02	0.00	4.02	2.00	0.00	7.99	0.02	0.00
4.04	2.00	0.00	7.98	0.02	0.00	4.07	2.00	0.00	7.97	0.03	0.00
4.08	2.00	0.00	7.96	0.01	0.00	4.10	2.00	0.00	7.95	0.02	0.00
4.12	2.00	0.00	7.94	0.02	0.00	4.14	2.00	0.00	7.93	0.02	0.00
4.26	2.00	0.00	7.87	0.12	0.00	4.26	2.00	0.00	7.87	0.00	0.00
4.26	2.00	0.00	7.87	0.00	0.00	4.26	2.00	0.00	7.87	0.00	0.00
4.26	2.00	0.00	7.87	0.00	0.00	4.28	2.00	0.00	7.86	0.02	0.00
4.30	2.00	0.00	7.85	0.02	0.00	4.32	2.00	0.00	7.84	0.02	0.00
4.34	2.00	0.00	7.83	0.02	0.00	4.36	2.00	0.00	7.82	0.02	0.00
4.38	2.00	0.00	7.81	0.02	0.00	4.40	2.00	0.00	7.80	0.02	0.00
4.42	2.00	0.00	7.79	0.02	0.00	4.44	2.00	0.00	7.78	0.02	0.00
4.46	2.00	0.00	7.77	0.02	0.00	4.48	2.00	0.00	7.76	0.02	0.00
4.50	2.00	0.00	7.75	0.02	0.00	4.52	2.00	0.00	7.74	0.02	0.00
4.54	2.00	0.00	7.73	0.02	0.00	4.56	2.00	0.00	7.72	0.02	0.00
4.58	2.00	0.00	7.71	0.02	0.00	4.60	2.00	0.00	7.70	0.02	0.00
4.62	2.00	0.00	7.69	0.02	0.00	4.64	2.00	0.00	7.68	0.02	0.00
4.66	2.00	0.00	7.67	0.02	0.00	4.68	2.00	0.00	7.66	0.02	0.00
4.70	2.00	0.00	7.65	0.02	0.00	4.72	2.00	0.00	7.64	0.02	0.00
4.74	2.00	0.00	7.63	0.02	0.00	4.76	2.00	0.00	7.62	0.02	0.00
4.78	2.00	0.00	7.61	0.02	0.00	4.80	2.00	0.00	7.60	0.02	0.00
4.82	2.00	0.00	7.59	0.02	0.00	4.84	2.00	0.00	7.58	0.02	0.00
4.86	2.00	0.00	7.57	0.02	0.00	4.88	2.00	0.00	7.56	0.02	0.00
4.90	2.00	0.00	7.55	0.02	0.00	4.92	2.00	0.00	7.54	0.02	0.00
4.94	2.00	0.00	7.53	0.02	0.00	4.96	2.00	0.00	7.52	0.02	0.00
4.98	2.00	0.00	7.51	0.02	0.00	5.01	2.00	0.00	7.50	0.03	0.00
5.02	2.00	0.00	7.49	0.01	0.00	5.04	2.00	0.00	7.48	0.02	0.00
5.06	2.00	0.00	7.47	0.02	0.00	5.08	2.00	0.00	7.46	0.02	0.00
5.10	2.00	0.00	7.45	0.02	0.00	5.12	2.00	0.00	7.44	0.02	0.00
5.14	2.00	0.00	7.43	0.02	0.00	5.16	2.00	0.00	7.42	0.02	0.00
5.18	2.00	0.00	7.41	0.02	0.00	5.20	2.00	0.00	7.40	0.02	0.00
5.22	2.00	0.00	7.39	0.02	0.00	5.24	2.00	0.00	7.38	0.02	0.00
5.26	2.00	0.00	7.37	0.02	0.00	5.28	2.00	0.00	7.36	0.02	0.00
5.30	2.00	0.00	7.35	0.02	0.00	5.32	2.00	0.00	7.34	0.02	0.00
5.34	2.00	0.00	7.33	0.02	0.00	5.36	2.00	0.00	7.32	0.02	0.00
5.38	2.00	0.00	7.31	0.02	0.00	5.40	2.00	0.00	7.30	0.02	0.00
5.42	2.00	0.00	7.29	0.02	0.00	5.44	2.00	0.00	7.28	0.02	0.00
5.46	2.00	0.00	7.27	0.02	0.00	5.48	2.00	0.00	7.26	0.02	0.00
5.50	2.00	0.00	7.25	0.02	0.00	5.52	2.00	0.00	7.24	0.02	0.00
5.54	2.00	0.00	7.23	0.02	0.00	5.56	2.00	0.00	7.22	0.02	0.00
5.58	2.00	0.00	7.21	0.02	0.00	5.60	2.00	0.00	7.20	0.02	0.00
5.62	2.00	0.00	7.19	0.02	0.00	5.64	2.00	0.00	7.18	0.02	0.00
5.66	2.00	0.00	7.17	0.02	0.00	5.68	2.00	0.00	7.16	0.02	0.00
5.70	2.00	0.00	7.15	0.02	0.00	5.72	2.00	0.00	7.14	0.02	0.00
5.74	2.00	0.00	7.13	0.02	0.00	5.76	2.00	0.00	7.12	0.02	0.00
5.78	2.00	0.00	7.11	0.02	0.00	5.80	2.00	0.00	7.10	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
5.82	2.00	0.00	7.09	0.02	0.00	5.84	2.00	0.00	7.08	0.02	0.00
5.86	2.00	0.00	7.07	0.02	0.00	5.88	2.00	0.00	7.06	0.02	0.00
5.90	2.00	0.00	7.05	0.02	0.00	5.92	2.00	0.00	7.04	0.02	0.00
5.94	2.00	0.00	7.03	0.02	0.00	5.97	2.00	0.00	7.02	0.03	0.00
5.98	2.00	0.00	7.01	0.01	0.00	6.00	2.00	0.00	7.00	0.02	0.00
6.02	2.00	0.00	6.99	0.02	0.00	6.04	2.00	0.00	6.98	0.02	0.00
6.06	2.00	0.00	6.97	0.02	0.00	6.08	2.00	0.00	6.96	0.02	0.00
6.10	2.00	0.00	6.95	0.02	0.00	6.12	2.00	0.00	6.94	0.02	0.00
6.14	2.00	0.00	6.93	0.02	0.00	6.16	2.00	0.00	6.92	0.02	0.00
6.18	2.00	0.00	6.91	0.02	0.00	6.20	2.00	0.00	6.90	0.02	0.00
6.22	2.00	0.00	6.89	0.02	0.00	6.24	2.00	0.00	6.88	0.02	0.00
6.26	2.00	0.00	6.87	0.02	0.00	6.28	2.00	0.00	6.86	0.02	0.00
6.30	2.00	0.00	6.85	0.02	0.00	6.32	2.00	0.00	6.84	0.02	0.00
6.34	2.00	0.00	6.83	0.02	0.00	6.36	2.00	0.00	6.82	0.02	0.00
6.38	2.00	0.00	6.81	0.02	0.00	6.41	2.00	0.00	6.80	0.03	0.00
6.42	2.00	0.00	6.79	0.01	0.00	6.44	2.00	0.00	6.78	0.02	0.00
6.46	2.00	0.00	6.77	0.02	0.00	6.48	2.00	0.00	6.76	0.02	0.00
6.50	2.00	0.00	6.75	0.02	0.00	6.52	2.00	0.00	6.74	0.02	0.00
6.54	2.00	0.00	6.73	0.02	0.00	6.56	2.00	0.00	6.72	0.02	0.00
6.58	2.00	0.00	6.71	0.02	0.00	6.60	2.00	0.00	6.70	0.02	0.00
6.62	2.00	0.00	6.69	0.02	0.00	6.64	2.00	0.00	6.68	0.02	0.00
6.66	2.00	0.00	6.67	0.02	0.00	6.68	2.00	0.00	6.66	0.02	0.00
6.70	2.00	0.00	6.65	0.02	0.00	6.72	2.00	0.00	6.64	0.02	0.00
6.74	2.00	0.00	6.63	0.02	0.00	6.76	2.00	0.00	6.62	0.02	0.00
6.78	2.00	0.00	6.61	0.02	0.00	6.81	2.00	0.00	6.60	0.03	0.00
6.82	2.00	0.00	6.59	0.01	0.00	6.84	2.00	0.00	6.58	0.02	0.00
6.87	2.00	0.00	6.57	0.03	0.00	6.88	2.00	0.00	6.56	0.01	0.00
6.90	2.00	0.00	6.55	0.02	0.00	6.92	2.00	0.00	6.54	0.02	0.00
6.94	2.00	0.00	6.53	0.02	0.00	6.96	2.00	0.00	6.52	0.02	0.00
6.98	2.00	0.00	6.51	0.02	0.00	7.00	2.00	0.00	6.50	0.02	0.00
7.02	2.00	0.00	6.49	0.02	0.00	7.04	2.00	0.00	6.48	0.02	0.00
7.06	2.00	0.00	6.47	0.02	0.00	7.08	2.00	0.00	6.46	0.02	0.00
7.10	2.00	0.00	6.45	0.02	0.00	7.12	2.00	0.00	6.44	0.02	0.00
7.15	2.00	0.00	6.43	0.03	0.00	7.16	2.00	0.00	6.42	0.01	0.00
7.18	2.00	0.00	6.41	0.02	0.00	7.20	2.00	0.00	6.40	0.02	0.00
7.30	2.00	0.00	6.35	0.10	0.00	7.30	2.00	0.00	6.35	0.00	0.00
7.30	2.00	0.00	6.35	0.00	0.00	7.32	2.00	0.00	6.34	0.02	0.00
7.34	2.00	0.00	6.33	0.02	0.00	7.36	2.00	0.00	6.32	0.02	0.00
7.38	2.00	0.00	6.31	0.02	0.00	7.40	2.00	0.00	6.30	0.02	0.00
7.42	2.00	0.00	6.29	0.02	0.00	7.44	2.00	0.00	6.28	0.02	0.00
7.46	2.00	0.00	6.27	0.02	0.00	7.48	2.00	0.00	6.26	0.02	0.00
7.50	2.00	0.00	6.25	0.02	0.00	7.52	2.00	0.00	6.24	0.02	0.00
7.54	2.00	0.00	6.23	0.02	0.00	7.56	2.00	0.00	6.22	0.02	0.00
7.58	2.00	0.00	6.21	0.02	0.00	7.60	2.00	0.00	6.20	0.02	0.00
7.62	2.00	0.00	6.19	0.02	0.00	7.64	2.00	0.00	6.18	0.02	0.00
7.66	2.00	0.00	6.17	0.02	0.00	7.68	2.00	0.00	6.16	0.02	0.00
7.70	2.00	0.00	6.15	0.02	0.00	7.72	2.00	0.00	6.14	0.02	0.00
7.74	2.00	0.00	6.13	0.02	0.00	7.76	2.00	0.00	6.12	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
7.78	2.00	0.00	6.11	0.02	0.00	7.80	2.00	0.00	6.10	0.02	0.00
7.83	2.00	0.00	6.09	0.03	0.00	7.84	2.00	0.00	6.08	0.01	0.00
7.86	2.00	0.00	6.07	0.02	0.00	7.88	2.00	0.00	6.06	0.02	0.00
7.90	2.00	0.00	6.05	0.02	0.00	7.93	2.00	0.00	6.04	0.03	0.00
7.94	2.00	0.00	6.03	0.01	0.00	7.96	2.00	0.00	6.02	0.02	0.00
7.98	2.00	0.00	6.01	0.02	0.00	8.00	2.00	0.00	6.00	0.02	0.00
8.02	2.00	0.00	5.99	0.02	0.00	8.04	2.00	0.00	5.98	0.02	0.00
8.06	2.00	0.00	5.97	0.02	0.00	8.08	2.00	0.00	5.96	0.02	0.00
8.10	2.00	0.00	5.95	0.02	0.00	8.12	2.00	0.00	5.94	0.02	0.00
8.14	2.00	0.00	5.93	0.02	0.00	8.16	2.00	0.00	5.92	0.02	0.00
8.18	2.00	0.00	5.91	0.02	0.00	8.20	2.00	0.00	5.90	0.02	0.00
8.22	2.00	0.00	5.89	0.02	0.00	8.24	2.00	0.00	5.88	0.02	0.00
8.26	2.00	0.00	5.87	0.02	0.00	8.28	2.00	0.00	5.86	0.02	0.00
8.30	2.00	0.00	5.85	0.02	0.00	8.32	2.00	0.00	5.84	0.02	0.00
8.34	2.00	0.00	5.83	0.02	0.00	8.36	2.00	0.00	5.82	0.02	0.00
8.38	2.00	0.00	5.81	0.02	0.00	8.40	2.00	0.00	5.80	0.02	0.00
8.43	2.00	0.00	5.79	0.03	0.00	8.44	2.00	0.00	5.78	0.01	0.00
8.46	2.00	0.00	5.77	0.02	0.00	8.48	2.00	0.00	5.76	0.02	0.00
8.50	2.00	0.00	5.75	0.02	0.00	8.52	2.00	0.00	5.74	0.02	0.00
8.54	2.00	0.00	5.73	0.02	0.00	8.56	2.00	0.00	5.72	0.02	0.00
8.58	2.00	0.00	5.71	0.02	0.00	8.60	2.00	0.00	5.70	0.02	0.00
8.62	2.00	0.00	5.69	0.02	0.00	8.64	2.00	0.00	5.68	0.02	0.00
8.66	2.00	0.00	5.67	0.02	0.00	8.68	2.00	0.00	5.66	0.02	0.00
8.70	2.00	0.00	5.65	0.02	0.00	8.72	2.00	0.00	5.64	0.02	0.00
8.74	2.00	0.00	5.63	0.02	0.00	8.76	2.00	0.00	5.62	0.02	0.00
8.78	2.00	0.00	5.61	0.02	0.00	8.80	2.00	0.00	5.60	0.02	0.00
8.82	2.00	0.00	5.59	0.02	0.00	8.84	2.00	0.00	5.58	0.02	0.00
8.86	2.00	0.00	5.57	0.02	0.00	8.88	2.00	0.00	5.56	0.02	0.00
8.90	2.00	0.00	5.55	0.02	0.00	8.92	2.00	0.00	5.54	0.02	0.00
8.94	2.00	0.00	5.53	0.02	0.00	8.96	2.00	0.00	5.52	0.02	0.00
8.98	2.00	0.00	5.51	0.02	0.00	9.00	2.00	0.00	5.50	0.02	0.00
9.02	2.00	0.00	5.49	0.02	0.00	9.05	2.00	0.00	5.47	0.03	0.00
9.06	2.00	0.00	5.47	0.01	0.00	9.08	2.00	0.00	5.46	0.02	0.00
9.10	2.00	0.00	5.45	0.02	0.00	9.12	2.00	0.00	5.44	0.02	0.00
9.14	2.00	0.00	5.43	0.02	0.00	9.16	2.00	0.00	5.42	0.02	0.00
9.18	2.00	0.00	5.41	0.02	0.00	9.21	2.00	0.00	5.39	0.03	0.00
9.22	2.00	0.00	5.39	0.01	0.00	9.24	2.00	0.00	5.38	0.02	0.00
9.26	2.00	0.00	5.37	0.02	0.00	9.28	2.00	0.00	5.36	0.02	0.00
9.30	2.00	0.00	5.35	0.02	0.00	9.32	2.00	0.00	5.34	0.02	0.00
9.34	2.00	0.00	5.33	0.02	0.00	9.36	2.00	0.00	5.32	0.02	0.00
9.38	2.00	0.00	5.31	0.02	0.00	9.40	2.00	0.00	5.30	0.02	0.00
9.42	2.00	0.00	5.29	0.02	0.00	9.44	2.00	0.00	5.28	0.02	0.00
9.47	2.00	0.00	5.27	0.03	0.00	9.48	2.00	0.00	5.26	0.01	0.00
9.50	2.00	0.00	5.25	0.02	0.00	9.53	2.00	0.00	5.24	0.03	0.00
9.54	2.00	0.00	5.23	0.01	0.00	9.56	2.00	0.00	5.22	0.02	0.00
9.58	2.00	0.00	5.21	0.02	0.00	9.60	2.00	0.00	5.20	0.02	0.00
9.62	2.00	0.00	5.19	0.02	0.00	9.64	2.00	0.00	5.18	0.02	0.00
9.66	2.00	0.00	5.17	0.02	0.00	9.68	2.00	0.00	5.16	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
9.70	2.00	0.00	5.15	0.02	0.00	9.72	2.00	0.00	5.14	0.02	0.00
9.74	2.00	0.00	5.13	0.02	0.00	9.76	2.00	0.00	5.12	0.02	0.00
9.79	2.00	0.00	5.11	0.03	0.00	9.80	2.00	0.00	5.10	0.01	0.00
9.82	2.00	0.00	5.09	0.02	0.00	9.85	2.00	0.00	5.08	0.03	0.00
9.86	2.00	0.00	5.07	0.01	0.00	9.88	2.00	0.00	5.06	0.02	0.00
9.90	2.00	0.00	5.05	0.02	0.00	9.92	2.00	0.00	5.04	0.02	0.00
9.94	2.00	0.00	5.03	0.02	0.00	9.96	2.00	0.00	5.02	0.02	0.00
9.98	2.00	0.00	5.01	0.02	0.00	10.00	2.00	0.00	5.00	0.02	0.00
10.02	2.00	0.00	4.99	0.02	0.00	10.04	2.00	0.00	4.98	0.02	0.00
10.06	2.00	0.00	4.97	0.02	0.00	10.08	2.00	0.00	4.96	0.02	0.00
10.11	2.00	0.00	4.95	0.03	0.00	10.12	2.00	0.00	4.94	0.01	0.00
10.14	2.00	0.00	4.93	0.02	0.00	10.16	2.00	0.00	4.92	0.02	0.00
10.18	2.00	0.00	4.91	0.02	0.00	10.20	2.00	0.00	4.90	0.02	0.00
10.22	2.00	0.00	4.89	0.02	0.00	10.24	2.00	0.00	4.88	0.02	0.00
10.26	2.00	0.00	4.87	0.02	0.00	10.28	2.00	0.00	4.86	0.02	0.00
10.30	2.00	0.00	4.85	0.02	0.00	10.32	2.00	0.00	4.84	0.02	0.00
10.34	2.00	0.00	4.83	0.02	0.00	10.36	2.00	0.00	4.82	0.02	0.00
10.38	2.00	0.00	4.81	0.02	0.00	10.40	2.00	0.00	4.80	0.02	0.00
10.42	2.00	0.00	4.79	0.02	0.00	10.44	2.00	0.00	4.78	0.02	0.00
10.46	2.00	0.00	4.77	0.02	0.00	10.48	2.00	0.00	4.76	0.02	0.00
10.50	2.00	0.00	4.75	0.02	0.00	10.52	2.00	0.00	4.74	0.02	0.00
10.54	2.00	0.00	4.73	0.02	0.00	10.56	2.00	0.00	4.72	0.02	0.00
10.58	2.00	0.00	4.71	0.02	0.00	10.60	2.00	0.00	4.70	0.02	0.00
10.62	2.00	0.00	4.69	0.02	0.00	10.64	2.00	0.00	4.68	0.02	0.00
10.66	2.00	0.00	4.67	0.02	0.00	10.70	2.00	0.00	4.65	0.04	0.00
10.70	2.00	0.00	4.65	0.00	0.00	10.72	2.00	0.00	4.64	0.02	0.00
10.75	2.00	0.00	4.63	0.03	0.00	10.76	2.00	0.00	4.62	0.01	0.00
10.78	2.00	0.00	4.61	0.02	0.00	10.80	2.00	0.00	4.60	0.02	0.00
10.82	2.00	0.00	4.59	0.02	0.00	10.84	2.00	0.00	4.58	0.02	0.00
10.86	2.00	0.00	4.57	0.02	0.00	10.88	2.00	0.00	4.56	0.02	0.00
10.90	2.00	0.00	4.55	0.02	0.00	10.92	2.00	0.00	4.54	0.02	0.00
10.94	2.00	0.00	4.53	0.02	0.00	10.96	2.00	0.00	4.52	0.02	0.00
10.98	2.00	0.00	4.51	0.02	0.00	11.00	2.00	0.00	4.50	0.02	0.00
11.02	2.00	0.00	4.49	0.02	0.00	11.06	2.00	0.00	4.47	0.04	0.00
11.06	2.00	0.00	4.47	0.00	0.00	11.08	2.00	0.00	4.46	0.02	0.00
11.10	2.00	0.00	4.45	0.02	0.00	11.12	2.00	0.00	4.44	0.02	0.00
11.14	2.00	0.00	4.43	0.02	0.00	11.16	2.00	0.00	4.42	0.02	0.00
11.18	2.00	0.00	4.41	0.02	0.00	11.20	2.00	0.00	4.40	0.02	0.00
11.23	2.00	0.00	4.39	0.03	0.00	11.24	2.00	0.00	4.38	0.01	0.00
11.26	2.00	0.00	4.37	0.02	0.00	11.28	2.00	0.00	4.36	0.02	0.00
11.30	2.00	0.00	4.35	0.02	0.00	11.32	2.00	0.00	4.34	0.02	0.00
11.34	2.00	0.00	4.33	0.02	0.00	11.36	2.00	0.00	4.32	0.02	0.00
11.38	2.00	0.00	4.31	0.02	0.00	11.40	2.00	0.00	4.30	0.02	0.00
11.42	2.00	0.00	4.29	0.02	0.00	11.44	2.00	0.00	4.28	0.02	0.00
11.46	2.00	0.00	4.27	0.02	0.00	11.48	2.00	0.00	4.26	0.02	0.00
11.50	2.00	0.00	4.25	0.02	0.00	11.52	2.00	0.00	4.24	0.02	0.00
11.54	2.00	0.00	4.23	0.02	0.00	11.56	2.00	0.00	4.22	0.02	0.00
11.58	2.00	0.00	4.21	0.02	0.00	11.60	2.00	0.00	4.20	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
11.62	2.00	0.00	4.19	0.02	0.00	11.64	2.00	0.00	4.18	0.02	0.00
11.66	2.00	0.00	4.17	0.02	0.00	11.68	2.00	0.00	4.16	0.02	0.00
11.70	2.00	0.00	4.15	0.02	0.00	11.72	2.00	0.00	4.14	0.02	0.00
11.74	2.00	0.00	4.13	0.02	0.00	11.76	2.00	0.00	4.12	0.02	0.00
11.78	2.00	0.00	4.11	0.02	0.00	11.80	2.00	0.00	4.10	0.02	0.00
11.82	2.00	0.00	4.09	0.02	0.00	11.84	2.00	0.00	4.08	0.02	0.00
11.87	2.00	0.00	4.07	0.03	0.00	11.88	2.00	0.00	4.06	0.01	0.00
11.90	2.00	0.00	4.05	0.02	0.00	11.92	2.00	0.00	4.04	0.02	0.00
11.94	2.00	0.00	4.03	0.02	0.00	11.96	2.00	0.00	4.02	0.02	0.00
11.98	2.00	0.00	4.01	0.02	0.00	12.00	2.00	0.00	4.00	0.02	0.00
12.02	2.00	0.00	3.99	0.02	0.00	12.04	2.00	0.00	3.98	0.02	0.00
12.06	2.00	0.00	3.97	0.02	0.00	12.08	2.00	0.00	3.96	0.02	0.00
12.10	2.00	0.00	3.95	0.02	0.00	12.12	2.00	0.00	3.94	0.02	0.00
12.14	2.00	0.00	3.93	0.02	0.00	12.16	2.00	0.00	3.92	0.02	0.00
12.18	2.00	0.00	3.91	0.02	0.00	12.20	2.00	0.00	3.90	0.02	0.00
12.22	2.00	0.00	3.89	0.02	0.00	12.24	2.00	0.00	3.88	0.02	0.00
12.26	2.00	0.00	3.87	0.02	0.00	12.28	2.00	0.00	3.86	0.02	0.00
12.30	2.00	0.00	3.85	0.02	0.00	12.32	2.00	0.00	3.84	0.02	0.00
12.34	2.00	0.00	3.83	0.02	0.00	12.36	2.00	0.00	3.82	0.02	0.00
12.38	2.00	0.00	3.81	0.02	0.00	12.40	2.00	0.00	3.80	0.02	0.00
12.42	2.00	0.00	3.79	0.02	0.00	12.44	2.00	0.00	3.78	0.02	0.00
12.46	2.00	0.00	3.77	0.02	0.00	12.48	2.00	0.00	3.76	0.02	0.00
12.51	2.00	0.00	3.75	0.03	0.00	12.52	2.00	0.00	3.74	0.01	0.00
12.54	2.00	0.00	3.73	0.02	0.00	12.56	2.00	0.00	3.72	0.02	0.00
12.58	2.00	0.00	3.71	0.02	0.00	12.60	2.00	0.00	3.70	0.02	0.00
12.62	2.00	0.00	3.69	0.02	0.00	12.64	2.00	0.00	3.68	0.02	0.00
12.66	2.00	0.00	3.67	0.02	0.00	12.68	2.00	0.00	3.66	0.02	0.00
12.70	2.00	0.00	3.65	0.02	0.00	12.72	2.00	0.00	3.64	0.02	0.00
12.75	2.00	0.00	3.63	0.03	0.00	12.76	2.00	0.00	3.62	0.01	0.00
12.78	2.00	0.00	3.61	0.02	0.00	12.80	2.00	0.00	3.60	0.02	0.00
12.82	2.00	0.00	3.59	0.02	0.00	12.84	2.00	0.00	3.58	0.02	0.00
12.86	2.00	0.00	3.57	0.02	0.00	12.88	2.00	0.00	3.56	0.02	0.00
12.90	2.00	0.00	3.55	0.02	0.00	12.92	2.00	0.00	3.54	0.02	0.00
12.94	2.00	0.00	3.53	0.02	0.00	12.96	2.00	0.00	3.52	0.02	0.00
12.98	2.00	0.00	3.51	0.02	0.00	13.01	2.00	0.00	3.50	0.03	0.00
13.02	2.00	0.00	3.49	0.01	0.00	13.04	2.00	0.00	3.48	0.02	0.00
13.06	2.00	0.00	3.47	0.02	0.00	13.08	2.00	0.00	3.46	0.02	0.00
13.10	2.00	0.00	3.45	0.02	0.00	13.12	2.00	0.00	3.44	0.02	0.00
13.14	2.00	0.00	3.43	0.02	0.00	13.16	2.00	0.00	3.42	0.02	0.00
13.18	2.00	0.00	3.41	0.02	0.00	13.20	2.00	0.00	3.40	0.02	0.00
13.23	2.00	0.00	3.39	0.03	0.00	13.24	2.00	0.00	3.38	0.01	0.00
13.26	2.00	0.00	3.37	0.02	0.00	13.29	2.00	0.00	3.36	0.03	0.00
13.30	2.00	0.00	3.35	0.01	0.00	13.32	2.00	0.00	3.34	0.02	0.00
13.34	2.00	0.00	3.33	0.02	0.00	13.36	2.00	0.00	3.32	0.02	0.00
13.38	2.00	0.00	3.31	0.02	0.00	13.40	2.00	0.00	3.30	0.02	0.00
13.42	2.00	0.00	3.29	0.02	0.00	13.44	2.00	0.00	3.28	0.02	0.00
13.46	2.00	0.00	3.27	0.02	0.00	13.48	2.00	0.00	3.26	0.02	0.00
13.50	2.00	0.00	3.25	0.02	0.00	13.52	2.00	0.00	3.24	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
13.54	2.00	0.00	3.23	0.02	0.00	13.56	2.00	0.00	3.22	0.02	0.00
13.58	2.00	0.00	3.21	0.02	0.00	13.60	2.00	0.00	3.20	0.02	0.00
13.62	2.00	0.00	3.19	0.02	0.00	13.64	2.00	0.00	3.18	0.02	0.00
13.66	2.00	0.00	3.17	0.02	0.00	13.68	2.00	0.00	3.16	0.02	0.00
13.70	2.00	0.00	3.15	0.02	0.00	13.72	2.00	0.00	3.14	0.02	0.00
13.74	2.00	0.00	3.13	0.02	0.00	13.76	2.00	0.00	3.12	0.02	0.00
13.78	2.00	0.00	3.11	0.02	0.00	13.80	2.00	0.00	3.10	0.02	0.00
13.82	2.00	0.00	3.09	0.02	0.00	13.85	2.00	0.00	3.08	0.03	0.00
13.86	2.00	0.00	3.07	0.01	0.00	13.88	2.00	0.00	3.06	0.02	0.00
13.90	2.00	0.00	3.05	0.02	0.00	13.92	2.00	0.00	3.04	0.02	0.00
13.94	2.00	0.00	3.03	0.02	0.00	13.96	2.00	0.00	3.02	0.02	0.00
13.98	2.00	0.00	3.01	0.02	0.00	14.00	2.00	0.00	3.00	0.02	0.00
14.02	2.00	0.00	2.99	0.02	0.00	14.04	2.00	0.00	2.98	0.02	0.00
14.06	2.00	0.00	2.97	0.02	0.00	14.08	2.00	0.00	2.96	0.02	0.00

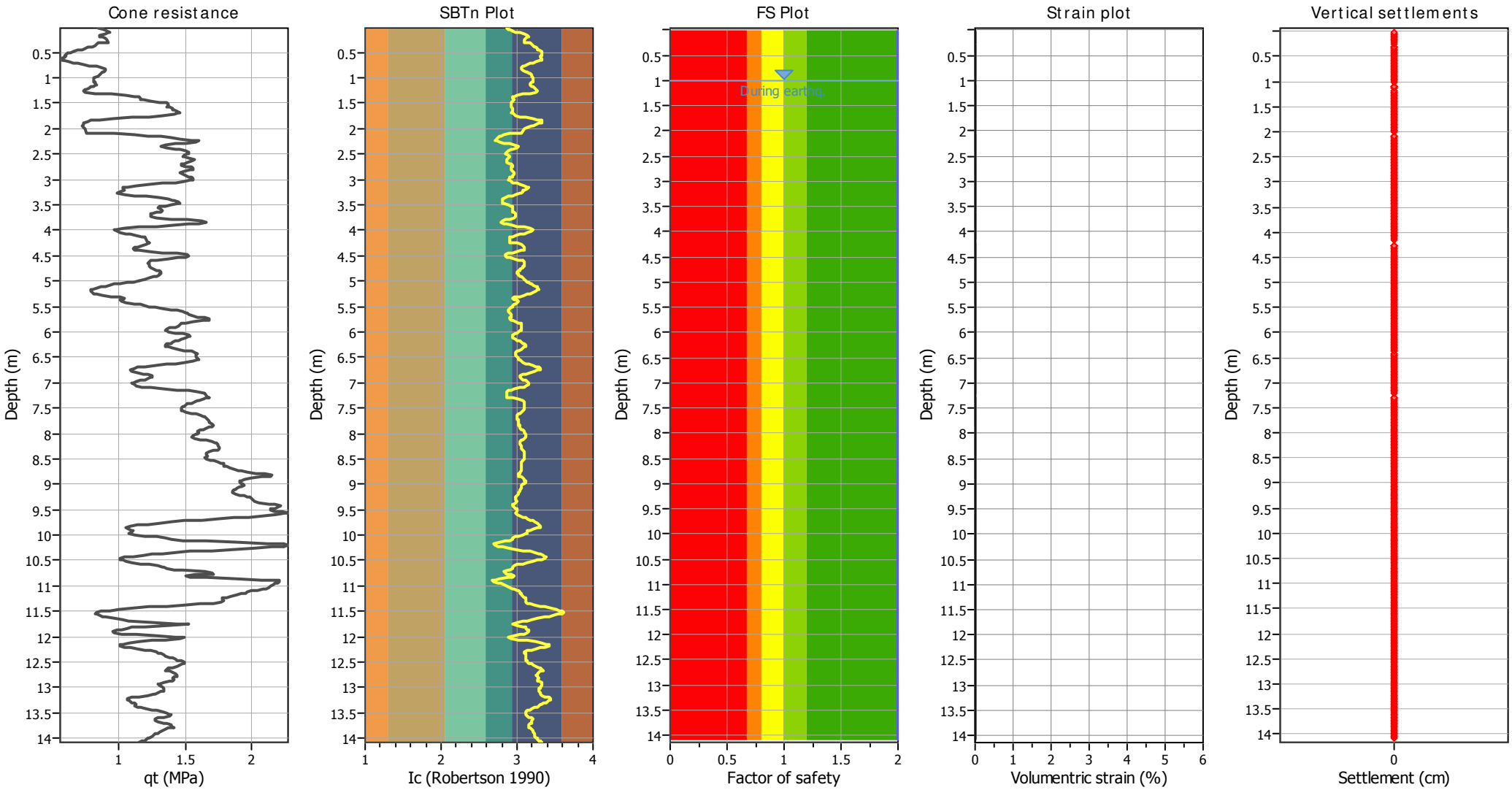
Overall liquefaction potential: 0.00

LPI = 0.00 - Liquefaction risk very low
LPI between 0.00 and 5.00 - Liquefaction risk low
LPI between 5.00 and 15.00 - Liquefaction risk high
LPI > 15.00 - Liquefaction risk very high

Abbreviations

FS: Calculated factor of safety for test point
F_L: 1 - FS
w_z: Function value of the extend of soil liquefaction according to depth
d_z: Layer thickness (m)
LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

q_t:	Total cone resistance (cone resistance q_c corrected for pore water effects)
I_c:	Soil Behaviour Type Index
FS:	Calculated Factor of Safety against liquefaction
Volumentric strain:	Post-liquefaction volumentric strain

:: Post-earthquake settlement due to soil liquefaction ::

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
1.00	13.20	2.00	0.00	1.00	0.00	1.09	13.69	2.00	0.00	1.00	0.00
1.09	13.69	2.00	0.00	1.00	0.00	1.09	13.81	2.00	0.00	1.00	0.00
1.09	13.81	2.00	0.00	1.00	0.00	1.11	13.78	2.00	0.00	1.00	0.00
1.13	13.87	2.00	0.00	1.00	0.00	1.14	14.14	2.00	0.00	1.00	0.00
1.17	13.49	2.00	0.00	1.00	0.00	1.18	13.24	2.00	0.00	1.00	0.00
1.20	12.87	2.00	0.00	1.00	0.00	1.22	12.85	2.00	0.00	1.00	0.00
1.24	12.28	2.00	0.00	1.00	0.00	1.26	12.15	2.00	0.00	1.00	0.00
1.28	12.13	2.00	0.00	1.00	0.00	1.30	13.08	2.00	0.00	1.00	0.00
1.32	15.99	2.00	0.00	1.00	0.00	1.34	17.95	2.00	0.00	1.00	0.00
1.36	18.67	2.00	0.00	1.00	0.00	1.38	19.24	2.00	0.00	1.00	0.00
1.40	19.49	2.00	0.00	1.00	0.00	1.42	19.27	2.00	0.00	1.00	0.00
1.44	19.25	2.00	0.00	1.00	0.00	1.46	20.48	2.00	0.00	1.00	0.00
1.48	22.15	2.00	0.00	1.00	0.00	1.50	22.88	2.00	0.00	1.00	0.00
1.52	23.09	2.00	0.00	1.00	0.00	1.54	22.72	2.00	0.00	1.00	0.00
1.56	22.70	2.00	0.00	1.00	0.00	1.58	22.95	2.00	0.00	1.00	0.00
1.60	23.44	2.00	0.00	1.00	0.00	1.62	23.53	2.00	0.00	1.00	0.00
1.64	23.31	2.00	0.00	1.00	0.00	1.66	24.07	2.00	0.00	1.00	0.00
1.68	24.60	2.00	0.00	1.00	0.00	1.70	24.46	2.00	0.00	1.00	0.00
1.72	23.48	2.00	0.00	1.00	0.00	1.74	22.63	2.00	0.00	1.00	0.00
1.78	20.51	2.00	0.00	1.00	0.00	1.78	18.21	2.00	0.00	1.00	0.00
1.80	15.99	2.00	0.00	1.00	0.00	1.82	13.24	2.00	0.00	1.00	0.00
1.84	13.21	2.00	0.00	1.00	0.00	1.86	12.15	2.00	0.00	1.00	0.00
1.88	11.99	2.00	0.00	1.00	0.00	1.90	11.71	2.00	0.00	1.00	0.00
1.92	11.78	2.00	0.00	1.00	0.00	1.94	11.69	2.00	0.00	1.00	0.00
1.96	11.53	2.00	0.00	1.00	0.00	1.98	11.48	2.00	0.00	1.00	0.00
2.00	12.25	2.00	0.00	1.00	0.00	2.08	12.29	2.00	0.00	1.00	0.00
2.08	12.29	2.00	0.00	1.00	0.00	2.08	12.29	2.00	0.00	1.00	0.00
2.10	16.43	2.00	0.00	1.00	0.00	2.12	17.87	2.00	0.00	1.00	0.00
2.14	20.10	2.00	0.00	1.00	0.00	2.16	21.54	2.00	0.00	1.00	0.00
2.18	22.46	2.00	0.00	1.00	0.00	2.20	23.91	2.00	0.00	1.00	0.00
2.22	25.38	2.00	0.00	1.00	0.00	2.24	26.41	2.00	0.00	1.00	0.00
2.26	25.83	2.00	0.00	1.00	0.00	2.28	24.45	2.00	0.00	1.00	0.00
2.30	22.72	2.00	0.00	1.00	0.00	2.32	21.92	2.00	0.00	1.00	0.00
2.34	20.81	2.00	0.00	1.00	0.00	2.36	20.58	2.00	0.00	1.00	0.00
2.38	21.84	2.00	0.00	1.00	0.00	2.40	22.24	2.00	0.00	1.00	0.00
2.42	23.11	2.00	0.00	1.00	0.00	2.44	23.65	2.00	0.00	1.00	0.00
2.46	23.91	2.00	0.00	1.00	0.00	2.48	24.03	2.00	0.00	1.00	0.00
2.50	23.78	2.00	0.00	1.00	0.00	2.52	23.35	2.00	0.00	1.00	0.00
2.54	22.79	2.00	0.00	1.00	0.00	2.56	22.92	2.00	0.00	1.00	0.00
2.58	23.63	2.00	0.00	1.00	0.00	2.60	24.43	2.00	0.00	1.00	0.00
2.62	24.54	2.00	0.00	1.00	0.00	2.64	23.81	2.00	0.00	1.00	0.00
2.66	23.46	2.00	0.00	1.00	0.00	2.68	23.00	2.00	0.00	1.00	0.00
2.70	22.41	2.00	0.00	1.00	0.00	2.72	22.16	2.00	0.00	1.00	0.00
2.74	23.16	2.00	0.00	1.00	0.00	2.76	23.41	2.00	0.00	1.00	0.00
2.78	23.83	2.00	0.00	1.00	0.00	2.81	23.50	2.00	0.00	1.00	0.00
2.82	23.41	2.00	0.00	1.00	0.00	2.84	22.64	2.00	0.00	1.00	0.00
2.86	21.88	2.00	0.00	1.00	0.00	2.88	21.79	2.00	0.00	1.00	0.00
2.90	22.25	2.00	0.00	1.00	0.00	2.92	22.54	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
2.94	23.00	2.00	0.00	1.00	0.00	2.96	23.05	2.00	0.00	1.00	0.00
2.98	23.29	2.00	0.00	1.00	0.00	3.00	23.37	2.00	0.00	1.00	0.00
3.02	22.95	2.00	0.00	1.00	0.00	3.04	22.11	2.00	0.00	1.00	0.00
3.06	21.21	2.00	0.00	1.00	0.00	3.08	19.95	2.00	0.00	1.00	0.00
3.10	17.80	2.00	0.00	1.00	0.00	3.12	16.73	2.00	0.00	1.00	0.00
3.14	15.61	2.00	0.00	1.00	0.00	3.16	14.95	2.00	0.00	1.00	0.00
3.18	15.04	2.00	0.00	1.00	0.00	3.20	15.37	2.00	0.00	1.00	0.00
3.22	15.29	2.00	0.00	1.00	0.00	3.24	14.84	2.00	0.00	1.00	0.00
3.26	14.03	2.00	0.00	1.00	0.00	3.28	14.30	2.00	0.00	1.00	0.00
3.30	14.67	2.00	0.00	1.00	0.00	3.32	16.24	2.00	0.00	1.00	0.00
3.34	17.05	2.00	0.00	1.00	0.00	3.36	18.69	2.00	0.00	1.00	0.00
3.38	20.11	2.00	0.00	1.00	0.00	3.40	20.40	2.00	0.00	1.00	0.00
3.42	20.13	2.00	0.00	1.00	0.00	3.44	20.65	2.00	0.00	1.00	0.00
3.46	21.39	2.00	0.00	1.00	0.00	3.48	20.36	2.00	0.00	1.00	0.00
3.50	20.18	2.00	0.00	1.00	0.00	3.52	18.95	2.00	0.00	1.00	0.00
3.54	18.39	2.00	0.00	1.00	0.00	3.56	18.28	2.00	0.00	1.00	0.00
3.58	18.51	2.00	0.00	1.00	0.00	3.60	19.03	2.00	0.00	1.00	0.00
3.63	18.91	2.00	0.00	1.00	0.00	3.64	17.98	2.00	0.00	1.00	0.00
3.66	17.84	2.00	0.00	1.00	0.00	3.68	17.48	2.00	0.00	1.00	0.00
3.70	17.41	2.00	0.00	1.00	0.00	3.72	17.60	2.00	0.00	1.00	0.00
3.74	17.18	2.00	0.00	1.00	0.00	3.76	17.66	2.00	0.00	1.00	0.00
3.78	19.07	2.00	0.00	1.00	0.00	3.80	21.42	2.00	0.00	1.00	0.00
3.82	22.54	2.00	0.00	1.00	0.00	3.84	23.13	2.00	0.00	1.00	0.00
3.86	22.83	2.00	0.00	1.00	0.00	3.88	20.67	2.00	0.00	1.00	0.00
3.90	19.80	2.00	0.00	1.00	0.00	3.92	17.92	2.00	0.00	1.00	0.00
3.94	15.84	2.00	0.00	1.00	0.00	3.96	13.99	2.00	0.00	1.00	0.00
3.98	13.17	2.00	0.00	1.00	0.00	4.00	12.79	2.00	0.00	1.00	0.00
4.02	12.86	2.00	0.00	1.00	0.00	4.04	13.49	2.00	0.00	1.00	0.00
4.07	13.68	2.00	0.00	1.00	0.00	4.08	14.29	2.00	0.00	1.00	0.00
4.10	15.26	2.00	0.00	1.00	0.00	4.12	15.78	2.00	0.00	1.00	0.00
4.14	16.16	2.00	0.00	1.00	0.00	4.26	16.32	2.00	0.00	1.00	0.00
4.26	16.32	2.00	0.00	1.00	0.00	4.26	16.29	2.00	0.00	1.00	0.00
4.26	16.28	2.00	0.00	1.00	0.00	4.26	16.46	2.00	0.00	1.00	0.00
4.28	16.17	2.00	0.00	1.00	0.00	4.30	15.45	2.00	0.00	1.00	0.00
4.32	14.95	2.00	0.00	1.00	0.00	4.34	14.76	2.00	0.00	1.00	0.00
4.36	14.36	2.00	0.00	1.00	0.00	4.38	14.33	2.00	0.00	1.00	0.00
4.40	14.85	2.00	0.00	1.00	0.00	4.42	15.66	2.00	0.00	1.00	0.00
4.44	17.14	2.00	0.00	1.00	0.00	4.46	18.71	2.00	0.00	1.00	0.00
4.48	20.17	2.00	0.00	1.00	0.00	4.50	19.91	2.00	0.00	1.00	0.00
4.52	19.56	2.00	0.00	1.00	0.00	4.54	19.52	2.00	0.00	1.00	0.00
4.56	17.87	2.00	0.00	1.00	0.00	4.58	16.71	2.00	0.00	1.00	0.00
4.60	16.19	2.00	0.00	1.00	0.00	4.62	15.95	2.00	0.00	1.00	0.00
4.64	15.82	2.00	0.00	1.00	0.00	4.66	15.73	2.00	0.00	1.00	0.00
4.68	16.06	2.00	0.00	1.00	0.00	4.70	15.84	2.00	0.00	1.00	0.00
4.72	15.60	2.00	0.00	1.00	0.00	4.74	15.90	2.00	0.00	1.00	0.00
4.76	15.93	2.00	0.00	1.00	0.00	4.78	16.03	2.00	0.00	1.00	0.00
4.80	16.40	2.00	0.00	1.00	0.00	4.82	16.77	2.00	0.00	1.00	0.00
4.84	16.68	2.00	0.00	1.00	0.00	4.86	16.54	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
4.88	16.48	2.00	0.00	1.00	0.00	4.90	16.22	2.00	0.00	1.00	0.00
4.92	15.86	2.00	0.00	1.00	0.00	4.94	15.66	2.00	0.00	1.00	0.00
4.96	14.98	2.00	0.00	1.00	0.00	4.98	14.47	2.00	0.00	1.00	0.00
5.01	14.31	2.00	0.00	1.00	0.00	5.02	13.49	2.00	0.00	1.00	0.00
5.04	12.79	2.00	0.00	1.00	0.00	5.06	12.26	2.00	0.00	1.00	0.00
5.08	11.56	2.00	0.00	1.00	0.00	5.10	11.21	2.00	0.00	1.00	0.00
5.12	10.54	2.00	0.00	1.00	0.00	5.14	10.17	2.00	0.00	1.00	0.00
5.16	9.64	2.00	0.00	1.00	0.00	5.18	9.39	2.00	0.00	1.00	0.00
5.20	9.31	2.00	0.00	1.00	0.00	5.22	9.59	2.00	0.00	1.00	0.00
5.24	9.61	2.00	0.00	1.00	0.00	5.26	9.86	2.00	0.00	1.00	0.00
5.28	10.22	2.00	0.00	1.00	0.00	5.30	11.29	2.00	0.00	1.00	0.00
5.32	12.12	2.00	0.00	1.00	0.00	5.34	12.80	2.00	0.00	1.00	0.00
5.36	12.64	2.00	0.00	1.00	0.00	5.38	12.11	2.00	0.00	1.00	0.00
5.40	11.92	2.00	0.00	1.00	0.00	5.42	12.49	2.00	0.00	1.00	0.00
5.44	13.34	2.00	0.00	1.00	0.00	5.46	13.96	2.00	0.00	1.00	0.00
5.48	14.59	2.00	0.00	1.00	0.00	5.50	14.80	2.00	0.00	1.00	0.00
5.52	15.07	2.00	0.00	1.00	0.00	5.54	15.98	2.00	0.00	1.00	0.00
5.56	16.68	2.00	0.00	1.00	0.00	5.58	17.46	2.00	0.00	1.00	0.00
5.60	17.86	2.00	0.00	1.00	0.00	5.62	18.35	2.00	0.00	1.00	0.00
5.64	18.55	2.00	0.00	1.00	0.00	5.66	18.36	2.00	0.00	1.00	0.00
5.68	18.84	2.00	0.00	1.00	0.00	5.70	19.40	2.00	0.00	1.00	0.00
5.72	19.69	2.00	0.00	1.00	0.00	5.74	20.53	2.00	0.00	1.00	0.00
5.76	20.64	2.00	0.00	1.00	0.00	5.78	19.64	2.00	0.00	1.00	0.00
5.80	19.00	2.00	0.00	1.00	0.00	5.82	17.97	2.00	0.00	1.00	0.00
5.84	17.72	2.00	0.00	1.00	0.00	5.86	17.50	2.00	0.00	1.00	0.00
5.88	17.52	2.00	0.00	1.00	0.00	5.90	17.05	2.00	0.00	1.00	0.00
5.92	16.57	2.00	0.00	1.00	0.00	5.94	16.04	2.00	0.00	1.00	0.00
5.97	16.14	2.00	0.00	1.00	0.00	5.98	15.92	2.00	0.00	1.00	0.00
6.00	15.98	2.00	0.00	1.00	0.00	6.02	16.42	2.00	0.00	1.00	0.00
6.04	17.38	2.00	0.00	1.00	0.00	6.06	17.71	2.00	0.00	1.00	0.00
6.08	18.10	2.00	0.00	1.00	0.00	6.10	18.13	2.00	0.00	1.00	0.00
6.12	17.54	2.00	0.00	1.00	0.00	6.14	17.27	2.00	0.00	1.00	0.00
6.16	17.15	2.00	0.00	1.00	0.00	6.18	16.58	2.00	0.00	1.00	0.00
6.20	16.61	2.00	0.00	1.00	0.00	6.22	16.33	2.00	0.00	1.00	0.00
6.24	16.14	2.00	0.00	1.00	0.00	6.26	15.57	2.00	0.00	1.00	0.00
6.28	15.57	2.00	0.00	1.00	0.00	6.30	16.01	2.00	0.00	1.00	0.00
6.32	16.28	2.00	0.00	1.00	0.00	6.34	16.50	2.00	0.00	1.00	0.00
6.36	17.29	2.00	0.00	1.00	0.00	6.38	17.72	2.00	0.00	1.00	0.00
6.41	18.28	2.00	0.00	1.00	0.00	6.42	18.21	2.00	0.00	1.00	0.00
6.44	18.26	2.00	0.00	1.00	0.00	6.46	18.10	2.00	0.00	1.00	0.00
6.48	18.09	2.00	0.00	1.00	0.00	6.50	18.20	2.00	0.00	1.00	0.00
6.52	18.34	2.00	0.00	1.00	0.00	6.54	18.39	2.00	0.00	1.00	0.00
6.56	18.47	2.00	0.00	1.00	0.00	6.58	17.96	2.00	0.00	1.00	0.00
6.60	17.10	2.00	0.00	1.00	0.00	6.62	16.37	2.00	0.00	1.00	0.00
6.64	15.84	2.00	0.00	1.00	0.00	6.66	14.55	2.00	0.00	1.00	0.00
6.68	13.56	2.00	0.00	1.00	0.00	6.70	13.00	2.00	0.00	1.00	0.00
6.72	12.68	2.00	0.00	1.00	0.00	6.74	12.39	2.00	0.00	1.00	0.00
6.76	11.76	2.00	0.00	1.00	0.00	6.78	12.36	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
6.81	12.72	2.00	0.00	1.00	0.00	6.82	13.03	2.00	0.00	1.00	0.00
6.84	13.68	2.00	0.00	1.00	0.00	6.87	13.79	2.00	0.00	1.00	0.00
6.88	13.81	2.00	0.00	1.00	0.00	6.90	13.67	2.00	0.00	1.00	0.00
6.92	13.44	2.00	0.00	1.00	0.00	6.94	13.16	2.00	0.00	1.00	0.00
6.96	12.83	2.00	0.00	1.00	0.00	6.98	12.37	2.00	0.00	1.00	0.00
7.00	11.93	2.00	0.00	1.00	0.00	7.02	11.94	2.00	0.00	1.00	0.00
7.04	12.01	2.00	0.00	1.00	0.00	7.06	12.36	2.00	0.00	1.00	0.00
7.08	12.48	2.00	0.00	1.00	0.00	7.10	13.23	2.00	0.00	1.00	0.00
7.12	14.32	2.00	0.00	1.00	0.00	7.15	15.82	2.00	0.00	1.00	0.00
7.16	16.59	2.00	0.00	1.00	0.00	7.18	17.36	2.00	0.00	1.00	0.00
7.20	18.02	2.00	0.00	1.00	0.00	7.30	18.28	2.00	0.00	1.00	0.00
7.30	18.28	2.00	0.00	1.00	0.00	7.30	18.20	2.00	0.00	1.00	0.00
7.32	17.71	2.00	0.00	1.00	0.00	7.34	17.51	2.00	0.00	1.00	0.00
7.36	17.25	2.00	0.00	1.00	0.00	7.38	17.25	2.00	0.00	1.00	0.00
7.40	16.77	2.00	0.00	1.00	0.00	7.42	16.31	2.00	0.00	1.00	0.00
7.44	16.23	2.00	0.00	1.00	0.00	7.46	16.06	2.00	0.00	1.00	0.00
7.48	16.06	2.00	0.00	1.00	0.00	7.50	15.91	2.00	0.00	1.00	0.00
7.52	15.91	2.00	0.00	1.00	0.00	7.54	15.91	2.00	0.00	1.00	0.00
7.56	15.68	2.00	0.00	1.00	0.00	7.58	16.26	2.00	0.00	1.00	0.00
7.60	16.50	2.00	0.00	1.00	0.00	7.62	17.08	2.00	0.00	1.00	0.00
7.64	17.49	2.00	0.00	1.00	0.00	7.66	17.67	2.00	0.00	1.00	0.00
7.68	17.64	2.00	0.00	1.00	0.00	7.70	17.82	2.00	0.00	1.00	0.00
7.72	18.02	2.00	0.00	1.00	0.00	7.74	18.05	2.00	0.00	1.00	0.00
7.76	17.67	2.00	0.00	1.00	0.00	7.78	18.16	2.00	0.00	1.00	0.00
7.80	17.95	2.00	0.00	1.00	0.00	7.83	18.32	2.00	0.00	1.00	0.00
7.84	18.28	2.00	0.00	1.00	0.00	7.86	18.13	2.00	0.00	1.00	0.00
7.88	17.88	2.00	0.00	1.00	0.00	7.90	17.63	2.00	0.00	1.00	0.00
7.93	17.40	2.00	0.00	1.00	0.00	7.94	16.90	2.00	0.00	1.00	0.00
7.96	16.81	2.00	0.00	1.00	0.00	7.98	16.78	2.00	0.00	1.00	0.00
8.00	16.96	2.00	0.00	1.00	0.00	8.02	16.56	2.00	0.00	1.00	0.00
8.04	16.44	2.00	0.00	1.00	0.00	8.06	16.11	2.00	0.00	1.00	0.00
8.08	16.11	2.00	0.00	1.00	0.00	8.10	16.33	2.00	0.00	1.00	0.00
8.12	16.73	2.00	0.00	1.00	0.00	8.14	17.49	2.00	0.00	1.00	0.00
8.16	17.62	2.00	0.00	1.00	0.00	8.18	17.99	2.00	0.00	1.00	0.00
8.20	18.09	2.00	0.00	1.00	0.00	8.22	18.01	2.00	0.00	1.00	0.00
8.24	18.16	2.00	0.00	1.00	0.00	8.26	18.23	2.00	0.00	1.00	0.00
8.28	18.05	2.00	0.00	1.00	0.00	8.30	18.13	2.00	0.00	1.00	0.00
8.32	18.13	2.00	0.00	1.00	0.00	8.34	17.75	2.00	0.00	1.00	0.00
8.36	17.21	2.00	0.00	1.00	0.00	8.38	16.99	2.00	0.00	1.00	0.00
8.40	16.92	2.00	0.00	1.00	0.00	8.43	17.09	2.00	0.00	1.00	0.00
8.44	17.18	2.00	0.00	1.00	0.00	8.46	17.08	2.00	0.00	1.00	0.00
8.48	16.74	2.00	0.00	1.00	0.00	8.50	16.88	2.00	0.00	1.00	0.00
8.52	17.17	2.00	0.00	1.00	0.00	8.54	17.59	2.00	0.00	1.00	0.00
8.56	17.56	2.00	0.00	1.00	0.00	8.58	18.15	2.00	0.00	1.00	0.00
8.60	18.30	2.00	0.00	1.00	0.00	8.62	18.08	2.00	0.00	1.00	0.00
8.64	18.25	2.00	0.00	1.00	0.00	8.66	18.25	2.00	0.00	1.00	0.00
8.68	18.57	2.00	0.00	1.00	0.00	8.70	18.93	2.00	0.00	1.00	0.00
8.72	19.12	2.00	0.00	1.00	0.00	8.74	19.43	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
8.76	19.70	2.00	0.00	1.00	0.00	8.78	20.45	2.00	0.00	1.00	0.00
8.80	21.17	2.00	0.00	1.00	0.00	8.82	21.75	2.00	0.00	1.00	0.00
8.84	21.85	2.00	0.00	1.00	0.00	8.86	21.06	2.00	0.00	1.00	0.00
8.88	19.58	2.00	0.00	1.00	0.00	8.90	19.34	2.00	0.00	1.00	0.00
8.92	19.40	2.00	0.00	1.00	0.00	8.94	19.02	2.00	0.00	1.00	0.00
8.96	18.94	2.00	0.00	1.00	0.00	8.98	19.05	2.00	0.00	1.00	0.00
9.00	19.55	2.00	0.00	1.00	0.00	9.02	19.19	2.00	0.00	1.00	0.00
9.05	19.19	2.00	0.00	1.00	0.00	9.06	18.89	2.00	0.00	1.00	0.00
9.08	18.68	2.00	0.00	1.00	0.00	9.10	18.61	2.00	0.00	1.00	0.00
9.12	18.46	2.00	0.00	1.00	0.00	9.14	18.32	2.00	0.00	1.00	0.00
9.16	18.39	2.00	0.00	1.00	0.00	9.18	18.40	2.00	0.00	1.00	0.00
9.21	18.83	2.00	0.00	1.00	0.00	9.22	19.29	2.00	0.00	1.00	0.00
9.24	19.32	2.00	0.00	1.00	0.00	9.26	19.53	2.00	0.00	1.00	0.00
9.28	19.72	2.00	0.00	1.00	0.00	9.30	19.88	2.00	0.00	1.00	0.00
9.32	19.70	2.00	0.00	1.00	0.00	9.34	19.63	2.00	0.00	1.00	0.00
9.36	20.31	2.00	0.00	1.00	0.00	9.38	20.71	2.00	0.00	1.00	0.00
9.40	21.78	2.00	0.00	1.00	0.00	9.42	21.60	2.00	0.00	1.00	0.00
9.44	21.79	2.00	0.00	1.00	0.00	9.47	21.34	2.00	0.00	1.00	0.00
9.48	21.00	2.00	0.00	1.00	0.00	9.50	20.75	2.00	0.00	1.00	0.00
9.53	21.09	2.00	0.00	1.00	0.00	9.54	22.05	2.00	0.00	1.00	0.00
9.56	22.42	2.00	0.00	1.00	0.00	9.58	22.21	2.00	0.00	1.00	0.00
9.60	21.51	2.00	0.00	1.00	0.00	9.62	20.29	2.00	0.00	1.00	0.00
9.64	19.22	2.00	0.00	1.00	0.00	9.66	18.17	2.00	0.00	1.00	0.00
9.68	17.06	2.00	0.00	1.00	0.00	9.70	15.59	2.00	0.00	1.00	0.00
9.72	14.31	2.00	0.00	1.00	0.00	9.74	13.24	2.00	0.00	1.00	0.00
9.76	12.44	2.00	0.00	1.00	0.00	9.79	11.53	2.00	0.00	1.00	0.00
9.80	10.66	2.00	0.00	1.00	0.00	9.82	10.17	2.00	0.00	1.00	0.00
9.85	9.73	2.00	0.00	1.00	0.00	9.86	9.66	2.00	0.00	1.00	0.00
9.88	9.88	2.00	0.00	1.00	0.00	9.90	10.37	2.00	0.00	1.00	0.00
9.92	10.43	2.00	0.00	1.00	0.00	9.94	10.06	2.00	0.00	1.00	0.00
9.96	9.88	2.00	0.00	1.00	0.00	9.98	9.76	2.00	0.00	1.00	0.00
10.00	9.96	2.00	0.00	1.00	0.00	10.02	10.88	2.00	0.00	1.00	0.00
10.04	11.88	2.00	0.00	1.00	0.00	10.06	12.28	2.00	0.00	1.00	0.00
10.08	12.69	2.00	0.00	1.00	0.00	10.11	13.13	2.00	0.00	1.00	0.00
10.12	14.67	2.00	0.00	1.00	0.00	10.14	17.49	2.00	0.00	1.00	0.00
10.16	19.79	2.00	0.00	1.00	0.00	10.18	20.87	2.00	0.00	1.00	0.00
10.20	21.13	2.00	0.00	1.00	0.00	10.22	20.83	2.00	0.00	1.00	0.00
10.24	20.32	2.00	0.00	1.00	0.00	10.26	18.75	2.00	0.00	1.00	0.00
10.28	17.43	2.00	0.00	1.00	0.00	10.30	15.60	2.00	0.00	1.00	0.00
10.32	14.36	2.00	0.00	1.00	0.00	10.34	12.91	2.00	0.00	1.00	0.00
10.36	12.20	2.00	0.00	1.00	0.00	10.38	11.48	2.00	0.00	1.00	0.00
10.40	10.77	2.00	0.00	1.00	0.00	10.42	9.95	2.00	0.00	1.00	0.00
10.44	9.28	2.00	0.00	1.00	0.00	10.46	8.94	2.00	0.00	1.00	0.00
10.48	9.00	2.00	0.00	1.00	0.00	10.50	9.01	2.00	0.00	1.00	0.00
10.52	9.42	2.00	0.00	1.00	0.00	10.54	9.81	2.00	0.00	1.00	0.00
10.56	10.24	2.00	0.00	1.00	0.00	10.58	11.12	2.00	0.00	1.00	0.00
10.60	11.61	2.00	0.00	1.00	0.00	10.62	12.04	2.00	0.00	1.00	0.00
10.64	12.08	2.00	0.00	1.00	0.00	10.66	12.05	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
10.70	12.43	2.00	0.00	1.00	0.00	10.70	13.50	2.00	0.00	1.00	0.00
10.72	13.87	2.00	0.00	1.00	0.00	10.75	17.16	2.00	0.00	1.00	0.00
10.76	15.32	2.00	0.00	1.00	0.00	10.78	14.16	2.00	0.00	1.00	0.00
10.80	13.20	2.00	0.00	1.00	0.00	10.82	12.93	2.00	0.00	1.00	0.00
10.84	14.30	2.00	0.00	1.00	0.00	10.86	16.19	2.00	0.00	1.00	0.00
10.88	19.08	2.00	0.00	1.00	0.00	10.90	19.88	2.00	0.00	1.00	0.00
10.92	20.05	2.00	0.00	1.00	0.00	10.94	19.59	2.00	0.00	1.00	0.00
10.96	19.47	2.00	0.00	1.00	0.00	10.98	19.36	2.00	0.00	1.00	0.00
11.00	19.40	2.00	0.00	1.00	0.00	11.02	19.16	2.00	0.00	1.00	0.00
11.06	19.04	2.00	0.00	1.00	0.00	11.06	19.05	2.00	0.00	1.00	0.00
11.08	18.19	2.00	0.00	1.00	0.00	11.10	17.80	2.00	0.00	1.00	0.00
11.12	17.54	2.00	0.00	1.00	0.00	11.14	17.43	2.00	0.00	1.00	0.00
11.16	17.23	2.00	0.00	1.00	0.00	11.18	16.77	2.00	0.00	1.00	0.00
11.20	16.42	2.00	0.00	1.00	0.00	11.23	15.87	2.00	0.00	1.00	0.00
11.24	15.77	2.00	0.00	1.00	0.00	11.26	15.57	2.00	0.00	1.00	0.00
11.28	15.79	2.00	0.00	1.00	0.00	11.30	15.85	2.00	0.00	1.00	0.00
11.32	15.57	2.00	0.00	1.00	0.00	11.34	15.27	2.00	0.00	1.00	0.00
11.36	14.36	2.00	0.00	1.00	0.00	11.38	13.06	2.00	0.00	1.00	0.00
11.40	11.84	2.00	0.00	1.00	0.00	11.42	10.83	2.00	0.00	1.00	0.00
11.44	9.48	2.00	0.00	1.00	0.00	11.46	8.62	2.00	0.00	1.00	0.00
11.48	7.84	2.00	0.00	1.00	0.00	11.50	7.43	2.00	0.00	1.00	0.00
11.52	7.05	2.00	0.00	1.00	0.00	11.54	6.75	2.00	0.00	1.00	0.00
11.56	7.09	2.00	0.00	1.00	0.00	11.58	7.30	2.00	0.00	1.00	0.00
11.60	7.28	2.00	0.00	1.00	0.00	11.62	7.53	2.00	0.00	1.00	0.00
11.64	8.05	2.00	0.00	1.00	0.00	11.66	8.81	2.00	0.00	1.00	0.00
11.68	9.46	2.00	0.00	1.00	0.00	11.70	8.97	2.00	0.00	1.00	0.00
11.72	9.32	2.00	0.00	1.00	0.00	11.74	14.58	2.00	0.00	1.00	0.00
11.76	13.72	2.00	0.00	1.00	0.00	11.78	11.69	2.00	0.00	1.00	0.00
11.80	10.03	2.00	0.00	1.00	0.00	11.82	9.27	2.00	0.00	1.00	0.00
11.84	8.93	2.00	0.00	1.00	0.00	11.87	8.71	2.00	0.00	1.00	0.00
11.88	8.13	2.00	0.00	1.00	0.00	11.90	7.75	2.00	0.00	1.00	0.00
11.92	7.79	2.00	0.00	1.00	0.00	11.94	8.28	2.00	0.00	1.00	0.00
11.96	9.13	2.00	0.00	1.00	0.00	11.98	10.58	2.00	0.00	1.00	0.00
12.00	12.32	2.00	0.00	1.00	0.00	12.02	12.93	2.00	0.00	1.00	0.00
12.04	12.33	2.00	0.00	1.00	0.00	12.06	11.55	2.00	0.00	1.00	0.00
12.08	10.58	2.00	0.00	1.00	0.00	12.10	9.63	2.00	0.00	1.00	0.00
12.12	9.00	2.00	0.00	1.00	0.00	12.14	8.60	2.00	0.00	1.00	0.00
12.16	8.33	2.00	0.00	1.00	0.00	12.18	8.22	2.00	0.00	1.00	0.00
12.20	8.56	2.00	0.00	1.00	0.00	12.22	9.13	2.00	0.00	1.00	0.00
12.24	9.39	2.00	0.00	1.00	0.00	12.26	9.82	2.00	0.00	1.00	0.00
12.28	10.46	2.00	0.00	1.00	0.00	12.30	10.66	2.00	0.00	1.00	0.00
12.32	10.80	2.00	0.00	1.00	0.00	12.34	10.89	2.00	0.00	1.00	0.00
12.36	11.07	2.00	0.00	1.00	0.00	12.38	11.33	2.00	0.00	1.00	0.00
12.40	11.36	2.00	0.00	1.00	0.00	12.42	11.81	2.00	0.00	1.00	0.00
12.44	11.86	2.00	0.00	1.00	0.00	12.46	11.93	2.00	0.00	1.00	0.00
12.48	12.15	2.00	0.00	1.00	0.00	12.51	12.76	2.00	0.00	1.00	0.00
12.52	12.50	2.00	0.00	1.00	0.00	12.54	12.51	2.00	0.00	1.00	0.00
12.56	12.33	2.00	0.00	1.00	0.00	12.58	12.22	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
12.60	11.69	2.00	0.00	1.00	0.00	12.62	11.57	2.00	0.00	1.00	0.00
12.64	11.31	2.00	0.00	1.00	0.00	12.66	11.17	2.00	0.00	1.00	0.00
12.68	11.26	2.00	0.00	1.00	0.00	12.70	11.91	2.00	0.00	1.00	0.00
12.72	11.92	2.00	0.00	1.00	0.00	12.75	11.73	2.00	0.00	1.00	0.00
12.76	12.18	2.00	0.00	1.00	0.00	12.78	12.03	2.00	0.00	1.00	0.00
12.80	11.57	2.00	0.00	1.00	0.00	12.82	11.68	2.00	0.00	1.00	0.00
12.84	11.77	2.00	0.00	1.00	0.00	12.86	11.72	2.00	0.00	1.00	0.00
12.88	11.46	2.00	0.00	1.00	0.00	12.90	11.04	2.00	0.00	1.00	0.00
12.92	10.72	2.00	0.00	1.00	0.00	12.94	10.61	2.00	0.00	1.00	0.00
12.96	10.81	2.00	0.00	1.00	0.00	12.98	10.96	2.00	0.00	1.00	0.00
13.01	11.01	2.00	0.00	1.00	0.00	13.02	10.94	2.00	0.00	1.00	0.00
13.04	11.19	2.00	0.00	1.00	0.00	13.06	11.02	2.00	0.00	1.00	0.00
13.08	10.85	2.00	0.00	1.00	0.00	13.10	10.63	2.00	0.00	1.00	0.00
13.12	10.36	2.00	0.00	1.00	0.00	13.14	10.37	2.00	0.00	1.00	0.00
13.16	10.17	2.00	0.00	1.00	0.00	13.18	9.30	2.00	0.00	1.00	0.00
13.20	8.83	2.00	0.00	1.00	0.00	13.23	8.49	2.00	0.00	1.00	0.00
13.24	8.65	2.00	0.00	1.00	0.00	13.26	8.66	2.00	0.00	1.00	0.00
13.29	8.75	2.00	0.00	1.00	0.00	13.30	9.08	2.00	0.00	1.00	0.00
13.32	9.23	2.00	0.00	1.00	0.00	13.34	8.90	2.00	0.00	1.00	0.00
13.36	9.03	2.00	0.00	1.00	0.00	13.38	8.98	2.00	0.00	1.00	0.00
13.40	9.38	2.00	0.00	1.00	0.00	13.42	9.65	2.00	0.00	1.00	0.00
13.44	10.03	2.00	0.00	1.00	0.00	13.46	10.32	2.00	0.00	1.00	0.00
13.48	10.72	2.00	0.00	1.00	0.00	13.50	11.07	2.00	0.00	1.00	0.00
13.52	11.19	2.00	0.00	1.00	0.00	13.54	11.13	2.00	0.00	1.00	0.00
13.56	11.26	2.00	0.00	1.00	0.00	13.58	10.84	2.00	0.00	1.00	0.00
13.60	10.19	2.00	0.00	1.00	0.00	13.62	10.09	2.00	0.00	1.00	0.00
13.64	10.14	2.00	0.00	1.00	0.00	13.66	10.14	2.00	0.00	1.00	0.00
13.68	10.15	2.00	0.00	1.00	0.00	13.70	10.73	2.00	0.00	1.00	0.00
13.72	11.16	2.00	0.00	1.00	0.00	13.74	10.60	2.00	0.00	1.00	0.00
13.76	11.49	2.00	0.00	1.00	0.00	13.78	11.33	2.00	0.00	1.00	0.00
13.80	10.98	2.00	0.00	1.00	0.00	13.82	10.39	2.00	0.00	1.00	0.00
13.85	10.77	2.00	0.00	1.00	0.00	13.86	10.27	2.00	0.00	1.00	0.00
13.88	10.52	2.00	0.00	1.00	0.00	13.90	10.16	2.00	0.00	1.00	0.00
13.92	9.99	2.00	0.00	1.00	0.00	13.94	10.04	2.00	0.00	1.00	0.00
13.96	9.90	2.00	0.00	1.00	0.00	13.98	9.69	2.00	0.00	1.00	0.00
14.00	9.50	2.00	0.00	1.00	0.00	14.02	9.61	2.00	0.00	1.00	0.00
14.04	9.33	2.00	0.00	1.00	0.00	14.06	9.18	2.00	0.00	1.00	0.00
14.08	8.90	2.00	0.00	1.00	0.00						

Total estimated settlement: 0.00

Abbreviations

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumentric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

:: Strength loss calculation Idriss & Boulanger (2008) ::

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.02	0.84	14.30	5.38	76.87	2.87	0.07	180.76
0.04	0.88	14.99	5.63	84.43	2.89	0.07	93.98
0.06	0.89	15.13	5.81	87.84	2.91	0.07	62.94
0.08	0.90	15.35	6.19	94.98	2.95	0.07	47.64
0.10	0.93	15.77	6.55	103.29	2.98	0.07	38.95
0.12	0.92	15.67	7.12	111.67	3.03	0.07	32.07
0.14	0.89	15.14	7.78	117.82	3.09	0.07	26.42
0.16	0.85	14.48	8.39	121.49	3.14	0.07	22.01
0.18	0.85	14.37	8.55	122.87	3.15	0.07	19.35
0.20	0.87	14.78	8.28	122.39	3.13	0.07	17.87
0.22	0.89	15.14	8.04	121.74	3.11	0.07	16.60
0.24	0.91	15.46	7.86	121.42	3.09	0.07	15.51
0.30	0.92	15.59	7.81	121.74	3.09	0.07	12.46
0.30	0.90	15.18	8.09	122.84	3.11	0.07	12.13
0.30	0.87	14.70	8.45	124.19	3.14	0.07	11.75
0.32	0.84	14.18	8.88	125.91	3.17	0.07	10.62
0.34	0.83	14.08	9.07	127.60	3.19	0.07	9.90
0.36	0.82	13.82	9.32	128.87	3.21	0.07	9.17
0.38	0.79	13.38	9.67	129.35	3.23	0.07	8.40
0.40	0.77	12.95	9.92	128.51	3.25	0.06	7.72
0.42	0.74	12.47	10.18	126.95	3.26	0.06	7.07
0.44	0.72	12.07	10.36	124.98	3.28	0.06	6.53
0.46	0.68	11.51	10.69	122.95	3.30	0.06	5.96
0.48	0.65	10.95	11.02	120.66	3.32	0.06	5.43
0.50	0.63	10.52	11.18	117.55	3.33	0.06	5.01
0.52	0.61	10.14	11.26	114.15	3.33	0.06	4.64
0.54	0.60	9.99	11.12	111.13	3.33	0.06	4.41
0.56	0.59	9.90	11.05	109.38	3.32	0.06	4.21
0.58	0.60	9.95	10.87	108.15	3.31	0.06	4.09
0.60	0.58	9.74	10.93	106.44	3.31	0.06	3.87
0.62	0.56	9.33	11.21	104.65	3.33	0.06	3.59
0.64	0.56	9.25	11.20	103.62	3.33	0.06	3.45
0.66	0.57	9.56	10.83	103.56	3.31	0.06	3.46
0.68	0.62	10.28	10.08	103.57	3.26	0.06	3.61
0.70	0.65	10.86	9.50	103.07	3.22	0.06	3.71
0.72	0.69	11.51	8.94	102.87	3.18	0.06	3.82
0.74	0.73	12.20	8.45	103.10	3.14	0.06	3.94
0.76	0.78	13.00	7.99	103.92	3.11	0.07	4.09
0.78	0.83	13.84	7.59	105.11	3.07	0.07	4.25
0.80	0.87	14.49	7.40	107.27	3.06	0.07	4.34
0.82	0.89	14.96	7.41	110.76	3.06	0.07	4.37
0.84	0.90	14.98	7.68	115.01	3.08	0.07	4.27
0.87	0.89	14.81	8.07	119.48	3.11	0.07	4.07
0.88	0.87	14.56	8.44	122.87	3.14	0.07	3.96
0.90	0.86	14.43	8.70	125.58	3.16	0.07	3.83
0.92	0.86	14.36	8.85	127.16	3.17	0.07	3.73
0.94	0.85	14.22	9.01	128.18	3.18	0.07	3.62
0.96	0.84	13.94	9.20	128.24	3.20	0.07	3.47

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.99	0.81	13.53	9.44	127.78	3.21	0.07	3.26
1.00	0.81	13.40	9.46	126.79	3.22	0.07	3.20
1.09	0.81	13.39	9.41	126.01	3.21	0.07	2.93
1.09	0.82	13.60	9.23	125.49	3.20	0.07	2.97
1.09	0.82	13.64	9.20	125.43	3.20	0.07	2.98
1.09	0.82	13.67	9.08	124.07	3.19	0.07	2.99
1.11	0.82	13.69	9.00	123.17	3.18	0.07	2.94
1.13	0.83	13.79	8.88	122.43	3.17	0.07	2.91
1.14	0.83	13.70	8.99	123.14	3.18	0.07	2.86
1.17	0.81	13.47	9.15	123.34	3.19	0.07	2.74
1.18	0.79	13.04	9.47	123.51	3.22	0.07	2.63
1.20	0.78	12.82	9.65	123.72	3.23	0.06	2.55
1.22	0.76	12.50	9.91	123.82	3.25	0.06	2.44
1.24	0.74	12.25	10.08	123.44	3.26	0.06	2.35
1.26	0.73	12.00	10.22	122.62	3.27	0.06	2.27
1.28	0.74	12.26	9.93	121.71	3.25	0.06	2.28
1.30	0.82	13.56	8.94	121.20	3.18	0.06	2.48
1.32	0.94	15.55	7.73	120.18	3.08	0.07	2.80
1.34	1.05	17.46	6.79	118.52	3.00	0.07	3.10
1.36	1.12	18.57	6.30	117.01	2.96	0.07	3.25
1.38	1.15	19.08	6.12	116.68	2.94	0.07	3.29
1.40	1.16	19.28	6.12	118.01	2.94	0.07	3.28
1.42	1.16	19.28	6.27	120.87	2.96	0.07	3.23
1.44	1.18	19.62	6.33	124.24	2.96	0.07	3.24
1.46	1.24	20.60	6.19	127.42	2.95	0.07	3.35
1.48	1.31	21.83	5.98	130.46	2.93	0.08	3.51
1.50	1.36	22.71	5.85	132.93	2.92	0.08	3.60
1.52	1.37	22.88	5.89	134.66	2.92	0.08	3.57
1.54	1.37	22.80	5.95	135.60	2.93	0.08	3.51
1.56	1.37	22.76	6.01	136.80	2.93	0.08	3.46
1.58	1.38	23.02	6.02	138.69	2.93	0.08	3.46
1.60	1.40	23.32	6.03	140.69	2.93	0.08	3.46
1.62	1.41	23.42	6.08	142.33	2.94	0.08	3.43
1.64	1.42	23.62	6.09	143.80	2.94	0.08	3.41
1.66	1.44	23.98	6.06	145.24	2.94	0.08	3.42
1.68	1.46	24.38	6.01	146.54	2.93	0.08	3.43
1.70	1.45	24.18	6.07	146.83	2.94	0.08	3.36
1.72	1.41	23.47	6.23	146.18	2.95	0.08	3.23
1.74	1.33	22.10	6.60	145.91	2.99	0.08	3.00
1.78	1.22	20.29	7.24	146.77	3.04	0.07	2.69
1.78	1.09	18.04	8.19	147.77	3.12	0.07	2.39
1.80	0.95	15.63	9.32	145.76	3.21	0.07	2.05
1.82	0.85	13.97	10.26	143.34	3.27	0.07	1.81
1.84	0.78	12.74	10.99	140.09	3.32	0.07	1.63
1.86	0.76	12.37	11.13	137.63	3.33	0.06	1.57
1.88	0.74	11.93	11.08	132.16	3.32	0.06	1.50
1.90	0.73	11.85	10.59	125.52	3.29	0.06	1.47
1.92	0.73	11.78	10.06	118.43	3.26	0.06	1.45

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
1.94	0.72	11.73	9.52	111.62	3.22	0.06	1.43
1.96	0.72	11.60	9.04	104.87	3.18	0.06	1.40
1.98	0.73	11.77	8.36	98.39	3.13	0.06	1.40
2.00	0.74	12.02	7.83	94.08	3.09	0.06	1.42
2.08	0.76	12.28	7.50	92.13	3.07	0.06	1.40
2.08	0.76	12.30	7.48	92.02	3.06	0.06	1.40
2.08	0.85	13.78	6.64	91.53	2.99	0.06	1.57
2.10	0.96	15.70	5.82	91.38	2.91	0.07	1.77
2.12	1.12	18.39	4.98	91.55	2.82	0.08	2.05
2.14	1.22	20.14	4.66	93.89	2.79	0.08	2.23
2.16	1.31	21.67	4.46	96.57	2.76	0.08	2.38
2.18	1.39	22.95	4.31	98.89	2.74	0.09	2.49
2.20	1.47	24.25	4.20	101.74	2.73	0.09	2.61
2.22	1.55	25.74	4.08	104.94	2.71	0.09	2.76
2.24	1.60	26.50	4.20	111.31	2.73	0.09	2.83
2.26	1.58	26.22	4.52	118.57	2.77	0.09	2.79
2.28	1.51	24.92	5.10	126.97	2.84	0.09	2.64
2.30	1.43	23.55	5.74	135.11	2.90	0.08	2.48
2.32	1.35	22.28	6.39	142.46	2.97	0.08	2.34
2.34	1.31	21.60	6.87	148.32	3.01	0.07	2.26
2.36	1.32	21.77	6.90	150.29	3.01	0.07	2.27
2.38	1.36	22.44	6.66	149.47	2.99	0.08	2.33
2.40	1.42	23.46	6.22	145.97	2.95	0.08	2.42
2.42	1.46	24.12	5.87	141.52	2.92	0.08	2.48
2.44	1.50	24.76	5.55	137.30	2.88	0.08	2.53
2.46	1.52	25.13	5.30	133.25	2.86	0.08	2.56
2.48	1.53	25.19	5.22	131.45	2.85	0.08	2.56
2.50	1.52	25.01	5.26	131.67	2.85	0.08	2.53
2.52	1.49	24.60	5.51	135.47	2.88	0.08	2.48
2.54	1.48	24.36	5.70	138.94	2.90	0.08	2.44
2.56	1.49	24.52	5.70	139.89	2.90	0.08	2.45
2.58	1.53	25.20	5.49	138.32	2.88	0.08	2.51
2.60	1.57	25.85	5.30	137.08	2.86	0.08	2.56
2.62	1.57	25.95	5.28	136.98	2.86	0.09	2.56
2.64	1.55	25.60	5.34	136.63	2.86	0.08	2.52
2.66	1.52	25.04	5.46	136.61	2.87	0.08	2.45
2.68	1.49	24.54	5.67	139.08	2.90	0.08	2.39
2.70	1.47	24.11	5.96	143.65	2.93	0.08	2.34
2.72	1.48	24.25	6.09	147.81	2.94	0.08	2.35
2.74	1.50	24.72	6.07	150.03	2.94	0.08	2.38
2.76	1.54	25.41	5.92	150.42	2.92	0.08	2.44
2.78	1.55	25.58	5.87	150.30	2.92	0.08	2.45
2.81	1.56	25.61	5.86	149.96	2.92	0.08	2.43
2.82	1.53	25.19	5.97	150.33	2.93	0.08	2.39
2.84	1.50	24.59	6.16	151.46	2.95	0.08	2.32
2.86	1.46	24.02	6.35	152.51	2.96	0.08	2.26
2.88	1.46	23.93	6.41	153.45	2.97	0.08	2.24
2.90	1.48	24.25	6.35	153.93	2.96	0.08	2.26

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
2.92	1.51	24.78	6.20	153.62	2.95	0.08	2.31
2.94	1.53	25.13	6.03	151.52	2.93	0.08	2.33
2.96	1.55	25.48	5.82	148.19	2.91	0.08	2.35
2.98	1.56	25.67	5.65	145.06	2.90	0.08	2.36
3.00	1.56	25.68	5.58	143.38	2.89	0.08	2.35
3.02	1.54	25.25	5.65	142.72	2.90	0.08	2.31
3.04	1.49	24.44	5.86	143.24	2.92	0.08	2.22
3.06	1.42	23.28	6.19	144.03	2.95	0.08	2.11
3.08	1.33	21.61	6.71	144.95	3.00	0.07	1.95
3.10	1.22	19.87	7.28	144.70	3.05	0.07	1.79
3.12	1.13	18.19	7.90	143.71	3.10	0.07	1.63
3.14	1.06	17.13	8.31	142.30	3.13	0.07	1.53
3.16	1.03	16.54	8.49	140.49	3.14	0.07	1.47
3.18	1.03	16.50	8.34	137.58	3.13	0.07	1.46
3.20	1.04	16.69	7.96	132.80	3.10	0.07	1.47
3.22	1.04	16.63	7.64	127.15	3.08	0.07	1.47
3.24	1.01	16.15	7.53	121.59	3.07	0.07	1.42
3.26	0.99	15.77	7.39	116.54	3.06	0.07	1.38
3.28	0.99	15.77	7.13	112.38	3.03	0.07	1.38
3.30	1.04	16.75	6.58	110.22	2.99	0.07	1.46
3.32	1.12	17.95	6.12	109.91	2.94	0.07	1.56
3.34	1.21	19.58	5.59	109.47	2.89	0.07	1.69
3.36	1.30	21.10	5.15	108.70	2.84	0.08	1.82
3.38	1.38	22.35	4.88	109.10	2.81	0.08	1.92
3.40	1.41	22.88	4.83	110.55	2.81	0.08	1.96
3.42	1.42	23.09	4.85	112.03	2.81	0.08	1.97
3.44	1.45	23.56	4.81	113.33	2.80	0.08	2.00
3.46	1.46	23.71	4.89	115.96	2.81	0.08	2.01
3.48	1.45	23.55	5.09	119.77	2.83	0.08	1.99
3.50	1.39	22.57	5.49	123.98	2.88	0.08	1.90
3.52	1.35	21.81	5.85	127.49	2.92	0.08	1.83
3.54	1.30	21.10	6.15	129.80	2.94	0.07	1.76
3.56	1.30	20.96	6.22	130.45	2.95	0.07	1.75
3.58	1.31	21.22	6.14	130.34	2.94	0.07	1.76
3.60	1.33	21.46	6.06	129.97	2.94	0.07	1.78
3.63	1.31	21.21	6.13	129.94	2.94	0.07	1.75
3.64	1.28	20.73	6.27	129.93	2.96	0.07	1.70
3.66	1.25	20.16	6.47	130.45	2.97	0.07	1.65
3.68	1.24	20.00	6.53	130.73	2.98	0.07	1.63
3.70	1.24	19.96	6.56	130.92	2.98	0.07	1.63
3.72	1.24	19.87	6.60	131.11	2.99	0.07	1.61
3.74	1.24	20.00	6.55	131.01	2.98	0.07	1.62
3.76	1.28	20.67	6.31	130.48	2.96	0.07	1.67
3.78	1.39	22.53	5.69	128.29	2.90	0.08	1.81
3.80	1.52	24.67	5.13	126.46	2.84	0.08	1.98
3.82	1.62	26.40	4.78	126.15	2.80	0.08	2.11
3.84	1.65	26.96	4.73	127.60	2.79	0.09	2.15
3.86	1.61	26.13	5.03	131.50	2.83	0.08	2.07

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
3.88	1.52	24.74	5.45	134.93	2.87	0.08	1.96
3.90	1.41	22.70	6.10	138.54	2.94	0.07	1.79
3.92	1.29	20.70	6.82	141.28	3.01	0.07	1.63
3.94	1.15	18.30	7.85	143.76	3.09	0.07	1.43
3.96	1.04	16.41	8.86	145.36	3.17	0.07	1.28
3.98	0.97	15.34	9.43	144.54	3.21	0.07	1.19
4.00	0.96	15.12	9.45	142.92	3.21	0.06	1.17
4.02	0.98	15.46	9.05	139.84	3.19	0.06	1.20
4.04	1.01	15.94	8.49	135.28	3.14	0.07	1.23
4.07	1.05	16.55	7.80	129.18	3.09	0.07	1.27
4.08	1.09	17.22	7.10	122.34	3.03	0.07	1.32
4.10	1.13	17.99	6.51	117.02	2.98	0.07	1.38
4.12	1.17	18.67	6.05	112.98	2.94	0.07	1.42
4.14	1.20	19.15	5.80	111.11	2.91	0.07	1.46
4.26	1.22	19.40	5.69	110.28	2.90	0.07	1.45
4.26	1.22	19.51	5.65	110.29	2.90	0.07	1.46
4.26	1.22	19.49	5.66	110.35	2.90	0.07	1.46
4.26	1.23	19.54	6.17	120.67	2.95	0.07	1.46
4.26	1.22	19.51	6.71	130.95	3.00	0.07	1.46
4.28	1.20	19.17	7.35	140.94	3.05	0.07	1.43
4.30	1.17	18.57	7.65	142.04	3.08	0.07	1.38
4.32	1.14	18.01	7.87	141.73	3.10	0.07	1.33
4.34	1.11	17.62	7.98	140.68	3.10	0.07	1.30
4.36	1.11	17.47	7.98	139.49	3.10	0.07	1.29
4.38	1.12	17.65	7.83	138.29	3.09	0.07	1.30
4.40	1.16	18.31	7.45	136.37	3.06	0.07	1.34
4.42	1.23	19.56	6.83	133.64	3.01	0.07	1.43
4.44	1.33	21.23	6.13	130.12	2.94	0.07	1.55
4.46	1.44	23.17	5.49	127.15	2.88	0.08	1.68
4.48	1.51	24.16	5.18	125.25	2.85	0.08	1.76
4.50	1.53	24.36	5.17	125.82	2.84	0.08	1.78
4.52	1.50	23.98	5.34	127.98	2.86	0.08	1.74
4.54	1.45	23.11	5.72	132.12	2.90	0.08	1.66
4.56	1.37	21.89	6.31	138.05	2.96	0.07	1.57
4.58	1.28	20.42	7.04	143.70	3.03	0.07	1.46
4.60	1.24	19.60	7.57	148.29	3.07	0.07	1.40
4.62	1.22	19.27	7.84	151.01	3.09	0.07	1.38
4.64	1.22	19.14	7.97	152.62	3.10	0.07	1.37
4.66	1.23	19.22	7.94	152.56	3.10	0.07	1.37
4.68	1.23	19.24	7.85	151.10	3.09	0.07	1.37
4.70	1.23	19.16	7.77	148.90	3.09	0.07	1.37
4.72	1.23	19.12	7.67	146.61	3.08	0.07	1.37
4.74	1.24	19.20	7.53	144.54	3.07	0.07	1.37
4.76	1.26	19.50	7.29	142.09	3.05	0.07	1.39
4.78	1.28	19.73	7.11	140.23	3.03	0.07	1.41
4.80	1.30	20.03	6.90	138.31	3.01	0.07	1.43
4.82	1.31	20.15	6.82	137.43	3.01	0.07	1.44
4.84	1.32	20.12	6.80	136.88	3.01	0.07	1.44

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
4.86	1.31	19.94	6.87	137.03	3.01	0.07	1.42
4.88	1.30	19.74	6.97	137.66	3.02	0.07	1.41
4.90	1.29	19.45	7.12	138.43	3.03	0.07	1.39
4.92	1.27	19.06	7.30	139.16	3.05	0.07	1.36
4.94	1.23	18.45	7.57	139.67	3.07	0.07	1.32
4.96	1.19	17.73	7.84	139.09	3.09	0.07	1.27
4.98	1.15	17.05	8.09	138.03	3.11	0.07	1.22
5.01	1.11	16.30	8.30	135.33	3.13	0.07	1.16
5.02	1.06	15.55	8.53	132.58	3.15	0.07	1.11
5.04	1.01	14.65	8.85	129.66	3.17	0.06	1.05
5.06	0.96	13.85	9.22	127.75	3.20	0.06	0.99
5.08	0.93	13.27	9.53	126.54	3.22	0.06	0.95
5.10	0.89	12.68	9.88	125.29	3.24	0.06	0.91
5.12	0.87	12.20	10.14	123.75	3.26	0.06	0.87
5.14	0.83	11.60	10.39	120.52	3.28	0.06	0.83
5.16	0.80	11.14	10.45	116.39	3.28	0.06	0.80
5.18	0.78	10.78	10.31	111.19	3.27	0.06	0.77
5.20	0.78	10.77	9.90	106.61	3.25	0.06	0.77
5.22	0.79	10.88	9.41	102.37	3.21	0.06	0.78
5.24	0.81	11.13	8.89	98.97	3.17	0.06	0.80
5.26	0.83	11.40	8.47	96.51	3.14	0.06	0.81
5.28	0.88	12.10	7.81	94.42	3.09	0.06	0.86
5.30	0.94	13.03	7.09	92.30	3.03	0.06	0.93
5.32	1.01	14.02	6.39	89.62	2.97	0.06	1.00
5.34	1.04	14.45	6.12	88.43	2.94	0.07	1.03
5.36	1.03	14.32	6.28	89.96	2.96	0.06	1.02
5.38	1.01	13.97	6.70	93.54	3.00	0.06	1.00
5.40	1.01	13.98	6.95	97.17	3.02	0.06	1.00
5.42	1.06	14.59	6.83	99.68	3.01	0.06	1.04
5.44	1.11	15.42	6.58	101.41	2.98	0.07	1.10
5.46	1.16	16.14	6.35	102.40	2.96	0.07	1.15
5.48	1.20	16.58	6.22	103.14	2.95	0.07	1.18
5.50	1.22	16.96	6.12	103.73	2.94	0.07	1.21
5.52	1.27	17.56	5.94	104.34	2.92	0.07	1.26
5.54	1.32	18.31	5.75	105.34	2.91	0.07	1.31
5.56	1.39	19.19	5.57	106.90	2.89	0.07	1.38
5.58	1.44	19.84	5.56	110.26	2.89	0.07	1.43
5.60	1.48	20.39	5.60	114.06	2.89	0.07	1.47
5.62	1.50	20.74	5.67	117.50	2.90	0.08	1.49
5.64	1.52	20.89	5.77	120.49	2.91	0.07	1.50
5.66	1.53	21.06	5.85	123.22	2.92	0.07	1.51
5.68	1.56	21.43	5.90	126.57	2.92	0.07	1.53
5.70	1.60	21.94	5.88	128.93	2.92	0.08	1.57
5.72	1.65	22.56	5.80	130.86	2.91	0.08	1.62
5.74	1.68	22.97	5.76	132.25	2.91	0.08	1.65
5.76	1.68	22.94	5.87	134.60	2.92	0.08	1.64
5.78	1.64	22.31	6.15	137.29	2.95	0.07	1.59
5.80	1.56	21.17	6.62	140.03	2.99	0.07	1.51

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
5.82	1.51	20.34	6.99	142.15	3.02	0.07	1.45
5.84	1.47	19.73	7.30	144.00	3.05	0.07	1.41
5.86	1.46	19.56	7.39	144.56	3.06	0.07	1.40
5.88	1.45	19.29	7.41	142.85	3.06	0.07	1.38
5.90	1.42	18.87	7.39	139.37	3.06	0.07	1.35
5.92	1.38	18.23	7.46	136.04	3.06	0.07	1.30
5.94	1.36	17.88	7.46	133.40	3.06	0.07	1.28
5.97	1.35	17.64	7.39	130.38	3.06	0.07	1.26
5.98	1.36	17.75	7.20	127.80	3.04	0.07	1.27
6.00	1.37	17.93	7.05	126.42	3.03	0.07	1.28
6.02	1.42	18.60	6.81	126.69	3.01	0.07	1.33
6.04	1.48	19.31	6.51	125.64	2.98	0.07	1.38
6.06	1.53	19.95	6.21	123.90	2.95	0.07	1.42
6.08	1.54	20.12	6.06	121.84	2.94	0.07	1.44
6.10	1.53	19.90	6.06	120.57	2.94	0.07	1.42
6.12	1.50	19.45	6.20	120.64	2.95	0.07	1.39
6.14	1.47	18.99	6.45	122.51	2.97	0.07	1.36
6.16	1.45	18.56	6.81	126.47	3.01	0.07	1.33
6.18	1.43	18.25	7.12	129.94	3.03	0.07	1.30
6.20	1.40	17.89	7.42	132.73	3.06	0.07	1.28
6.22	1.39	17.69	7.63	135.02	3.08	0.07	1.26
6.24	1.37	17.27	7.95	137.29	3.10	0.07	1.23
6.26	1.35	16.98	8.15	138.39	3.12	0.07	1.21
6.28	1.35	16.95	8.15	138.10	3.12	0.07	1.21
6.30	1.37	17.24	7.94	136.82	3.10	0.07	1.23
6.32	1.41	17.61	7.69	135.46	3.08	0.07	1.26
6.34	1.45	18.12	7.39	133.88	3.06	0.07	1.29
6.36	1.49	18.68	7.07	131.98	3.03	0.07	1.33
6.38	1.54	19.36	6.70	129.62	3.00	0.07	1.38
6.41	1.57	19.66	6.51	128.01	2.98	0.07	1.40
6.42	1.59	19.84	6.43	127.66	2.97	0.07	1.42
6.44	1.58	19.71	6.53	128.66	2.98	0.07	1.41
6.46	1.58	19.62	6.63	130.15	2.99	0.07	1.40
6.48	1.58	19.57	6.74	131.92	3.00	0.07	1.40
6.50	1.59	19.62	6.83	134.02	3.01	0.07	1.40
6.52	1.60	19.69	6.90	135.81	3.01	0.07	1.41
6.54	1.60	19.74	6.96	137.38	3.02	0.07	1.41
6.56	1.59	19.55	7.07	138.28	3.03	0.07	1.40
6.58	1.56	19.01	7.32	139.23	3.05	0.07	1.36
6.60	1.49	18.15	7.70	139.70	3.08	0.07	1.30
6.62	1.43	17.28	8.11	140.10	3.11	0.07	1.23
6.64	1.36	16.26	8.66	140.78	3.16	0.07	1.16
6.66	1.28	15.17	9.30	141.12	3.20	0.07	1.08
6.68	1.20	14.07	10.03	141.09	3.25	0.07	1.00
6.70	1.14	13.35	10.49	140.11	3.29	0.06	0.95
6.72	1.11	12.92	10.73	138.62	3.30	0.06	0.92
6.74	1.08	12.50	10.70	133.70	3.30	0.06	0.89
6.76	1.08	12.44	10.34	128.56	3.28	0.06	0.89

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
6.78	1.10	12.64	9.68	122.31	3.23	0.06	0.90
6.81	1.14	13.14	8.98	118.10	3.18	0.06	0.94
6.82	1.19	13.69	8.24	112.82	3.12	0.06	0.98
6.84	1.22	14.11	7.68	108.37	3.08	0.07	1.01
6.87	1.25	14.39	7.27	104.65	3.05	0.07	1.03
6.88	1.25	14.39	7.12	102.36	3.03	0.07	1.03
6.90	1.24	14.22	7.15	101.64	3.04	0.07	1.02
6.92	1.22	13.94	7.34	102.29	3.05	0.07	1.00
6.94	1.19	13.59	7.67	104.32	3.08	0.07	0.97
6.96	1.16	13.17	8.07	106.27	3.11	0.06	0.94
6.98	1.13	12.73	8.46	107.67	3.14	0.06	0.91
7.00	1.11	12.42	8.70	108.10	3.16	0.06	0.89
7.02	1.10	12.29	8.74	107.38	3.16	0.06	0.88
7.04	1.11	12.43	8.51	105.87	3.15	0.06	0.89
7.06	1.13	12.63	8.24	104.04	3.12	0.06	0.90
7.08	1.17	13.10	7.77	101.83	3.09	0.06	0.94
7.10	1.23	13.85	7.18	99.45	3.04	0.07	0.99
7.12	1.34	15.11	6.42	96.98	2.97	0.07	1.08
7.15	1.44	16.33	5.84	95.31	2.91	0.07	1.17
7.16	1.53	17.38	5.46	94.96	2.88	0.07	1.25
7.18	1.59	18.10	5.31	96.04	2.86	0.08	1.30
7.20	1.64	18.68	5.28	98.61	2.86	0.08	1.34
7.30	1.67	18.84	5.33	100.37	2.86	0.08	1.35
7.30	1.68	18.93	5.38	101.87	2.87	0.08	1.36
7.30	1.66	18.73	6.11	114.49	2.94	0.07	1.34
7.32	1.63	18.37	6.88	126.32	3.01	0.07	1.31
7.34	1.60	17.97	7.63	137.07	3.08	0.07	1.28
7.36	1.59	17.79	7.73	137.56	3.08	0.07	1.27
7.38	1.57	17.50	7.82	136.89	3.09	0.07	1.25
7.40	1.55	17.14	7.89	135.17	3.10	0.07	1.22
7.42	1.52	16.77	7.96	133.44	3.10	0.07	1.20
7.44	1.50	16.50	7.98	131.59	3.10	0.07	1.18
7.46	1.49	16.37	7.93	129.82	3.10	0.07	1.17
7.48	1.48	16.20	7.90	128.01	3.10	0.07	1.16
7.50	1.48	16.11	7.84	126.21	3.09	0.07	1.15
7.52	1.47	16.03	7.77	124.54	3.09	0.07	1.14
7.54	1.47	15.94	7.74	123.32	3.08	0.07	1.14
7.56	1.48	16.05	7.61	122.13	3.07	0.07	1.15
7.58	1.50	16.25	7.45	121.01	3.06	0.07	1.16
7.60	1.54	16.72	7.16	119.68	3.04	0.07	1.19
7.62	1.58	17.14	6.95	119.04	3.02	0.07	1.22
7.64	1.62	17.54	6.80	119.25	3.00	0.07	1.25
7.66	1.64	17.72	6.77	119.92	3.00	0.07	1.27
7.68	1.65	17.81	6.77	120.53	3.00	0.07	1.27
7.70	1.66	17.91	6.77	121.26	3.00	0.07	1.28
7.72	1.67	18.02	6.80	122.62	3.01	0.07	1.29
7.74	1.67	17.97	6.87	123.40	3.01	0.07	1.28
7.76	1.68	18.02	6.92	124.73	3.02	0.07	1.29

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
7.78	1.68	17.99	7.01	126.16	3.02	0.07	1.29
7.80	1.70	18.22	7.03	128.06	3.03	0.07	1.30
7.83	1.71	18.22	7.08	129.07	3.03	0.07	1.30
7.84	1.72	18.27	7.06	128.99	3.03	0.07	1.31
7.86	1.70	18.06	7.11	128.43	3.03	0.07	1.29
7.88	1.68	17.80	7.18	127.87	3.04	0.07	1.27
7.90	1.66	17.53	7.29	127.85	3.05	0.07	1.25
7.93	1.64	17.17	7.52	129.05	3.07	0.07	1.23
7.94	1.61	16.89	7.73	130.59	3.08	0.07	1.21
7.96	1.60	16.65	7.92	131.95	3.10	0.07	1.19
7.98	1.60	16.65	7.96	132.52	3.10	0.07	1.19
8.00	1.60	16.55	8.01	132.58	3.11	0.07	1.18
8.02	1.59	16.41	8.05	132.08	3.11	0.07	1.17
8.04	1.56	16.11	8.12	130.79	3.12	0.07	1.15
8.06	1.55	15.94	8.11	129.21	3.11	0.07	1.14
8.08	1.55	15.90	8.01	127.44	3.11	0.07	1.14
8.10	1.57	16.12	7.82	126.08	3.09	0.07	1.15
8.12	1.62	16.60	7.55	125.29	3.07	0.07	1.19
8.14	1.66	17.04	7.36	125.38	3.05	0.07	1.22
8.16	1.70	17.47	7.23	126.38	3.04	0.07	1.25
8.18	1.72	17.66	7.22	127.52	3.04	0.07	1.26
8.20	1.74	17.78	7.23	128.63	3.04	0.07	1.27
8.22	1.74	17.82	7.27	129.59	3.05	0.07	1.27
8.24	1.75	17.85	7.31	130.46	3.05	0.07	1.28
8.26	1.75	17.85	7.36	131.41	3.05	0.07	1.27
8.28	1.76	17.82	7.44	132.53	3.06	0.07	1.27
8.30	1.75	17.77	7.51	133.43	3.07	0.07	1.27
8.32	1.75	17.65	7.58	133.77	3.07	0.07	1.26
8.34	1.72	17.30	7.71	133.39	3.08	0.07	1.24
8.36	1.68	16.87	7.86	132.62	3.09	0.07	1.21
8.38	1.66	16.56	7.95	131.58	3.10	0.07	1.18
8.40	1.66	16.50	7.92	130.65	3.10	0.07	1.18
8.43	1.66	16.53	7.87	130.12	3.10	0.07	1.18
8.44	1.67	16.58	7.85	130.16	3.09	0.07	1.18
8.46	1.66	16.44	7.92	130.20	3.10	0.07	1.17
8.48	1.65	16.32	7.96	129.95	3.10	0.07	1.17
8.50	1.66	16.34	7.93	129.48	3.10	0.07	1.17
8.52	1.69	16.61	7.75	128.82	3.09	0.07	1.19
8.54	1.71	16.83	7.62	128.29	3.08	0.07	1.20
8.56	1.74	17.16	7.46	127.93	3.06	0.07	1.23
8.58	1.77	17.39	7.38	128.26	3.05	0.07	1.24
8.60	1.79	17.56	7.36	129.21	3.05	0.07	1.25
8.62	1.79	17.59	7.42	130.49	3.06	0.07	1.26
8.64	1.80	17.57	7.50	131.82	3.07	0.07	1.25
8.66	1.81	17.72	7.49	132.76	3.06	0.07	1.27
8.68	1.84	17.94	7.47	133.98	3.06	0.07	1.28
8.70	1.87	18.22	7.43	135.29	3.06	0.07	1.30
8.72	1.90	18.50	7.39	136.69	3.06	0.07	1.32

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
8.74	1.93	18.76	7.33	137.57	3.05	0.07	1.34
8.76	1.97	19.20	7.24	139.05	3.04	0.07	1.37
8.78	2.03	19.79	7.11	140.78	3.03	0.07	1.41
8.80	2.10	20.48	6.99	143.11	3.02	0.07	1.46
8.82	2.15	20.96	6.91	144.82	3.01	0.08	1.50
8.84	2.15	20.90	7.00	146.24	3.02	0.08	1.49
8.86	2.08	20.12	7.33	147.43	3.05	0.07	1.44
8.88	2.00	19.22	7.69	147.82	3.08	0.07	1.37
8.90	1.94	18.62	7.93	147.57	3.10	0.07	1.33
8.92	1.93	18.40	7.99	147.05	3.11	0.07	1.31
8.94	1.92	18.25	8.03	146.55	3.11	0.07	1.30
8.96	1.91	18.13	8.04	145.73	3.11	0.07	1.29
8.98	1.93	18.30	7.86	143.86	3.09	0.07	1.31
9.00	1.94	18.39	7.69	141.46	3.08	0.07	1.31
9.02	1.95	18.44	7.51	138.50	3.07	0.07	1.32
9.05	1.93	18.18	7.46	135.66	3.06	0.07	1.30
9.06	1.91	17.98	7.36	132.34	3.05	0.07	1.28
9.08	1.89	17.74	7.31	129.80	3.05	0.07	1.27
9.10	1.88	17.57	7.25	127.34	3.04	0.07	1.25
9.12	1.87	17.42	7.21	125.57	3.04	0.07	1.24
9.14	1.86	17.33	7.13	123.55	3.03	0.07	1.24
9.16	1.86	17.30	7.07	122.26	3.03	0.07	1.24
9.18	1.88	17.47	6.93	121.05	3.02	0.07	1.25
9.21	1.92	17.75	6.78	120.24	3.00	0.07	1.27
9.22	1.95	18.06	6.64	119.95	2.99	0.07	1.29
9.24	1.97	18.27	6.57	120.05	2.98	0.07	1.30
9.26	1.99	18.38	6.52	119.90	2.98	0.07	1.31
9.28	2.01	18.54	6.44	119.38	2.97	0.07	1.32
9.30	2.01	18.55	6.46	119.88	2.97	0.07	1.32
9.32	2.01	18.48	6.59	121.80	2.99	0.07	1.32
9.34	2.02	18.61	6.65	123.81	2.99	0.07	1.33
9.36	2.06	18.94	6.59	124.83	2.99	0.07	1.35
9.38	2.14	19.65	6.34	124.59	2.96	0.07	1.40
9.40	2.18	20.05	6.22	124.73	2.95	0.08	1.43
9.42	2.22	20.38	6.15	125.26	2.94	0.08	1.46
9.44	2.20	20.19	6.28	126.79	2.96	0.08	1.44
9.47	2.18	19.94	6.43	128.18	2.97	0.08	1.42
9.48	2.15	19.59	6.64	130.03	2.99	0.07	1.40
9.50	2.14	19.48	6.79	132.28	3.00	0.07	1.39
9.53	2.18	19.79	6.79	134.34	3.00	0.07	1.41
9.54	2.24	20.34	6.66	135.43	2.99	0.08	1.45
9.56	2.28	20.69	6.52	134.96	2.98	0.08	1.48
9.58	2.26	20.47	6.53	133.74	2.98	0.08	1.46
9.60	2.19	19.74	6.76	133.48	3.00	0.08	1.41
9.62	2.09	18.72	7.13	133.43	3.03	0.07	1.34
9.64	1.98	17.61	7.60	133.79	3.07	0.07	1.26
9.66	1.87	16.54	8.01	132.47	3.11	0.07	1.18
9.68	1.75	15.34	8.48	130.07	3.14	0.07	1.10

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.70	1.62	14.05	8.95	125.78	3.18	0.07	1.00
9.72	1.49	12.77	9.47	120.91	3.22	0.07	0.91
9.74	1.39	11.75	9.82	115.33	3.24	0.07	0.84
9.76	1.30	10.85	10.15	110.11	3.26	0.06	0.78
9.79	1.22	10.03	10.41	104.36	3.28	0.06	0.72
9.80	1.14	9.31	10.66	99.19	3.30	0.06	0.66
9.82	1.09	8.74	10.79	94.28	3.30	0.06	0.62
9.85	1.06	8.41	10.70	90.03	3.30	0.06	0.60
9.86	1.05	8.34	10.28	85.70	3.27	0.06	0.60
9.88	1.07	8.55	9.50	81.21	3.22	0.06	0.61
9.90	1.10	8.80	8.77	77.20	3.17	0.06	0.63
9.92	1.11	8.86	8.41	74.47	3.14	0.06	0.63
9.94	1.09	8.69	8.33	72.36	3.13	0.06	0.62
9.96	1.07	8.46	8.34	70.58	3.13	0.06	0.60
9.98	1.07	8.46	8.18	69.27	3.12	0.06	0.60
10.00	1.11	8.86	7.70	68.24	3.08	0.06	0.63
10.02	1.20	9.62	7.05	67.78	3.03	0.06	0.69
10.04	1.28	10.40	6.46	67.21	2.97	0.06	0.74
10.06	1.35	10.99	6.18	67.88	2.95	0.06	0.78
10.08	1.39	11.41	6.06	69.11	2.94	0.07	0.82
10.11	1.48	12.24	5.81	71.05	2.91	0.07	0.87
10.12	1.66	13.92	5.16	71.84	2.84	0.07	0.99
10.14	1.90	16.19	4.47	72.32	2.76	0.08	1.15
10.16	2.12	18.26	4.01	73.11	2.70	0.08	1.30
10.18	2.24	19.38	3.93	76.24	2.69	0.08	1.38
10.20	2.27	19.61	4.09	80.31	2.71	0.08	1.40
10.22	2.24	19.31	4.39	84.79	2.75	0.08	1.37
10.24	2.15	18.40	4.89	89.99	2.81	0.08	1.31
10.26	2.03	17.18	5.56	95.49	2.89	0.08	1.23
10.28	1.86	15.56	6.56	102.03	2.98	0.07	1.11
10.30	1.70	14.07	7.58	106.69	3.07	0.07	1.00
10.32	1.54	12.57	8.76	110.11	3.16	0.07	0.90
10.34	1.43	11.46	9.67	110.78	3.23	0.06	0.82
10.36	1.33	10.53	10.44	109.93	3.28	0.06	0.75
10.38	1.26	9.85	10.90	107.36	3.31	0.06	0.70
10.40	1.18	9.13	11.34	103.52	3.34	0.06	0.65
10.42	1.10	8.42	11.77	99.09	3.37	0.06	0.60
10.44	1.04	7.84	12.05	94.47	3.38	0.06	0.56
10.46	1.01	7.55	11.85	89.43	3.37	0.06	0.54
10.48	1.01	7.47	11.27	84.26	3.34	0.06	0.53
10.50	1.03	7.63	10.32	78.75	3.27	0.06	0.55
10.52	1.06	7.89	9.40	74.19	3.21	0.06	0.56
10.54	1.10	8.29	8.45	70.01	3.14	0.06	0.59
10.56	1.16	8.84	7.57	66.96	3.07	0.06	0.63
10.58	1.23	9.42	6.85	64.50	3.01	0.06	0.67
10.60	1.29	10.00	6.30	63.03	2.96	0.06	0.71
10.62	1.33	10.30	6.09	62.73	2.94	0.07	0.74
10.64	1.34	10.43	6.09	63.50	2.94	0.07	0.75

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
10.66	1.36	10.56	6.07	64.06	2.94	0.07	0.75
10.70	1.41	10.99	5.82	64.01	2.91	0.07	0.79
10.70	1.48	11.59	5.53	64.06	2.88	0.07	0.83
10.72	1.64	13.08	5.09	66.57	2.83	0.07	0.93
10.75	1.70	13.57	5.21	70.73	2.85	0.08	0.97
10.76	1.71	13.63	5.41	73.67	2.87	0.07	0.97
10.78	1.58	12.41	6.00	74.40	2.93	0.07	0.89
10.80	1.51	11.77	6.26	73.66	2.96	0.07	0.84
10.82	1.53	11.97	6.08	72.73	2.94	0.07	0.85
10.84	1.66	13.05	5.47	71.32	2.88	0.07	0.93
10.86	1.89	15.16	4.60	69.78	2.78	0.08	1.08
10.88	2.08	16.93	4.07	68.90	2.71	0.08	1.20
10.90	2.21	18.07	3.86	69.69	2.68	0.08	1.28
10.92	2.22	18.07	4.01	72.44	2.70	0.08	1.28
10.94	2.20	17.88	4.33	77.35	2.74	0.08	1.27
10.96	2.18	17.59	4.71	82.92	2.79	0.08	1.25
10.98	2.16	17.43	5.04	87.91	2.83	0.08	1.24
11.00	2.14	17.20	5.42	93.23	2.87	0.08	1.23
11.02	2.13	17.03	5.78	98.37	2.91	0.08	1.22
11.06	2.12	16.86	6.05	102.03	2.94	0.07	1.20
11.06	2.08	16.58	6.37	105.68	2.97	0.07	1.18
11.08	2.05	16.20	6.66	107.88	2.99	0.07	1.16
11.10	2.00	15.75	7.03	110.68	3.03	0.07	1.13
11.12	1.97	15.52	7.18	111.39	3.04	0.07	1.11
11.14	1.95	15.33	7.27	111.38	3.05	0.07	1.09
11.16	1.93	15.07	7.35	110.71	3.05	0.07	1.08
11.18	1.89	14.73	7.47	110.06	3.06	0.07	1.05
11.20	1.84	14.29	7.69	109.83	3.08	0.07	1.02
11.23	1.81	13.95	7.85	109.53	3.09	0.07	1.00
11.24	1.78	13.70	8.00	109.62	3.11	0.07	0.98
11.26	1.78	13.67	8.05	110.15	3.11	0.07	0.98
11.28	1.79	13.71	8.09	110.96	3.11	0.07	0.98
11.30	1.79	13.70	8.14	111.42	3.12	0.07	0.98
11.32	1.77	13.50	8.23	111.15	3.12	0.07	0.96
11.34	1.71	13.00	8.49	110.30	3.14	0.07	0.93
11.36	1.62	12.16	8.98	109.22	3.18	0.07	0.87
11.38	1.49	11.04	9.77	107.83	3.24	0.06	0.79
11.40	1.36	9.90	10.69	105.81	3.30	0.06	0.71
11.42	1.23	8.75	11.79	103.09	3.37	0.06	0.62
11.44	1.11	7.72	12.97	100.07	3.44	0.06	0.55
11.46	1.00	6.77	14.27	96.57	3.51	0.06	0.48
11.48	0.93	6.11	15.24	93.17	3.56	0.06	0.44
11.50	0.87	5.62	15.87	89.28	3.59	0.06	0.40
11.52	0.83	5.29	16.14	85.47	3.61	0.06	0.38
11.54	0.82	5.21	15.76	82.09	3.59	0.06	0.37
11.56	0.84	5.30	14.90	78.97	3.54	0.06	0.38
11.58	0.86	5.47	13.80	75.50	3.48	0.06	0.39
11.60	0.87	5.61	12.76	71.54	3.43	0.06	0.40

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
11.62	0.90	5.84	11.67	68.21	3.36	0.06	0.42
11.64	0.96	6.33	10.36	65.58	3.28	0.06	0.45
11.66	1.04	6.94	9.12	63.31	3.19	0.06	0.50
11.68	1.07	7.22	8.34	60.22	3.13	0.06	0.52
11.70	1.09	7.38	7.75	57.17	3.09	0.06	0.53
11.72	1.27	8.91	6.73	59.92	3.00	0.06	0.64
11.74	1.44	10.31	6.15	63.38	2.94	0.07	0.74
11.76	1.52	10.97	6.09	66.80	2.94	0.07	0.78
11.78	1.36	9.56	6.82	65.19	3.01	0.06	0.68
11.80	1.20	8.20	7.60	62.33	3.07	0.06	0.59
11.82	1.10	7.39	8.01	59.21	3.11	0.06	0.53
11.84	1.06	7.03	8.11	57.00	3.11	0.06	0.50
11.87	1.02	6.71	8.31	55.74	3.13	0.06	0.48
11.88	0.98	6.38	8.58	54.71	3.15	0.06	0.46
11.90	0.95	6.13	8.74	53.57	3.16	0.06	0.44
11.92	0.97	6.22	8.48	52.76	3.14	0.06	0.44
11.94	1.02	6.68	7.94	53.03	3.10	0.06	0.48
11.96	1.13	7.57	7.17	54.26	3.04	0.06	0.54
11.98	1.29	8.85	6.26	55.42	2.96	0.06	0.63
12.00	1.43	10.03	5.62	56.35	2.89	0.07	0.72
12.02	1.49	10.54	5.49	57.89	2.88	0.07	0.75
12.04	1.46	10.20	6.00	61.17	2.93	0.07	0.73
12.06	1.36	9.36	7.00	65.55	3.02	0.06	0.67
12.08	1.25	8.45	8.37	70.75	3.13	0.06	0.60
12.10	1.15	7.65	9.83	75.17	3.24	0.06	0.55
12.12	1.08	7.04	11.17	78.69	3.33	0.06	0.50
12.14	1.03	6.66	12.11	80.68	3.39	0.06	0.48
12.16	1.01	6.44	12.65	81.44	3.42	0.06	0.46
12.18	1.01	6.45	12.57	81.03	3.41	0.06	0.46
12.20	1.04	6.71	11.88	79.67	3.37	0.06	0.48
12.22	1.09	7.08	10.91	77.25	3.31	0.06	0.51
12.24	1.14	7.47	9.96	74.44	3.25	0.06	0.53
12.26	1.19	7.88	9.02	71.06	3.18	0.06	0.56
12.28	1.24	8.26	8.33	68.85	3.13	0.06	0.59
12.30	1.28	8.56	7.95	68.03	3.10	0.06	0.61
12.32	1.30	8.69	7.96	69.19	3.10	0.06	0.62
12.34	1.31	8.82	8.05	70.95	3.11	0.06	0.63
12.36	1.33	8.97	8.07	72.42	3.11	0.06	0.64
12.38	1.35	9.11	8.13	74.06	3.12	0.06	0.65
12.40	1.38	9.33	8.09	75.43	3.11	0.06	0.67
12.42	1.40	9.48	8.11	76.86	3.11	0.06	0.68
12.44	1.43	9.65	8.13	78.42	3.12	0.06	0.69
12.46	1.44	9.75	8.24	80.30	3.12	0.06	0.70
12.48	1.47	9.99	8.25	82.39	3.13	0.06	0.71
12.51	1.49	10.11	8.40	84.96	3.14	0.06	0.72
12.52	1.50	10.17	8.66	88.06	3.16	0.06	0.73
12.54	1.48	10.00	9.11	91.04	3.19	0.06	0.71
12.56	1.47	9.88	9.49	93.76	3.22	0.06	0.71

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
12.58	1.43	9.61	9.99	96.02	3.25	0.06	0.69
12.60	1.41	9.38	10.47	98.27	3.28	0.06	0.67
12.62	1.38	9.11	10.97	99.92	3.32	0.06	0.65
12.64	1.36	8.97	11.22	100.61	3.33	0.06	0.64
12.66	1.35	8.89	11.29	100.40	3.34	0.06	0.64
12.68	1.38	9.08	10.97	99.63	3.32	0.06	0.65
12.70	1.41	9.30	10.64	99.00	3.30	0.06	0.66
12.72	1.43	9.43	10.32	97.34	3.27	0.06	0.67
12.75	1.44	9.49	10.16	96.40	3.26	0.06	0.68
12.76	1.44	9.51	10.05	95.56	3.26	0.06	0.68
12.78	1.43	9.45	10.16	95.97	3.26	0.06	0.67
12.80	1.42	9.29	10.33	95.95	3.27	0.06	0.66
12.82	1.41	9.21	10.39	95.74	3.28	0.06	0.66
12.84	1.41	9.24	10.33	95.45	3.27	0.06	0.66
12.86	1.41	9.17	10.39	95.24	3.28	0.06	0.65
12.88	1.38	8.94	10.67	95.36	3.30	0.06	0.64
12.90	1.34	8.63	11.03	95.15	3.32	0.06	0.62
12.92	1.31	8.36	11.28	94.33	3.34	0.06	0.60
12.94	1.30	8.28	11.26	93.26	3.33	0.06	0.59
12.96	1.31	8.35	11.08	92.48	3.32	0.06	0.60
12.98	1.33	8.47	10.83	91.74	3.31	0.06	0.61
13.01	1.33	8.50	10.70	90.99	3.30	0.06	0.61
13.02	1.34	8.57	10.53	90.18	3.29	0.06	0.61
13.04	1.34	8.55	10.48	89.63	3.28	0.06	0.61
13.06	1.34	8.51	10.46	89.00	3.28	0.06	0.61
13.08	1.32	8.34	10.57	88.12	3.29	0.06	0.60
13.10	1.29	8.14	10.69	87.01	3.30	0.06	0.58
13.12	1.28	7.99	10.73	85.70	3.30	0.06	0.57
13.14	1.26	7.84	10.80	84.65	3.31	0.06	0.56
13.16	1.22	7.50	11.19	83.98	3.33	0.06	0.54
13.18	1.16	7.03	11.89	83.58	3.37	0.06	0.50
13.20	1.09	6.52	12.72	82.94	3.42	0.06	0.47
13.23	1.07	6.31	13.01	82.13	3.44	0.06	0.45
13.24	1.06	6.28	12.98	81.45	3.44	0.06	0.45
13.26	1.08	6.37	12.64	80.45	3.42	0.06	0.45
13.29	1.10	6.50	12.11	78.77	3.39	0.06	0.46
13.30	1.12	6.69	11.43	76.40	3.35	0.06	0.48
13.32	1.13	6.72	11.02	74.06	3.32	0.06	0.48
13.34	1.12	6.70	10.75	72.03	3.30	0.06	0.48
13.36	1.12	6.62	10.61	70.26	3.29	0.06	0.47
13.38	1.14	6.78	10.13	68.66	3.26	0.06	0.48
13.40	1.17	6.97	9.69	67.54	3.23	0.06	0.50
13.42	1.21	7.29	9.19	66.98	3.20	0.06	0.52
13.44	1.25	7.56	8.82	66.68	3.17	0.06	0.54
13.46	1.29	7.87	8.47	66.70	3.14	0.06	0.56
13.48	1.33	8.17	8.23	67.25	3.12	0.06	0.58
13.50	1.37	8.42	8.09	68.15	3.11	0.06	0.60
13.52	1.38	8.54	8.10	69.21	3.11	0.06	0.61

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
13.54	1.39	8.60	8.12	69.77	3.11	0.06	0.61
13.56	1.38	8.49	8.32	70.62	3.13	0.06	0.61
13.58	1.34	8.20	8.71	71.39	3.16	0.06	0.59
13.60	1.30	7.84	9.14	71.69	3.19	0.06	0.56
13.62	1.27	7.63	9.30	71.01	3.20	0.06	0.55
13.64	1.27	7.61	9.22	70.16	3.20	0.06	0.54
13.66	1.27	7.64	9.23	70.46	3.20	0.06	0.55
13.68	1.30	7.82	9.19	71.79	3.20	0.06	0.56
13.70	1.34	8.12	9.02	73.23	3.18	0.06	0.58
13.72	1.36	8.26	8.79	72.62	3.17	0.06	0.59
13.74	1.39	8.47	8.60	72.79	3.15	0.06	0.60
13.76	1.40	8.50	8.62	73.26	3.15	0.06	0.61
13.78	1.41	8.59	8.73	74.92	3.16	0.06	0.61
13.80	1.37	8.28	8.97	74.25	3.18	0.06	0.59
13.82	1.35	8.12	9.13	74.16	3.19	0.06	0.58
13.85	1.33	7.92	9.33	73.94	3.21	0.06	0.57
13.86	1.33	7.95	9.35	74.33	3.21	0.06	0.57
13.88	1.31	7.76	9.49	73.67	3.22	0.06	0.55
13.90	1.29	7.66	9.56	73.20	3.22	0.06	0.55
13.92	1.28	7.51	9.70	72.83	3.23	0.06	0.54
13.94	1.27	7.42	9.74	72.29	3.23	0.06	0.53
13.96	1.25	7.33	9.80	71.77	3.24	0.06	0.52
13.98	1.23	7.16	9.99	71.56	3.25	0.06	0.51
14.00	1.22	7.07	10.14	71.64	3.26	0.06	0.50
14.02	1.21	6.95	10.36	72.04	3.28	0.06	0.50
14.04	1.19	6.85	10.57	72.38	3.29	0.06	0.49
14.06	1.18	6.72	10.81	72.63	3.31	0.06	0.48
14.08	1.15	6.52	11.25	73.37	3.33	0.06	0.47

Abbreviations

q_t:	Total cone resistance
K_c:	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c:	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

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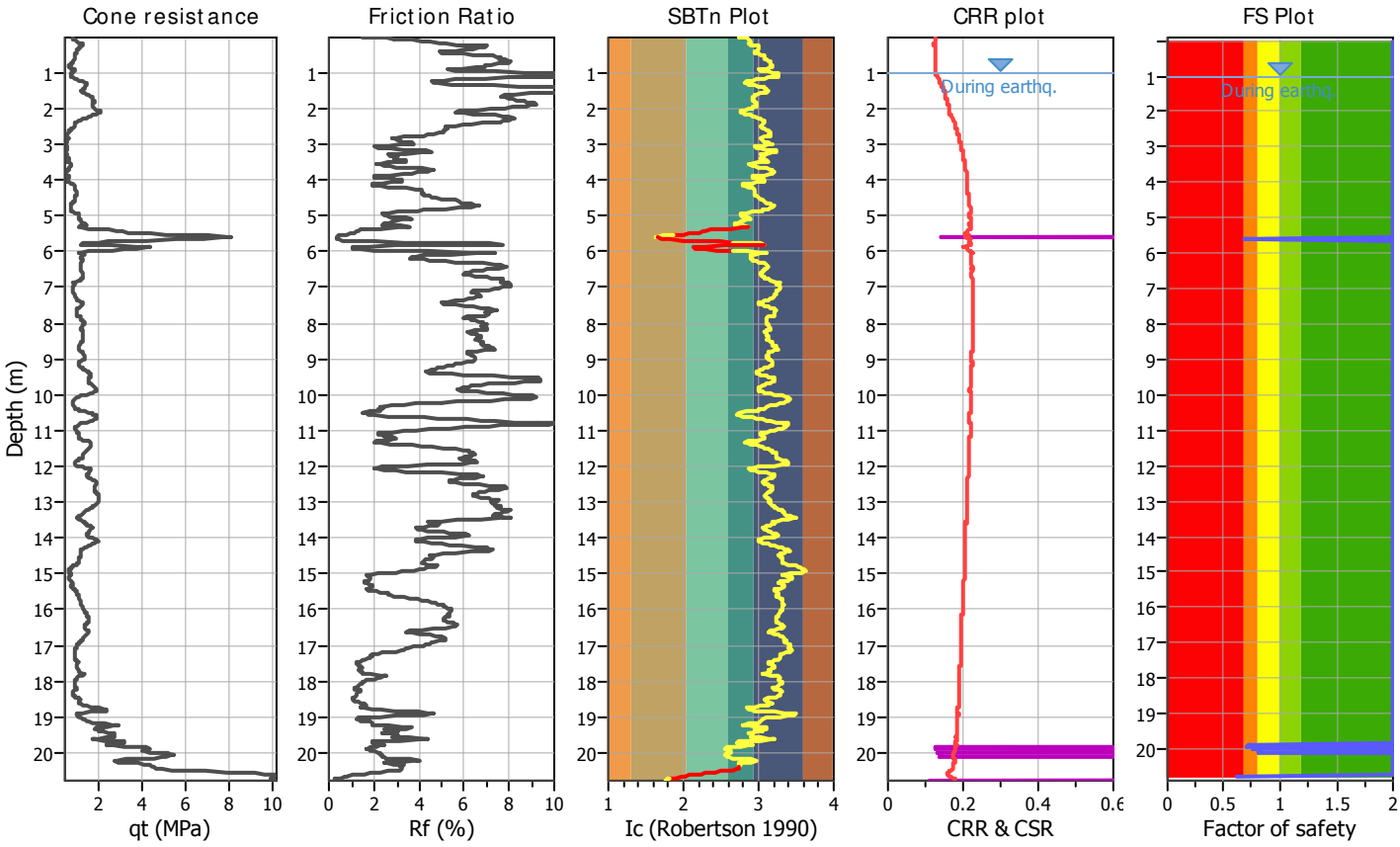
LIQUEFACTION ANALYSIS REPORT

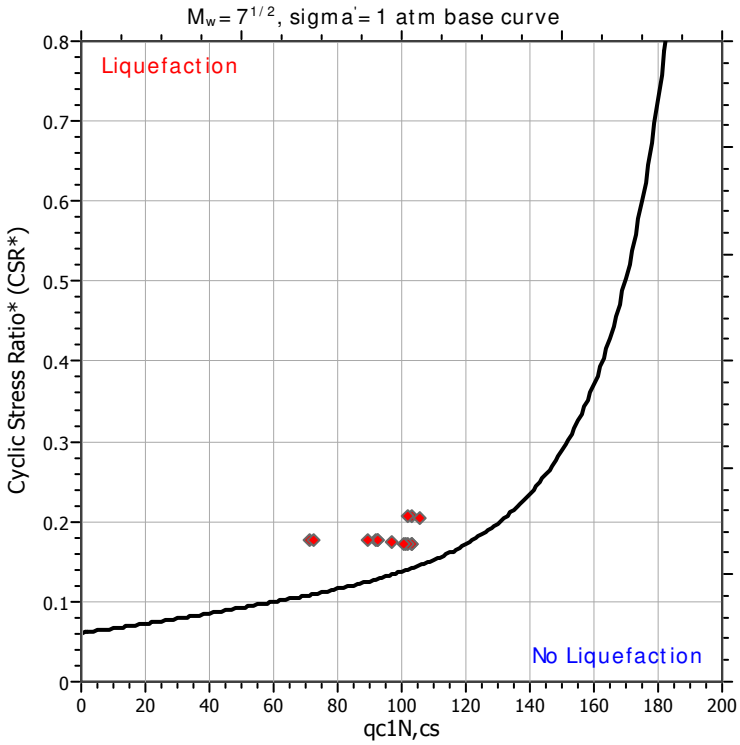
Project title : Location :

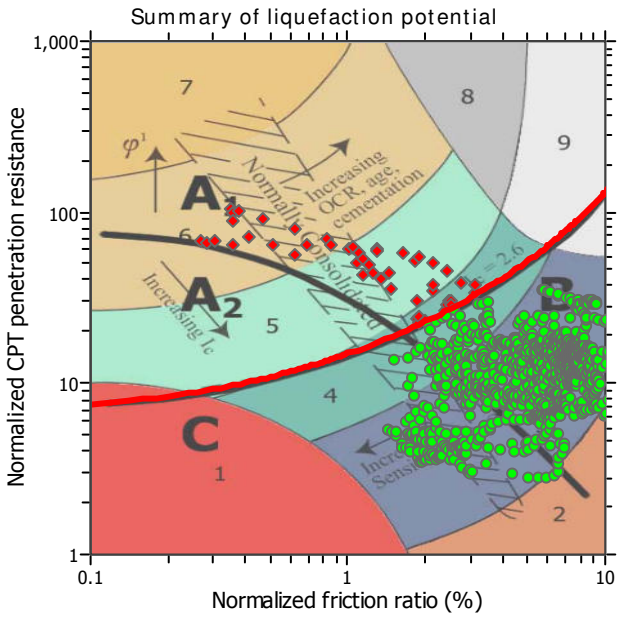
CPT file : CPTu-05_Biancolina

Input parameters and analysis data

Analysis method:	B&I (2014)	G.W.T. (in-situ):	1.80 m	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.00 m	Fill height:	N/A	Limit depth applied:	No
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	N/A
Earthquake magnitude M_w:	6.14	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.23	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		

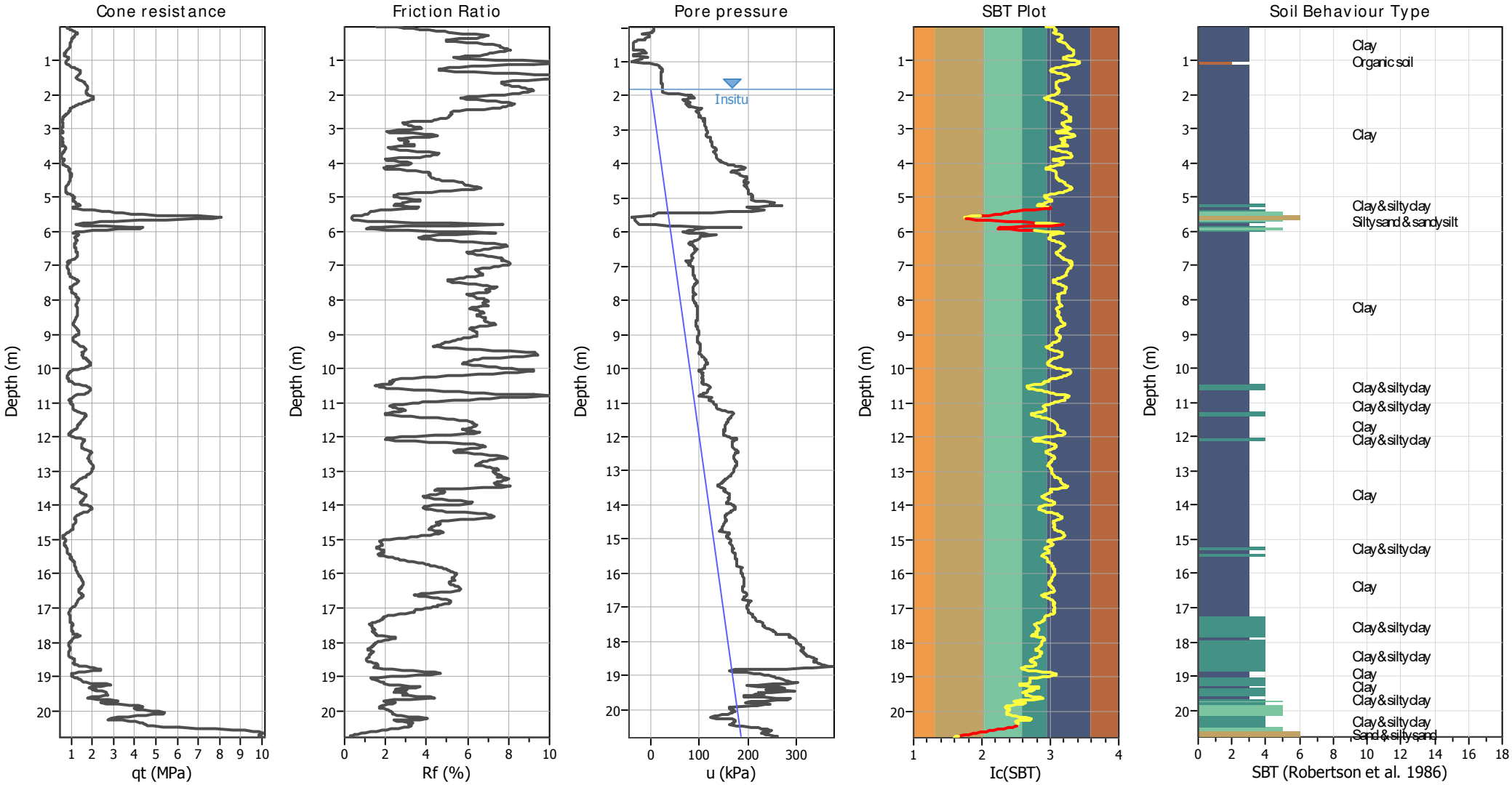






Zone A_1: Cyclic liquefaction likely depending on size and duration of cyclic loading
Zone A_2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



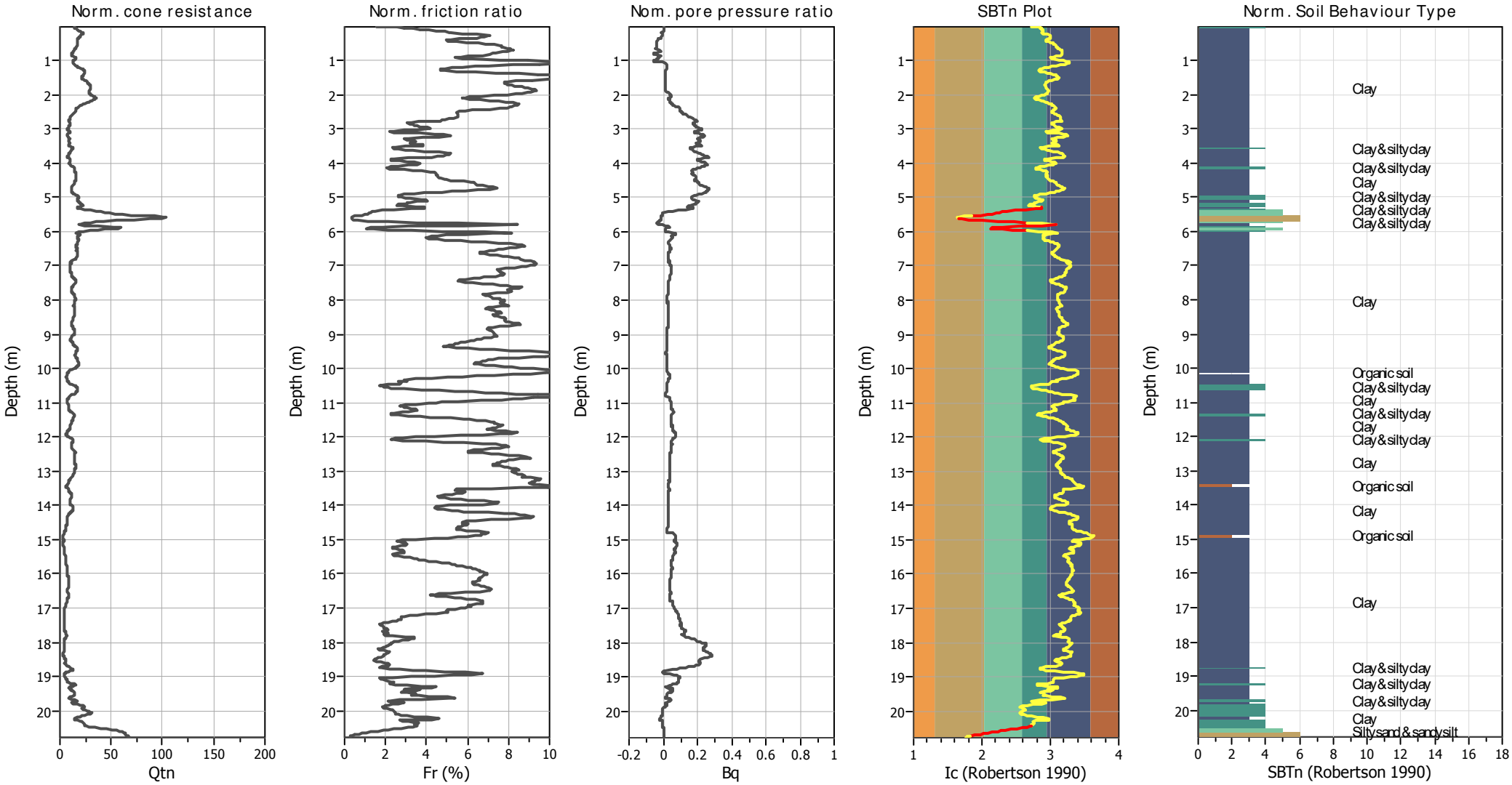
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	1.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.23	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	1.80 m	Fill height:	N/A	Limit depth:	N/A

SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

CPT basic interpretation plots (normalized)



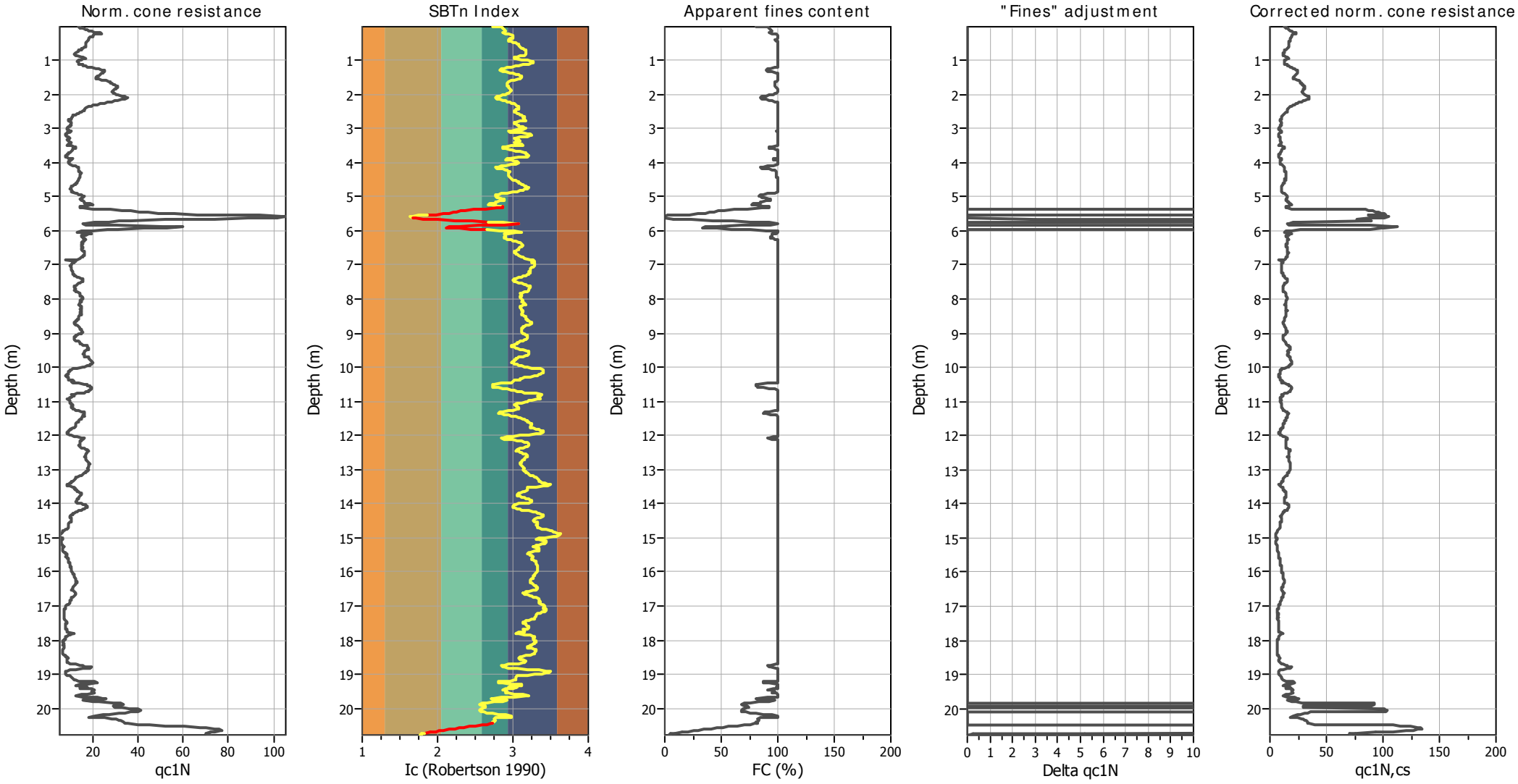
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	1.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.23	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	1.80 m	Fill height:	N/A	Limit depth:	N/A

SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

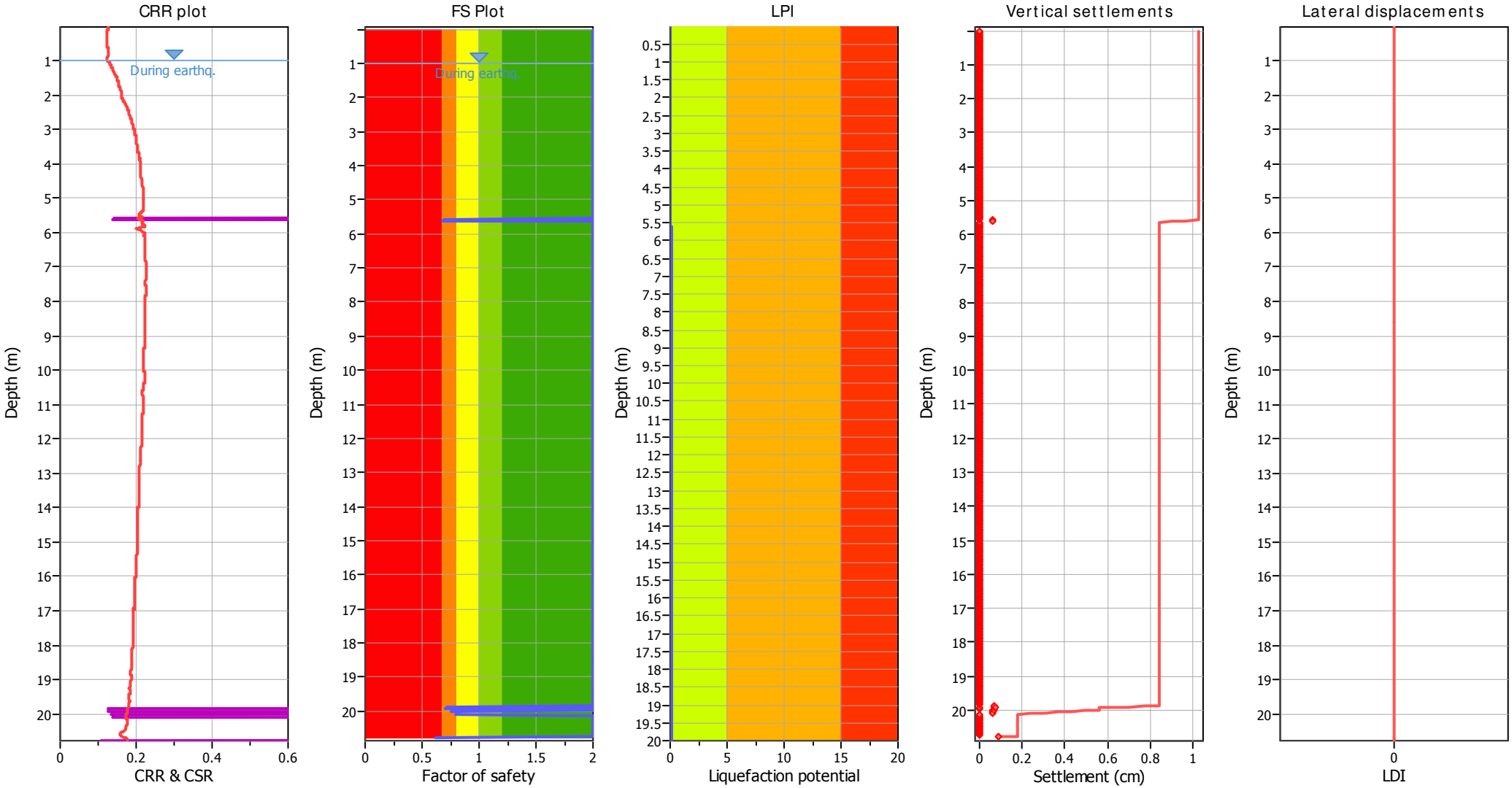
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	1.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.23	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	1.80 m	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	1.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.23	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	1.80 m	Fill height:	N/A	Limit depth:	N/A

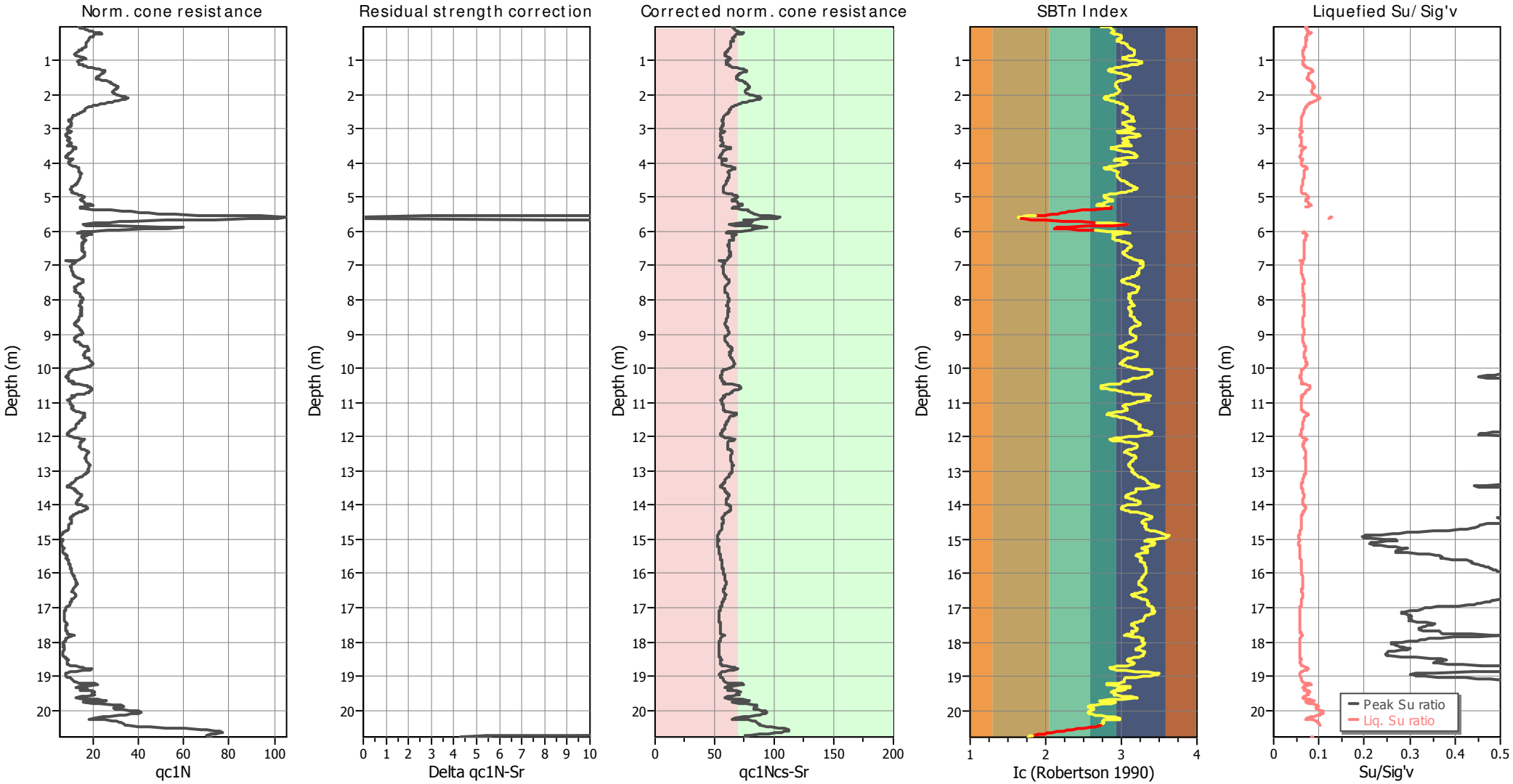
F.S. color scheme

- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

LPI color scheme

- Very high risk
- High risk
- Low risk

Check for strength loss plots (Idriss & Boulanger (2008))



Input parameters and analysis data

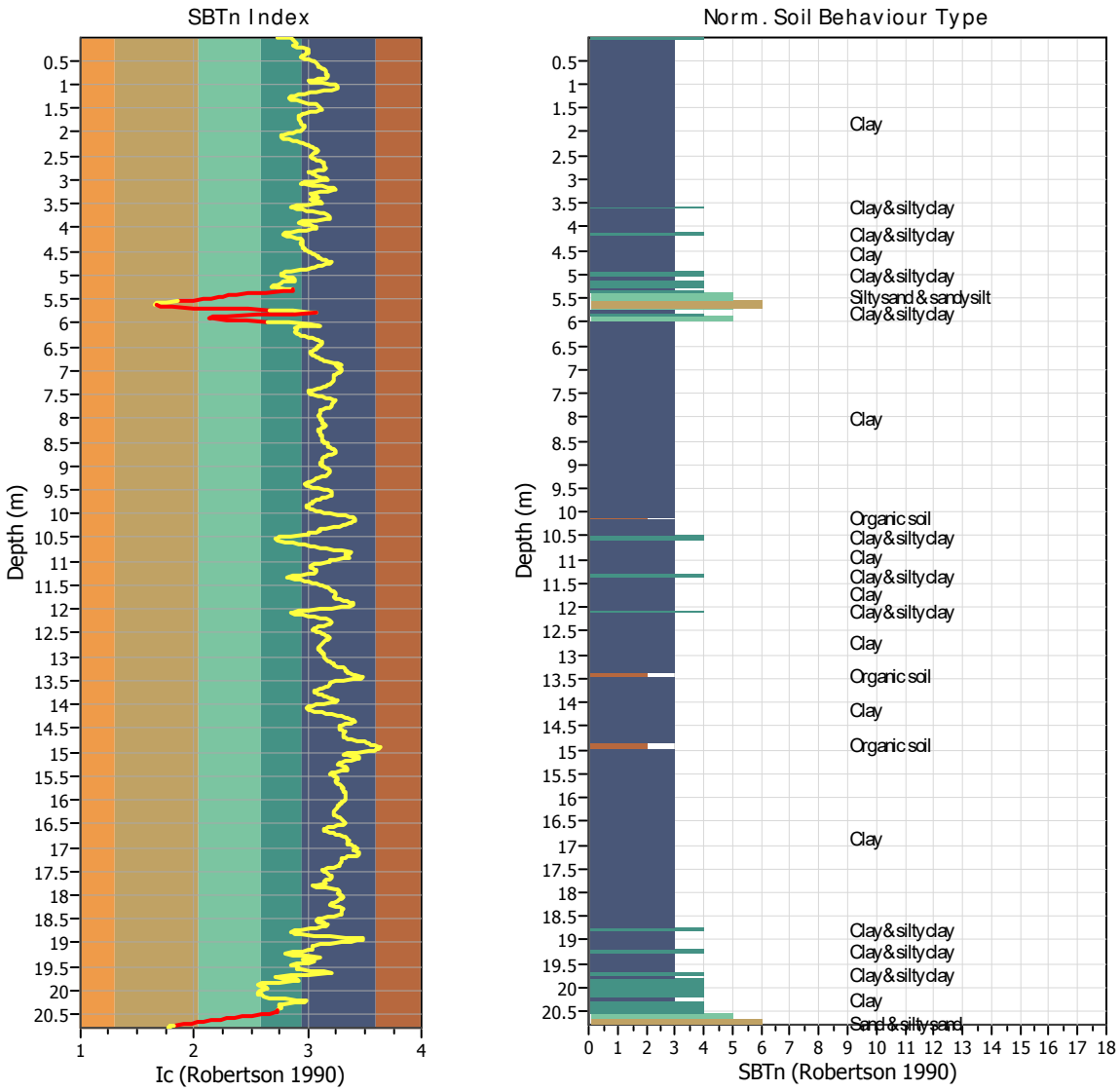
Analysis method:	B&I (2014)	Depth to GWT (erthq.):	1.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.23	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	1.80 m	Fill height:	N/A	Limit depth:	N/A

TRANSITION LAYER DETECTION ALGORITHM REPORT
Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vise-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between 1.80 < I_c < 3.0) and a rate of change of I_c. Transitions typically occur when the rate of change of I_c is fast (i.e. delta I_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties		General statistics	
I_c minimum check value:	1.70	Total points in CPT file:	1039
I_c maximum check value:	3.00	Total points excluded:	47
I_c change ratio value:	0.0100	Exclusion percentage:	4.52%
Minimum number of points in layer:	4	Number of layers detected:	5

Transition layer No	Number of points	Depth	SBT_n number	SBT_n description
Transition layer 1	13	Start depth: 5.32 (m)	3	Clay
		End depth: 5.56 (m)	6	Sand & silty sand
Transition layer 2	7	Start depth: 5.64 (m)	6	Sand & silty sand
		End depth: 5.76 (m)	3	Clay
Transition layer 3	5	Start depth: 5.82 (m)	3	Clay
		End depth: 5.90 (m)	5	Silty sand & sandy silt
Transition layer 4	6	Start depth: 5.90 (m)	5	Silty sand & sandy silt
		End depth: 6.00 (m)	3	Clay
Transition layer 5	16	Start depth: 20.44 (m)	4	Clay & silty clay
		End depth: 20.74 (m)	6	Sand & silty sand

Start depth: Depth where the transition layer begins
End depth: Depth where the transition layer ends

:: Field input data ::

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
1	0.02	0.81	9.33	4.98	41.77	15.79
2	0.04	0.78	18.34	4.74	48.61	16.37
3	0.06	0.84	24.46	4.92	49.55	16.59
4	0.08	0.90	30.00	4.55	50.39	16.87
5	0.10	0.97	35.96	3.63	50.65	17.07
6	0.12	1.01	39.90	1.85	51.36	17.28
7	0.14	1.06	48.52	1.05	51.74	17.46
8	0.16	1.14	54.74	0.31	52.21	17.67
9	0.18	1.22	64.38	-18.46	51.07	17.84
10	0.20	1.37	69.77	-7.75	50.18	17.96
11	0.22	1.39	72.40	-5.60	51.98	18.07
12	0.24	1.20	83.94	-3.08	55.20	18.12
13	0.26	1.17	84.21	-3.08	58.38	18.14
14	0.28	1.18	81.75	-5.91	58.35	18.11
15	0.30	1.17	77.78	-14.52	58.12	18.05
16	0.32	1.12	74.20	-14.03	58.41	17.98
17	0.34	1.07	69.88	-14.34	58.57	17.89
18	0.36	1.05	63.58	-17.23	57.84	17.79
19	0.38	1.05	57.53	-27.38	56.55	17.68
20	0.40	1.04	53.89	-32.49	54.95	17.59
21	0.42	1.06	49.77	-34.95	54.33	17.54
22	0.44	1.04	50.74	-36.62	54.72	17.53
23	0.46	1.01	53.53	-37.11	56.81	17.58
24	0.48	0.98	58.51	-37.42	59.10	17.65
25	0.50	0.97	62.42	-37.54	60.92	17.74
26	0.52	0.99	66.98	-37.72	62.12	17.81
27	0.54	0.99	70.99	-37.85	63.21	17.88
28	0.56	0.99	75.04	-37.91	63.98	17.92
29	0.58	0.99	74.28	-37.66	64.29	17.94
30	0.60	0.99	73.58	-37.72	64.53	17.92
31	0.62	0.96	72.31	-37.97	65.38	17.89
32	0.64	0.91	71.32	-37.91	66.64	17.86
33	0.66	0.89	70.04	-37.17	67.98	17.83
34	0.68	0.85	69.09	-16.62	68.79	17.79
35	0.70	0.84	66.75	-14.52	69.86	17.75
36	0.72	0.80	65.31	-19.63	70.23	17.71
37	0.74	0.80	62.50	-10.65	70.19	17.65
38	0.76	0.79	58.59	-18.52	70.27	17.56
39	0.78	0.73	53.47	-29.91	70.32	17.44
40	0.80	0.71	47.61	-36.18	71.26	17.33
41	0.82	0.68	46.88	-37.35	71.51	17.28
42	0.84	0.68	47.30	-28.92	71.45	17.27
43	0.86	0.70	47.30	-6.46	69.37	17.29
44	0.88	0.77	46.63	-17.42	64.96	17.29
45	0.90	0.86	43.62	-22.15	62.02	17.34
46	0.92	0.89	50.27	-20.62	59.17	17.39
47	0.94	0.97	49.28	-31.88	59.95	17.50
48	0.96	0.92	56.61	-29.91	61.69	17.59

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
49	0.98	0.88	62.19	-41.54	67.26	17.70
50	1.00	0.79	71.80	-42.22	72.45	17.80
51	1.02	0.77	76.54	-40.62	76.50	17.91
52	1.04	0.80	85.74	-14.77	78.04	17.98
53	1.06	0.79	87.92	-4.68	78.54	18.03
54	1.08	0.79	87.18	7.51	78.61	18.02
55	1.10	0.78	82.37	12.43	77.51	17.97
56	1.12	0.79	76.92	16.06	73.45	17.89
57	1.14	0.89	68.56	16.49	68.74	17.82
58	1.16	0.93	64.36	16.49	63.77	17.76
59	1.18	0.98	60.77	19.20	60.62	17.72
60	1.20	1.03	59.67	21.23	56.94	17.71
61	1.22	1.15	58.33	22.03	53.50	17.72
62	1.24	1.24	58.07	22.22	50.60	17.76
63	1.26	1.32	61.30	22.28	48.58	17.81
64	1.28	1.39	62.29	21.97	47.60	17.91
65	1.30	1.47	69.82	21.54	47.69	18.02
66	1.32	1.47	78.12	21.17	49.38	18.17
67	1.34	1.45	90.13	20.86	52.35	18.33
68	1.36	1.43	105.86	20.55	55.47	18.48
69	1.39	1.42	117.71	20.43	58.71	18.62
70	1.40	1.39	132.80	20.37	61.20	18.72
71	1.42	1.37	139.37	20.31	63.26	18.78
72	1.44	1.35	141.77	20.25	64.39	18.79
73	1.46	1.32	139.10	20.18	65.16	18.77
74	1.48	1.29	136.02	20.12	65.95	18.74
75	1.50	1.25	134.16	20.18	66.62	18.72
76	1.52	1.24	133.68	20.25	66.85	18.71
77	1.54	1.26	133.22	20.43	65.79	18.71
78	1.56	1.33	132.26	20.62	63.36	18.71
79	1.58	1.42	128.70	20.86	59.97	18.71
80	1.60	1.53	123.21	21.17	56.98	18.70
81	1.62	1.59	122.88	21.29	54.99	18.70
82	1.65	1.62	123.94	21.48	54.22	18.72
83	1.66	1.64	125.50	21.66	53.79	18.75
84	1.68	1.69	129.72	21.78	53.68	18.78
85	1.70	1.70	134.39	21.97	53.53	18.83
86	1.72	1.74	139.07	22.15	53.60	18.88
87	1.74	1.77	144.51	22.34	53.74	18.92
88	1.76	1.78	148.90	22.46	53.94	18.97
89	1.78	1.82	154.53	22.71	54.22	19.01
90	1.80	1.82	158.37	22.83	54.48	19.04
91	1.82	1.81	159.71	23.02	54.82	19.05
92	1.84	1.80	160.25	23.20	55.51	19.05
93	1.86	1.74	160.88	23.38	56.21	19.05
94	1.88	1.73	161.10	23.57	56.67	19.04
95	1.90	1.73	157.35	23.88	56.75	19.01
96	1.92	1.68	152.16	34.09	56.34	18.98

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
97	1.95	1.70	149.18	56.00	55.91	18.96
98	1.96	1.72	148.48	72.25	55.00	18.95
99	1.98	1.76	146.55	74.34	53.91	18.94
100	2.00	1.80	142.03	82.28	52.52	18.91
101	2.03	1.84	136.49	77.42	50.16	18.87
102	2.04	1.96	126.30	87.69	47.63	18.83
103	2.06	2.04	122.23	89.91	45.38	18.79
104	2.08	2.07	118.67	81.05	44.32	18.77
105	2.10	2.08	117.77	70.15	43.86	18.76
106	2.12	2.09	118.02	65.97	44.19	18.76
107	2.14	2.03	120.29	67.63	45.32	18.78
108	2.16	1.95	125.93	73.48	47.53	18.80
109	2.18	1.83	130.51	80.68	49.81	18.82
110	2.20	1.76	130.79	72.92	51.86	18.81
111	2.22	1.68	129.41	71.69	53.80	18.78
112	2.24	1.55	127.23	75.88	55.78	18.74
113	2.26	1.48	124.54	78.34	57.71	18.67
114	2.28	1.39	115.92	74.95	59.24	18.58
115	2.30	1.27	106.21	78.95	60.57	18.46
116	2.32	1.20	97.17	78.22	61.58	18.34
117	2.34	1.15	89.92	82.34	62.54	18.23
118	2.36	1.07	84.99	98.95	63.60	18.12
119	2.38	1.00	78.10	106.09	64.43	18.03
120	2.40	0.98	73.32	100.55	64.43	17.92
121	2.42	0.95	66.17	99.63	63.55	17.81
122	2.44	0.94	60.02	93.54	62.61	17.70
123	2.46	0.94	57.20	93.72	61.50	17.62
124	2.48	0.93	53.19	95.26	60.74	17.53
125	2.50	0.90	48.64	99.02	60.14	17.44
126	2.52	0.88	45.47	98.83	60.37	17.36
127	2.54	0.85	44.96	98.77	61.26	17.30
128	2.56	0.80	43.03	98.89	62.82	17.24
129	2.58	0.75	40.70	101.17	64.10	17.15
130	2.60	0.72	37.39	101.60	65.81	17.04
131	2.62	0.66	34.99	98.22	67.07	16.95
132	2.64	0.64	34.03	102.03	68.42	16.88
133	2.66	0.63	32.81	104.25	69.17	16.84
134	2.68	0.60	31.66	109.85	69.13	16.77
135	2.70	0.61	29.10	109.35	68.70	16.68
136	2.72	0.59	26.28	109.11	68.82	16.58
137	2.74	0.54	25.19	108.98	69.82	16.47
138	2.76	0.52	23.08	109.48	70.50	16.37
139	2.78	0.52	21.03	109.60	68.76	16.26
140	2.80	0.54	19.23	110.09	64.65	16.16
141	2.82	0.59	16.80	110.28	61.15	16.10
142	2.84	0.60	17.22	110.40	59.42	16.09
143	2.86	0.60	18.31	110.52	59.89	16.13
144	2.88	0.60	18.63	110.58	61.69	16.15

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
145	2.90	0.55	18.42	112.98	62.30	16.17
146	2.92	0.59	19.57	113.17	63.40	16.19
147	2.94	0.57	19.86	113.23	64.07	16.23
148	2.96	0.55	20.37	112.86	67.57	16.22
149	2.98	0.48	20.60	113.17	70.18	16.17
150	3.00	0.47	18.10	113.54	70.96	16.07
151	3.02	0.48	16.30	114.15	67.56	15.94
152	3.04	0.51	14.35	115.38	62.13	15.83
153	3.06	0.58	12.71	116.25	57.00	15.73
154	3.08	0.61	11.85	116.43	54.63	15.71
155	3.10	0.59	13.03	115.63	56.08	15.78
156	3.12	0.56	15.21	112.68	61.13	15.94
157	3.14	0.51	18.58	112.74	66.77	16.08
158	3.16	0.48	20.11	113.17	71.75	16.17
159	3.18	0.47	21.04	114.89	74.92	16.22
160	3.21	0.45	21.91	116.80	76.63	16.28
161	3.22	0.47	23.57	121.48	75.85	16.31
162	3.24	0.50	22.55	123.63	71.77	16.30
163	3.26	0.55	19.63	123.88	65.80	16.19
164	3.28	0.59	16.33	124.18	61.11	16.06
165	3.30	0.59	15.30	123.94	59.73	15.97
166	3.32	0.55	15.82	123.57	61.34	15.95
167	3.34	0.52	16.14	123.51	64.03	16.00
168	3.36	0.53	17.83	124.49	64.59	16.06
169	3.38	0.57	18.51	126.83	62.50	16.11
170	3.40	0.62	17.67	127.20	60.27	16.14
171	3.42	0.62	17.99	126.95	60.18	16.16
172	3.44	0.58	19.34	126.52	62.98	16.18
173	3.46	0.53	19.50	126.46	66.29	16.17
174	3.48	0.51	18.89	127.08	67.34	16.14
175	3.50	0.54	18.34	128.37	63.74	16.13
176	3.52	0.64	17.86	132.80	57.72	16.12
177	3.54	0.72	16.48	133.91	52.18	16.13
178	3.56	0.78	16.80	133.66	49.47	16.14
179	3.58	0.78	17.05	133.48	50.41	16.19
180	3.60	0.70	18.66	133.17	52.56	16.22
181	3.63	0.70	18.85	132.18	55.33	16.27
182	3.64	0.69	20.70	129.05	57.74	16.38
183	3.66	0.66	24.61	131.57	61.32	16.51
184	3.68	0.63	27.40	132.18	65.63	16.62
185	3.70	0.59	29.32	133.11	69.10	16.65
186	3.72	0.56	28.07	133.48	70.86	16.61
187	3.74	0.56	25.76	133.60	71.65	16.54
188	3.76	0.53	25.02	133.66	71.95	16.43
189	3.78	0.50	22.11	133.54	72.76	16.32
190	3.80	0.48	19.86	133.66	73.20	16.19
191	3.82	0.46	18.74	135.32	72.66	16.07
192	3.84	0.47	16.66	137.17	69.74	15.97

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
193	3.86	0.51	14.86	138.34	63.93	15.87
194	3.88	0.58	13.32	140.62	55.99	15.81
195	3.90	0.71	12.51	143.38	52.90	15.85
196	3.92	0.66	15.27	142.34	52.76	15.89
197	3.94	0.61	14.56	142.71	56.57	15.98
198	3.96	0.60	16.90	147.14	59.88	16.06
199	3.98	0.58	19.27	151.75	62.39	16.16
200	4.00	0.57	19.37	156.18	63.74	16.23
201	4.03	0.59	20.62	159.51	63.42	16.27
202	4.04	0.60	20.84	170.83	61.48	16.28
203	4.06	0.64	19.18	173.23	57.42	16.25
204	4.08	0.72	17.61	185.42	52.76	16.20
205	4.10	0.78	17.19	193.91	48.63	16.18
206	4.12	0.84	16.55	193.60	46.11	16.20
207	4.14	0.89	17.60	193.11	44.68	16.24
208	4.16	0.90	18.02	184.80	45.05	16.33
209	4.18	0.89	20.71	178.46	46.96	16.47
210	4.20	0.88	24.75	167.82	49.45	16.63
211	4.22	0.88	27.98	164.68	51.94	16.79
212	4.24	0.88	31.73	165.72	53.82	16.93
213	4.26	0.89	35.35	170.46	55.20	17.08
214	4.28	0.93	40.57	180.92	55.43	17.20
215	4.30	0.97	42.30	181.85	54.95	17.27
216	4.32	0.98	41.31	182.22	54.53	17.28
217	4.34	0.97	41.15	183.94	54.69	17.28
218	4.36	0.95	42.04	193.35	55.04	17.27
219	4.38	0.95	41.46	198.65	55.10	17.28
220	4.40	0.96	41.40	198.83	54.96	17.28
221	4.42	0.96	42.10	199.38	55.31	17.29
222	4.44	0.94	42.97	198.22	56.10	17.31
223	4.46	0.93	43.54	194.40	57.03	17.32
224	4.48	0.93	44.57	192.49	57.61	17.34
225	4.50	0.93	45.69	191.20	58.47	17.38
226	4.52	0.91	47.61	192.86	59.69	17.43
227	4.54	0.90	51.06	200.55	61.26	17.47
228	4.56	0.89	51.67	198.65	62.84	17.50
229	4.58	0.86	52.95	199.57	63.84	17.50
230	4.60	0.86	52.50	197.17	64.45	17.49
231	4.62	0.84	50.39	194.09	64.87	17.46
232	4.64	0.82	50.19	193.66	65.95	17.43
233	4.66	0.79	50.00	196.00	67.69	17.41
234	4.68	0.75	49.39	198.09	69.79	17.39
235	4.70	0.72	49.58	198.83	71.51	17.37
236	4.72	0.70	49.32	199.02	72.97	17.36
237	4.74	0.69	48.94	200.00	73.36	17.33
238	4.76	0.68	46.53	200.62	72.43	17.27
239	4.78	0.70	42.59	201.17	70.09	17.19
240	4.80	0.72	39.00	201.78	67.46	17.10

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
241	4.82	0.72	35.83	202.15	64.78	16.99
242	4.84	0.74	31.91	202.52	62.81	16.89
243	4.86	0.73	29.86	202.09	61.41	16.81
244	4.88	0.72	29.06	203.32	58.09	16.74
245	4.90	0.84	25.61	207.51	53.99	16.70
246	4.92	0.90	24.71	209.35	49.24	16.66
247	4.94	0.97	24.39	209.91	46.48	16.69
248	4.96	1.04	25.42	210.71	44.59	16.75
249	4.98	1.10	27.43	208.68	43.79	16.85
250	5.00	1.12	29.52	210.77	43.86	16.93
251	5.02	1.12	30.77	209.85	45.28	17.01
252	5.04	1.07	34.36	206.83	46.87	17.07
253	5.06	1.06	35.32	207.45	50.06	17.18
254	5.08	1.00	42.08	217.11	51.32	17.26
255	5.11	1.06	42.01	234.28	50.90	17.29
256	5.12	1.12	38.23	254.65	47.73	17.23
257	5.14	1.16	33.90	253.23	45.24	17.16
258	5.16	1.18	34.06	250.09	44.32	17.14
259	5.18	1.17	35.47	247.94	44.23	17.16
260	5.20	1.20	35.63	252.92	42.50	17.17
261	5.22	1.36	33.23	269.85	40.13	17.18
262	5.24	1.45	34.10	247.51	39.19	17.20
263	5.26	1.35	36.37	222.40	41.44	17.26
264	5.28	1.20	40.09	197.97	46.14	17.30
265	5.30	1.04	42.26	210.83	50.10	17.29
266	5.32	1.02	38.87	213.11	50.37	17.25
267	5.34	1.14	37.07	224.92	45.32	17.26
268	5.36	1.46	37.81	235.94	36.83	17.31
269	5.38	2.06	34.70	209.97	29.91	17.38
270	5.40	2.45	34.99	162.22	24.97	17.42
271	5.42	2.77	34.95	124.92	22.51	17.51
272	5.44	3.09	38.45	12.74	20.71	17.59
273	5.46	3.38	39.50	8.43	19.29	17.71
274	5.48	3.76	42.74	5.48	17.57	17.82
275	5.50	4.33	45.59	4.18	15.18	17.89
276	5.52	5.13	41.46	0.18	12.63	17.90
277	5.54	5.79	37.96	-4.55	9.47	17.82
278	5.56	7.22	30.72	-43.38	5.00	17.73
279	5.58	8.07	27.87	-37.42	5.00	17.66
280	5.60	8.27	29.18	-35.57	5.00	17.63
281	5.62	7.98	27.26	-34.71	5.00	17.57
282	5.64	6.86	24.98	-34.22	5.00	17.38
283	5.66	5.64	20.02	-33.60	5.00	17.20
284	5.68	4.03	21.39	-32.80	12.89	17.24
285	5.70	2.81	33.98	-31.32	20.31	17.49
286	5.72	2.45	48.08	-29.72	29.35	17.82
287	5.74	2.06	67.21	-27.02	38.63	18.11
288	5.76	1.55	87.74	-24.49	49.66	18.26

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
289	5.78	1.23	96.17	7.63	60.40	18.31
290	5.80	1.14	96.16	36.00	64.11	18.28
291	5.82	1.25	88.50	60.43	50.87	18.30
292	5.84	2.35	75.14	114.34	33.36	18.36
293	5.86	4.07	69.63	186.28	22.25	18.33
294	5.88	4.79	55.84	117.54	17.61	18.18
295	5.90	4.18	42.10	95.94	16.56	17.93
296	5.92	3.70	38.03	91.26	17.77	17.74
297	5.94	3.39	39.37	87.45	22.11	17.80
298	5.96	2.43	55.84	76.74	28.52	17.96
299	5.98	2.08	67.57	72.62	37.88	18.02
300	6.00	1.54	65.30	64.62	47.87	18.06
301	6.02	1.12	79.07	78.65	60.05	18.05
302	6.05	0.97	84.23	108.25	66.34	18.10
303	6.06	1.19	82.85	120.68	61.17	18.14
304	6.08	1.49	78.81	135.32	54.82	18.08
305	6.10	1.38	63.24	111.63	51.41	17.91
306	6.12	1.27	50.96	102.71	51.90	17.67
307	6.14	1.15	47.60	101.29	52.33	17.49
308	6.16	1.13	42.28	100.49	51.96	17.40
309	6.18	1.21	41.35	100.06	51.27	17.39
310	6.20	1.20	45.90	97.91	51.31	17.50
311	6.22	1.26	53.62	97.85	52.52	17.65
312	6.24	1.29	59.90	93.05	53.46	17.76
313	6.26	1.26	60.83	88.92	54.84	17.83
314	6.28	1.25	65.53	85.35	56.61	17.90
315	6.30	1.24	71.08	78.95	58.66	17.97
316	6.32	1.21	75.56	77.35	61.27	18.06
317	6.34	1.18	83.41	78.09	63.59	18.14
318	6.36	1.19	89.37	78.95	65.27	18.21
319	6.38	1.19	92.19	87.26	66.37	18.26
320	6.40	1.16	93.76	87.88	67.24	18.27
321	6.42	1.16	93.99	89.78	67.75	18.27
322	6.44	1.17	93.31	88.25	67.53	18.27
323	6.46	1.17	92.03	89.42	66.40	18.25
324	6.48	1.21	87.83	96.37	65.43	18.22
325	6.50	1.20	85.94	95.26	64.46	18.18
326	6.52	1.19	82.64	90.52	64.01	18.14
327	6.54	1.20	79.79	91.08	63.46	18.11
328	6.56	1.20	78.50	91.08	62.56	18.09
329	6.58	1.24	78.41	89.72	61.35	18.09
330	6.60	1.28	77.03	88.86	60.22	18.09
331	6.62	1.29	77.35	87.75	59.77	18.10
332	6.64	1.29	80.07	86.65	59.83	18.12
333	6.66	1.31	80.58	84.31	60.45	18.16
334	6.68	1.30	84.65	83.26	61.48	18.20
335	6.70	1.27	89.20	82.03	62.59	18.24
336	6.72	1.29	90.90	82.34	63.63	18.28

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
337	6.74	1.27	92.82	85.35	64.46	18.29
338	6.76	1.24	93.27	85.11	66.26	18.29
339	6.78	1.18	94.74	83.88	67.67	18.27
340	6.80	1.16	90.25	84.00	68.81	18.23
341	6.82	1.12	86.28	83.14	69.73	18.17
342	6.84	1.06	83.20	81.29	75.51	17.88
343	6.86	0.59	46.58	71.38	77.88	17.83
344	6.88	0.98	79.61	73.97	80.13	17.78
345	6.90	0.93	77.30	80.00	76.30	17.97
346	6.92	0.91	73.94	80.12	77.60	17.92
347	6.94	0.88	72.18	78.34	78.64	17.87
348	6.96	0.86	71.47	77.48	79.71	17.84
349	6.98	0.84	68.65	81.97	80.28	17.79
350	7.00	0.82	64.68	84.98	80.22	17.72
351	7.02	0.81	61.93	85.42	80.27	17.67
352	7.04	0.80	60.42	86.22	79.79	17.64
353	7.06	0.82	59.42	86.52	78.66	17.61
354	7.08	0.84	56.80	86.58	76.76	17.58
355	7.10	0.85	55.07	87.02	75.44	17.55
356	7.12	0.85	54.58	86.83	75.16	17.54
357	7.14	0.84	55.48	86.71	75.37	17.56
358	7.16	0.86	57.18	86.65	75.17	17.59
359	7.19	0.89	58.97	87.38	74.96	17.63
360	7.20	0.89	59.87	87.63	74.62	17.66
361	7.22	0.90	61.54	87.75	74.70	17.69
362	7.24	0.91	63.30	87.75	74.54	17.73
363	7.26	0.92	64.20	87.45	73.70	17.75
364	7.28	0.96	63.97	88.49	72.91	17.76
365	7.31	0.97	64.33	89.48	71.32	17.77
366	7.32	1.01	63.62	89.91	69.87	17.77
367	7.34	1.04	62.53	89.91	68.21	17.78
368	7.36	1.06	63.52	90.40	66.70	17.80
369	7.38	1.12	65.32	91.82	64.27	17.84
370	7.41	1.22	65.03	93.72	61.38	17.88
371	7.42	1.30	65.57	94.95	59.16	17.90
372	7.44	1.31	66.66	95.08	58.34	17.93
373	7.46	1.32	68.10	94.58	58.43	17.96
374	7.48	1.33	69.77	93.72	59.56	17.99
375	7.50	1.27	72.49	92.68	61.50	18.01
376	7.52	1.22	74.38	91.51	64.41	18.02
377	7.54	1.15	75.95	90.46	67.16	18.02
378	7.56	1.10	75.63	89.42	69.50	18.01
379	7.58	1.07	75.18	88.18	71.37	17.99
380	7.60	1.04	75.76	86.65	73.02	17.98
381	7.62	1.00	75.44	85.78	74.66	17.97
382	7.64	0.98	74.22	85.23	76.06	17.94
383	7.66	0.96	73.42	86.52	75.80	17.92
384	7.68	1.00	71.40	86.71	74.85	17.91

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
385	7.70	1.01	71.11	86.71	73.40	17.91
386	7.72	1.03	71.34	86.40	73.48	17.91
387	7.74	1.01	72.52	86.58	73.74	17.93
388	7.76	1.02	73.64	86.58	74.16	17.94
389	7.78	1.02	73.87	88.98	72.97	17.95
390	7.80	1.08	72.81	90.95	69.86	17.96
391	7.82	1.20	71.40	92.12	67.07	17.97
392	7.84	1.20	72.61	91.75	65.48	17.99
393	7.86	1.20	73.61	86.03	65.98	18.01
394	7.88	1.20	75.76	85.66	66.69	18.05
395	7.90	1.20	78.80	85.78	66.62	18.09
396	7.92	1.26	80.82	86.09	65.82	18.14
397	7.94	1.31	83.93	86.09	65.33	18.21
398	7.96	1.32	90.72	86.15	65.46	18.27
399	7.98	1.33	92.77	86.40	65.81	18.30
400	8.01	1.34	92.19	86.58	65.97	18.30
401	8.02	1.32	90.81	88.06	67.01	18.29
402	8.04	1.25	92.32	90.22	67.53	18.28
403	8.06	1.30	90.52	91.02	67.66	18.26
404	8.08	1.29	87.03	91.08	66.98	18.24
405	8.10	1.27	86.04	91.94	67.60	18.21
406	8.12	1.23	85.84	91.63	68.95	18.20
407	8.15	1.19	86.03	92.86	70.26	18.18
408	8.17	1.17	84.75	95.26	70.09	18.17
409	8.18	1.23	83.40	95.88	68.74	18.16
410	8.20	1.27	83.05	96.37	66.80	18.16
411	8.22	1.30	82.05	96.62	65.54	18.17
412	8.24	1.32	81.67	96.86	64.78	18.16
413	8.26	1.32	81.51	96.86	65.00	18.17
414	8.28	1.30	83.72	96.80	65.94	18.19
415	8.30	1.28	85.99	96.62	66.47	18.21
416	8.32	1.32	86.95	96.98	66.57	18.24
417	8.34	1.33	88.74	96.92	66.62	18.25
418	8.36	1.30	89.35	96.49	67.39	18.26
419	8.38	1.28	89.96	96.25	67.83	18.25
420	8.40	1.29	87.59	96.18	67.77	18.24
421	8.42	1.29	86.15	96.43	67.16	18.21
422	8.44	1.30	83.97	96.37	66.82	18.20
423	8.46	1.31	84.51	96.31	67.03	18.20
424	8.48	1.27	85.15	95.51	68.08	18.20
425	8.50	1.23	85.56	94.95	69.25	18.19
426	8.52	1.22	84.60	94.77	70.25	18.18
427	8.54	1.20	83.93	94.46	70.82	18.16
428	8.56	1.19	83.74	94.46	71.05	18.15
429	8.58	1.20	81.65	94.28	71.41	18.13
430	8.60	1.16	80.47	93.66	71.67	18.10
431	8.62	1.15	79.12	93.42	72.64	18.08
432	8.64	1.12	79.09	92.86	73.69	18.07

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
433	8.66	1.09	79.22	92.06	75.11	18.05
434	8.68	1.06	77.58	91.88	75.96	18.04
435	8.70	1.07	77.77	92.25	76.95	18.03
436	8.72	1.04	80.11	92.80	76.97	18.05
437	8.74	1.07	80.50	93.91	76.24	18.07
438	8.76	1.12	79.50	94.95	73.78	18.08
439	8.78	1.18	78.93	95.75	71.41	18.08
440	8.80	1.21	77.90	96.18	69.64	18.08
441	8.82	1.24	78.03	96.25	68.06	18.09
442	8.84	1.30	78.33	96.31	67.33	18.12
443	8.86	1.30	81.38	96.43	66.84	18.16
444	8.88	1.32	84.19	97.11	67.08	18.19
445	8.90	1.33	85.32	97.35	66.90	18.23
446	8.92	1.36	88.78	97.78	66.79	18.26
447	8.94	1.38	90.44	98.09	66.54	18.29
448	8.96	1.39	91.15	98.22	66.57	18.30
449	8.98	1.38	90.09	98.03	66.96	18.29
450	9.00	1.34	88.36	97.42	67.62	18.25
451	9.02	1.31	85.31	97.11	68.45	18.21
452	9.04	1.27	82.84	96.74	69.80	18.15
453	9.06	1.17	77.72	95.69	71.34	18.07
454	9.08	1.13	73.01	95.20	72.48	17.98
455	9.10	1.11	68.61	94.95	72.75	17.90
456	9.12	1.08	64.70	94.34	72.34	17.82
457	9.14	1.08	60.89	94.22	72.11	17.77
458	9.16	1.07	59.93	94.40	71.70	17.73
459	9.18	1.07	58.84	94.52	71.17	17.72
460	9.20	1.10	59.19	95.32	69.84	17.74
461	9.22	1.16	60.79	96.74	67.36	17.78
462	9.24	1.26	62.36	98.03	64.83	17.83
463	9.26	1.32	63.77	99.88	63.24	17.87
464	9.29	1.32	64.48	100.80	62.58	17.88
465	9.30	1.32	62.59	101.17	62.09	17.88
466	9.32	1.36	63.19	100.92	60.59	17.88
467	9.34	1.44	63.83	101.97	58.58	17.93
468	9.36	1.54	66.11	102.65	56.72	17.99
469	9.38	1.62	70.69	103.08	56.69	18.10
470	9.40	1.61	81.27	102.28	57.61	18.24
471	9.42	1.67	91.10	102.28	59.21	18.38
472	9.44	1.70	101.16	102.09	60.86	18.51
473	9.46	1.67	112.38	102.52	62.74	18.62
474	9.48	1.68	121.83	102.46	65.35	18.71
475	9.50	1.62	131.73	100.43	68.55	18.79
476	9.52	1.52	140.47	98.46	71.85	18.83
477	9.54	1.50	143.48	98.34	73.45	18.86
478	9.56	1.55	144.83	99.38	73.48	18.88
479	9.58	1.55	146.17	103.08	73.71	18.89
480	9.60	1.50	147.04	104.18	73.99	18.88

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
481	9.62	1.52	143.06	105.35	73.74	18.86
482	9.64	1.53	136.65	106.03	72.04	18.81
483	9.66	1.56	128.16	108.25	70.39	18.75
484	9.68	1.57	122.68	111.38	67.99	18.71
485	9.70	1.65	117.49	111.75	65.76	18.67
486	9.72	1.70	114.79	111.94	63.84	18.66
487	9.74	1.72	113.99	112.18	62.62	18.65
488	9.76	1.76	112.93	112.74	61.54	18.64
489	9.78	1.79	110.14	112.74	60.77	18.65
490	9.80	1.81	114.02	112.55	60.16	18.66
491	9.82	1.85	114.72	112.62	59.22	18.66
492	9.84	1.90	108.08	118.22	58.10	18.65
493	9.86	1.93	109.97	116.37	57.67	18.66
494	9.88	1.91	114.17	113.23	58.39	18.69
495	9.90	1.89	118.21	111.51	60.13	18.73
496	9.92	1.82	123.88	112.06	61.79	18.76
497	9.94	1.79	125.77	112.06	64.01	18.77
498	9.96	1.70	126.95	111.02	66.32	18.76
499	9.98	1.58	124.90	109.54	68.95	18.72
500	10.00	1.52	121.44	108.74	73.10	18.65
501	10.03	1.27	114.26	103.32	77.51	18.55
502	10.04	1.17	107.25	99.51	83.16	18.44
503	10.06	1.06	101.28	99.14	86.58	18.33
504	10.08	1.00	94.71	99.57	89.55	18.23
505	10.10	0.94	87.53	101.54	90.54	18.12
506	10.12	0.93	79.91	104.55	90.74	17.99
507	10.14	0.89	69.81	106.22	90.56	17.86
508	10.16	0.85	64.20	105.05	89.99	17.72
509	10.18	0.84	56.74	105.60	88.32	17.58
510	10.20	0.84	48.89	107.20	86.06	17.40
511	10.22	0.80	40.97	106.28	84.27	17.20
512	10.24	0.77	34.79	105.91	82.80	17.02
513	10.26	0.78	31.39	105.97	80.04	16.87
514	10.28	0.80	27.81	106.09	75.45	16.74
515	10.30	0.86	24.12	106.58	69.95	16.61
516	10.32	0.91	20.95	107.26	65.95	16.51
517	10.34	0.91	20.73	106.95	65.09	16.48
518	10.36	0.88	22.37	105.66	65.80	16.53
519	10.38	0.91	23.75	105.17	63.87	16.59
520	10.40	1.05	23.27	107.63	59.76	16.61
521	10.42	1.12	21.80	106.71	58.67	16.68
522	10.44	1.04	27.21	104.12	59.12	16.74
523	10.46	1.07	26.83	106.15	56.58	16.81
524	10.48	1.35	25.07	113.78	49.03	16.79
525	10.50	1.60	22.13	118.34	42.77	16.82
526	10.52	1.73	24.79	118.83	42.02	17.03
527	10.54	1.72	37.54	121.66	41.59	17.16
528	10.56	1.85	30.88	121.78	42.21	17.31

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
529	10.58	1.88	36.62	119.51	42.55	17.45
530	10.60	1.90	49.72	118.52	46.08	17.76
531	10.62	1.90	66.38	118.15	49.81	18.04
532	10.64	1.90	78.95	118.22	53.80	18.27
533	10.66	1.85	94.14	116.74	56.82	18.42
534	10.68	1.84	100.93	115.94	60.24	18.56
535	10.70	1.78	114.52	113.66	62.88	18.63
536	10.72	1.71	116.25	111.82	66.33	18.67
537	10.74	1.60	119.61	108.92	70.00	18.67
538	10.76	1.48	122.24	106.46	75.40	18.66
539	10.78	1.30	123.62	102.89	81.47	18.63
540	10.80	1.18	122.65	100.74	88.11	18.58
541	10.82	1.06	118.23	99.57	88.49	18.48
542	10.84	1.17	96.69	126.34	87.01	18.34
543	10.86	1.10	86.60	123.63	83.67	18.16
544	10.88	1.03	75.32	122.46	84.19	17.98
545	10.90	0.97	62.89	120.55	85.59	17.78
546	10.92	0.87	56.51	118.65	86.17	17.60
547	10.94	0.87	50.20	120.62	82.72	17.46
548	10.96	1.00	42.92	128.55	77.25	17.32
549	10.98	0.99	37.48	128.92	73.15	17.19
550	11.00	0.95	35.11	127.51	72.45	17.09
551	11.03	0.95	34.05	128.80	70.76	17.00
552	11.04	1.00	29.31	132.25	66.52	16.88
553	11.06	1.06	24.18	133.78	62.52	16.76
554	11.08	1.07	24.12	133.91	60.24	16.70
555	11.10	1.08	24.82	135.38	60.14	16.71
556	11.12	1.08	25.01	135.69	60.56	16.76
557	11.14	1.08	26.94	136.25	61.33	16.78
558	11.16	1.06	26.55	135.75	62.33	16.83
559	11.18	1.07	28.76	136.43	63.34	16.91
560	11.20	1.09	32.35	140.92	63.80	17.02
561	11.22	1.13	34.73	148.18	63.69	17.11
562	11.24	1.16	35.43	152.31	61.88	17.14
563	11.26	1.24	34.34	159.20	58.47	17.15
564	11.28	1.37	33.16	166.83	54.33	17.16
565	11.30	1.49	33.48	170.71	49.87	17.16
566	11.32	1.63	30.92	170.95	47.38	17.18
567	11.34	1.66	33.06	169.35	46.56	17.25
568	11.36	1.68	38.42	168.62	48.27	17.40
569	11.38	1.67	45.21	167.08	51.31	17.59
570	11.40	1.61	54.60	164.43	54.67	17.76
571	11.42	1.59	61.36	163.75	57.01	17.90
572	11.44	1.64	65.17	164.00	59.39	18.02
573	11.46	1.58	76.45	162.28	61.54	18.13
574	11.48	1.55	80.55	160.92	64.15	18.21
575	11.50	1.55	84.14	159.88	65.81	18.25
576	11.52	1.51	86.03	158.65	67.53	18.28

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
577	11.54	1.46	88.40	157.91	69.61	18.30
578	11.56	1.42	91.12	157.60	71.40	18.31
579	11.58	1.40	90.61	156.80	72.16	18.30
580	11.60	1.40	87.69	156.18	72.64	18.28
581	11.62	1.36	87.05	154.52	73.69	18.26
582	11.64	1.30	87.46	153.60	75.08	18.23
583	11.66	1.28	84.25	152.86	76.50	18.20
584	11.68	1.24	82.23	151.88	76.78	18.16
585	11.70	1.24	80.18	151.94	76.73	18.13
586	11.72	1.26	80.02	152.62	76.15	18.12
587	11.74	1.25	77.94	152.92	75.89	18.09
588	11.76	1.23	75.12	153.29	75.62	18.03
589	11.78	1.22	69.38	152.68	76.47	17.97
590	11.80	1.14	67.71	149.91	79.02	17.88
591	11.82	1.01	63.69	150.40	81.70	17.84
592	11.84	1.05	65.55	152.18	85.23	17.80
593	11.86	0.95	65.74	150.58	87.20	17.79
594	11.88	0.92	63.53	150.22	89.88	17.74
595	11.90	0.91	60.33	150.71	90.11	17.66
596	11.92	0.89	53.98	151.20	89.34	17.54
597	11.94	0.87	47.32	151.20	86.66	17.40
598	11.96	0.90	41.58	153.91	81.39	17.26
599	11.99	0.98	36.01	157.78	73.57	17.12
600	12.00	1.09	30.11	162.52	65.75	17.00
601	12.02	1.21	28.51	166.46	58.78	16.97
602	12.04	1.39	30.08	172.31	53.13	17.03
603	12.06	1.59	30.78	176.98	49.55	17.14
604	12.08	1.67	33.99	177.42	49.26	17.29
605	12.10	1.62	41.46	173.11	51.59	17.45
606	12.12	1.58	47.16	170.95	55.11	17.62
607	12.14	1.57	54.95	169.35	58.31	17.79
608	12.16	1.55	63.95	168.49	62.09	17.97
609	12.18	1.51	77.47	167.82	66.41	18.16
610	12.20	1.48	90.48	168.12	69.99	18.30
611	12.22	1.48	96.63	168.49	72.16	18.39
612	12.24	1.48	98.62	168.37	73.19	18.44
613	12.26	1.48	103.94	168.25	73.86	18.47
614	12.28	1.48	104.80	168.49	74.21	18.49
615	12.30	1.48	102.71	168.98	73.62	18.47
616	12.32	1.50	99.25	169.97	72.66	18.44
617	12.34	1.52	96.49	170.65	70.86	18.42
618	12.36	1.58	94.73	171.82	68.18	18.42
619	12.38	1.73	95.85	174.22	65.46	18.46
620	12.40	1.80	98.64	175.82	63.10	18.51
621	12.42	1.89	101.91	178.46	61.86	18.55
622	12.44	1.94	104.60	178.83	61.37	18.60
623	12.46	1.95	109.78	179.08	62.36	18.65
624	12.48	1.88	115.49	174.89	63.94	18.70

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
625	12.50	1.87	119.39	174.34	65.66	18.75
626	12.52	1.87	126.63	173.60	67.07	18.80
627	12.54	1.84	132.84	172.18	68.68	18.86
628	12.56	1.82	139.79	171.51	70.30	18.90
629	12.58	1.80	143.32	171.69	71.72	18.93
630	12.61	1.77	145.40	171.57	72.53	18.93
631	12.62	1.76	142.51	171.63	72.27	18.92
632	12.64	1.80	138.05	172.37	71.04	18.89
633	12.66	1.84	134.07	172.92	69.76	18.87
634	12.68	1.84	131.82	172.68	69.12	18.84
635	12.70	1.83	130.19	172.92	68.79	18.83
636	12.72	1.84	127.78	173.85	67.89	18.82
637	12.74	1.91	126.50	175.75	67.27	18.82
638	12.76	1.90	129.26	176.31	66.39	18.83
639	12.78	1.95	129.42	177.35	66.04	18.84
640	12.80	1.98	130.09	178.15	65.06	18.85
641	12.82	2.02	129.21	176.98	64.65	18.87
642	12.84	2.04	134.53	176.92	64.90	18.90
643	12.86	2.01	138.35	175.51	65.74	18.93
644	12.88	2.00	141.26	174.95	66.61	18.96
645	12.90	2.00	144.21	173.85	67.10	18.98
646	12.92	2.00	146.55	172.55	67.60	19.00
647	12.94	1.99	149.78	171.69	68.52	19.02
648	12.96	1.95	152.02	170.40	69.13	19.02
649	12.98	1.95	148.55	172.43	69.05	19.00
650	13.00	1.97	143.75	172.06	68.55	18.98
651	13.02	1.96	142.94	171.51	68.63	18.96
652	13.04	1.91	142.27	170.28	69.43	18.94
653	13.06	1.87	140.79	169.35	70.31	18.92
654	13.08	1.83	137.01	167.02	71.31	18.89
655	13.10	1.77	135.44	165.42	72.66	18.86
656	13.12	1.70	133.70	164.55	74.04	18.84
657	13.14	1.68	132.58	164.25	74.59	18.80
658	13.16	1.67	124.54	162.46	74.68	18.76
659	13.18	1.63	121.69	160.18	75.58	18.72
660	13.20	1.55	122.71	157.91	77.85	18.69
661	13.22	1.47	121.62	155.69	80.64	18.65
662	13.24	1.39	115.44	153.72	82.38	18.59
663	13.26	1.37	109.45	152.12	83.12	18.52
664	13.28	1.34	104.64	150.58	83.53	18.46
665	13.30	1.30	101.50	150.09	84.40	18.41
666	13.32	1.26	98.45	149.48	84.77	18.35
667	13.34	1.25	91.34	147.75	85.70	18.29
668	13.36	1.18	89.13	146.09	86.88	18.22
669	13.38	1.14	85.76	142.95	88.99	18.17
670	13.40	1.10	83.07	141.66	91.56	18.12
671	13.42	1.03	82.11	138.77	95.39	18.08
672	13.44	0.95	82.46	138.34	98.30	18.05

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
673	13.46	0.97	79.64	141.29	95.94	18.02
674	13.48	1.09	73.61	143.63	89.29	17.99
675	13.50	1.19	70.86	148.25	81.66	17.95
676	13.52	1.28	64.58	152.06	76.24	17.89
677	13.54	1.33	60.32	154.22	72.50	17.83
678	13.56	1.35	58.37	153.42	71.99	17.81
679	13.58	1.30	61.28	151.26	72.44	17.87
680	13.60	1.36	68.20	153.29	73.07	17.96
681	13.62	1.42	72.21	155.51	71.75	18.04
682	13.64	1.49	73.08	159.14	70.07	18.09
683	13.66	1.55	74.20	160.86	67.80	18.11
684	13.68	1.63	74.20	162.71	65.68	18.12
685	13.70	1.68	72.06	163.38	63.62	18.09
686	13.72	1.68	66.48	162.95	62.15	18.04
687	13.74	1.69	64.30	162.58	62.16	18.00
688	13.76	1.62	66.13	163.51	63.12	17.99
689	13.78	1.59	65.97	161.60	65.09	18.01
690	13.80	1.56	69.43	159.32	66.90	18.06
691	13.82	1.54	75.44	161.29	68.87	18.13
692	13.84	1.54	80.70	162.34	70.48	18.19
693	13.86	1.52	82.62	160.37	71.90	18.24
694	13.88	1.50	85.92	159.45	73.89	18.29
695	13.90	1.46	92.36	159.51	75.93	18.33
696	13.92	1.44	93.42	157.42	77.35	18.34
697	13.94	1.43	90.69	157.42	77.21	18.32
698	13.97	1.44	87.55	158.65	73.70	18.28
699	13.98	1.63	80.31	164.12	68.97	18.24
700	14.00	1.73	76.20	167.32	64.05	18.19
701	14.02	1.80	72.65	169.85	60.92	18.17
702	14.04	1.90	73.19	172.31	59.29	18.19
703	14.06	1.93	76.68	172.86	58.14	18.22
704	14.08	1.98	75.78	174.46	57.98	18.25
705	14.10	1.97	77.67	174.89	58.61	18.27
706	14.12	1.91	82.74	172.68	60.34	18.31
707	14.14	1.86	85.46	169.78	62.85	18.34
708	14.16	1.77	87.28	168.62	64.80	18.35
709	14.18	1.74	87.06	166.03	66.83	18.35
710	14.20	1.68	88.50	164.00	69.62	18.37
711	14.22	1.57	96.28	160.68	73.70	18.40
712	14.24	1.47	99.23	158.22	78.09	18.43
713	14.26	1.41	100.51	156.80	80.95	18.42
714	14.28	1.38	97.72	155.75	83.25	18.38
715	14.30	1.29	94.29	153.72	85.38	18.34
716	14.32	1.24	92.95	153.42	87.77	18.29
717	14.34	1.20	89.87	152.37	89.56	18.23
718	14.36	1.14	84.04	151.94	90.55	18.16
719	14.38	1.13	80.42	152.43	90.36	18.09
720	14.40	1.14	76.54	153.54	87.43	18.02

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
721	14.42	1.21	68.05	155.94	83.86	17.93
722	14.44	1.21	62.18	156.18	80.51	17.83
723	14.46	1.22	58.24	154.95	79.36	17.76
724	14.48	1.19	56.00	153.23	78.88	17.70
725	14.50	1.19	54.36	152.86	79.23	17.66
726	14.52	1.17	53.53	151.75	79.95	17.65
727	14.54	1.15	54.43	151.32	81.39	17.64
728	14.56	1.11	53.88	150.46	82.75	17.61
729	14.58	1.08	51.64	149.17	83.37	17.57
730	14.60	1.08	49.18	149.17	82.93	17.51
731	14.62	1.09	47.28	148.55	82.60	17.48
732	14.64	1.07	47.45	148.06	82.25	17.45
733	14.66	1.08	45.91	147.20	82.59	17.43
734	14.68	1.05	44.79	146.65	82.85	17.40
735	14.70	1.04	44.79	146.28	83.64	17.37
736	14.72	1.02	43.15	145.42	85.58	17.35
737	14.74	0.96	43.44	143.82	88.70	17.33
738	14.76	0.91	44.02	142.46	93.33	17.30
739	14.78	0.85	43.12	140.55	98.46	17.22
740	14.80	0.75	38.03	160.18	100.00	17.14
741	14.82	0.78	36.82	161.42	100.00	17.02
742	14.84	0.73	33.39	160.62	100.00	16.92
743	14.86	0.68	29.93	159.82	100.00	16.77
744	14.88	0.64	26.63	157.66	100.00	16.64
745	14.90	0.62	25.12	156.86	100.00	16.51
746	14.92	0.61	22.37	157.05	100.00	16.42
747	14.94	0.62	20.77	157.54	100.00	16.31
748	14.96	0.60	19.29	157.11	100.00	16.23
749	14.98	0.63	17.88	158.28	100.00	16.14
750	15.00	0.68	16.12	161.11	92.25	16.07
751	15.02	0.78	14.75	164.31	84.94	15.99
752	15.04	0.78	13.24	165.54	82.34	15.89
753	15.06	0.72	12.38	164.12	85.48	15.80
754	15.09	0.66	12.54	162.34	90.09	15.74
755	15.10	0.64	11.93	162.46	93.07	15.72
756	15.12	0.64	12.09	163.02	93.77	15.72
757	15.14	0.65	12.70	164.98	94.00	15.76
758	15.16	0.65	13.15	165.78	92.18	15.79
759	15.18	0.69	12.70	167.88	88.43	15.78
760	15.20	0.73	12.10	168.18	84.35	15.77
761	15.23	0.75	12.06	168.86	81.27	15.78
762	15.24	0.78	12.45	169.35	79.35	15.83
763	15.26	0.82	13.51	169.72	78.41	15.90
764	15.28	0.82	14.15	169.42	79.71	15.96
765	15.30	0.77	14.66	168.49	82.25	16.01
766	15.32	0.76	15.40	168.31	84.28	16.04
767	15.34	0.78	15.88	169.11	84.84	16.03
768	15.37	0.75	14.35	169.29	84.98	16.04

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
769	15.38	0.77	15.79	169.05	83.88	16.02
770	15.40	0.80	14.89	170.89	80.32	16.04
771	15.42	0.87	14.35	173.05	76.09	16.04
772	15.44	0.91	14.89	174.15	73.61	16.11
773	15.46	0.93	16.98	174.71	72.90	16.23
774	15.48	0.98	18.87	175.14	73.96	16.38
775	15.50	0.96	21.47	174.52	75.03	16.50
776	15.52	0.97	22.91	174.22	77.26	16.60
777	15.54	0.96	25.12	174.22	78.54	16.68
778	15.56	0.97	26.63	175.20	78.67	16.76
779	15.58	1.02	27.72	176.55	77.59	16.84
780	15.60	1.06	29.54	176.80	76.63	16.93
781	15.62	1.08	32.23	176.62	76.61	17.04
782	15.64	1.11	35.85	177.42	77.27	17.13
783	15.66	1.11	37.62	177.42	78.53	17.23
784	15.68	1.10	41.56	176.43	79.86	17.32
785	15.70	1.12	44.31	176.62	81.38	17.40
786	15.72	1.11	46.52	177.05	81.48	17.45
787	15.74	1.15	47.36	177.42	81.81	17.50
788	15.76	1.14	49.66	177.48	81.40	17.55
789	15.78	1.18	52.38	177.91	82.38	17.61
790	15.82	1.16	55.56	189.48	82.72	17.68
791	15.82	1.19	58.54	187.82	83.08	17.74
792	15.84	1.21	59.89	186.58	83.23	17.78
793	15.86	1.19	61.33	185.60	83.54	17.81
794	15.88	1.22	64.02	185.66	83.66	17.84
795	15.90	1.23	64.15	185.35	83.46	17.87
796	15.93	1.24	65.71	185.29	83.42	17.89
797	15.94	1.24	66.80	185.91	83.13	17.92
798	15.96	1.27	67.60	186.22	83.21	17.94
799	15.98	1.26	69.72	186.28	83.47	17.98
800	16.00	1.27	72.53	186.83	83.49	18.01
801	16.02	1.32	73.78	188.18	82.44	18.05
802	16.04	1.36	75.57	189.11	81.20	18.08
803	16.06	1.37	75.67	189.35	80.54	18.10
804	16.08	1.38	76.15	189.78	80.33	18.10
805	16.10	1.39	76.59	190.58	79.60	18.12
806	16.12	1.43	76.94	191.08	78.87	18.13
807	16.14	1.44	77.23	190.89	78.28	18.15
808	16.16	1.46	80.05	191.38	78.16	18.17
809	16.18	1.47	80.43	191.75	78.03	18.19
810	16.20	1.48	81.33	191.75	77.10	18.20
811	16.22	1.53	80.56	193.60	76.18	18.20
812	16.24	1.53	79.47	193.72	75.33	18.20
813	16.26	1.53	79.18	193.54	75.38	18.20
814	16.28	1.53	80.30	193.35	75.30	18.21
815	16.30	1.55	81.10	193.05	75.43	18.22
816	16.32	1.55	82.18	193.54	75.62	18.23

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
817	16.34	1.53	82.34	192.98	76.68	18.24
818	16.36	1.49	83.85	191.51	77.79	18.24
819	16.38	1.48	83.56	190.83	78.94	18.23
820	16.40	1.45	81.89	190.22	80.17	18.21
821	16.42	1.40	82.11	189.17	81.21	18.19
822	16.44	1.39	80.70	189.23	82.31	18.17
823	16.46	1.36	78.94	188.86	82.61	18.15
824	16.48	1.35	77.65	188.86	83.31	18.11
825	16.50	1.31	75.41	188.80	83.58	18.07
826	16.52	1.30	71.98	190.22	82.13	18.01
827	16.54	1.36	64.64	193.23	78.67	17.92
828	16.56	1.42	58.90	195.38	74.58	17.84
829	16.58	1.46	55.96	196.12	71.29	17.78
830	16.60	1.52	53.97	197.17	69.66	17.76
831	16.62	1.51	54.16	197.35	68.28	17.74
832	16.64	1.55	52.78	198.65	68.86	17.76
833	16.66	1.50	56.40	197.60	69.86	17.80
834	16.68	1.50	60.99	196.37	72.79	17.87
835	16.70	1.43	64.45	193.66	75.05	17.92
836	16.72	1.41	65.95	193.48	77.09	17.94
837	16.74	1.39	65.22	192.06	79.31	17.94
838	16.76	1.30	67.84	190.03	82.06	17.95
839	16.78	1.26	69.51	189.60	84.24	17.95
840	16.80	1.27	67.08	205.85	84.65	17.94
841	16.82	1.28	67.30	205.72	84.73	17.93
842	16.84	1.24	66.50	203.08	85.57	17.91
843	16.86	1.21	65.25	201.66	86.22	17.87
844	16.88	1.21	62.18	201.97	85.64	17.81
845	16.90	1.21	56.50	201.23	85.02	17.74
846	16.92	1.18	54.71	201.48	85.56	17.67
847	16.94	1.13	54.07	199.94	87.75	17.61
848	16.96	1.06	50.16	197.78	89.49	17.52
849	16.98	1.03	45.19	198.65	90.73	17.42
850	17.00	1.00	43.14	197.91	91.82	17.33
851	17.02	0.95	41.28	197.42	92.15	17.25
852	17.04	0.96	36.86	198.40	91.62	17.16
853	17.06	0.96	34.81	200.06	90.20	17.07
854	17.08	0.94	33.18	200.86	90.66	17.01
855	17.10	0.91	31.93	200.43	92.74	16.96
856	17.12	0.86	31.77	200.92	94.21	16.91
857	17.14	0.86	29.33	201.29	94.27	16.84
858	17.17	0.87	26.83	203.88	92.08	16.75
859	17.18	0.88	25.07	206.95	88.88	16.65
860	17.20	0.91	22.19	209.05	85.81	16.56
861	17.22	0.92	20.81	209.85	83.11	16.45
862	17.24	0.91	18.66	209.35	81.31	16.36
863	17.26	0.92	17.58	210.15	81.02	16.30
864	17.28	0.89	17.90	210.65	81.02	16.28

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
865	17.30	0.90	17.96	213.23	81.19	16.29
866	17.32	0.92	18.06	214.89	80.24	16.29
867	17.34	0.93	17.58	216.12	80.00	16.28
868	17.36	0.91	17.42	216.12	80.01	16.24
869	17.38	0.90	16.56	217.60	79.56	16.20
870	17.40	0.92	15.60	219.57	77.63	16.13
871	17.42	0.94	14.54	224.62	74.59	16.10
872	17.44	1.00	14.61	230.83	71.36	16.05
873	17.46	1.03	13.36	232.55	68.74	16.02
874	17.48	1.04	12.91	231.88	67.92	15.99
875	17.50	1.03	13.55	231.02	68.61	16.01
876	17.52	1.01	13.97	232.31	70.19	16.03
877	17.54	0.99	13.91	233.29	71.19	16.02
878	17.56	0.98	13.56	232.74	71.53	16.00
879	17.58	0.98	13.17	233.17	72.35	16.02
880	17.60	0.96	14.71	233.66	73.46	16.06
881	17.62	0.96	15.19	239.57	74.54	16.11
882	17.64	0.96	15.19	245.05	73.95	16.09
883	17.66	0.97	13.82	250.65	71.94	16.06
884	17.68	1.03	13.88	251.20	69.55	16.07
885	17.70	1.07	14.84	253.35	68.31	16.13
886	17.72	1.08	15.87	256.18	68.99	16.23
887	17.74	1.06	17.54	257.72	69.78	16.29
888	17.76	1.08	17.70	259.32	69.69	16.32
889	17.78	1.10	16.93	259.94	63.84	16.44
890	17.80	1.48	20.98	287.32	61.63	16.64
891	17.82	1.40	26.46	290.34	63.35	16.88
892	17.84	1.21	31.30	285.17	70.14	17.00
893	17.86	1.15	31.81	285.91	76.14	16.97
894	17.88	1.05	26.88	290.34	78.61	16.86
895	17.90	1.01	24.83	293.17	79.89	16.71
896	17.92	0.98	22.68	297.42	79.58	16.60
897	17.94	0.99	20.79	299.32	78.80	16.48
898	17.96	0.96	18.13	299.51	77.86	16.34
899	17.98	0.93	15.92	300.00	78.49	16.17
900	18.00	0.87	14.12	299.88	79.76	16.04
901	18.02	0.84	13.48	300.68	81.42	15.95
902	18.04	0.83	13.13	302.34	81.94	15.92
903	18.06	0.84	13.13	304.49	81.74	15.90
904	18.08	0.84	12.84	307.57	80.53	15.90
905	18.10	0.87	13.00	309.48	79.36	15.89
906	18.12	0.87	12.58	310.40	78.56	15.88
907	18.14	0.86	12.33	309.23	77.57	15.86
908	18.16	0.90	12.30	312.00	75.71	15.84
909	18.18	0.93	11.62	316.49	73.39	15.79
910	18.20	0.93	10.69	316.62	72.05	15.75
911	18.22	0.93	10.92	314.83	72.91	15.76
912	18.24	0.90	11.88	312.98	76.25	15.83

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
913	18.26	0.84	13.29	310.65	79.78	15.87
914	18.28	0.83	12.58	311.14	82.03	15.85
915	18.30	0.82	11.72	314.15	81.62	15.79
916	18.32	0.83	11.37	316.49	81.03	15.74
917	18.34	0.82	11.08	316.92	80.70	15.71
918	18.36	0.82	10.89	318.46	80.66	15.69
919	18.38	0.82	10.70	320.06	80.60	15.66
920	18.40	0.82	10.50	320.62	80.35	15.68
921	18.42	0.83	11.14	322.40	78.99	15.71
922	18.44	0.88	11.37	327.08	75.03	15.77
923	18.46	0.99	11.47	334.89	70.77	15.82
924	18.48	1.03	12.01	335.88	66.91	15.90
925	18.50	1.11	13.00	341.35	64.80	15.95
926	18.52	1.13	12.56	342.03	63.28	15.95
927	18.54	1.12	11.72	342.15	63.51	15.95
928	18.56	1.10	13.00	339.38	65.40	16.00
929	18.58	1.06	14.51	338.65	68.30	16.12
930	18.60	1.05	16.15	338.65	70.19	16.23
931	18.62	1.08	17.40	342.58	70.78	16.35
932	18.64	1.12	19.77	345.35	69.50	16.47
933	18.66	1.20	20.98	349.85	67.38	16.59
934	18.68	1.29	22.49	354.34	64.20	16.70
935	18.70	1.42	24.32	359.75	60.08	16.78
936	18.72	1.58	24.03	367.14	54.80	16.88
937	18.74	1.87	25.98	376.49	50.87	17.02
938	18.76	2.01	30.37	332.98	49.11	17.21
939	18.78	2.09	35.94	319.88	49.54	17.63
940	18.80	2.54	62.70	278.83	51.03	17.96
941	18.82	2.45	69.46	189.72	54.86	18.17
942	18.84	2.00	71.29	173.35	62.29	18.12
943	18.86	1.57	64.65	161.85	72.98	17.98
944	18.88	1.28	58.28	162.95	84.29	17.80
945	18.90	1.08	54.88	171.69	93.55	17.63
946	18.92	0.99	48.73	198.52	98.14	17.47
947	18.94	0.98	41.84	214.71	97.39	17.33
948	18.96	1.00	38.63	225.42	93.35	17.18
949	18.98	1.01	32.42	235.88	88.19	17.00
950	19.00	1.04	24.72	243.32	80.25	16.73
951	19.02	1.13	17.96	251.69	71.93	16.47
952	19.04	1.21	15.85	256.55	65.82	16.31
953	19.06	1.25	16.29	259.94	62.88	16.33
954	19.08	1.32	17.80	265.35	61.64	16.45
955	19.10	1.40	20.75	272.43	60.92	16.61
956	19.12	1.45	23.54	274.77	60.94	16.82
957	19.15	1.52	28.79	279.63	60.91	17.02
958	19.16	1.63	33.60	283.14	59.27	17.22
959	19.19	1.83	37.06	292.55	55.59	17.41
960	19.20	2.15	41.67	304.06	49.96	17.64

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
961	19.22	2.72	51.44	303.32	46.38	17.90
962	19.24	2.92	61.89	282.71	46.03	18.16
963	19.26	2.83	76.30	253.29	50.19	18.31
964	19.28	2.33	81.04	220.00	57.27	18.32
965	19.30	1.87	73.29	197.91	65.99	18.19
966	19.32	1.59	65.37	221.66	66.64	18.02
967	19.34	2.01	55.44	264.31	60.24	17.92
968	19.36	2.33	51.76	278.28	55.19	17.88
969	19.38	2.13	55.15	249.66	57.18	17.94
970	19.40	1.88	65.40	237.91	61.91	18.01
971	19.42	1.91	65.98	259.14	59.03	18.07
972	19.44	2.55	60.56	299.38	52.43	18.07
973	19.46	2.77	58.45	285.54	49.31	18.16
974	19.48	2.61	74.88	250.58	50.96	18.30
975	19.50	2.59	83.88	221.54	53.44	18.42
976	19.52	2.65	83.59	231.32	52.78	18.42
977	19.54	2.74	74.72	235.08	51.67	18.39
978	19.56	2.70	75.64	215.57	54.55	18.44
979	19.58	2.32	98.55	211.20	59.71	18.41
980	19.60	1.94	75.96	191.63	68.33	18.35
981	19.62	1.63	77.59	191.57	73.61	18.22
982	19.64	1.64	79.48	234.28	71.57	18.20
983	19.66	2.08	71.31	258.40	59.44	18.22
984	19.68	2.89	64.87	290.15	48.58	18.21
985	19.70	3.23	62.78	283.51	41.78	18.19
986	19.72	3.40	59.64	262.03	41.56	18.17
987	19.74	2.88	60.66	233.35	45.64	18.09
988	19.76	2.24	57.33	207.32	51.81	17.98
989	19.78	2.12	52.68	194.58	53.71	18.00
990	19.80	2.65	65.61	224.62	49.72	18.09
991	19.82	3.04	64.56	221.48	43.26	18.29
992	19.84	3.83	73.34	246.15	38.12	18.41
993	19.86	4.27	77.69	236.25	34.92	18.53
994	19.88	4.39	77.98	220.12	33.58	18.53
995	19.90	4.33	72.21	209.23	33.68	18.48
996	19.92	4.03	68.01	166.89	34.77	18.44
997	19.94	3.90	73.04	162.22	36.69	18.49
998	19.96	3.95	84.77	163.51	37.24	18.62
999	19.98	4.36	93.61	165.97	36.58	18.79
1000	20.00	4.73	104.89	164.80	35.01	18.96
1001	20.02	5.22	119.88	172.00	33.93	19.09
1002	20.04	5.42	125.23	174.46	33.42	19.19
1003	20.06	5.43	129.78	172.12	33.47	19.20
1004	20.08	5.30	124.91	168.18	33.81	19.18
1005	20.10	5.14	117.95	165.11	34.68	19.12
1006	20.12	4.83	118.01	159.32	36.15	19.08
1007	20.15	4.52	116.12	153.54	38.48	19.04
1008	20.16	4.18	114.42	146.40	41.88	18.99

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
1009	20.18	3.63	115.22	137.23	46.16	18.95
1010	20.20	3.26	115.22	132.06	52.02	18.92
1011	20.22	2.76	119.96	122.46	57.39	18.85
1012	20.25	2.48	109.38	133.48	57.08	18.69
1013	20.26	2.91	74.55	158.28	51.47	18.56
1014	20.28	3.38	80.99	167.75	44.73	18.54
1015	20.30	3.81	93.26	173.54	42.75	18.75
1016	20.32	4.06	115.17	175.14	42.96	19.00
1017	20.34	4.21	140.28	172.98	43.74	19.18
1018	20.36	4.34	148.96	171.51	43.72	19.27
1019	20.38	4.46	144.60	170.58	42.84	19.29
1020	20.40	4.52	141.07	166.71	42.00	19.28
1021	20.42	4.56	143.34	164.12	42.07	19.31
1022	20.44	4.57	154.33	162.09	42.17	19.35
1023	20.46	4.70	157.14	162.95	40.98	19.43
1024	20.48	5.32	167.46	176.18	38.40	19.52
1025	20.50	5.95	176.84	188.49	34.98	19.64
1026	20.52	6.81	187.89	206.15	31.02	19.71
1027	20.54	7.87	179.30	222.52	27.19	19.75
1028	20.56	8.71	173.12	229.78	24.42	19.77
1029	20.58	9.11	179.94	241.54	22.04	19.72
1030	20.60	9.58	147.00	246.95	19.89	19.61
1031	20.62	9.83	121.23	248.31	17.22	19.40
1032	20.64	10.07	99.86	242.46	15.25	19.19
1033	20.66	10.05	83.55	231.32	13.70	18.96
1034	20.68	9.86	67.24	227.57	12.22	18.69
1035	20.70	9.77	46.86	230.58	10.47	18.32
1036	20.72	9.76	30.13	236.25	5.00	17.92
1037	20.74	9.83	24.91	243.51	5.00	17.66
1038	20.76	10.02	26.19	254.83	5.00	17.61
1039	20.78	10.12	31.15	262.77	5.00	17.77

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (m)
q_c:	Measured cone resistance (MPa)
f_s:	Sleeve friction resistance (kPa)
u:	Pore pressure (kPa)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (kN/m^3)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1	0.02	0.32	0.00	0.32	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
2	0.04	0.64	0.00	0.64	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
3	0.06	0.98	0.00	0.98	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
4	0.08	1.31	0.00	1.31	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
5	0.10	1.65	0.00	1.65	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
6	0.12	2.00	0.00	2.00	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
7	0.14	2.35	0.00	2.35	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
8	0.16	2.70	0.00	2.70	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
9	0.18	3.06	0.00	3.06	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
10	0.20	3.42	0.00	3.42	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
11	0.22	3.78	0.00	3.78	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
12	0.24	4.14	0.00	4.14	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
13	0.26	4.50	0.00	4.50	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
14	0.28	4.87	0.00	4.87	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
15	0.30	5.23	0.00	5.23	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
16	0.32	5.59	0.00	5.59	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
17	0.34	5.94	0.00	5.94	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
18	0.36	6.30	0.00	6.30	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
19	0.38	6.65	0.00	6.65	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
20	0.40	7.01	0.00	7.01	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
21	0.42	7.36	0.00	7.36	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
22	0.44	7.71	0.00	7.71	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
23	0.46	8.06	0.00	8.06	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
24	0.48	8.41	0.00	8.41	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
25	0.50	8.77	0.00	8.77	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
26	0.52	9.12	0.00	9.12	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
27	0.54	9.48	0.00	9.48	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
28	0.56	9.84	0.00	9.84	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
29	0.58	10.20	0.00	10.20	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
30	0.60	10.56	0.00	10.56	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
31	0.62	10.91	0.00	10.91	1.00	0.149	1.43	0.105	1.10	1.00	2.000	No
32	0.64	11.27	0.00	11.27	1.00	0.149	1.43	0.105	1.10	1.00	2.000	No
33	0.66	11.63	0.00	11.63	1.00	0.149	1.43	0.105	1.10	1.00	2.000	No
34	0.68	11.98	0.00	11.98	1.00	0.149	1.43	0.105	1.10	1.00	2.000	No
35	0.70	12.34	0.00	12.34	1.00	0.149	1.43	0.105	1.10	1.00	2.000	No
36	0.72	12.69	0.00	12.69	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
37	0.74	13.05	0.00	13.05	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
38	0.76	13.40	0.00	13.40	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
39	0.78	13.75	0.00	13.75	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
40	0.80	14.09	0.00	14.09	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
41	0.82	14.44	0.00	14.44	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
42	0.84	14.78	0.00	14.78	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
43	0.86	15.13	0.00	15.13	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
44	0.88	15.48	0.00	15.48	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
45	0.90	15.82	0.00	15.82	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
46	0.92	16.17	0.00	16.17	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
47	0.94	16.52	0.00	16.52	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
48	0.96	16.87	0.00	16.87	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
49	0.98	17.23	0.00	17.23	0.99	0.149	1.43	0.104	1.10	1.00	2.000	No
50	1.00	17.58	0.00	17.58	0.99	0.149	1.43	0.104	1.10	1.00	2.000	No
51	1.02	17.94	0.20	17.74	0.99	0.150	1.43	0.105	1.10	1.00	0.126	No
52	1.04	18.30	0.39	17.91	0.99	0.152	1.43	0.106	1.10	1.00	0.128	No
53	1.06	18.66	0.59	18.07	0.99	0.153	1.43	0.107	1.10	1.00	0.129	No
54	1.08	19.02	0.78	18.24	0.99	0.155	1.43	0.108	1.10	1.00	0.130	No
55	1.10	19.38	0.98	18.40	0.99	0.156	1.43	0.109	1.10	1.00	0.131	No
56	1.12	19.74	1.18	18.56	0.99	0.158	1.43	0.110	1.10	1.00	0.133	No
57	1.14	20.09	1.37	18.72	0.99	0.159	1.43	0.111	1.10	1.00	0.133	No
58	1.16	20.45	1.57	18.88	0.99	0.161	1.43	0.112	1.10	1.00	0.134	No
59	1.18	20.80	1.77	19.04	0.99	0.162	1.43	0.113	1.10	1.00	0.135	No
60	1.20	21.16	1.96	19.20	0.99	0.163	1.43	0.114	1.10	1.00	0.136	No
61	1.22	21.51	2.16	19.35	0.99	0.165	1.43	0.115	1.10	1.00	0.137	No
62	1.24	21.87	2.35	19.51	0.99	0.166	1.43	0.116	1.10	1.00	0.138	No
63	1.26	22.22	2.55	19.67	0.99	0.167	1.43	0.117	1.10	1.00	0.138	No
64	1.28	22.58	2.75	19.84	0.99	0.169	1.43	0.118	1.10	1.00	0.139	No
65	1.30	22.94	2.94	20.00	0.99	0.170	1.43	0.119	1.10	1.00	0.140	No
66	1.32	23.31	3.14	20.17	0.99	0.171	1.43	0.120	1.10	1.00	0.141	No
67	1.34	23.67	3.34	20.34	0.99	0.172	1.43	0.121	1.10	1.00	0.142	No
68	1.36	24.04	3.53	20.51	0.99	0.173	1.43	0.121	1.10	1.00	0.143	No
69	1.39	24.60	3.83	20.77	0.99	0.175	1.43	0.123	1.10	1.00	0.144	No
70	1.40	24.79	3.92	20.86	0.99	0.176	1.43	0.123	1.10	1.00	0.145	No
71	1.42	25.16	4.12	21.04	0.99	0.177	1.43	0.124	1.10	1.00	0.146	No
72	1.44	25.54	4.32	21.22	0.99	0.178	1.43	0.124	1.10	1.00	0.147	No
73	1.46	25.91	4.51	21.40	0.99	0.179	1.43	0.125	1.10	1.00	0.148	No
74	1.48	26.29	4.71	21.58	0.99	0.180	1.43	0.126	1.10	1.00	0.149	No
75	1.50	26.66	4.91	21.76	0.99	0.181	1.43	0.127	1.10	1.00	0.150	No
76	1.52	27.04	5.10	21.94	0.99	0.182	1.43	0.127	1.10	1.00	0.151	No
77	1.54	27.41	5.30	22.11	0.99	0.183	1.43	0.128	1.10	1.00	0.151	No
78	1.56	27.79	5.49	22.29	0.99	0.184	1.43	0.129	1.10	1.00	0.152	No
79	1.58	28.16	5.69	22.47	0.99	0.185	1.43	0.129	1.10	1.00	0.152	No
80	1.60	28.53	5.89	22.65	0.99	0.186	1.43	0.130	1.10	1.00	0.152	No
81	1.62	28.91	6.08	22.83	0.99	0.186	1.43	0.131	1.10	1.00	0.152	No
82	1.65	29.47	6.38	23.09	0.98	0.188	1.43	0.131	1.10	1.00	0.153	No
83	1.66	29.66	6.47	23.18	0.98	0.188	1.43	0.132	1.10	1.00	0.154	No
84	1.68	30.03	6.67	23.36	0.98	0.189	1.43	0.132	1.10	1.00	0.154	No
85	1.70	30.41	6.87	23.54	0.98	0.190	1.43	0.133	1.10	1.00	0.154	No
86	1.72	30.79	7.06	23.72	0.98	0.191	1.43	0.134	1.10	1.00	0.155	No
87	1.74	31.17	7.26	23.91	0.98	0.192	1.43	0.134	1.10	1.00	0.155	No
88	1.76	31.55	7.46	24.09	0.98	0.192	1.43	0.135	1.10	1.00	0.156	No
89	1.78	31.93	7.65	24.27	0.98	0.193	1.43	0.135	1.10	1.00	0.156	No
90	1.80	32.31	7.85	24.46	0.98	0.194	1.43	0.136	1.10	1.00	0.157	No
91	1.82	32.69	8.04	24.64	0.98	0.195	1.43	0.136	1.10	1.00	0.158	No
92	1.84	33.07	8.24	24.83	0.98	0.195	1.43	0.137	1.10	1.00	0.158	No
93	1.86	33.45	8.44	25.01	0.98	0.196	1.43	0.137	1.10	1.00	0.159	No
94	1.88	33.83	8.63	25.20	0.98	0.197	1.43	0.138	1.10	1.00	0.160	No
95	1.90	34.21	8.83	25.38	0.98	0.198	1.43	0.138	1.10	1.00	0.160	No
96	1.92	34.59	9.03	25.56	0.98	0.198	1.43	0.139	1.10	1.00	0.161	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
97	1.95	35.16	9.32	25.84	0.98	0.199	1.43	0.139	1.10	1.00	0.162	No
98	1.96	35.35	9.42	25.93	0.98	0.200	1.43	0.140	1.10	1.00	0.162	No
99	1.98	35.73	9.61	26.11	0.98	0.200	1.43	0.140	1.10	1.00	0.162	No
100	2.00	36.11	9.81	26.30	0.98	0.201	1.43	0.141	1.10	1.00	0.163	No
101	2.03	36.67	10.10	26.57	0.98	0.202	1.43	0.141	1.10	1.00	0.163	No
102	2.04	36.86	10.20	26.66	0.98	0.202	1.43	0.142	1.10	1.00	0.163	No
103	2.06	37.24	10.40	26.84	0.98	0.203	1.43	0.142	1.10	1.00	0.163	No
104	2.08	37.61	10.59	27.02	0.98	0.203	1.43	0.142	1.10	1.00	0.163	No
105	2.10	37.99	10.79	27.19	0.98	0.204	1.43	0.143	1.10	1.00	0.164	No
106	2.12	38.36	10.99	27.37	0.98	0.205	1.43	0.143	1.10	1.00	0.164	No
107	2.14	38.74	11.18	27.55	0.98	0.205	1.43	0.144	1.10	1.00	0.165	No
108	2.16	39.11	11.38	27.73	0.98	0.206	1.43	0.144	1.10	1.00	0.166	No
109	2.18	39.49	11.58	27.91	0.98	0.206	1.43	0.144	1.10	1.00	0.167	No
110	2.20	39.87	11.77	28.09	0.98	0.207	1.43	0.145	1.10	1.00	0.168	No
111	2.22	40.24	11.97	28.27	0.98	0.208	1.43	0.145	1.10	1.00	0.169	No
112	2.24	40.62	12.16	28.45	0.97	0.208	1.43	0.146	1.10	1.00	0.170	No
113	2.26	40.99	12.36	28.63	0.97	0.209	1.43	0.146	1.10	1.00	0.171	No
114	2.28	41.36	12.56	28.80	0.97	0.209	1.43	0.146	1.10	1.00	0.172	No
115	2.30	41.73	12.75	28.98	0.97	0.210	1.43	0.147	1.10	1.00	0.173	No
116	2.32	42.10	12.95	29.15	0.97	0.210	1.43	0.147	1.10	1.00	0.174	No
117	2.34	42.46	13.15	29.32	0.97	0.211	1.43	0.148	1.10	1.00	0.175	No
118	2.36	42.82	13.34	29.48	0.97	0.211	1.43	0.148	1.10	1.00	0.176	No
119	2.38	43.18	13.54	29.65	0.97	0.212	1.43	0.148	1.10	1.00	0.177	No
120	2.40	43.54	13.73	29.81	0.97	0.212	1.43	0.149	1.10	1.00	0.177	No
121	2.42	43.90	13.93	29.97	0.97	0.213	1.43	0.149	1.10	1.00	0.178	No
122	2.44	44.25	14.13	30.13	0.97	0.213	1.43	0.149	1.10	1.00	0.179	No
123	2.46	44.61	14.32	30.28	0.97	0.214	1.43	0.150	1.10	1.00	0.179	No
124	2.48	44.96	14.52	30.44	0.97	0.214	1.43	0.150	1.10	1.00	0.179	No
125	2.50	45.30	14.72	30.59	0.97	0.215	1.43	0.150	1.10	1.00	0.180	No
126	2.52	45.65	14.91	30.74	0.97	0.215	1.43	0.151	1.10	1.00	0.181	No
127	2.54	46.00	15.11	30.89	0.97	0.216	1.43	0.151	1.10	1.00	0.181	No
128	2.56	46.34	15.30	31.04	0.97	0.216	1.43	0.151	1.10	1.00	0.182	No
129	2.58	46.69	15.50	31.19	0.97	0.217	1.43	0.152	1.10	1.00	0.183	No
130	2.60	47.03	15.70	31.33	0.97	0.217	1.43	0.152	1.10	1.00	0.183	No
131	2.62	47.36	15.89	31.47	0.97	0.218	1.43	0.152	1.10	1.00	0.184	No
132	2.64	47.70	16.09	31.61	0.97	0.218	1.43	0.153	1.10	1.00	0.185	No
133	2.66	48.04	16.28	31.75	0.97	0.219	1.43	0.153	1.10	1.00	0.185	No
134	2.68	48.37	16.48	31.89	0.97	0.219	1.43	0.154	1.09	1.00	0.186	No
135	2.70	48.71	16.68	32.03	0.97	0.220	1.43	0.154	1.09	1.00	0.187	No
136	2.72	49.04	16.87	32.17	0.97	0.220	1.43	0.154	1.09	1.00	0.187	No
137	2.74	49.37	17.07	32.30	0.97	0.221	1.43	0.155	1.09	1.00	0.188	No
138	2.76	49.70	17.27	32.43	0.97	0.221	1.43	0.155	1.09	1.00	0.189	No
139	2.78	50.02	17.46	32.56	0.97	0.222	1.43	0.155	1.09	1.00	0.189	No
140	2.80	50.35	17.66	32.69	0.97	0.222	1.43	0.156	1.09	1.00	0.189	No
141	2.82	50.67	17.85	32.81	0.96	0.223	1.43	0.156	1.09	1.00	0.189	No
142	2.84	50.99	18.05	32.94	0.96	0.223	1.43	0.156	1.09	1.00	0.190	No
143	2.86	51.31	18.25	33.07	0.96	0.224	1.43	0.157	1.09	1.00	0.190	No
144	2.88	51.63	18.44	33.19	0.96	0.224	1.43	0.157	1.09	1.00	0.191	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
145	2.90	51.96	18.64	33.32	0.96	0.225	1.43	0.157	1.09	1.00	0.192	No
146	2.92	52.28	18.84	33.45	0.96	0.225	1.43	0.158	1.09	1.00	0.192	No
147	2.94	52.61	19.03	33.57	0.96	0.225	1.43	0.158	1.09	1.00	0.192	No
148	2.96	52.93	19.23	33.70	0.96	0.226	1.43	0.158	1.09	1.00	0.193	No
149	2.98	53.25	19.42	33.83	0.96	0.226	1.43	0.158	1.09	1.00	0.194	No
150	3.00	53.58	19.62	33.96	0.96	0.227	1.43	0.159	1.09	1.00	0.194	No
151	3.02	53.89	19.82	34.08	0.96	0.227	1.43	0.159	1.09	1.00	0.195	No
152	3.04	54.21	20.01	34.20	0.96	0.228	1.43	0.159	1.09	1.00	0.195	No
153	3.06	54.53	20.21	34.32	0.96	0.228	1.43	0.160	1.09	1.00	0.195	No
154	3.08	54.84	20.40	34.43	0.96	0.229	1.43	0.160	1.09	1.00	0.195	No
155	3.10	55.16	20.60	34.55	0.96	0.229	1.43	0.160	1.09	1.00	0.196	No
156	3.12	55.47	20.80	34.68	0.96	0.229	1.43	0.161	1.09	1.00	0.196	No
157	3.14	55.80	20.99	34.80	0.96	0.230	1.43	0.161	1.09	1.00	0.197	No
158	3.16	56.12	21.19	34.93	0.96	0.230	1.43	0.161	1.09	1.00	0.198	No
159	3.18	56.44	21.39	35.06	0.96	0.231	1.43	0.161	1.08	1.00	0.198	No
160	3.21	56.93	21.68	35.25	0.96	0.231	1.43	0.162	1.08	1.00	0.199	No
161	3.22	57.09	21.78	35.32	0.96	0.231	1.43	0.162	1.08	1.00	0.199	No
162	3.24	57.42	21.97	35.45	0.96	0.232	1.43	0.162	1.08	1.00	0.199	No
163	3.26	57.74	22.17	35.57	0.96	0.232	1.43	0.163	1.08	1.00	0.199	No
164	3.28	58.07	22.37	35.70	0.96	0.233	1.43	0.163	1.09	1.00	0.199	No
165	3.30	58.39	22.56	35.82	0.96	0.233	1.43	0.163	1.08	1.00	0.200	No
166	3.32	58.70	22.76	35.94	0.96	0.233	1.43	0.163	1.08	1.00	0.200	No
167	3.34	59.02	22.96	36.07	0.96	0.234	1.43	0.164	1.08	1.00	0.201	No
168	3.36	59.35	23.15	36.19	0.95	0.234	1.43	0.164	1.08	1.00	0.201	No
169	3.38	59.67	23.35	36.32	0.95	0.234	1.43	0.164	1.08	1.00	0.201	No
170	3.40	59.99	23.54	36.45	0.95	0.235	1.43	0.164	1.08	1.00	0.201	No
171	3.42	60.31	23.74	36.57	0.95	0.235	1.43	0.165	1.08	1.00	0.202	No
172	3.44	60.64	23.94	36.70	0.95	0.235	1.43	0.165	1.08	1.00	0.202	No
173	3.46	60.96	24.13	36.83	0.95	0.236	1.43	0.165	1.08	1.00	0.203	No
174	3.48	61.28	24.33	36.95	0.95	0.236	1.43	0.165	1.08	1.00	0.204	No
175	3.50	61.61	24.53	37.08	0.95	0.237	1.43	0.166	1.08	1.00	0.204	No
176	3.52	61.93	24.72	37.21	0.95	0.237	1.43	0.166	1.08	1.00	0.203	No
177	3.54	62.25	24.92	37.33	0.95	0.237	1.43	0.166	1.08	1.00	0.203	No
178	3.56	62.57	25.11	37.46	0.95	0.238	1.43	0.166	1.08	1.00	0.203	No
179	3.58	62.90	25.31	37.59	0.95	0.238	1.43	0.166	1.08	1.00	0.204	No
180	3.60	63.22	25.51	37.72	0.95	0.238	1.43	0.167	1.08	1.00	0.204	No
181	3.63	63.71	25.80	37.91	0.95	0.239	1.43	0.167	1.08	1.00	0.205	No
182	3.64	63.87	25.90	37.98	0.95	0.239	1.43	0.167	1.08	1.00	0.205	No
183	3.66	64.20	26.09	38.11	0.95	0.239	1.43	0.167	1.08	1.00	0.206	No
184	3.68	64.54	26.29	38.25	0.95	0.239	1.43	0.168	1.08	1.00	0.206	No
185	3.70	64.87	26.49	38.38	0.95	0.240	1.43	0.168	1.08	1.00	0.207	No
186	3.72	65.20	26.68	38.52	0.95	0.240	1.43	0.168	1.08	1.00	0.207	No
187	3.74	65.53	26.88	38.65	0.95	0.240	1.43	0.168	1.08	1.00	0.207	No
188	3.76	65.86	27.08	38.79	0.95	0.240	1.43	0.168	1.08	1.00	0.208	No
189	3.78	66.19	27.27	38.92	0.95	0.241	1.43	0.169	1.08	1.00	0.208	No
190	3.80	66.51	27.47	39.04	0.95	0.241	1.43	0.169	1.08	1.00	0.209	No
191	3.82	66.83	27.66	39.17	0.95	0.241	1.43	0.169	1.08	1.00	0.209	No
192	3.84	67.15	27.86	39.29	0.95	0.242	1.43	0.169	1.08	1.00	0.210	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
193	3.86	67.47	28.06	39.41	0.95	0.242	1.43	0.169	1.08	1.00	0.210	No
194	3.88	67.79	28.25	39.53	0.94	0.242	1.43	0.170	1.08	1.00	0.209	No
195	3.90	68.10	28.45	39.65	0.94	0.243	1.43	0.170	1.08	1.00	0.209	No
196	3.92	68.42	28.65	39.78	0.94	0.243	1.43	0.170	1.08	1.00	0.210	No
197	3.94	68.74	28.84	39.90	0.94	0.243	1.43	0.170	1.08	1.00	0.210	No
198	3.96	69.06	29.04	40.02	0.94	0.243	1.43	0.170	1.08	1.00	0.211	No
199	3.98	69.38	29.23	40.15	0.94	0.244	1.43	0.171	1.07	1.00	0.211	No
200	4.00	69.71	29.43	40.28	0.94	0.244	1.43	0.171	1.07	1.00	0.211	No
201	4.03	70.20	29.72	40.47	0.94	0.244	1.43	0.171	1.07	1.00	0.212	No
202	4.04	70.36	29.82	40.54	0.94	0.244	1.43	0.171	1.07	1.00	0.212	No
203	4.06	70.68	30.02	40.67	0.94	0.245	1.43	0.171	1.07	1.00	0.212	No
204	4.08	71.01	30.21	40.79	0.94	0.245	1.43	0.171	1.08	1.00	0.211	No
205	4.10	71.33	30.41	40.92	0.94	0.245	1.43	0.172	1.08	1.00	0.212	No
206	4.12	71.66	30.61	41.05	0.94	0.245	1.43	0.172	1.08	1.00	0.212	No
207	4.14	71.98	30.80	41.18	0.94	0.246	1.43	0.172	1.08	1.00	0.211	No
208	4.16	72.31	31.00	41.31	0.94	0.246	1.43	0.172	1.08	1.00	0.212	No
209	4.18	72.64	31.20	41.44	0.94	0.246	1.43	0.172	1.08	1.00	0.212	No
210	4.20	72.97	31.39	41.58	0.94	0.246	1.43	0.172	1.07	1.00	0.212	No
211	4.22	73.31	31.59	41.72	0.94	0.246	1.43	0.173	1.07	1.00	0.212	No
212	4.24	73.64	31.78	41.86	0.94	0.247	1.43	0.173	1.07	1.00	0.212	No
213	4.26	73.99	31.98	42.01	0.94	0.247	1.43	0.173	1.07	1.00	0.212	No
214	4.28	74.33	32.18	42.15	0.94	0.247	1.43	0.173	1.07	1.00	0.212	No
215	4.30	74.68	32.37	42.30	0.94	0.247	1.43	0.173	1.07	1.00	0.212	No
216	4.32	75.02	32.57	42.45	0.94	0.247	1.43	0.173	1.07	1.00	0.212	No
217	4.34	75.37	32.77	42.60	0.94	0.247	1.43	0.173	1.07	1.00	0.213	No
218	4.36	75.71	32.96	42.75	0.94	0.248	1.43	0.173	1.07	1.00	0.213	No
219	4.38	76.06	33.16	42.90	0.93	0.248	1.43	0.173	1.07	1.00	0.213	No
220	4.40	76.40	33.35	43.05	0.93	0.248	1.43	0.174	1.07	1.00	0.213	No
221	4.42	76.75	33.55	43.20	0.93	0.248	1.43	0.174	1.07	1.00	0.214	No
222	4.44	77.09	33.75	43.35	0.93	0.248	1.43	0.174	1.07	1.00	0.214	No
223	4.46	77.44	33.94	43.50	0.93	0.248	1.43	0.174	1.07	1.00	0.214	No
224	4.48	77.79	34.14	43.65	0.93	0.249	1.43	0.174	1.07	1.00	0.214	No
225	4.50	78.14	34.34	43.80	0.93	0.249	1.43	0.174	1.07	1.00	0.215	No
226	4.52	78.48	34.53	43.95	0.93	0.249	1.43	0.174	1.07	1.00	0.215	No
227	4.54	78.83	34.73	44.11	0.93	0.249	1.43	0.174	1.07	1.00	0.215	No
228	4.56	79.18	34.92	44.26	0.93	0.249	1.43	0.174	1.07	1.00	0.215	No
229	4.58	79.53	35.12	44.41	0.93	0.249	1.43	0.174	1.07	1.00	0.216	No
230	4.60	79.88	35.32	44.57	0.93	0.249	1.43	0.175	1.07	1.00	0.216	No
231	4.62	80.23	35.51	44.72	0.93	0.249	1.43	0.175	1.07	1.00	0.216	No
232	4.64	80.58	35.71	44.87	0.93	0.250	1.43	0.175	1.07	1.00	0.217	No
233	4.66	80.93	35.90	45.03	0.93	0.250	1.43	0.175	1.07	1.00	0.217	No
234	4.68	81.28	36.10	45.18	0.93	0.250	1.43	0.175	1.07	1.00	0.217	No
235	4.70	81.62	36.30	45.33	0.93	0.250	1.43	0.175	1.07	1.00	0.218	No
236	4.72	81.97	36.49	45.48	0.93	0.250	1.43	0.175	1.07	1.00	0.218	No
237	4.74	82.32	36.69	45.63	0.93	0.250	1.43	0.175	1.07	1.00	0.218	No
238	4.76	82.66	36.89	45.78	0.93	0.250	1.43	0.175	1.06	1.00	0.219	No
239	4.78	83.01	37.08	45.93	0.93	0.250	1.43	0.175	1.06	1.00	0.219	No
240	4.80	83.35	37.28	46.07	0.93	0.251	1.43	0.175	1.06	1.00	0.219	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
241	4.82	83.69	37.47	46.22	0.93	0.251	1.43	0.175	1.06	1.00	0.219	No
242	4.84	84.03	37.67	46.36	0.93	0.251	1.43	0.176	1.06	1.00	0.219	No
243	4.86	84.36	37.87	46.50	0.93	0.251	1.43	0.176	1.06	1.00	0.219	No
244	4.88	84.70	38.06	46.64	0.92	0.251	1.43	0.176	1.06	1.00	0.219	No
245	4.90	85.03	38.26	46.77	0.92	0.251	1.43	0.176	1.06	1.00	0.219	No
246	4.92	85.37	38.46	46.91	0.92	0.251	1.43	0.176	1.06	1.00	0.219	No
247	4.94	85.70	38.65	47.05	0.92	0.251	1.43	0.176	1.06	1.00	0.219	No
248	4.96	86.03	38.85	47.19	0.92	0.252	1.43	0.176	1.06	1.00	0.218	No
249	4.98	86.37	39.04	47.33	0.92	0.252	1.43	0.176	1.07	1.00	0.218	No
250	5.00	86.71	39.24	47.47	0.92	0.252	1.43	0.176	1.07	1.00	0.218	No
251	5.02	87.05	39.44	47.61	0.92	0.252	1.43	0.176	1.06	1.00	0.218	No
252	5.04	87.39	39.63	47.76	0.92	0.252	1.43	0.176	1.06	1.00	0.219	No
253	5.06	87.74	39.83	47.91	0.92	0.252	1.43	0.176	1.06	1.00	0.219	No
254	5.08	88.08	40.02	48.06	0.92	0.252	1.43	0.177	1.06	1.00	0.219	No
255	5.11	88.60	40.32	48.28	0.92	0.252	1.43	0.177	1.06	1.00	0.219	No
256	5.12	88.77	40.42	48.35	0.92	0.252	1.43	0.177	1.06	1.00	0.219	No
257	5.14	89.11	40.61	48.50	0.92	0.253	1.43	0.177	1.06	1.00	0.219	No
258	5.16	89.46	40.81	48.65	0.92	0.253	1.43	0.177	1.06	1.00	0.219	No
259	5.18	89.80	41.01	48.79	0.92	0.253	1.43	0.177	1.06	1.00	0.219	No
260	5.20	90.14	41.20	48.94	0.92	0.253	1.43	0.177	1.06	1.00	0.219	No
261	5.22	90.49	41.40	49.09	0.92	0.253	1.43	0.177	1.06	1.00	0.218	No
262	5.24	90.83	41.59	49.24	0.92	0.253	1.43	0.177	1.06	1.00	0.218	No
263	5.26	91.18	41.79	49.39	0.92	0.253	1.43	0.177	1.06	1.00	0.219	No
264	5.28	91.52	41.99	49.54	0.92	0.253	1.43	0.177	1.06	1.00	0.220	No
265	5.30	91.87	42.18	49.69	0.92	0.253	1.43	0.177	1.06	1.00	0.221	No
266	5.32	92.21	42.38	49.83	0.92	0.253	1.43	0.177	1.06	1.00	2.000	Yes
267	5.34	92.56	42.58	49.98	0.92	0.253	1.43	0.177	1.06	1.00	2.000	Yes
268	5.36	92.91	42.77	50.13	0.91	0.253	1.43	0.177	1.06	1.00	2.000	Yes
269	5.38	93.25	42.97	50.28	0.91	0.253	1.43	0.177	1.07	1.00	2.000	Yes
270	5.40	93.60	43.16	50.44	0.91	0.254	1.43	0.177	1.07	1.00	2.000	Yes
271	5.42	93.95	43.36	50.59	0.91	0.254	1.43	0.177	1.07	1.00	2.000	Yes
272	5.44	94.30	43.56	50.75	0.91	0.254	1.43	0.178	1.07	1.00	2.000	Yes
273	5.46	94.66	43.75	50.90	0.91	0.254	1.43	0.178	1.07	1.00	2.000	Yes
274	5.48	95.01	43.95	51.06	0.91	0.254	1.43	0.178	1.07	1.00	2.000	Yes
275	5.50	95.37	44.15	51.23	0.91	0.254	1.43	0.178	1.07	1.00	2.000	Yes
276	5.52	95.73	44.34	51.39	0.91	0.254	1.43	0.178	1.07	1.00	2.000	Yes
277	5.54	96.09	44.54	51.55	0.91	0.254	1.43	0.178	1.07	1.00	2.000	Yes
278	5.56	96.44	44.73	51.71	0.91	0.254	1.43	0.178	1.07	1.00	2.000	Yes
279	5.58	96.79	44.93	51.86	0.91	0.254	1.43	0.178	1.07	1.00	0.206	No
280	5.60	97.15	45.13	52.02	0.91	0.254	1.43	0.178	1.07	1.00	0.204	No
281	5.62	97.50	45.32	52.18	0.91	0.254	1.43	0.178	1.07	1.00	0.207	No
282	5.64	97.85	45.52	52.33	0.91	0.254	1.43	0.178	1.06	1.00	2.000	Yes
283	5.66	98.19	45.71	52.47	0.91	0.254	1.43	0.178	1.06	1.00	2.000	Yes
284	5.68	98.53	45.91	52.62	0.91	0.254	1.43	0.178	1.06	1.00	2.000	Yes
285	5.70	98.88	46.11	52.78	0.91	0.254	1.43	0.178	1.06	1.00	2.000	Yes
286	5.72	99.24	46.30	52.94	0.91	0.254	1.43	0.178	1.06	1.00	2.000	Yes
287	5.74	99.60	46.50	53.10	0.91	0.254	1.43	0.178	1.06	1.00	2.000	Yes
288	5.76	99.97	46.70	53.27	0.91	0.254	1.43	0.178	1.06	1.00	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
289	5.78	100.33	46.89	53.44	0.91	0.254	1.43	0.178	1.06	1.00	0.221	No
290	5.80	100.70	47.09	53.61	0.91	0.254	1.43	0.178	1.05	1.00	0.222	No
291	5.82	101.07	47.28	53.78	0.90	0.254	1.43	0.178	1.06	1.00	2.000	Yes
292	5.84	101.43	47.48	53.95	0.90	0.254	1.43	0.178	1.06	1.00	2.000	Yes
293	5.86	101.80	47.68	54.12	0.90	0.254	1.43	0.178	1.07	1.00	2.000	Yes
294	5.88	102.16	47.87	54.29	0.90	0.254	1.43	0.178	1.07	1.00	2.000	Yes
295	5.90	102.52	48.07	54.45	0.90	0.254	1.43	0.178	1.07	1.00	2.000	Yes
296	5.92	102.88	48.27	54.61	0.90	0.254	1.43	0.178	1.06	1.00	2.000	Yes
297	5.94	103.23	48.46	54.77	0.90	0.254	1.43	0.178	1.06	1.00	2.000	Yes
298	5.96	103.59	48.66	54.93	0.90	0.254	1.43	0.178	1.06	1.00	2.000	Yes
299	5.98	103.95	48.85	55.10	0.90	0.254	1.43	0.178	1.06	1.00	2.000	Yes
300	6.00	104.31	49.05	55.26	0.90	0.254	1.43	0.178	1.05	1.00	2.000	Yes
301	6.02	104.67	49.25	55.43	0.90	0.254	1.43	0.178	1.05	1.00	0.223	No
302	6.05	105.22	49.54	55.68	0.90	0.254	1.43	0.178	1.05	1.00	0.224	No
303	6.06	105.40	49.64	55.76	0.90	0.254	1.43	0.178	1.05	1.00	0.223	No
304	6.08	105.76	49.83	55.93	0.90	0.254	1.43	0.178	1.05	1.00	0.221	No
305	6.10	106.12	50.03	56.09	0.90	0.254	1.43	0.178	1.05	1.00	0.222	No
306	6.12	106.47	50.23	56.24	0.90	0.254	1.43	0.178	1.05	1.00	0.222	No
307	6.14	106.82	50.42	56.40	0.90	0.254	1.43	0.178	1.05	1.00	0.223	No
308	6.16	107.17	50.62	56.55	0.90	0.254	1.43	0.178	1.05	1.00	0.224	No
309	6.18	107.52	50.82	56.70	0.90	0.254	1.43	0.178	1.05	1.00	0.223	No
310	6.20	107.87	51.01	56.86	0.90	0.254	1.43	0.178	1.05	1.00	0.223	No
311	6.22	108.22	51.21	57.01	0.90	0.254	1.43	0.178	1.05	1.00	0.223	No
312	6.24	108.58	51.40	57.17	0.90	0.254	1.43	0.178	1.05	1.00	0.223	No
313	6.26	108.93	51.60	57.33	0.89	0.254	1.43	0.178	1.05	1.00	0.223	No
314	6.28	109.29	51.80	57.49	0.89	0.254	1.43	0.178	1.05	1.00	0.223	No
315	6.30	109.65	51.99	57.66	0.89	0.254	1.43	0.178	1.05	1.00	0.223	No
316	6.32	110.01	52.19	57.82	0.89	0.254	1.43	0.178	1.05	1.00	0.223	No
317	6.34	110.37	52.39	57.99	0.89	0.254	1.43	0.178	1.05	1.00	0.224	No
318	6.36	110.74	52.58	58.16	0.89	0.254	1.43	0.178	1.05	1.00	0.224	No
319	6.38	111.10	52.78	58.33	0.89	0.254	1.43	0.178	1.05	1.00	0.224	No
320	6.40	111.47	52.97	58.49	0.89	0.254	1.43	0.178	1.05	1.00	0.224	No
321	6.42	111.83	53.17	58.66	0.89	0.254	1.43	0.178	1.05	1.00	0.224	No
322	6.44	112.20	53.37	58.83	0.89	0.254	1.43	0.178	1.05	1.00	0.224	No
323	6.46	112.56	53.56	59.00	0.89	0.254	1.43	0.178	1.05	1.00	0.224	No
324	6.48	112.93	53.76	59.17	0.89	0.254	1.43	0.178	1.05	1.00	0.224	No
325	6.50	113.29	53.96	59.34	0.89	0.254	1.43	0.178	1.05	1.00	0.224	No
326	6.52	113.65	54.15	59.50	0.89	0.254	1.43	0.178	1.05	1.00	0.224	No
327	6.54	114.02	54.35	59.67	0.89	0.254	1.43	0.178	1.05	1.00	0.224	No
328	6.56	114.38	54.54	59.84	0.89	0.254	1.43	0.178	1.05	1.00	0.224	No
329	6.58	114.74	54.74	60.00	0.89	0.254	1.43	0.178	1.05	1.00	0.224	No
330	6.60	115.10	54.94	60.17	0.89	0.254	1.43	0.178	1.05	1.00	0.223	No
331	6.62	115.46	55.13	60.33	0.89	0.254	1.43	0.178	1.05	1.00	0.223	No
332	6.64	115.83	55.33	60.50	0.89	0.254	1.43	0.178	1.04	1.00	0.223	No
333	6.66	116.19	55.52	60.67	0.89	0.254	1.43	0.178	1.04	1.00	0.223	No
334	6.68	116.55	55.72	60.83	0.89	0.254	1.43	0.178	1.04	1.00	0.223	No
335	6.70	116.92	55.92	61.00	0.89	0.254	1.43	0.178	1.04	1.00	0.224	No
336	6.72	117.28	56.11	61.17	0.88	0.254	1.43	0.178	1.04	1.00	0.224	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
337	6.74	117.65	56.31	61.34	0.88	0.254	1.43	0.177	1.04	1.00	0.224	No
338	6.76	118.02	56.51	61.51	0.88	0.254	1.43	0.177	1.04	1.00	0.224	No
339	6.78	118.38	56.70	61.68	0.88	0.253	1.43	0.177	1.04	1.00	0.224	No
340	6.80	118.75	56.90	61.85	0.88	0.253	1.43	0.177	1.04	1.00	0.224	No
341	6.82	119.11	57.09	62.02	0.88	0.253	1.43	0.177	1.04	1.00	0.225	No
342	6.84	119.47	57.29	62.18	0.88	0.253	1.43	0.177	1.04	1.00	0.225	No
343	6.86	119.82	57.49	62.34	0.88	0.253	1.43	0.177	1.04	1.00	0.228	No
344	6.88	120.18	57.68	62.50	0.88	0.253	1.43	0.177	1.04	1.00	0.226	No
345	6.90	120.54	57.88	62.66	0.88	0.253	1.43	0.177	1.04	1.00	0.226	No
346	6.92	120.90	58.08	62.82	0.88	0.253	1.43	0.177	1.04	1.00	0.226	No
347	6.94	121.25	58.27	62.98	0.88	0.253	1.43	0.177	1.04	1.00	0.226	No
348	6.96	121.61	58.47	63.14	0.88	0.253	1.43	0.177	1.04	1.00	0.226	No
349	6.98	121.97	58.66	63.30	0.88	0.253	1.43	0.177	1.04	1.00	0.226	No
350	7.00	122.32	58.86	63.46	0.88	0.253	1.43	0.177	1.04	1.00	0.227	No
351	7.02	122.67	59.06	63.62	0.88	0.253	1.43	0.177	1.04	1.00	0.227	No
352	7.04	123.03	59.25	63.78	0.88	0.253	1.43	0.177	1.04	1.00	0.227	No
353	7.06	123.38	59.45	63.93	0.88	0.253	1.43	0.177	1.04	1.00	0.227	No
354	7.08	123.73	59.64	64.09	0.88	0.253	1.43	0.177	1.04	1.00	0.227	No
355	7.10	124.08	59.84	64.24	0.88	0.253	1.43	0.177	1.04	1.00	0.227	No
356	7.12	124.43	60.04	64.40	0.88	0.253	1.43	0.177	1.04	1.00	0.227	No
357	7.14	124.78	60.23	64.55	0.88	0.253	1.43	0.177	1.04	1.00	0.227	No
358	7.16	125.14	60.43	64.71	0.87	0.253	1.43	0.177	1.04	1.00	0.227	No
359	7.19	125.67	60.72	64.94	0.87	0.253	1.43	0.177	1.04	1.00	0.226	No
360	7.20	125.84	60.82	65.02	0.87	0.253	1.43	0.177	1.04	1.00	0.226	No
361	7.22	126.20	61.02	65.18	0.87	0.253	1.43	0.177	1.04	1.00	0.226	No
362	7.24	126.55	61.21	65.34	0.87	0.253	1.43	0.177	1.04	1.00	0.226	No
363	7.26	126.91	61.41	65.49	0.87	0.253	1.43	0.177	1.04	1.00	0.226	No
364	7.28	127.26	61.61	65.65	0.87	0.253	1.43	0.177	1.04	1.00	0.226	No
365	7.31	127.79	61.90	65.89	0.87	0.253	1.43	0.177	1.04	1.00	0.226	No
366	7.32	127.97	62.00	65.97	0.87	0.253	1.43	0.177	1.04	1.00	0.226	No
367	7.34	128.33	62.20	66.13	0.87	0.253	1.43	0.177	1.04	1.00	0.226	No
368	7.36	128.68	62.39	66.29	0.87	0.253	1.43	0.177	1.04	1.00	0.226	No
369	7.38	129.04	62.59	66.45	0.87	0.252	1.43	0.177	1.04	1.00	0.225	No
370	7.41	129.58	62.88	66.69	0.87	0.252	1.43	0.177	1.04	1.00	0.225	No
371	7.42	129.75	62.98	66.77	0.87	0.252	1.43	0.177	1.04	1.00	0.224	No
372	7.44	130.11	63.18	66.94	0.87	0.252	1.43	0.177	1.04	1.00	0.224	No
373	7.46	130.47	63.37	67.10	0.87	0.252	1.43	0.177	1.04	1.00	0.224	No
374	7.48	130.83	63.57	67.26	0.87	0.252	1.43	0.177	1.04	1.00	0.224	No
375	7.50	131.19	63.77	67.43	0.87	0.252	1.43	0.176	1.04	1.00	0.225	No
376	7.52	131.55	63.96	67.59	0.87	0.252	1.43	0.176	1.03	1.00	0.225	No
377	7.54	131.91	64.16	67.76	0.87	0.252	1.43	0.176	1.03	1.00	0.225	No
378	7.56	132.27	64.35	67.92	0.87	0.252	1.43	0.176	1.03	1.00	0.226	No
379	7.58	132.63	64.55	68.08	0.87	0.252	1.43	0.176	1.03	1.00	0.226	No
380	7.60	132.99	64.75	68.25	0.86	0.252	1.43	0.176	1.03	1.00	0.226	No
381	7.62	133.35	64.94	68.41	0.86	0.252	1.43	0.176	1.03	1.00	0.226	No
382	7.64	133.71	65.14	68.57	0.86	0.252	1.43	0.176	1.03	1.00	0.226	No
383	7.66	134.07	65.33	68.74	0.86	0.252	1.43	0.176	1.03	1.00	0.226	No
384	7.68	134.43	65.53	68.90	0.86	0.252	1.43	0.176	1.03	1.00	0.226	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
385	7.70	134.79	65.73	69.06	0.86	0.252	1.43	0.176	1.03	1.00	0.226	No
386	7.72	135.14	65.92	69.22	0.86	0.252	1.43	0.176	1.03	1.00	0.226	No
387	7.74	135.50	66.12	69.38	0.86	0.251	1.43	0.176	1.03	1.00	0.226	No
388	7.76	135.86	66.32	69.55	0.86	0.251	1.43	0.176	1.03	1.00	0.226	No
389	7.78	136.22	66.51	69.71	0.86	0.251	1.43	0.176	1.03	1.00	0.226	No
390	7.80	136.58	66.71	69.87	0.86	0.251	1.43	0.176	1.03	1.00	0.226	No
391	7.82	136.94	66.90	70.04	0.86	0.251	1.43	0.176	1.03	1.00	0.225	No
392	7.84	137.30	67.10	70.20	0.86	0.251	1.43	0.176	1.03	1.00	0.225	No
393	7.86	137.66	67.30	70.36	0.86	0.251	1.43	0.176	1.03	1.00	0.225	No
394	7.88	138.02	67.49	70.53	0.86	0.251	1.43	0.176	1.03	1.00	0.225	No
395	7.90	138.38	67.69	70.69	0.86	0.251	1.43	0.176	1.03	1.00	0.225	No
396	7.92	138.75	67.89	70.86	0.86	0.251	1.43	0.176	1.03	1.00	0.225	No
397	7.94	139.11	68.08	71.03	0.86	0.251	1.43	0.176	1.03	1.00	0.224	No
398	7.96	139.47	68.28	71.20	0.86	0.251	1.43	0.176	1.03	1.00	0.224	No
399	7.98	139.84	68.47	71.37	0.86	0.251	1.43	0.175	1.03	1.00	0.224	No
400	8.01	140.39	68.77	71.62	0.86	0.251	1.43	0.175	1.03	1.00	0.224	No
401	8.02	140.57	68.87	71.71	0.85	0.251	1.43	0.175	1.03	1.00	0.224	No
402	8.04	140.94	69.06	71.88	0.85	0.250	1.43	0.175	1.03	1.00	0.225	No
403	8.06	141.30	69.26	72.04	0.85	0.250	1.43	0.175	1.03	1.00	0.224	No
404	8.08	141.67	69.45	72.21	0.85	0.250	1.43	0.175	1.03	1.00	0.224	No
405	8.10	142.03	69.65	72.38	0.85	0.250	1.43	0.175	1.03	1.00	0.224	No
406	8.12	142.40	69.85	72.55	0.85	0.250	1.43	0.175	1.03	1.00	0.225	No
407	8.15	142.94	70.14	72.80	0.85	0.250	1.43	0.175	1.03	1.00	0.225	No
408	8.17	143.31	70.34	72.97	0.85	0.250	1.43	0.175	1.03	1.00	0.225	No
409	8.18	143.49	70.44	73.05	0.85	0.250	1.43	0.175	1.03	1.00	0.225	No
410	8.20	143.85	70.63	73.22	0.85	0.250	1.43	0.175	1.03	1.00	0.224	No
411	8.22	144.21	70.83	73.39	0.85	0.250	1.43	0.175	1.03	1.00	0.224	No
412	8.24	144.58	71.02	73.55	0.85	0.250	1.43	0.175	1.03	1.00	0.224	No
413	8.26	144.94	71.22	73.72	0.85	0.250	1.43	0.175	1.03	1.00	0.224	No
414	8.28	145.30	71.42	73.89	0.85	0.250	1.43	0.175	1.03	1.00	0.224	No
415	8.30	145.67	71.61	74.06	0.85	0.249	1.43	0.175	1.03	1.00	0.224	No
416	8.32	146.03	71.81	74.22	0.85	0.249	1.43	0.175	1.03	1.00	0.224	No
417	8.34	146.40	72.01	74.39	0.85	0.249	1.43	0.174	1.03	1.00	0.224	No
418	8.36	146.76	72.20	74.56	0.85	0.249	1.43	0.174	1.03	1.00	0.224	No
419	8.38	147.13	72.40	74.73	0.85	0.249	1.43	0.174	1.03	1.00	0.224	No
420	8.40	147.49	72.59	74.90	0.85	0.249	1.43	0.174	1.03	1.00	0.224	No
421	8.42	147.86	72.79	75.07	0.85	0.249	1.43	0.174	1.03	1.00	0.224	No
422	8.44	148.22	72.99	75.23	0.84	0.249	1.43	0.174	1.03	1.00	0.224	No
423	8.46	148.59	73.18	75.40	0.84	0.249	1.43	0.174	1.03	1.00	0.224	No
424	8.48	148.95	73.38	75.57	0.84	0.249	1.43	0.174	1.03	1.00	0.224	No
425	8.50	149.31	73.58	75.74	0.84	0.249	1.43	0.174	1.02	1.00	0.224	No
426	8.52	149.68	73.77	75.91	0.84	0.249	1.43	0.174	1.02	1.00	0.224	No
427	8.54	150.04	73.97	76.07	0.84	0.248	1.43	0.174	1.02	1.00	0.224	No
428	8.56	150.40	74.16	76.24	0.84	0.248	1.43	0.174	1.02	1.00	0.224	No
429	8.58	150.77	74.36	76.41	0.84	0.248	1.43	0.174	1.02	1.00	0.224	No
430	8.60	151.13	74.56	76.57	0.84	0.248	1.43	0.174	1.02	1.00	0.224	No
431	8.62	151.49	74.75	76.74	0.84	0.248	1.43	0.174	1.02	1.00	0.224	No
432	8.64	151.85	74.95	76.90	0.84	0.248	1.43	0.174	1.02	1.00	0.224	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
433	8.66	152.21	75.14	77.07	0.84	0.248	1.43	0.174	1.02	1.00	0.225	No
434	8.68	152.57	75.34	77.23	0.84	0.248	1.43	0.173	1.02	1.00	0.225	No
435	8.70	152.93	75.54	77.40	0.84	0.248	1.43	0.173	1.02	1.00	0.225	No
436	8.72	153.29	75.73	77.56	0.84	0.248	1.43	0.173	1.02	1.00	0.225	No
437	8.74	153.65	75.93	77.73	0.84	0.248	1.43	0.173	1.02	1.00	0.225	No
438	8.76	154.02	76.13	77.89	0.84	0.248	1.43	0.173	1.02	1.00	0.224	No
439	8.78	154.38	76.32	78.06	0.84	0.247	1.43	0.173	1.02	1.00	0.224	No
440	8.80	154.74	76.52	78.22	0.84	0.247	1.43	0.173	1.02	1.00	0.224	No
441	8.82	155.10	76.71	78.39	0.84	0.247	1.43	0.173	1.02	1.00	0.224	No
442	8.84	155.46	76.91	78.55	0.84	0.247	1.43	0.173	1.02	1.00	0.223	No
443	8.86	155.83	77.11	78.72	0.83	0.247	1.43	0.173	1.02	1.00	0.223	No
444	8.88	156.19	77.30	78.89	0.83	0.247	1.43	0.173	1.02	1.00	0.223	No
445	8.90	156.56	77.50	79.06	0.83	0.247	1.43	0.173	1.02	1.00	0.223	No
446	8.92	156.92	77.70	79.23	0.83	0.247	1.43	0.173	1.02	1.00	0.223	No
447	8.94	157.29	77.89	79.39	0.83	0.247	1.43	0.173	1.02	1.00	0.223	No
448	8.96	157.65	78.09	79.56	0.83	0.247	1.43	0.173	1.02	1.00	0.223	No
449	8.98	158.02	78.28	79.73	0.83	0.247	1.43	0.173	1.02	1.00	0.223	No
450	9.00	158.38	78.48	79.90	0.83	0.246	1.43	0.173	1.02	1.00	0.223	No
451	9.02	158.75	78.68	80.07	0.83	0.246	1.43	0.172	1.02	1.00	0.223	No
452	9.04	159.11	78.87	80.24	0.83	0.246	1.43	0.172	1.02	1.00	0.223	No
453	9.06	159.47	79.07	80.40	0.83	0.246	1.43	0.172	1.02	1.00	0.224	No
454	9.08	159.83	79.26	80.57	0.83	0.246	1.43	0.172	1.02	1.00	0.224	No
455	9.10	160.19	79.46	80.73	0.83	0.246	1.43	0.172	1.02	1.00	0.224	No
456	9.12	160.55	79.66	80.89	0.83	0.246	1.43	0.172	1.02	1.00	0.224	No
457	9.14	160.90	79.85	81.05	0.83	0.246	1.43	0.172	1.02	1.00	0.224	No
458	9.16	161.26	80.05	81.21	0.83	0.246	1.43	0.172	1.02	1.00	0.224	No
459	9.18	161.61	80.25	81.36	0.83	0.246	1.43	0.172	1.02	1.00	0.224	No
460	9.20	161.96	80.44	81.52	0.83	0.246	1.43	0.172	1.02	1.00	0.224	No
461	9.22	162.32	80.64	81.68	0.83	0.246	1.43	0.172	1.02	1.00	0.223	No
462	9.24	162.68	80.83	81.84	0.83	0.245	1.43	0.172	1.02	1.00	0.223	No
463	9.26	163.03	81.03	82.00	0.83	0.245	1.43	0.172	1.02	1.00	0.223	No
464	9.29	163.57	81.32	82.25	0.82	0.245	1.43	0.172	1.02	1.00	0.223	No
465	9.30	163.75	81.42	82.33	0.82	0.245	1.43	0.172	1.02	1.00	0.222	No
466	9.32	164.11	81.62	82.49	0.82	0.245	1.43	0.172	1.02	1.00	0.222	No
467	9.34	164.47	81.82	82.65	0.82	0.245	1.43	0.171	1.02	1.00	0.222	No
468	9.36	164.83	82.01	82.81	0.82	0.245	1.43	0.171	1.02	1.00	0.221	No
469	9.38	165.19	82.21	82.98	0.82	0.245	1.43	0.171	1.02	1.00	0.221	No
470	9.40	165.55	82.40	83.15	0.82	0.245	1.43	0.171	1.02	1.00	0.221	No
471	9.42	165.92	82.60	83.32	0.82	0.245	1.43	0.171	1.02	1.00	0.221	No
472	9.44	166.29	82.80	83.49	0.82	0.245	1.43	0.171	1.02	1.00	0.220	No
473	9.46	166.66	82.99	83.67	0.82	0.244	1.43	0.171	1.02	1.00	0.220	No
474	9.48	167.04	83.19	83.85	0.82	0.244	1.43	0.171	1.02	1.00	0.220	No
475	9.50	167.41	83.39	84.03	0.82	0.244	1.43	0.171	1.02	1.00	0.221	No
476	9.52	167.79	83.58	84.21	0.82	0.244	1.43	0.171	1.02	1.00	0.221	No
477	9.54	168.17	83.78	84.39	0.82	0.244	1.43	0.171	1.02	1.00	0.221	No
478	9.56	168.54	83.97	84.57	0.82	0.244	1.43	0.171	1.02	1.00	0.221	No
479	9.58	168.92	84.17	84.75	0.82	0.244	1.43	0.171	1.02	1.00	0.221	No
480	9.60	169.30	84.37	84.93	0.82	0.244	1.43	0.170	1.02	1.00	0.221	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
481	9.62	169.68	84.56	85.11	0.82	0.243	1.43	0.170	1.02	1.00	0.221	No
482	9.64	170.05	84.76	85.29	0.82	0.243	1.43	0.170	1.02	1.00	0.221	No
483	9.66	170.43	84.95	85.47	0.82	0.243	1.43	0.170	1.01	1.00	0.220	No
484	9.68	170.80	85.15	85.65	0.82	0.243	1.43	0.170	1.01	1.00	0.220	No
485	9.70	171.18	85.35	85.83	0.81	0.243	1.43	0.170	1.01	1.00	0.220	No
486	9.72	171.55	85.54	86.01	0.81	0.243	1.43	0.170	1.01	1.00	0.220	No
487	9.74	171.92	85.74	86.18	0.81	0.243	1.43	0.170	1.01	1.00	0.219	No
488	9.76	172.29	85.94	86.36	0.81	0.243	1.43	0.170	1.01	1.00	0.219	No
489	9.78	172.67	86.13	86.54	0.81	0.243	1.43	0.170	1.01	1.00	0.219	No
490	9.80	173.04	86.33	86.71	0.81	0.242	1.43	0.170	1.01	1.00	0.219	No
491	9.82	173.41	86.52	86.89	0.81	0.242	1.43	0.170	1.01	1.00	0.219	No
492	9.84	173.79	86.72	87.07	0.81	0.242	1.43	0.170	1.01	1.00	0.218	No
493	9.86	174.16	86.92	87.24	0.81	0.242	1.43	0.169	1.01	1.00	0.218	No
494	9.88	174.53	87.11	87.42	0.81	0.242	1.43	0.169	1.01	1.00	0.218	No
495	9.90	174.91	87.31	87.60	0.81	0.242	1.43	0.169	1.01	1.00	0.218	No
496	9.92	175.28	87.51	87.78	0.81	0.242	1.43	0.169	1.01	1.00	0.219	No
497	9.94	175.66	87.70	87.96	0.81	0.242	1.43	0.169	1.01	1.00	0.219	No
498	9.96	176.03	87.90	88.14	0.81	0.241	1.43	0.169	1.01	1.00	0.219	No
499	9.98	176.41	88.09	88.31	0.81	0.241	1.43	0.169	1.01	1.00	0.219	No
500	10.00	176.78	88.29	88.49	0.81	0.241	1.43	0.169	1.01	1.00	0.220	No
501	10.03	177.34	88.58	88.75	0.81	0.241	1.43	0.169	1.01	1.00	0.221	No
502	10.04	177.52	88.68	88.84	0.81	0.241	1.43	0.169	1.01	1.00	0.221	No
503	10.06	177.89	88.88	89.01	0.81	0.241	1.43	0.169	1.01	1.00	0.221	No
504	10.08	178.25	89.07	89.18	0.81	0.241	1.43	0.169	1.01	1.00	0.221	No
505	10.10	178.62	89.27	89.34	0.81	0.241	1.43	0.168	1.01	1.00	0.222	No
506	10.12	178.98	89.47	89.51	0.80	0.241	1.43	0.168	1.01	1.00	0.222	No
507	10.14	179.33	89.66	89.67	0.80	0.241	1.43	0.168	1.01	1.00	0.222	No
508	10.16	179.69	89.86	89.83	0.80	0.240	1.43	0.168	1.01	1.00	0.222	No
509	10.18	180.04	90.06	89.98	0.80	0.240	1.43	0.168	1.01	1.00	0.222	No
510	10.20	180.39	90.25	90.13	0.80	0.240	1.43	0.168	1.01	1.00	0.222	No
511	10.22	180.73	90.45	90.28	0.80	0.240	1.43	0.168	1.01	1.00	0.222	No
512	10.24	181.07	90.64	90.43	0.80	0.240	1.43	0.168	1.01	1.00	0.222	No
513	10.26	181.41	90.84	90.57	0.80	0.240	1.43	0.168	1.01	1.00	0.222	No
514	10.28	181.74	91.04	90.71	0.80	0.240	1.43	0.168	1.01	1.00	0.222	No
515	10.30	182.08	91.23	90.84	0.80	0.240	1.43	0.168	1.01	1.00	0.221	No
516	10.32	182.41	91.43	90.98	0.80	0.240	1.43	0.168	1.01	1.00	0.221	No
517	10.34	182.73	91.63	91.11	0.80	0.240	1.43	0.168	1.01	1.00	0.221	No
518	10.36	183.07	91.82	91.24	0.80	0.240	1.43	0.168	1.01	1.00	0.221	No
519	10.38	183.40	92.02	91.38	0.80	0.240	1.43	0.168	1.01	1.00	0.221	No
520	10.40	183.73	92.21	91.52	0.80	0.240	1.43	0.168	1.01	1.00	0.221	No
521	10.42	184.06	92.41	91.65	0.80	0.240	1.43	0.168	1.01	1.00	0.220	No
522	10.44	184.40	92.61	91.79	0.80	0.239	1.43	0.168	1.01	1.00	0.221	No
523	10.46	184.73	92.80	91.93	0.80	0.239	1.43	0.168	1.01	1.00	0.220	No
524	10.48	185.07	93.00	92.07	0.80	0.239	1.43	0.168	1.01	1.00	0.220	No
525	10.50	185.41	93.19	92.21	0.80	0.239	1.43	0.167	1.01	1.00	0.219	No
526	10.52	185.75	93.39	92.36	0.80	0.239	1.43	0.167	1.01	1.00	0.218	No
527	10.54	186.09	93.59	92.50	0.79	0.239	1.43	0.167	1.01	1.00	0.218	No
528	10.56	186.44	93.78	92.65	0.79	0.239	1.43	0.167	1.01	1.00	0.218	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
529	10.58	186.79	93.98	92.81	0.79	0.239	1.43	0.167	1.01	1.00	0.218	No
530	10.60	187.14	94.18	92.96	0.79	0.239	1.43	0.167	1.01	1.00	0.217	No
531	10.62	187.50	94.37	93.13	0.79	0.239	1.43	0.167	1.01	1.00	0.217	No
532	10.64	187.87	94.57	93.30	0.79	0.239	1.43	0.167	1.01	1.00	0.217	No
533	10.66	188.24	94.76	93.47	0.79	0.238	1.43	0.167	1.01	1.00	0.217	No
534	10.68	188.61	94.96	93.65	0.79	0.238	1.43	0.167	1.01	1.00	0.217	No
535	10.70	188.98	95.16	93.82	0.79	0.238	1.43	0.167	1.01	1.00	0.217	No
536	10.72	189.35	95.35	94.00	0.79	0.238	1.43	0.167	1.01	1.00	0.217	No
537	10.74	189.73	95.55	94.18	0.79	0.238	1.43	0.167	1.01	1.00	0.218	No
538	10.76	190.10	95.75	94.35	0.79	0.238	1.43	0.166	1.01	1.00	0.218	No
539	10.78	190.47	95.94	94.53	0.79	0.238	1.43	0.166	1.01	1.00	0.219	No
540	10.80	190.84	96.14	94.71	0.79	0.238	1.43	0.166	1.01	1.00	0.219	No
541	10.82	191.21	96.33	94.88	0.79	0.237	1.43	0.166	1.01	1.00	0.219	No
542	10.84	191.58	96.53	95.05	0.79	0.237	1.43	0.166	1.01	1.00	0.219	No
543	10.86	191.94	96.73	95.22	0.79	0.237	1.43	0.166	1.01	1.00	0.219	No
544	10.88	192.30	96.92	95.38	0.79	0.237	1.43	0.166	1.00	1.00	0.219	No
545	10.90	192.66	97.12	95.54	0.79	0.237	1.43	0.166	1.00	1.00	0.219	No
546	10.92	193.01	97.32	95.69	0.79	0.237	1.43	0.166	1.00	1.00	0.220	No
547	10.94	193.36	97.51	95.85	0.79	0.237	1.43	0.166	1.00	1.00	0.220	No
548	10.96	193.71	97.71	96.00	0.78	0.237	1.43	0.166	1.00	1.00	0.219	No
549	10.98	194.05	97.90	96.15	0.78	0.237	1.43	0.166	1.00	1.00	0.219	No
550	11.00	194.39	98.10	96.29	0.78	0.237	1.43	0.166	1.00	1.00	0.219	No
551	11.03	194.90	98.39	96.51	0.78	0.236	1.43	0.166	1.00	1.00	0.219	No
552	11.04	195.07	98.49	96.58	0.78	0.236	1.43	0.165	1.00	1.00	0.219	No
553	11.06	195.41	98.69	96.72	0.78	0.236	1.43	0.165	1.00	1.00	0.219	No
554	11.08	195.74	98.88	96.85	0.78	0.236	1.43	0.165	1.00	1.00	0.219	No
555	11.10	196.07	99.08	96.99	0.78	0.236	1.43	0.165	1.00	1.00	0.219	No
556	11.12	196.41	99.28	97.13	0.78	0.236	1.43	0.165	1.00	1.00	0.219	No
557	11.14	196.74	99.47	97.27	0.78	0.236	1.43	0.165	1.00	1.00	0.218	No
558	11.16	197.08	99.67	97.41	0.78	0.236	1.43	0.165	1.00	1.00	0.218	No
559	11.18	197.42	99.87	97.55	0.78	0.236	1.43	0.165	1.00	1.00	0.218	No
560	11.20	197.76	100.06	97.70	0.78	0.236	1.43	0.165	1.00	1.00	0.218	No
561	11.22	198.10	100.26	97.84	0.78	0.236	1.43	0.165	1.00	1.00	0.218	No
562	11.24	198.44	100.45	97.99	0.78	0.236	1.43	0.165	1.00	1.00	0.218	No
563	11.26	198.79	100.65	98.14	0.78	0.236	1.43	0.165	1.00	1.00	0.218	No
564	11.28	199.13	100.85	98.28	0.78	0.235	1.43	0.165	1.00	1.00	0.217	No
565	11.30	199.47	101.04	98.43	0.78	0.235	1.43	0.165	1.00	1.00	0.217	No
566	11.32	199.82	101.24	98.58	0.78	0.235	1.43	0.165	1.00	1.00	0.216	No
567	11.34	200.16	101.44	98.73	0.78	0.235	1.43	0.165	1.00	1.00	0.216	No
568	11.36	200.51	101.63	98.88	0.78	0.235	1.43	0.165	1.00	1.00	0.216	No
569	11.38	200.86	101.83	99.03	0.77	0.235	1.43	0.164	1.00	1.00	0.216	No
570	11.40	201.22	102.02	99.19	0.77	0.235	1.43	0.164	1.00	1.00	0.216	No
571	11.42	201.58	102.22	99.36	0.77	0.235	1.43	0.164	1.00	1.00	0.216	No
572	11.44	201.94	102.42	99.52	0.77	0.235	1.43	0.164	1.00	1.00	0.216	No
573	11.46	202.30	102.61	99.69	0.77	0.234	1.43	0.164	1.00	1.00	0.216	No
574	11.48	202.66	102.81	99.85	0.77	0.234	1.43	0.164	1.00	1.00	0.216	No
575	11.50	203.03	103.01	100.02	0.77	0.234	1.43	0.164	1.00	1.00	0.216	No
576	11.52	203.39	103.20	100.19	0.77	0.234	1.43	0.164	1.00	1.00	0.216	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
577	11.54	203.76	103.40	100.36	0.77	0.234	1.43	0.164	1.00	1.00	0.216	No
578	11.56	204.13	103.59	100.53	0.77	0.234	1.43	0.164	1.00	1.00	0.216	No
579	11.58	204.49	103.79	100.70	0.77	0.234	1.43	0.164	1.00	1.00	0.216	No
580	11.60	204.86	103.99	100.87	0.77	0.234	1.43	0.164	1.00	1.00	0.216	No
581	11.62	205.22	104.18	101.04	0.77	0.234	1.43	0.163	1.00	1.00	0.216	No
582	11.64	205.59	104.38	101.21	0.77	0.233	1.43	0.163	1.00	1.00	0.216	No
583	11.66	205.95	104.57	101.38	0.77	0.233	1.43	0.163	1.00	1.00	0.216	No
584	11.68	206.31	104.77	101.54	0.77	0.233	1.43	0.163	1.00	1.00	0.216	No
585	11.70	206.68	104.97	101.71	0.77	0.233	1.43	0.163	1.00	1.00	0.216	No
586	11.72	207.04	105.16	101.88	0.77	0.233	1.43	0.163	1.00	1.00	0.216	No
587	11.74	207.40	105.36	102.04	0.77	0.233	1.43	0.163	1.00	1.00	0.216	No
588	11.76	207.76	105.56	102.21	0.77	0.233	1.43	0.163	1.00	1.00	0.216	No
589	11.78	208.12	105.75	102.37	0.77	0.233	1.43	0.163	1.00	1.00	0.216	No
590	11.80	208.48	105.95	102.53	0.76	0.232	1.43	0.163	1.00	1.00	0.216	No
591	11.82	208.83	106.14	102.69	0.76	0.232	1.43	0.163	1.00	1.00	0.216	No
592	11.84	209.19	106.34	102.85	0.76	0.232	1.43	0.163	1.00	1.00	0.216	No
593	11.86	209.55	106.54	103.01	0.76	0.232	1.43	0.163	1.00	1.00	0.216	No
594	11.88	209.90	106.73	103.17	0.76	0.232	1.43	0.162	1.00	1.00	0.216	No
595	11.90	210.25	106.93	103.33	0.76	0.232	1.43	0.162	1.00	1.00	0.216	No
596	11.92	210.61	107.13	103.48	0.76	0.232	1.43	0.162	1.00	1.00	0.216	No
597	11.94	210.95	107.32	103.63	0.76	0.232	1.43	0.162	1.00	1.00	0.216	No
598	11.96	211.30	107.52	103.78	0.76	0.232	1.43	0.162	1.00	1.00	0.216	No
599	11.99	211.81	107.81	104.00	0.76	0.231	1.43	0.162	1.00	1.00	0.216	No
600	12.00	211.98	107.91	104.07	0.76	0.231	1.43	0.162	1.00	1.00	0.216	No
601	12.02	212.32	108.11	104.22	0.76	0.231	1.43	0.162	1.00	1.00	0.215	No
602	12.04	212.66	108.30	104.36	0.76	0.231	1.43	0.162	1.00	1.00	0.215	No
603	12.06	213.00	108.50	104.51	0.76	0.231	1.43	0.162	1.00	1.00	0.214	No
604	12.08	213.35	108.69	104.66	0.76	0.231	1.43	0.162	1.00	1.00	0.214	No
605	12.10	213.70	108.89	104.81	0.76	0.231	1.43	0.162	1.00	1.00	0.214	No
606	12.12	214.05	109.09	104.96	0.76	0.231	1.43	0.162	1.00	1.00	0.214	No
607	12.14	214.41	109.28	105.12	0.76	0.231	1.43	0.162	1.00	1.00	0.214	No
608	12.16	214.77	109.48	105.29	0.76	0.231	1.43	0.161	1.00	1.00	0.214	No
609	12.18	215.13	109.68	105.45	0.76	0.231	1.43	0.161	1.00	1.00	0.214	No
610	12.20	215.50	109.87	105.62	0.76	0.230	1.43	0.161	1.00	1.00	0.214	No
611	12.22	215.86	110.07	105.80	0.75	0.230	1.43	0.161	1.00	1.00	0.213	No
612	12.24	216.23	110.26	105.97	0.75	0.230	1.43	0.161	1.00	1.00	0.213	No
613	12.26	216.60	110.46	106.14	0.75	0.230	1.43	0.161	1.00	1.00	0.213	No
614	12.28	216.97	110.66	106.32	0.75	0.230	1.43	0.161	1.00	1.00	0.213	No
615	12.30	217.34	110.85	106.49	0.75	0.230	1.43	0.161	1.00	1.00	0.213	No
616	12.32	217.71	111.05	106.66	0.75	0.230	1.43	0.161	1.00	1.00	0.213	No
617	12.34	218.08	111.25	106.83	0.75	0.229	1.43	0.161	1.00	1.00	0.213	No
618	12.36	218.45	111.44	107.01	0.75	0.229	1.43	0.161	1.00	1.00	0.213	No
619	12.38	218.82	111.64	107.18	0.75	0.229	1.43	0.160	1.00	1.00	0.212	No
620	12.40	219.19	111.83	107.35	0.75	0.229	1.43	0.160	0.99	1.00	0.212	No
621	12.42	219.56	112.03	107.53	0.75	0.229	1.43	0.160	0.99	1.00	0.211	No
622	12.44	219.93	112.23	107.70	0.75	0.229	1.43	0.160	0.99	1.00	0.211	No
623	12.46	220.30	112.42	107.88	0.75	0.229	1.43	0.160	0.99	1.00	0.211	No
624	12.48	220.68	112.62	108.06	0.75	0.229	1.43	0.160	0.99	1.00	0.211	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
625	12.50	221.05	112.82	108.24	0.75	0.228	1.43	0.160	0.99	1.00	0.211	No
626	12.52	221.43	113.01	108.42	0.75	0.228	1.43	0.160	0.99	1.00	0.211	No
627	12.54	221.80	113.21	108.60	0.75	0.228	1.43	0.160	0.99	1.00	0.211	No
628	12.56	222.18	113.40	108.78	0.75	0.228	1.43	0.160	0.99	1.00	0.211	No
629	12.58	222.56	113.60	108.96	0.75	0.228	1.43	0.160	0.99	1.00	0.211	No
630	12.61	223.13	113.89	109.24	0.75	0.228	1.43	0.159	0.99	1.00	0.211	No
631	12.62	223.32	113.99	109.33	0.75	0.228	1.43	0.159	0.99	1.00	0.211	No
632	12.64	223.70	114.19	109.51	0.74	0.228	1.43	0.159	0.99	1.00	0.211	No
633	12.66	224.07	114.38	109.69	0.74	0.227	1.43	0.159	0.99	1.00	0.210	No
634	12.68	224.45	114.58	109.87	0.74	0.227	1.43	0.159	0.99	1.00	0.210	No
635	12.70	224.83	114.78	110.05	0.74	0.227	1.43	0.159	0.99	1.00	0.210	No
636	12.72	225.20	114.97	110.23	0.74	0.227	1.43	0.159	0.99	1.00	0.210	No
637	12.74	225.58	115.17	110.41	0.74	0.227	1.43	0.159	0.99	1.00	0.210	No
638	12.76	225.96	115.37	110.59	0.74	0.227	1.43	0.159	0.99	1.00	0.210	No
639	12.78	226.33	115.56	110.77	0.74	0.227	1.43	0.159	0.99	1.00	0.209	No
640	12.80	226.71	115.76	110.95	0.74	0.226	1.43	0.158	0.99	1.00	0.209	No
641	12.82	227.09	115.95	111.13	0.74	0.226	1.43	0.158	0.99	1.00	0.209	No
642	12.84	227.47	116.15	111.32	0.74	0.226	1.43	0.158	0.99	1.00	0.209	No
643	12.86	227.84	116.35	111.50	0.74	0.226	1.43	0.158	0.99	1.00	0.209	No
644	12.88	228.22	116.54	111.68	0.74	0.226	1.43	0.158	0.99	1.00	0.209	No
645	12.90	228.60	116.74	111.86	0.74	0.226	1.43	0.158	0.99	1.00	0.209	No
646	12.92	228.98	116.94	112.05	0.74	0.226	1.43	0.158	0.99	1.00	0.209	No
647	12.94	229.36	117.13	112.23	0.74	0.225	1.43	0.158	0.99	1.00	0.209	No
648	12.96	229.74	117.33	112.42	0.74	0.225	1.43	0.158	0.99	1.00	0.209	No
649	12.98	230.12	117.52	112.60	0.74	0.225	1.43	0.158	0.99	1.00	0.209	No
650	13.00	230.50	117.72	112.78	0.74	0.225	1.43	0.158	0.99	1.00	0.208	No
651	13.02	230.88	117.92	112.97	0.74	0.225	1.43	0.157	0.99	1.00	0.208	No
652	13.04	231.26	118.11	113.15	0.74	0.225	1.43	0.157	0.99	1.00	0.208	No
653	13.06	231.64	118.31	113.33	0.74	0.225	1.43	0.157	0.99	1.00	0.208	No
654	13.08	232.02	118.50	113.51	0.73	0.224	1.43	0.157	0.99	1.00	0.208	No
655	13.10	232.39	118.70	113.69	0.73	0.224	1.43	0.157	0.99	1.00	0.209	No
656	13.12	232.77	118.90	113.87	0.73	0.224	1.43	0.157	0.99	1.00	0.209	No
657	13.14	233.15	119.09	114.05	0.73	0.224	1.43	0.157	0.99	1.00	0.209	No
658	13.16	233.52	119.29	114.23	0.73	0.224	1.43	0.157	0.99	1.00	0.209	No
659	13.18	233.90	119.49	114.41	0.73	0.224	1.43	0.157	0.99	1.00	0.209	No
660	13.20	234.27	119.68	114.59	0.73	0.224	1.43	0.157	0.99	1.00	0.209	No
661	13.22	234.64	119.88	114.77	0.73	0.224	1.43	0.156	0.99	1.00	0.209	No
662	13.24	235.02	120.07	114.94	0.73	0.223	1.43	0.156	0.99	1.00	0.209	No
663	13.26	235.39	120.27	115.12	0.73	0.223	1.43	0.156	0.99	1.00	0.209	No
664	13.28	235.75	120.47	115.29	0.73	0.223	1.43	0.156	0.99	1.00	0.209	No
665	13.30	236.12	120.66	115.46	0.73	0.223	1.43	0.156	0.99	1.00	0.209	No
666	13.32	236.49	120.86	115.63	0.73	0.223	1.43	0.156	0.99	1.00	0.209	No
667	13.34	236.86	121.06	115.80	0.73	0.223	1.43	0.156	0.99	1.00	0.209	No
668	13.36	237.22	121.25	115.97	0.73	0.223	1.43	0.156	0.99	1.00	0.209	No
669	13.38	237.58	121.45	116.14	0.73	0.223	1.43	0.156	0.99	1.00	0.209	No
670	13.40	237.95	121.64	116.30	0.73	0.222	1.43	0.156	0.99	1.00	0.209	No
671	13.42	238.31	121.84	116.47	0.73	0.222	1.43	0.156	0.99	1.00	0.209	No
672	13.44	238.67	122.04	116.63	0.73	0.222	1.43	0.156	0.99	1.00	0.209	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
673	13.46	239.03	122.23	116.80	0.73	0.222	1.43	0.155	0.99	1.00	0.209	No
674	13.48	239.39	122.43	116.96	0.73	0.222	1.43	0.155	0.99	1.00	0.209	No
675	13.50	239.75	122.63	117.12	0.72	0.222	1.43	0.155	0.99	1.00	0.209	No
676	13.52	240.11	122.82	117.28	0.72	0.222	1.43	0.155	0.99	1.00	0.208	No
677	13.54	240.46	123.02	117.45	0.72	0.222	1.43	0.155	0.99	1.00	0.208	No
678	13.56	240.82	123.21	117.61	0.72	0.221	1.43	0.155	0.99	1.00	0.208	No
679	13.58	241.18	123.41	117.77	0.72	0.221	1.43	0.155	0.99	1.00	0.208	No
680	13.60	241.54	123.61	117.93	0.72	0.221	1.43	0.155	0.99	1.00	0.208	No
681	13.62	241.90	123.80	118.09	0.72	0.221	1.43	0.155	0.99	1.00	0.207	No
682	13.64	242.26	124.00	118.26	0.72	0.221	1.43	0.155	0.99	1.00	0.207	No
683	13.66	242.62	124.19	118.43	0.72	0.221	1.43	0.155	0.99	1.00	0.207	No
684	13.68	242.98	124.39	118.59	0.72	0.221	1.43	0.155	0.99	1.00	0.207	No
685	13.70	243.34	124.59	118.76	0.72	0.221	1.43	0.154	0.99	1.00	0.206	No
686	13.72	243.71	124.78	118.92	0.72	0.221	1.43	0.154	0.99	1.00	0.206	No
687	13.74	244.07	124.98	119.09	0.72	0.220	1.43	0.154	0.99	1.00	0.206	No
688	13.76	244.43	125.18	119.25	0.72	0.220	1.43	0.154	0.99	1.00	0.206	No
689	13.78	244.79	125.37	119.41	0.72	0.220	1.43	0.154	0.99	1.00	0.206	No
690	13.80	245.15	125.57	119.58	0.72	0.220	1.43	0.154	0.99	1.00	0.206	No
691	13.82	245.51	125.76	119.75	0.72	0.220	1.43	0.154	0.99	1.00	0.206	No
692	13.84	245.87	125.96	119.91	0.72	0.220	1.43	0.154	0.99	1.00	0.206	No
693	13.86	246.24	126.16	120.08	0.72	0.220	1.43	0.154	0.99	1.00	0.206	No
694	13.88	246.60	126.35	120.25	0.72	0.220	1.43	0.154	0.99	1.00	0.206	No
695	13.90	246.97	126.55	120.42	0.72	0.219	1.43	0.154	0.99	1.00	0.206	No
696	13.92	247.34	126.75	120.59	0.72	0.219	1.43	0.154	0.99	1.00	0.206	No
697	13.94	247.70	126.94	120.76	0.71	0.219	1.43	0.153	0.99	1.00	0.206	No
698	13.97	248.25	127.24	121.02	0.71	0.219	1.43	0.153	0.99	1.00	0.206	No
699	13.98	248.43	127.33	121.10	0.71	0.219	1.43	0.153	0.98	1.00	0.205	No
700	14.00	248.80	127.53	121.27	0.71	0.219	1.43	0.153	0.98	1.00	0.205	No
701	14.02	249.16	127.73	121.44	0.71	0.219	1.43	0.153	0.98	1.00	0.205	No
702	14.04	249.53	127.92	121.60	0.71	0.219	1.43	0.153	0.98	1.00	0.204	No
703	14.06	249.89	128.12	121.77	0.71	0.218	1.43	0.153	0.98	1.00	0.204	No
704	14.08	250.25	128.31	121.94	0.71	0.218	1.43	0.153	0.98	1.00	0.204	No
705	14.10	250.62	128.51	122.11	0.71	0.218	1.43	0.153	0.98	1.00	0.204	No
706	14.12	250.99	128.71	122.28	0.71	0.218	1.43	0.153	0.98	1.00	0.204	No
707	14.14	251.35	128.90	122.45	0.71	0.218	1.43	0.153	0.98	1.00	0.204	No
708	14.16	251.72	129.10	122.62	0.71	0.218	1.43	0.152	0.98	1.00	0.204	No
709	14.18	252.09	129.30	122.79	0.71	0.218	1.43	0.152	0.98	1.00	0.204	No
710	14.20	252.45	129.49	122.96	0.71	0.218	1.43	0.152	0.98	1.00	0.204	No
711	14.22	252.82	129.69	123.13	0.71	0.217	1.43	0.152	0.98	1.00	0.204	No
712	14.24	253.19	129.88	123.31	0.71	0.217	1.43	0.152	0.98	1.00	0.205	No
713	14.26	253.56	130.08	123.48	0.71	0.217	1.43	0.152	0.98	1.00	0.205	No
714	14.28	253.93	130.28	123.65	0.71	0.217	1.43	0.152	0.98	1.00	0.205	No
715	14.30	254.29	130.47	123.82	0.71	0.217	1.43	0.152	0.98	1.00	0.205	No
716	14.32	254.66	130.67	123.99	0.71	0.217	1.43	0.152	0.98	1.00	0.205	No
717	14.34	255.02	130.87	124.16	0.71	0.217	1.43	0.152	0.98	1.00	0.205	No
718	14.36	255.39	131.06	124.33	0.71	0.217	1.43	0.152	0.98	1.00	0.205	No
719	14.38	255.75	131.26	124.49	0.70	0.216	1.43	0.152	0.98	1.00	0.205	No
720	14.40	256.11	131.45	124.66	0.70	0.216	1.43	0.151	0.98	1.00	0.205	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
721	14.42	256.47	131.65	124.82	0.70	0.216	1.43	0.151	0.98	1.00	0.204	No
722	14.44	256.83	131.85	124.98	0.70	0.216	1.43	0.151	0.98	1.00	0.204	No
723	14.46	257.18	132.04	125.14	0.70	0.216	1.43	0.151	0.98	1.00	0.204	No
724	14.48	257.53	132.24	125.30	0.70	0.216	1.43	0.151	0.98	1.00	0.204	No
725	14.50	257.89	132.44	125.45	0.70	0.216	1.43	0.151	0.98	1.00	0.204	No
726	14.52	258.24	132.63	125.61	0.70	0.216	1.43	0.151	0.98	1.00	0.204	No
727	14.54	258.59	132.83	125.77	0.70	0.216	1.43	0.151	0.98	1.00	0.204	No
728	14.56	258.95	133.02	125.92	0.70	0.215	1.43	0.151	0.98	1.00	0.204	No
729	14.58	259.30	133.22	126.08	0.70	0.215	1.43	0.151	0.98	1.00	0.204	No
730	14.60	259.65	133.42	126.23	0.70	0.215	1.43	0.151	0.98	1.00	0.204	No
731	14.62	260.00	133.61	126.38	0.70	0.215	1.43	0.151	0.98	1.00	0.204	No
732	14.64	260.35	133.81	126.54	0.70	0.215	1.43	0.150	0.98	1.00	0.204	No
733	14.66	260.69	134.00	126.69	0.70	0.215	1.43	0.150	0.98	1.00	0.204	No
734	14.68	261.04	134.20	126.84	0.70	0.215	1.43	0.150	0.98	1.00	0.204	No
735	14.70	261.39	134.40	126.99	0.70	0.215	1.43	0.150	0.98	1.00	0.204	No
736	14.72	261.74	134.59	127.14	0.70	0.215	1.43	0.150	0.98	1.00	0.204	No
737	14.74	262.08	134.79	127.29	0.70	0.214	1.43	0.150	0.98	1.00	0.204	No
738	14.76	262.43	134.99	127.44	0.70	0.214	1.43	0.150	0.98	1.00	0.204	No
739	14.78	262.77	135.18	127.59	0.70	0.214	1.43	0.150	0.98	1.00	0.204	No
740	14.80	263.12	135.38	127.74	0.70	0.214	1.43	0.150	0.98	1.00	0.204	No
741	14.82	263.46	135.57	127.88	0.69	0.214	1.43	0.150	0.98	1.00	0.204	No
742	14.84	263.80	135.77	128.03	0.69	0.214	1.43	0.150	0.98	1.00	0.204	No
743	14.86	264.13	135.97	128.16	0.69	0.214	1.43	0.150	0.98	1.00	0.204	No
744	14.88	264.46	136.16	128.30	0.69	0.214	1.43	0.150	0.98	1.00	0.204	No
745	14.90	264.79	136.36	128.43	0.69	0.214	1.43	0.150	0.98	1.00	0.204	No
746	14.92	265.12	136.56	128.57	0.69	0.214	1.43	0.149	0.98	1.00	0.204	No
747	14.94	265.45	136.75	128.70	0.69	0.213	1.43	0.149	0.98	1.00	0.204	No
748	14.96	265.77	136.95	128.83	0.69	0.213	1.43	0.149	0.98	1.00	0.203	No
749	14.98	266.10	137.14	128.95	0.69	0.213	1.43	0.149	0.98	1.00	0.203	No
750	15.00	266.42	137.34	129.08	0.69	0.213	1.43	0.149	0.98	1.00	0.203	No
751	15.02	266.74	137.54	129.20	0.69	0.213	1.43	0.149	0.98	1.00	0.203	No
752	15.04	267.05	137.73	129.32	0.69	0.213	1.43	0.149	0.98	1.00	0.203	No
753	15.06	267.37	137.93	129.44	0.69	0.213	1.43	0.149	0.98	1.00	0.203	No
754	15.09	267.84	138.22	129.62	0.69	0.213	1.43	0.149	0.98	1.00	0.203	No
755	15.10	268.00	138.32	129.68	0.69	0.213	1.43	0.149	0.98	1.00	0.203	No
756	15.12	268.31	138.52	129.80	0.69	0.213	1.43	0.149	0.98	1.00	0.203	No
757	15.14	268.63	138.71	129.92	0.69	0.213	1.43	0.149	0.98	1.00	0.203	No
758	15.16	268.95	138.91	130.04	0.69	0.213	1.43	0.149	0.98	1.00	0.203	No
759	15.18	269.26	139.11	130.16	0.69	0.212	1.43	0.149	0.98	1.00	0.203	No
760	15.20	269.58	139.30	130.27	0.69	0.212	1.43	0.149	0.98	1.00	0.202	No
761	15.23	270.05	139.60	130.45	0.69	0.212	1.43	0.149	0.98	1.00	0.202	No
762	15.24	270.21	139.69	130.51	0.69	0.212	1.43	0.149	0.98	1.00	0.202	No
763	15.26	270.53	139.89	130.64	0.69	0.212	1.43	0.148	0.98	1.00	0.202	No
764	15.28	270.85	140.09	130.76	0.68	0.212	1.43	0.148	0.98	1.00	0.202	No
765	15.30	271.17	140.28	130.88	0.68	0.212	1.43	0.148	0.98	1.00	0.202	No
766	15.32	271.49	140.48	131.01	0.68	0.212	1.43	0.148	0.98	1.00	0.202	No
767	15.34	271.81	140.68	131.13	0.68	0.212	1.43	0.148	0.98	1.00	0.202	No
768	15.37	272.29	140.97	131.32	0.68	0.212	1.43	0.148	0.98	1.00	0.202	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
769	15.38	272.45	141.07	131.38	0.68	0.212	1.43	0.148	0.98	1.00	0.202	No
770	15.40	272.77	141.26	131.51	0.68	0.212	1.43	0.148	0.98	1.00	0.202	No
771	15.42	273.09	141.46	131.63	0.68	0.211	1.43	0.148	0.98	1.00	0.201	No
772	15.44	273.41	141.66	131.76	0.68	0.211	1.43	0.148	0.98	1.00	0.201	No
773	15.46	273.74	141.85	131.88	0.68	0.211	1.43	0.148	0.98	1.00	0.201	No
774	15.48	274.06	142.05	132.02	0.68	0.211	1.43	0.148	0.98	1.00	0.201	No
775	15.50	274.39	142.25	132.15	0.68	0.211	1.43	0.148	0.98	1.00	0.201	No
776	15.52	274.73	142.44	132.29	0.68	0.211	1.43	0.148	0.98	1.00	0.201	No
777	15.54	275.06	142.64	132.42	0.68	0.211	1.43	0.148	0.98	1.00	0.201	No
778	15.56	275.40	142.83	132.56	0.68	0.211	1.43	0.148	0.98	1.00	0.201	No
779	15.58	275.73	143.03	132.70	0.68	0.211	1.43	0.147	0.98	1.00	0.201	No
780	15.60	276.07	143.23	132.84	0.68	0.211	1.43	0.147	0.98	1.00	0.200	No
781	15.62	276.41	143.42	132.99	0.68	0.210	1.43	0.147	0.98	1.00	0.200	No
782	15.64	276.75	143.62	133.14	0.68	0.210	1.43	0.147	0.98	1.00	0.200	No
783	15.66	277.10	143.81	133.28	0.68	0.210	1.43	0.147	0.98	1.00	0.200	No
784	15.68	277.45	144.01	133.43	0.68	0.210	1.43	0.147	0.98	1.00	0.200	No
785	15.70	277.79	144.21	133.59	0.68	0.210	1.43	0.147	0.98	1.00	0.200	No
786	15.72	278.14	144.40	133.74	0.68	0.210	1.43	0.147	0.98	1.00	0.200	No
787	15.74	278.49	144.60	133.89	0.67	0.210	1.43	0.147	0.98	1.00	0.200	No
788	15.76	278.84	144.80	134.05	0.67	0.210	1.43	0.147	0.98	1.00	0.200	No
789	15.78	279.20	144.99	134.20	0.67	0.210	1.43	0.147	0.98	1.00	0.199	No
790	15.82	279.90	145.38	134.52	0.67	0.209	1.43	0.147	0.98	1.00	0.199	No
791	15.82	279.90	145.38	134.52	0.67	0.209	1.43	0.147	0.98	1.00	0.199	No
792	15.84	280.26	145.58	134.68	0.67	0.209	1.43	0.146	0.98	1.00	0.199	No
793	15.86	280.61	145.78	134.84	0.67	0.209	1.43	0.146	0.98	1.00	0.199	No
794	15.88	280.97	145.97	135.00	0.67	0.209	1.43	0.146	0.98	1.00	0.199	No
795	15.90	281.33	146.17	135.16	0.67	0.209	1.43	0.146	0.98	1.00	0.199	No
796	15.93	281.87	146.46	135.40	0.67	0.209	1.43	0.146	0.98	1.00	0.199	No
797	15.94	282.04	146.56	135.48	0.67	0.209	1.43	0.146	0.98	1.00	0.199	No
798	15.96	282.40	146.76	135.65	0.67	0.209	1.43	0.146	0.98	1.00	0.198	No
799	15.98	282.76	146.95	135.81	0.67	0.208	1.43	0.146	0.98	1.00	0.198	No
800	16.00	283.12	147.15	135.97	0.67	0.208	1.43	0.146	0.98	1.00	0.198	No
801	16.02	283.48	147.35	136.14	0.67	0.208	1.43	0.146	0.98	1.00	0.198	No
802	16.04	283.85	147.54	136.30	0.67	0.208	1.43	0.146	0.98	1.00	0.198	No
803	16.06	284.21	147.74	136.47	0.67	0.208	1.43	0.146	0.98	1.00	0.198	No
804	16.08	284.57	147.93	136.64	0.67	0.208	1.43	0.145	0.98	1.00	0.198	No
805	16.10	284.93	148.13	136.80	0.67	0.208	1.43	0.145	0.98	1.00	0.198	No
806	16.12	285.29	148.33	136.97	0.67	0.208	1.43	0.145	0.97	1.00	0.197	No
807	16.14	285.66	148.52	137.13	0.67	0.207	1.43	0.145	0.97	1.00	0.197	No
808	16.16	286.02	148.72	137.30	0.67	0.207	1.43	0.145	0.97	1.00	0.197	No
809	16.18	286.39	148.92	137.47	0.67	0.207	1.43	0.145	0.97	1.00	0.197	No
810	16.20	286.75	149.11	137.64	0.66	0.207	1.43	0.145	0.97	1.00	0.197	No
811	16.22	287.11	149.31	137.81	0.66	0.207	1.43	0.145	0.97	1.00	0.197	No
812	16.24	287.48	149.50	137.97	0.66	0.207	1.43	0.145	0.97	1.00	0.197	No
813	16.26	287.84	149.70	138.14	0.66	0.207	1.43	0.145	0.97	1.00	0.197	No
814	16.28	288.21	149.90	138.31	0.66	0.207	1.43	0.145	0.97	1.00	0.196	No
815	16.30	288.57	150.09	138.48	0.66	0.206	1.43	0.145	0.97	1.00	0.196	No
816	16.32	288.93	150.29	138.65	0.66	0.206	1.43	0.144	0.97	1.00	0.196	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
817	16.34	289.30	150.49	138.81	0.66	0.206	1.43	0.144	0.97	1.00	0.196	No
818	16.36	289.66	150.68	138.98	0.66	0.206	1.43	0.144	0.97	1.00	0.196	No
819	16.38	290.03	150.88	139.15	0.66	0.206	1.43	0.144	0.97	1.00	0.196	No
820	16.40	290.39	151.07	139.32	0.66	0.206	1.43	0.144	0.97	1.00	0.196	No
821	16.42	290.76	151.27	139.49	0.66	0.206	1.43	0.144	0.97	1.00	0.196	No
822	16.44	291.12	151.47	139.65	0.66	0.206	1.43	0.144	0.97	1.00	0.196	No
823	16.46	291.48	151.66	139.82	0.66	0.205	1.43	0.144	0.97	1.00	0.196	No
824	16.48	291.85	151.86	139.99	0.66	0.205	1.43	0.144	0.97	1.00	0.196	No
825	16.50	292.21	152.06	140.15	0.66	0.205	1.43	0.144	0.97	1.00	0.196	No
826	16.52	292.57	152.25	140.32	0.66	0.205	1.43	0.144	0.97	1.00	0.196	No
827	16.54	292.93	152.45	140.48	0.66	0.205	1.43	0.144	0.97	1.00	0.196	No
828	16.56	293.28	152.64	140.64	0.66	0.205	1.43	0.143	0.97	1.00	0.195	No
829	16.58	293.64	152.84	140.80	0.66	0.205	1.43	0.143	0.97	1.00	0.195	No
830	16.60	293.99	153.04	140.96	0.66	0.205	1.43	0.143	0.97	1.00	0.195	No
831	16.62	294.35	153.23	141.12	0.66	0.205	1.43	0.143	0.97	1.00	0.195	No
832	16.64	294.70	153.43	141.27	0.66	0.204	1.43	0.143	0.97	1.00	0.195	No
833	16.66	295.06	153.62	141.43	0.66	0.204	1.43	0.143	0.97	1.00	0.195	No
834	16.68	295.42	153.82	141.60	0.65	0.204	1.43	0.143	0.97	1.00	0.195	No
835	16.70	295.77	154.02	141.76	0.65	0.204	1.43	0.143	0.97	1.00	0.195	No
836	16.72	296.13	154.21	141.92	0.65	0.204	1.43	0.143	0.97	1.00	0.195	No
837	16.74	296.49	154.41	142.08	0.65	0.204	1.43	0.143	0.97	1.00	0.195	No
838	16.76	296.85	154.61	142.25	0.65	0.204	1.43	0.143	0.97	1.00	0.195	No
839	16.78	297.21	154.80	142.41	0.65	0.204	1.43	0.143	0.97	1.00	0.195	No
840	16.80	297.57	155.00	142.57	0.65	0.204	1.43	0.142	0.97	1.00	0.195	No
841	16.82	297.93	155.19	142.73	0.65	0.203	1.43	0.142	0.97	1.00	0.194	No
842	16.84	298.29	155.39	142.90	0.65	0.203	1.43	0.142	0.97	1.00	0.194	No
843	16.86	298.64	155.59	143.06	0.65	0.203	1.43	0.142	0.97	1.00	0.194	No
844	16.88	299.00	155.78	143.22	0.65	0.203	1.43	0.142	0.97	1.00	0.194	No
845	16.90	299.35	155.98	143.38	0.65	0.203	1.43	0.142	0.97	1.00	0.194	No
846	16.92	299.71	156.18	143.53	0.65	0.203	1.43	0.142	0.97	1.00	0.194	No
847	16.94	300.06	156.37	143.69	0.65	0.203	1.43	0.142	0.97	1.00	0.194	No
848	16.96	300.41	156.57	143.84	0.65	0.203	1.43	0.142	0.97	1.00	0.194	No
849	16.98	300.76	156.76	144.00	0.65	0.203	1.43	0.142	0.97	1.00	0.194	No
850	17.00	301.11	156.96	144.15	0.65	0.202	1.43	0.142	0.97	1.00	0.194	No
851	17.02	301.45	157.16	144.29	0.65	0.202	1.43	0.142	0.97	1.00	0.194	No
852	17.04	301.79	157.35	144.44	0.65	0.202	1.43	0.142	0.97	1.00	0.194	No
853	17.06	302.14	157.55	144.59	0.65	0.202	1.43	0.141	0.97	1.00	0.194	No
854	17.08	302.48	157.74	144.73	0.65	0.202	1.43	0.141	0.97	1.00	0.194	No
855	17.10	302.81	157.94	144.87	0.65	0.202	1.43	0.141	0.97	1.00	0.194	No
856	17.12	303.15	158.14	145.02	0.65	0.202	1.43	0.141	0.97	1.00	0.194	No
857	17.14	303.49	158.33	145.16	0.65	0.202	1.43	0.141	0.97	1.00	0.194	No
858	17.17	303.99	158.63	145.36	0.64	0.202	1.43	0.141	0.97	1.00	0.194	No
859	17.18	304.16	158.73	145.43	0.64	0.201	1.43	0.141	0.97	1.00	0.194	No
860	17.20	304.49	158.92	145.57	0.64	0.201	1.43	0.141	0.97	1.00	0.194	No
861	17.22	304.82	159.12	145.70	0.64	0.201	1.43	0.141	0.97	1.00	0.193	No
862	17.24	305.15	159.31	145.83	0.64	0.201	1.43	0.141	0.97	1.00	0.193	No
863	17.26	305.47	159.51	145.96	0.64	0.201	1.43	0.141	0.97	1.00	0.193	No
864	17.28	305.80	159.71	146.09	0.64	0.201	1.43	0.141	0.97	1.00	0.193	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
865	17.30	306.12	159.90	146.22	0.64	0.201	1.43	0.141	0.97	1.00	0.193	No
866	17.32	306.45	160.10	146.35	0.64	0.201	1.43	0.141	0.97	1.00	0.193	No
867	17.34	306.77	160.30	146.48	0.64	0.201	1.43	0.141	0.97	1.00	0.193	No
868	17.36	307.10	160.49	146.61	0.64	0.201	1.43	0.140	0.97	1.00	0.193	No
869	17.38	307.42	160.69	146.74	0.64	0.201	1.43	0.140	0.97	1.00	0.193	No
870	17.40	307.75	160.88	146.86	0.64	0.200	1.43	0.140	0.97	1.00	0.193	No
871	17.42	308.07	161.08	146.99	0.64	0.200	1.43	0.140	0.97	1.00	0.193	No
872	17.44	308.39	161.28	147.11	0.64	0.200	1.43	0.140	0.97	1.00	0.193	No
873	17.46	308.71	161.47	147.24	0.64	0.200	1.43	0.140	0.97	1.00	0.192	No
874	17.48	309.03	161.67	147.36	0.64	0.200	1.43	0.140	0.97	1.00	0.192	No
875	17.50	309.35	161.87	147.48	0.64	0.200	1.43	0.140	0.97	1.00	0.192	No
876	17.52	309.67	162.06	147.61	0.64	0.200	1.43	0.140	0.97	1.00	0.192	No
877	17.54	309.99	162.26	147.73	0.64	0.200	1.43	0.140	0.97	1.00	0.192	No
878	17.56	310.31	162.45	147.86	0.64	0.200	1.43	0.140	0.97	1.00	0.192	No
879	17.58	310.63	162.65	147.98	0.64	0.200	1.43	0.140	0.97	1.00	0.192	No
880	17.60	310.95	162.85	148.11	0.64	0.200	1.43	0.140	0.97	1.00	0.192	No
881	17.62	311.27	163.04	148.23	0.64	0.200	1.43	0.140	0.97	1.00	0.192	No
882	17.64	311.60	163.24	148.36	0.64	0.199	1.43	0.140	0.97	1.00	0.192	No
883	17.66	311.92	163.43	148.48	0.63	0.199	1.43	0.140	0.97	1.00	0.192	No
884	17.68	312.24	163.63	148.61	0.63	0.199	1.43	0.139	0.97	1.00	0.192	No
885	17.70	312.56	163.83	148.73	0.63	0.199	1.43	0.139	0.97	1.00	0.191	No
886	17.72	312.89	164.02	148.86	0.63	0.199	1.43	0.139	0.97	1.00	0.191	No
887	17.74	313.21	164.22	148.99	0.63	0.199	1.43	0.139	0.97	1.00	0.191	No
888	17.76	313.54	164.42	149.12	0.63	0.199	1.43	0.139	0.97	1.00	0.191	No
889	17.78	313.87	164.61	149.25	0.63	0.199	1.43	0.139	0.97	1.00	0.191	No
890	17.80	314.20	164.81	149.39	0.63	0.199	1.43	0.139	0.97	1.00	0.190	No
891	17.82	314.54	165.00	149.53	0.63	0.199	1.43	0.139	0.97	1.00	0.190	No
892	17.84	314.88	165.20	149.68	0.63	0.198	1.43	0.139	0.97	1.00	0.191	No
893	17.86	315.22	165.40	149.82	0.63	0.198	1.43	0.139	0.97	1.00	0.191	No
894	17.88	315.55	165.59	149.96	0.63	0.198	1.43	0.139	0.97	1.00	0.191	No
895	17.90	315.89	165.79	150.10	0.63	0.198	1.43	0.139	0.97	1.00	0.191	No
896	17.92	316.22	165.99	150.23	0.63	0.198	1.43	0.139	0.97	1.00	0.191	No
897	17.94	316.55	166.18	150.37	0.63	0.198	1.43	0.139	0.97	1.00	0.191	No
898	17.96	316.88	166.38	150.50	0.63	0.198	1.43	0.139	0.97	1.00	0.191	No
899	17.98	317.20	166.57	150.63	0.63	0.198	1.43	0.138	0.97	1.00	0.191	No
900	18.00	317.52	166.77	150.75	0.63	0.198	1.43	0.138	0.97	1.00	0.191	No
901	18.02	317.84	166.97	150.87	0.63	0.198	1.43	0.138	0.97	1.00	0.191	No
902	18.04	318.16	167.16	150.99	0.63	0.198	1.43	0.138	0.97	1.00	0.191	No
903	18.06	318.48	167.36	151.12	0.63	0.197	1.43	0.138	0.97	1.00	0.190	No
904	18.08	318.79	167.55	151.24	0.63	0.197	1.43	0.138	0.97	1.00	0.190	No
905	18.10	319.11	167.75	151.36	0.63	0.197	1.43	0.138	0.97	1.00	0.190	No
906	18.12	319.43	167.95	151.48	0.63	0.197	1.43	0.138	0.97	1.00	0.190	No
907	18.14	319.75	168.14	151.60	0.63	0.197	1.43	0.138	0.97	1.00	0.190	No
908	18.16	320.06	168.34	151.72	0.62	0.197	1.43	0.138	0.97	1.00	0.190	No
909	18.18	320.38	168.54	151.84	0.62	0.197	1.43	0.138	0.97	1.00	0.190	No
910	18.20	320.69	168.73	151.96	0.62	0.197	1.43	0.138	0.97	1.00	0.190	No
911	18.22	321.01	168.93	152.08	0.62	0.197	1.43	0.138	0.97	1.00	0.190	No
912	18.24	321.33	169.12	152.20	0.62	0.197	1.43	0.138	0.97	1.00	0.190	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
913	18.26	321.64	169.32	152.32	0.62	0.197	1.43	0.138	0.97	1.00	0.190	No
914	18.28	321.96	169.52	152.44	0.62	0.197	1.43	0.138	0.97	1.00	0.190	No
915	18.30	322.28	169.71	152.56	0.62	0.196	1.43	0.138	0.97	1.00	0.190	No
916	18.32	322.59	169.91	152.68	0.62	0.196	1.43	0.137	0.97	1.00	0.190	No
917	18.34	322.90	170.11	152.80	0.62	0.196	1.43	0.137	0.97	1.00	0.190	No
918	18.36	323.22	170.30	152.92	0.62	0.196	1.43	0.137	0.97	1.00	0.189	No
919	18.38	323.53	170.50	153.03	0.62	0.196	1.43	0.137	0.97	1.00	0.189	No
920	18.40	323.85	170.69	153.15	0.62	0.196	1.43	0.137	0.97	1.00	0.189	No
921	18.42	324.16	170.89	153.27	0.62	0.196	1.43	0.137	0.97	1.00	0.189	No
922	18.44	324.47	171.09	153.39	0.62	0.196	1.43	0.137	0.97	1.00	0.189	No
923	18.46	324.79	171.28	153.51	0.62	0.196	1.43	0.137	0.97	1.00	0.189	No
924	18.48	325.11	171.48	153.63	0.62	0.196	1.43	0.137	0.97	1.00	0.189	No
925	18.50	325.43	171.68	153.75	0.62	0.196	1.43	0.137	0.97	1.00	0.189	No
926	18.52	325.75	171.87	153.88	0.62	0.196	1.43	0.137	0.97	1.00	0.189	No
927	18.54	326.07	172.07	154.00	0.62	0.195	1.43	0.137	0.97	1.00	0.188	No
928	18.56	326.39	172.26	154.12	0.62	0.195	1.43	0.137	0.97	1.00	0.188	No
929	18.58	326.71	172.46	154.25	0.62	0.195	1.43	0.137	0.97	1.00	0.188	No
930	18.60	327.03	172.66	154.38	0.62	0.195	1.43	0.137	0.97	1.00	0.188	No
931	18.62	327.36	172.85	154.51	0.62	0.195	1.43	0.137	0.97	1.00	0.188	No
932	18.64	327.69	173.05	154.64	0.62	0.195	1.43	0.137	0.97	1.00	0.188	No
933	18.66	328.02	173.24	154.78	0.62	0.195	1.43	0.136	0.97	1.00	0.188	No
934	18.68	328.36	173.44	154.91	0.61	0.195	1.43	0.136	0.97	1.00	0.188	No
935	18.70	328.69	173.64	155.05	0.61	0.195	1.43	0.136	0.96	1.00	0.187	No
936	18.72	329.03	173.83	155.20	0.61	0.195	1.43	0.136	0.96	1.00	0.187	No
937	18.74	329.37	174.03	155.34	0.61	0.195	1.43	0.136	0.96	1.00	0.187	No
938	18.76	329.71	174.23	155.49	0.61	0.194	1.43	0.136	0.96	1.00	0.186	No
939	18.78	330.07	174.42	155.64	0.61	0.194	1.43	0.136	0.96	1.00	0.186	No
940	18.80	330.42	174.62	155.81	0.61	0.194	1.43	0.136	0.96	1.00	0.185	No
941	18.82	330.79	174.81	155.97	0.61	0.194	1.43	0.136	0.96	1.00	0.185	No
942	18.84	331.15	175.01	156.14	0.61	0.194	1.43	0.136	0.96	1.00	0.186	No
943	18.86	331.51	175.21	156.30	0.61	0.194	1.43	0.136	0.96	1.00	0.186	No
944	18.88	331.87	175.40	156.46	0.61	0.194	1.43	0.136	0.96	1.00	0.187	No
945	18.90	332.22	175.60	156.62	0.61	0.194	1.43	0.136	0.97	1.00	0.187	No
946	18.92	332.57	175.80	156.77	0.61	0.194	1.43	0.135	0.97	1.00	0.187	No
947	18.94	332.91	175.99	156.92	0.61	0.193	1.43	0.135	0.97	1.00	0.187	No
948	18.96	333.26	176.19	157.07	0.61	0.193	1.43	0.135	0.97	1.00	0.187	No
949	18.98	333.60	176.38	157.21	0.61	0.193	1.43	0.135	0.96	1.00	0.187	No
950	19.00	333.93	176.58	157.35	0.61	0.193	1.43	0.135	0.96	1.00	0.187	No
951	19.02	334.26	176.78	157.49	0.61	0.193	1.43	0.135	0.96	1.00	0.186	No
952	19.04	334.59	176.97	157.62	0.61	0.193	1.43	0.135	0.96	1.00	0.186	No
953	19.06	334.91	177.17	157.75	0.61	0.193	1.43	0.135	0.96	1.00	0.186	No
954	19.08	335.24	177.36	157.88	0.61	0.193	1.43	0.135	0.96	1.00	0.186	No
955	19.10	335.58	177.56	158.02	0.61	0.193	1.43	0.135	0.96	1.00	0.186	No
956	19.12	335.91	177.76	158.16	0.61	0.193	1.43	0.135	0.96	1.00	0.186	No
957	19.15	336.42	178.05	158.37	0.61	0.192	1.43	0.135	0.96	1.00	0.185	No
958	19.16	336.60	178.15	158.45	0.61	0.192	1.43	0.135	0.96	1.00	0.185	No
959	19.19	337.12	178.44	158.67	0.61	0.192	1.43	0.135	0.96	1.00	0.185	No
960	19.20	337.29	178.54	158.75	0.61	0.192	1.43	0.135	0.96	1.00	0.184	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
961	19.22	337.65	178.74	158.91	0.60	0.192	1.43	0.134	0.96	1.00	0.183	No
962	19.24	338.02	178.93	159.08	0.60	0.192	1.43	0.134	0.96	1.00	0.182	No
963	19.26	338.38	179.13	159.25	0.60	0.192	1.43	0.134	0.96	1.00	0.182	No
964	19.28	338.75	179.33	159.42	0.60	0.192	1.43	0.134	0.96	1.00	0.183	No
965	19.30	339.11	179.52	159.59	0.60	0.192	1.43	0.134	0.96	1.00	0.184	No
966	19.32	339.47	179.72	159.75	0.60	0.192	1.43	0.134	0.96	1.00	0.185	No
967	19.34	339.83	179.92	159.92	0.60	0.191	1.43	0.134	0.96	1.00	0.184	No
968	19.36	340.19	180.11	160.08	0.60	0.191	1.43	0.134	0.96	1.00	0.183	No
969	19.38	340.55	180.31	160.24	0.60	0.191	1.43	0.134	0.96	1.00	0.183	No
970	19.40	340.91	180.50	160.40	0.60	0.191	1.43	0.134	0.96	1.00	0.184	No
971	19.42	341.27	180.70	160.57	0.60	0.191	1.43	0.134	0.96	1.00	0.184	No
972	19.44	341.63	180.90	160.73	0.60	0.191	1.43	0.134	0.96	1.00	0.182	No
973	19.46	341.99	181.09	160.90	0.60	0.191	1.43	0.134	0.96	1.00	0.182	No
974	19.48	342.36	181.29	161.07	0.60	0.191	1.43	0.133	0.96	1.00	0.182	No
975	19.50	342.73	181.49	161.24	0.60	0.191	1.43	0.133	0.96	1.00	0.182	No
976	19.52	343.10	181.68	161.41	0.60	0.190	1.43	0.133	0.96	1.00	0.182	No
977	19.54	343.46	181.88	161.59	0.60	0.190	1.43	0.133	0.96	1.00	0.181	No
978	19.56	343.83	182.07	161.76	0.60	0.190	1.43	0.133	0.96	1.00	0.181	No
979	19.58	344.20	182.27	161.93	0.60	0.190	1.43	0.133	0.96	1.00	0.182	No
980	19.60	344.57	182.47	162.10	0.60	0.190	1.43	0.133	0.96	1.00	0.183	No
981	19.62	344.93	182.66	162.27	0.60	0.190	1.43	0.133	0.96	1.00	0.183	No
982	19.64	345.30	182.86	162.44	0.60	0.190	1.43	0.133	0.96	1.00	0.183	No
983	19.66	345.66	183.05	162.61	0.60	0.190	1.43	0.133	0.96	1.00	0.182	No
984	19.68	346.02	183.25	162.77	0.60	0.190	1.43	0.133	0.96	1.00	0.181	No
985	19.70	346.39	183.45	162.94	0.60	0.189	1.43	0.133	0.96	1.00	0.180	No
986	19.72	346.75	183.64	163.11	0.60	0.189	1.43	0.133	0.95	1.00	0.179	No
987	19.74	347.11	183.84	163.27	0.60	0.189	1.43	0.132	0.96	1.00	0.180	No
988	19.76	347.47	184.04	163.44	0.59	0.189	1.43	0.132	0.96	1.00	0.182	No
989	19.78	347.83	184.23	163.60	0.59	0.189	1.43	0.132	0.96	1.00	0.182	No
990	19.80	348.19	184.43	163.77	0.59	0.189	1.43	0.132	0.96	1.00	0.181	No
991	19.82	348.56	184.62	163.94	0.59	0.189	1.43	0.132	0.96	1.00	0.180	No
992	19.84	348.93	184.82	164.11	0.59	0.189	1.43	0.132	0.95	1.00	0.178	No
993	19.86	349.30	185.02	164.28	0.59	0.189	1.43	0.132	0.95	1.00	0.177	No
994	19.88	349.67	185.21	164.46	0.59	0.188	1.43	0.132	0.95	1.00	0.177	No
995	19.90	350.04	185.41	164.63	0.59	0.188	1.43	0.132	0.95	1.00	0.177	No
996	19.92	350.41	185.61	164.80	0.59	0.188	1.43	0.132	0.95	1.00	0.177	No
997	19.94	350.78	185.80	164.98	0.59	0.188	1.43	0.132	0.95	1.00	0.178	No
998	19.96	351.15	186.00	165.15	0.59	0.188	1.43	0.132	0.95	1.00	0.177	No
999	19.98	351.53	186.19	165.33	0.59	0.188	1.43	0.132	0.95	1.00	0.176	No
1000	20.00	351.91	186.39	165.52	0.59	0.188	1.43	0.131	0.95	1.00	0.175	No
1001	20.02	352.29	186.59	165.70	0.59	0.188	1.43	0.131	0.95	1.00	0.173	No
1002	20.04	352.67	186.78	165.89	0.59	0.188	1.43	0.131	0.95	1.00	0.172	No
1003	20.06	353.06	186.98	166.08	0.59	0.187	1.43	0.131	0.95	1.00	0.172	No
1004	20.08	353.44	187.17	166.26	0.59	0.187	1.43	0.131	0.95	1.00	0.173	No
1005	20.10	353.82	187.37	166.45	0.59	0.187	1.43	0.131	0.95	1.00	0.173	No
1006	20.12	354.20	187.57	166.64	0.59	0.187	1.43	0.131	0.95	1.00	0.174	No
1007	20.15	354.77	187.86	166.91	0.59	0.187	1.43	0.131	0.95	1.00	0.175	No
1008	20.16	354.96	187.96	167.00	0.59	0.187	1.43	0.131	0.95	1.00	0.175	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1009	20.18	355.34	188.16	167.19	0.59	0.187	1.43	0.131	0.95	1.00	0.177	No
1010	20.20	355.72	188.35	167.37	0.59	0.187	1.43	0.131	0.95	1.00	0.177	No
1011	20.22	356.10	188.55	167.55	0.59	0.186	1.43	0.131	0.95	1.00	0.178	No
1012	20.25	356.66	188.84	167.82	0.59	0.186	1.43	0.130	0.96	1.00	0.179	No
1013	20.26	356.84	188.94	167.90	0.59	0.186	1.43	0.130	0.95	1.00	0.178	No
1014	20.28	357.21	189.14	168.08	0.59	0.186	1.43	0.130	0.95	1.00	0.177	No
1015	20.30	357.59	189.33	168.26	0.59	0.186	1.43	0.130	0.95	1.00	0.176	No
1016	20.32	357.97	189.53	168.44	0.59	0.186	1.43	0.130	0.95	1.00	0.175	No
1017	20.34	358.35	189.73	168.63	0.58	0.186	1.43	0.130	0.95	1.00	0.174	No
1018	20.36	358.74	189.92	168.82	0.58	0.186	1.43	0.130	0.95	1.00	0.174	No
1019	20.38	359.12	190.12	169.01	0.58	0.186	1.43	0.130	0.95	1.00	0.174	No
1020	20.40	359.51	190.31	169.20	0.58	0.185	1.43	0.130	0.95	1.00	0.173	No
1021	20.42	359.90	190.51	169.39	0.58	0.185	1.43	0.130	0.95	1.00	0.173	No
1022	20.44	360.28	190.71	169.58	0.58	0.185	1.43	0.130	0.95	1.00	2.000	Yes
1023	20.46	360.67	190.90	169.77	0.58	0.185	1.43	0.130	0.95	1.00	2.000	Yes
1024	20.48	361.06	191.10	169.96	0.58	0.185	1.43	0.129	0.94	1.00	2.000	Yes
1025	20.50	361.46	191.30	170.16	0.58	0.185	1.43	0.129	0.94	1.00	2.000	Yes
1026	20.52	361.85	191.49	170.36	0.58	0.185	1.43	0.129	0.94	1.00	2.000	Yes
1027	20.54	362.24	191.69	170.56	0.58	0.185	1.43	0.129	0.93	1.00	2.000	Yes
1028	20.56	362.64	191.88	170.76	0.58	0.184	1.43	0.129	0.93	1.00	2.000	Yes
1029	20.58	363.03	192.08	170.95	0.58	0.184	1.43	0.129	0.93	1.00	2.000	Yes
1030	20.60	363.43	192.28	171.15	0.58	0.184	1.43	0.129	0.93	1.00	2.000	Yes
1031	20.62	363.81	192.47	171.34	0.58	0.184	1.43	0.129	0.93	1.00	2.000	Yes
1032	20.64	364.20	192.67	171.53	0.58	0.184	1.43	0.129	0.93	1.00	2.000	Yes
1033	20.66	364.58	192.86	171.71	0.58	0.184	1.43	0.129	0.93	1.00	2.000	Yes
1034	20.68	364.95	193.06	171.89	0.58	0.184	1.43	0.129	0.94	1.00	2.000	Yes
1035	20.70	365.32	193.26	172.06	0.58	0.184	1.43	0.129	0.95	1.00	2.000	Yes
1036	20.72	365.68	193.45	172.22	0.58	0.184	1.43	0.129	0.95	1.00	2.000	Yes
1037	20.74	366.03	193.65	172.38	0.58	0.183	1.43	0.128	0.96	1.00	2.000	Yes
1038	20.76	366.38	193.85	172.54	0.58	0.183	1.43	0.128	0.95	1.00	0.178	No
1039	20.78	366.74	194.04	172.70	0.58	0.183	1.43	0.128	0.95	1.00	0.177	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (m)
σ_v: Total overburden pressure at test point (kPa)
u_0: Water pressure at test point (kPa)
σ_v': Effective overburden pressure based on GWT during earthquake (kPa)
r_d: Nonlinear shear mass factor
CSR: Cyclic Stress Ratio
MSF: Magnitude Scaling Factor
CSR_{eq}: CSR adjusted for M=7.5
K_σ: Effective overburden stress factor
CSR^*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1	0.02	0.80	80.96	2.72	0.57	1.70	13.66	0.00	13.66	4.000	No	Yes	2.00
2	0.04	0.80	90.57	2.84	0.57	1.70	13.15	0.00	13.15	4.000	No	Yes	2.00
3	0.06	0.84	91.81	2.86	0.57	1.70	14.09	0.00	14.09	4.000	No	Yes	2.00
4	0.08	0.90	92.92	2.87	0.56	1.70	15.10	0.00	15.10	4.000	No	Yes	2.00
5	0.10	0.96	93.26	2.88	0.56	1.70	16.23	0.00	16.23	4.000	No	Yes	2.00
6	0.12	1.01	94.18	2.89	0.56	1.70	17.02	0.00	17.02	4.000	No	Yes	2.00
7	0.14	1.07	94.67	2.90	0.55	1.70	17.76	0.00	17.76	4.000	No	Yes	2.00
8	0.16	1.14	95.27	2.90	0.55	1.70	19.07	0.00	19.07	4.000	No	Yes	2.00
9	0.18	1.24	93.80	2.89	0.55	1.70	20.47	0.00	20.47	4.000	No	Yes	2.00
10	0.20	1.32	92.65	2.87	0.54	1.70	22.94	0.00	22.94	4.000	No	Yes	2.00
11	0.22	1.32	94.98	2.90	0.54	1.70	23.36	0.00	23.36	4.000	No	Yes	2.00
12	0.24	1.25	99.03	2.95	0.55	1.70	20.16	0.00	20.16	4.000	No	Yes	2.00
13	0.26	1.18	100.00	3.00	0.55	1.70	19.57	0.00	19.57	4.000	No	Yes	2.00
14	0.28	1.17	100.00	3.00	0.55	1.70	19.73	0.00	19.73	4.000	No	Yes	2.00
15	0.30	1.15	100.00	2.99	0.55	1.70	19.55	0.00	19.55	4.000	No	Yes	2.00
16	0.32	1.11	100.00	3.00	0.55	1.70	18.77	0.00	18.77	4.000	No	Yes	2.00
17	0.34	1.08	100.00	3.00	0.55	1.70	17.95	0.00	17.95	4.000	No	Yes	2.00
18	0.36	1.05	100.00	2.99	0.55	1.70	17.61	0.00	17.61	4.000	No	Yes	2.00
19	0.38	1.04	100.00	2.97	0.55	1.70	17.66	0.00	17.66	4.000	No	Yes	2.00
20	0.40	1.05	98.71	2.95	0.55	1.70	17.51	0.00	17.51	4.000	No	Yes	2.00
21	0.42	1.04	97.95	2.94	0.55	1.70	17.78	0.00	17.78	4.000	No	Yes	2.00
22	0.44	1.03	98.44	2.94	0.55	1.70	17.48	0.00	17.48	4.000	No	Yes	2.00
23	0.46	1.00	100.00	2.97	0.56	1.70	16.98	0.00	16.98	4.000	No	Yes	2.00
24	0.48	0.98	100.00	3.01	0.56	1.70	16.46	0.00	16.46	4.000	No	Yes	2.00
25	0.50	0.97	100.00	3.04	0.56	1.70	16.35	0.00	16.35	4.000	No	Yes	2.00
26	0.52	0.98	100.00	3.05	0.56	1.70	16.59	0.00	16.59	4.000	No	Yes	2.00
27	0.54	0.98	100.00	3.07	0.56	1.70	16.60	0.00	16.60	4.000	No	Yes	2.00
28	0.56	0.98	100.00	3.08	0.56	1.70	16.57	0.00	16.57	4.000	No	Yes	2.00
29	0.58	0.98	100.00	3.08	0.56	1.70	16.53	0.00	16.53	4.000	No	Yes	2.00
30	0.60	0.97	100.00	3.09	0.56	1.70	16.54	0.00	16.54	4.000	No	Yes	2.00
31	0.62	0.94	100.00	3.10	0.56	1.70	16.04	0.00	16.04	4.000	No	Yes	2.00
32	0.64	0.91	100.00	3.12	0.56	1.70	15.33	0.00	15.33	4.000	No	Yes	2.00
33	0.66	0.88	100.00	3.13	0.56	1.70	14.89	0.00	14.89	4.000	No	Yes	2.00
34	0.68	0.86	100.00	3.14	0.57	1.70	14.34	0.00	14.34	4.000	No	Yes	2.00
35	0.70	0.83	100.00	3.16	0.57	1.70	14.06	0.00	14.06	4.000	No	Yes	2.00
36	0.72	0.81	100.00	3.16	0.57	1.70	13.42	0.00	13.42	4.000	No	Yes	2.00
37	0.74	0.79	100.00	3.16	0.57	1.70	13.37	0.00	13.37	4.000	No	Yes	2.00
38	0.76	0.77	100.00	3.16	0.57	1.70	13.31	0.00	13.31	4.000	No	Yes	2.00
39	0.78	0.74	100.00	3.17	0.57	1.70	12.21	0.00	12.21	4.000	No	Yes	2.00
40	0.80	0.70	100.00	3.18	0.58	1.70	11.88	0.00	11.88	4.000	No	Yes	2.00
41	0.82	0.68	100.00	3.18	0.58	1.70	11.43	0.00	11.43	4.000	No	Yes	2.00
42	0.84	0.68	100.00	3.18	0.58	1.70	11.36	0.00	11.36	4.000	No	Yes	2.00
43	0.86	0.71	100.00	3.15	0.58	1.70	11.81	0.00	11.81	4.000	No	Yes	2.00
44	0.88	0.78	100.00	3.09	0.57	1.70	12.88	0.00	12.88	4.000	No	Yes	2.00
45	0.90	0.84	100.00	3.05	0.57	1.70	14.50	0.00	14.50	4.000	No	Yes	2.00
46	0.92	0.90	100.00	3.01	0.56	1.70	14.95	0.00	14.95	4.000	No	Yes	2.00
47	0.94	0.92	100.00	3.02	0.56	1.70	16.21	0.00	16.21	4.000	No	Yes	2.00
48	0.96	0.92	100.00	3.05	0.56	1.70	15.51	0.00	15.51	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
49	0.98	0.86	100.00	3.12	0.56	1.70	14.73	0.00	14.73	4.000	No	Yes	2.00
50	1.00	0.81	100.00	3.19	0.57	1.70	13.32	0.00	13.32	4.000	No	Yes	2.00
51	1.02	0.78	100.00	3.24	0.57	1.70	12.93	0.00	12.93	4.000	No	Yes	2.00
52	1.04	0.78	100.00	3.26	0.57	1.70	13.40	0.00	13.40	4.000	No	Yes	2.00
53	1.06	0.79	100.00	3.27	0.57	1.70	13.27	0.00	13.27	4.000	No	Yes	2.00
54	1.08	0.79	100.00	3.27	0.57	1.70	13.19	0.00	13.19	4.000	No	Yes	2.00
55	1.10	0.79	100.00	3.26	0.57	1.70	13.02	0.00	13.02	4.000	No	Yes	2.00
56	1.12	0.82	100.00	3.21	0.57	1.70	13.25	0.00	13.25	4.000	No	Yes	2.00
57	1.14	0.87	100.00	3.14	0.56	1.70	14.94	0.00	14.94	4.000	No	Yes	2.00
58	1.16	0.94	100.00	3.08	0.56	1.70	15.55	0.00	15.55	4.000	No	Yes	2.00
59	1.18	0.99	100.00	3.03	0.56	1.70	16.48	0.00	16.48	4.000	No	Yes	2.00
60	1.20	1.06	100.00	2.98	0.55	1.70	17.36	0.00	17.36	4.000	No	Yes	2.00
61	1.22	1.14	96.90	2.92	0.55	1.70	19.23	0.00	19.23	4.000	No	Yes	2.00
62	1.24	1.24	93.19	2.88	0.54	1.70	20.80	0.00	20.80	4.000	No	Yes	2.00
63	1.26	1.32	90.52	2.84	0.54	1.70	22.09	0.00	22.09	4.000	No	Yes	2.00
64	1.28	1.40	89.20	2.83	0.54	1.70	23.34	0.00	23.34	4.000	No	Yes	2.00
65	1.30	1.45	89.32	2.83	0.53	1.70	24.63	0.00	24.63	4.000	No	Yes	2.00
66	1.32	1.47	91.59	2.86	0.53	1.70	24.73	0.00	24.73	4.000	No	Yes	2.00
67	1.34	1.46	95.45	2.91	0.53	1.70	24.36	0.00	24.36	4.000	No	Yes	2.00
68	1.36	1.44	99.35	2.95	0.53	1.70	23.95	0.00	23.95	4.000	No	Yes	2.00
69	1.39	1.42	100.00	3.00	0.53	1.70	23.86	0.00	23.86	4.000	No	Yes	2.00
70	1.40	1.40	100.00	3.04	0.53	1.70	23.29	0.00	23.29	4.000	No	Yes	2.00
71	1.42	1.38	100.00	3.07	0.54	1.70	23.03	0.00	23.03	4.000	No	Yes	2.00
72	1.44	1.35	100.00	3.08	0.54	1.70	22.70	0.00	22.70	4.000	No	Yes	2.00
73	1.46	1.32	100.00	3.10	0.54	1.70	22.09	0.00	22.09	4.000	No	Yes	2.00
74	1.48	1.29	100.00	3.11	0.54	1.70	21.63	0.00	21.63	4.000	No	Yes	2.00
75	1.50	1.26	100.00	3.12	0.54	1.70	20.97	0.00	20.97	4.000	No	Yes	2.00
76	1.52	1.25	100.00	3.12	0.54	1.70	20.74	0.00	20.74	4.000	No	Yes	2.00
77	1.54	1.28	100.00	3.10	0.54	1.70	21.11	0.00	21.11	4.000	No	Yes	2.00
78	1.56	1.34	100.00	3.07	0.54	1.70	22.31	0.00	22.31	4.000	No	Yes	2.00
79	1.58	1.43	100.00	3.02	0.53	1.70	23.90	0.00	23.90	4.000	No	Yes	2.00
80	1.60	1.52	100.00	2.98	0.53	1.70	25.64	0.00	25.64	4.000	No	Yes	2.00
81	1.62	1.58	98.76	2.95	0.52	1.70	26.66	0.00	26.66	4.000	No	Yes	2.00
82	1.65	1.62	97.81	2.94	0.52	1.70	27.21	0.00	27.21	4.000	No	Yes	2.00
83	1.66	1.65	97.27	2.93	0.52	1.70	27.45	0.00	27.45	4.000	No	Yes	2.00
84	1.68	1.68	97.14	2.93	0.52	1.70	28.31	0.00	28.31	4.000	No	Yes	2.00
85	1.70	1.72	96.94	2.92	0.52	1.70	28.60	0.00	28.60	4.000	No	Yes	2.00
86	1.72	1.75	97.03	2.93	0.52	1.70	29.27	0.00	29.27	4.000	No	Yes	2.00
87	1.74	1.77	97.22	2.93	0.51	1.70	29.76	0.00	29.76	4.000	No	Yes	2.00
88	1.76	1.79	97.46	2.93	0.51	1.70	29.81	0.00	29.81	4.000	No	Yes	2.00
89	1.78	1.81	97.81	2.94	0.51	1.70	30.45	0.00	30.45	4.000	No	Yes	2.00
90	1.80	1.82	98.14	2.94	0.51	1.70	30.55	0.00	30.55	4.000	No	Yes	2.00
91	1.82	1.82	98.55	2.94	0.51	1.70	30.32	0.00	30.32	4.000	No	Yes	2.00
92	1.84	1.79	99.41	2.96	0.51	1.70	30.28	0.00	30.28	4.000	No	Yes	2.00
93	1.86	1.76	100.00	2.97	0.52	1.70	29.26	0.00	29.26	4.000	No	Yes	2.00
94	1.88	1.74	100.00	2.97	0.52	1.70	28.94	0.00	28.94	4.000	No	Yes	2.00
95	1.90	1.72	100.00	2.97	0.52	1.70	29.03	0.00	29.03	4.000	No	Yes	2.00
96	1.92	1.71	100.00	2.97	0.52	1.70	28.26	0.00	28.26	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
97	1.95	1.72	99.90	2.96	0.52	1.70	28.58	0.00	28.58	4.000	No	Yes	2.00
98	1.96	1.74	98.78	2.95	0.52	1.70	28.94	0.00	28.94	4.000	No	Yes	2.00
99	1.98	1.78	97.42	2.93	0.52	1.70	29.52	0.00	29.52	4.000	No	Yes	2.00
100	2.00	1.81	95.66	2.91	0.51	1.70	30.18	0.00	30.18	4.000	No	Yes	2.00
101	2.03	1.88	92.61	2.87	0.51	1.70	30.84	0.00	30.84	4.000	No	Yes	2.00
102	2.04	1.96	89.24	2.83	0.51	1.70	32.88	0.00	32.88	4.000	No	Yes	2.00
103	2.06	2.04	86.14	2.79	0.50	1.70	34.24	0.00	34.24	4.000	No	Yes	2.00
104	2.08	2.08	84.65	2.77	0.50	1.70	34.70	0.00	34.70	4.000	No	Yes	2.00
105	2.10	2.09	83.99	2.76	0.50	1.70	34.84	0.00	34.84	4.000	No	Yes	2.00
106	2.12	2.08	84.46	2.77	0.50	1.70	35.09	0.00	35.09	4.000	No	Yes	2.00
107	2.14	2.04	86.07	2.79	0.51	1.70	34.01	0.00	34.01	4.000	No	Yes	2.00
108	2.16	1.95	89.11	2.83	0.51	1.70	32.70	0.00	32.70	4.000	No	Yes	2.00
109	2.18	1.86	92.16	2.86	0.51	1.70	30.66	0.00	30.66	4.000	No	Yes	2.00
110	2.20	1.77	94.83	2.90	0.52	1.70	29.51	0.00	29.51	4.000	No	Yes	2.00
111	2.22	1.68	97.29	2.93	0.52	1.70	28.27	0.00	28.27	4.000	No	Yes	2.00
112	2.24	1.59	99.74	2.96	0.53	1.70	26.08	0.00	26.08	4.000	No	Yes	2.00
113	2.26	1.49	100.00	2.99	0.53	1.70	24.85	0.00	24.85	4.000	No	Yes	2.00
114	2.28	1.40	100.00	3.01	0.53	1.70	23.29	0.00	23.29	4.000	No	Yes	2.00
115	2.30	1.30	100.00	3.03	0.54	1.70	21.38	0.00	21.38	4.000	No	Yes	2.00
116	2.32	1.22	100.00	3.05	0.55	1.70	20.07	0.00	20.07	4.000	No	Yes	2.00
117	2.34	1.15	100.00	3.06	0.55	1.70	19.23	0.00	19.23	4.000	No	Yes	2.00
118	2.36	1.09	100.00	3.07	0.55	1.70	17.91	0.00	17.91	4.000	No	Yes	2.00
119	2.38	1.04	100.00	3.09	0.56	1.70	16.72	0.00	16.72	4.000	No	Yes	2.00
120	2.40	1.00	100.00	3.09	0.56	1.70	16.52	0.00	16.52	4.000	No	Yes	2.00
121	2.42	0.98	100.00	3.07	0.56	1.70	15.96	0.00	15.96	4.000	No	Yes	2.00
122	2.44	0.96	100.00	3.06	0.56	1.70	15.76	0.00	15.76	4.000	No	Yes	2.00
123	2.46	0.95	100.00	3.04	0.56	1.70	15.71	0.00	15.71	4.000	No	Yes	2.00
124	2.48	0.94	100.00	3.03	0.56	1.70	15.58	0.00	15.58	4.000	No	Yes	2.00
125	2.50	0.92	100.00	3.02	0.56	1.70	15.11	0.00	15.11	4.000	No	Yes	2.00
126	2.52	0.90	100.00	3.03	0.56	1.70	14.75	0.00	14.75	4.000	No	Yes	2.00
127	2.54	0.86	100.00	3.04	0.57	1.70	14.20	0.00	14.20	4.000	No	Yes	2.00
128	2.56	0.82	100.00	3.06	0.57	1.70	13.46	0.00	13.46	4.000	No	Yes	2.00
129	2.58	0.78	100.00	3.08	0.57	1.70	12.64	0.00	12.64	4.000	No	Yes	2.00
130	2.60	0.73	100.00	3.10	0.57	1.70	12.05	0.00	12.05	4.000	No	Yes	2.00
131	2.62	0.69	100.00	3.12	0.58	1.70	11.00	0.00	11.00	4.000	No	Yes	2.00
132	2.64	0.66	100.00	3.14	0.58	1.70	10.80	0.00	10.80	4.000	No	Yes	2.00
133	2.66	0.64	100.00	3.15	0.58	1.70	10.49	0.00	10.49	4.000	No	Yes	2.00
134	2.68	0.63	100.00	3.15	0.58	1.70	10.03	0.00	10.03	4.000	No	Yes	2.00
135	2.70	0.62	100.00	3.14	0.58	1.70	10.15	0.00	10.15	4.000	No	Yes	2.00
136	2.72	0.60	100.00	3.15	0.58	1.70	9.84	0.00	9.84	4.000	No	Yes	2.00
137	2.74	0.57	100.00	3.16	0.59	1.70	9.03	0.00	9.03	4.000	No	Yes	2.00
138	2.76	0.55	100.00	3.17	0.59	1.70	8.68	0.00	8.68	4.000	No	Yes	2.00
139	2.78	0.55	100.00	3.14	0.59	1.70	8.68	0.00	8.68	4.000	No	Yes	2.00
140	2.80	0.57	100.00	3.09	0.59	1.70	9.04	0.00	9.04	4.000	No	Yes	2.00
141	2.82	0.60	100.00	3.04	0.58	1.70	9.94	0.00	9.94	4.000	No	Yes	2.00
142	2.84	0.62	100.00	3.01	0.58	1.70	10.13	0.00	10.13	4.000	No	Yes	2.00
143	2.86	0.62	100.00	3.02	0.58	1.70	10.00	0.00	10.00	4.000	No	Yes	2.00
144	2.88	0.60	100.00	3.05	0.58	1.69	9.99	0.00	9.99	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
145	2.90	0.60	100.00	3.06	0.59	1.69	9.15	0.00	9.15	4.000	No	Yes	2.00
146	2.92	0.59	100.00	3.07	0.58	1.69	9.82	0.00	9.82	4.000	No	Yes	2.00
147	2.94	0.59	100.00	3.08	0.58	1.69	9.50	0.00	9.50	4.000	No	Yes	2.00
148	2.96	0.55	100.00	3.13	0.59	1.69	9.07	0.00	9.07	4.000	No	Yes	2.00
149	2.98	0.52	100.00	3.16	0.59	1.69	7.97	0.00	7.97	4.000	No	Yes	2.00
150	3.00	0.50	100.00	3.17	0.59	1.69	7.84	0.00	7.84	4.000	No	Yes	2.00
151	3.02	0.51	100.00	3.13	0.59	1.68	8.01	0.00	8.01	4.000	No	Yes	2.00
152	3.04	0.55	100.00	3.05	0.59	1.68	8.48	0.00	8.48	4.000	No	Yes	2.00
153	3.06	0.59	100.00	2.98	0.58	1.67	9.59	0.00	9.59	4.000	No	Yes	2.00
154	3.08	0.62	98.32	2.94	0.58	1.66	10.02	0.00	10.02	4.000	No	Yes	2.00
155	3.10	0.61	100.00	2.96	0.58	1.66	9.70	0.00	9.70	4.000	No	Yes	2.00
156	3.12	0.58	100.00	3.04	0.59	1.66	9.24	0.00	9.24	4.000	No	Yes	2.00
157	3.14	0.54	100.00	3.12	0.59	1.66	8.37	0.00	8.37	4.000	No	Yes	2.00
158	3.16	0.51	100.00	3.18	0.59	1.66	7.91	0.00	7.91	4.000	No	Yes	2.00
159	3.18	0.49	100.00	3.22	0.59	1.66	7.71	0.00	7.71	4.000	No	Yes	2.00
160	3.21	0.49	100.00	3.25	0.59	1.66	7.39	0.00	7.39	4.000	No	Yes	2.00
161	3.22	0.50	100.00	3.24	0.59	1.66	7.61	0.00	7.61	4.000	No	Yes	2.00
162	3.24	0.53	100.00	3.18	0.59	1.65	8.18	0.00	8.18	4.000	No	Yes	2.00
163	3.26	0.57	100.00	3.10	0.59	1.64	8.90	0.00	8.90	4.000	No	Yes	2.00
164	3.28	0.60	100.00	3.04	0.58	1.64	9.50	0.00	9.50	4.000	No	Yes	2.00
165	3.30	0.60	100.00	3.02	0.58	1.63	9.52	0.00	9.52	4.000	No	Yes	2.00
166	3.32	0.58	100.00	3.04	0.59	1.64	8.92	0.00	8.92	4.000	No	Yes	2.00
167	3.34	0.56	100.00	3.08	0.59	1.64	8.46	0.00	8.46	4.000	No	Yes	2.00
168	3.36	0.56	100.00	3.09	0.59	1.63	8.48	0.00	8.48	4.000	No	Yes	2.00
169	3.38	0.60	100.00	3.06	0.59	1.63	9.08	0.00	9.08	4.000	No	Yes	2.00
170	3.40	0.63	100.00	3.03	0.58	1.62	9.89	0.00	9.89	4.000	No	Yes	2.00
171	3.42	0.63	100.00	3.02	0.58	1.62	9.83	0.00	9.83	4.000	No	Yes	2.00
172	3.44	0.60	100.00	3.07	0.59	1.62	9.27	0.00	9.27	4.000	No	Yes	2.00
173	3.46	0.57	100.00	3.11	0.59	1.62	8.49	0.00	8.49	4.000	No	Yes	2.00
174	3.48	0.55	100.00	3.13	0.59	1.62	8.11	0.00	8.11	4.000	No	Yes	2.00
175	3.50	0.59	100.00	3.08	0.59	1.61	8.53	0.00	8.53	4.000	No	Yes	2.00
176	3.52	0.66	100.00	2.99	0.58	1.60	10.08	0.00	10.08	4.000	No	Yes	2.00
177	3.54	0.74	95.23	2.90	0.58	1.60	11.32	0.00	11.32	4.000	No	Yes	2.00
178	3.56	0.79	91.72	2.86	0.58	1.59	12.29	0.00	12.29	4.000	No	Yes	2.00
179	3.58	0.78	92.95	2.87	0.58	1.59	12.19	0.00	12.19	4.000	No	Yes	2.00
180	3.60	0.75	95.72	2.91	0.58	1.59	11.00	0.00	11.00	4.000	No	Yes	2.00
181	3.63	0.72	99.19	2.95	0.58	1.58	10.89	0.00	10.89	4.000	No	Yes	2.00
182	3.64	0.71	100.00	2.99	0.58	1.58	10.77	0.00	10.77	4.000	No	Yes	2.00
183	3.66	0.69	100.00	3.04	0.58	1.58	10.36	0.00	10.36	4.000	No	Yes	2.00
184	3.68	0.66	100.00	3.10	0.58	1.58	9.88	0.00	9.88	4.000	No	Yes	2.00
185	3.70	0.62	100.00	3.15	0.59	1.58	9.29	0.00	9.29	4.000	No	Yes	2.00
186	3.72	0.60	100.00	3.17	0.59	1.58	8.78	0.00	8.78	4.000	No	Yes	2.00
187	3.74	0.58	100.00	3.18	0.59	1.58	8.69	0.00	8.69	4.000	No	Yes	2.00
188	3.76	0.56	100.00	3.19	0.59	1.58	8.31	0.00	8.31	4.000	No	Yes	2.00
189	3.78	0.53	100.00	3.20	0.59	1.58	7.83	0.00	7.83	4.000	No	Yes	2.00
190	3.80	0.51	100.00	3.20	0.59	1.58	7.50	0.00	7.50	4.000	No	Yes	2.00
191	3.82	0.50	100.00	3.20	0.59	1.58	7.23	0.00	7.23	4.000	No	Yes	2.00
192	3.84	0.51	100.00	3.16	0.59	1.57	7.25	0.00	7.25	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
193	3.86	0.55	100.00	3.08	0.59	1.57	7.93	0.00	7.93	4.000	No	Yes	2.00
194	3.88	0.63	100.00	2.96	0.59	1.56	8.97	0.00	8.97	4.000	No	Yes	2.00
195	3.90	0.68	96.15	2.91	0.58	1.55	10.82	0.00	10.82	4.000	No	Yes	2.00
196	3.92	0.69	95.97	2.91	0.58	1.55	10.11	0.00	10.11	4.000	No	Yes	2.00
197	3.94	0.65	100.00	2.97	0.58	1.55	9.36	0.00	9.36	4.000	No	Yes	2.00
198	3.96	0.62	100.00	3.02	0.59	1.55	9.18	0.00	9.18	4.000	No	Yes	2.00
199	3.98	0.61	100.00	3.06	0.59	1.55	8.82	0.00	8.82	4.000	No	Yes	2.00
200	4.00	0.61	100.00	3.08	0.59	1.55	8.73	0.00	8.73	4.000	No	Yes	2.00
201	4.03	0.62	100.00	3.07	0.59	1.54	8.99	0.00	8.99	4.000	No	Yes	2.00
202	4.04	0.65	100.00	3.04	0.59	1.54	9.19	0.00	9.19	4.000	No	Yes	2.00
203	4.06	0.69	100.00	2.98	0.58	1.54	9.76	0.00	9.76	4.000	No	Yes	2.00
204	4.08	0.75	95.98	2.91	0.58	1.53	10.94	0.00	10.94	4.000	No	Yes	2.00
205	4.10	0.82	90.59	2.84	0.58	1.53	11.76	0.00	11.76	4.000	No	Yes	2.00
206	4.12	0.87	87.16	2.80	0.58	1.52	12.56	0.00	12.56	4.000	No	Yes	2.00
207	4.14	0.91	85.17	2.78	0.57	1.52	13.32	0.00	13.32	4.000	No	Yes	2.00
208	4.16	0.93	85.68	2.78	0.57	1.51	13.46	0.00	13.46	4.000	No	Yes	2.00
209	4.18	0.93	88.33	2.82	0.57	1.51	13.30	0.00	13.30	4.000	No	Yes	2.00
210	4.20	0.92	91.69	2.86	0.57	1.51	13.10	0.00	13.10	4.000	No	Yes	2.00
211	4.22	0.91	94.93	2.90	0.57	1.50	13.13	0.00	13.13	4.000	No	Yes	2.00
212	4.24	0.92	97.31	2.93	0.57	1.50	13.00	0.00	13.00	4.000	No	Yes	2.00
213	4.26	0.93	99.03	2.95	0.57	1.50	13.11	0.00	13.11	4.000	No	Yes	2.00
214	4.28	0.96	99.31	2.95	0.57	1.49	13.75	0.00	13.75	4.000	No	Yes	2.00
215	4.30	1.00	98.72	2.95	0.57	1.49	14.25	0.00	14.25	4.000	No	Yes	2.00
216	4.32	1.01	98.20	2.94	0.57	1.49	14.35	0.00	14.35	4.000	No	Yes	2.00
217	4.34	1.00	98.40	2.94	0.57	1.48	14.19	0.00	14.19	4.000	No	Yes	2.00
218	4.36	1.00	98.83	2.95	0.57	1.48	13.96	0.00	13.96	4.000	No	Yes	2.00
219	4.38	1.00	98.91	2.95	0.57	1.48	13.93	0.00	13.93	4.000	No	Yes	2.00
220	4.40	1.00	98.73	2.95	0.57	1.48	14.07	0.00	14.07	4.000	No	Yes	2.00
221	4.42	1.00	99.16	2.95	0.57	1.48	14.03	0.00	14.03	4.000	No	Yes	2.00
222	4.44	0.99	100.00	2.96	0.57	1.47	13.74	0.00	13.74	4.000	No	Yes	2.00
223	4.46	0.97	100.00	2.98	0.57	1.47	13.55	0.00	13.55	4.000	No	Yes	2.00
224	4.48	0.97	100.00	2.99	0.57	1.47	13.46	0.00	13.46	4.000	No	Yes	2.00
225	4.50	0.96	100.00	3.00	0.57	1.47	13.52	0.00	13.52	4.000	No	Yes	2.00
226	4.52	0.96	100.00	3.02	0.57	1.47	13.23	0.00	13.23	4.000	No	Yes	2.00
227	4.54	0.94	100.00	3.04	0.57	1.46	13.07	0.00	13.07	4.000	No	Yes	2.00
228	4.56	0.92	100.00	3.06	0.57	1.46	12.78	0.00	12.78	4.000	No	Yes	2.00
229	4.58	0.91	100.00	3.08	0.57	1.46	12.43	0.00	12.43	4.000	No	Yes	2.00
230	4.60	0.89	100.00	3.09	0.57	1.46	12.37	0.00	12.37	4.000	No	Yes	2.00
231	4.62	0.88	100.00	3.09	0.57	1.46	12.14	0.00	12.14	4.000	No	Yes	2.00
232	4.64	0.86	100.00	3.11	0.58	1.46	11.79	0.00	11.79	4.000	No	Yes	2.00
233	4.66	0.82	100.00	3.13	0.58	1.46	11.28	0.00	11.28	4.000	No	Yes	2.00
234	4.68	0.79	100.00	3.16	0.58	1.46	10.76	0.00	10.76	4.000	No	Yes	2.00
235	4.70	0.76	100.00	3.18	0.58	1.45	10.29	0.00	10.29	4.000	No	Yes	2.00
236	4.72	0.74	100.00	3.20	0.58	1.45	10.10	0.00	10.10	4.000	No	Yes	2.00
237	4.74	0.73	100.00	3.20	0.58	1.45	9.82	0.00	9.82	4.000	No	Yes	2.00
238	4.76	0.73	100.00	3.19	0.58	1.45	9.76	0.00	9.76	4.000	No	Yes	2.00
239	4.78	0.74	100.00	3.16	0.58	1.45	10.00	0.00	10.00	4.000	No	Yes	2.00
240	4.80	0.75	100.00	3.13	0.58	1.44	10.20	0.00	10.20	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
241	4.82	0.76	100.00	3.09	0.58	1.44	10.21	0.00	10.21	4.000	No	Yes	2.00
242	4.84	0.77	100.00	3.06	0.58	1.44	10.45	0.00	10.45	4.000	No	Yes	2.00
243	4.86	0.77	100.00	3.04	0.58	1.44	10.33	0.00	10.33	4.000	No	Yes	2.00
244	4.88	0.80	100.00	2.99	0.58	1.43	10.22	0.00	10.22	4.000	No	Yes	2.00
245	4.90	0.86	97.52	2.93	0.58	1.43	11.81	0.00	11.81	4.000	No	Yes	2.00
246	4.92	0.94	91.41	2.86	0.57	1.42	12.63	0.00	12.63	4.000	No	Yes	2.00
247	4.94	1.01	87.68	2.81	0.57	1.42	13.54	0.00	13.54	4.000	No	Yes	2.00
248	4.96	1.08	85.03	2.78	0.57	1.42	14.54	0.00	14.54	4.000	No	Yes	2.00
249	4.98	1.13	83.90	2.76	0.57	1.41	15.32	0.00	15.32	4.000	No	Yes	2.00
250	5.00	1.16	84.00	2.76	0.57	1.41	15.58	0.00	15.58	4.000	No	Yes	2.00
251	5.02	1.15	86.01	2.79	0.57	1.41	15.55	0.00	15.55	4.000	No	Yes	2.00
252	5.04	1.13	88.20	2.82	0.57	1.41	14.90	0.00	14.90	4.000	No	Yes	2.00
253	5.06	1.09	92.48	2.87	0.57	1.40	14.70	0.00	14.70	4.000	No	Yes	2.00
254	5.08	1.08	94.13	2.89	0.57	1.40	13.80	0.00	13.80	4.000	No	Yes	2.00
255	5.11	1.11	93.59	2.88	0.57	1.40	14.58	0.00	14.58	4.000	No	Yes	2.00
256	5.12	1.16	89.38	2.83	0.56	1.39	15.42	0.00	15.42	4.000	No	Yes	2.00
257	5.14	1.21	85.95	2.79	0.56	1.39	15.97	0.00	15.97	4.000	No	Yes	2.00
258	5.16	1.22	84.65	2.77	0.56	1.39	16.20	0.00	16.20	4.000	No	Yes	2.00
259	5.18	1.23	84.52	2.77	0.56	1.39	16.08	0.00	16.08	4.000	No	Yes	2.00
260	5.20	1.30	82.03	2.74	0.56	1.39	16.38	0.00	16.38	4.000	No	Yes	2.00
261	5.22	1.39	78.52	2.69	0.56	1.38	18.56	0.00	18.56	4.000	No	Yes	2.00
262	5.24	1.44	77.08	2.68	0.55	1.37	19.65	0.00	19.65	4.000	No	Yes	2.00
263	5.26	1.38	80.48	2.72	0.56	1.37	18.29	0.00	18.29	4.000	No	Yes	2.00
264	5.28	1.24	87.20	2.80	0.56	1.38	16.30	0.00	16.30	4.000	No	Yes	2.00
265	5.30	1.13	92.54	2.87	0.57	1.38	14.15	0.00	14.15	4.000	No	Yes	2.00
266	5.32	1.11	92.90	2.87	0.57	1.38	13.81	0.00	13.81	4.000	Yes	Yes	2.00
267	5.34	1.25	86.07	2.79	0.57	1.37	15.42	0.00	15.42	4.000	Yes	Yes	2.00
268	5.36	1.60	73.38	2.63	0.56	1.36	19.67	0.00	19.67	4.000	Yes	Yes	2.00
269	5.38	2.03	61.61	2.48	0.54	1.35	27.42	56.81	84.23	4.000	Yes	No	2.00
270	5.40	2.46	52.13	2.36	0.53	1.34	32.34	55.36	87.70	4.000	Yes	No	2.00
271	5.42	2.79	46.97	2.30	0.52	1.33	36.33	54.36	90.69	4.000	Yes	No	2.00
272	5.44	3.09	43.00	2.25	0.51	1.32	40.35	53.41	93.76	4.000	Yes	No	2.00
273	5.46	3.41	39.70	2.21	0.51	1.32	44.02	52.35	96.38	4.000	Yes	No	2.00
274	5.48	3.83	35.51	2.16	0.50	1.31	48.62	50.38	99.00	4.000	Yes	No	2.00
275	5.50	4.41	29.30	2.08	0.49	1.31	55.84	45.78	101.62	4.000	Yes	No	2.00
276	5.52	5.08	22.04	1.99	0.49	1.30	65.88	36.53	102.41	4.000	Yes	No	2.00
277	5.54	6.04	11.88	1.86	0.53	1.32	75.68	12.07	87.75	4.000	Yes	No	2.00
278	5.56	7.02	2.89	1.75	0.51	1.31	93.55	0.00	93.55	4.000	Yes	No	2.00
279	5.58	7.85	0.00	1.67	0.49	1.30	103.28	0.00	103.28	0.142	No	No	0.69
280	5.60	8.10	0.00	1.64	0.49	1.29	105.46	0.00	105.46	0.145	No	No	0.71
281	5.62	7.70	0.00	1.67	0.49	1.29	101.91	0.00	101.91	0.140	No	No	0.68
282	5.64	6.82	0.00	1.71	0.52	1.31	88.98	0.00	88.98	4.000	Yes	No	2.00
283	5.66	5.50	8.12	1.81	0.55	1.33	74.14	2.99	77.13	4.000	Yes	No	2.00
284	5.68	4.15	22.82	2.00	0.53	1.31	52.16	35.80	87.96	4.000	Yes	No	2.00
285	5.70	3.09	42.07	2.24	0.53	1.31	36.29	51.89	88.18	4.000	Yes	No	2.00
286	5.72	2.43	60.59	2.47	0.52	1.31	31.60	57.73	89.32	4.000	Yes	No	2.00
287	5.74	2.02	76.21	2.67	0.53	1.31	26.65	0.00	26.65	4.000	Yes	Yes	2.00
288	5.76	1.61	91.96	2.86	0.55	1.32	20.22	0.00	20.22	4.000	Yes	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
289	5.78	1.31	100.00	3.03	0.56	1.32	16.09	0.00	16.09	4.000	No	Yes	2.00
290	5.80	1.21	100.00	3.08	0.56	1.33	14.95	0.00	14.95	4.000	No	Yes	2.00
291	5.82	1.59	93.55	2.88	0.56	1.32	16.27	0.00	16.27	4.000	Yes	Yes	2.00
292	5.84	2.58	67.66	2.56	0.52	1.30	30.01	58.90	88.91	4.000	Yes	No	2.00
293	5.86	3.76	46.41	2.29	0.48	1.27	50.88	57.85	108.72	4.000	Yes	No	2.00
294	5.88	4.37	35.62	2.16	0.47	1.26	59.50	52.93	112.43	4.000	Yes	No	2.00
295	5.90	4.24	32.95	2.12	0.49	1.27	52.53	48.98	101.51	4.000	Yes	No	2.00
296	5.92	3.77	36.01	2.16	0.51	1.28	46.62	50.32	96.94	4.000	Yes	No	2.00
297	5.94	3.19	46.10	2.29	0.50	1.27	42.56	55.56	98.12	4.000	Yes	No	2.00
298	5.96	2.65	59.05	2.45	0.53	1.29	30.89	57.12	88.01	4.000	Yes	No	2.00
299	5.98	2.03	75.05	2.65	0.53	1.29	26.48	0.00	26.48	4.000	Yes	Yes	2.00
300	6.00	1.60	89.57	2.83	0.55	1.30	19.72	0.00	19.72	4.000	Yes	Yes	2.00
301	6.02	1.23	100.00	3.02	0.57	1.31	14.44	0.00	14.44	4.000	No	Yes	2.00
302	6.05	1.11	100.00	3.11	0.57	1.31	12.55	0.00	12.55	4.000	No	Yes	2.00
303	6.06	1.24	100.00	3.04	0.56	1.30	15.25	0.00	15.25	4.000	No	Yes	2.00
304	6.08	1.38	98.56	2.94	0.55	1.29	18.99	0.00	18.99	4.000	No	Yes	2.00
305	6.10	1.41	94.24	2.89	0.56	1.29	17.60	0.00	17.60	4.000	No	Yes	2.00
306	6.12	1.29	94.88	2.90	0.56	1.29	16.25	0.00	16.25	4.000	No	Yes	2.00
307	6.14	1.20	95.42	2.91	0.57	1.29	14.67	0.00	14.67	4.000	No	Yes	2.00
308	6.16	1.18	94.95	2.90	0.57	1.29	14.44	0.00	14.44	4.000	No	Yes	2.00
309	6.18	1.20	94.07	2.89	0.56	1.29	15.38	0.00	15.38	4.000	No	Yes	2.00
310	6.20	1.24	94.12	2.89	0.56	1.29	15.21	0.00	15.21	4.000	No	Yes	2.00
311	6.22	1.27	95.66	2.91	0.56	1.28	15.97	0.00	15.97	4.000	No	Yes	2.00
312	6.24	1.29	96.86	2.92	0.56	1.28	16.38	0.00	16.38	4.000	No	Yes	2.00
313	6.26	1.29	98.58	2.94	0.56	1.28	15.91	0.00	15.91	4.000	No	Yes	2.00
314	6.28	1.27	100.00	2.97	0.56	1.28	15.77	0.00	15.77	4.000	No	Yes	2.00
315	6.30	1.25	100.00	3.00	0.56	1.28	15.69	0.00	15.69	4.000	No	Yes	2.00
316	6.32	1.23	100.00	3.04	0.56	1.28	15.26	0.00	15.26	4.000	No	Yes	2.00
317	6.34	1.21	100.00	3.07	0.56	1.28	14.81	0.00	14.81	4.000	No	Yes	2.00
318	6.36	1.20	100.00	3.10	0.56	1.27	14.99	0.00	14.99	4.000	No	Yes	2.00
319	6.38	1.20	100.00	3.11	0.56	1.27	14.97	0.00	14.97	4.000	No	Yes	2.00
320	6.40	1.19	100.00	3.12	0.57	1.27	14.55	0.00	14.55	4.000	No	Yes	2.00
321	6.42	1.18	100.00	3.13	0.57	1.27	14.52	0.00	14.52	4.000	No	Yes	2.00
322	6.44	1.18	100.00	3.13	0.56	1.27	14.61	0.00	14.61	4.000	No	Yes	2.00
323	6.46	1.20	100.00	3.11	0.56	1.26	14.61	0.00	14.61	4.000	No	Yes	2.00
324	6.48	1.21	100.00	3.10	0.56	1.26	15.07	0.00	15.07	4.000	No	Yes	2.00
325	6.50	1.22	100.00	3.09	0.56	1.26	14.93	0.00	14.93	4.000	No	Yes	2.00
326	6.52	1.22	100.00	3.08	0.56	1.26	14.79	0.00	14.79	4.000	No	Yes	2.00
327	6.54	1.21	100.00	3.07	0.56	1.26	14.88	0.00	14.88	4.000	No	Yes	2.00
328	6.56	1.23	100.00	3.06	0.56	1.26	14.86	0.00	14.86	4.000	No	Yes	2.00
329	6.58	1.26	100.00	3.04	0.56	1.25	15.30	0.00	15.30	4.000	No	Yes	2.00
330	6.60	1.29	100.00	3.03	0.56	1.25	15.81	0.00	15.81	4.000	No	Yes	2.00
331	6.62	1.31	100.00	3.02	0.56	1.25	15.90	0.00	15.90	4.000	No	Yes	2.00
332	6.64	1.31	100.00	3.02	0.56	1.25	15.91	0.00	15.91	4.000	No	Yes	2.00
333	6.66	1.32	100.00	3.03	0.56	1.24	16.08	0.00	16.08	4.000	No	Yes	2.00
334	6.68	1.31	100.00	3.04	0.56	1.24	15.91	0.00	15.91	4.000	No	Yes	2.00
335	6.70	1.30	100.00	3.06	0.56	1.24	15.63	0.00	15.63	4.000	No	Yes	2.00
336	6.72	1.30	100.00	3.07	0.56	1.24	15.80	0.00	15.80	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
337	6.74	1.28	100.00	3.09	0.56	1.24	15.52	0.00	15.52	4.000	No	Yes	2.00
338	6.76	1.25	100.00	3.11	0.56	1.24	15.13	0.00	15.13	4.000	No	Yes	2.00
339	6.78	1.21	100.00	3.13	0.57	1.24	14.41	0.00	14.41	4.000	No	Yes	2.00
340	6.80	1.17	100.00	3.15	0.57	1.24	14.10	0.00	14.10	4.000	No	Yes	2.00
341	6.82	1.13	100.00	3.16	0.57	1.24	13.71	0.00	13.71	4.000	No	Yes	2.00
342	6.84	0.94	100.00	3.23	0.57	1.23	12.90	0.00	12.90	4.000	No	Yes	2.00
343	6.86	0.89	100.00	3.26	0.59	1.24	7.23	0.00	7.23	4.000	No	Yes	2.00
344	6.88	0.85	100.00	3.29	0.57	1.23	11.94	0.00	11.94	4.000	No	Yes	2.00
345	6.90	0.96	100.00	3.24	0.58	1.23	11.34	0.00	11.34	4.000	No	Yes	2.00
346	6.92	0.92	100.00	3.26	0.58	1.23	11.07	0.00	11.07	4.000	No	Yes	2.00
347	6.94	0.90	100.00	3.27	0.58	1.23	10.70	0.00	10.70	4.000	No	Yes	2.00
348	6.96	0.87	100.00	3.28	0.58	1.23	10.41	0.00	10.41	4.000	No	Yes	2.00
349	6.98	0.86	100.00	3.29	0.58	1.23	10.17	0.00	10.17	4.000	No	Yes	2.00
350	7.00	0.84	100.00	3.29	0.58	1.23	9.93	0.00	9.93	4.000	No	Yes	2.00
351	7.02	0.83	100.00	3.29	0.58	1.23	9.84	0.00	9.84	4.000	No	Yes	2.00
352	7.04	0.83	100.00	3.28	0.58	1.22	9.63	0.00	9.63	4.000	No	Yes	2.00
353	7.06	0.83	100.00	3.27	0.58	1.22	9.84	0.00	9.84	4.000	No	Yes	2.00
354	7.08	0.85	100.00	3.25	0.58	1.22	10.07	0.00	10.07	4.000	No	Yes	2.00
355	7.10	0.86	100.00	3.23	0.58	1.22	10.25	0.00	10.25	4.000	No	Yes	2.00
356	7.12	0.87	100.00	3.23	0.58	1.22	10.20	0.00	10.20	4.000	No	Yes	2.00
357	7.14	0.87	100.00	3.23	0.58	1.22	10.13	0.00	10.13	4.000	No	Yes	2.00
358	7.16	0.88	100.00	3.23	0.58	1.21	10.29	0.00	10.29	4.000	No	Yes	2.00
359	7.19	0.90	100.00	3.22	0.58	1.21	10.63	0.00	10.63	4.000	No	Yes	2.00
360	7.20	0.91	100.00	3.22	0.58	1.21	10.59	0.00	10.59	4.000	No	Yes	2.00
361	7.22	0.92	100.00	3.22	0.58	1.21	10.77	0.00	10.77	4.000	No	Yes	2.00
362	7.24	0.93	100.00	3.22	0.58	1.21	10.90	0.00	10.90	4.000	No	Yes	2.00
363	7.26	0.95	100.00	3.21	0.58	1.21	10.99	0.00	10.99	4.000	No	Yes	2.00
364	7.28	0.97	100.00	3.20	0.58	1.20	11.44	0.00	11.44	4.000	No	Yes	2.00
365	7.31	1.00	100.00	3.18	0.58	1.20	11.45	0.00	11.45	4.000	No	Yes	2.00
366	7.32	1.02	100.00	3.16	0.57	1.20	11.99	0.00	11.99	4.000	No	Yes	2.00
367	7.34	1.06	100.00	3.14	0.57	1.20	12.27	0.00	12.27	4.000	No	Yes	2.00
368	7.36	1.09	100.00	3.12	0.57	1.20	12.55	0.00	12.55	4.000	No	Yes	2.00
369	7.38	1.15	100.00	3.08	0.57	1.19	13.22	0.00	13.22	4.000	No	Yes	2.00
370	7.41	1.23	100.00	3.04	0.57	1.19	14.36	0.00	14.36	4.000	No	Yes	2.00
371	7.42	1.30	100.00	3.01	0.56	1.19	15.22	0.00	15.22	4.000	No	Yes	2.00
372	7.44	1.33	100.00	3.00	0.56	1.19	15.39	0.00	15.39	4.000	No	Yes	2.00
373	7.46	1.34	100.00	3.00	0.56	1.18	15.48	0.00	15.48	4.000	No	Yes	2.00
374	7.48	1.33	100.00	3.02	0.56	1.18	15.54	0.00	15.54	4.000	No	Yes	2.00
375	7.50	1.29	100.00	3.04	0.56	1.18	14.82	0.00	14.82	4.000	No	Yes	2.00
376	7.52	1.23	100.00	3.09	0.57	1.18	14.18	0.00	14.18	4.000	No	Yes	2.00
377	7.54	1.17	100.00	3.12	0.57	1.18	13.46	0.00	13.46	4.000	No	Yes	2.00
378	7.56	1.13	100.00	3.15	0.57	1.18	12.80	0.00	12.80	4.000	No	Yes	2.00
379	7.58	1.09	100.00	3.18	0.57	1.18	12.46	0.00	12.46	4.000	No	Yes	2.00
380	7.60	1.06	100.00	3.20	0.57	1.18	12.12	0.00	12.12	4.000	No	Yes	2.00
381	7.62	1.02	100.00	3.22	0.58	1.18	11.67	0.00	11.67	4.000	No	Yes	2.00
382	7.64	1.00	100.00	3.24	0.58	1.18	11.34	0.00	11.34	4.000	No	Yes	2.00
383	7.66	0.99	100.00	3.24	0.58	1.18	11.11	0.00	11.11	4.000	No	Yes	2.00
384	7.68	1.01	100.00	3.22	0.58	1.17	11.57	0.00	11.57	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
385	7.70	1.03	100.00	3.21	0.58	1.17	11.72	0.00	11.72	4.000	No	Yes	2.00
386	7.72	1.03	100.00	3.21	0.58	1.17	11.89	0.00	11.89	4.000	No	Yes	2.00
387	7.74	1.03	100.00	3.21	0.58	1.17	11.61	0.00	11.61	4.000	No	Yes	2.00
388	7.76	1.03	100.00	3.21	0.58	1.17	11.72	0.00	11.72	4.000	No	Yes	2.00
389	7.78	1.06	100.00	3.20	0.58	1.17	11.79	0.00	11.79	4.000	No	Yes	2.00
390	7.80	1.12	100.00	3.16	0.57	1.16	12.38	0.00	12.38	4.000	No	Yes	2.00
391	7.82	1.18	100.00	3.12	0.57	1.16	13.70	0.00	13.70	4.000	No	Yes	2.00
392	7.84	1.22	100.00	3.10	0.57	1.16	13.79	0.00	13.79	4.000	No	Yes	2.00
393	7.86	1.22	100.00	3.11	0.57	1.16	13.74	0.00	13.74	4.000	No	Yes	2.00
394	7.88	1.22	100.00	3.12	0.57	1.16	13.65	0.00	13.65	4.000	No	Yes	2.00
395	7.90	1.24	100.00	3.12	0.57	1.16	13.70	0.00	13.70	4.000	No	Yes	2.00
396	7.92	1.28	100.00	3.10	0.57	1.15	14.34	0.00	14.34	4.000	No	Yes	2.00
397	7.94	1.32	100.00	3.10	0.56	1.15	14.93	0.00	14.93	4.000	No	Yes	2.00
398	7.96	1.34	100.00	3.10	0.56	1.15	15.01	0.00	15.01	4.000	No	Yes	2.00
399	7.98	1.35	100.00	3.10	0.56	1.15	15.10	0.00	15.10	4.000	No	Yes	2.00
400	8.01	1.35	100.00	3.11	0.56	1.15	15.20	0.00	15.20	4.000	No	Yes	2.00
401	8.02	1.32	100.00	3.12	0.56	1.15	14.90	0.00	14.90	4.000	No	Yes	2.00
402	8.04	1.31	100.00	3.13	0.57	1.15	14.11	0.00	14.11	4.000	No	Yes	2.00
403	8.06	1.30	100.00	3.13	0.56	1.14	14.64	0.00	14.64	4.000	No	Yes	2.00
404	8.08	1.30	100.00	3.12	0.57	1.14	14.52	0.00	14.52	4.000	No	Yes	2.00
405	8.10	1.28	100.00	3.13	0.57	1.14	14.26	0.00	14.26	4.000	No	Yes	2.00
406	8.12	1.24	100.00	3.15	0.57	1.14	13.79	0.00	13.79	4.000	No	Yes	2.00
407	8.15	1.21	100.00	3.16	0.57	1.14	13.34	0.00	13.34	4.000	No	Yes	2.00
408	8.17	1.21	100.00	3.16	0.57	1.14	13.16	0.00	13.16	4.000	No	Yes	2.00
409	8.18	1.24	100.00	3.14	0.57	1.14	13.75	0.00	13.75	4.000	No	Yes	2.00
410	8.20	1.28	100.00	3.12	0.57	1.13	14.17	0.00	14.17	4.000	No	Yes	2.00
411	8.22	1.31	100.00	3.10	0.57	1.13	14.57	0.00	14.57	4.000	No	Yes	2.00
412	8.24	1.33	100.00	3.09	0.56	1.13	14.70	0.00	14.70	4.000	No	Yes	2.00
413	8.26	1.33	100.00	3.09	0.56	1.13	14.73	0.00	14.73	4.000	No	Yes	2.00
414	8.28	1.32	100.00	3.11	0.57	1.13	14.50	0.00	14.50	4.000	No	Yes	2.00
415	8.30	1.32	100.00	3.11	0.57	1.13	14.20	0.00	14.20	4.000	No	Yes	2.00
416	8.32	1.33	100.00	3.12	0.56	1.13	14.67	0.00	14.67	4.000	No	Yes	2.00
417	8.34	1.34	100.00	3.12	0.56	1.12	14.78	0.00	14.78	4.000	No	Yes	2.00
418	8.36	1.32	100.00	3.13	0.57	1.12	14.40	0.00	14.40	4.000	No	Yes	2.00
419	8.38	1.31	100.00	3.13	0.57	1.12	14.22	0.00	14.22	4.000	No	Yes	2.00
420	8.40	1.31	100.00	3.13	0.57	1.12	14.33	0.00	14.33	4.000	No	Yes	2.00
421	8.42	1.31	100.00	3.12	0.57	1.12	14.24	0.00	14.24	4.000	No	Yes	2.00
422	8.44	1.32	100.00	3.12	0.57	1.12	14.32	0.00	14.32	4.000	No	Yes	2.00
423	8.46	1.31	100.00	3.12	0.57	1.12	14.40	0.00	14.40	4.000	No	Yes	2.00
424	8.48	1.29	100.00	3.14	0.57	1.12	14.00	0.00	14.00	4.000	No	Yes	2.00
425	8.50	1.26	100.00	3.15	0.57	1.12	13.57	0.00	13.57	4.000	No	Yes	2.00
426	8.52	1.24	100.00	3.16	0.57	1.11	13.47	0.00	13.47	4.000	No	Yes	2.00
427	8.54	1.22	100.00	3.17	0.57	1.11	13.15	0.00	13.15	4.000	No	Yes	2.00
428	8.56	1.21	100.00	3.17	0.57	1.11	13.03	0.00	13.03	4.000	No	Yes	2.00
429	8.58	1.20	100.00	3.18	0.57	1.11	13.11	0.00	13.11	4.000	No	Yes	2.00
430	8.60	1.18	100.00	3.18	0.57	1.11	12.66	0.00	12.66	4.000	No	Yes	2.00
431	8.62	1.16	100.00	3.20	0.57	1.11	12.54	0.00	12.54	4.000	No	Yes	2.00
432	8.64	1.14	100.00	3.21	0.57	1.11	12.28	0.00	12.28	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
433	8.66	1.11	100.00	3.23	0.58	1.11	11.88	0.00	11.88	4.000	No	Yes	2.00
434	8.68	1.09	100.00	3.24	0.58	1.11	11.53	0.00	11.53	4.000	No	Yes	2.00
435	8.70	1.07	100.00	3.25	0.58	1.10	11.67	0.00	11.67	4.000	No	Yes	2.00
436	8.72	1.08	100.00	3.25	0.58	1.10	11.32	0.00	11.32	4.000	No	Yes	2.00
437	8.74	1.10	100.00	3.24	0.58	1.10	11.69	0.00	11.69	4.000	No	Yes	2.00
438	8.76	1.15	100.00	3.21	0.57	1.10	12.21	0.00	12.21	4.000	No	Yes	2.00
439	8.78	1.19	100.00	3.18	0.57	1.10	12.84	0.00	12.84	4.000	No	Yes	2.00
440	8.80	1.23	100.00	3.16	0.57	1.10	13.15	0.00	13.15	4.000	No	Yes	2.00
441	8.82	1.27	100.00	3.14	0.57	1.10	13.42	0.00	13.42	4.000	No	Yes	2.00
442	8.84	1.30	100.00	3.13	0.57	1.09	14.01	0.00	14.01	4.000	No	Yes	2.00
443	8.86	1.33	100.00	3.12	0.57	1.09	13.99	0.00	13.99	4.000	No	Yes	2.00
444	8.88	1.34	100.00	3.12	0.57	1.09	14.27	0.00	14.27	4.000	No	Yes	2.00
445	8.90	1.36	100.00	3.12	0.57	1.09	14.31	0.00	14.31	4.000	No	Yes	2.00
446	8.92	1.38	100.00	3.12	0.56	1.09	14.67	0.00	14.67	4.000	No	Yes	2.00
447	8.94	1.40	100.00	3.11	0.56	1.09	14.80	0.00	14.80	4.000	No	Yes	2.00
448	8.96	1.40	100.00	3.11	0.56	1.09	14.93	0.00	14.93	4.000	No	Yes	2.00
449	8.98	1.39	100.00	3.12	0.56	1.09	14.74	0.00	14.74	4.000	No	Yes	2.00
450	9.00	1.36	100.00	3.13	0.57	1.08	14.32	0.00	14.32	4.000	No	Yes	2.00
451	9.02	1.32	100.00	3.14	0.57	1.08	13.98	0.00	13.98	4.000	No	Yes	2.00
452	9.04	1.27	100.00	3.16	0.57	1.08	13.56	0.00	13.56	4.000	No	Yes	2.00
453	9.06	1.21	100.00	3.18	0.57	1.08	12.54	0.00	12.54	4.000	No	Yes	2.00
454	9.08	1.16	100.00	3.19	0.57	1.08	12.03	0.00	12.03	4.000	No	Yes	2.00
455	9.10	1.12	100.00	3.20	0.58	1.08	11.83	0.00	11.83	4.000	No	Yes	2.00
456	9.12	1.11	100.00	3.19	0.58	1.08	11.49	0.00	11.49	4.000	No	Yes	2.00
457	9.14	1.09	100.00	3.19	0.58	1.08	11.45	0.00	11.45	4.000	No	Yes	2.00
458	9.16	1.09	100.00	3.18	0.58	1.08	11.36	0.00	11.36	4.000	No	Yes	2.00
459	9.18	1.10	100.00	3.18	0.58	1.08	11.33	0.00	11.33	4.000	No	Yes	2.00
460	9.20	1.13	100.00	3.16	0.58	1.07	11.66	0.00	11.66	4.000	No	Yes	2.00
461	9.22	1.19	100.00	3.13	0.57	1.07	12.29	0.00	12.29	4.000	No	Yes	2.00
462	9.24	1.27	100.00	3.09	0.57	1.07	13.31	0.00	13.31	4.000	No	Yes	2.00
463	9.26	1.32	100.00	3.07	0.57	1.07	13.94	0.00	13.94	4.000	No	Yes	2.00
464	9.29	1.34	100.00	3.06	0.57	1.07	13.89	0.00	13.89	4.000	No	Yes	2.00
465	9.30	1.35	100.00	3.05	0.57	1.07	13.91	0.00	13.91	4.000	No	Yes	2.00
466	9.32	1.39	100.00	3.03	0.57	1.07	14.29	0.00	14.29	4.000	No	Yes	2.00
467	9.34	1.47	100.00	3.00	0.56	1.07	15.19	0.00	15.19	4.000	No	Yes	2.00
468	9.36	1.55	100.00	2.97	0.56	1.06	16.15	0.00	16.15	4.000	No	Yes	2.00
469	9.38	1.61	100.00	2.97	0.56	1.06	16.95	0.00	16.95	4.000	No	Yes	2.00
470	9.40	1.65	100.00	2.99	0.56	1.06	16.90	0.00	16.90	4.000	No	Yes	2.00
471	9.42	1.68	100.00	3.01	0.55	1.06	17.42	0.00	17.42	4.000	No	Yes	2.00
472	9.44	1.70	100.00	3.03	0.55	1.06	17.72	0.00	17.72	4.000	No	Yes	2.00
473	9.46	1.70	100.00	3.06	0.55	1.06	17.46	0.00	17.46	4.000	No	Yes	2.00
474	9.48	1.68	100.00	3.10	0.55	1.06	17.54	0.00	17.54	4.000	No	Yes	2.00
475	9.50	1.63	100.00	3.14	0.56	1.06	16.90	0.00	16.90	4.000	No	Yes	2.00
476	9.52	1.57	100.00	3.19	0.56	1.06	15.86	0.00	15.86	4.000	No	Yes	2.00
477	9.54	1.54	100.00	3.21	0.56	1.05	15.57	0.00	15.57	4.000	No	Yes	2.00
478	9.56	1.55	100.00	3.21	0.56	1.05	16.13	0.00	16.13	4.000	No	Yes	2.00
479	9.58	1.55	100.00	3.21	0.56	1.05	16.10	0.00	16.10	4.000	No	Yes	2.00
480	9.60	1.54	100.00	3.21	0.56	1.05	15.52	0.00	15.52	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
481	9.62	1.54	100.00	3.21	0.56	1.05	15.78	0.00	15.78	4.000	No	Yes	2.00
482	9.64	1.56	100.00	3.19	0.56	1.05	15.86	0.00	15.86	4.000	No	Yes	2.00
483	9.66	1.57	100.00	3.17	0.56	1.05	16.08	0.00	16.08	4.000	No	Yes	2.00
484	9.68	1.62	100.00	3.13	0.56	1.05	16.20	0.00	16.20	4.000	No	Yes	2.00
485	9.70	1.66	100.00	3.10	0.56	1.04	17.05	0.00	17.05	4.000	No	Yes	2.00
486	9.72	1.71	100.00	3.08	0.55	1.04	17.51	0.00	17.51	4.000	No	Yes	2.00
487	9.74	1.75	100.00	3.06	0.55	1.04	17.68	0.00	17.68	4.000	No	Yes	2.00
488	9.76	1.78	100.00	3.04	0.55	1.04	18.08	0.00	18.08	4.000	No	Yes	2.00
489	9.78	1.81	100.00	3.03	0.55	1.04	18.42	0.00	18.42	4.000	No	Yes	2.00
490	9.80	1.84	100.00	3.02	0.55	1.04	18.58	0.00	18.58	4.000	No	Yes	2.00
491	9.82	1.88	100.00	3.01	0.55	1.04	18.94	0.00	18.94	4.000	No	Yes	2.00
492	9.84	1.92	100.00	2.99	0.55	1.04	19.42	0.00	19.42	4.000	No	Yes	2.00
493	9.86	1.93	100.00	2.99	0.55	1.04	19.70	0.00	19.70	4.000	No	Yes	2.00
494	9.88	1.93	100.00	3.00	0.55	1.03	19.46	0.00	19.46	4.000	No	Yes	2.00
495	9.90	1.89	100.00	3.02	0.55	1.03	19.27	0.00	19.27	4.000	No	Yes	2.00
496	9.92	1.86	100.00	3.05	0.55	1.03	18.51	0.00	18.51	4.000	No	Yes	2.00
497	9.94	1.79	100.00	3.08	0.55	1.03	18.25	0.00	18.25	4.000	No	Yes	2.00
498	9.96	1.71	100.00	3.11	0.56	1.03	17.28	0.00	17.28	4.000	No	Yes	2.00
499	9.98	1.62	100.00	3.15	0.56	1.03	16.09	0.00	16.09	4.000	No	Yes	2.00
500	10.00	1.48	100.00	3.20	0.56	1.03	15.38	0.00	15.38	4.000	No	Yes	2.00
501	10.03	1.34	100.00	3.26	0.57	1.03	12.91	0.00	12.91	4.000	No	Yes	2.00
502	10.04	1.19	100.00	3.32	0.58	1.03	11.85	0.00	11.85	4.000	No	Yes	2.00
503	10.06	1.10	100.00	3.36	0.58	1.03	10.77	0.00	10.77	4.000	No	Yes	2.00
504	10.08	1.02	100.00	3.40	0.58	1.03	10.16	0.00	10.16	4.000	No	Yes	2.00
505	10.10	0.98	100.00	3.41	0.58	1.02	9.53	0.00	9.53	4.000	No	Yes	2.00
506	10.12	0.94	100.00	3.41	0.58	1.02	9.40	0.00	9.40	4.000	No	Yes	2.00
507	10.14	0.91	100.00	3.41	0.59	1.02	8.96	0.00	8.96	4.000	No	Yes	2.00
508	10.16	0.88	100.00	3.40	0.59	1.02	8.52	0.00	8.52	4.000	No	Yes	2.00
509	10.18	0.87	100.00	3.38	0.59	1.02	8.49	0.00	8.49	4.000	No	Yes	2.00
510	10.20	0.85	100.00	3.36	0.59	1.02	8.50	0.00	8.50	4.000	No	Yes	2.00
511	10.22	0.83	100.00	3.34	0.59	1.02	8.05	0.00	8.05	4.000	No	Yes	2.00
512	10.24	0.80	100.00	3.32	0.59	1.02	7.77	0.00	7.77	4.000	No	Yes	2.00
513	10.26	0.81	100.00	3.29	0.59	1.02	7.81	0.00	7.81	4.000	No	Yes	2.00
514	10.28	0.83	100.00	3.23	0.59	1.02	8.04	0.00	8.04	4.000	No	Yes	2.00
515	10.30	0.88	100.00	3.16	0.59	1.02	8.60	0.00	8.60	4.000	No	Yes	2.00
516	10.32	0.91	100.00	3.11	0.59	1.01	9.09	0.00	9.09	4.000	No	Yes	2.00
517	10.34	0.92	100.00	3.09	0.59	1.01	9.08	0.00	9.08	4.000	No	Yes	2.00
518	10.36	0.92	100.00	3.10	0.59	1.01	8.81	0.00	8.81	4.000	No	Yes	2.00
519	10.38	0.97	100.00	3.08	0.59	1.01	9.11	0.00	9.11	4.000	No	Yes	2.00
520	10.40	1.05	100.00	3.02	0.58	1.01	10.44	0.00	10.44	4.000	No	Yes	2.00
521	10.42	1.09	100.00	3.00	0.58	1.01	11.14	0.00	11.14	4.000	No	Yes	2.00
522	10.44	1.10	100.00	3.01	0.58	1.01	10.34	0.00	10.34	4.000	No	Yes	2.00
523	10.46	1.17	100.00	2.97	0.58	1.01	10.67	0.00	10.67	4.000	No	Yes	2.00
524	10.48	1.36	91.12	2.85	0.57	1.01	13.40	0.00	13.40	4.000	No	Yes	2.00
525	10.50	1.58	82.42	2.74	0.57	1.01	15.90	0.00	15.90	4.000	No	Yes	2.00
526	10.52	1.71	81.32	2.73	0.56	1.01	17.18	0.00	17.18	4.000	No	Yes	2.00
527	10.54	1.79	80.69	2.72	0.56	1.01	17.10	0.00	17.10	4.000	No	Yes	2.00
528	10.56	1.84	81.61	2.73	0.56	1.00	18.33	0.00	18.33	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
529	10.58	1.90	82.11	2.74	0.56	1.00	18.60	0.00	18.60	4.000	No	Yes	2.00
530	10.60	1.92	87.11	2.80	0.55	1.00	18.84	0.00	18.84	4.000	No	Yes	2.00
531	10.62	1.93	92.16	2.86	0.55	1.00	18.79	0.00	18.79	4.000	No	Yes	2.00
532	10.64	1.91	97.28	2.93	0.55	1.00	18.80	0.00	18.80	4.000	No	Yes	2.00
533	10.66	1.89	100.00	2.97	0.55	1.00	18.23	0.00	18.23	4.000	No	Yes	2.00
534	10.68	1.84	100.00	3.03	0.55	1.00	18.10	0.00	18.10	4.000	No	Yes	2.00
535	10.70	1.80	100.00	3.06	0.55	1.00	17.53	0.00	17.53	4.000	No	Yes	2.00
536	10.72	1.72	100.00	3.11	0.56	1.00	16.85	0.00	16.85	4.000	No	Yes	2.00
537	10.74	1.62	100.00	3.16	0.56	1.00	15.70	0.00	15.70	4.000	No	Yes	2.00
538	10.76	1.48	100.00	3.23	0.57	1.00	14.50	0.00	14.50	4.000	No	Yes	2.00
539	10.78	1.34	100.00	3.30	0.57	0.99	12.73	0.00	12.73	4.000	No	Yes	2.00
540	10.80	1.20	100.00	3.38	0.58	0.99	11.52	0.00	11.52	4.000	No	Yes	2.00
541	10.82	1.16	100.00	3.39	0.58	0.99	10.37	0.00	10.37	4.000	No	Yes	2.00
542	10.84	1.13	100.00	3.37	0.58	0.99	11.42	0.00	11.42	4.000	No	Yes	2.00
543	10.86	1.12	100.00	3.33	0.58	0.99	10.74	0.00	10.74	4.000	No	Yes	2.00
544	10.88	1.06	100.00	3.34	0.58	0.99	10.09	0.00	10.09	4.000	No	Yes	2.00
545	10.90	0.98	100.00	3.35	0.58	0.99	9.46	0.00	9.46	4.000	No	Yes	2.00
546	10.92	0.93	100.00	3.36	0.59	0.99	8.52	0.00	8.52	4.000	No	Yes	2.00
547	10.94	0.94	100.00	3.32	0.59	0.99	8.47	0.00	8.47	4.000	No	Yes	2.00
548	10.96	0.98	100.00	3.25	0.58	0.99	9.68	0.00	9.68	4.000	No	Yes	2.00
549	10.98	1.00	100.00	3.20	0.58	0.98	9.61	0.00	9.61	4.000	No	Yes	2.00
550	11.00	0.99	100.00	3.19	0.59	0.98	9.21	0.00	9.21	4.000	No	Yes	2.00
551	11.03	0.99	100.00	3.17	0.59	0.98	9.24	0.00	9.24	4.000	No	Yes	2.00
552	11.04	1.03	100.00	3.11	0.58	0.98	9.69	0.00	9.69	4.000	No	Yes	2.00
553	11.06	1.07	100.00	3.06	0.58	0.98	10.27	0.00	10.27	4.000	No	Yes	2.00
554	11.08	1.10	100.00	3.03	0.58	0.98	10.33	0.00	10.33	4.000	No	Yes	2.00
555	11.10	1.10	100.00	3.02	0.58	0.98	10.49	0.00	10.49	4.000	No	Yes	2.00
556	11.12	1.11	100.00	3.03	0.58	0.98	10.46	0.00	10.46	4.000	No	Yes	2.00
557	11.14	1.10	100.00	3.04	0.58	0.98	10.45	0.00	10.45	4.000	No	Yes	2.00
558	11.16	1.10	100.00	3.06	0.58	0.98	10.24	0.00	10.24	4.000	No	Yes	2.00
559	11.18	1.10	100.00	3.07	0.58	0.98	10.33	0.00	10.33	4.000	No	Yes	2.00
560	11.20	1.13	100.00	3.08	0.58	0.98	10.50	0.00	10.50	4.000	No	Yes	2.00
561	11.22	1.16	100.00	3.08	0.58	0.98	10.91	0.00	10.91	4.000	No	Yes	2.00
562	11.24	1.21	100.00	3.05	0.58	0.98	11.13	0.00	11.13	4.000	No	Yes	2.00
563	11.26	1.29	100.00	3.00	0.57	0.97	11.91	0.00	11.91	4.000	No	Yes	2.00
564	11.28	1.40	97.94	2.94	0.57	0.97	13.17	0.00	13.17	4.000	No	Yes	2.00
565	11.30	1.53	92.24	2.87	0.57	0.97	14.28	0.00	14.28	4.000	No	Yes	2.00
566	11.32	1.63	88.91	2.82	0.56	0.97	15.69	0.00	15.69	4.000	No	Yes	2.00
567	11.34	1.69	87.78	2.81	0.56	0.97	15.88	0.00	15.88	4.000	No	Yes	2.00
568	11.36	1.70	90.11	2.84	0.56	0.97	16.10	0.00	16.10	4.000	No	Yes	2.00
569	11.38	1.69	94.12	2.89	0.56	0.97	15.95	0.00	15.95	4.000	No	Yes	2.00
570	11.40	1.66	98.37	2.94	0.56	0.97	15.42	0.00	15.42	4.000	No	Yes	2.00
571	11.42	1.65	100.00	2.98	0.56	0.97	15.21	0.00	15.21	4.000	No	Yes	2.00
572	11.44	1.64	100.00	3.01	0.56	0.97	15.65	0.00	15.65	4.000	No	Yes	2.00
573	11.46	1.62	100.00	3.04	0.56	0.97	15.11	0.00	15.11	4.000	No	Yes	2.00
574	11.48	1.59	100.00	3.08	0.56	0.97	14.79	0.00	14.79	4.000	No	Yes	2.00
575	11.50	1.57	100.00	3.10	0.56	0.97	14.72	0.00	14.72	4.000	No	Yes	2.00
576	11.52	1.54	100.00	3.13	0.57	0.96	14.35	0.00	14.35	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
577	11.54	1.49	100.00	3.16	0.57	0.96	13.86	0.00	13.86	4.000	No	Yes	2.00
578	11.56	1.46	100.00	3.18	0.57	0.96	13.49	0.00	13.49	4.000	No	Yes	2.00
579	11.58	1.44	100.00	3.19	0.57	0.96	13.25	0.00	13.25	4.000	No	Yes	2.00
580	11.60	1.42	100.00	3.20	0.57	0.96	13.25	0.00	13.25	4.000	No	Yes	2.00
581	11.62	1.39	100.00	3.21	0.57	0.96	12.90	0.00	12.90	4.000	No	Yes	2.00
582	11.64	1.35	100.00	3.23	0.57	0.96	12.32	0.00	12.32	4.000	No	Yes	2.00
583	11.66	1.30	100.00	3.24	0.57	0.96	12.11	0.00	12.11	4.000	No	Yes	2.00
584	11.68	1.29	100.00	3.25	0.58	0.96	11.71	0.00	11.71	4.000	No	Yes	2.00
585	11.70	1.28	100.00	3.25	0.58	0.96	11.74	0.00	11.74	4.000	No	Yes	2.00
586	11.72	1.28	100.00	3.24	0.57	0.96	11.90	0.00	11.90	4.000	No	Yes	2.00
587	11.74	1.28	100.00	3.24	0.58	0.95	11.82	0.00	11.82	4.000	No	Yes	2.00
588	11.76	1.27	100.00	3.23	0.58	0.95	11.61	0.00	11.61	4.000	No	Yes	2.00
589	11.78	1.23	100.00	3.24	0.58	0.95	11.44	0.00	11.44	4.000	No	Yes	2.00
590	11.80	1.15	100.00	3.28	0.58	0.95	10.69	0.00	10.69	4.000	No	Yes	2.00
591	11.82	1.10	100.00	3.31	0.58	0.95	9.50	0.00	9.50	4.000	No	Yes	2.00
592	11.84	1.04	100.00	3.35	0.58	0.95	9.85	0.00	9.85	4.000	No	Yes	2.00
593	11.86	1.01	100.00	3.37	0.59	0.95	8.94	0.00	8.94	4.000	No	Yes	2.00
594	11.88	0.96	100.00	3.40	0.59	0.95	8.65	0.00	8.65	4.000	No	Yes	2.00
595	11.90	0.94	100.00	3.40	0.59	0.95	8.51	0.00	8.51	4.000	No	Yes	2.00
596	11.92	0.92	100.00	3.40	0.59	0.95	8.26	0.00	8.26	4.000	No	Yes	2.00
597	11.94	0.92	100.00	3.37	0.59	0.95	8.08	0.00	8.08	4.000	No	Yes	2.00
598	11.96	0.95	100.00	3.30	0.59	0.94	8.43	0.00	8.43	4.000	No	Yes	2.00
599	11.99	1.02	100.00	3.21	0.59	0.94	9.13	0.00	9.13	4.000	No	Yes	2.00
600	12.00	1.13	100.00	3.10	0.58	0.94	10.18	0.00	10.18	4.000	No	Yes	2.00
601	12.02	1.26	100.00	3.00	0.58	0.94	11.25	0.00	11.25	4.000	No	Yes	2.00
602	12.04	1.43	96.44	2.92	0.57	0.94	12.93	0.00	12.93	4.000	No	Yes	2.00
603	12.06	1.59	91.82	2.86	0.57	0.94	14.81	0.00	14.81	4.000	No	Yes	2.00
604	12.08	1.66	91.43	2.86	0.56	0.94	15.57	0.00	15.57	4.000	No	Yes	2.00
605	12.10	1.66	94.48	2.89	0.56	0.94	15.05	0.00	15.05	4.000	No	Yes	2.00
606	12.12	1.62	98.92	2.95	0.56	0.94	14.67	0.00	14.67	4.000	No	Yes	2.00
607	12.14	1.60	100.00	3.00	0.57	0.94	14.58	0.00	14.58	4.000	No	Yes	2.00
608	12.16	1.58	100.00	3.05	0.57	0.94	14.39	0.00	14.39	4.000	No	Yes	2.00
609	12.18	1.55	100.00	3.11	0.57	0.94	14.03	0.00	14.03	4.000	No	Yes	2.00
610	12.20	1.53	100.00	3.16	0.57	0.94	13.67	0.00	13.67	4.000	No	Yes	2.00
611	12.22	1.51	100.00	3.19	0.57	0.94	13.72	0.00	13.72	4.000	No	Yes	2.00
612	12.24	1.51	100.00	3.20	0.57	0.94	13.64	0.00	13.64	4.000	No	Yes	2.00
613	12.26	1.51	100.00	3.21	0.57	0.94	13.67	0.00	13.67	4.000	No	Yes	2.00
614	12.28	1.51	100.00	3.22	0.57	0.93	13.67	0.00	13.67	4.000	No	Yes	2.00
615	12.30	1.52	100.00	3.21	0.57	0.93	13.61	0.00	13.61	4.000	No	Yes	2.00
616	12.32	1.53	100.00	3.20	0.57	0.93	13.85	0.00	13.85	4.000	No	Yes	2.00
617	12.34	1.57	100.00	3.17	0.57	0.93	13.94	0.00	13.94	4.000	No	Yes	2.00
618	12.36	1.64	100.00	3.14	0.57	0.93	14.55	0.00	14.55	4.000	No	Yes	2.00
619	12.38	1.74	100.00	3.10	0.56	0.93	15.87	0.00	15.87	4.000	No	Yes	2.00
620	12.40	1.84	100.00	3.07	0.56	0.93	16.55	0.00	16.55	4.000	No	Yes	2.00
621	12.42	1.91	100.00	3.05	0.55	0.93	17.38	0.00	17.38	4.000	No	Yes	2.00
622	12.44	1.96	100.00	3.04	0.55	0.93	17.82	0.00	17.82	4.000	No	Yes	2.00
623	12.46	1.96	100.00	3.06	0.55	0.93	17.88	0.00	17.88	4.000	No	Yes	2.00
624	12.48	1.93	100.00	3.08	0.56	0.93	17.23	0.00	17.23	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
625	12.50	1.91	100.00	3.10	0.56	0.93	17.08	0.00	17.08	4.000	No	Yes	2.00
626	12.52	1.89	100.00	3.12	0.56	0.93	17.12	0.00	17.12	4.000	No	Yes	2.00
627	12.54	1.88	100.00	3.14	0.56	0.93	16.81	0.00	16.81	4.000	No	Yes	2.00
628	12.56	1.86	100.00	3.17	0.56	0.92	16.62	0.00	16.62	4.000	No	Yes	2.00
629	12.58	1.83	100.00	3.18	0.56	0.92	16.42	0.00	16.42	4.000	No	Yes	2.00
630	12.61	1.81	100.00	3.19	0.56	0.92	16.11	0.00	16.11	4.000	No	Yes	2.00
631	12.62	1.81	100.00	3.19	0.56	0.92	16.02	0.00	16.02	4.000	No	Yes	2.00
632	12.64	1.83	100.00	3.17	0.56	0.92	16.38	0.00	16.38	4.000	No	Yes	2.00
633	12.66	1.86	100.00	3.16	0.56	0.92	16.69	0.00	16.69	4.000	No	Yes	2.00
634	12.68	1.87	100.00	3.15	0.56	0.92	16.69	0.00	16.69	4.000	No	Yes	2.00
635	12.70	1.87	100.00	3.14	0.56	0.92	16.58	0.00	16.58	4.000	No	Yes	2.00
636	12.72	1.89	100.00	3.13	0.56	0.92	16.67	0.00	16.67	4.000	No	Yes	2.00
637	12.74	1.92	100.00	3.12	0.56	0.92	17.28	0.00	17.28	4.000	No	Yes	2.00
638	12.76	1.95	100.00	3.11	0.56	0.92	17.16	0.00	17.16	4.000	No	Yes	2.00
639	12.78	1.98	100.00	3.11	0.55	0.92	17.68	0.00	17.68	4.000	No	Yes	2.00
640	12.80	2.02	100.00	3.09	0.55	0.92	17.87	0.00	17.87	4.000	No	Yes	2.00
641	12.82	2.05	100.00	3.09	0.55	0.92	18.22	0.00	18.22	4.000	No	Yes	2.00
642	12.84	2.06	100.00	3.09	0.55	0.91	18.45	0.00	18.45	4.000	No	Yes	2.00
643	12.86	2.05	100.00	3.10	0.55	0.91	18.09	0.00	18.09	4.000	No	Yes	2.00
644	12.88	2.04	100.00	3.12	0.55	0.91	17.99	0.00	17.99	4.000	No	Yes	2.00
645	12.90	2.04	100.00	3.12	0.55	0.91	18.04	0.00	18.04	4.000	No	Yes	2.00
646	12.92	2.04	100.00	3.13	0.55	0.91	18.02	0.00	18.02	4.000	No	Yes	2.00
647	12.94	2.02	100.00	3.14	0.55	0.91	17.91	0.00	17.91	4.000	No	Yes	2.00
648	12.96	2.00	100.00	3.15	0.55	0.91	17.48	0.00	17.48	4.000	No	Yes	2.00
649	12.98	1.99	100.00	3.15	0.55	0.91	17.49	0.00	17.49	4.000	No	Yes	2.00
650	13.00	1.99	100.00	3.14	0.55	0.91	17.68	0.00	17.68	4.000	No	Yes	2.00
651	13.02	1.98	100.00	3.14	0.55	0.91	17.53	0.00	17.53	4.000	No	Yes	2.00
652	13.04	1.95	100.00	3.15	0.56	0.91	17.08	0.00	17.08	4.000	No	Yes	2.00
653	13.06	1.91	100.00	3.17	0.56	0.91	16.72	0.00	16.72	4.000	No	Yes	2.00
654	13.08	1.86	100.00	3.18	0.56	0.90	16.36	0.00	16.36	4.000	No	Yes	2.00
655	13.10	1.80	100.00	3.20	0.56	0.90	15.79	0.00	15.79	4.000	No	Yes	2.00
656	13.12	1.75	100.00	3.21	0.56	0.90	15.14	0.00	15.14	4.000	No	Yes	2.00
657	13.14	1.72	100.00	3.22	0.56	0.90	14.95	0.00	14.95	4.000	No	Yes	2.00
658	13.16	1.69	100.00	3.22	0.56	0.90	14.81	0.00	14.81	4.000	No	Yes	2.00
659	13.18	1.65	100.00	3.23	0.57	0.90	14.48	0.00	14.48	4.000	No	Yes	2.00
660	13.20	1.58	100.00	3.26	0.57	0.90	13.77	0.00	13.77	4.000	No	Yes	2.00
661	13.22	1.50	100.00	3.29	0.57	0.90	12.98	0.00	12.98	4.000	No	Yes	2.00
662	13.24	1.44	100.00	3.32	0.57	0.90	12.28	0.00	12.28	4.000	No	Yes	2.00
663	13.26	1.39	100.00	3.32	0.57	0.89	12.08	0.00	12.08	4.000	No	Yes	2.00
664	13.28	1.36	100.00	3.33	0.58	0.89	11.80	0.00	11.80	4.000	No	Yes	2.00
665	13.30	1.33	100.00	3.34	0.58	0.89	11.43	0.00	11.43	4.000	No	Yes	2.00
666	13.32	1.30	100.00	3.34	0.58	0.89	11.10	0.00	11.10	4.000	No	Yes	2.00
667	13.34	1.26	100.00	3.35	0.58	0.89	11.01	0.00	11.01	4.000	No	Yes	2.00
668	13.36	1.22	100.00	3.37	0.58	0.89	10.39	0.00	10.39	4.000	No	Yes	2.00
669	13.38	1.17	100.00	3.39	0.58	0.89	9.96	0.00	9.96	4.000	No	Yes	2.00
670	13.40	1.12	100.00	3.42	0.58	0.89	9.66	0.00	9.66	4.000	No	Yes	2.00
671	13.42	1.05	100.00	3.46	0.59	0.89	8.98	0.00	8.98	4.000	No	Yes	2.00
672	13.44	1.01	100.00	3.49	0.59	0.89	8.31	0.00	8.31	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
673	13.46	1.03	100.00	3.47	0.59	0.89	8.47	0.00	8.47	4.000	No	Yes	2.00
674	13.48	1.11	100.00	3.40	0.58	0.89	9.49	0.00	9.49	4.000	No	Yes	2.00
675	13.50	1.22	100.00	3.31	0.58	0.89	10.42	0.00	10.42	4.000	No	Yes	2.00
676	13.52	1.30	100.00	3.24	0.58	0.89	11.22	0.00	11.22	4.000	No	Yes	2.00
677	13.54	1.35	100.00	3.19	0.58	0.88	11.61	0.00	11.61	4.000	No	Yes	2.00
678	13.56	1.36	100.00	3.19	0.58	0.88	11.81	0.00	11.81	4.000	No	Yes	2.00
679	13.58	1.37	100.00	3.19	0.58	0.88	11.31	0.00	11.31	4.000	No	Yes	2.00
680	13.60	1.39	100.00	3.20	0.58	0.88	11.89	0.00	11.89	4.000	No	Yes	2.00
681	13.62	1.45	100.00	3.18	0.57	0.88	12.36	0.00	12.36	4.000	No	Yes	2.00
682	13.64	1.52	100.00	3.16	0.57	0.88	12.95	0.00	12.95	4.000	No	Yes	2.00
683	13.66	1.59	100.00	3.13	0.57	0.88	13.47	0.00	13.47	4.000	No	Yes	2.00
684	13.68	1.65	100.00	3.10	0.57	0.88	14.20	0.00	14.20	4.000	No	Yes	2.00
685	13.70	1.70	100.00	3.07	0.56	0.88	14.59	0.00	14.59	4.000	No	Yes	2.00
686	13.72	1.72	100.00	3.05	0.56	0.88	14.64	0.00	14.64	4.000	No	Yes	2.00
687	13.74	1.70	100.00	3.05	0.56	0.88	14.72	0.00	14.72	4.000	No	Yes	2.00
688	13.76	1.67	100.00	3.07	0.57	0.88	14.09	0.00	14.09	4.000	No	Yes	2.00
689	13.78	1.62	100.00	3.09	0.57	0.88	13.76	0.00	13.76	4.000	No	Yes	2.00
690	13.80	1.59	100.00	3.12	0.57	0.88	13.48	0.00	13.48	4.000	No	Yes	2.00
691	13.82	1.58	100.00	3.15	0.57	0.88	13.35	0.00	13.35	4.000	No	Yes	2.00
692	13.84	1.57	100.00	3.17	0.57	0.88	13.28	0.00	13.28	4.000	No	Yes	2.00
693	13.86	1.55	100.00	3.19	0.57	0.88	13.15	0.00	13.15	4.000	No	Yes	2.00
694	13.88	1.53	100.00	3.21	0.57	0.87	12.98	0.00	12.98	4.000	No	Yes	2.00
695	13.90	1.50	100.00	3.24	0.57	0.87	12.58	0.00	12.58	4.000	No	Yes	2.00
696	13.92	1.47	100.00	3.25	0.57	0.87	12.38	0.00	12.38	4.000	No	Yes	2.00
697	13.94	1.47	100.00	3.25	0.57	0.87	12.31	0.00	12.31	4.000	No	Yes	2.00
698	13.97	1.53	100.00	3.21	0.57	0.87	12.41	0.00	12.41	4.000	No	Yes	2.00
699	13.98	1.63	100.00	3.15	0.57	0.87	14.02	0.00	14.02	4.000	No	Yes	2.00
700	14.00	1.75	100.00	3.08	0.56	0.87	14.89	0.00	14.89	4.000	No	Yes	2.00
701	14.02	1.85	100.00	3.04	0.56	0.87	15.49	0.00	15.49	4.000	No	Yes	2.00
702	14.04	1.91	100.00	3.01	0.56	0.87	16.39	0.00	16.39	4.000	No	Yes	2.00
703	14.06	1.97	100.00	2.99	0.56	0.87	16.59	0.00	16.59	4.000	No	Yes	2.00
704	14.08	1.99	100.00	2.99	0.56	0.87	17.00	0.00	17.00	4.000	No	Yes	2.00
705	14.10	1.99	100.00	3.00	0.56	0.87	16.96	0.00	16.96	4.000	No	Yes	2.00
706	14.12	1.95	100.00	3.03	0.56	0.87	16.42	0.00	16.42	4.000	No	Yes	2.00
707	14.14	1.88	100.00	3.06	0.56	0.87	15.95	0.00	15.95	4.000	No	Yes	2.00
708	14.16	1.82	100.00	3.09	0.56	0.87	15.16	0.00	15.16	4.000	No	Yes	2.00
709	14.18	1.76	100.00	3.12	0.56	0.87	14.88	0.00	14.88	4.000	No	Yes	2.00
710	14.20	1.70	100.00	3.16	0.57	0.87	14.34	0.00	14.34	4.000	No	Yes	2.00
711	14.22	1.61	100.00	3.21	0.57	0.86	13.41	0.00	13.41	4.000	No	Yes	2.00
712	14.24	1.51	100.00	3.26	0.57	0.86	12.49	0.00	12.49	4.000	No	Yes	2.00
713	14.26	1.45	100.00	3.30	0.57	0.86	11.97	0.00	11.97	4.000	No	Yes	2.00
714	14.28	1.39	100.00	3.33	0.58	0.86	11.69	0.00	11.69	4.000	No	Yes	2.00
715	14.30	1.33	100.00	3.35	0.58	0.86	10.93	0.00	10.93	4.000	No	Yes	2.00
716	14.32	1.27	100.00	3.38	0.58	0.86	10.48	0.00	10.48	4.000	No	Yes	2.00
717	14.34	1.22	100.00	3.40	0.58	0.86	10.15	0.00	10.15	4.000	No	Yes	2.00
718	14.36	1.19	100.00	3.41	0.58	0.86	9.66	0.00	9.66	4.000	No	Yes	2.00
719	14.38	1.17	100.00	3.41	0.58	0.86	9.51	0.00	9.51	4.000	No	Yes	2.00
720	14.40	1.19	100.00	3.37	0.58	0.86	9.66	0.00	9.66	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
721	14.42	1.22	100.00	3.33	0.58	0.85	10.20	0.00	10.20	4.000	No	Yes	2.00
722	14.44	1.24	100.00	3.29	0.58	0.85	10.23	0.00	10.23	4.000	No	Yes	2.00
723	14.46	1.24	100.00	3.28	0.58	0.85	10.27	0.00	10.27	4.000	No	Yes	2.00
724	14.48	1.23	100.00	3.27	0.58	0.85	10.06	0.00	10.06	4.000	No	Yes	2.00
725	14.50	1.21	100.00	3.28	0.58	0.85	9.99	0.00	9.99	4.000	No	Yes	2.00
726	14.52	1.20	100.00	3.29	0.58	0.85	9.81	0.00	9.81	4.000	No	Yes	2.00
727	14.54	1.17	100.00	3.30	0.58	0.85	9.62	0.00	9.62	4.000	No	Yes	2.00
728	14.56	1.14	100.00	3.32	0.59	0.85	9.30	0.00	9.30	4.000	No	Yes	2.00
729	14.58	1.12	100.00	3.33	0.59	0.85	9.09	0.00	9.09	4.000	No	Yes	2.00
730	14.60	1.11	100.00	3.32	0.59	0.85	9.05	0.00	9.05	4.000	No	Yes	2.00
731	14.62	1.11	100.00	3.32	0.59	0.85	9.08	0.00	9.08	4.000	No	Yes	2.00
732	14.64	1.11	100.00	3.31	0.59	0.85	8.98	0.00	8.98	4.000	No	Yes	2.00
733	14.66	1.10	100.00	3.32	0.59	0.85	8.99	0.00	8.99	4.000	No	Yes	2.00
734	14.68	1.09	100.00	3.32	0.59	0.85	8.79	0.00	8.79	4.000	No	Yes	2.00
735	14.70	1.07	100.00	3.33	0.59	0.85	8.70	0.00	8.70	4.000	No	Yes	2.00
736	14.72	1.04	100.00	3.35	0.59	0.84	8.50	0.00	8.50	4.000	No	Yes	2.00
737	14.74	0.99	100.00	3.39	0.59	0.84	7.97	0.00	7.97	4.000	No	Yes	2.00
738	14.76	0.93	100.00	3.44	0.59	0.84	7.56	0.00	7.56	4.000	No	Yes	2.00
739	14.78	0.86	100.00	3.50	0.59	0.84	7.02	0.00	7.02	4.000	No	Yes	2.00
740	14.80	0.82	100.00	3.52	0.60	0.84	6.22	0.00	6.22	4.000	No	Yes	2.00
741	14.82	0.79	100.00	3.54	0.60	0.84	6.49	0.00	6.49	4.000	No	Yes	2.00
742	14.84	0.76	100.00	3.55	0.60	0.84	6.04	0.00	6.04	4.000	No	Yes	2.00
743	14.86	0.72	100.00	3.59	0.60	0.84	5.65	0.00	5.65	4.000	No	Yes	2.00
744	14.88	0.68	100.00	3.62	0.60	0.84	5.28	0.00	5.28	4.000	No	Yes	2.00
745	14.90	0.65	100.00	3.63	0.60	0.84	5.10	0.00	5.10	4.000	No	Yes	2.00
746	14.92	0.65	100.00	3.62	0.60	0.84	5.01	0.00	5.01	4.000	No	Yes	2.00
747	14.94	0.64	100.00	3.61	0.60	0.84	5.14	0.00	5.14	4.000	No	Yes	2.00
748	14.96	0.65	100.00	3.58	0.60	0.83	4.93	0.00	4.93	4.000	No	Yes	2.00
749	14.98	0.67	100.00	3.53	0.60	0.83	5.18	0.00	5.18	4.000	No	Yes	2.00
750	15.00	0.73	100.00	3.43	0.60	0.83	5.64	0.00	5.64	4.000	No	Yes	2.00
751	15.02	0.78	100.00	3.35	0.60	0.84	6.45	0.00	6.45	4.000	No	Yes	2.00
752	15.04	0.79	100.00	3.32	0.60	0.83	6.41	0.00	6.41	4.000	No	Yes	2.00
753	15.06	0.75	100.00	3.35	0.60	0.83	5.89	0.00	5.89	4.000	No	Yes	2.00
754	15.09	0.71	100.00	3.40	0.60	0.83	5.42	0.00	5.42	4.000	No	Yes	2.00
755	15.10	0.68	100.00	3.44	0.60	0.83	5.27	0.00	5.27	4.000	No	Yes	2.00
756	15.12	0.68	100.00	3.44	0.60	0.83	5.27	0.00	5.27	4.000	No	Yes	2.00
757	15.14	0.68	100.00	3.45	0.60	0.83	5.31	0.00	5.31	4.000	No	Yes	2.00
758	15.16	0.70	100.00	3.43	0.60	0.83	5.35	0.00	5.35	4.000	No	Yes	2.00
759	15.18	0.73	100.00	3.39	0.60	0.83	5.68	0.00	5.68	4.000	No	Yes	2.00
760	15.20	0.76	100.00	3.34	0.60	0.83	6.02	0.00	6.02	4.000	No	Yes	2.00
761	15.23	0.79	100.00	3.30	0.60	0.83	6.16	0.00	6.16	4.000	No	Yes	2.00
762	15.24	0.82	100.00	3.28	0.60	0.83	6.43	0.00	6.43	4.000	No	Yes	2.00
763	15.26	0.84	100.00	3.27	0.60	0.83	6.72	0.00	6.72	4.000	No	Yes	2.00
764	15.28	0.84	100.00	3.28	0.60	0.83	6.70	0.00	6.70	4.000	No	Yes	2.00
765	15.30	0.82	100.00	3.31	0.60	0.83	6.33	0.00	6.33	4.000	No	Yes	2.00
766	15.32	0.80	100.00	3.34	0.60	0.83	6.23	0.00	6.23	4.000	No	Yes	2.00
767	15.34	0.80	100.00	3.34	0.60	0.83	6.35	0.00	6.35	4.000	No	Yes	2.00
768	15.37	0.80	100.00	3.35	0.60	0.83	6.16	0.00	6.16	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
769	15.38	0.81	100.00	3.33	0.60	0.83	6.25	0.00	6.25	4.000	No	Yes	2.00
770	15.40	0.85	100.00	3.29	0.60	0.83	6.52	0.00	6.52	4.000	No	Yes	2.00
771	15.42	0.90	100.00	3.24	0.59	0.83	7.13	0.00	7.13	4.000	No	Yes	2.00
772	15.44	0.94	100.00	3.21	0.59	0.83	7.44	0.00	7.44	4.000	No	Yes	2.00
773	15.46	0.98	100.00	3.20	0.59	0.83	7.63	0.00	7.63	4.000	No	Yes	2.00
774	15.48	0.99	100.00	3.21	0.59	0.83	7.97	0.00	7.97	4.000	No	Yes	2.00
775	15.50	1.00	100.00	3.23	0.59	0.83	7.83	0.00	7.83	4.000	No	Yes	2.00
776	15.52	1.00	100.00	3.25	0.59	0.83	7.89	0.00	7.89	4.000	No	Yes	2.00
777	15.54	1.00	100.00	3.27	0.59	0.83	7.79	0.00	7.79	4.000	No	Yes	2.00
778	15.56	1.02	100.00	3.27	0.59	0.82	7.86	0.00	7.86	4.000	No	Yes	2.00
779	15.58	1.05	100.00	3.26	0.59	0.82	8.28	0.00	8.28	4.000	No	Yes	2.00
780	15.60	1.09	100.00	3.25	0.59	0.82	8.60	0.00	8.60	4.000	No	Yes	2.00
781	15.62	1.12	100.00	3.25	0.59	0.82	8.75	0.00	8.75	4.000	No	Yes	2.00
782	15.64	1.13	100.00	3.25	0.59	0.82	9.00	0.00	9.00	4.000	No	Yes	2.00
783	15.66	1.14	100.00	3.27	0.59	0.82	8.99	0.00	8.99	4.000	No	Yes	2.00
784	15.68	1.14	100.00	3.29	0.59	0.82	8.95	0.00	8.95	4.000	No	Yes	2.00
785	15.70	1.14	100.00	3.30	0.59	0.82	9.06	0.00	9.06	4.000	No	Yes	2.00
786	15.72	1.16	100.00	3.30	0.59	0.82	8.97	0.00	8.97	4.000	No	Yes	2.00
787	15.74	1.17	100.00	3.31	0.59	0.82	9.29	0.00	9.29	4.000	No	Yes	2.00
788	15.76	1.19	100.00	3.30	0.59	0.82	9.27	0.00	9.27	4.000	No	Yes	2.00
789	15.78	1.19	100.00	3.32	0.58	0.82	9.53	0.00	9.53	4.000	No	Yes	2.00
790	15.82	1.21	100.00	3.32	0.58	0.82	9.35	0.00	9.35	4.000	No	Yes	2.00
791	15.82	1.22	100.00	3.32	0.58	0.82	9.66	0.00	9.66	4.000	No	Yes	2.00
792	15.84	1.24	100.00	3.33	0.58	0.82	9.77	0.00	9.77	4.000	No	Yes	2.00
793	15.86	1.24	100.00	3.33	0.58	0.82	9.63	0.00	9.63	4.000	No	Yes	2.00
794	15.88	1.25	100.00	3.33	0.58	0.82	9.83	0.00	9.83	4.000	No	Yes	2.00
795	15.90	1.27	100.00	3.33	0.58	0.82	9.96	0.00	9.96	4.000	No	Yes	2.00
796	15.93	1.27	100.00	3.33	0.58	0.82	9.97	0.00	9.97	4.000	No	Yes	2.00
797	15.94	1.29	100.00	3.32	0.58	0.82	10.02	0.00	10.02	4.000	No	Yes	2.00
798	15.96	1.30	100.00	3.33	0.58	0.82	10.28	0.00	10.28	4.000	No	Yes	2.00
799	15.98	1.30	100.00	3.33	0.58	0.82	10.15	0.00	10.15	4.000	No	Yes	2.00
800	16.00	1.32	100.00	3.33	0.58	0.82	10.20	0.00	10.20	4.000	No	Yes	2.00
801	16.02	1.35	100.00	3.32	0.58	0.82	10.59	0.00	10.59	4.000	No	Yes	2.00
802	16.04	1.39	100.00	3.30	0.58	0.82	10.98	0.00	10.98	4.000	No	Yes	2.00
803	16.06	1.41	100.00	3.29	0.58	0.82	11.01	0.00	11.01	4.000	No	Yes	2.00
804	16.08	1.42	100.00	3.29	0.58	0.81	11.07	0.00	11.07	4.000	No	Yes	2.00
805	16.10	1.44	100.00	3.28	0.58	0.81	11.15	0.00	11.15	4.000	No	Yes	2.00
806	16.12	1.46	100.00	3.27	0.58	0.81	11.48	0.00	11.48	4.000	No	Yes	2.00
807	16.14	1.48	100.00	3.27	0.58	0.81	11.55	0.00	11.55	4.000	No	Yes	2.00
808	16.16	1.49	100.00	3.26	0.58	0.81	11.69	0.00	11.69	4.000	No	Yes	2.00
809	16.18	1.50	100.00	3.26	0.58	0.81	11.75	0.00	11.75	4.000	No	Yes	2.00
810	16.20	1.53	100.00	3.25	0.58	0.81	11.85	0.00	11.85	4.000	No	Yes	2.00
811	16.22	1.55	100.00	3.24	0.57	0.81	12.28	0.00	12.28	4.000	No	Yes	2.00
812	16.24	1.57	100.00	3.23	0.57	0.81	12.27	0.00	12.27	4.000	No	Yes	2.00
813	16.26	1.57	100.00	3.23	0.57	0.81	12.27	0.00	12.27	4.000	No	Yes	2.00
814	16.28	1.58	100.00	3.23	0.57	0.81	12.24	0.00	12.24	4.000	No	Yes	2.00
815	16.30	1.58	100.00	3.23	0.57	0.81	12.42	0.00	12.42	4.000	No	Yes	2.00
816	16.32	1.58	100.00	3.23	0.57	0.81	12.37	0.00	12.37	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
817	16.34	1.56	100.00	3.25	0.57	0.81	12.24	0.00	12.24	4.000	No	Yes	2.00
818	16.36	1.54	100.00	3.26	0.57	0.81	11.90	0.00	11.90	4.000	No	Yes	2.00
819	16.38	1.51	100.00	3.27	0.58	0.81	11.76	0.00	11.76	4.000	No	Yes	2.00
820	16.40	1.48	100.00	3.29	0.58	0.81	11.53	0.00	11.53	4.000	No	Yes	2.00
821	16.42	1.45	100.00	3.30	0.58	0.81	11.10	0.00	11.10	4.000	No	Yes	2.00
822	16.44	1.42	100.00	3.31	0.58	0.80	11.03	0.00	11.03	4.000	No	Yes	2.00
823	16.46	1.41	100.00	3.32	0.58	0.80	10.79	0.00	10.79	4.000	No	Yes	2.00
824	16.48	1.38	100.00	3.33	0.58	0.80	10.73	0.00	10.73	4.000	No	Yes	2.00
825	16.50	1.36	100.00	3.33	0.58	0.80	10.41	0.00	10.41	4.000	No	Yes	2.00
826	16.52	1.36	100.00	3.31	0.58	0.80	10.31	0.00	10.31	4.000	No	Yes	2.00
827	16.54	1.40	100.00	3.27	0.58	0.80	10.77	0.00	10.77	4.000	No	Yes	2.00
828	16.56	1.46	100.00	3.22	0.58	0.80	11.27	0.00	11.27	4.000	No	Yes	2.00
829	16.58	1.51	100.00	3.18	0.58	0.80	11.59	0.00	11.59	4.000	No	Yes	2.00
830	16.60	1.54	100.00	3.16	0.57	0.80	12.01	0.00	12.01	4.000	No	Yes	2.00
831	16.62	1.57	100.00	3.14	0.57	0.80	11.97	0.00	11.97	4.000	No	Yes	2.00
832	16.64	1.56	100.00	3.15	0.57	0.80	12.26	0.00	12.26	4.000	No	Yes	2.00
833	16.66	1.55	100.00	3.16	0.58	0.80	11.82	0.00	11.82	4.000	No	Yes	2.00
834	16.68	1.51	100.00	3.20	0.58	0.80	11.83	0.00	11.83	4.000	No	Yes	2.00
835	16.70	1.48	100.00	3.23	0.58	0.80	11.24	0.00	11.24	4.000	No	Yes	2.00
836	16.72	1.45	100.00	3.25	0.58	0.80	11.10	0.00	11.10	4.000	No	Yes	2.00
837	16.74	1.41	100.00	3.28	0.58	0.80	10.93	0.00	10.93	4.000	No	Yes	2.00
838	16.76	1.36	100.00	3.31	0.58	0.80	10.24	0.00	10.24	4.000	No	Yes	2.00
839	16.78	1.32	100.00	3.34	0.58	0.79	9.90	0.00	9.90	4.000	No	Yes	2.00
840	16.80	1.31	100.00	3.34	0.58	0.79	9.96	0.00	9.96	4.000	No	Yes	2.00
841	16.82	1.30	100.00	3.34	0.58	0.79	10.01	0.00	10.01	4.000	No	Yes	2.00
842	16.84	1.28	100.00	3.35	0.58	0.79	9.69	0.00	9.69	4.000	No	Yes	2.00
843	16.86	1.26	100.00	3.36	0.58	0.79	9.49	0.00	9.49	4.000	No	Yes	2.00
844	16.88	1.25	100.00	3.35	0.58	0.79	9.47	0.00	9.47	4.000	No	Yes	2.00
845	16.90	1.24	100.00	3.35	0.58	0.79	9.42	0.00	9.42	4.000	No	Yes	2.00
846	16.92	1.21	100.00	3.35	0.59	0.79	9.19	0.00	9.19	4.000	No	Yes	2.00
847	16.94	1.16	100.00	3.38	0.59	0.79	8.80	0.00	8.80	4.000	No	Yes	2.00
848	16.96	1.11	100.00	3.40	0.59	0.79	8.21	0.00	8.21	4.000	No	Yes	2.00
849	16.98	1.07	100.00	3.41	0.59	0.79	8.04	0.00	8.04	4.000	No	Yes	2.00
850	17.00	1.04	100.00	3.42	0.59	0.79	7.78	0.00	7.78	4.000	No	Yes	2.00
851	17.02	1.01	100.00	3.43	0.59	0.79	7.37	0.00	7.37	4.000	No	Yes	2.00
852	17.04	1.00	100.00	3.42	0.59	0.79	7.48	0.00	7.48	4.000	No	Yes	2.00
853	17.06	1.00	100.00	3.41	0.59	0.79	7.45	0.00	7.45	4.000	No	Yes	2.00
854	17.08	0.98	100.00	3.41	0.59	0.78	7.30	0.00	7.30	4.000	No	Yes	2.00
855	17.10	0.95	100.00	3.43	0.59	0.78	7.03	0.00	7.03	4.000	No	Yes	2.00
856	17.12	0.92	100.00	3.45	0.60	0.78	6.68	0.00	6.68	4.000	No	Yes	2.00
857	17.14	0.91	100.00	3.45	0.60	0.78	6.67	0.00	6.67	4.000	No	Yes	2.00
858	17.17	0.91	100.00	3.43	0.60	0.78	6.69	0.00	6.69	4.000	No	Yes	2.00
859	17.18	0.93	100.00	3.39	0.60	0.78	6.80	0.00	6.80	4.000	No	Yes	2.00
860	17.20	0.94	100.00	3.36	0.59	0.78	6.99	0.00	6.99	4.000	No	Yes	2.00
861	17.22	0.95	100.00	3.32	0.59	0.78	7.06	0.00	7.06	4.000	No	Yes	2.00
862	17.24	0.96	100.00	3.30	0.59	0.78	7.03	0.00	7.03	4.000	No	Yes	2.00
863	17.26	0.95	100.00	3.30	0.59	0.78	7.10	0.00	7.10	4.000	No	Yes	2.00
864	17.28	0.95	100.00	3.30	0.59	0.78	6.86	0.00	6.86	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
865	17.30	0.95	100.00	3.30	0.59	0.78	6.95	0.00	6.95	4.000	No	Yes	2.00
866	17.32	0.96	100.00	3.29	0.59	0.78	7.10	0.00	7.10	4.000	No	Yes	2.00
867	17.34	0.96	100.00	3.29	0.59	0.78	7.12	0.00	7.12	4.000	No	Yes	2.00
868	17.36	0.96	100.00	3.29	0.59	0.78	6.97	0.00	6.97	4.000	No	Yes	2.00
869	17.38	0.95	100.00	3.28	0.59	0.78	6.93	0.00	6.93	4.000	No	Yes	2.00
870	17.40	0.97	100.00	3.26	0.59	0.78	7.04	0.00	7.04	4.000	No	Yes	2.00
871	17.42	1.00	100.00	3.22	0.59	0.78	7.24	0.00	7.24	4.000	No	Yes	2.00
872	17.44	1.04	100.00	3.18	0.59	0.78	7.69	0.00	7.69	4.000	No	Yes	2.00
873	17.46	1.07	100.00	3.14	0.59	0.78	7.89	0.00	7.89	4.000	No	Yes	2.00
874	17.48	1.08	100.00	3.13	0.59	0.78	8.02	0.00	8.02	4.000	No	Yes	2.00
875	17.50	1.07	100.00	3.14	0.59	0.78	7.87	0.00	7.87	4.000	No	Yes	2.00
876	17.52	1.05	100.00	3.16	0.59	0.78	7.71	0.00	7.71	4.000	No	Yes	2.00
877	17.54	1.04	100.00	3.18	0.59	0.78	7.54	0.00	7.54	4.000	No	Yes	2.00
878	17.56	1.03	100.00	3.18	0.59	0.78	7.49	0.00	7.49	4.000	No	Yes	2.00
879	17.58	1.02	100.00	3.19	0.59	0.77	7.47	0.00	7.47	4.000	No	Yes	2.00
880	17.60	1.01	100.00	3.21	0.59	0.77	7.36	0.00	7.36	4.000	No	Yes	2.00
881	17.62	1.01	100.00	3.22	0.59	0.77	7.31	0.00	7.31	4.000	No	Yes	2.00
882	17.64	1.01	100.00	3.21	0.59	0.77	7.34	0.00	7.34	4.000	No	Yes	2.00
883	17.66	1.04	100.00	3.19	0.59	0.77	7.43	0.00	7.43	4.000	No	Yes	2.00
884	17.68	1.08	100.00	3.16	0.59	0.77	7.85	0.00	7.85	4.000	No	Yes	2.00
885	17.70	1.11	100.00	3.14	0.59	0.77	8.21	0.00	8.21	4.000	No	Yes	2.00
886	17.72	1.12	100.00	3.15	0.59	0.77	8.24	0.00	8.24	4.000	No	Yes	2.00
887	17.74	1.12	100.00	3.16	0.59	0.77	8.07	0.00	8.07	4.000	No	Yes	2.00
888	17.76	1.13	100.00	3.16	0.59	0.77	8.25	0.00	8.25	4.000	No	Yes	2.00
889	17.78	1.27	100.00	3.08	0.59	0.77	8.42	0.00	8.42	4.000	No	Yes	2.00
890	17.80	1.38	100.00	3.05	0.58	0.78	11.30	0.00	11.30	4.000	No	Yes	2.00
891	17.82	1.42	100.00	3.07	0.58	0.77	10.71	0.00	10.71	4.000	No	Yes	2.00
892	17.84	1.31	100.00	3.16	0.59	0.77	9.24	0.00	9.24	4.000	No	Yes	2.00
893	17.86	1.19	100.00	3.24	0.59	0.77	8.73	0.00	8.73	4.000	No	Yes	2.00
894	17.88	1.13	100.00	3.27	0.59	0.77	7.96	0.00	7.96	4.000	No	Yes	2.00
895	17.90	1.07	100.00	3.29	0.59	0.77	7.67	0.00	7.67	4.000	No	Yes	2.00
896	17.92	1.05	100.00	3.28	0.59	0.77	7.43	0.00	7.43	4.000	No	Yes	2.00
897	17.94	1.04	100.00	3.27	0.59	0.77	7.50	0.00	7.50	4.000	No	Yes	2.00
898	17.96	1.02	100.00	3.26	0.59	0.77	7.28	0.00	7.28	4.000	No	Yes	2.00
899	17.98	0.98	100.00	3.27	0.59	0.77	7.05	0.00	7.05	4.000	No	Yes	2.00
900	18.00	0.94	100.00	3.28	0.60	0.77	6.56	0.00	6.56	4.000	No	Yes	2.00
901	18.02	0.91	100.00	3.30	0.60	0.77	6.36	0.00	6.36	4.000	No	Yes	2.00
902	18.04	0.90	100.00	3.31	0.60	0.76	6.25	0.00	6.25	4.000	No	Yes	2.00
903	18.06	0.90	100.00	3.31	0.60	0.76	6.30	0.00	6.30	4.000	No	Yes	2.00
904	18.08	0.91	100.00	3.29	0.60	0.76	6.33	0.00	6.33	4.000	No	Yes	2.00
905	18.10	0.92	100.00	3.28	0.60	0.76	6.56	0.00	6.56	4.000	No	Yes	2.00
906	18.12	0.93	100.00	3.27	0.60	0.76	6.56	0.00	6.56	4.000	No	Yes	2.00
907	18.14	0.94	100.00	3.26	0.60	0.76	6.50	0.00	6.50	4.000	No	Yes	2.00
908	18.16	0.96	100.00	3.23	0.60	0.76	6.76	0.00	6.76	4.000	No	Yes	2.00
909	18.18	0.98	100.00	3.21	0.59	0.76	6.99	0.00	6.99	4.000	No	Yes	2.00
910	18.20	0.99	100.00	3.19	0.59	0.76	7.01	0.00	7.01	4.000	No	Yes	2.00
911	18.22	0.98	100.00	3.20	0.59	0.76	7.01	0.00	7.01	4.000	No	Yes	2.00
912	18.24	0.95	100.00	3.24	0.60	0.76	6.76	0.00	6.76	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
913	18.26	0.92	100.00	3.28	0.60	0.76	6.33	0.00	6.33	4.000	No	Yes	2.00
914	18.28	0.89	100.00	3.31	0.60	0.76	6.20	0.00	6.20	4.000	No	Yes	2.00
915	18.30	0.89	100.00	3.31	0.60	0.76	6.13	0.00	6.13	4.000	No	Yes	2.00
916	18.32	0.89	100.00	3.30	0.60	0.76	6.20	0.00	6.20	4.000	No	Yes	2.00
917	18.34	0.88	100.00	3.30	0.60	0.76	6.16	0.00	6.16	4.000	No	Yes	2.00
918	18.36	0.88	100.00	3.30	0.60	0.76	6.11	0.00	6.11	4.000	No	Yes	2.00
919	18.38	0.88	100.00	3.29	0.60	0.76	6.12	0.00	6.12	4.000	No	Yes	2.00
920	18.40	0.88	100.00	3.29	0.60	0.76	6.10	0.00	6.10	4.000	No	Yes	2.00
921	18.42	0.91	100.00	3.27	0.60	0.76	6.20	0.00	6.20	4.000	No	Yes	2.00
922	18.44	0.96	100.00	3.23	0.60	0.76	6.57	0.00	6.57	4.000	No	Yes	2.00
923	18.46	1.03	100.00	3.17	0.59	0.76	7.38	0.00	7.38	4.000	No	Yes	2.00
924	18.48	1.11	100.00	3.12	0.59	0.76	7.75	0.00	7.75	4.000	No	Yes	2.00
925	18.50	1.16	100.00	3.09	0.59	0.76	8.32	0.00	8.32	4.000	No	Yes	2.00
926	18.52	1.19	100.00	3.07	0.59	0.76	8.48	0.00	8.48	4.000	No	Yes	2.00
927	18.54	1.19	100.00	3.07	0.59	0.76	8.40	0.00	8.40	4.000	No	Yes	2.00
928	18.56	1.16	100.00	3.10	0.59	0.76	8.22	0.00	8.22	4.000	No	Yes	2.00
929	18.58	1.14	100.00	3.14	0.59	0.76	7.95	0.00	7.95	4.000	No	Yes	2.00
930	18.60	1.13	100.00	3.16	0.59	0.76	7.84	0.00	7.84	4.000	No	Yes	2.00
931	18.62	1.15	100.00	3.17	0.59	0.76	8.05	0.00	8.05	4.000	No	Yes	2.00
932	18.64	1.20	100.00	3.15	0.59	0.76	8.39	0.00	8.39	4.000	No	Yes	2.00
933	18.66	1.28	100.00	3.13	0.59	0.76	8.99	0.00	8.99	4.000	No	Yes	2.00
934	18.68	1.38	100.00	3.08	0.58	0.76	9.67	0.00	9.67	4.000	No	Yes	2.00
935	18.70	1.50	100.00	3.02	0.58	0.76	10.63	0.00	10.63	4.000	No	Yes	2.00
936	18.72	1.70	98.53	2.94	0.58	0.76	11.90	0.00	11.90	4.000	No	Yes	2.00
937	18.74	1.89	93.55	2.88	0.57	0.76	14.05	0.00	14.05	4.000	No	Yes	2.00
938	18.76	2.06	91.24	2.85	0.56	0.76	15.18	0.00	15.18	4.000	No	Yes	2.00
939	18.78	2.28	91.80	2.86	0.56	0.76	15.77	0.00	15.77	4.000	No	Yes	2.00
940	18.80	2.41	93.75	2.88	0.55	0.77	19.23	0.00	19.23	4.000	No	Yes	2.00
941	18.82	2.37	98.61	2.95	0.55	0.77	18.54	0.00	18.54	4.000	No	Yes	2.00
942	18.84	2.04	100.00	3.06	0.56	0.76	15.04	0.00	15.04	4.000	No	Yes	2.00
943	18.86	1.65	100.00	3.20	0.58	0.76	11.73	0.00	11.73	4.000	No	Yes	2.00
944	18.88	1.34	100.00	3.34	0.58	0.75	9.50	0.00	9.50	4.000	No	Yes	2.00
945	18.90	1.15	100.00	3.44	0.59	0.75	8.02	0.00	8.02	4.000	No	Yes	2.00
946	18.92	1.05	100.00	3.49	0.59	0.75	7.29	0.00	7.29	4.000	No	Yes	2.00
947	18.94	1.03	100.00	3.48	0.59	0.75	7.23	0.00	7.23	4.000	No	Yes	2.00
948	18.96	1.04	100.00	3.44	0.59	0.75	7.36	0.00	7.36	4.000	No	Yes	2.00
949	18.98	1.06	100.00	3.38	0.59	0.75	7.50	0.00	7.50	4.000	No	Yes	2.00
950	19.00	1.11	100.00	3.29	0.59	0.75	7.66	0.00	7.66	4.000	No	Yes	2.00
951	19.02	1.18	100.00	3.19	0.59	0.75	8.34	0.00	8.34	4.000	No	Yes	2.00
952	19.04	1.25	100.00	3.10	0.59	0.75	8.96	0.00	8.96	4.000	No	Yes	2.00
953	19.06	1.31	100.00	3.06	0.59	0.75	9.27	0.00	9.27	4.000	No	Yes	2.00
954	19.08	1.38	100.00	3.05	0.58	0.75	9.79	0.00	9.79	4.000	No	Yes	2.00
955	19.10	1.45	100.00	3.04	0.58	0.75	10.38	0.00	10.38	4.000	No	Yes	2.00
956	19.12	1.51	100.00	3.04	0.58	0.75	10.76	0.00	10.76	4.000	No	Yes	2.00
957	19.15	1.59	100.00	3.04	0.58	0.75	11.31	0.00	11.31	4.000	No	Yes	2.00
958	19.16	1.72	100.00	3.01	0.57	0.75	12.07	0.00	12.07	4.000	No	Yes	2.00
959	19.19	1.92	99.51	2.96	0.57	0.75	13.60	0.00	13.60	4.000	No	Yes	2.00
960	19.20	2.29	92.35	2.87	0.56	0.76	16.01	0.00	16.01	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
961	19.22	2.65	87.53	2.81	0.55	0.76	20.42	0.00	20.42	4.000	No	Yes	2.00
962	19.24	2.88	87.05	2.80	0.54	0.76	21.97	0.00	21.97	4.000	No	Yes	2.00
963	19.26	2.74	92.66	2.87	0.54	0.76	21.30	0.00	21.30	4.000	No	Yes	2.00
964	19.28	2.39	100.00	2.98	0.55	0.76	17.44	0.00	17.44	4.000	No	Yes	2.00
965	19.30	1.97	100.00	3.11	0.57	0.75	13.84	0.00	13.84	4.000	No	Yes	2.00
966	19.32	1.87	100.00	3.12	0.58	0.75	11.78	0.00	11.78	4.000	No	Yes	2.00
967	19.34	2.03	100.00	3.03	0.56	0.75	14.92	0.00	14.92	4.000	No	Yes	2.00
968	19.36	2.21	99.01	2.95	0.56	0.76	17.39	0.00	17.39	4.000	No	Yes	2.00
969	19.38	2.16	100.00	2.98	0.56	0.75	15.79	0.00	15.79	4.000	No	Yes	2.00
970	19.40	2.02	100.00	3.05	0.57	0.75	13.88	0.00	13.88	4.000	No	Yes	2.00
971	19.42	2.16	100.00	3.01	0.57	0.75	14.16	0.00	14.16	4.000	No	Yes	2.00
972	19.44	2.46	95.55	2.91	0.55	0.76	18.98	0.00	18.98	4.000	No	Yes	2.00
973	19.46	2.70	91.50	2.86	0.55	0.76	20.66	0.00	20.66	4.000	No	Yes	2.00
974	19.48	2.71	93.66	2.88	0.55	0.76	19.47	0.00	19.47	4.000	No	Yes	2.00
975	19.50	2.66	96.84	2.92	0.55	0.75	19.28	0.00	19.28	4.000	No	Yes	2.00
976	19.52	2.71	96.00	2.91	0.55	0.76	19.75	0.00	19.75	4.000	No	Yes	2.00
977	19.54	2.74	94.58	2.89	0.55	0.76	20.42	0.00	20.42	4.000	No	Yes	2.00
978	19.56	2.63	98.22	2.94	0.55	0.75	20.09	0.00	20.09	4.000	No	Yes	2.00
979	19.58	2.36	100.00	3.02	0.56	0.75	17.20	0.00	17.20	4.000	No	Yes	2.00
980	19.60	2.01	100.00	3.14	0.57	0.75	14.31	0.00	14.31	4.000	No	Yes	2.00
981	19.62	1.78	100.00	3.21	0.57	0.74	11.97	0.00	11.97	4.000	No	Yes	2.00
982	19.64	1.83	100.00	3.18	0.57	0.74	11.98	0.00	11.98	4.000	No	Yes	2.00
983	19.66	2.25	100.00	3.01	0.56	0.75	15.36	0.00	15.36	4.000	No	Yes	2.00
984	19.68	2.79	90.53	2.84	0.54	0.75	21.48	0.00	21.48	4.000	No	Yes	2.00
985	19.70	3.23	80.98	2.72	0.54	0.76	24.08	0.00	24.08	4.000	No	Yes	2.00
986	19.72	3.22	80.66	2.72	0.53	0.76	25.36	0.00	25.36	4.000	No	Yes	2.00
987	19.74	2.89	86.51	2.79	0.54	0.75	21.35	0.00	21.35	4.000	No	Yes	2.00
988	19.76	2.45	94.76	2.90	0.56	0.75	16.49	0.00	16.49	4.000	No	Yes	2.00
989	19.78	2.38	97.17	2.93	0.56	0.74	15.54	0.00	15.54	4.000	No	Yes	2.00
990	19.80	2.64	92.05	2.86	0.55	0.75	19.57	0.00	19.57	4.000	No	Yes	2.00
991	19.82	3.22	83.14	2.75	0.54	0.75	22.51	0.00	22.51	4.000	No	Yes	2.00
992	19.84	3.76	75.42	2.66	0.52	0.76	28.67	0.00	28.67	4.000	No	Yes	2.00
993	19.86	4.21	70.28	2.59	0.52	0.76	32.03	60.00	92.02	0.128	No	No	0.72
994	19.88	4.37	68.04	2.56	0.51	0.76	32.96	59.83	92.80	0.129	No	No	0.73
995	19.90	4.29	68.20	2.57	0.52	0.76	32.49	59.73	92.22	0.128	No	No	0.73
996	19.92	4.12	70.03	2.59	0.52	0.76	30.14	59.40	89.55	0.125	No	No	0.71
997	19.94	3.99	73.15	2.63	0.52	0.76	29.06	0.00	29.06	4.000	No	Yes	2.00
998	19.96	4.10	74.03	2.64	0.52	0.76	29.46	0.00	29.46	4.000	No	Yes	2.00
999	19.98	4.38	72.99	2.62	0.51	0.76	32.66	0.00	32.66	4.000	No	Yes	2.00
1000	20.00	4.80	70.43	2.59	0.51	0.76	35.60	61.07	96.67	0.133	No	No	0.76
1001	20.02	5.16	68.63	2.57	0.50	0.77	39.48	61.84	101.32	0.139	No	No	0.80
1002	20.04	5.39	67.77	2.56	0.49	0.77	41.04	62.11	103.15	0.142	No	No	0.82
1003	20.06	5.42	67.86	2.56	0.49	0.77	41.11	62.15	103.26	0.142	No	No	0.82
1004	20.08	5.32	68.43	2.57	0.49	0.77	40.02	61.96	101.98	0.140	No	No	0.81
1005	20.10	5.12	69.89	2.59	0.50	0.76	38.72	61.87	100.60	0.138	No	No	0.80
1006	20.12	4.86	72.30	2.62	0.50	0.76	36.28	0.00	36.28	4.000	No	Yes	2.00
1007	20.15	4.54	75.98	2.66	0.51	0.76	33.83	0.00	33.83	4.000	No	Yes	2.00
1008	20.16	4.14	81.12	2.73	0.51	0.76	31.17	0.00	31.17	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1009	20.18	3.72	87.23	2.80	0.53	0.75	26.87	0.00	26.87	4.000	No	Yes	2.00
1010	20.20	3.24	95.03	2.90	0.53	0.75	24.02	0.00	24.02	4.000	No	Yes	2.00
1011	20.22	2.86	100.00	2.98	0.54	0.74	20.23	0.00	20.23	4.000	No	Yes	2.00
1012	20.25	2.74	100.00	2.98	0.55	0.74	18.02	0.00	18.02	4.000	No	Yes	2.00
1013	20.26	2.95	94.32	2.89	0.54	0.74	21.29	0.00	21.29	4.000	No	Yes	2.00
1014	20.28	3.40	85.23	2.78	0.53	0.75	24.88	0.00	24.88	4.000	No	Yes	2.00
1015	20.30	3.79	82.40	2.74	0.52	0.75	28.19	0.00	28.19	4.000	No	Yes	2.00
1016	20.32	4.06	82.70	2.75	0.52	0.75	30.12	0.00	30.12	4.000	No	Yes	2.00
1017	20.34	4.24	83.82	2.76	0.51	0.75	31.21	0.00	31.21	4.000	No	Yes	2.00
1018	20.36	4.37	83.80	2.76	0.51	0.75	32.24	0.00	32.24	4.000	No	Yes	2.00
1019	20.38	4.47	82.52	2.74	0.51	0.75	33.16	0.00	33.16	4.000	No	Yes	2.00
1020	20.40	4.55	81.30	2.73	0.51	0.75	33.60	0.00	33.60	4.000	No	Yes	2.00
1021	20.42	4.58	81.40	2.73	0.51	0.75	33.92	0.00	33.92	4.000	No	Yes	2.00
1022	20.44	4.65	81.55	2.73	0.51	0.75	34.00	0.00	34.00	4.000	Yes	Yes	2.00
1023	20.46	4.90	79.79	2.71	0.50	0.75	34.99	0.00	34.99	4.000	Yes	Yes	2.00
1024	20.48	5.36	75.85	2.66	0.49	0.76	39.84	0.00	39.84	4.000	Yes	Yes	2.00
1025	20.50	6.07	70.38	2.59	0.48	0.76	44.81	63.75	108.56	4.000	Yes	No	2.00
1026	20.52	6.92	63.60	2.51	0.46	0.77	51.71	64.19	115.90	4.000	Yes	No	2.00
1027	20.54	7.84	56.51	2.42	0.45	0.78	60.31	64.51	124.82	4.000	Yes	No	2.00
1028	20.56	8.61	51.00	2.35	0.44	0.78	67.14	64.23	131.37	4.000	Yes	No	2.00
1029	20.58	9.18	45.95	2.29	0.43	0.78	70.28	62.60	132.87	4.000	Yes	No	2.00
1030	20.60	9.56	41.11	2.23	0.43	0.78	74.06	60.58	134.63	4.000	Yes	No	2.00
1031	20.62	9.88	34.65	2.15	0.44	0.78	75.70	55.70	131.40	4.000	Yes	No	2.00
1032	20.64	10.03	29.51	2.08	0.44	0.78	77.17	50.29	127.47	4.000	Yes	No	2.00
1033	20.66	10.04	25.20	2.03	0.46	0.77	76.35	43.86	120.21	4.000	Yes	No	2.00
1034	20.68	9.94	20.81	1.97	0.48	0.76	73.96	35.24	109.20	4.000	Yes	No	2.00
1035	20.70	9.84	15.25	1.90	0.51	0.74	71.79	21.37	93.16	4.000	Yes	No	2.00
1036	20.72	9.83	9.29	1.83	0.56	0.73	69.83	5.22	75.05	4.000	Yes	No	2.00
1037	20.74	9.92	5.41	1.78	0.57	0.72	69.80	0.26	70.05	4.000	Yes	No	2.00
1038	20.76	10.01	4.27	1.77	0.57	0.72	71.18	0.03	71.21	0.108	No	No	0.61
1039	20.78	10.14	5.58	1.78	0.57	0.72	72.02	0.33	72.34	0.109	No	No	0.62

Abbreviations

Depth: Depth from free surface, at which CPT was performed (m)
q_t: Total cone resistance
FC: Fines content (%)
I_c: Soil behavior type index
m: Stress exponent
C_N: Overburden correction factor
q_{c1N}: Normalized and adjusted cone resistance
Δq_{c1N}: Cone resistance correction factor due to fines
$q_{c1N,cs}$: Normalized and adjusted cone resistance
$CRR_{7.5}$: Cyclic resistance ratio for M_w=7.5
FS: Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
0.02	2.00	0.00	9.99	0.02	0.00	0.04	2.00	0.00	9.98	0.02	0.00
0.06	2.00	0.00	9.97	0.02	0.00	0.08	2.00	0.00	9.96	0.02	0.00
0.10	2.00	0.00	9.95	0.02	0.00	0.12	2.00	0.00	9.94	0.02	0.00
0.14	2.00	0.00	9.93	0.02	0.00	0.16	2.00	0.00	9.92	0.02	0.00
0.18	2.00	0.00	9.91	0.02	0.00	0.20	2.00	0.00	9.90	0.02	0.00
0.22	2.00	0.00	9.89	0.02	0.00	0.24	2.00	0.00	9.88	0.02	0.00
0.26	2.00	0.00	9.87	0.02	0.00	0.28	2.00	0.00	9.86	0.02	0.00
0.30	2.00	0.00	9.85	0.02	0.00	0.32	2.00	0.00	9.84	0.02	0.00
0.34	2.00	0.00	9.83	0.02	0.00	0.36	2.00	0.00	9.82	0.02	0.00
0.38	2.00	0.00	9.81	0.02	0.00	0.40	2.00	0.00	9.80	0.02	0.00
0.42	2.00	0.00	9.79	0.02	0.00	0.44	2.00	0.00	9.78	0.02	0.00
0.46	2.00	0.00	9.77	0.02	0.00	0.48	2.00	0.00	9.76	0.02	0.00
0.50	2.00	0.00	9.75	0.02	0.00	0.52	2.00	0.00	9.74	0.02	0.00
0.54	2.00	0.00	9.73	0.02	0.00	0.56	2.00	0.00	9.72	0.02	0.00
0.58	2.00	0.00	9.71	0.02	0.00	0.60	2.00	0.00	9.70	0.02	0.00
0.62	2.00	0.00	9.69	0.02	0.00	0.64	2.00	0.00	9.68	0.02	0.00
0.66	2.00	0.00	9.67	0.02	0.00	0.68	2.00	0.00	9.66	0.02	0.00
0.70	2.00	0.00	9.65	0.02	0.00	0.72	2.00	0.00	9.64	0.02	0.00
0.74	2.00	0.00	9.63	0.02	0.00	0.76	2.00	0.00	9.62	0.02	0.00
0.78	2.00	0.00	9.61	0.02	0.00	0.80	2.00	0.00	9.60	0.02	0.00
0.82	2.00	0.00	9.59	0.02	0.00	0.84	2.00	0.00	9.58	0.02	0.00
0.86	2.00	0.00	9.57	0.02	0.00	0.88	2.00	0.00	9.56	0.02	0.00
0.90	2.00	0.00	9.55	0.02	0.00	0.92	2.00	0.00	9.54	0.02	0.00
0.94	2.00	0.00	9.53	0.02	0.00	0.96	2.00	0.00	9.52	0.02	0.00
0.98	2.00	0.00	9.51	0.02	0.00	1.00	2.00	0.00	9.50	0.02	0.00
1.02	2.00	0.00	9.49	0.02	0.00	1.04	2.00	0.00	9.48	0.02	0.00
1.06	2.00	0.00	9.47	0.02	0.00	1.08	2.00	0.00	9.46	0.02	0.00
1.10	2.00	0.00	9.45	0.02	0.00	1.12	2.00	0.00	9.44	0.02	0.00
1.14	2.00	0.00	9.43	0.02	0.00	1.16	2.00	0.00	9.42	0.02	0.00
1.18	2.00	0.00	9.41	0.02	0.00	1.20	2.00	0.00	9.40	0.02	0.00
1.22	2.00	0.00	9.39	0.02	0.00	1.24	2.00	0.00	9.38	0.02	0.00
1.26	2.00	0.00	9.37	0.02	0.00	1.28	2.00	0.00	9.36	0.02	0.00
1.30	2.00	0.00	9.35	0.02	0.00	1.32	2.00	0.00	9.34	0.02	0.00
1.34	2.00	0.00	9.33	0.02	0.00	1.36	2.00	0.00	9.32	0.02	0.00
1.39	2.00	0.00	9.31	0.03	0.00	1.40	2.00	0.00	9.30	0.01	0.00
1.42	2.00	0.00	9.29	0.02	0.00	1.44	2.00	0.00	9.28	0.02	0.00
1.46	2.00	0.00	9.27	0.02	0.00	1.48	2.00	0.00	9.26	0.02	0.00
1.50	2.00	0.00	9.25	0.02	0.00	1.52	2.00	0.00	9.24	0.02	0.00
1.54	2.00	0.00	9.23	0.02	0.00	1.56	2.00	0.00	9.22	0.02	0.00
1.58	2.00	0.00	9.21	0.02	0.00	1.60	2.00	0.00	9.20	0.02	0.00
1.62	2.00	0.00	9.19	0.02	0.00	1.65	2.00	0.00	9.18	0.03	0.00
1.66	2.00	0.00	9.17	0.01	0.00	1.68	2.00	0.00	9.16	0.02	0.00
1.70	2.00	0.00	9.15	0.02	0.00	1.72	2.00	0.00	9.14	0.02	0.00
1.74	2.00	0.00	9.13	0.02	0.00	1.76	2.00	0.00	9.12	0.02	0.00
1.78	2.00	0.00	9.11	0.02	0.00	1.80	2.00	0.00	9.10	0.02	0.00
1.82	2.00	0.00	9.09	0.02	0.00	1.84	2.00	0.00	9.08	0.02	0.00
1.86	2.00	0.00	9.07	0.02	0.00	1.88	2.00	0.00	9.06	0.02	0.00
1.90	2.00	0.00	9.05	0.02	0.00	1.92	2.00	0.00	9.04	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
1.95	2.00	0.00	9.03	0.03	0.00	1.96	2.00	0.00	9.02	0.01	0.00
1.98	2.00	0.00	9.01	0.02	0.00	2.00	2.00	0.00	9.00	0.02	0.00
2.03	2.00	0.00	8.99	0.03	0.00	2.04	2.00	0.00	8.98	0.01	0.00
2.06	2.00	0.00	8.97	0.02	0.00	2.08	2.00	0.00	8.96	0.02	0.00
2.10	2.00	0.00	8.95	0.02	0.00	2.12	2.00	0.00	8.94	0.02	0.00
2.14	2.00	0.00	8.93	0.02	0.00	2.16	2.00	0.00	8.92	0.02	0.00
2.18	2.00	0.00	8.91	0.02	0.00	2.20	2.00	0.00	8.90	0.02	0.00
2.22	2.00	0.00	8.89	0.02	0.00	2.24	2.00	0.00	8.88	0.02	0.00
2.26	2.00	0.00	8.87	0.02	0.00	2.28	2.00	0.00	8.86	0.02	0.00
2.30	2.00	0.00	8.85	0.02	0.00	2.32	2.00	0.00	8.84	0.02	0.00
2.34	2.00	0.00	8.83	0.02	0.00	2.36	2.00	0.00	8.82	0.02	0.00
2.38	2.00	0.00	8.81	0.02	0.00	2.40	2.00	0.00	8.80	0.02	0.00
2.42	2.00	0.00	8.79	0.02	0.00	2.44	2.00	0.00	8.78	0.02	0.00
2.46	2.00	0.00	8.77	0.02	0.00	2.48	2.00	0.00	8.76	0.02	0.00
2.50	2.00	0.00	8.75	0.02	0.00	2.52	2.00	0.00	8.74	0.02	0.00
2.54	2.00	0.00	8.73	0.02	0.00	2.56	2.00	0.00	8.72	0.02	0.00
2.58	2.00	0.00	8.71	0.02	0.00	2.60	2.00	0.00	8.70	0.02	0.00
2.62	2.00	0.00	8.69	0.02	0.00	2.64	2.00	0.00	8.68	0.02	0.00
2.66	2.00	0.00	8.67	0.02	0.00	2.68	2.00	0.00	8.66	0.02	0.00
2.70	2.00	0.00	8.65	0.02	0.00	2.72	2.00	0.00	8.64	0.02	0.00
2.74	2.00	0.00	8.63	0.02	0.00	2.76	2.00	0.00	8.62	0.02	0.00
2.78	2.00	0.00	8.61	0.02	0.00	2.80	2.00	0.00	8.60	0.02	0.00
2.82	2.00	0.00	8.59	0.02	0.00	2.84	2.00	0.00	8.58	0.02	0.00
2.86	2.00	0.00	8.57	0.02	0.00	2.88	2.00	0.00	8.56	0.02	0.00
2.90	2.00	0.00	8.55	0.02	0.00	2.92	2.00	0.00	8.54	0.02	0.00
2.94	2.00	0.00	8.53	0.02	0.00	2.96	2.00	0.00	8.52	0.02	0.00
2.98	2.00	0.00	8.51	0.02	0.00	3.00	2.00	0.00	8.50	0.02	0.00
3.02	2.00	0.00	8.49	0.02	0.00	3.04	2.00	0.00	8.48	0.02	0.00
3.06	2.00	0.00	8.47	0.02	0.00	3.08	2.00	0.00	8.46	0.02	0.00
3.10	2.00	0.00	8.45	0.02	0.00	3.12	2.00	0.00	8.44	0.02	0.00
3.14	2.00	0.00	8.43	0.02	0.00	3.16	2.00	0.00	8.42	0.02	0.00
3.18	2.00	0.00	8.41	0.02	0.00	3.21	2.00	0.00	8.40	0.03	0.00
3.22	2.00	0.00	8.39	0.01	0.00	3.24	2.00	0.00	8.38	0.02	0.00
3.26	2.00	0.00	8.37	0.02	0.00	3.28	2.00	0.00	8.36	0.02	0.00
3.30	2.00	0.00	8.35	0.02	0.00	3.32	2.00	0.00	8.34	0.02	0.00
3.34	2.00	0.00	8.33	0.02	0.00	3.36	2.00	0.00	8.32	0.02	0.00
3.38	2.00	0.00	8.31	0.02	0.00	3.40	2.00	0.00	8.30	0.02	0.00
3.42	2.00	0.00	8.29	0.02	0.00	3.44	2.00	0.00	8.28	0.02	0.00
3.46	2.00	0.00	8.27	0.02	0.00	3.48	2.00	0.00	8.26	0.02	0.00
3.50	2.00	0.00	8.25	0.02	0.00	3.52	2.00	0.00	8.24	0.02	0.00
3.54	2.00	0.00	8.23	0.02	0.00	3.56	2.00	0.00	8.22	0.02	0.00
3.58	2.00	0.00	8.21	0.02	0.00	3.60	2.00	0.00	8.20	0.02	0.00
3.63	2.00	0.00	8.19	0.03	0.00	3.64	2.00	0.00	8.18	0.01	0.00
3.66	2.00	0.00	8.17	0.02	0.00	3.68	2.00	0.00	8.16	0.02	0.00
3.70	2.00	0.00	8.15	0.02	0.00	3.72	2.00	0.00	8.14	0.02	0.00
3.74	2.00	0.00	8.13	0.02	0.00	3.76	2.00	0.00	8.12	0.02	0.00
3.78	2.00	0.00	8.11	0.02	0.00	3.80	2.00	0.00	8.10	0.02	0.00
3.82	2.00	0.00	8.09	0.02	0.00	3.84	2.00	0.00	8.08	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
3.86	2.00	0.00	8.07	0.02	0.00	3.88	2.00	0.00	8.06	0.02	0.00
3.90	2.00	0.00	8.05	0.02	0.00	3.92	2.00	0.00	8.04	0.02	0.00
3.94	2.00	0.00	8.03	0.02	0.00	3.96	2.00	0.00	8.02	0.02	0.00
3.98	2.00	0.00	8.01	0.02	0.00	4.00	2.00	0.00	8.00	0.02	0.00
4.03	2.00	0.00	7.99	0.03	0.00	4.04	2.00	0.00	7.98	0.01	0.00
4.06	2.00	0.00	7.97	0.02	0.00	4.08	2.00	0.00	7.96	0.02	0.00
4.10	2.00	0.00	7.95	0.02	0.00	4.12	2.00	0.00	7.94	0.02	0.00
4.14	2.00	0.00	7.93	0.02	0.00	4.16	2.00	0.00	7.92	0.02	0.00
4.18	2.00	0.00	7.91	0.02	0.00	4.20	2.00	0.00	7.90	0.02	0.00
4.22	2.00	0.00	7.89	0.02	0.00	4.24	2.00	0.00	7.88	0.02	0.00
4.26	2.00	0.00	7.87	0.02	0.00	4.28	2.00	0.00	7.86	0.02	0.00
4.30	2.00	0.00	7.85	0.02	0.00	4.32	2.00	0.00	7.84	0.02	0.00
4.34	2.00	0.00	7.83	0.02	0.00	4.36	2.00	0.00	7.82	0.02	0.00
4.38	2.00	0.00	7.81	0.02	0.00	4.40	2.00	0.00	7.80	0.02	0.00
4.42	2.00	0.00	7.79	0.02	0.00	4.44	2.00	0.00	7.78	0.02	0.00
4.46	2.00	0.00	7.77	0.02	0.00	4.48	2.00	0.00	7.76	0.02	0.00
4.50	2.00	0.00	7.75	0.02	0.00	4.52	2.00	0.00	7.74	0.02	0.00
4.54	2.00	0.00	7.73	0.02	0.00	4.56	2.00	0.00	7.72	0.02	0.00
4.58	2.00	0.00	7.71	0.02	0.00	4.60	2.00	0.00	7.70	0.02	0.00
4.62	2.00	0.00	7.69	0.02	0.00	4.64	2.00	0.00	7.68	0.02	0.00
4.66	2.00	0.00	7.67	0.02	0.00	4.68	2.00	0.00	7.66	0.02	0.00
4.70	2.00	0.00	7.65	0.02	0.00	4.72	2.00	0.00	7.64	0.02	0.00
4.74	2.00	0.00	7.63	0.02	0.00	4.76	2.00	0.00	7.62	0.02	0.00
4.78	2.00	0.00	7.61	0.02	0.00	4.80	2.00	0.00	7.60	0.02	0.00
4.82	2.00	0.00	7.59	0.02	0.00	4.84	2.00	0.00	7.58	0.02	0.00
4.86	2.00	0.00	7.57	0.02	0.00	4.88	2.00	0.00	7.56	0.02	0.00
4.90	2.00	0.00	7.55	0.02	0.00	4.92	2.00	0.00	7.54	0.02	0.00
4.94	2.00	0.00	7.53	0.02	0.00	4.96	2.00	0.00	7.52	0.02	0.00
4.98	2.00	0.00	7.51	0.02	0.00	5.00	2.00	0.00	7.50	0.02	0.00
5.02	2.00	0.00	7.49	0.02	0.00	5.04	2.00	0.00	7.48	0.02	0.00
5.06	2.00	0.00	7.47	0.02	0.00	5.08	2.00	0.00	7.46	0.02	0.00
5.11	2.00	0.00	7.45	0.03	0.00	5.12	2.00	0.00	7.44	0.01	0.00
5.14	2.00	0.00	7.43	0.02	0.00	5.16	2.00	0.00	7.42	0.02	0.00
5.18	2.00	0.00	7.41	0.02	0.00	5.20	2.00	0.00	7.40	0.02	0.00
5.22	2.00	0.00	7.39	0.02	0.00	5.24	2.00	0.00	7.38	0.02	0.00
5.26	2.00	0.00	7.37	0.02	0.00	5.28	2.00	0.00	7.36	0.02	0.00
5.30	2.00	0.00	7.35	0.02	0.00	5.32	2.00	0.00	7.34	0.02	0.00
5.34	2.00	0.00	7.33	0.02	0.00	5.36	2.00	0.00	7.32	0.02	0.00
5.38	2.00	0.00	7.31	0.02	0.00	5.40	2.00	0.00	7.30	0.02	0.00
5.42	2.00	0.00	7.29	0.02	0.00	5.44	2.00	0.00	7.28	0.02	0.00
5.46	2.00	0.00	7.27	0.02	0.00	5.48	2.00	0.00	7.26	0.02	0.00
5.50	2.00	0.00	7.25	0.02	0.00	5.52	2.00	0.00	7.24	0.02	0.00
5.54	2.00	0.00	7.23	0.02	0.00	5.56	2.00	0.00	7.22	0.02	0.00
5.58	0.69	0.31	7.21	0.02	0.04	5.60	0.71	0.29	7.20	0.02	0.04
5.62	0.68	0.32	7.19	0.02	0.05	5.64	2.00	0.00	7.18	0.02	0.00
5.66	2.00	0.00	7.17	0.02	0.00	5.68	2.00	0.00	7.16	0.02	0.00
5.70	2.00	0.00	7.15	0.02	0.00	5.72	2.00	0.00	7.14	0.02	0.00
5.74	2.00	0.00	7.13	0.02	0.00	5.76	2.00	0.00	7.12	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
5.78	2.00	0.00	7.11	0.02	0.00	5.80	2.00	0.00	7.10	0.02	0.00
5.82	2.00	0.00	7.09	0.02	0.00	5.84	2.00	0.00	7.08	0.02	0.00
5.86	2.00	0.00	7.07	0.02	0.00	5.88	2.00	0.00	7.06	0.02	0.00
5.90	2.00	0.00	7.05	0.02	0.00	5.92	2.00	0.00	7.04	0.02	0.00
5.94	2.00	0.00	7.03	0.02	0.00	5.96	2.00	0.00	7.02	0.02	0.00
5.98	2.00	0.00	7.01	0.02	0.00	6.00	2.00	0.00	7.00	0.02	0.00
6.02	2.00	0.00	6.99	0.02	0.00	6.05	2.00	0.00	6.98	0.03	0.00
6.06	2.00	0.00	6.97	0.01	0.00	6.08	2.00	0.00	6.96	0.02	0.00
6.10	2.00	0.00	6.95	0.02	0.00	6.12	2.00	0.00	6.94	0.02	0.00
6.14	2.00	0.00	6.93	0.02	0.00	6.16	2.00	0.00	6.92	0.02	0.00
6.18	2.00	0.00	6.91	0.02	0.00	6.20	2.00	0.00	6.90	0.02	0.00
6.22	2.00	0.00	6.89	0.02	0.00	6.24	2.00	0.00	6.88	0.02	0.00
6.26	2.00	0.00	6.87	0.02	0.00	6.28	2.00	0.00	6.86	0.02	0.00
6.30	2.00	0.00	6.85	0.02	0.00	6.32	2.00	0.00	6.84	0.02	0.00
6.34	2.00	0.00	6.83	0.02	0.00	6.36	2.00	0.00	6.82	0.02	0.00
6.38	2.00	0.00	6.81	0.02	0.00	6.40	2.00	0.00	6.80	0.02	0.00
6.42	2.00	0.00	6.79	0.02	0.00	6.44	2.00	0.00	6.78	0.02	0.00
6.46	2.00	0.00	6.77	0.02	0.00	6.48	2.00	0.00	6.76	0.02	0.00
6.50	2.00	0.00	6.75	0.02	0.00	6.52	2.00	0.00	6.74	0.02	0.00
6.54	2.00	0.00	6.73	0.02	0.00	6.56	2.00	0.00	6.72	0.02	0.00
6.58	2.00	0.00	6.71	0.02	0.00	6.60	2.00	0.00	6.70	0.02	0.00
6.62	2.00	0.00	6.69	0.02	0.00	6.64	2.00	0.00	6.68	0.02	0.00
6.66	2.00	0.00	6.67	0.02	0.00	6.68	2.00	0.00	6.66	0.02	0.00
6.70	2.00	0.00	6.65	0.02	0.00	6.72	2.00	0.00	6.64	0.02	0.00
6.74	2.00	0.00	6.63	0.02	0.00	6.76	2.00	0.00	6.62	0.02	0.00
6.78	2.00	0.00	6.61	0.02	0.00	6.80	2.00	0.00	6.60	0.02	0.00
6.82	2.00	0.00	6.59	0.02	0.00	6.84	2.00	0.00	6.58	0.02	0.00
6.86	2.00	0.00	6.57	0.02	0.00	6.88	2.00	0.00	6.56	0.02	0.00
6.90	2.00	0.00	6.55	0.02	0.00	6.92	2.00	0.00	6.54	0.02	0.00
6.94	2.00	0.00	6.53	0.02	0.00	6.96	2.00	0.00	6.52	0.02	0.00
6.98	2.00	0.00	6.51	0.02	0.00	7.00	2.00	0.00	6.50	0.02	0.00
7.02	2.00	0.00	6.49	0.02	0.00	7.04	2.00	0.00	6.48	0.02	0.00
7.06	2.00	0.00	6.47	0.02	0.00	7.08	2.00	0.00	6.46	0.02	0.00
7.10	2.00	0.00	6.45	0.02	0.00	7.12	2.00	0.00	6.44	0.02	0.00
7.14	2.00	0.00	6.43	0.02	0.00	7.16	2.00	0.00	6.42	0.02	0.00
7.19	2.00	0.00	6.41	0.03	0.00	7.20	2.00	0.00	6.40	0.01	0.00
7.22	2.00	0.00	6.39	0.02	0.00	7.24	2.00	0.00	6.38	0.02	0.00
7.26	2.00	0.00	6.37	0.02	0.00	7.28	2.00	0.00	6.36	0.02	0.00
7.31	2.00	0.00	6.35	0.03	0.00	7.32	2.00	0.00	6.34	0.01	0.00
7.34	2.00	0.00	6.33	0.02	0.00	7.36	2.00	0.00	6.32	0.02	0.00
7.38	2.00	0.00	6.31	0.02	0.00	7.41	2.00	0.00	6.30	0.03	0.00
7.42	2.00	0.00	6.29	0.01	0.00	7.44	2.00	0.00	6.28	0.02	0.00
7.46	2.00	0.00	6.27	0.02	0.00	7.48	2.00	0.00	6.26	0.02	0.00
7.50	2.00	0.00	6.25	0.02	0.00	7.52	2.00	0.00	6.24	0.02	0.00
7.54	2.00	0.00	6.23	0.02	0.00	7.56	2.00	0.00	6.22	0.02	0.00
7.58	2.00	0.00	6.21	0.02	0.00	7.60	2.00	0.00	6.20	0.02	0.00
7.62	2.00	0.00	6.19	0.02	0.00	7.64	2.00	0.00	6.18	0.02	0.00
7.66	2.00	0.00	6.17	0.02	0.00	7.68	2.00	0.00	6.16	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
7.70	2.00	0.00	6.15	0.02	0.00	7.72	2.00	0.00	6.14	0.02	0.00
7.74	2.00	0.00	6.13	0.02	0.00	7.76	2.00	0.00	6.12	0.02	0.00
7.78	2.00	0.00	6.11	0.02	0.00	7.80	2.00	0.00	6.10	0.02	0.00
7.82	2.00	0.00	6.09	0.02	0.00	7.84	2.00	0.00	6.08	0.02	0.00
7.86	2.00	0.00	6.07	0.02	0.00	7.88	2.00	0.00	6.06	0.02	0.00
7.90	2.00	0.00	6.05	0.02	0.00	7.92	2.00	0.00	6.04	0.02	0.00
7.94	2.00	0.00	6.03	0.02	0.00	7.96	2.00	0.00	6.02	0.02	0.00
7.98	2.00	0.00	6.01	0.02	0.00	8.01	2.00	0.00	6.00	0.03	0.00
8.02	2.00	0.00	5.99	0.01	0.00	8.04	2.00	0.00	5.98	0.02	0.00
8.06	2.00	0.00	5.97	0.02	0.00	8.08	2.00	0.00	5.96	0.02	0.00
8.10	2.00	0.00	5.95	0.02	0.00	8.12	2.00	0.00	5.94	0.02	0.00
8.15	2.00	0.00	5.93	0.03	0.00	8.17	2.00	0.00	5.92	0.02	0.00
8.18	2.00	0.00	5.91	0.01	0.00	8.20	2.00	0.00	5.90	0.02	0.00
8.22	2.00	0.00	5.89	0.02	0.00	8.24	2.00	0.00	5.88	0.02	0.00
8.26	2.00	0.00	5.87	0.02	0.00	8.28	2.00	0.00	5.86	0.02	0.00
8.30	2.00	0.00	5.85	0.02	0.00	8.32	2.00	0.00	5.84	0.02	0.00
8.34	2.00	0.00	5.83	0.02	0.00	8.36	2.00	0.00	5.82	0.02	0.00
8.38	2.00	0.00	5.81	0.02	0.00	8.40	2.00	0.00	5.80	0.02	0.00
8.42	2.00	0.00	5.79	0.02	0.00	8.44	2.00	0.00	5.78	0.02	0.00
8.46	2.00	0.00	5.77	0.02	0.00	8.48	2.00	0.00	5.76	0.02	0.00
8.50	2.00	0.00	5.75	0.02	0.00	8.52	2.00	0.00	5.74	0.02	0.00
8.54	2.00	0.00	5.73	0.02	0.00	8.56	2.00	0.00	5.72	0.02	0.00
8.58	2.00	0.00	5.71	0.02	0.00	8.60	2.00	0.00	5.70	0.02	0.00
8.62	2.00	0.00	5.69	0.02	0.00	8.64	2.00	0.00	5.68	0.02	0.00
8.66	2.00	0.00	5.67	0.02	0.00	8.68	2.00	0.00	5.66	0.02	0.00
8.70	2.00	0.00	5.65	0.02	0.00	8.72	2.00	0.00	5.64	0.02	0.00
8.74	2.00	0.00	5.63	0.02	0.00	8.76	2.00	0.00	5.62	0.02	0.00
8.78	2.00	0.00	5.61	0.02	0.00	8.80	2.00	0.00	5.60	0.02	0.00
8.82	2.00	0.00	5.59	0.02	0.00	8.84	2.00	0.00	5.58	0.02	0.00
8.86	2.00	0.00	5.57	0.02	0.00	8.88	2.00	0.00	5.56	0.02	0.00
8.90	2.00	0.00	5.55	0.02	0.00	8.92	2.00	0.00	5.54	0.02	0.00
8.94	2.00	0.00	5.53	0.02	0.00	8.96	2.00	0.00	5.52	0.02	0.00
8.98	2.00	0.00	5.51	0.02	0.00	9.00	2.00	0.00	5.50	0.02	0.00
9.02	2.00	0.00	5.49	0.02	0.00	9.04	2.00	0.00	5.48	0.02	0.00
9.06	2.00	0.00	5.47	0.02	0.00	9.08	2.00	0.00	5.46	0.02	0.00
9.10	2.00	0.00	5.45	0.02	0.00	9.12	2.00	0.00	5.44	0.02	0.00
9.14	2.00	0.00	5.43	0.02	0.00	9.16	2.00	0.00	5.42	0.02	0.00
9.18	2.00	0.00	5.41	0.02	0.00	9.20	2.00	0.00	5.40	0.02	0.00
9.22	2.00	0.00	5.39	0.02	0.00	9.24	2.00	0.00	5.38	0.02	0.00
9.26	2.00	0.00	5.37	0.02	0.00	9.29	2.00	0.00	5.36	0.03	0.00
9.30	2.00	0.00	5.35	0.01	0.00	9.32	2.00	0.00	5.34	0.02	0.00
9.34	2.00	0.00	5.33	0.02	0.00	9.36	2.00	0.00	5.32	0.02	0.00
9.38	2.00	0.00	5.31	0.02	0.00	9.40	2.00	0.00	5.30	0.02	0.00
9.42	2.00	0.00	5.29	0.02	0.00	9.44	2.00	0.00	5.28	0.02	0.00
9.46	2.00	0.00	5.27	0.02	0.00	9.48	2.00	0.00	5.26	0.02	0.00
9.50	2.00	0.00	5.25	0.02	0.00	9.52	2.00	0.00	5.24	0.02	0.00
9.54	2.00	0.00	5.23	0.02	0.00	9.56	2.00	0.00	5.22	0.02	0.00
9.58	2.00	0.00	5.21	0.02	0.00	9.60	2.00	0.00	5.20	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
9.62	2.00	0.00	5.19	0.02	0.00	9.64	2.00	0.00	5.18	0.02	0.00
9.66	2.00	0.00	5.17	0.02	0.00	9.68	2.00	0.00	5.16	0.02	0.00
9.70	2.00	0.00	5.15	0.02	0.00	9.72	2.00	0.00	5.14	0.02	0.00
9.74	2.00	0.00	5.13	0.02	0.00	9.76	2.00	0.00	5.12	0.02	0.00
9.78	2.00	0.00	5.11	0.02	0.00	9.80	2.00	0.00	5.10	0.02	0.00
9.82	2.00	0.00	5.09	0.02	0.00	9.84	2.00	0.00	5.08	0.02	0.00
9.86	2.00	0.00	5.07	0.02	0.00	9.88	2.00	0.00	5.06	0.02	0.00
9.90	2.00	0.00	5.05	0.02	0.00	9.92	2.00	0.00	5.04	0.02	0.00
9.94	2.00	0.00	5.03	0.02	0.00	9.96	2.00	0.00	5.02	0.02	0.00
9.98	2.00	0.00	5.01	0.02	0.00	10.00	2.00	0.00	5.00	0.02	0.00
10.03	2.00	0.00	4.99	0.03	0.00	10.04	2.00	0.00	4.98	0.01	0.00
10.06	2.00	0.00	4.97	0.02	0.00	10.08	2.00	0.00	4.96	0.02	0.00
10.10	2.00	0.00	4.95	0.02	0.00	10.12	2.00	0.00	4.94	0.02	0.00
10.14	2.00	0.00	4.93	0.02	0.00	10.16	2.00	0.00	4.92	0.02	0.00
10.18	2.00	0.00	4.91	0.02	0.00	10.20	2.00	0.00	4.90	0.02	0.00
10.22	2.00	0.00	4.89	0.02	0.00	10.24	2.00	0.00	4.88	0.02	0.00
10.26	2.00	0.00	4.87	0.02	0.00	10.28	2.00	0.00	4.86	0.02	0.00
10.30	2.00	0.00	4.85	0.02	0.00	10.32	2.00	0.00	4.84	0.02	0.00
10.34	2.00	0.00	4.83	0.02	0.00	10.36	2.00	0.00	4.82	0.02	0.00
10.38	2.00	0.00	4.81	0.02	0.00	10.40	2.00	0.00	4.80	0.02	0.00
10.42	2.00	0.00	4.79	0.02	0.00	10.44	2.00	0.00	4.78	0.02	0.00
10.46	2.00	0.00	4.77	0.02	0.00	10.48	2.00	0.00	4.76	0.02	0.00
10.50	2.00	0.00	4.75	0.02	0.00	10.52	2.00	0.00	4.74	0.02	0.00
10.54	2.00	0.00	4.73	0.02	0.00	10.56	2.00	0.00	4.72	0.02	0.00
10.58	2.00	0.00	4.71	0.02	0.00	10.60	2.00	0.00	4.70	0.02	0.00
10.62	2.00	0.00	4.69	0.02	0.00	10.64	2.00	0.00	4.68	0.02	0.00
10.66	2.00	0.00	4.67	0.02	0.00	10.68	2.00	0.00	4.66	0.02	0.00
10.70	2.00	0.00	4.65	0.02	0.00	10.72	2.00	0.00	4.64	0.02	0.00
10.74	2.00	0.00	4.63	0.02	0.00	10.76	2.00	0.00	4.62	0.02	0.00
10.78	2.00	0.00	4.61	0.02	0.00	10.80	2.00	0.00	4.60	0.02	0.00
10.82	2.00	0.00	4.59	0.02	0.00	10.84	2.00	0.00	4.58	0.02	0.00
10.86	2.00	0.00	4.57	0.02	0.00	10.88	2.00	0.00	4.56	0.02	0.00
10.90	2.00	0.00	4.55	0.02	0.00	10.92	2.00	0.00	4.54	0.02	0.00
10.94	2.00	0.00	4.53	0.02	0.00	10.96	2.00	0.00	4.52	0.02	0.00
10.98	2.00	0.00	4.51	0.02	0.00	11.00	2.00	0.00	4.50	0.02	0.00
11.03	2.00	0.00	4.49	0.03	0.00	11.04	2.00	0.00	4.48	0.01	0.00
11.06	2.00	0.00	4.47	0.02	0.00	11.08	2.00	0.00	4.46	0.02	0.00
11.10	2.00	0.00	4.45	0.02	0.00	11.12	2.00	0.00	4.44	0.02	0.00
11.14	2.00	0.00	4.43	0.02	0.00	11.16	2.00	0.00	4.42	0.02	0.00
11.18	2.00	0.00	4.41	0.02	0.00	11.20	2.00	0.00	4.40	0.02	0.00
11.22	2.00	0.00	4.39	0.02	0.00	11.24	2.00	0.00	4.38	0.02	0.00
11.26	2.00	0.00	4.37	0.02	0.00	11.28	2.00	0.00	4.36	0.02	0.00
11.30	2.00	0.00	4.35	0.02	0.00	11.32	2.00	0.00	4.34	0.02	0.00
11.34	2.00	0.00	4.33	0.02	0.00	11.36	2.00	0.00	4.32	0.02	0.00
11.38	2.00	0.00	4.31	0.02	0.00	11.40	2.00	0.00	4.30	0.02	0.00
11.42	2.00	0.00	4.29	0.02	0.00	11.44	2.00	0.00	4.28	0.02	0.00
11.46	2.00	0.00	4.27	0.02	0.00	11.48	2.00	0.00	4.26	0.02	0.00
11.50	2.00	0.00	4.25	0.02	0.00	11.52	2.00	0.00	4.24	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
11.54	2.00	0.00	4.23	0.02	0.00	11.56	2.00	0.00	4.22	0.02	0.00
11.58	2.00	0.00	4.21	0.02	0.00	11.60	2.00	0.00	4.20	0.02	0.00
11.62	2.00	0.00	4.19	0.02	0.00	11.64	2.00	0.00	4.18	0.02	0.00
11.66	2.00	0.00	4.17	0.02	0.00	11.68	2.00	0.00	4.16	0.02	0.00
11.70	2.00	0.00	4.15	0.02	0.00	11.72	2.00	0.00	4.14	0.02	0.00
11.74	2.00	0.00	4.13	0.02	0.00	11.76	2.00	0.00	4.12	0.02	0.00
11.78	2.00	0.00	4.11	0.02	0.00	11.80	2.00	0.00	4.10	0.02	0.00
11.82	2.00	0.00	4.09	0.02	0.00	11.84	2.00	0.00	4.08	0.02	0.00
11.86	2.00	0.00	4.07	0.02	0.00	11.88	2.00	0.00	4.06	0.02	0.00
11.90	2.00	0.00	4.05	0.02	0.00	11.92	2.00	0.00	4.04	0.02	0.00
11.94	2.00	0.00	4.03	0.02	0.00	11.96	2.00	0.00	4.02	0.02	0.00
11.99	2.00	0.00	4.01	0.03	0.00	12.00	2.00	0.00	4.00	0.01	0.00
12.02	2.00	0.00	3.99	0.02	0.00	12.04	2.00	0.00	3.98	0.02	0.00
12.06	2.00	0.00	3.97	0.02	0.00	12.08	2.00	0.00	3.96	0.02	0.00
12.10	2.00	0.00	3.95	0.02	0.00	12.12	2.00	0.00	3.94	0.02	0.00
12.14	2.00	0.00	3.93	0.02	0.00	12.16	2.00	0.00	3.92	0.02	0.00
12.18	2.00	0.00	3.91	0.02	0.00	12.20	2.00	0.00	3.90	0.02	0.00
12.22	2.00	0.00	3.89	0.02	0.00	12.24	2.00	0.00	3.88	0.02	0.00
12.26	2.00	0.00	3.87	0.02	0.00	12.28	2.00	0.00	3.86	0.02	0.00
12.30	2.00	0.00	3.85	0.02	0.00	12.32	2.00	0.00	3.84	0.02	0.00
12.34	2.00	0.00	3.83	0.02	0.00	12.36	2.00	0.00	3.82	0.02	0.00
12.38	2.00	0.00	3.81	0.02	0.00	12.40	2.00	0.00	3.80	0.02	0.00
12.42	2.00	0.00	3.79	0.02	0.00	12.44	2.00	0.00	3.78	0.02	0.00
12.46	2.00	0.00	3.77	0.02	0.00	12.48	2.00	0.00	3.76	0.02	0.00
12.50	2.00	0.00	3.75	0.02	0.00	12.52	2.00	0.00	3.74	0.02	0.00
12.54	2.00	0.00	3.73	0.02	0.00	12.56	2.00	0.00	3.72	0.02	0.00
12.58	2.00	0.00	3.71	0.02	0.00	12.61	2.00	0.00	3.70	0.03	0.00
12.62	2.00	0.00	3.69	0.01	0.00	12.64	2.00	0.00	3.68	0.02	0.00
12.66	2.00	0.00	3.67	0.02	0.00	12.68	2.00	0.00	3.66	0.02	0.00
12.70	2.00	0.00	3.65	0.02	0.00	12.72	2.00	0.00	3.64	0.02	0.00
12.74	2.00	0.00	3.63	0.02	0.00	12.76	2.00	0.00	3.62	0.02	0.00
12.78	2.00	0.00	3.61	0.02	0.00	12.80	2.00	0.00	3.60	0.02	0.00
12.82	2.00	0.00	3.59	0.02	0.00	12.84	2.00	0.00	3.58	0.02	0.00
12.86	2.00	0.00	3.57	0.02	0.00	12.88	2.00	0.00	3.56	0.02	0.00
12.90	2.00	0.00	3.55	0.02	0.00	12.92	2.00	0.00	3.54	0.02	0.00
12.94	2.00	0.00	3.53	0.02	0.00	12.96	2.00	0.00	3.52	0.02	0.00
12.98	2.00	0.00	3.51	0.02	0.00	13.00	2.00	0.00	3.50	0.02	0.00
13.02	2.00	0.00	3.49	0.02	0.00	13.04	2.00	0.00	3.48	0.02	0.00
13.06	2.00	0.00	3.47	0.02	0.00	13.08	2.00	0.00	3.46	0.02	0.00
13.10	2.00	0.00	3.45	0.02	0.00	13.12	2.00	0.00	3.44	0.02	0.00
13.14	2.00	0.00	3.43	0.02	0.00	13.16	2.00	0.00	3.42	0.02	0.00
13.18	2.00	0.00	3.41	0.02	0.00	13.20	2.00	0.00	3.40	0.02	0.00
13.22	2.00	0.00	3.39	0.02	0.00	13.24	2.00	0.00	3.38	0.02	0.00
13.26	2.00	0.00	3.37	0.02	0.00	13.28	2.00	0.00	3.36	0.02	0.00
13.30	2.00	0.00	3.35	0.02	0.00	13.32	2.00	0.00	3.34	0.02	0.00
13.34	2.00	0.00	3.33	0.02	0.00	13.36	2.00	0.00	3.32	0.02	0.00
13.38	2.00	0.00	3.31	0.02	0.00	13.40	2.00	0.00	3.30	0.02	0.00
13.42	2.00	0.00	3.29	0.02	0.00	13.44	2.00	0.00	3.28	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
13.46	2.00	0.00	3.27	0.02	0.00	13.48	2.00	0.00	3.26	0.02	0.00
13.50	2.00	0.00	3.25	0.02	0.00	13.52	2.00	0.00	3.24	0.02	0.00
13.54	2.00	0.00	3.23	0.02	0.00	13.56	2.00	0.00	3.22	0.02	0.00
13.58	2.00	0.00	3.21	0.02	0.00	13.60	2.00	0.00	3.20	0.02	0.00
13.62	2.00	0.00	3.19	0.02	0.00	13.64	2.00	0.00	3.18	0.02	0.00
13.66	2.00	0.00	3.17	0.02	0.00	13.68	2.00	0.00	3.16	0.02	0.00
13.70	2.00	0.00	3.15	0.02	0.00	13.72	2.00	0.00	3.14	0.02	0.00
13.74	2.00	0.00	3.13	0.02	0.00	13.76	2.00	0.00	3.12	0.02	0.00
13.78	2.00	0.00	3.11	0.02	0.00	13.80	2.00	0.00	3.10	0.02	0.00
13.82	2.00	0.00	3.09	0.02	0.00	13.84	2.00	0.00	3.08	0.02	0.00
13.86	2.00	0.00	3.07	0.02	0.00	13.88	2.00	0.00	3.06	0.02	0.00
13.90	2.00	0.00	3.05	0.02	0.00	13.92	2.00	0.00	3.04	0.02	0.00
13.94	2.00	0.00	3.03	0.02	0.00	13.97	2.00	0.00	3.02	0.03	0.00
13.98	2.00	0.00	3.01	0.01	0.00	14.00	2.00	0.00	3.00	0.02	0.00
14.02	2.00	0.00	2.99	0.02	0.00	14.04	2.00	0.00	2.98	0.02	0.00
14.06	2.00	0.00	2.97	0.02	0.00	14.08	2.00	0.00	2.96	0.02	0.00
14.10	2.00	0.00	2.95	0.02	0.00	14.12	2.00	0.00	2.94	0.02	0.00
14.14	2.00	0.00	2.93	0.02	0.00	14.16	2.00	0.00	2.92	0.02	0.00
14.18	2.00	0.00	2.91	0.02	0.00	14.20	2.00	0.00	2.90	0.02	0.00
14.22	2.00	0.00	2.89	0.02	0.00	14.24	2.00	0.00	2.88	0.02	0.00
14.26	2.00	0.00	2.87	0.02	0.00	14.28	2.00	0.00	2.86	0.02	0.00
14.30	2.00	0.00	2.85	0.02	0.00	14.32	2.00	0.00	2.84	0.02	0.00
14.34	2.00	0.00	2.83	0.02	0.00	14.36	2.00	0.00	2.82	0.02	0.00
14.38	2.00	0.00	2.81	0.02	0.00	14.40	2.00	0.00	2.80	0.02	0.00
14.42	2.00	0.00	2.79	0.02	0.00	14.44	2.00	0.00	2.78	0.02	0.00
14.46	2.00	0.00	2.77	0.02	0.00	14.48	2.00	0.00	2.76	0.02	0.00
14.50	2.00	0.00	2.75	0.02	0.00	14.52	2.00	0.00	2.74	0.02	0.00
14.54	2.00	0.00	2.73	0.02	0.00	14.56	2.00	0.00	2.72	0.02	0.00
14.58	2.00	0.00	2.71	0.02	0.00	14.60	2.00	0.00	2.70	0.02	0.00
14.62	2.00	0.00	2.69	0.02	0.00	14.64	2.00	0.00	2.68	0.02	0.00
14.66	2.00	0.00	2.67	0.02	0.00	14.68	2.00	0.00	2.66	0.02	0.00
14.70	2.00	0.00	2.65	0.02	0.00	14.72	2.00	0.00	2.64	0.02	0.00
14.74	2.00	0.00	2.63	0.02	0.00	14.76	2.00	0.00	2.62	0.02	0.00
14.78	2.00	0.00	2.61	0.02	0.00	14.80	2.00	0.00	2.60	0.02	0.00
14.82	2.00	0.00	2.59	0.02	0.00	14.84	2.00	0.00	2.58	0.02	0.00
14.86	2.00	0.00	2.57	0.02	0.00	14.88	2.00	0.00	2.56	0.02	0.00
14.90	2.00	0.00	2.55	0.02	0.00	14.92	2.00	0.00	2.54	0.02	0.00
14.94	2.00	0.00	2.53	0.02	0.00	14.96	2.00	0.00	2.52	0.02	0.00
14.98	2.00	0.00	2.51	0.02	0.00	15.00	2.00	0.00	2.50	0.02	0.00
15.02	2.00	0.00	2.49	0.02	0.00	15.04	2.00	0.00	2.48	0.02	0.00
15.06	2.00	0.00	2.47	0.02	0.00	15.09	2.00	0.00	2.46	0.03	0.00
15.10	2.00	0.00	2.45	0.01	0.00	15.12	2.00	0.00	2.44	0.02	0.00
15.14	2.00	0.00	2.43	0.02	0.00	15.16	2.00	0.00	2.42	0.02	0.00
15.18	2.00	0.00	2.41	0.02	0.00	15.20	2.00	0.00	2.40	0.02	0.00
15.23	2.00	0.00	2.38	0.03	0.00	15.24	2.00	0.00	2.38	0.01	0.00
15.26	2.00	0.00	2.37	0.02	0.00	15.28	2.00	0.00	2.36	0.02	0.00
15.30	2.00	0.00	2.35	0.02	0.00	15.32	2.00	0.00	2.34	0.02	0.00
15.34	2.00	0.00	2.33	0.02	0.00	15.37	2.00	0.00	2.32	0.03	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
15.38	2.00	0.00	2.31	0.01	0.00	15.40	2.00	0.00	2.30	0.02	0.00
15.42	2.00	0.00	2.29	0.02	0.00	15.44	2.00	0.00	2.28	0.02	0.00
15.46	2.00	0.00	2.27	0.02	0.00	15.48	2.00	0.00	2.26	0.02	0.00
15.50	2.00	0.00	2.25	0.02	0.00	15.52	2.00	0.00	2.24	0.02	0.00
15.54	2.00	0.00	2.23	0.02	0.00	15.56	2.00	0.00	2.22	0.02	0.00
15.58	2.00	0.00	2.21	0.02	0.00	15.60	2.00	0.00	2.20	0.02	0.00
15.62	2.00	0.00	2.19	0.02	0.00	15.64	2.00	0.00	2.18	0.02	0.00
15.66	2.00	0.00	2.17	0.02	0.00	15.68	2.00	0.00	2.16	0.02	0.00
15.70	2.00	0.00	2.15	0.02	0.00	15.72	2.00	0.00	2.14	0.02	0.00
15.74	2.00	0.00	2.13	0.02	0.00	15.76	2.00	0.00	2.12	0.02	0.00
15.78	2.00	0.00	2.11	0.02	0.00	15.82	2.00	0.00	2.09	0.04	0.00
15.82	2.00	0.00	2.09	0.00	0.00	15.84	2.00	0.00	2.08	0.02	0.00
15.86	2.00	0.00	2.07	0.02	0.00	15.88	2.00	0.00	2.06	0.02	0.00
15.90	2.00	0.00	2.05	0.02	0.00	15.93	2.00	0.00	2.04	0.03	0.00
15.94	2.00	0.00	2.03	0.01	0.00	15.96	2.00	0.00	2.02	0.02	0.00
15.98	2.00	0.00	2.01	0.02	0.00	16.00	2.00	0.00	2.00	0.02	0.00
16.02	2.00	0.00	1.99	0.02	0.00	16.04	2.00	0.00	1.98	0.02	0.00
16.06	2.00	0.00	1.97	0.02	0.00	16.08	2.00	0.00	1.96	0.02	0.00
16.10	2.00	0.00	1.95	0.02	0.00	16.12	2.00	0.00	1.94	0.02	0.00
16.14	2.00	0.00	1.93	0.02	0.00	16.16	2.00	0.00	1.92	0.02	0.00
16.18	2.00	0.00	1.91	0.02	0.00	16.20	2.00	0.00	1.90	0.02	0.00
16.22	2.00	0.00	1.89	0.02	0.00	16.24	2.00	0.00	1.88	0.02	0.00
16.26	2.00	0.00	1.87	0.02	0.00	16.28	2.00	0.00	1.86	0.02	0.00
16.30	2.00	0.00	1.85	0.02	0.00	16.32	2.00	0.00	1.84	0.02	0.00
16.34	2.00	0.00	1.83	0.02	0.00	16.36	2.00	0.00	1.82	0.02	0.00
16.38	2.00	0.00	1.81	0.02	0.00	16.40	2.00	0.00	1.80	0.02	0.00
16.42	2.00	0.00	1.79	0.02	0.00	16.44	2.00	0.00	1.78	0.02	0.00
16.46	2.00	0.00	1.77	0.02	0.00	16.48	2.00	0.00	1.76	0.02	0.00
16.50	2.00	0.00	1.75	0.02	0.00	16.52	2.00	0.00	1.74	0.02	0.00
16.54	2.00	0.00	1.73	0.02	0.00	16.56	2.00	0.00	1.72	0.02	0.00
16.58	2.00	0.00	1.71	0.02	0.00	16.60	2.00	0.00	1.70	0.02	0.00
16.62	2.00	0.00	1.69	0.02	0.00	16.64	2.00	0.00	1.68	0.02	0.00
16.66	2.00	0.00	1.67	0.02	0.00	16.68	2.00	0.00	1.66	0.02	0.00
16.70	2.00	0.00	1.65	0.02	0.00	16.72	2.00	0.00	1.64	0.02	0.00
16.74	2.00	0.00	1.63	0.02	0.00	16.76	2.00	0.00	1.62	0.02	0.00
16.78	2.00	0.00	1.61	0.02	0.00	16.80	2.00	0.00	1.60	0.02	0.00
16.82	2.00	0.00	1.59	0.02	0.00	16.84	2.00	0.00	1.58	0.02	0.00
16.86	2.00	0.00	1.57	0.02	0.00	16.88	2.00	0.00	1.56	0.02	0.00
16.90	2.00	0.00	1.55	0.02	0.00	16.92	2.00	0.00	1.54	0.02	0.00
16.94	2.00	0.00	1.53	0.02	0.00	16.96	2.00	0.00	1.52	0.02	0.00
16.98	2.00	0.00	1.51	0.02	0.00	17.00	2.00	0.00	1.50	0.02	0.00
17.02	2.00	0.00	1.49	0.02	0.00	17.04	2.00	0.00	1.48	0.02	0.00
17.06	2.00	0.00	1.47	0.02	0.00	17.08	2.00	0.00	1.46	0.02	0.00
17.10	2.00	0.00	1.45	0.02	0.00	17.12	2.00	0.00	1.44	0.02	0.00
17.14	2.00	0.00	1.43	0.02	0.00	17.17	2.00	0.00	1.42	0.03	0.00
17.18	2.00	0.00	1.41	0.01	0.00	17.20	2.00	0.00	1.40	0.02	0.00
17.22	2.00	0.00	1.39	0.02	0.00	17.24	2.00	0.00	1.38	0.02	0.00
17.26	2.00	0.00	1.37	0.02	0.00	17.28	2.00	0.00	1.36	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
17.30	2.00	0.00	1.35	0.02	0.00	17.32	2.00	0.00	1.34	0.02	0.00
17.34	2.00	0.00	1.33	0.02	0.00	17.36	2.00	0.00	1.32	0.02	0.00
17.38	2.00	0.00	1.31	0.02	0.00	17.40	2.00	0.00	1.30	0.02	0.00
17.42	2.00	0.00	1.29	0.02	0.00	17.44	2.00	0.00	1.28	0.02	0.00
17.46	2.00	0.00	1.27	0.02	0.00	17.48	2.00	0.00	1.26	0.02	0.00
17.50	2.00	0.00	1.25	0.02	0.00	17.52	2.00	0.00	1.24	0.02	0.00
17.54	2.00	0.00	1.23	0.02	0.00	17.56	2.00	0.00	1.22	0.02	0.00
17.58	2.00	0.00	1.21	0.02	0.00	17.60	2.00	0.00	1.20	0.02	0.00
17.62	2.00	0.00	1.19	0.02	0.00	17.64	2.00	0.00	1.18	0.02	0.00
17.66	2.00	0.00	1.17	0.02	0.00	17.68	2.00	0.00	1.16	0.02	0.00
17.70	2.00	0.00	1.15	0.02	0.00	17.72	2.00	0.00	1.14	0.02	0.00
17.74	2.00	0.00	1.13	0.02	0.00	17.76	2.00	0.00	1.12	0.02	0.00
17.78	2.00	0.00	1.11	0.02	0.00	17.80	2.00	0.00	1.10	0.02	0.00
17.82	2.00	0.00	1.09	0.02	0.00	17.84	2.00	0.00	1.08	0.02	0.00
17.86	2.00	0.00	1.07	0.02	0.00	17.88	2.00	0.00	1.06	0.02	0.00
17.90	2.00	0.00	1.05	0.02	0.00	17.92	2.00	0.00	1.04	0.02	0.00
17.94	2.00	0.00	1.03	0.02	0.00	17.96	2.00	0.00	1.02	0.02	0.00
17.98	2.00	0.00	1.01	0.02	0.00	18.00	2.00	0.00	1.00	0.02	0.00
18.02	2.00	0.00	0.99	0.02	0.00	18.04	2.00	0.00	0.98	0.02	0.00
18.06	2.00	0.00	0.97	0.02	0.00	18.08	2.00	0.00	0.96	0.02	0.00
18.10	2.00	0.00	0.95	0.02	0.00	18.12	2.00	0.00	0.94	0.02	0.00
18.14	2.00	0.00	0.93	0.02	0.00	18.16	2.00	0.00	0.92	0.02	0.00
18.18	2.00	0.00	0.91	0.02	0.00	18.20	2.00	0.00	0.90	0.02	0.00
18.22	2.00	0.00	0.89	0.02	0.00	18.24	2.00	0.00	0.88	0.02	0.00
18.26	2.00	0.00	0.87	0.02	0.00	18.28	2.00	0.00	0.86	0.02	0.00
18.30	2.00	0.00	0.85	0.02	0.00	18.32	2.00	0.00	0.84	0.02	0.00
18.34	2.00	0.00	0.83	0.02	0.00	18.36	2.00	0.00	0.82	0.02	0.00
18.38	2.00	0.00	0.81	0.02	0.00	18.40	2.00	0.00	0.80	0.02	0.00
18.42	2.00	0.00	0.79	0.02	0.00	18.44	2.00	0.00	0.78	0.02	0.00
18.46	2.00	0.00	0.77	0.02	0.00	18.48	2.00	0.00	0.76	0.02	0.00
18.50	2.00	0.00	0.75	0.02	0.00	18.52	2.00	0.00	0.74	0.02	0.00
18.54	2.00	0.00	0.73	0.02	0.00	18.56	2.00	0.00	0.72	0.02	0.00
18.58	2.00	0.00	0.71	0.02	0.00	18.60	2.00	0.00	0.70	0.02	0.00
18.62	2.00	0.00	0.69	0.02	0.00	18.64	2.00	0.00	0.68	0.02	0.00
18.66	2.00	0.00	0.67	0.02	0.00	18.68	2.00	0.00	0.66	0.02	0.00
18.70	2.00	0.00	0.65	0.02	0.00	18.72	2.00	0.00	0.64	0.02	0.00
18.74	2.00	0.00	0.63	0.02	0.00	18.76	2.00	0.00	0.62	0.02	0.00
18.78	2.00	0.00	0.61	0.02	0.00	18.80	2.00	0.00	0.60	0.02	0.00
18.82	2.00	0.00	0.59	0.02	0.00	18.84	2.00	0.00	0.58	0.02	0.00
18.86	2.00	0.00	0.57	0.02	0.00	18.88	2.00	0.00	0.56	0.02	0.00
18.90	2.00	0.00	0.55	0.02	0.00	18.92	2.00	0.00	0.54	0.02	0.00
18.94	2.00	0.00	0.53	0.02	0.00	18.96	2.00	0.00	0.52	0.02	0.00
18.98	2.00	0.00	0.51	0.02	0.00	19.00	2.00	0.00	0.50	0.02	0.00
19.02	2.00	0.00	0.49	0.02	0.00	19.04	2.00	0.00	0.48	0.02	0.00
19.06	2.00	0.00	0.47	0.02	0.00	19.08	2.00	0.00	0.46	0.02	0.00
19.10	2.00	0.00	0.45	0.02	0.00	19.12	2.00	0.00	0.44	0.02	0.00
19.15	2.00	0.00	0.43	0.03	0.00	19.16	2.00	0.00	0.42	0.01	0.00
19.19	2.00	0.00	0.40	0.03	0.00	19.20	2.00	0.00	0.40	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
19.22	2.00	0.00	0.39	0.02	0.00	19.24	2.00	0.00	0.38	0.02	0.00
19.26	2.00	0.00	0.37	0.02	0.00	19.28	2.00	0.00	0.36	0.02	0.00
19.30	2.00	0.00	0.35	0.02	0.00	19.32	2.00	0.00	0.34	0.02	0.00
19.34	2.00	0.00	0.33	0.02	0.00	19.36	2.00	0.00	0.32	0.02	0.00
19.38	2.00	0.00	0.31	0.02	0.00	19.40	2.00	0.00	0.30	0.02	0.00
19.42	2.00	0.00	0.29	0.02	0.00	19.44	2.00	0.00	0.28	0.02	0.00
19.46	2.00	0.00	0.27	0.02	0.00	19.48	2.00	0.00	0.26	0.02	0.00
19.50	2.00	0.00	0.25	0.02	0.00	19.52	2.00	0.00	0.24	0.02	0.00
19.54	2.00	0.00	0.23	0.02	0.00	19.56	2.00	0.00	0.22	0.02	0.00
19.58	2.00	0.00	0.21	0.02	0.00	19.60	2.00	0.00	0.20	0.02	0.00
19.62	2.00	0.00	0.19	0.02	0.00	19.64	2.00	0.00	0.18	0.02	0.00
19.66	2.00	0.00	0.17	0.02	0.00	19.68	2.00	0.00	0.16	0.02	0.00
19.70	2.00	0.00	0.15	0.02	0.00	19.72	2.00	0.00	0.14	0.02	0.00
19.74	2.00	0.00	0.13	0.02	0.00	19.76	2.00	0.00	0.12	0.02	0.00
19.78	2.00	0.00	0.11	0.02	0.00	19.80	2.00	0.00	0.10	0.02	0.00
19.82	2.00	0.00	0.09	0.02	0.00	19.84	2.00	0.00	0.08	0.02	0.00
19.86	0.72	0.28	0.07	0.02	0.00	19.88	0.73	0.27	0.06	0.02	0.00
19.90	0.73	0.27	0.05	0.02	0.00	19.92	0.71	0.29	0.04	0.02	0.00
19.94	2.00	0.00	0.03	0.02	0.00	19.96	2.00	0.00	0.02	0.02	0.00
19.98	2.00	0.00	0.01	0.02	0.00	20.00	0.76	0.24	0.00	0.02	0.00
20.02	0.80	0.00	0.00	0.00	0.00	20.04	0.82	0.00	0.00	0.00	0.00
20.06	0.82	0.00	0.00	0.00	0.00	20.08	0.81	0.00	0.00	0.00	0.00
20.10	0.80	0.00	0.00	0.00	0.00	20.12	2.00	0.00	0.00	0.00	0.00
20.15	2.00	0.00	0.00	0.00	0.00	20.16	2.00	0.00	0.00	0.00	0.00
20.18	2.00	0.00	0.00	0.00	0.00	20.20	2.00	0.00	0.00	0.00	0.00
20.22	2.00	0.00	0.00	0.00	0.00	20.25	2.00	0.00	0.00	0.00	0.00
20.26	2.00	0.00	0.00	0.00	0.00	20.28	2.00	0.00	0.00	0.00	0.00
20.30	2.00	0.00	0.00	0.00	0.00	20.32	2.00	0.00	0.00	0.00	0.00
20.34	2.00	0.00	0.00	0.00	0.00	20.36	2.00	0.00	0.00	0.00	0.00
20.38	2.00	0.00	0.00	0.00	0.00	20.40	2.00	0.00	0.00	0.00	0.00
20.42	2.00	0.00	0.00	0.00	0.00	20.44	2.00	0.00	0.00	0.00	0.00
20.46	2.00	0.00	0.00	0.00	0.00	20.48	2.00	0.00	0.00	0.00	0.00
20.50	2.00	0.00	0.00	0.00	0.00	20.52	2.00	0.00	0.00	0.00	0.00
20.54	2.00	0.00	0.00	0.00	0.00	20.56	2.00	0.00	0.00	0.00	0.00
20.58	2.00	0.00	0.00	0.00	0.00	20.60	2.00	0.00	0.00	0.00	0.00
20.62	2.00	0.00	0.00	0.00	0.00	20.64	2.00	0.00	0.00	0.00	0.00
20.66	2.00	0.00	0.00	0.00	0.00	20.68	2.00	0.00	0.00	0.00	0.00
20.70	2.00	0.00	0.00	0.00	0.00	20.72	2.00	0.00	0.00	0.00	0.00
20.74	2.00	0.00	0.00	0.00	0.00	20.76	0.61	0.00	0.00	0.00	0.00
20.78	0.62	0.00	0.00	0.00	0.00						

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI

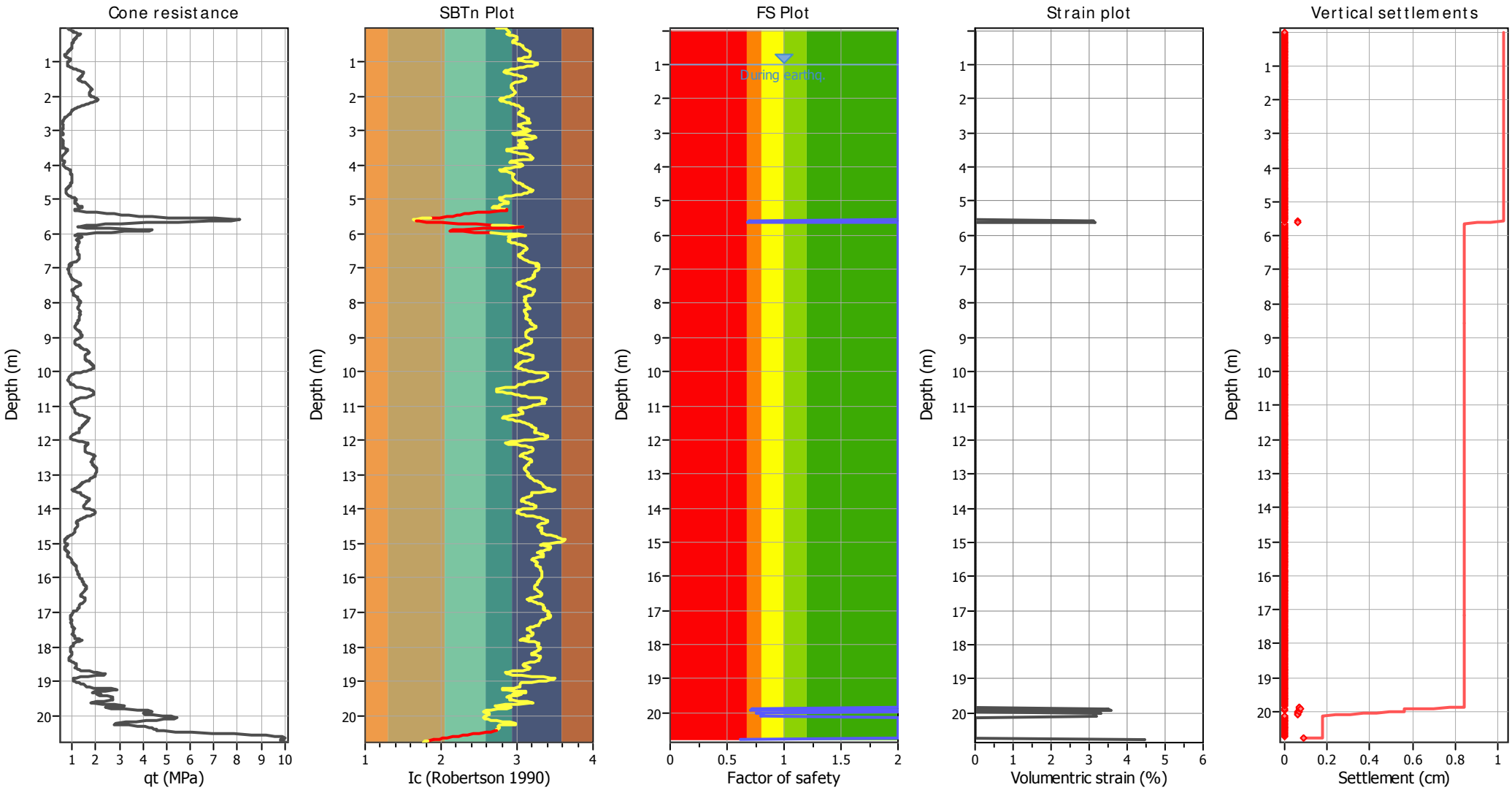
Overall liquefaction potential: 0.13

LPI = 0.00 - Liquefaction risk very low
LPI between 0.00 and 5.00 - Liquefaction risk low
LPI between 5.00 and 15.00 - Liquefaction risk high
LPI > 15.00 - Liquefaction risk very high

Abbreviations

FS: Calculated factor of safety for test point
F_L: 1 - FS
w_z: Function value of the extend of soil liquefaction according to depth
d_z: Layer thickness (m)
LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

q_t:	Total cone resistance (cone resistance q_c corrected for pore water effects)
I_c:	Soil Behaviour Type Index
FS:	Calculated Factor of Safety against liquefaction
Volumentric strain:	Post-liquefaction volumentric strain

:: Post-earthquake settlement due to soil liquefaction ::

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
1.00	13.32	2.00	0.00	1.00	0.00	1.02	12.93	2.00	0.00	1.00	0.00
1.04	13.40	2.00	0.00	1.00	0.00	1.06	13.27	2.00	0.00	1.00	0.00
1.08	13.19	2.00	0.00	1.00	0.00	1.10	13.02	2.00	0.00	1.00	0.00
1.12	13.25	2.00	0.00	1.00	0.00	1.14	14.94	2.00	0.00	1.00	0.00
1.16	15.55	2.00	0.00	1.00	0.00	1.18	16.48	2.00	0.00	1.00	0.00
1.20	17.36	2.00	0.00	1.00	0.00	1.22	19.23	2.00	0.00	1.00	0.00
1.24	20.80	2.00	0.00	1.00	0.00	1.26	22.09	2.00	0.00	1.00	0.00
1.28	23.34	2.00	0.00	1.00	0.00	1.30	24.63	2.00	0.00	1.00	0.00
1.32	24.73	2.00	0.00	1.00	0.00	1.34	24.36	2.00	0.00	1.00	0.00
1.36	23.95	2.00	0.00	1.00	0.00	1.39	23.86	2.00	0.00	1.00	0.00
1.40	23.29	2.00	0.00	1.00	0.00	1.42	23.03	2.00	0.00	1.00	0.00
1.44	22.70	2.00	0.00	1.00	0.00	1.46	22.09	2.00	0.00	1.00	0.00
1.48	21.63	2.00	0.00	1.00	0.00	1.50	20.97	2.00	0.00	1.00	0.00
1.52	20.74	2.00	0.00	1.00	0.00	1.54	21.11	2.00	0.00	1.00	0.00
1.56	22.31	2.00	0.00	1.00	0.00	1.58	23.90	2.00	0.00	1.00	0.00
1.60	25.64	2.00	0.00	1.00	0.00	1.62	26.66	2.00	0.00	1.00	0.00
1.65	27.21	2.00	0.00	1.00	0.00	1.66	27.45	2.00	0.00	1.00	0.00
1.68	28.31	2.00	0.00	1.00	0.00	1.70	28.60	2.00	0.00	1.00	0.00
1.72	29.27	2.00	0.00	1.00	0.00	1.74	29.76	2.00	0.00	1.00	0.00
1.76	29.81	2.00	0.00	1.00	0.00	1.78	30.45	2.00	0.00	1.00	0.00
1.80	30.55	2.00	0.00	1.00	0.00	1.82	30.32	2.00	0.00	1.00	0.00
1.84	30.28	2.00	0.00	1.00	0.00	1.86	29.26	2.00	0.00	1.00	0.00
1.88	28.94	2.00	0.00	1.00	0.00	1.90	29.03	2.00	0.00	1.00	0.00
1.92	28.26	2.00	0.00	1.00	0.00	1.95	28.58	2.00	0.00	1.00	0.00
1.96	28.94	2.00	0.00	1.00	0.00	1.98	29.52	2.00	0.00	1.00	0.00
2.00	30.18	2.00	0.00	1.00	0.00	2.03	30.84	2.00	0.00	1.00	0.00
2.04	32.88	2.00	0.00	1.00	0.00	2.06	34.24	2.00	0.00	1.00	0.00
2.08	34.70	2.00	0.00	1.00	0.00	2.10	34.84	2.00	0.00	1.00	0.00
2.12	35.09	2.00	0.00	1.00	0.00	2.14	34.01	2.00	0.00	1.00	0.00
2.16	32.70	2.00	0.00	1.00	0.00	2.18	30.66	2.00	0.00	1.00	0.00
2.20	29.51	2.00	0.00	1.00	0.00	2.22	28.27	2.00	0.00	1.00	0.00
2.24	26.08	2.00	0.00	1.00	0.00	2.26	24.85	2.00	0.00	1.00	0.00
2.28	23.29	2.00	0.00	1.00	0.00	2.30	21.38	2.00	0.00	1.00	0.00
2.32	20.07	2.00	0.00	1.00	0.00	2.34	19.23	2.00	0.00	1.00	0.00
2.36	17.91	2.00	0.00	1.00	0.00	2.38	16.72	2.00	0.00	1.00	0.00
2.40	16.52	2.00	0.00	1.00	0.00	2.42	15.96	2.00	0.00	1.00	0.00
2.44	15.76	2.00	0.00	1.00	0.00	2.46	15.71	2.00	0.00	1.00	0.00
2.48	15.58	2.00	0.00	1.00	0.00	2.50	15.11	2.00	0.00	1.00	0.00
2.52	14.75	2.00	0.00	1.00	0.00	2.54	14.20	2.00	0.00	1.00	0.00
2.56	13.46	2.00	0.00	1.00	0.00	2.58	12.64	2.00	0.00	1.00	0.00
2.60	12.05	2.00	0.00	1.00	0.00	2.62	11.00	2.00	0.00	1.00	0.00
2.64	10.80	2.00	0.00	1.00	0.00	2.66	10.49	2.00	0.00	1.00	0.00
2.68	10.03	2.00	0.00	1.00	0.00	2.70	10.15	2.00	0.00	1.00	0.00
2.72	9.84	2.00	0.00	1.00	0.00	2.74	9.03	2.00	0.00	1.00	0.00
2.76	8.68	2.00	0.00	1.00	0.00	2.78	8.68	2.00	0.00	1.00	0.00
2.80	9.04	2.00	0.00	1.00	0.00	2.82	9.94	2.00	0.00	1.00	0.00
2.84	10.13	2.00	0.00	1.00	0.00	2.86	10.00	2.00	0.00	1.00	0.00
2.88	9.99	2.00	0.00	1.00	0.00	2.90	9.15	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
2.92	9.82	2.00	0.00	1.00	0.00	2.94	9.50	2.00	0.00	1.00	0.00
2.96	9.07	2.00	0.00	1.00	0.00	2.98	7.97	2.00	0.00	1.00	0.00
3.00	7.84	2.00	0.00	1.00	0.00	3.02	8.01	2.00	0.00	1.00	0.00
3.04	8.48	2.00	0.00	1.00	0.00	3.06	9.59	2.00	0.00	1.00	0.00
3.08	10.02	2.00	0.00	1.00	0.00	3.10	9.70	2.00	0.00	1.00	0.00
3.12	9.24	2.00	0.00	1.00	0.00	3.14	8.37	2.00	0.00	1.00	0.00
3.16	7.91	2.00	0.00	1.00	0.00	3.18	7.71	2.00	0.00	1.00	0.00
3.21	7.39	2.00	0.00	1.00	0.00	3.22	7.61	2.00	0.00	1.00	0.00
3.24	8.18	2.00	0.00	1.00	0.00	3.26	8.90	2.00	0.00	1.00	0.00
3.28	9.50	2.00	0.00	1.00	0.00	3.30	9.52	2.00	0.00	1.00	0.00
3.32	8.92	2.00	0.00	1.00	0.00	3.34	8.46	2.00	0.00	1.00	0.00
3.36	8.48	2.00	0.00	1.00	0.00	3.38	9.08	2.00	0.00	1.00	0.00
3.40	9.89	2.00	0.00	1.00	0.00	3.42	9.83	2.00	0.00	1.00	0.00
3.44	9.27	2.00	0.00	1.00	0.00	3.46	8.49	2.00	0.00	1.00	0.00
3.48	8.11	2.00	0.00	1.00	0.00	3.50	8.53	2.00	0.00	1.00	0.00
3.52	10.08	2.00	0.00	1.00	0.00	3.54	11.32	2.00	0.00	1.00	0.00
3.56	12.29	2.00	0.00	1.00	0.00	3.58	12.19	2.00	0.00	1.00	0.00
3.60	11.00	2.00	0.00	1.00	0.00	3.63	10.89	2.00	0.00	1.00	0.00
3.64	10.77	2.00	0.00	1.00	0.00	3.66	10.36	2.00	0.00	1.00	0.00
3.68	9.88	2.00	0.00	1.00	0.00	3.70	9.29	2.00	0.00	1.00	0.00
3.72	8.78	2.00	0.00	1.00	0.00	3.74	8.69	2.00	0.00	1.00	0.00
3.76	8.31	2.00	0.00	1.00	0.00	3.78	7.83	2.00	0.00	1.00	0.00
3.80	7.50	2.00	0.00	1.00	0.00	3.82	7.23	2.00	0.00	1.00	0.00
3.84	7.25	2.00	0.00	1.00	0.00	3.86	7.93	2.00	0.00	1.00	0.00
3.88	8.97	2.00	0.00	1.00	0.00	3.90	10.82	2.00	0.00	1.00	0.00
3.92	10.11	2.00	0.00	1.00	0.00	3.94	9.36	2.00	0.00	1.00	0.00
3.96	9.18	2.00	0.00	1.00	0.00	3.98	8.82	2.00	0.00	1.00	0.00
4.00	8.73	2.00	0.00	1.00	0.00	4.03	8.99	2.00	0.00	1.00	0.00
4.04	9.19	2.00	0.00	1.00	0.00	4.06	9.76	2.00	0.00	1.00	0.00
4.08	10.94	2.00	0.00	1.00	0.00	4.10	11.76	2.00	0.00	1.00	0.00
4.12	12.56	2.00	0.00	1.00	0.00	4.14	13.32	2.00	0.00	1.00	0.00
4.16	13.46	2.00	0.00	1.00	0.00	4.18	13.30	2.00	0.00	1.00	0.00
4.20	13.10	2.00	0.00	1.00	0.00	4.22	13.13	2.00	0.00	1.00	0.00
4.24	13.00	2.00	0.00	1.00	0.00	4.26	13.11	2.00	0.00	1.00	0.00
4.28	13.75	2.00	0.00	1.00	0.00	4.30	14.25	2.00	0.00	1.00	0.00
4.32	14.35	2.00	0.00	1.00	0.00	4.34	14.19	2.00	0.00	1.00	0.00
4.36	13.96	2.00	0.00	1.00	0.00	4.38	13.93	2.00	0.00	1.00	0.00
4.40	14.07	2.00	0.00	1.00	0.00	4.42	14.03	2.00	0.00	1.00	0.00
4.44	13.74	2.00	0.00	1.00	0.00	4.46	13.55	2.00	0.00	1.00	0.00
4.48	13.46	2.00	0.00	1.00	0.00	4.50	13.52	2.00	0.00	1.00	0.00
4.52	13.23	2.00	0.00	1.00	0.00	4.54	13.07	2.00	0.00	1.00	0.00
4.56	12.78	2.00	0.00	1.00	0.00	4.58	12.43	2.00	0.00	1.00	0.00
4.60	12.37	2.00	0.00	1.00	0.00	4.62	12.14	2.00	0.00	1.00	0.00
4.64	11.79	2.00	0.00	1.00	0.00	4.66	11.28	2.00	0.00	1.00	0.00
4.68	10.76	2.00	0.00	1.00	0.00	4.70	10.29	2.00	0.00	1.00	0.00
4.72	10.10	2.00	0.00	1.00	0.00	4.74	9.82	2.00	0.00	1.00	0.00
4.76	9.76	2.00	0.00	1.00	0.00	4.78	10.00	2.00	0.00	1.00	0.00
4.80	10.20	2.00	0.00	1.00	0.00	4.82	10.21	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
4.84	10.45	2.00	0.00	1.00	0.00	4.86	10.33	2.00	0.00	1.00	0.00
4.88	10.22	2.00	0.00	1.00	0.00	4.90	11.81	2.00	0.00	1.00	0.00
4.92	12.63	2.00	0.00	1.00	0.00	4.94	13.54	2.00	0.00	1.00	0.00
4.96	14.54	2.00	0.00	1.00	0.00	4.98	15.32	2.00	0.00	1.00	0.00
5.00	15.58	2.00	0.00	1.00	0.00	5.02	15.55	2.00	0.00	1.00	0.00
5.04	14.90	2.00	0.00	1.00	0.00	5.06	14.70	2.00	0.00	1.00	0.00
5.08	13.80	2.00	0.00	1.00	0.00	5.11	14.58	2.00	0.00	1.00	0.00
5.12	15.42	2.00	0.00	1.00	0.00	5.14	15.97	2.00	0.00	1.00	0.00
5.16	16.20	2.00	0.00	1.00	0.00	5.18	16.08	2.00	0.00	1.00	0.00
5.20	16.38	2.00	0.00	1.00	0.00	5.22	18.56	2.00	0.00	1.00	0.00
5.24	19.65	2.00	0.00	1.00	0.00	5.26	18.29	2.00	0.00	1.00	0.00
5.28	16.30	2.00	0.00	1.00	0.00	5.30	14.15	2.00	0.00	1.00	0.00
5.32	13.81	2.00	0.00	1.00	0.00	5.34	15.42	2.00	0.00	1.00	0.00
5.36	19.67	2.00	0.00	1.00	0.00	5.38	84.23	2.00	0.00	1.00	0.00
5.40	87.70	2.00	0.00	1.00	0.00	5.42	90.69	2.00	0.00	1.00	0.00
5.44	93.76	2.00	0.00	1.00	0.00	5.46	96.38	2.00	0.00	1.00	0.00
5.48	99.00	2.00	0.00	1.00	0.00	5.50	101.62	2.00	0.00	1.00	0.00
5.52	102.41	2.00	0.00	1.00	0.00	5.54	87.75	2.00	0.00	1.00	0.00
5.56	93.55	2.00	0.00	1.00	0.00	5.58	103.28	0.69	3.11	1.00	0.06
5.60	105.46	0.71	3.04	1.00	0.06	5.62	101.91	0.68	3.15	1.00	0.06
5.64	88.98	2.00	0.00	1.00	0.00	5.66	77.13	2.00	0.00	1.00	0.00
5.68	87.96	2.00	0.00	1.00	0.00	5.70	88.18	2.00	0.00	1.00	0.00
5.72	89.32	2.00	0.00	1.00	0.00	5.74	26.65	2.00	0.00	1.00	0.00
5.76	20.22	2.00	0.00	1.00	0.00	5.78	16.09	2.00	0.00	1.00	0.00
5.80	14.95	2.00	0.00	1.00	0.00	5.82	16.27	2.00	0.00	1.00	0.00
5.84	88.91	2.00	0.00	1.00	0.00	5.86	108.72	2.00	0.00	1.00	0.00
5.88	112.43	2.00	0.00	1.00	0.00	5.90	101.51	2.00	0.00	1.00	0.00
5.92	96.94	2.00	0.00	1.00	0.00	5.94	98.12	2.00	0.00	1.00	0.00
5.96	88.01	2.00	0.00	1.00	0.00	5.98	26.48	2.00	0.00	1.00	0.00
6.00	19.72	2.00	0.00	1.00	0.00	6.02	14.44	2.00	0.00	1.00	0.00
6.05	12.55	2.00	0.00	1.00	0.00	6.06	15.25	2.00	0.00	1.00	0.00
6.08	18.99	2.00	0.00	1.00	0.00	6.10	17.60	2.00	0.00	1.00	0.00
6.12	16.25	2.00	0.00	1.00	0.00	6.14	14.67	2.00	0.00	1.00	0.00
6.16	14.44	2.00	0.00	1.00	0.00	6.18	15.38	2.00	0.00	1.00	0.00
6.20	15.21	2.00	0.00	1.00	0.00	6.22	15.97	2.00	0.00	1.00	0.00
6.24	16.38	2.00	0.00	1.00	0.00	6.26	15.91	2.00	0.00	1.00	0.00
6.28	15.77	2.00	0.00	1.00	0.00	6.30	15.69	2.00	0.00	1.00	0.00
6.32	15.26	2.00	0.00	1.00	0.00	6.34	14.81	2.00	0.00	1.00	0.00
6.36	14.99	2.00	0.00	1.00	0.00	6.38	14.97	2.00	0.00	1.00	0.00
6.40	14.55	2.00	0.00	1.00	0.00	6.42	14.52	2.00	0.00	1.00	0.00
6.44	14.61	2.00	0.00	1.00	0.00	6.46	14.61	2.00	0.00	1.00	0.00
6.48	15.07	2.00	0.00	1.00	0.00	6.50	14.93	2.00	0.00	1.00	0.00
6.52	14.79	2.00	0.00	1.00	0.00	6.54	14.88	2.00	0.00	1.00	0.00
6.56	14.86	2.00	0.00	1.00	0.00	6.58	15.30	2.00	0.00	1.00	0.00
6.60	15.81	2.00	0.00	1.00	0.00	6.62	15.90	2.00	0.00	1.00	0.00
6.64	15.91	2.00	0.00	1.00	0.00	6.66	16.08	2.00	0.00	1.00	0.00
6.68	15.91	2.00	0.00	1.00	0.00	6.70	15.63	2.00	0.00	1.00	0.00
6.72	15.80	2.00	0.00	1.00	0.00	6.74	15.52	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
6.76	15.13	2.00	0.00	1.00	0.00	6.78	14.41	2.00	0.00	1.00	0.00
6.80	14.10	2.00	0.00	1.00	0.00	6.82	13.71	2.00	0.00	1.00	0.00
6.84	12.90	2.00	0.00	1.00	0.00	6.86	7.23	2.00	0.00	1.00	0.00
6.88	11.94	2.00	0.00	1.00	0.00	6.90	11.34	2.00	0.00	1.00	0.00
6.92	11.07	2.00	0.00	1.00	0.00	6.94	10.70	2.00	0.00	1.00	0.00
6.96	10.41	2.00	0.00	1.00	0.00	6.98	10.17	2.00	0.00	1.00	0.00
7.00	9.93	2.00	0.00	1.00	0.00	7.02	9.84	2.00	0.00	1.00	0.00
7.04	9.63	2.00	0.00	1.00	0.00	7.06	9.84	2.00	0.00	1.00	0.00
7.08	10.07	2.00	0.00	1.00	0.00	7.10	10.25	2.00	0.00	1.00	0.00
7.12	10.20	2.00	0.00	1.00	0.00	7.14	10.13	2.00	0.00	1.00	0.00
7.16	10.29	2.00	0.00	1.00	0.00	7.19	10.63	2.00	0.00	1.00	0.00
7.20	10.59	2.00	0.00	1.00	0.00	7.22	10.77	2.00	0.00	1.00	0.00
7.24	10.90	2.00	0.00	1.00	0.00	7.26	10.99	2.00	0.00	1.00	0.00
7.28	11.44	2.00	0.00	1.00	0.00	7.31	11.45	2.00	0.00	1.00	0.00
7.32	11.99	2.00	0.00	1.00	0.00	7.34	12.27	2.00	0.00	1.00	0.00
7.36	12.55	2.00	0.00	1.00	0.00	7.38	13.22	2.00	0.00	1.00	0.00
7.41	14.36	2.00	0.00	1.00	0.00	7.42	15.22	2.00	0.00	1.00	0.00
7.44	15.39	2.00	0.00	1.00	0.00	7.46	15.48	2.00	0.00	1.00	0.00
7.48	15.54	2.00	0.00	1.00	0.00	7.50	14.82	2.00	0.00	1.00	0.00
7.52	14.18	2.00	0.00	1.00	0.00	7.54	13.46	2.00	0.00	1.00	0.00
7.56	12.80	2.00	0.00	1.00	0.00	7.58	12.46	2.00	0.00	1.00	0.00
7.60	12.12	2.00	0.00	1.00	0.00	7.62	11.67	2.00	0.00	1.00	0.00
7.64	11.34	2.00	0.00	1.00	0.00	7.66	11.11	2.00	0.00	1.00	0.00
7.68	11.57	2.00	0.00	1.00	0.00	7.70	11.72	2.00	0.00	1.00	0.00
7.72	11.89	2.00	0.00	1.00	0.00	7.74	11.61	2.00	0.00	1.00	0.00
7.76	11.72	2.00	0.00	1.00	0.00	7.78	11.79	2.00	0.00	1.00	0.00
7.80	12.38	2.00	0.00	1.00	0.00	7.82	13.70	2.00	0.00	1.00	0.00
7.84	13.79	2.00	0.00	1.00	0.00	7.86	13.74	2.00	0.00	1.00	0.00
7.88	13.65	2.00	0.00	1.00	0.00	7.90	13.70	2.00	0.00	1.00	0.00
7.92	14.34	2.00	0.00	1.00	0.00	7.94	14.93	2.00	0.00	1.00	0.00
7.96	15.01	2.00	0.00	1.00	0.00	7.98	15.10	2.00	0.00	1.00	0.00
8.01	15.20	2.00	0.00	1.00	0.00	8.02	14.90	2.00	0.00	1.00	0.00
8.04	14.11	2.00	0.00	1.00	0.00	8.06	14.64	2.00	0.00	1.00	0.00
8.08	14.52	2.00	0.00	1.00	0.00	8.10	14.26	2.00	0.00	1.00	0.00
8.12	13.79	2.00	0.00	1.00	0.00	8.15	13.34	2.00	0.00	1.00	0.00
8.17	13.16	2.00	0.00	1.00	0.00	8.18	13.75	2.00	0.00	1.00	0.00
8.20	14.17	2.00	0.00	1.00	0.00	8.22	14.57	2.00	0.00	1.00	0.00
8.24	14.70	2.00	0.00	1.00	0.00	8.26	14.73	2.00	0.00	1.00	0.00
8.28	14.50	2.00	0.00	1.00	0.00	8.30	14.20	2.00	0.00	1.00	0.00
8.32	14.67	2.00	0.00	1.00	0.00	8.34	14.78	2.00	0.00	1.00	0.00
8.36	14.40	2.00	0.00	1.00	0.00	8.38	14.22	2.00	0.00	1.00	0.00
8.40	14.33	2.00	0.00	1.00	0.00	8.42	14.24	2.00	0.00	1.00	0.00
8.44	14.32	2.00	0.00	1.00	0.00	8.46	14.40	2.00	0.00	1.00	0.00
8.48	14.00	2.00	0.00	1.00	0.00	8.50	13.57	2.00	0.00	1.00	0.00
8.52	13.47	2.00	0.00	1.00	0.00	8.54	13.15	2.00	0.00	1.00	0.00
8.56	13.03	2.00	0.00	1.00	0.00	8.58	13.11	2.00	0.00	1.00	0.00
8.60	12.66	2.00	0.00	1.00	0.00	8.62	12.54	2.00	0.00	1.00	0.00
8.64	12.28	2.00	0.00	1.00	0.00	8.66	11.88	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
8.68	11.53	2.00	0.00	1.00	0.00	8.70	11.67	2.00	0.00	1.00	0.00
8.72	11.32	2.00	0.00	1.00	0.00	8.74	11.69	2.00	0.00	1.00	0.00
8.76	12.21	2.00	0.00	1.00	0.00	8.78	12.84	2.00	0.00	1.00	0.00
8.80	13.15	2.00	0.00	1.00	0.00	8.82	13.42	2.00	0.00	1.00	0.00
8.84	14.01	2.00	0.00	1.00	0.00	8.86	13.99	2.00	0.00	1.00	0.00
8.88	14.27	2.00	0.00	1.00	0.00	8.90	14.31	2.00	0.00	1.00	0.00
8.92	14.67	2.00	0.00	1.00	0.00	8.94	14.80	2.00	0.00	1.00	0.00
8.96	14.93	2.00	0.00	1.00	0.00	8.98	14.74	2.00	0.00	1.00	0.00
9.00	14.32	2.00	0.00	1.00	0.00	9.02	13.98	2.00	0.00	1.00	0.00
9.04	13.56	2.00	0.00	1.00	0.00	9.06	12.54	2.00	0.00	1.00	0.00
9.08	12.03	2.00	0.00	1.00	0.00	9.10	11.83	2.00	0.00	1.00	0.00
9.12	11.49	2.00	0.00	1.00	0.00	9.14	11.45	2.00	0.00	1.00	0.00
9.16	11.36	2.00	0.00	1.00	0.00	9.18	11.33	2.00	0.00	1.00	0.00
9.20	11.66	2.00	0.00	1.00	0.00	9.22	12.29	2.00	0.00	1.00	0.00
9.24	13.31	2.00	0.00	1.00	0.00	9.26	13.94	2.00	0.00	1.00	0.00
9.29	13.89	2.00	0.00	1.00	0.00	9.30	13.91	2.00	0.00	1.00	0.00
9.32	14.29	2.00	0.00	1.00	0.00	9.34	15.19	2.00	0.00	1.00	0.00
9.36	16.15	2.00	0.00	1.00	0.00	9.38	16.95	2.00	0.00	1.00	0.00
9.40	16.90	2.00	0.00	1.00	0.00	9.42	17.42	2.00	0.00	1.00	0.00
9.44	17.72	2.00	0.00	1.00	0.00	9.46	17.46	2.00	0.00	1.00	0.00
9.48	17.54	2.00	0.00	1.00	0.00	9.50	16.90	2.00	0.00	1.00	0.00
9.52	15.86	2.00	0.00	1.00	0.00	9.54	15.57	2.00	0.00	1.00	0.00
9.56	16.13	2.00	0.00	1.00	0.00	9.58	16.10	2.00	0.00	1.00	0.00
9.60	15.52	2.00	0.00	1.00	0.00	9.62	15.78	2.00	0.00	1.00	0.00
9.64	15.86	2.00	0.00	1.00	0.00	9.66	16.08	2.00	0.00	1.00	0.00
9.68	16.20	2.00	0.00	1.00	0.00	9.70	17.05	2.00	0.00	1.00	0.00
9.72	17.51	2.00	0.00	1.00	0.00	9.74	17.68	2.00	0.00	1.00	0.00
9.76	18.08	2.00	0.00	1.00	0.00	9.78	18.42	2.00	0.00	1.00	0.00
9.80	18.58	2.00	0.00	1.00	0.00	9.82	18.94	2.00	0.00	1.00	0.00
9.84	19.42	2.00	0.00	1.00	0.00	9.86	19.70	2.00	0.00	1.00	0.00
9.88	19.46	2.00	0.00	1.00	0.00	9.90	19.27	2.00	0.00	1.00	0.00
9.92	18.51	2.00	0.00	1.00	0.00	9.94	18.25	2.00	0.00	1.00	0.00
9.96	17.28	2.00	0.00	1.00	0.00	9.98	16.09	2.00	0.00	1.00	0.00
10.00	15.38	2.00	0.00	1.00	0.00	10.03	12.91	2.00	0.00	1.00	0.00
10.04	11.85	2.00	0.00	1.00	0.00	10.06	10.77	2.00	0.00	1.00	0.00
10.08	10.16	2.00	0.00	1.00	0.00	10.10	9.53	2.00	0.00	1.00	0.00
10.12	9.40	2.00	0.00	1.00	0.00	10.14	8.96	2.00	0.00	1.00	0.00
10.16	8.52	2.00	0.00	1.00	0.00	10.18	8.49	2.00	0.00	1.00	0.00
10.20	8.50	2.00	0.00	1.00	0.00	10.22	8.05	2.00	0.00	1.00	0.00
10.24	7.77	2.00	0.00	1.00	0.00	10.26	7.81	2.00	0.00	1.00	0.00
10.28	8.04	2.00	0.00	1.00	0.00	10.30	8.60	2.00	0.00	1.00	0.00
10.32	9.09	2.00	0.00	1.00	0.00	10.34	9.08	2.00	0.00	1.00	0.00
10.36	8.81	2.00	0.00	1.00	0.00	10.38	9.11	2.00	0.00	1.00	0.00
10.40	10.44	2.00	0.00	1.00	0.00	10.42	11.14	2.00	0.00	1.00	0.00
10.44	10.34	2.00	0.00	1.00	0.00	10.46	10.67	2.00	0.00	1.00	0.00
10.48	13.40	2.00	0.00	1.00	0.00	10.50	15.90	2.00	0.00	1.00	0.00
10.52	17.18	2.00	0.00	1.00	0.00	10.54	17.10	2.00	0.00	1.00	0.00
10.56	18.33	2.00	0.00	1.00	0.00	10.58	18.60	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
10.60	18.84	2.00	0.00	1.00	0.00	10.62	18.79	2.00	0.00	1.00	0.00
10.64	18.80	2.00	0.00	1.00	0.00	10.66	18.23	2.00	0.00	1.00	0.00
10.68	18.10	2.00	0.00	1.00	0.00	10.70	17.53	2.00	0.00	1.00	0.00
10.72	16.85	2.00	0.00	1.00	0.00	10.74	15.70	2.00	0.00	1.00	0.00
10.76	14.50	2.00	0.00	1.00	0.00	10.78	12.73	2.00	0.00	1.00	0.00
10.80	11.52	2.00	0.00	1.00	0.00	10.82	10.37	2.00	0.00	1.00	0.00
10.84	11.42	2.00	0.00	1.00	0.00	10.86	10.74	2.00	0.00	1.00	0.00
10.88	10.09	2.00	0.00	1.00	0.00	10.90	9.46	2.00	0.00	1.00	0.00
10.92	8.52	2.00	0.00	1.00	0.00	10.94	8.47	2.00	0.00	1.00	0.00
10.96	9.68	2.00	0.00	1.00	0.00	10.98	9.61	2.00	0.00	1.00	0.00
11.00	9.21	2.00	0.00	1.00	0.00	11.03	9.24	2.00	0.00	1.00	0.00
11.04	9.69	2.00	0.00	1.00	0.00	11.06	10.27	2.00	0.00	1.00	0.00
11.08	10.33	2.00	0.00	1.00	0.00	11.10	10.49	2.00	0.00	1.00	0.00
11.12	10.46	2.00	0.00	1.00	0.00	11.14	10.45	2.00	0.00	1.00	0.00
11.16	10.24	2.00	0.00	1.00	0.00	11.18	10.33	2.00	0.00	1.00	0.00
11.20	10.50	2.00	0.00	1.00	0.00	11.22	10.91	2.00	0.00	1.00	0.00
11.24	11.13	2.00	0.00	1.00	0.00	11.26	11.91	2.00	0.00	1.00	0.00
11.28	13.17	2.00	0.00	1.00	0.00	11.30	14.28	2.00	0.00	1.00	0.00
11.32	15.69	2.00	0.00	1.00	0.00	11.34	15.88	2.00	0.00	1.00	0.00
11.36	16.10	2.00	0.00	1.00	0.00	11.38	15.95	2.00	0.00	1.00	0.00
11.40	15.42	2.00	0.00	1.00	0.00	11.42	15.21	2.00	0.00	1.00	0.00
11.44	15.65	2.00	0.00	1.00	0.00	11.46	15.11	2.00	0.00	1.00	0.00
11.48	14.79	2.00	0.00	1.00	0.00	11.50	14.72	2.00	0.00	1.00	0.00
11.52	14.35	2.00	0.00	1.00	0.00	11.54	13.86	2.00	0.00	1.00	0.00
11.56	13.49	2.00	0.00	1.00	0.00	11.58	13.25	2.00	0.00	1.00	0.00
11.60	13.25	2.00	0.00	1.00	0.00	11.62	12.90	2.00	0.00	1.00	0.00
11.64	12.32	2.00	0.00	1.00	0.00	11.66	12.11	2.00	0.00	1.00	0.00
11.68	11.71	2.00	0.00	1.00	0.00	11.70	11.74	2.00	0.00	1.00	0.00
11.72	11.90	2.00	0.00	1.00	0.00	11.74	11.82	2.00	0.00	1.00	0.00
11.76	11.61	2.00	0.00	1.00	0.00	11.78	11.44	2.00	0.00	1.00	0.00
11.80	10.69	2.00	0.00	1.00	0.00	11.82	9.50	2.00	0.00	1.00	0.00
11.84	9.85	2.00	0.00	1.00	0.00	11.86	8.94	2.00	0.00	1.00	0.00
11.88	8.65	2.00	0.00	1.00	0.00	11.90	8.51	2.00	0.00	1.00	0.00
11.92	8.26	2.00	0.00	1.00	0.00	11.94	8.08	2.00	0.00	1.00	0.00
11.96	8.43	2.00	0.00	1.00	0.00	11.99	9.13	2.00	0.00	1.00	0.00
12.00	10.18	2.00	0.00	1.00	0.00	12.02	11.25	2.00	0.00	1.00	0.00
12.04	12.93	2.00	0.00	1.00	0.00	12.06	14.81	2.00	0.00	1.00	0.00
12.08	15.57	2.00	0.00	1.00	0.00	12.10	15.05	2.00	0.00	1.00	0.00
12.12	14.67	2.00	0.00	1.00	0.00	12.14	14.58	2.00	0.00	1.00	0.00
12.16	14.39	2.00	0.00	1.00	0.00	12.18	14.03	2.00	0.00	1.00	0.00
12.20	13.67	2.00	0.00	1.00	0.00	12.22	13.72	2.00	0.00	1.00	0.00
12.24	13.64	2.00	0.00	1.00	0.00	12.26	13.67	2.00	0.00	1.00	0.00
12.28	13.67	2.00	0.00	1.00	0.00	12.30	13.61	2.00	0.00	1.00	0.00
12.32	13.85	2.00	0.00	1.00	0.00	12.34	13.94	2.00	0.00	1.00	0.00
12.36	14.55	2.00	0.00	1.00	0.00	12.38	15.87	2.00	0.00	1.00	0.00
12.40	16.55	2.00	0.00	1.00	0.00	12.42	17.38	2.00	0.00	1.00	0.00
12.44	17.82	2.00	0.00	1.00	0.00	12.46	17.88	2.00	0.00	1.00	0.00
12.48	17.23	2.00	0.00	1.00	0.00	12.50	17.08	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
12.52	17.12	2.00	0.00	1.00	0.00	12.54	16.81	2.00	0.00	1.00	0.00
12.56	16.62	2.00	0.00	1.00	0.00	12.58	16.42	2.00	0.00	1.00	0.00
12.61	16.11	2.00	0.00	1.00	0.00	12.62	16.02	2.00	0.00	1.00	0.00
12.64	16.38	2.00	0.00	1.00	0.00	12.66	16.69	2.00	0.00	1.00	0.00
12.68	16.69	2.00	0.00	1.00	0.00	12.70	16.58	2.00	0.00	1.00	0.00
12.72	16.67	2.00	0.00	1.00	0.00	12.74	17.28	2.00	0.00	1.00	0.00
12.76	17.16	2.00	0.00	1.00	0.00	12.78	17.68	2.00	0.00	1.00	0.00
12.80	17.87	2.00	0.00	1.00	0.00	12.82	18.22	2.00	0.00	1.00	0.00
12.84	18.45	2.00	0.00	1.00	0.00	12.86	18.09	2.00	0.00	1.00	0.00
12.88	17.99	2.00	0.00	1.00	0.00	12.90	18.04	2.00	0.00	1.00	0.00
12.92	18.02	2.00	0.00	1.00	0.00	12.94	17.91	2.00	0.00	1.00	0.00
12.96	17.48	2.00	0.00	1.00	0.00	12.98	17.49	2.00	0.00	1.00	0.00
13.00	17.68	2.00	0.00	1.00	0.00	13.02	17.53	2.00	0.00	1.00	0.00
13.04	17.08	2.00	0.00	1.00	0.00	13.06	16.72	2.00	0.00	1.00	0.00
13.08	16.36	2.00	0.00	1.00	0.00	13.10	15.79	2.00	0.00	1.00	0.00
13.12	15.14	2.00	0.00	1.00	0.00	13.14	14.95	2.00	0.00	1.00	0.00
13.16	14.81	2.00	0.00	1.00	0.00	13.18	14.48	2.00	0.00	1.00	0.00
13.20	13.77	2.00	0.00	1.00	0.00	13.22	12.98	2.00	0.00	1.00	0.00
13.24	12.28	2.00	0.00	1.00	0.00	13.26	12.08	2.00	0.00	1.00	0.00
13.28	11.80	2.00	0.00	1.00	0.00	13.30	11.43	2.00	0.00	1.00	0.00
13.32	11.10	2.00	0.00	1.00	0.00	13.34	11.01	2.00	0.00	1.00	0.00
13.36	10.39	2.00	0.00	1.00	0.00	13.38	9.96	2.00	0.00	1.00	0.00
13.40	9.66	2.00	0.00	1.00	0.00	13.42	8.98	2.00	0.00	1.00	0.00
13.44	8.31	2.00	0.00	1.00	0.00	13.46	8.47	2.00	0.00	1.00	0.00
13.48	9.49	2.00	0.00	1.00	0.00	13.50	10.42	2.00	0.00	1.00	0.00
13.52	11.22	2.00	0.00	1.00	0.00	13.54	11.61	2.00	0.00	1.00	0.00
13.56	11.81	2.00	0.00	1.00	0.00	13.58	11.31	2.00	0.00	1.00	0.00
13.60	11.89	2.00	0.00	1.00	0.00	13.62	12.36	2.00	0.00	1.00	0.00
13.64	12.95	2.00	0.00	1.00	0.00	13.66	13.47	2.00	0.00	1.00	0.00
13.68	14.20	2.00	0.00	1.00	0.00	13.70	14.59	2.00	0.00	1.00	0.00
13.72	14.64	2.00	0.00	1.00	0.00	13.74	14.72	2.00	0.00	1.00	0.00
13.76	14.09	2.00	0.00	1.00	0.00	13.78	13.76	2.00	0.00	1.00	0.00
13.80	13.48	2.00	0.00	1.00	0.00	13.82	13.35	2.00	0.00	1.00	0.00
13.84	13.28	2.00	0.00	1.00	0.00	13.86	13.15	2.00	0.00	1.00	0.00
13.88	12.98	2.00	0.00	1.00	0.00	13.90	12.58	2.00	0.00	1.00	0.00
13.92	12.38	2.00	0.00	1.00	0.00	13.94	12.31	2.00	0.00	1.00	0.00
13.97	12.41	2.00	0.00	1.00	0.00	13.98	14.02	2.00	0.00	1.00	0.00
14.00	14.89	2.00	0.00	1.00	0.00	14.02	15.49	2.00	0.00	1.00	0.00
14.04	16.39	2.00	0.00	1.00	0.00	14.06	16.59	2.00	0.00	1.00	0.00
14.08	17.00	2.00	0.00	1.00	0.00	14.10	16.96	2.00	0.00	1.00	0.00
14.12	16.42	2.00	0.00	1.00	0.00	14.14	15.95	2.00	0.00	1.00	0.00
14.16	15.16	2.00	0.00	1.00	0.00	14.18	14.88	2.00	0.00	1.00	0.00
14.20	14.34	2.00	0.00	1.00	0.00	14.22	13.41	2.00	0.00	1.00	0.00
14.24	12.49	2.00	0.00	1.00	0.00	14.26	11.97	2.00	0.00	1.00	0.00
14.28	11.69	2.00	0.00	1.00	0.00	14.30	10.93	2.00	0.00	1.00	0.00
14.32	10.48	2.00	0.00	1.00	0.00	14.34	10.15	2.00	0.00	1.00	0.00
14.36	9.66	2.00	0.00	1.00	0.00	14.38	9.51	2.00	0.00	1.00	0.00
14.40	9.66	2.00	0.00	1.00	0.00	14.42	10.20	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
14.44	10.23	2.00	0.00	1.00	0.00	14.46	10.27	2.00	0.00	1.00	0.00
14.48	10.06	2.00	0.00	1.00	0.00	14.50	9.99	2.00	0.00	1.00	0.00
14.52	9.81	2.00	0.00	1.00	0.00	14.54	9.62	2.00	0.00	1.00	0.00
14.56	9.30	2.00	0.00	1.00	0.00	14.58	9.09	2.00	0.00	1.00	0.00
14.60	9.05	2.00	0.00	1.00	0.00	14.62	9.08	2.00	0.00	1.00	0.00
14.64	8.98	2.00	0.00	1.00	0.00	14.66	8.99	2.00	0.00	1.00	0.00
14.68	8.79	2.00	0.00	1.00	0.00	14.70	8.70	2.00	0.00	1.00	0.00
14.72	8.50	2.00	0.00	1.00	0.00	14.74	7.97	2.00	0.00	1.00	0.00
14.76	7.56	2.00	0.00	1.00	0.00	14.78	7.02	2.00	0.00	1.00	0.00
14.80	6.22	2.00	0.00	1.00	0.00	14.82	6.49	2.00	0.00	1.00	0.00
14.84	6.04	2.00	0.00	1.00	0.00	14.86	5.65	2.00	0.00	1.00	0.00
14.88	5.28	2.00	0.00	1.00	0.00	14.90	5.10	2.00	0.00	1.00	0.00
14.92	5.01	2.00	0.00	1.00	0.00	14.94	5.14	2.00	0.00	1.00	0.00
14.96	4.93	2.00	0.00	1.00	0.00	14.98	5.18	2.00	0.00	1.00	0.00
15.00	5.64	2.00	0.00	1.00	0.00	15.02	6.45	2.00	0.00	1.00	0.00
15.04	6.41	2.00	0.00	1.00	0.00	15.06	5.89	2.00	0.00	1.00	0.00
15.09	5.42	2.00	0.00	1.00	0.00	15.10	5.27	2.00	0.00	1.00	0.00
15.12	5.27	2.00	0.00	1.00	0.00	15.14	5.31	2.00	0.00	1.00	0.00
15.16	5.35	2.00	0.00	1.00	0.00	15.18	5.68	2.00	0.00	1.00	0.00
15.20	6.02	2.00	0.00	1.00	0.00	15.23	6.16	2.00	0.00	1.00	0.00
15.24	6.43	2.00	0.00	1.00	0.00	15.26	6.72	2.00	0.00	1.00	0.00
15.28	6.70	2.00	0.00	1.00	0.00	15.30	6.33	2.00	0.00	1.00	0.00
15.32	6.23	2.00	0.00	1.00	0.00	15.34	6.35	2.00	0.00	1.00	0.00
15.37	6.16	2.00	0.00	1.00	0.00	15.38	6.25	2.00	0.00	1.00	0.00
15.40	6.52	2.00	0.00	1.00	0.00	15.42	7.13	2.00	0.00	1.00	0.00
15.44	7.44	2.00	0.00	1.00	0.00	15.46	7.63	2.00	0.00	1.00	0.00
15.48	7.97	2.00	0.00	1.00	0.00	15.50	7.83	2.00	0.00	1.00	0.00
15.52	7.89	2.00	0.00	1.00	0.00	15.54	7.79	2.00	0.00	1.00	0.00
15.56	7.86	2.00	0.00	1.00	0.00	15.58	8.28	2.00	0.00	1.00	0.00
15.60	8.60	2.00	0.00	1.00	0.00	15.62	8.75	2.00	0.00	1.00	0.00
15.64	9.00	2.00	0.00	1.00	0.00	15.66	8.99	2.00	0.00	1.00	0.00
15.68	8.95	2.00	0.00	1.00	0.00	15.70	9.06	2.00	0.00	1.00	0.00
15.72	8.97	2.00	0.00	1.00	0.00	15.74	9.29	2.00	0.00	1.00	0.00
15.76	9.27	2.00	0.00	1.00	0.00	15.78	9.53	2.00	0.00	1.00	0.00
15.82	9.35	2.00	0.00	1.00	0.00	15.82	9.66	2.00	0.00	1.00	0.00
15.84	9.77	2.00	0.00	1.00	0.00	15.86	9.63	2.00	0.00	1.00	0.00
15.88	9.83	2.00	0.00	1.00	0.00	15.90	9.96	2.00	0.00	1.00	0.00
15.93	9.97	2.00	0.00	1.00	0.00	15.94	10.02	2.00	0.00	1.00	0.00
15.96	10.28	2.00	0.00	1.00	0.00	15.98	10.15	2.00	0.00	1.00	0.00
16.00	10.20	2.00	0.00	1.00	0.00	16.02	10.59	2.00	0.00	1.00	0.00
16.04	10.98	2.00	0.00	1.00	0.00	16.06	11.01	2.00	0.00	1.00	0.00
16.08	11.07	2.00	0.00	1.00	0.00	16.10	11.15	2.00	0.00	1.00	0.00
16.12	11.48	2.00	0.00	1.00	0.00	16.14	11.55	2.00	0.00	1.00	0.00
16.16	11.69	2.00	0.00	1.00	0.00	16.18	11.75	2.00	0.00	1.00	0.00
16.20	11.85	2.00	0.00	1.00	0.00	16.22	12.28	2.00	0.00	1.00	0.00
16.24	12.27	2.00	0.00	1.00	0.00	16.26	12.27	2.00	0.00	1.00	0.00
16.28	12.24	2.00	0.00	1.00	0.00	16.30	12.42	2.00	0.00	1.00	0.00
16.32	12.37	2.00	0.00	1.00	0.00	16.34	12.24	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
16.36	11.90	2.00	0.00	1.00	0.00	16.38	11.76	2.00	0.00	1.00	0.00
16.40	11.53	2.00	0.00	1.00	0.00	16.42	11.10	2.00	0.00	1.00	0.00
16.44	11.03	2.00	0.00	1.00	0.00	16.46	10.79	2.00	0.00	1.00	0.00
16.48	10.73	2.00	0.00	1.00	0.00	16.50	10.41	2.00	0.00	1.00	0.00
16.52	10.31	2.00	0.00	1.00	0.00	16.54	10.77	2.00	0.00	1.00	0.00
16.56	11.27	2.00	0.00	1.00	0.00	16.58	11.59	2.00	0.00	1.00	0.00
16.60	12.01	2.00	0.00	1.00	0.00	16.62	11.97	2.00	0.00	1.00	0.00
16.64	12.26	2.00	0.00	1.00	0.00	16.66	11.82	2.00	0.00	1.00	0.00
16.68	11.83	2.00	0.00	1.00	0.00	16.70	11.24	2.00	0.00	1.00	0.00
16.72	11.10	2.00	0.00	1.00	0.00	16.74	10.93	2.00	0.00	1.00	0.00
16.76	10.24	2.00	0.00	1.00	0.00	16.78	9.90	2.00	0.00	1.00	0.00
16.80	9.96	2.00	0.00	1.00	0.00	16.82	10.01	2.00	0.00	1.00	0.00
16.84	9.69	2.00	0.00	1.00	0.00	16.86	9.49	2.00	0.00	1.00	0.00
16.88	9.47	2.00	0.00	1.00	0.00	16.90	9.42	2.00	0.00	1.00	0.00
16.92	9.19	2.00	0.00	1.00	0.00	16.94	8.80	2.00	0.00	1.00	0.00
16.96	8.21	2.00	0.00	1.00	0.00	16.98	8.04	2.00	0.00	1.00	0.00
17.00	7.78	2.00	0.00	1.00	0.00	17.02	7.37	2.00	0.00	1.00	0.00
17.04	7.48	2.00	0.00	1.00	0.00	17.06	7.45	2.00	0.00	1.00	0.00
17.08	7.30	2.00	0.00	1.00	0.00	17.10	7.03	2.00	0.00	1.00	0.00
17.12	6.68	2.00	0.00	1.00	0.00	17.14	6.67	2.00	0.00	1.00	0.00
17.17	6.69	2.00	0.00	1.00	0.00	17.18	6.80	2.00	0.00	1.00	0.00
17.20	6.99	2.00	0.00	1.00	0.00	17.22	7.06	2.00	0.00	1.00	0.00
17.24	7.03	2.00	0.00	1.00	0.00	17.26	7.10	2.00	0.00	1.00	0.00
17.28	6.86	2.00	0.00	1.00	0.00	17.30	6.95	2.00	0.00	1.00	0.00
17.32	7.10	2.00	0.00	1.00	0.00	17.34	7.12	2.00	0.00	1.00	0.00
17.36	6.97	2.00	0.00	1.00	0.00	17.38	6.93	2.00	0.00	1.00	0.00
17.40	7.04	2.00	0.00	1.00	0.00	17.42	7.24	2.00	0.00	1.00	0.00
17.44	7.69	2.00	0.00	1.00	0.00	17.46	7.89	2.00	0.00	1.00	0.00
17.48	8.02	2.00	0.00	1.00	0.00	17.50	7.87	2.00	0.00	1.00	0.00
17.52	7.71	2.00	0.00	1.00	0.00	17.54	7.54	2.00	0.00	1.00	0.00
17.56	7.49	2.00	0.00	1.00	0.00	17.58	7.47	2.00	0.00	1.00	0.00
17.60	7.36	2.00	0.00	1.00	0.00	17.62	7.31	2.00	0.00	1.00	0.00
17.64	7.34	2.00	0.00	1.00	0.00	17.66	7.43	2.00	0.00	1.00	0.00
17.68	7.85	2.00	0.00	1.00	0.00	17.70	8.21	2.00	0.00	1.00	0.00
17.72	8.24	2.00	0.00	1.00	0.00	17.74	8.07	2.00	0.00	1.00	0.00
17.76	8.25	2.00	0.00	1.00	0.00	17.78	8.42	2.00	0.00	1.00	0.00
17.80	11.30	2.00	0.00	1.00	0.00	17.82	10.71	2.00	0.00	1.00	0.00
17.84	9.24	2.00	0.00	1.00	0.00	17.86	8.73	2.00	0.00	1.00	0.00
17.88	7.96	2.00	0.00	1.00	0.00	17.90	7.67	2.00	0.00	1.00	0.00
17.92	7.43	2.00	0.00	1.00	0.00	17.94	7.50	2.00	0.00	1.00	0.00
17.96	7.28	2.00	0.00	1.00	0.00	17.98	7.05	2.00	0.00	1.00	0.00
18.00	6.56	2.00	0.00	1.00	0.00	18.02	6.36	2.00	0.00	1.00	0.00
18.04	6.25	2.00	0.00	1.00	0.00	18.06	6.30	2.00	0.00	1.00	0.00
18.08	6.33	2.00	0.00	1.00	0.00	18.10	6.56	2.00	0.00	1.00	0.00
18.12	6.56	2.00	0.00	1.00	0.00	18.14	6.50	2.00	0.00	1.00	0.00
18.16	6.76	2.00	0.00	1.00	0.00	18.18	6.99	2.00	0.00	1.00	0.00
18.20	7.01	2.00	0.00	1.00	0.00	18.22	7.01	2.00	0.00	1.00	0.00
18.24	6.76	2.00	0.00	1.00	0.00	18.26	6.33	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
18.28	6.20	2.00	0.00	1.00	0.00	18.30	6.13	2.00	0.00	1.00	0.00
18.32	6.20	2.00	0.00	1.00	0.00	18.34	6.16	2.00	0.00	1.00	0.00
18.36	6.11	2.00	0.00	1.00	0.00	18.38	6.12	2.00	0.00	1.00	0.00
18.40	6.10	2.00	0.00	1.00	0.00	18.42	6.20	2.00	0.00	1.00	0.00
18.44	6.57	2.00	0.00	1.00	0.00	18.46	7.38	2.00	0.00	1.00	0.00
18.48	7.75	2.00	0.00	1.00	0.00	18.50	8.32	2.00	0.00	1.00	0.00
18.52	8.48	2.00	0.00	1.00	0.00	18.54	8.40	2.00	0.00	1.00	0.00
18.56	8.22	2.00	0.00	1.00	0.00	18.58	7.95	2.00	0.00	1.00	0.00
18.60	7.84	2.00	0.00	1.00	0.00	18.62	8.05	2.00	0.00	1.00	0.00
18.64	8.39	2.00	0.00	1.00	0.00	18.66	8.99	2.00	0.00	1.00	0.00
18.68	9.67	2.00	0.00	1.00	0.00	18.70	10.63	2.00	0.00	1.00	0.00
18.72	11.90	2.00	0.00	1.00	0.00	18.74	14.05	2.00	0.00	1.00	0.00
18.76	15.18	2.00	0.00	1.00	0.00	18.78	15.77	2.00	0.00	1.00	0.00
18.80	19.23	2.00	0.00	1.00	0.00	18.82	18.54	2.00	0.00	1.00	0.00
18.84	15.04	2.00	0.00	1.00	0.00	18.86	11.73	2.00	0.00	1.00	0.00
18.88	9.50	2.00	0.00	1.00	0.00	18.90	8.02	2.00	0.00	1.00	0.00
18.92	7.29	2.00	0.00	1.00	0.00	18.94	7.23	2.00	0.00	1.00	0.00
18.96	7.36	2.00	0.00	1.00	0.00	18.98	7.50	2.00	0.00	1.00	0.00
19.00	7.66	2.00	0.00	1.00	0.00	19.02	8.34	2.00	0.00	1.00	0.00
19.04	8.96	2.00	0.00	1.00	0.00	19.06	9.27	2.00	0.00	1.00	0.00
19.08	9.79	2.00	0.00	1.00	0.00	19.10	10.38	2.00	0.00	1.00	0.00
19.12	10.76	2.00	0.00	1.00	0.00	19.15	11.31	2.00	0.00	1.00	0.00
19.16	12.07	2.00	0.00	1.00	0.00	19.19	13.60	2.00	0.00	1.00	0.00
19.20	16.01	2.00	0.00	1.00	0.00	19.22	20.42	2.00	0.00	1.00	0.00
19.24	21.97	2.00	0.00	1.00	0.00	19.26	21.30	2.00	0.00	1.00	0.00
19.28	17.44	2.00	0.00	1.00	0.00	19.30	13.84	2.00	0.00	1.00	0.00
19.32	11.78	2.00	0.00	1.00	0.00	19.34	14.92	2.00	0.00	1.00	0.00
19.36	17.39	2.00	0.00	1.00	0.00	19.38	15.79	2.00	0.00	1.00	0.00
19.40	13.88	2.00	0.00	1.00	0.00	19.42	14.16	2.00	0.00	1.00	0.00
19.44	18.98	2.00	0.00	1.00	0.00	19.46	20.66	2.00	0.00	1.00	0.00
19.48	19.47	2.00	0.00	1.00	0.00	19.50	19.28	2.00	0.00	1.00	0.00
19.52	19.75	2.00	0.00	1.00	0.00	19.54	20.42	2.00	0.00	1.00	0.00
19.56	20.09	2.00	0.00	1.00	0.00	19.58	17.20	2.00	0.00	1.00	0.00
19.60	14.31	2.00	0.00	1.00	0.00	19.62	11.97	2.00	0.00	1.00	0.00
19.64	11.98	2.00	0.00	1.00	0.00	19.66	15.36	2.00	0.00	1.00	0.00
19.68	21.48	2.00	0.00	1.00	0.00	19.70	24.08	2.00	0.00	1.00	0.00
19.72	25.36	2.00	0.00	1.00	0.00	19.74	21.35	2.00	0.00	1.00	0.00
19.76	16.49	2.00	0.00	1.00	0.00	19.78	15.54	2.00	0.00	1.00	0.00
19.80	19.57	2.00	0.00	1.00	0.00	19.82	22.51	2.00	0.00	1.00	0.00
19.84	28.67	2.00	0.00	1.00	0.00	19.86	92.02	0.72	3.49	1.00	0.07
19.88	92.80	0.73	3.47	1.00	0.07	19.90	92.22	0.73	3.49	1.00	0.07
19.92	89.55	0.71	3.59	1.00	0.07	19.94	29.06	2.00	0.00	1.00	0.00
19.96	29.46	2.00	0.00	1.00	0.00	19.98	32.66	2.00	0.00	1.00	0.00
20.00	96.67	0.76	3.33	1.00	0.07	20.02	101.32	0.80	3.17	1.00	0.06
20.04	103.15	0.82	3.11	1.00	0.06	20.06	103.26	0.82	3.11	1.00	0.06
20.08	101.98	0.81	3.15	1.00	0.06	20.10	100.60	0.80	3.19	1.00	0.06
20.12	36.28	2.00	0.00	1.00	0.00	20.15	33.83	2.00	0.00	1.00	0.00
20.16	31.17	2.00	0.00	1.00	0.00	20.18	26.87	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
20.20	24.02	2.00	0.00	1.00	0.00	20.22	20.23	2.00	0.00	1.00	0.00
20.25	18.02	2.00	0.00	1.00	0.00	20.26	21.29	2.00	0.00	1.00	0.00
20.28	24.88	2.00	0.00	1.00	0.00	20.30	28.19	2.00	0.00	1.00	0.00
20.32	30.12	2.00	0.00	1.00	0.00	20.34	31.21	2.00	0.00	1.00	0.00
20.36	32.24	2.00	0.00	1.00	0.00	20.38	33.16	2.00	0.00	1.00	0.00
20.40	33.60	2.00	0.00	1.00	0.00	20.42	33.92	2.00	0.00	1.00	0.00
20.44	34.00	2.00	0.00	1.00	0.00	20.46	34.99	2.00	0.00	1.00	0.00
20.48	39.84	2.00	0.00	1.00	0.00	20.50	108.56	2.00	0.00	1.00	0.00
20.52	115.90	2.00	0.00	1.00	0.00	20.54	124.82	2.00	0.00	1.00	0.00
20.56	131.37	2.00	0.00	1.00	0.00	20.58	132.87	2.00	0.00	1.00	0.00
20.60	134.63	2.00	0.00	1.00	0.00	20.62	131.40	2.00	0.00	1.00	0.00
20.64	127.47	2.00	0.00	1.00	0.00	20.66	120.21	2.00	0.00	1.00	0.00
20.68	109.20	2.00	0.00	1.00	0.00	20.70	93.16	2.00	0.00	1.00	0.00
20.72	75.05	2.00	0.00	1.00	0.00	20.74	70.05	2.00	0.00	1.00	0.00
20.76	71.21	0.61	4.48	1.00	0.09	20.78	72.34	0.62	4.41	1.00	0.09

Total estimated settlement: 1.03

Abbreviations

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumentric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

:: Strength loss calculation Idriss & Boulanger (2008) ::

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.02	0.80	13.68	4.18	57.15	2.72	0.07	181.93
0.04	0.80	13.65	5.18	70.63	2.84	0.07	89.12
0.06	0.84	14.30	5.32	76.05	2.86	0.07	61.61
0.08	0.90	15.33	5.45	83.53	2.87	0.07	49.09
0.10	0.96	16.31	5.49	89.53	2.88	0.07	41.45
0.12	1.01	17.20	5.60	96.31	2.89	0.07	36.15
0.14	1.07	18.15	5.66	102.72	2.90	0.07	32.48
0.16	1.14	19.29	5.73	110.57	2.90	0.08	30.00
0.18	1.24	21.02	5.55	116.75	2.89	0.08	28.88
0.20	1.32	22.46	5.42	121.64	2.87	0.08	27.61
0.22	1.32	22.37	5.70	127.41	2.90	0.08	24.87
0.24	1.25	21.23	6.21	131.77	2.95	0.07	21.53
0.26	1.18	19.99	6.73	134.49	3.00	0.07	18.65
0.28	1.17	19.77	6.72	132.86	3.00	0.07	17.07
0.30	1.15	19.48	6.68	130.17	2.99	0.07	15.66
0.32	1.11	18.86	6.73	126.95	3.00	0.07	14.18
0.34	1.08	18.20	6.76	122.98	3.00	0.07	12.86
0.36	1.05	17.80	6.64	118.15	2.99	0.07	11.87
0.38	1.04	17.63	6.43	113.29	2.97	0.07	11.13
0.40	1.05	17.66	6.17	108.89	2.95	0.07	10.59
0.42	1.04	17.58	6.07	106.68	2.94	0.07	10.04
0.44	1.03	17.39	6.13	106.60	2.94	0.07	9.48
0.46	1.00	16.93	6.47	109.53	2.97	0.07	8.83
0.48	0.98	16.54	6.85	113.24	3.01	0.07	8.26
0.50	0.97	16.40	7.15	117.30	3.04	0.07	7.86
0.52	0.98	16.45	7.35	120.92	3.05	0.07	7.57
0.54	0.98	16.51	7.54	124.47	3.07	0.07	7.32
0.56	0.98	16.49	7.67	126.46	3.08	0.07	7.04
0.58	0.98	16.46	7.72	127.15	3.08	0.07	6.78
0.60	0.97	16.28	7.76	126.38	3.09	0.07	6.48
0.62	0.94	15.87	7.91	125.50	3.10	0.07	6.11
0.64	0.91	15.31	8.13	124.39	3.12	0.07	5.71
0.66	0.88	14.75	8.36	123.33	3.13	0.07	5.33
0.68	0.86	14.34	8.50	121.94	3.14	0.07	5.03
0.70	0.83	13.86	8.69	120.44	3.16	0.07	4.72
0.72	0.81	13.53	8.76	118.48	3.16	0.07	4.48
0.74	0.79	13.27	8.75	116.10	3.16	0.07	4.27
0.76	0.77	12.84	8.76	112.54	3.16	0.07	4.03
0.78	0.74	12.30	8.77	107.92	3.17	0.06	3.76
0.80	0.70	11.64	8.94	104.03	3.18	0.06	3.47
0.82	0.68	11.35	8.98	101.96	3.18	0.06	3.30
0.84	0.68	11.35	8.97	101.86	3.18	0.06	3.23
0.86	0.71	11.86	8.61	102.06	3.15	0.06	3.29
0.88	0.78	12.92	7.84	101.26	3.09	0.06	3.51
0.90	0.84	13.96	7.33	102.40	3.05	0.07	3.71
0.92	0.90	15.06	6.86	103.30	3.01	0.07	3.91
0.94	0.92	15.39	6.99	107.54	3.02	0.07	3.91
0.96	0.92	15.29	7.28	111.28	3.05	0.07	3.81

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.98	0.86	14.29	8.24	117.71	3.12	0.07	3.49
1.00	0.81	13.40	9.15	122.67	3.19	0.07	3.20
1.02	0.78	12.98	9.88	128.23	3.24	0.06	3.04
1.04	0.78	13.00	10.16	132.06	3.26	0.07	2.98
1.06	0.79	13.13	10.25	134.64	3.27	0.07	2.96
1.08	0.79	13.03	10.27	133.77	3.27	0.07	2.88
1.10	0.79	13.04	10.06	131.23	3.26	0.06	2.83
1.12	0.82	13.64	9.33	127.24	3.21	0.07	2.90
1.14	0.87	14.49	8.49	123.06	3.14	0.07	3.03
1.16	0.94	15.58	7.63	118.90	3.08	0.07	3.20
1.18	0.99	16.39	7.10	116.37	3.03	0.07	3.31
1.20	1.06	17.64	6.49	114.46	2.98	0.07	3.50
1.22	1.14	19.09	5.94	113.32	2.92	0.07	3.73
1.24	1.24	20.69	5.48	113.35	2.88	0.08	3.97
1.26	1.32	22.07	5.17	114.11	2.84	0.08	4.17
1.28	1.40	23.35	5.02	117.29	2.83	0.08	4.35
1.30	1.45	24.24	5.04	122.07	2.83	0.09	4.44
1.32	1.47	24.57	5.29	130.06	2.86	0.09	4.43
1.34	1.46	24.34	5.75	140.02	2.91	0.08	4.32
1.36	1.44	24.03	6.25	150.23	2.95	0.08	4.20
1.39	1.42	23.66	6.78	160.48	3.00	0.08	4.04
1.40	1.40	23.35	7.20	168.03	3.04	0.08	3.96
1.42	1.38	22.95	7.55	173.18	3.07	0.08	3.83
1.44	1.35	22.54	7.74	174.45	3.08	0.08	3.71
1.46	1.32	22.06	7.87	173.65	3.10	0.08	3.58
1.48	1.29	21.47	8.01	171.92	3.11	0.08	3.43
1.50	1.26	21.01	8.12	170.66	3.12	0.07	3.31
1.52	1.25	20.83	8.16	170.02	3.12	0.07	3.24
1.54	1.28	21.27	7.98	169.75	3.10	0.07	3.26
1.56	1.34	22.33	7.56	168.89	3.07	0.08	3.38
1.58	1.43	23.86	6.99	166.77	3.02	0.08	3.56
1.60	1.52	25.32	6.50	164.52	2.98	0.08	3.73
1.62	1.58	26.44	6.17	163.21	2.95	0.08	3.84
1.65	1.62	27.04	6.05	163.60	2.94	0.08	3.86
1.66	1.65	27.59	5.98	165.05	2.93	0.09	3.91
1.68	1.68	28.05	5.96	167.34	2.93	0.09	3.92
1.70	1.72	28.67	5.94	170.27	2.92	0.09	3.96
1.72	1.75	29.15	5.95	173.46	2.93	0.09	3.98
1.74	1.77	29.55	5.97	176.57	2.93	0.09	3.98
1.76	1.79	29.95	6.01	179.85	2.93	0.09	3.99
1.78	1.81	30.21	6.05	182.78	2.94	0.09	3.98
1.80	1.82	30.37	6.09	185.04	2.94	0.09	3.95
1.82	1.82	30.31	6.15	186.26	2.94	0.09	3.92
1.84	1.79	29.87	6.26	186.89	2.96	0.09	3.84
1.86	1.76	29.40	6.37	187.26	2.97	0.09	3.76
1.88	1.74	28.97	6.45	186.73	2.97	0.08	3.68
1.90	1.72	28.64	6.46	184.96	2.97	0.08	3.62
1.92	1.71	28.54	6.39	182.46	2.97	0.08	3.59

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
1.95	1.72	28.56	6.32	180.57	2.96	0.08	3.56
1.96	1.74	29.03	6.18	179.26	2.95	0.09	3.61
1.98	1.78	29.59	6.00	177.57	2.93	0.09	3.66
2.00	1.81	30.23	5.78	174.74	2.91	0.09	3.72
2.03	1.88	31.37	5.41	169.78	2.87	0.09	3.83
2.04	1.96	32.75	5.03	164.64	2.83	0.10	3.99
2.06	2.04	34.05	4.69	159.81	2.79	0.10	4.12
2.08	2.08	34.68	4.54	157.45	2.77	0.10	4.18
2.10	2.09	34.94	4.47	156.30	2.76	0.10	4.19
2.12	2.08	34.69	4.52	156.82	2.77	0.10	4.14
2.14	2.04	33.96	4.69	159.14	2.79	0.10	4.03
2.16	1.95	32.47	5.01	162.78	2.83	0.10	3.83
2.18	1.86	30.95	5.36	165.86	2.86	0.09	3.64
2.20	1.77	29.45	5.68	167.18	2.90	0.09	3.44
2.22	1.68	27.89	5.98	166.88	2.93	0.09	3.24
2.24	1.59	26.31	6.30	165.81	2.96	0.08	3.05
2.26	1.49	24.63	6.62	162.98	2.99	0.08	2.84
2.28	1.40	23.04	6.87	158.28	3.01	0.08	2.64
2.30	1.30	21.42	7.09	151.89	3.03	0.08	2.44
2.32	1.22	20.05	7.26	145.58	3.05	0.07	2.28
2.34	1.15	18.89	7.42	140.24	3.06	0.07	2.14
2.36	1.09	17.79	7.60	135.28	3.07	0.07	2.00
2.38	1.04	16.89	7.75	130.82	3.09	0.07	1.89
2.40	1.00	16.22	7.75	125.68	3.09	0.07	1.81
2.42	0.98	15.88	7.60	120.61	3.07	0.07	1.76
2.44	0.96	15.59	7.44	115.92	3.06	0.07	1.72
2.46	0.95	15.45	7.25	112.01	3.04	0.07	1.70
2.48	0.94	15.23	7.12	108.46	3.03	0.07	1.67
2.50	0.92	14.91	7.02	104.67	3.02	0.07	1.63
2.52	0.90	14.44	7.06	101.94	3.03	0.07	1.57
2.54	0.86	13.88	7.21	100.03	3.04	0.07	1.51
2.56	0.82	13.16	7.47	98.33	3.06	0.07	1.42
2.58	0.78	12.43	7.69	95.61	3.08	0.06	1.34
2.60	0.73	11.59	7.98	92.58	3.10	0.06	1.24
2.62	0.69	10.97	8.20	89.99	3.12	0.06	1.17
2.64	0.66	10.44	8.44	88.12	3.14	0.06	1.11
2.66	0.64	10.12	8.57	86.75	3.15	0.06	1.07
2.68	0.63	9.90	8.56	84.80	3.15	0.06	1.05
2.70	0.62	9.68	8.49	82.20	3.14	0.06	1.02
2.72	0.60	9.34	8.51	79.47	3.15	0.06	0.98
2.74	0.57	8.84	8.68	76.75	3.16	0.06	0.92
2.76	0.55	8.44	8.80	74.31	3.17	0.06	0.88
2.78	0.55	8.44	8.50	71.72	3.14	0.06	0.88
2.80	0.57	8.86	7.78	68.97	3.09	0.06	0.92
2.82	0.60	9.35	7.19	67.20	3.04	0.06	0.97
2.84	0.62	9.68	6.90	66.76	3.01	0.06	1.00
2.86	0.62	9.70	6.98	67.69	3.02	0.06	1.00
2.88	0.60	9.38	7.28	68.26	3.05	0.06	0.96

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
2.90	0.60	9.33	7.38	68.87	3.06	0.06	0.95
2.92	0.59	9.17	7.57	69.44	3.07	0.06	0.93
2.94	0.59	9.16	7.68	70.37	3.08	0.06	0.93
2.96	0.55	8.52	8.29	70.62	3.13	0.06	0.86
2.98	0.52	7.95	8.75	69.50	3.16	0.06	0.80
3.00	0.50	7.58	8.89	67.39	3.17	0.06	0.76
3.02	0.51	7.78	8.29	64.45	3.13	0.06	0.78
3.04	0.55	8.41	7.35	61.82	3.05	0.06	0.84
3.06	0.59	9.13	6.50	59.34	2.98	0.06	0.91
3.08	0.62	9.57	6.12	58.54	2.94	0.06	0.95
3.10	0.61	9.46	6.35	60.04	2.96	0.06	0.94
3.12	0.58	8.88	7.19	63.79	3.04	0.06	0.88
3.14	0.54	8.25	8.15	67.23	3.12	0.06	0.81
3.16	0.51	7.72	9.03	69.66	3.18	0.06	0.76
3.18	0.49	7.38	9.59	70.85	3.22	0.06	0.72
3.21	0.49	7.29	9.90	72.22	3.25	0.06	0.71
3.22	0.50	7.48	9.76	73.03	3.24	0.06	0.73
3.24	0.53	8.03	9.03	72.53	3.18	0.06	0.78
3.26	0.57	8.72	7.98	69.62	3.10	0.06	0.84
3.28	0.60	9.21	7.18	66.17	3.04	0.06	0.89
3.30	0.60	9.23	6.95	64.17	3.02	0.06	0.89
3.32	0.58	8.86	7.22	64.02	3.04	0.06	0.85
3.34	0.56	8.50	7.68	65.26	3.08	0.06	0.81
3.36	0.56	8.57	7.77	66.64	3.09	0.06	0.82
3.38	0.60	9.11	7.42	67.54	3.06	0.06	0.87
3.40	0.63	9.62	7.04	67.70	3.03	0.06	0.91
3.42	0.63	9.70	7.03	68.12	3.02	0.06	0.92
3.44	0.60	9.20	7.50	68.95	3.07	0.06	0.87
3.46	0.57	8.58	8.07	69.19	3.11	0.06	0.81
3.48	0.55	8.32	8.25	68.61	3.13	0.06	0.78
3.50	0.59	8.92	7.63	68.03	3.08	0.06	0.83
3.52	0.66	10.12	6.62	66.95	2.99	0.06	0.94
3.54	0.74	11.52	5.73	65.98	2.90	0.07	1.07
3.56	0.79	12.32	5.31	65.36	2.86	0.07	1.14
3.58	0.78	12.21	5.45	66.56	2.87	0.07	1.13
3.60	0.75	11.71	5.79	67.76	2.91	0.07	1.08
3.63	0.72	11.19	6.23	69.70	2.95	0.06	1.03
3.64	0.71	10.97	6.62	72.62	2.99	0.06	1.01
3.66	0.69	10.60	7.22	76.52	3.04	0.06	0.97
3.68	0.66	10.07	7.95	80.07	3.10	0.06	0.92
3.70	0.62	9.49	8.56	81.22	3.15	0.06	0.86
3.72	0.60	9.06	8.87	80.34	3.17	0.06	0.82
3.74	0.58	8.70	9.01	78.41	3.18	0.06	0.79
3.76	0.56	8.36	9.06	75.76	3.19	0.06	0.75
3.78	0.53	7.93	9.21	72.98	3.20	0.06	0.71
3.80	0.51	7.53	9.29	69.95	3.20	0.06	0.68
3.82	0.50	7.33	9.19	67.32	3.20	0.06	0.65
3.84	0.51	7.50	8.67	65.06	3.16	0.06	0.67

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
3.86	0.55	8.17	7.66	62.56	3.08	0.06	0.73
3.88	0.63	9.53	6.34	60.39	2.96	0.06	0.85
3.90	0.68	10.37	5.84	60.55	2.91	0.07	0.92
3.92	0.69	10.53	5.82	61.25	2.91	0.06	0.93
3.94	0.65	9.92	6.43	63.79	2.97	0.06	0.87
3.96	0.62	9.45	6.98	65.92	3.02	0.06	0.83
3.98	0.61	9.24	7.40	68.33	3.06	0.06	0.81
4.00	0.61	9.19	7.63	70.12	3.08	0.06	0.80
4.03	0.62	9.36	7.57	70.90	3.07	0.06	0.81
4.04	0.65	9.79	7.24	70.89	3.04	0.06	0.85
4.06	0.69	10.57	6.57	69.46	2.98	0.06	0.92
4.08	0.75	11.60	5.82	67.47	2.91	0.07	1.00
4.10	0.82	12.71	5.18	65.80	2.84	0.07	1.09
4.12	0.87	13.65	4.80	65.51	2.80	0.07	1.17
4.14	0.91	14.31	4.59	65.74	2.78	0.07	1.23
4.16	0.93	14.60	4.65	67.85	2.78	0.07	1.25
4.18	0.93	14.51	4.93	71.52	2.82	0.07	1.24
4.20	0.92	14.39	5.30	76.33	2.86	0.07	1.22
4.22	0.91	14.29	5.69	81.28	2.90	0.07	1.21
4.24	0.92	14.32	5.99	85.73	2.93	0.07	1.21
4.26	0.93	14.60	6.21	90.66	2.95	0.07	1.23
4.28	0.96	15.14	6.25	94.54	2.95	0.07	1.27
4.30	1.00	15.67	6.17	96.62	2.95	0.07	1.31
4.32	1.01	15.87	6.10	96.79	2.94	0.07	1.33
4.34	1.00	15.79	6.13	96.71	2.94	0.07	1.31
4.36	1.00	15.66	6.18	96.80	2.95	0.07	1.30
4.38	1.00	15.65	6.19	96.89	2.95	0.07	1.30
4.40	1.00	15.71	6.17	96.90	2.95	0.07	1.30
4.42	1.00	15.65	6.23	97.45	2.95	0.07	1.29
4.44	0.99	15.46	6.35	98.25	2.96	0.07	1.27
4.46	0.97	15.24	6.50	99.15	2.98	0.07	1.25
4.48	0.97	15.17	6.60	100.10	2.99	0.07	1.24
4.50	0.96	15.06	6.74	101.51	3.00	0.07	1.22
4.52	0.96	14.93	6.94	103.70	3.02	0.07	1.21
4.54	0.94	14.66	7.21	105.66	3.04	0.06	1.19
4.56	0.92	14.36	7.47	107.34	3.06	0.06	1.16
4.58	0.91	14.09	7.65	107.75	3.08	0.06	1.13
4.60	0.89	13.85	7.75	107.30	3.09	0.06	1.11
4.62	0.88	13.60	7.82	106.39	3.09	0.06	1.09
4.64	0.86	13.17	8.01	105.50	3.11	0.06	1.05
4.66	0.82	12.64	8.31	105.01	3.13	0.06	1.00
4.68	0.79	12.05	8.68	104.56	3.16	0.06	0.95
4.70	0.76	11.59	8.98	104.10	3.18	0.06	0.92
4.72	0.74	11.22	9.25	103.72	3.20	0.06	0.88
4.74	0.73	11.02	9.32	102.66	3.20	0.06	0.87
4.76	0.73	11.00	9.15	100.57	3.19	0.06	0.86
4.78	0.74	11.17	8.73	97.52	3.16	0.06	0.87
4.80	0.75	11.37	8.27	94.02	3.13	0.06	0.89

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
4.82	0.76	11.57	7.81	90.29	3.09	0.06	0.90
4.84	0.77	11.63	7.47	86.88	3.06	0.06	0.90
4.86	0.77	11.65	7.23	84.23	3.04	0.06	0.90
4.88	0.80	12.22	6.68	81.65	2.99	0.06	0.94
4.90	0.86	13.19	6.01	79.31	2.93	0.07	1.01
4.92	0.94	14.58	5.27	76.85	2.86	0.07	1.12
4.94	1.01	15.73	4.86	76.37	2.81	0.07	1.20
4.96	1.08	16.86	4.58	77.20	2.78	0.07	1.29
4.98	1.13	17.73	4.46	79.16	2.76	0.08	1.35
5.00	1.16	18.18	4.47	81.33	2.76	0.08	1.38
5.02	1.15	18.02	4.68	84.35	2.79	0.08	1.37
5.04	1.13	17.68	4.91	86.88	2.82	0.07	1.34
5.06	1.09	16.98	5.40	91.62	2.87	0.07	1.28
5.08	1.08	16.91	5.59	94.55	2.89	0.07	1.27
5.11	1.11	17.28	5.53	95.52	2.88	0.07	1.29
5.12	1.16	18.26	5.04	92.09	2.83	0.07	1.37
5.14	1.21	18.97	4.67	88.69	2.79	0.08	1.41
5.16	1.22	19.27	4.54	87.46	2.77	0.08	1.43
5.18	1.23	19.46	4.53	88.07	2.77	0.08	1.44
5.20	1.30	20.32	4.28	86.99	2.74	0.08	1.52
5.22	1.39	21.61	3.95	85.39	2.69	0.08	1.63
5.24	1.44	22.26	3.82	85.15	2.68	0.08	1.68
5.26	1.38	21.41	4.13	88.50	2.72	0.08	1.60
5.28	1.24	19.39	4.81	93.18	2.80	0.08	1.43
5.30	1.13	17.59	5.40	95.02	2.87	0.07	1.28
5.32	1.11	17.26	5.45	93.99	2.87	0.07	1.26
5.34	1.25	19.38	4.69	90.83	2.79	0.08	1.43
5.36	1.60	24.35	3.51	85.58	2.63	0.08	1.86
5.38	2.03	30.33	2.68	81.34	2.48	0.09	0.67
5.40	2.46	36.04	2.17	78.26	2.36	0.09	0.69
5.42	2.79	40.41	1.95	78.71	2.30	0.09	0.71
5.44	3.09	44.39	1.80	79.83	2.25	0.09	0.72
5.46	3.41	48.66	1.69	82.16	2.21	0.09	0.73
5.48	3.83	54.06	1.57	84.69	2.16	0.09	0.74
5.50	4.41	61.38	1.42	87.01	2.08	0.10	0.76
5.52	5.08	69.61	1.28	89.43	1.99	0.10	0.78
5.54	6.04	80.78	1.15	93.24	1.86	0.10	0.80
5.56	7.02	91.88	1.00	91.88	1.75	0.11	0.82
5.58	7.85	101.07	1.00	101.07	1.67	0.12	0.83
5.60	8.10	103.73	1.00	103.73	1.64	0.13	0.83
5.62	7.70	98.81	1.00	98.81	1.67	0.12	0.83
5.64	6.82	88.05	1.00	88.05	1.71	0.10	0.81
5.66	5.50	72.14	1.00	72.14	1.81	0.09	0.78
5.68	4.15	55.96	1.30	72.58	2.00	0.08	0.75
5.70	3.09	43.16	1.77	76.22	2.24	0.08	0.72
5.72	2.43	35.15	2.62	92.11	2.47	0.09	0.69
5.74	2.02	29.88	3.75	112.06	2.67	0.09	2.25
5.76	1.61	24.40	5.34	130.17	2.86	0.08	1.77

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
5.78	1.31	19.74	7.06	139.44	3.03	0.07	1.41
5.80	1.21	18.11	7.69	139.32	3.08	0.07	1.29
5.82	1.59	23.97	5.52	132.35	2.88	0.07	1.73
5.84	2.58	37.42	3.08	115.28	2.56	0.09	0.70
5.86	3.76	52.53	1.93	101.14	2.29	0.11	0.74
5.88	4.37	59.70	1.57	93.68	2.16	0.11	0.76
5.90	4.24	57.41	1.50	86.16	2.12	0.10	0.75
5.92	3.77	51.17	1.58	80.85	2.16	0.09	0.74
5.94	3.19	43.91	1.91	84.02	2.29	0.10	0.72
5.96	2.65	37.21	2.53	94.19	2.45	0.09	0.70
5.98	2.03	29.15	3.65	106.43	2.65	0.09	2.19
6.00	1.60	23.21	5.06	117.53	2.83	0.08	1.69
6.02	1.23	17.76	7.00	124.39	3.02	0.07	1.27
6.05	1.11	15.90	8.08	128.36	3.11	0.06	1.14
6.06	1.24	17.87	7.19	128.51	3.04	0.07	1.28
6.08	1.38	19.95	6.15	122.64	2.94	0.07	1.43
6.10	1.41	20.17	5.61	113.07	2.89	0.07	1.45
6.12	1.29	18.33	5.68	104.19	2.90	0.07	1.32
6.14	1.20	17.01	5.75	97.81	2.91	0.07	1.22
6.16	1.18	16.61	5.69	94.55	2.90	0.07	1.19
6.18	1.20	16.78	5.59	93.74	2.89	0.07	1.21
6.20	1.24	17.39	5.59	97.26	2.89	0.07	1.25
6.22	1.27	17.84	5.78	103.10	2.91	0.07	1.28
6.24	1.29	18.14	5.93	107.56	2.92	0.07	1.30
6.26	1.29	18.05	6.15	111.03	2.94	0.07	1.29
6.28	1.27	17.73	6.44	114.13	2.97	0.07	1.27
6.30	1.25	17.43	6.77	118.04	3.00	0.07	1.24
6.32	1.23	17.00	7.21	122.56	3.04	0.07	1.21
6.34	1.21	16.70	7.60	126.92	3.07	0.07	1.19
6.36	1.20	16.56	7.89	130.69	3.10	0.07	1.18
6.38	1.20	16.44	8.08	132.88	3.11	0.07	1.17
6.40	1.19	16.24	8.23	133.69	3.12	0.07	1.16
6.42	1.18	16.07	8.32	133.73	3.13	0.07	1.15
6.44	1.18	16.08	8.28	133.18	3.13	0.07	1.15
6.46	1.20	16.29	8.09	131.71	3.11	0.07	1.16
6.48	1.21	16.41	7.92	129.90	3.10	0.07	1.17
6.50	1.22	16.46	7.75	127.58	3.09	0.07	1.18
6.52	1.22	16.35	7.67	125.51	3.08	0.07	1.17
6.54	1.21	16.30	7.58	123.58	3.07	0.07	1.16
6.56	1.23	16.48	7.43	122.43	3.06	0.07	1.18
6.58	1.26	16.84	7.22	121.63	3.04	0.07	1.20
6.60	1.29	17.24	7.03	121.21	3.03	0.07	1.23
6.62	1.31	17.46	6.96	121.48	3.02	0.07	1.25
6.64	1.31	17.54	6.97	122.21	3.02	0.07	1.25
6.66	1.32	17.52	7.07	123.85	3.03	0.07	1.25
6.68	1.31	17.38	7.24	125.89	3.04	0.07	1.24
6.70	1.30	17.24	7.43	128.15	3.06	0.07	1.23
6.72	1.30	17.06	7.61	129.84	3.07	0.07	1.22

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
6.74	1.28	16.85	7.75	130.57	3.09	0.07	1.20
6.76	1.25	16.27	8.06	131.14	3.11	0.07	1.16
6.78	1.21	15.68	8.31	130.24	3.13	0.07	1.12
6.80	1.17	15.09	8.51	128.34	3.15	0.07	1.08
6.82	1.13	14.47	8.67	125.39	3.16	0.07	1.03
6.84	0.94	11.72	9.70	113.69	3.23	0.06	0.84
6.86	0.89	10.99	10.13	111.38	3.26	0.06	0.79
6.88	0.85	10.36	10.54	109.25	3.29	0.06	0.74
6.90	0.96	11.86	9.85	116.78	3.24	0.06	0.85
6.92	0.92	11.36	10.08	114.55	3.26	0.06	0.81
6.94	0.90	10.98	10.27	112.76	3.27	0.06	0.78
6.96	0.87	10.61	10.47	111.08	3.28	0.06	0.76
6.98	0.86	10.31	10.57	108.95	3.29	0.06	0.74
7.00	0.84	10.08	10.56	106.44	3.29	0.06	0.72
7.02	0.83	9.86	10.57	104.20	3.29	0.06	0.70
7.04	0.83	9.81	10.48	102.83	3.28	0.06	0.70
7.06	0.83	9.89	10.27	101.62	3.27	0.06	0.71
7.08	0.85	10.12	9.93	100.47	3.25	0.06	0.72
7.10	0.86	10.25	9.69	99.31	3.23	0.06	0.73
7.12	0.87	10.26	9.64	98.90	3.23	0.06	0.73
7.14	0.87	10.27	9.68	99.34	3.23	0.06	0.73
7.16	0.88	10.42	9.64	100.47	3.23	0.06	0.74
7.19	0.90	10.57	9.60	101.54	3.22	0.06	0.76
7.20	0.91	10.76	9.54	102.71	3.22	0.06	0.77
7.22	0.92	10.86	9.56	103.72	3.22	0.06	0.78
7.24	0.93	11.00	9.53	104.77	3.22	0.06	0.79
7.26	0.95	11.25	9.38	105.44	3.21	0.06	0.80
7.28	0.97	11.45	9.23	105.73	3.20	0.06	0.82
7.31	1.00	11.81	8.95	105.68	3.18	0.06	0.84
7.32	1.02	12.13	8.69	105.46	3.16	0.06	0.87
7.34	1.06	12.54	8.40	105.35	3.14	0.06	0.90
7.36	1.09	13.00	8.14	105.84	3.12	0.06	0.93
7.38	1.15	13.81	7.72	106.56	3.08	0.07	0.99
7.41	1.23	14.81	7.23	107.03	3.04	0.07	1.06
7.42	1.30	15.65	6.86	107.32	3.01	0.07	1.12
7.44	1.33	16.06	6.72	107.96	3.00	0.07	1.15
7.46	1.34	16.17	6.74	108.90	3.00	0.07	1.15
7.48	1.33	15.93	6.92	110.25	3.02	0.07	1.14
7.50	1.29	15.41	7.25	111.66	3.04	0.07	1.10
7.52	1.23	14.58	7.74	112.91	3.09	0.07	1.04
7.54	1.17	13.79	8.22	113.31	3.12	0.07	0.98
7.56	1.13	13.11	8.63	113.10	3.15	0.06	0.94
7.58	1.09	12.57	8.96	112.66	3.18	0.06	0.90
7.60	1.06	12.13	9.25	112.23	3.20	0.06	0.87
7.62	1.02	11.69	9.55	111.58	3.22	0.06	0.83
7.64	1.00	11.29	9.80	110.64	3.24	0.06	0.81
7.66	0.99	11.24	9.75	109.64	3.24	0.06	0.80
7.68	1.01	11.37	9.58	108.98	3.22	0.06	0.81

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
7.70	1.03	11.66	9.32	108.65	3.21	0.06	0.83
7.72	1.03	11.65	9.34	108.80	3.21	0.06	0.83
7.74	1.03	11.64	9.38	109.24	3.21	0.06	0.83
7.76	1.03	11.59	9.46	109.65	3.21	0.06	0.83
7.78	1.06	11.88	9.25	109.82	3.20	0.06	0.85
7.80	1.12	12.62	8.69	109.67	3.16	0.06	0.90
7.82	1.18	13.36	8.20	109.60	3.12	0.07	0.95
7.84	1.22	13.85	7.93	109.82	3.10	0.07	0.99
7.86	1.22	13.82	8.01	110.70	3.11	0.07	0.99
7.88	1.22	13.76	8.14	111.96	3.12	0.07	0.98
7.90	1.24	13.97	8.12	113.50	3.12	0.07	1.00
7.92	1.28	14.44	7.99	115.31	3.10	0.07	1.03
7.94	1.32	14.92	7.90	117.87	3.10	0.07	1.07
7.96	1.34	15.19	7.92	120.33	3.10	0.07	1.08
7.98	1.35	15.27	7.98	121.94	3.10	0.07	1.09
8.01	1.35	15.20	8.01	121.76	3.11	0.07	1.09
8.02	1.32	14.83	8.19	121.50	3.12	0.07	1.06
8.04	1.31	14.61	8.28	120.96	3.13	0.07	1.04
8.06	1.30	14.45	8.31	120.02	3.13	0.07	1.03
8.08	1.30	14.49	8.19	118.64	3.12	0.07	1.04
8.10	1.28	14.16	8.30	117.45	3.13	0.07	1.01
8.12	1.24	13.71	8.53	116.95	3.15	0.07	0.98
8.15	1.21	13.28	8.76	116.32	3.16	0.07	0.95
8.17	1.21	13.25	8.73	115.70	3.16	0.07	0.95
8.18	1.24	13.56	8.49	115.18	3.14	0.07	0.97
8.20	1.28	14.07	8.16	114.70	3.12	0.07	1.00
8.22	1.31	14.40	7.94	114.33	3.10	0.07	1.03
8.24	1.33	14.60	7.81	113.94	3.09	0.07	1.04
8.26	1.33	14.56	7.84	114.18	3.09	0.07	1.04
8.28	1.32	14.35	8.01	114.93	3.11	0.07	1.03
8.30	1.32	14.32	8.10	115.94	3.11	0.07	1.02
8.32	1.33	14.40	8.12	116.89	3.12	0.07	1.03
8.34	1.34	14.46	8.13	117.48	3.12	0.07	1.03
8.36	1.32	14.28	8.26	117.91	3.13	0.07	1.02
8.38	1.31	14.10	8.34	117.51	3.13	0.07	1.01
8.40	1.31	14.02	8.32	116.73	3.13	0.07	1.00
8.42	1.31	14.04	8.22	115.42	3.12	0.07	1.00
8.44	1.32	14.06	8.16	114.69	3.12	0.07	1.00
8.46	1.31	13.95	8.20	114.35	3.12	0.07	1.00
8.48	1.29	13.66	8.38	114.46	3.14	0.07	0.98
8.50	1.26	13.31	8.58	114.23	3.15	0.07	0.95
8.52	1.24	12.98	8.76	113.72	3.16	0.07	0.93
8.54	1.22	12.77	8.86	113.14	3.17	0.07	0.91
8.56	1.21	12.62	8.90	112.38	3.17	0.06	0.90
8.58	1.20	12.43	8.97	111.48	3.18	0.07	0.89
8.60	1.18	12.24	9.01	110.34	3.18	0.06	0.87
8.62	1.16	11.92	9.19	109.53	3.20	0.06	0.85
8.64	1.14	11.63	9.37	108.98	3.21	0.06	0.83

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
8.66	1.11	11.24	9.63	108.28	3.23	0.06	0.80
8.68	1.09	11.01	9.78	107.73	3.24	0.06	0.79
8.70	1.07	10.80	9.96	107.62	3.25	0.06	0.77
8.72	1.08	10.85	9.97	108.14	3.25	0.06	0.78
8.74	1.10	11.04	9.83	108.56	3.24	0.06	0.79
8.76	1.15	11.58	9.39	108.69	3.21	0.06	0.83
8.78	1.19	12.09	8.97	108.44	3.18	0.06	0.86
8.80	1.23	12.51	8.65	108.28	3.16	0.07	0.89
8.82	1.27	12.92	8.38	108.25	3.14	0.07	0.92
8.84	1.30	13.21	8.25	108.97	3.13	0.07	0.94
8.86	1.33	13.51	8.16	110.24	3.12	0.07	0.96
8.88	1.34	13.60	8.20	111.58	3.12	0.07	0.97
8.90	1.36	13.83	8.17	113.03	3.12	0.07	0.99
8.92	1.38	14.01	8.15	114.22	3.12	0.07	1.00
8.94	1.40	14.22	8.11	115.32	3.11	0.07	1.02
8.96	1.40	14.23	8.12	115.48	3.11	0.07	1.02
8.98	1.39	14.04	8.18	114.91	3.12	0.07	1.00
9.00	1.36	13.68	8.30	113.56	3.13	0.07	0.98
9.02	1.32	13.25	8.44	111.88	3.14	0.07	0.95
9.04	1.27	12.60	8.68	109.41	3.16	0.07	0.90
9.06	1.21	11.89	8.95	106.50	3.18	0.06	0.85
9.08	1.16	11.27	9.16	103.18	3.19	0.06	0.80
9.10	1.12	10.88	9.21	100.18	3.20	0.06	0.78
9.12	1.11	10.67	9.13	97.42	3.19	0.06	0.76
9.14	1.09	10.49	9.09	95.36	3.19	0.06	0.75
9.16	1.09	10.42	9.02	93.97	3.18	0.06	0.74
9.18	1.10	10.48	8.92	93.56	3.18	0.06	0.75
9.20	1.13	10.80	8.69	93.86	3.16	0.06	0.77
9.22	1.19	11.50	8.25	94.89	3.13	0.06	0.82
9.24	1.27	12.30	7.82	96.09	3.09	0.07	0.88
9.26	1.32	12.86	7.54	96.95	3.07	0.07	0.92
9.29	1.34	13.04	7.43	96.91	3.06	0.07	0.93
9.30	1.35	13.17	7.35	96.76	3.05	0.07	0.94
9.32	1.39	13.61	7.09	96.56	3.03	0.07	0.97
9.34	1.47	14.39	6.76	97.28	3.00	0.07	1.03
9.36	1.55	15.31	6.45	98.82	2.97	0.07	1.09
9.38	1.61	15.90	6.45	102.57	2.97	0.07	1.14
9.40	1.65	16.33	6.60	107.79	2.99	0.07	1.17
9.42	1.68	16.59	6.86	113.86	3.01	0.07	1.18
9.44	1.70	16.77	7.14	119.72	3.03	0.07	1.20
9.46	1.70	16.79	7.46	125.20	3.06	0.07	1.20
9.48	1.68	16.49	7.90	130.30	3.10	0.07	1.18
9.50	1.63	15.91	8.46	134.59	3.14	0.07	1.14
9.52	1.57	15.20	9.05	137.47	3.19	0.07	1.09
9.54	1.54	14.91	9.33	139.11	3.21	0.07	1.07
9.56	1.55	14.98	9.34	139.88	3.21	0.07	1.07
9.58	1.55	14.96	9.38	140.25	3.21	0.07	1.07
9.60	1.54	14.83	9.43	139.78	3.21	0.07	1.06

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.62	1.54	14.73	9.38	138.19	3.21	0.07	1.05
9.64	1.56	14.91	9.08	135.37	3.19	0.07	1.07
9.66	1.57	15.05	8.79	132.19	3.17	0.07	1.07
9.68	1.62	15.45	8.36	129.20	3.13	0.07	1.10
9.70	1.66	15.93	7.97	127.04	3.10	0.07	1.14
9.72	1.71	16.42	7.64	125.56	3.08	0.07	1.17
9.74	1.75	16.77	7.44	124.70	3.06	0.07	1.20
9.76	1.78	17.07	7.25	123.80	3.04	0.07	1.22
9.78	1.81	17.36	7.12	123.71	3.03	0.07	1.24
9.80	1.84	17.64	7.02	123.91	3.02	0.07	1.26
9.82	1.88	17.98	6.87	123.42	3.01	0.07	1.28
9.84	1.92	18.35	6.68	122.56	2.99	0.07	1.31
9.86	1.93	18.51	6.61	122.33	2.99	0.07	1.32
9.88	1.93	18.43	6.73	124.03	3.00	0.07	1.32
9.90	1.89	18.01	7.02	126.35	3.02	0.07	1.29
9.92	1.86	17.57	7.30	128.20	3.05	0.07	1.26
9.94	1.79	16.87	7.67	129.45	3.08	0.07	1.20
9.96	1.71	16.02	8.07	129.31	3.11	0.07	1.14
9.98	1.62	15.02	8.53	128.16	3.15	0.07	1.07
10.00	1.48	13.51	9.27	125.22	3.20	0.07	0.97
10.03	1.34	12.03	10.06	121.10	3.26	0.06	0.86
10.04	1.19	10.46	11.10	116.10	3.32	0.06	0.75
10.06	1.10	9.51	11.74	111.60	3.36	0.06	0.68
10.08	1.02	8.71	12.30	107.10	3.40	0.06	0.62
10.10	0.98	8.24	12.49	102.83	3.41	0.06	0.59
10.12	0.94	7.82	12.53	98.01	3.41	0.06	0.56
10.14	0.91	7.48	12.49	93.41	3.41	0.06	0.53
10.16	0.88	7.17	12.38	88.73	3.40	0.06	0.51
10.18	0.87	7.01	12.07	84.55	3.38	0.06	0.50
10.20	0.85	6.84	11.65	79.65	3.36	0.06	0.49
10.22	0.83	6.59	11.31	74.52	3.34	0.06	0.47
10.24	0.80	6.35	11.04	70.06	3.32	0.06	0.45
10.26	0.81	6.34	10.53	66.72	3.29	0.06	0.45
10.28	0.83	6.61	9.69	64.10	3.23	0.06	0.47
10.30	0.88	7.04	8.71	61.30	3.16	0.06	0.50
10.32	0.91	7.39	8.01	59.16	3.11	0.06	0.53
10.34	0.92	7.45	7.86	58.56	3.09	0.06	0.53
10.36	0.92	7.45	7.98	59.47	3.10	0.06	0.53
10.38	0.97	7.90	7.65	60.45	3.08	0.06	0.56
10.40	1.05	8.68	6.96	60.39	3.02	0.06	0.62
10.42	1.09	9.09	6.77	61.56	3.00	0.06	0.65
10.44	1.10	9.15	6.85	62.70	3.01	0.06	0.65
10.46	1.17	9.91	6.43	63.74	2.97	0.06	0.71
10.48	1.36	11.78	5.24	61.71	2.85	0.07	0.84
10.50	1.58	13.96	4.32	60.29	2.74	0.08	1.00
10.52	1.71	15.19	4.21	64.00	2.73	0.08	1.09
10.54	1.79	16.00	4.15	66.44	2.72	0.08	1.14
10.56	1.84	16.46	4.24	69.80	2.73	0.08	1.18

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
10.58	1.90	17.03	4.29	73.04	2.74	0.08	1.22
10.60	1.92	17.17	4.80	82.35	2.80	0.08	1.23
10.62	1.93	17.22	5.36	92.27	2.86	0.08	1.23
10.64	1.91	17.00	5.98	101.68	2.93	0.07	1.21
10.66	1.89	16.75	6.47	108.37	2.97	0.07	1.20
10.68	1.84	16.31	7.04	114.76	3.03	0.07	1.17
10.70	1.80	15.83	7.48	118.43	3.06	0.07	1.13
10.72	1.72	15.01	8.07	121.22	3.11	0.07	1.07
10.74	1.62	13.99	8.72	121.93	3.16	0.07	1.00
10.76	1.48	12.60	9.68	122.02	3.23	0.07	0.90
10.78	1.34	11.20	10.79	120.86	3.30	0.06	0.80
10.80	1.20	9.82	12.03	118.08	3.38	0.06	0.70
10.82	1.16	9.39	12.10	113.59	3.39	0.06	0.67
10.84	1.13	9.14	11.82	108.02	3.37	0.06	0.65
10.86	1.12	9.05	11.20	101.34	3.33	0.06	0.65
10.88	1.06	8.39	11.30	94.79	3.34	0.06	0.60
10.90	0.98	7.65	11.56	88.40	3.35	0.06	0.55
10.92	0.93	7.11	11.67	82.89	3.36	0.06	0.51
10.94	0.94	7.18	11.02	79.10	3.32	0.06	0.51
10.96	0.98	7.54	10.02	75.48	3.25	0.06	0.54
10.98	1.00	7.78	9.28	72.16	3.20	0.06	0.56
11.00	0.99	7.63	9.15	69.81	3.19	0.06	0.54
11.03	0.99	7.65	8.85	67.66	3.17	0.06	0.55
11.04	1.03	8.00	8.11	64.84	3.11	0.06	0.57
11.06	1.07	8.35	7.42	61.97	3.06	0.06	0.60
11.08	1.10	8.61	7.04	60.57	3.03	0.06	0.61
11.10	1.10	8.67	7.02	60.81	3.02	0.06	0.62
11.12	1.11	8.70	7.09	61.68	3.03	0.06	0.62
11.14	1.10	8.61	7.22	62.17	3.04	0.06	0.62
11.16	1.10	8.56	7.39	63.27	3.06	0.06	0.61
11.18	1.10	8.58	7.56	64.84	3.07	0.06	0.61
11.20	1.13	8.80	7.64	67.17	3.08	0.06	0.63
11.22	1.16	9.06	7.62	69.03	3.08	0.06	0.65
11.24	1.21	9.52	7.31	69.62	3.05	0.06	0.68
11.26	1.29	10.27	6.74	69.21	3.00	0.06	0.73
11.28	1.40	11.30	6.07	68.55	2.94	0.07	0.81
11.30	1.53	12.53	5.37	67.28	2.87	0.07	0.89
11.32	1.63	13.42	4.99	66.98	2.82	0.07	0.96
11.34	1.69	14.01	4.87	68.20	2.81	0.08	1.00
11.36	1.70	14.07	5.12	72.10	2.84	0.07	1.00
11.38	1.69	13.89	5.59	77.67	2.89	0.07	0.99
11.40	1.66	13.59	6.12	83.18	2.94	0.07	0.97
11.42	1.65	13.47	6.50	87.60	2.98	0.07	0.96
11.44	1.64	13.36	6.89	92.12	3.01	0.07	0.95
11.46	1.62	13.21	7.25	95.86	3.04	0.07	0.94
11.48	1.59	12.90	7.70	99.31	3.08	0.07	0.92
11.50	1.57	12.64	7.98	100.91	3.10	0.07	0.90
11.52	1.54	12.33	8.28	102.12	3.13	0.07	0.88

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
11.54	1.49	11.92	8.65	103.07	3.16	0.07	0.85
11.56	1.46	11.55	8.97	103.56	3.18	0.07	0.83
11.58	1.44	11.34	9.10	103.25	3.19	0.07	0.81
11.60	1.42	11.14	9.19	102.37	3.20	0.07	0.80
11.62	1.39	10.84	9.37	101.57	3.21	0.06	0.77
11.64	1.35	10.46	9.62	100.63	3.23	0.06	0.75
11.66	1.30	10.06	9.88	99.43	3.24	0.06	0.72
11.68	1.29	9.86	9.93	97.98	3.25	0.06	0.70
11.70	1.28	9.79	9.92	97.15	3.25	0.06	0.70
11.72	1.28	9.82	9.82	96.40	3.24	0.06	0.70
11.74	1.28	9.77	9.77	95.44	3.24	0.06	0.70
11.76	1.27	9.61	9.72	93.42	3.23	0.06	0.69
11.78	1.23	9.24	9.88	91.24	3.24	0.06	0.66
11.80	1.15	8.55	10.34	88.45	3.28	0.06	0.61
11.82	1.10	8.04	10.83	87.09	3.31	0.06	0.57
11.84	1.04	7.47	11.49	85.85	3.35	0.06	0.53
11.86	1.01	7.19	11.86	85.30	3.37	0.06	0.51
11.88	0.96	6.76	12.36	83.55	3.40	0.06	0.48
11.90	0.94	6.54	12.41	81.08	3.40	0.06	0.47
11.92	0.92	6.35	12.26	77.86	3.40	0.06	0.45
11.94	0.92	6.32	11.76	74.31	3.37	0.06	0.45
11.96	0.95	6.60	10.78	71.10	3.30	0.06	0.47
11.99	1.02	7.26	9.35	67.90	3.21	0.06	0.52
12.00	1.13	8.17	7.97	65.12	3.10	0.06	0.58
12.02	1.26	9.38	6.79	63.70	3.00	0.06	0.67
12.04	1.43	10.85	5.88	63.76	2.92	0.07	0.78
12.06	1.59	12.23	5.32	65.03	2.86	0.07	0.87
12.08	1.66	12.89	5.27	68.01	2.86	0.07	0.92
12.10	1.66	12.83	5.63	72.28	2.89	0.07	0.92
12.12	1.62	12.50	6.19	77.42	2.95	0.07	0.89
12.14	1.60	12.28	6.72	82.46	3.00	0.07	0.88
12.16	1.58	12.06	7.35	88.65	3.05	0.07	0.86
12.18	1.55	11.77	8.09	95.19	3.11	0.07	0.84
12.20	1.53	11.55	8.71	100.62	3.16	0.07	0.82
12.22	1.51	11.41	9.10	103.87	3.19	0.07	0.82
12.24	1.51	11.40	9.28	105.87	3.20	0.07	0.81
12.26	1.51	11.38	9.40	107.01	3.21	0.07	0.81
12.28	1.51	11.36	9.47	107.54	3.22	0.07	0.81
12.30	1.52	11.41	9.36	106.81	3.21	0.07	0.81
12.32	1.53	11.49	9.19	105.54	3.20	0.07	0.82
12.34	1.57	11.77	8.87	104.42	3.17	0.07	0.84
12.36	1.64	12.40	8.40	104.12	3.14	0.07	0.89
12.38	1.74	13.21	7.92	104.66	3.10	0.07	0.94
12.40	1.84	14.09	7.52	105.93	3.07	0.07	1.01
12.42	1.91	14.69	7.31	107.33	3.05	0.07	1.05
12.44	1.96	15.09	7.23	109.07	3.04	0.07	1.08
12.46	1.96	15.03	7.39	111.13	3.06	0.07	1.07
12.48	1.93	14.79	7.66	113.29	3.08	0.07	1.06

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
12.50	1.91	14.54	7.96	115.67	3.10	0.07	1.04
12.52	1.89	14.39	8.20	118.05	3.12	0.07	1.03
12.54	1.88	14.23	8.48	120.76	3.14	0.07	1.02
12.56	1.86	14.00	8.77	122.82	3.17	0.07	1.00
12.58	1.83	13.78	9.02	124.26	3.18	0.07	0.98
12.61	1.81	13.57	9.17	124.35	3.19	0.07	0.97
12.62	1.81	13.56	9.12	123.62	3.19	0.07	0.97
12.64	1.83	13.73	8.90	122.15	3.17	0.07	0.98
12.66	1.86	13.92	8.67	120.74	3.16	0.07	0.99
12.68	1.87	13.97	8.56	119.62	3.15	0.07	1.00
12.70	1.87	13.96	8.50	118.66	3.14	0.07	1.00
12.72	1.89	14.13	8.35	117.91	3.13	0.07	1.01
12.74	1.92	14.30	8.24	117.76	3.12	0.07	1.02
12.76	1.95	14.60	8.09	118.01	3.11	0.07	1.04
12.78	1.98	14.77	8.02	118.47	3.11	0.07	1.05
12.80	2.02	15.08	7.85	118.46	3.09	0.07	1.08
12.82	2.05	15.31	7.78	119.15	3.09	0.07	1.09
12.84	2.06	15.36	7.83	120.22	3.09	0.07	1.10
12.86	2.05	15.28	7.97	121.78	3.10	0.07	1.09
12.88	2.04	15.14	8.12	122.96	3.12	0.07	1.08
12.90	2.04	15.10	8.21	123.95	3.12	0.07	1.08
12.92	2.04	15.06	8.30	124.97	3.13	0.07	1.08
12.94	2.02	14.88	8.46	125.83	3.14	0.07	1.06
12.96	2.00	14.71	8.56	125.92	3.15	0.07	1.05
12.98	1.99	14.62	8.55	125.02	3.15	0.07	1.04
13.00	1.99	14.63	8.46	123.76	3.14	0.07	1.04
13.02	1.98	14.49	8.48	122.80	3.14	0.07	1.03
13.04	1.95	14.18	8.62	122.20	3.15	0.07	1.01
13.06	1.91	13.81	8.77	121.16	3.17	0.07	0.99
13.08	1.86	13.41	8.95	119.97	3.18	0.07	0.96
13.10	1.80	12.91	9.19	118.66	3.20	0.07	0.92
13.12	1.75	12.47	9.44	117.70	3.21	0.07	0.89
13.14	1.72	12.16	9.53	115.97	3.22	0.07	0.87
13.16	1.69	11.95	9.55	114.17	3.22	0.07	0.85
13.18	1.65	11.58	9.71	112.49	3.23	0.07	0.83
13.20	1.58	11.01	10.13	111.50	3.26	0.07	0.79
13.22	1.50	10.33	10.64	109.85	3.29	0.06	0.74
13.24	1.44	9.80	10.96	107.41	3.32	0.06	0.70
13.26	1.39	9.43	11.10	104.64	3.32	0.06	0.67
13.28	1.36	9.16	11.17	102.38	3.33	0.06	0.65
13.30	1.33	8.86	11.34	100.41	3.34	0.06	0.63
13.32	1.30	8.61	11.40	98.20	3.34	0.06	0.62
13.34	1.26	8.29	11.58	95.95	3.35	0.06	0.59
13.36	1.22	7.93	11.80	93.56	3.37	0.06	0.57
13.38	1.17	7.51	12.19	91.60	3.39	0.06	0.54
13.40	1.12	7.07	12.68	89.70	3.42	0.06	0.51
13.42	1.05	6.56	13.41	88.01	3.46	0.06	0.47
13.44	1.01	6.20	13.97	86.54	3.49	0.06	0.44

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
13.46	1.03	6.35	13.51	85.80	3.47	0.06	0.45
13.48	1.11	6.99	12.25	85.60	3.40	0.06	0.50
13.50	1.22	7.82	10.83	84.67	3.31	0.06	0.56
13.52	1.30	8.46	9.83	83.20	3.24	0.06	0.60
13.54	1.35	8.88	9.16	81.33	3.19	0.06	0.63
13.56	1.36	8.90	9.07	80.71	3.19	0.06	0.64
13.58	1.37	8.98	9.15	82.13	3.19	0.06	0.64
13.60	1.39	9.14	9.26	84.61	3.20	0.06	0.65
13.62	1.45	9.63	9.03	86.90	3.18	0.06	0.69
13.64	1.52	10.10	8.73	88.14	3.16	0.06	0.72
13.66	1.59	10.65	8.33	88.69	3.13	0.07	0.76
13.68	1.65	11.13	7.96	88.64	3.10	0.07	0.80
13.70	1.70	11.48	7.61	87.33	3.07	0.07	0.82
13.72	1.72	11.62	7.36	85.52	3.05	0.07	0.83
13.74	1.70	11.47	7.36	84.37	3.05	0.07	0.82
13.76	1.67	11.19	7.52	84.19	3.07	0.07	0.80
13.78	1.62	10.81	7.86	84.99	3.09	0.07	0.77
13.80	1.59	10.59	8.17	86.51	3.12	0.07	0.76
13.82	1.58	10.44	8.52	88.90	3.15	0.07	0.75
13.84	1.57	10.33	8.80	90.94	3.17	0.07	0.74
13.86	1.55	10.21	9.05	92.47	3.19	0.07	0.73
13.88	1.53	9.99	9.41	94.04	3.21	0.06	0.71
13.90	1.50	9.75	9.78	95.37	3.24	0.06	0.70
13.92	1.47	9.55	10.04	95.81	3.25	0.06	0.68
13.94	1.47	9.49	10.01	95.01	3.25	0.06	0.68
13.97	1.53	9.97	9.37	93.43	3.21	0.06	0.71
13.98	1.63	10.74	8.53	91.64	3.15	0.07	0.77
14.00	1.75	11.65	7.68	89.45	3.08	0.07	0.83
14.02	1.85	12.34	7.15	88.27	3.04	0.07	0.88
14.04	1.91	12.84	6.88	88.31	3.01	0.07	0.92
14.06	1.97	13.28	6.69	88.79	2.99	0.07	0.95
14.08	1.99	13.44	6.66	89.51	2.99	0.07	0.96
14.10	1.99	13.38	6.76	90.51	3.00	0.07	0.96
14.12	1.95	13.06	7.05	92.10	3.03	0.07	0.93
14.14	1.88	12.52	7.48	93.58	3.06	0.07	0.89
14.16	1.82	12.05	7.81	94.13	3.09	0.07	0.86
14.18	1.76	11.57	8.16	94.41	3.12	0.07	0.83
14.20	1.70	11.04	8.65	95.51	3.16	0.07	0.79
14.22	1.61	10.32	9.38	96.79	3.21	0.07	0.74
14.24	1.51	9.61	10.17	97.76	3.26	0.06	0.69
14.26	1.45	9.10	10.70	97.30	3.30	0.06	0.65
14.28	1.39	8.63	11.12	95.95	3.33	0.06	0.62
14.30	1.33	8.18	11.52	94.22	3.35	0.06	0.58
14.32	1.27	7.72	11.97	92.36	3.38	0.06	0.55
14.34	1.22	7.34	12.30	90.25	3.40	0.06	0.52
14.36	1.19	7.04	12.49	87.98	3.41	0.06	0.50
14.38	1.17	6.89	12.45	85.87	3.41	0.06	0.49
14.40	1.19	7.05	11.90	83.94	3.37	0.06	0.50

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
14.42	1.22	7.26	11.23	81.59	3.33	0.06	0.52
14.44	1.24	7.44	10.61	78.95	3.29	0.06	0.53
14.46	1.24	7.39	10.40	76.88	3.28	0.06	0.53
14.48	1.23	7.31	10.32	75.43	3.27	0.06	0.52
14.50	1.21	7.17	10.38	74.42	3.28	0.06	0.51
14.52	1.20	7.04	10.51	73.95	3.29	0.06	0.50
14.54	1.17	6.83	10.78	73.55	3.30	0.06	0.49
14.56	1.14	6.61	11.03	72.89	3.32	0.06	0.47
14.58	1.12	6.44	11.14	71.70	3.33	0.06	0.46
14.60	1.11	6.37	11.06	70.42	3.32	0.06	0.45
14.62	1.11	6.33	11.00	69.60	3.32	0.06	0.45
14.64	1.11	6.30	10.94	68.95	3.31	0.06	0.45
14.66	1.10	6.21	11.00	68.33	3.32	0.06	0.44
14.68	1.09	6.13	11.05	67.70	3.32	0.06	0.44
14.70	1.07	5.98	11.19	66.94	3.33	0.06	0.43
14.72	1.04	5.73	11.55	66.26	3.35	0.06	0.41
14.74	0.99	5.39	12.14	65.45	3.39	0.06	0.39
14.76	0.93	4.95	13.02	64.45	3.44	0.06	0.35
14.78	0.86	4.44	14.00	62.15	3.50	0.06	0.32
14.80	0.82	4.13	14.52	60.00	3.52	0.06	0.30
14.82	0.79	3.85	14.91	57.40	3.54	0.06	0.27
14.84	0.76	3.68	15.05	55.40	3.55	0.06	0.26
14.86	0.72	3.32	15.73	52.25	3.59	0.06	0.24
14.88	0.68	3.04	16.31	49.61	3.62	0.06	0.22
14.90	0.65	2.85	16.63	47.35	3.63	0.06	0.20
14.92	0.65	2.80	16.41	46.02	3.62	0.06	0.20
14.94	0.64	2.75	16.22	44.59	3.61	0.06	0.20
14.96	0.65	2.80	15.66	43.82	3.58	0.06	0.20
14.98	0.67	2.94	14.70	43.28	3.53	0.06	0.21
15.00	0.73	3.39	12.81	43.45	3.43	0.06	0.24
15.02	0.78	3.75	11.44	42.92	3.35	0.06	0.27
15.04	0.79	3.82	10.95	41.89	3.32	0.06	0.27
15.06	0.75	3.52	11.54	40.62	3.35	0.06	0.25
15.09	0.71	3.18	12.40	39.45	3.40	0.06	0.23
15.10	0.68	3.00	12.97	38.90	3.44	0.06	0.21
15.12	0.68	2.96	13.10	38.84	3.44	0.06	0.21
15.14	0.68	2.99	13.14	39.26	3.45	0.06	0.21
15.16	0.70	3.11	12.80	39.75	3.43	0.06	0.22
15.18	0.73	3.31	12.09	40.05	3.39	0.06	0.24
15.20	0.76	3.55	11.32	40.19	3.34	0.06	0.25
15.23	0.79	3.76	10.75	40.47	3.30	0.06	0.27
15.24	0.82	3.97	10.40	41.25	3.28	0.06	0.28
15.26	0.84	4.12	10.23	42.14	3.27	0.06	0.29
15.28	0.84	4.09	10.47	42.79	3.28	0.06	0.29
15.30	0.82	3.94	10.93	43.13	3.31	0.06	0.28
15.32	0.80	3.84	11.31	43.45	3.34	0.06	0.27
15.34	0.80	3.79	11.42	43.25	3.34	0.06	0.27
15.37	0.80	3.79	11.44	43.34	3.35	0.06	0.27

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
15.38	0.81	3.84	11.24	43.14	3.33	0.06	0.27
15.40	0.85	4.12	10.58	43.60	3.29	0.06	0.29
15.42	0.90	4.47	9.81	43.79	3.24	0.06	0.32
15.44	0.94	4.78	9.36	44.79	3.21	0.06	0.34
15.46	0.98	5.03	9.23	46.40	3.20	0.06	0.36
15.48	0.99	5.14	9.42	48.40	3.21	0.06	0.37
15.50	1.00	5.21	9.62	50.08	3.23	0.06	0.37
15.52	1.00	5.15	10.02	51.62	3.25	0.06	0.37
15.54	1.00	5.16	10.25	52.88	3.27	0.06	0.37
15.56	1.02	5.27	10.28	54.15	3.27	0.06	0.38
15.58	1.05	5.50	10.08	55.44	3.26	0.06	0.39
15.60	1.09	5.75	9.90	56.99	3.25	0.06	0.41
15.62	1.12	5.96	9.90	58.98	3.25	0.06	0.43
15.64	1.13	6.07	10.02	60.79	3.25	0.06	0.43
15.66	1.14	6.12	10.25	62.71	3.27	0.06	0.44
15.68	1.14	6.13	10.49	64.33	3.29	0.06	0.44
15.70	1.14	6.12	10.77	65.94	3.30	0.06	0.44
15.72	1.16	6.22	10.79	67.08	3.30	0.06	0.44
15.74	1.17	6.27	10.85	68.08	3.31	0.06	0.45
15.76	1.19	6.43	10.78	69.28	3.30	0.06	0.46
15.78	1.19	6.45	10.96	70.66	3.32	0.06	0.46
15.82	1.21	6.55	11.02	72.20	3.32	0.06	0.47
15.82	1.22	6.63	11.09	73.52	3.32	0.06	0.47
15.84	1.24	6.70	11.12	74.49	3.33	0.06	0.48
15.86	1.24	6.74	11.17	75.37	3.33	0.06	0.48
15.88	1.25	6.79	11.20	76.06	3.33	0.06	0.49
15.90	1.27	6.88	11.16	76.82	3.33	0.06	0.49
15.93	1.27	6.93	11.15	77.25	3.33	0.06	0.49
15.94	1.29	7.02	11.10	77.88	3.32	0.06	0.50
15.96	1.30	7.06	11.11	78.51	3.33	0.06	0.50
15.98	1.30	7.11	11.16	79.37	3.33	0.06	0.51
16.00	1.32	7.20	11.17	80.35	3.33	0.06	0.51
16.02	1.35	7.43	10.97	81.49	3.32	0.06	0.53
16.04	1.39	7.65	10.74	82.20	3.30	0.06	0.55
16.06	1.41	7.78	10.62	82.67	3.29	0.06	0.56
16.08	1.42	7.83	10.58	82.84	3.29	0.06	0.56
16.10	1.44	7.96	10.45	83.14	3.28	0.06	0.57
16.12	1.46	8.09	10.31	83.41	3.27	0.06	0.58
16.14	1.48	8.23	10.20	84.03	3.27	0.06	0.59
16.16	1.49	8.30	10.18	84.56	3.26	0.06	0.59
16.18	1.50	8.39	10.16	85.19	3.26	0.06	0.60
16.20	1.53	8.55	9.99	85.39	3.25	0.06	0.61
16.22	1.55	8.69	9.82	85.35	3.24	0.06	0.62
16.24	1.57	8.80	9.67	85.11	3.23	0.06	0.63
16.26	1.57	8.79	9.68	85.02	3.23	0.06	0.63
16.28	1.58	8.82	9.66	85.25	3.23	0.06	0.63
16.30	1.58	8.84	9.69	85.65	3.23	0.06	0.63
16.32	1.58	8.84	9.72	85.90	3.23	0.06	0.63

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
16.34	1.56	8.69	9.91	86.10	3.25	0.06	0.62
16.36	1.54	8.51	10.12	86.07	3.26	0.06	0.61
16.38	1.51	8.30	10.33	85.74	3.27	0.06	0.59
16.40	1.48	8.07	10.55	85.19	3.29	0.06	0.58
16.42	1.45	7.86	10.74	84.49	3.30	0.06	0.56
16.44	1.42	7.65	10.95	83.77	3.31	0.06	0.55
16.46	1.41	7.54	11.00	82.97	3.32	0.06	0.54
16.48	1.38	7.36	11.13	81.96	3.33	0.06	0.53
16.50	1.36	7.22	11.18	80.77	3.33	0.06	0.52
16.52	1.36	7.23	10.91	78.93	3.31	0.06	0.52
16.54	1.40	7.47	10.28	76.79	3.27	0.06	0.53
16.56	1.46	7.83	9.53	74.61	3.22	0.06	0.56
16.58	1.51	8.17	8.95	73.08	3.18	0.06	0.58
16.60	1.54	8.36	8.66	72.35	3.16	0.06	0.60
16.62	1.57	8.54	8.41	71.86	3.14	0.06	0.61
16.64	1.56	8.48	8.52	72.23	3.15	0.06	0.61
16.66	1.55	8.44	8.69	73.35	3.16	0.06	0.60
16.68	1.51	8.15	9.21	75.07	3.20	0.06	0.58
16.70	1.48	7.94	9.62	76.38	3.23	0.06	0.57
16.72	1.45	7.68	9.99	76.75	3.25	0.06	0.55
16.74	1.41	7.40	10.39	76.91	3.28	0.06	0.53
16.76	1.36	7.06	10.90	76.95	3.31	0.06	0.50
16.78	1.32	6.79	11.31	76.78	3.34	0.06	0.49
16.80	1.31	6.73	11.38	76.57	3.34	0.06	0.48
16.82	1.30	6.67	11.40	76.02	3.34	0.06	0.48
16.84	1.28	6.54	11.55	75.51	3.35	0.06	0.47
16.86	1.26	6.38	11.67	74.49	3.36	0.06	0.46
16.88	1.25	6.30	11.57	72.89	3.35	0.06	0.45
16.90	1.24	6.21	11.45	71.15	3.35	0.06	0.44
16.92	1.21	6.02	11.55	69.57	3.35	0.06	0.43
16.94	1.16	5.68	11.96	67.95	3.38	0.06	0.41
16.96	1.11	5.36	12.29	65.82	3.40	0.06	0.38
16.98	1.07	5.07	12.52	63.47	3.41	0.06	0.36
17.00	1.04	4.83	12.73	61.49	3.42	0.06	0.35
17.02	1.01	4.67	12.79	59.73	3.43	0.06	0.33
17.04	1.00	4.58	12.69	58.08	3.42	0.06	0.33
17.06	1.00	4.56	12.42	56.59	3.41	0.06	0.33
17.08	0.98	4.43	12.51	55.39	3.41	0.06	0.32
17.10	0.95	4.21	12.91	54.30	3.43	0.06	0.30
17.12	0.92	4.03	13.19	53.13	3.45	0.06	0.29
17.14	0.91	3.93	13.20	51.92	3.45	0.06	0.28
17.17	0.91	3.96	12.78	50.67	3.43	0.06	0.28
17.18	0.93	4.06	12.17	49.40	3.39	0.06	0.29
17.20	0.94	4.16	11.60	48.27	3.36	0.06	0.30
17.22	0.95	4.22	11.09	46.87	3.32	0.06	0.30
17.24	0.96	4.25	10.76	45.76	3.30	0.06	0.30
17.26	0.95	4.19	10.71	44.90	3.30	0.06	0.30
17.28	0.95	4.17	10.71	44.67	3.30	0.06	0.30

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
17.30	0.95	4.17	10.74	44.78	3.30	0.06	0.30
17.32	0.96	4.24	10.56	44.80	3.29	0.06	0.30
17.34	0.96	4.24	10.52	44.65	3.29	0.06	0.30
17.36	0.96	4.20	10.52	44.16	3.29	0.06	0.30
17.38	0.95	4.17	10.44	43.58	3.28	0.06	0.30
17.40	0.97	4.25	10.09	42.87	3.26	0.06	0.30
17.42	1.00	4.46	9.54	42.55	3.22	0.06	0.32
17.44	1.04	4.70	8.96	42.10	3.18	0.06	0.34
17.46	1.07	4.92	8.50	41.76	3.14	0.06	0.35
17.48	1.08	4.96	8.35	41.44	3.13	0.06	0.35
17.50	1.07	4.91	8.47	41.59	3.14	0.06	0.35
17.52	1.05	4.78	8.75	41.79	3.16	0.06	0.34
17.54	1.04	4.67	8.93	41.69	3.18	0.06	0.33
17.56	1.03	4.60	8.99	41.36	3.18	0.06	0.33
17.58	1.02	4.55	9.13	41.55	3.19	0.06	0.32
17.60	1.01	4.50	9.33	42.00	3.21	0.06	0.32
17.62	1.01	4.47	9.53	42.55	3.22	0.06	0.32
17.64	1.01	4.49	9.42	42.30	3.21	0.06	0.32
17.66	1.04	4.64	9.06	42.05	3.19	0.06	0.33
17.68	1.08	4.88	8.64	42.14	3.16	0.06	0.35
17.70	1.11	5.10	8.42	42.94	3.14	0.06	0.36
17.72	1.12	5.16	8.54	44.08	3.15	0.06	0.37
17.74	1.12	5.18	8.68	44.91	3.16	0.06	0.37
17.76	1.13	5.22	8.66	45.24	3.16	0.06	0.37
17.78	1.27	6.11	7.64	46.73	3.08	0.06	0.44
17.80	1.38	6.79	7.27	49.39	3.05	0.06	0.49
17.82	1.42	7.03	7.56	53.12	3.07	0.06	0.50
17.84	1.31	6.32	8.74	55.26	3.16	0.06	0.45
17.86	1.19	5.57	9.82	54.66	3.24	0.06	0.40
17.88	1.13	5.14	10.27	52.75	3.27	0.06	0.37
17.90	1.07	4.79	10.50	50.26	3.29	0.06	0.34
17.92	1.05	4.66	10.44	48.68	3.28	0.06	0.33
17.94	1.04	4.55	10.30	46.91	3.27	0.06	0.33
17.96	1.02	4.45	10.13	45.03	3.26	0.06	0.32
17.98	0.98	4.19	10.24	42.87	3.27	0.06	0.30
18.00	0.94	3.93	10.48	41.18	3.28	0.06	0.28
18.02	0.91	3.71	10.78	40.01	3.30	0.06	0.27
18.04	0.90	3.64	10.88	39.59	3.31	0.06	0.26
18.06	0.90	3.63	10.84	39.37	3.31	0.06	0.26
18.08	0.91	3.72	10.62	39.47	3.29	0.06	0.27
18.10	0.92	3.79	10.40	39.41	3.28	0.06	0.27
18.12	0.93	3.83	10.26	39.31	3.27	0.06	0.27
18.14	0.94	3.89	10.07	39.16	3.26	0.06	0.28
18.16	0.96	4.01	9.74	39.00	3.23	0.06	0.29
18.18	0.98	4.14	9.32	38.63	3.21	0.06	0.30
18.20	0.99	4.21	9.08	38.23	3.19	0.06	0.30
18.22	0.98	4.14	9.23	38.23	3.20	0.06	0.30
18.24	0.95	3.95	9.84	38.85	3.24	0.06	0.28

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
18.26	0.92	3.72	10.48	39.03	3.28	0.06	0.27
18.28	0.89	3.55	10.89	38.69	3.31	0.06	0.25
18.30	0.89	3.52	10.82	38.03	3.31	0.06	0.25
18.32	0.89	3.50	10.71	37.53	3.30	0.06	0.25
18.34	0.88	3.50	10.65	37.25	3.30	0.06	0.25
18.36	0.88	3.48	10.64	36.99	3.30	0.06	0.25
18.38	0.88	3.46	10.63	36.76	3.29	0.06	0.25
18.40	0.88	3.48	10.59	36.88	3.29	0.06	0.25
18.42	0.91	3.61	10.34	37.29	3.27	0.06	0.26
18.44	0.96	3.96	9.62	38.09	3.23	0.06	0.28
18.46	1.03	4.39	8.85	38.84	3.17	0.06	0.31
18.48	1.11	4.86	8.17	39.77	3.12	0.06	0.35
18.50	1.16	5.16	7.81	40.32	3.09	0.06	0.37
18.52	1.19	5.34	7.55	40.30	3.07	0.06	0.38
18.54	1.19	5.31	7.59	40.28	3.07	0.06	0.38
18.56	1.16	5.16	7.91	40.84	3.10	0.06	0.37
18.58	1.14	5.00	8.42	42.12	3.14	0.06	0.36
18.60	1.13	4.96	8.75	43.37	3.16	0.06	0.35
18.62	1.15	5.07	8.86	44.94	3.17	0.06	0.36
18.64	1.20	5.39	8.63	46.48	3.15	0.06	0.38
18.66	1.28	5.83	8.26	48.10	3.13	0.06	0.42
18.68	1.38	6.43	7.71	49.56	3.08	0.06	0.46
18.70	1.50	7.21	7.01	50.56	3.02	0.06	0.52
18.72	1.70	8.39	6.14	51.54	2.94	0.06	0.60
18.74	1.89	9.59	5.52	52.94	2.88	0.07	0.68
18.76	2.06	10.59	5.25	55.63	2.85	0.07	0.76
18.78	2.28	11.90	5.32	63.30	2.86	0.07	0.85
18.80	2.41	12.71	5.55	70.53	2.88	0.08	0.91
18.82	2.37	12.45	6.15	76.61	2.95	0.07	0.89
18.84	2.04	10.42	7.38	76.92	3.06	0.07	0.74
18.86	1.65	8.02	9.25	74.15	3.20	0.06	0.57
18.88	1.34	6.15	11.31	69.56	3.34	0.06	0.44
18.90	1.15	4.97	13.06	64.94	3.44	0.06	0.36
18.92	1.05	4.38	13.94	61.06	3.49	0.06	0.31
18.94	1.03	4.22	13.79	58.25	3.48	0.06	0.30
18.96	1.04	4.29	13.02	55.88	3.44	0.06	0.31
18.98	1.06	4.42	12.04	53.20	3.38	0.06	0.32
19.00	1.11	4.69	10.57	49.54	3.29	0.06	0.33
19.02	1.18	5.09	9.06	46.07	3.19	0.06	0.36
19.04	1.25	5.52	7.99	44.08	3.10	0.06	0.39
19.06	1.31	5.91	7.48	44.21	3.06	0.06	0.42
19.08	1.38	6.29	7.27	45.75	3.05	0.06	0.45
19.10	1.45	6.69	7.15	47.84	3.04	0.06	0.48
19.12	1.51	7.10	7.15	50.76	3.04	0.06	0.51
19.15	1.59	7.54	7.15	53.90	3.04	0.06	0.54
19.16	1.72	8.30	6.87	57.04	3.01	0.06	0.59
19.19	1.92	9.53	6.27	59.79	2.96	0.07	0.68
19.20	2.29	11.72	5.38	63.09	2.87	0.07	0.84

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
19.22	2.65	13.89	4.84	67.22	2.81	0.08	0.99
19.24	2.88	15.22	4.79	72.91	2.80	0.08	1.09
19.26	2.74	14.40	5.42	78.03	2.87	0.08	1.03
19.28	2.39	12.25	6.54	80.19	2.98	0.07	0.88
19.30	1.97	9.76	8.02	78.26	3.11	0.07	0.70
19.32	1.87	9.12	8.13	74.15	3.12	0.06	0.65
19.34	2.03	10.07	7.04	70.86	3.03	0.07	0.72
19.36	2.21	11.12	6.21	69.04	2.95	0.07	0.79
19.38	2.16	10.84	6.53	70.77	2.98	0.07	0.77
19.40	2.02	9.99	7.32	73.06	3.05	0.07	0.71
19.42	2.16	10.82	6.83	73.97	3.01	0.07	0.77
19.44	2.46	12.59	5.77	72.59	2.91	0.08	0.90
19.46	2.70	13.95	5.28	73.70	2.86	0.08	1.00
19.48	2.71	13.99	5.54	77.45	2.88	0.08	1.00
19.50	2.66	13.73	5.93	81.35	2.92	0.07	0.98
19.52	2.71	13.95	5.82	81.24	2.91	0.08	1.00
19.54	2.74	14.15	5.65	79.91	2.89	0.08	1.01
19.56	2.63	13.48	6.10	82.26	2.94	0.07	0.96
19.58	2.36	11.88	6.95	82.55	3.02	0.07	0.85
19.60	2.01	9.78	8.42	82.33	3.14	0.07	0.70
19.62	1.78	8.43	9.36	78.89	3.21	0.06	0.60
19.64	1.83	8.72	8.99	78.44	3.18	0.06	0.62
19.66	2.25	11.20	6.90	77.31	3.01	0.07	0.80
19.68	2.79	14.32	5.17	74.07	2.84	0.08	1.02
19.70	3.23	17.11	4.18	71.50	2.72	0.09	1.20
19.72	3.22	17.06	4.15	70.79	2.72	0.09	1.20
19.74	2.89	14.83	4.73	70.20	2.79	0.08	1.06
19.76	2.45	12.30	5.67	69.72	2.90	0.07	0.88
19.78	2.38	11.83	5.97	70.63	2.93	0.07	0.85
19.80	2.64	13.37	5.35	71.48	2.86	0.08	0.96
19.82	3.22	16.85	4.39	73.95	2.75	0.09	1.19
19.84	3.76	20.40	3.68	75.12	2.66	0.09	1.42
19.86	4.21	23.38	3.27	76.50	2.59	0.10	0.64
19.88	4.37	24.48	3.11	76.09	2.56	0.10	0.65
19.90	4.29	23.95	3.12	74.71	2.57	0.10	0.64
19.92	4.12	22.79	3.25	74.15	2.59	0.09	0.64
19.94	3.99	21.80	3.50	76.21	2.63	0.09	1.51
19.96	4.10	22.37	3.57	79.80	2.64	0.09	1.55
19.98	4.38	24.07	3.48	83.84	2.62	0.10	1.66
20.00	4.80	26.76	3.28	87.87	2.59	0.10	0.66
20.02	5.16	29.00	3.15	91.35	2.57	0.11	0.67
20.04	5.39	30.45	3.09	94.05	2.56	0.11	0.67
20.06	5.42	30.56	3.09	94.58	2.56	0.11	0.67
20.08	5.32	29.91	3.14	93.79	2.57	0.11	0.67
20.10	5.12	28.55	3.24	92.60	2.59	0.11	0.66
20.12	4.86	26.80	3.43	91.84	2.62	0.10	1.85
20.15	4.54	24.61	3.73	91.81	2.66	0.10	1.71
20.16	4.14	21.94	4.19	91.99	2.73	0.10	1.55

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
20.18	3.72	19.22	4.81	92.39	2.80	0.09	1.37
20.20	3.24	16.49	5.70	94.01	2.90	0.08	1.18
20.22	2.86	14.27	6.56	93.68	2.98	0.07	1.02
20.25	2.74	13.59	6.51	88.52	2.98	0.07	0.97
20.26	2.95	14.77	5.62	82.96	2.89	0.08	1.06
20.28	3.40	17.34	4.60	79.76	2.78	0.09	1.24
20.30	3.79	19.67	4.32	84.90	2.74	0.09	1.39
20.32	4.06	21.20	4.34	92.12	2.75	0.10	1.50
20.34	4.24	22.10	4.46	98.49	2.76	0.10	1.57
20.36	4.37	22.82	4.45	101.63	2.76	0.10	1.62
20.38	4.47	23.47	4.33	101.57	2.74	0.10	1.66
20.40	4.55	23.94	4.21	100.81	2.73	0.10	1.69
20.42	4.58	24.12	4.22	101.80	2.73	0.10	1.70
20.44	4.65	24.44	4.23	103.46	2.73	0.10	1.73
20.46	4.90	25.98	4.07	105.71	2.71	0.10	1.83
20.48	5.36	28.89	3.72	107.45	2.66	0.11	2.01
20.50	6.07	33.43	3.28	109.63	2.59	0.12	0.68
20.52	6.92	39.10	2.81	109.74	2.51	0.12	0.70
20.54	7.84	45.43	2.39	108.62	2.42	0.13	0.72
20.56	8.61	50.82	2.12	107.73	2.35	0.14	0.74
20.58	9.18	55.05	1.91	105.00	2.29	0.14	0.75
20.60	9.56	58.12	1.73	100.76	2.23	0.14	0.75
20.62	9.88	61.18	1.54	94.44	2.15	0.13	0.76
20.64	10.03	63.00	1.42	89.59	2.08	0.13	0.76
20.66	10.04	63.76	1.34	85.29	2.03	0.12	0.77
20.68	9.94	63.82	1.27	80.78	1.97	0.11	0.77
20.70	9.84	64.11	1.19	76.41	1.90	0.10	0.77
20.72	9.83	65.10	1.00	65.10	1.83	0.09	0.77
20.74	9.92	66.35	1.00	66.35	1.78	0.08	0.77
20.76	10.01	67.13	1.00	67.13	1.77	0.08	0.77
20.78	10.14	67.75	1.00	67.75	1.78	0.09	0.77

Abbreviations

q_t:	Total cone resistance
K_c:	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c:	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

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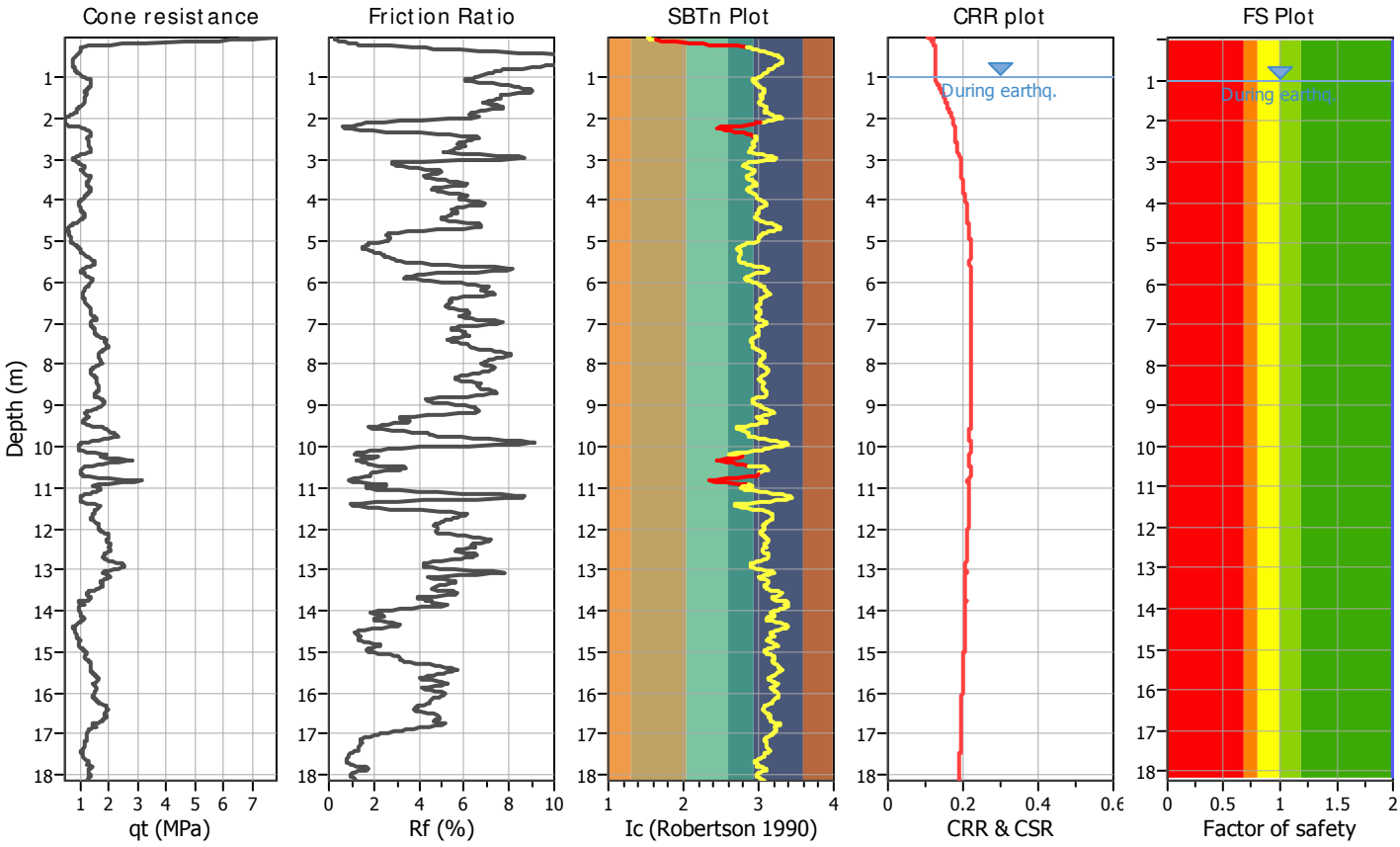
LIQUEFACTION ANALYSIS REPORT

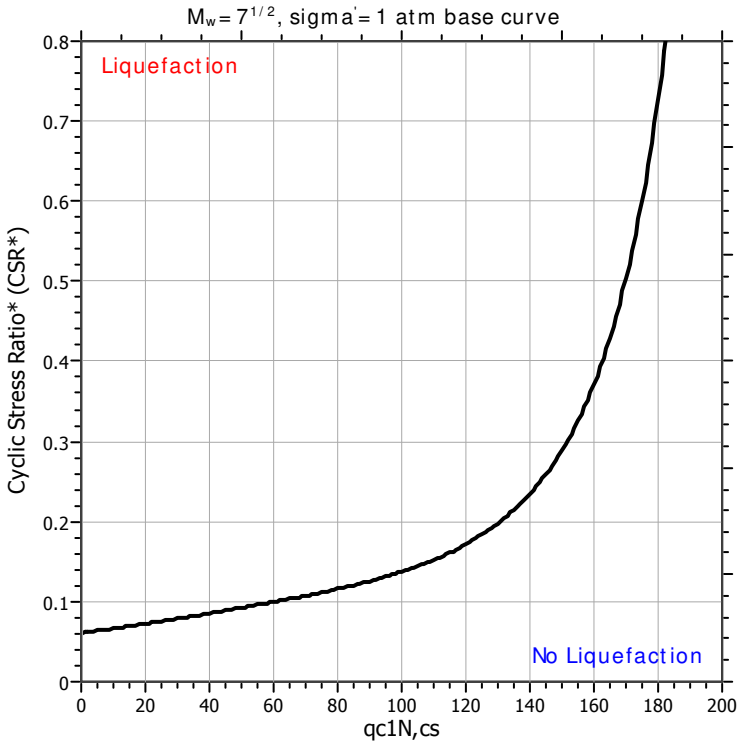
Project title : Location :

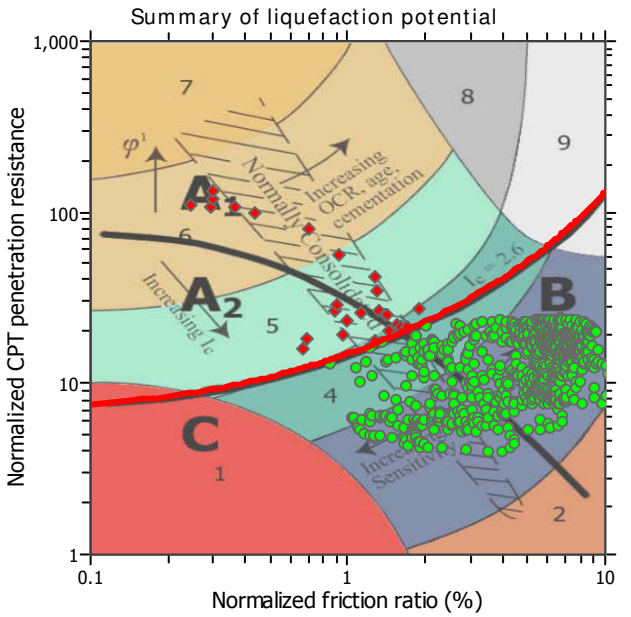
CPT file : CPTu-06_Biancolina

Input parameters and analysis data

Analysis method:	B&I (2014)	G.W.T. (in-situ):	1.80 m	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.00 m	Fill height:	N/A	Limit depth applied:	No
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	N/A
Earthquake magnitude M_w:	6.14	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.23	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		

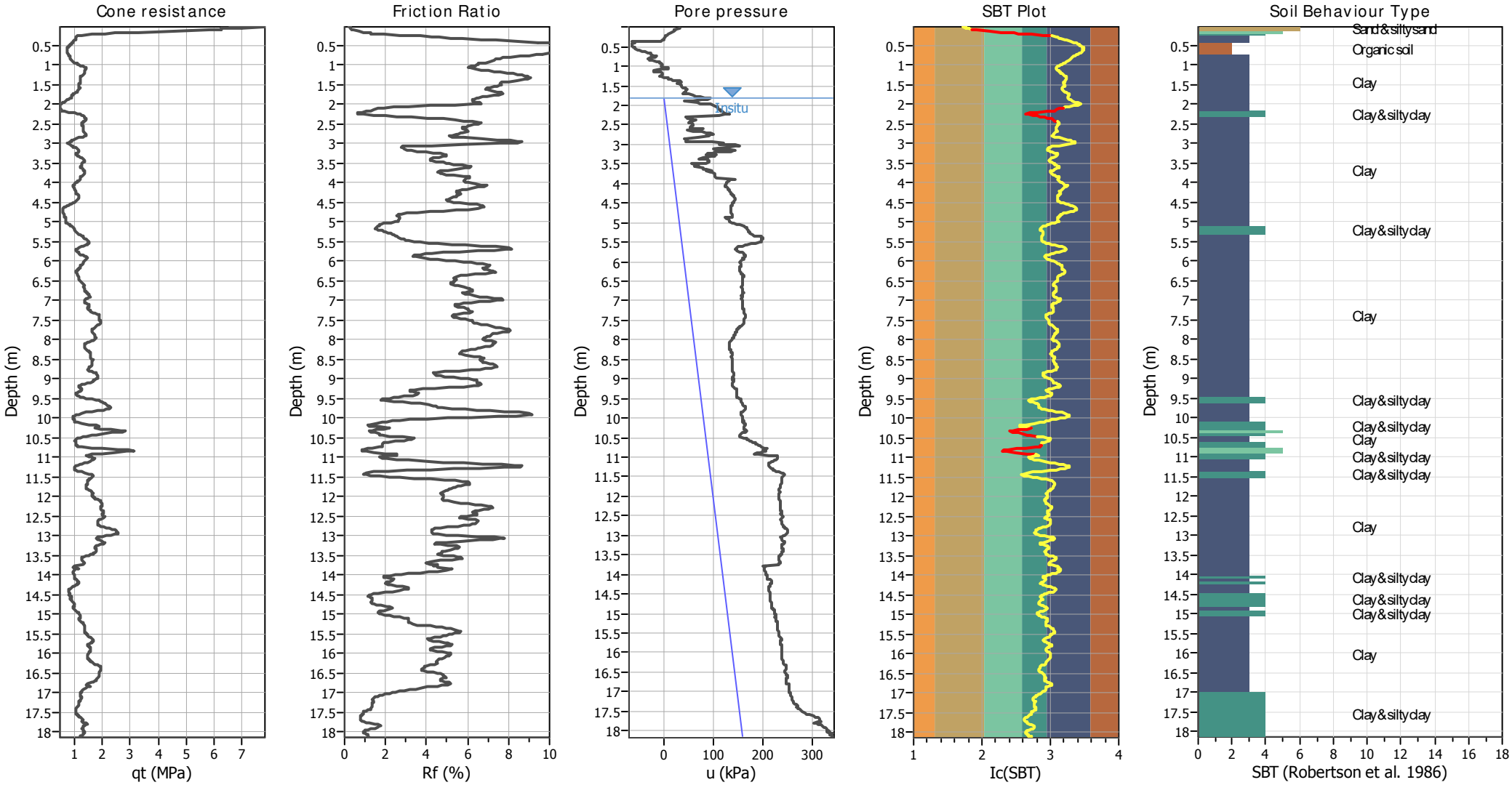






Zone A_1: Cyclic liquefaction likely depending on size and duration of cyclic loading
Zone A_2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



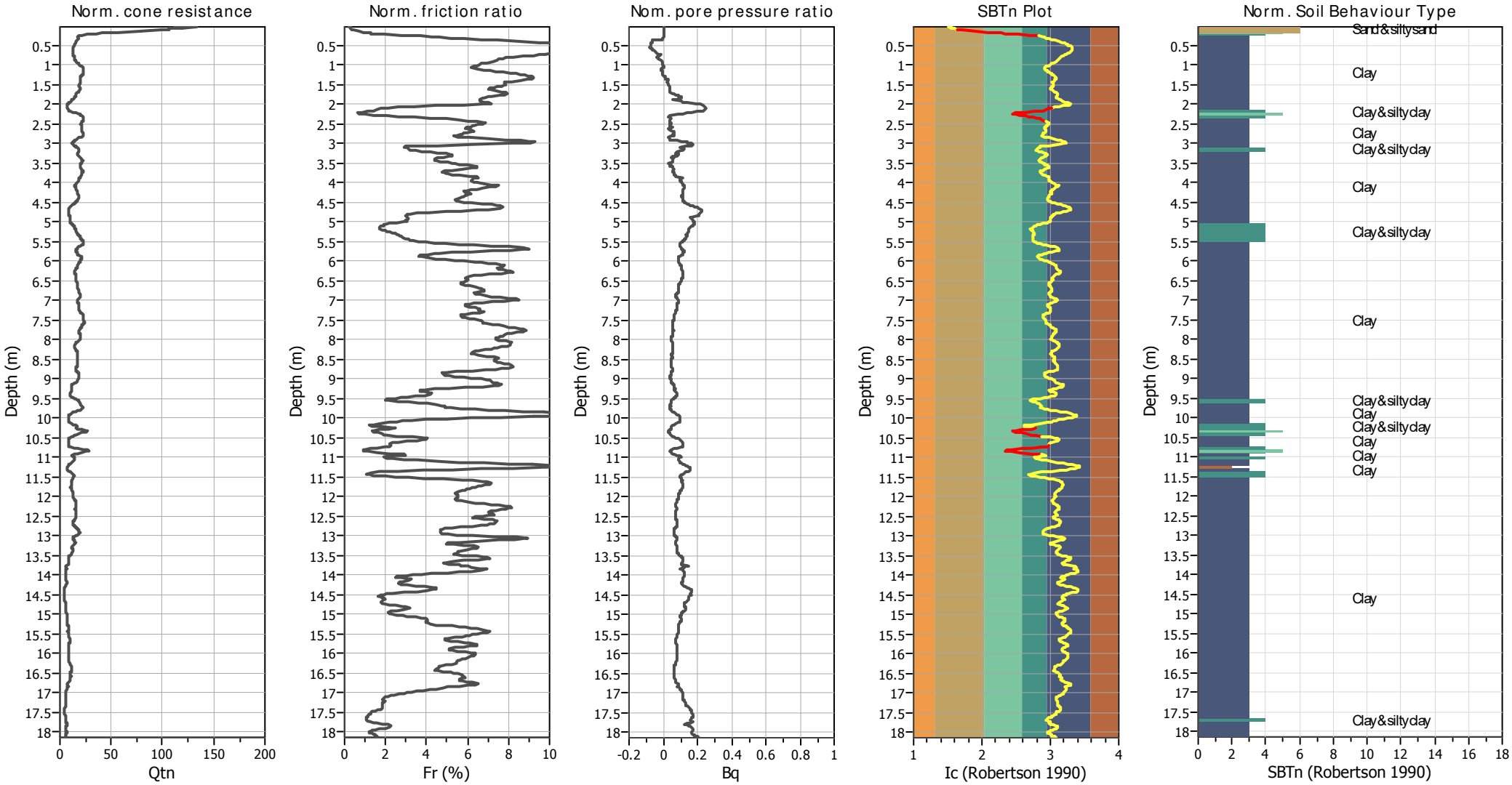
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	1.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.23	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	1.80 m	Fill height:	N/A	Limit depth:	N/A

SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

CPT basic interpretation plots (normalized)



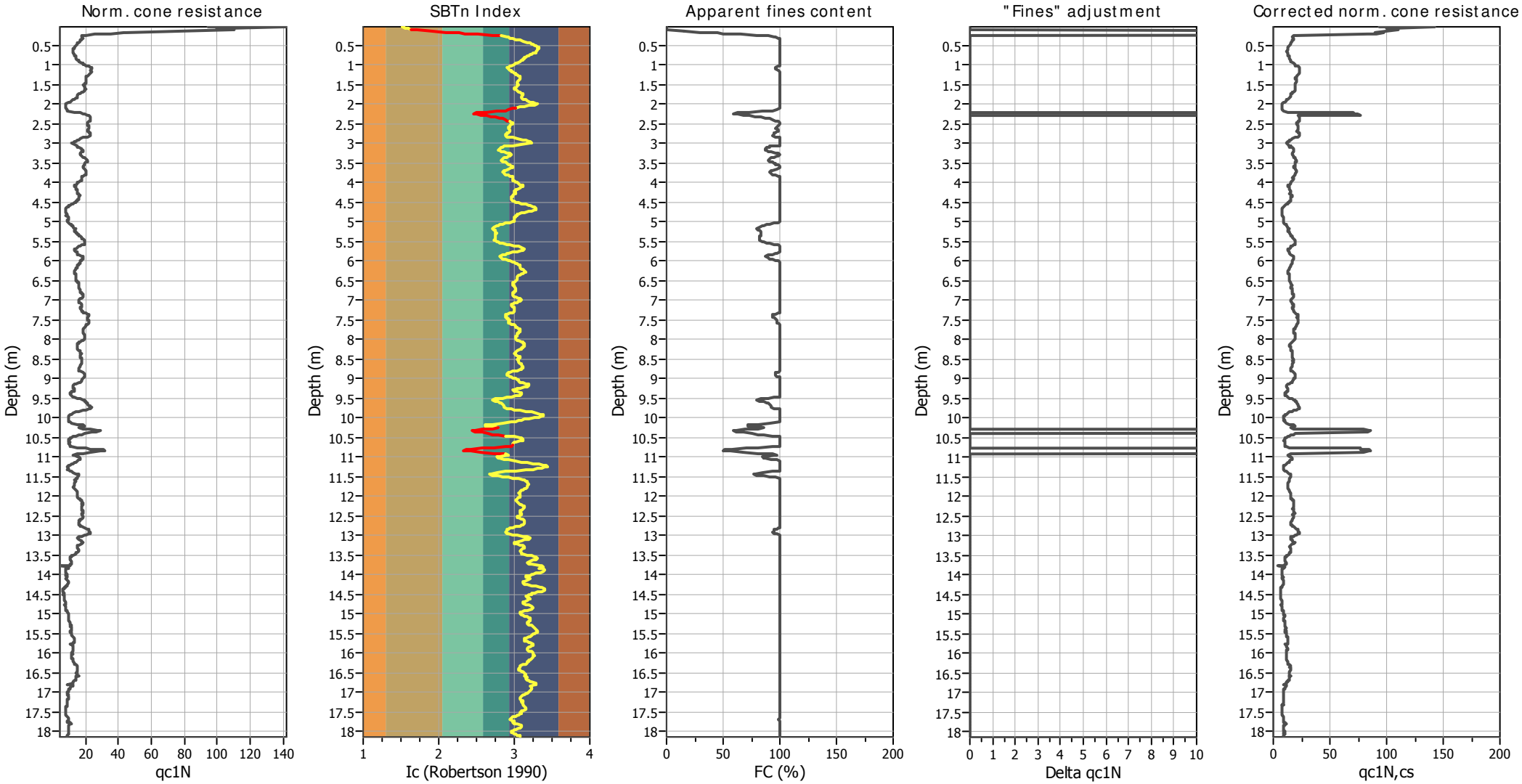
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	1.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.23	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	1.80 m	Fill height:	N/A	Limit depth:	N/A

SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

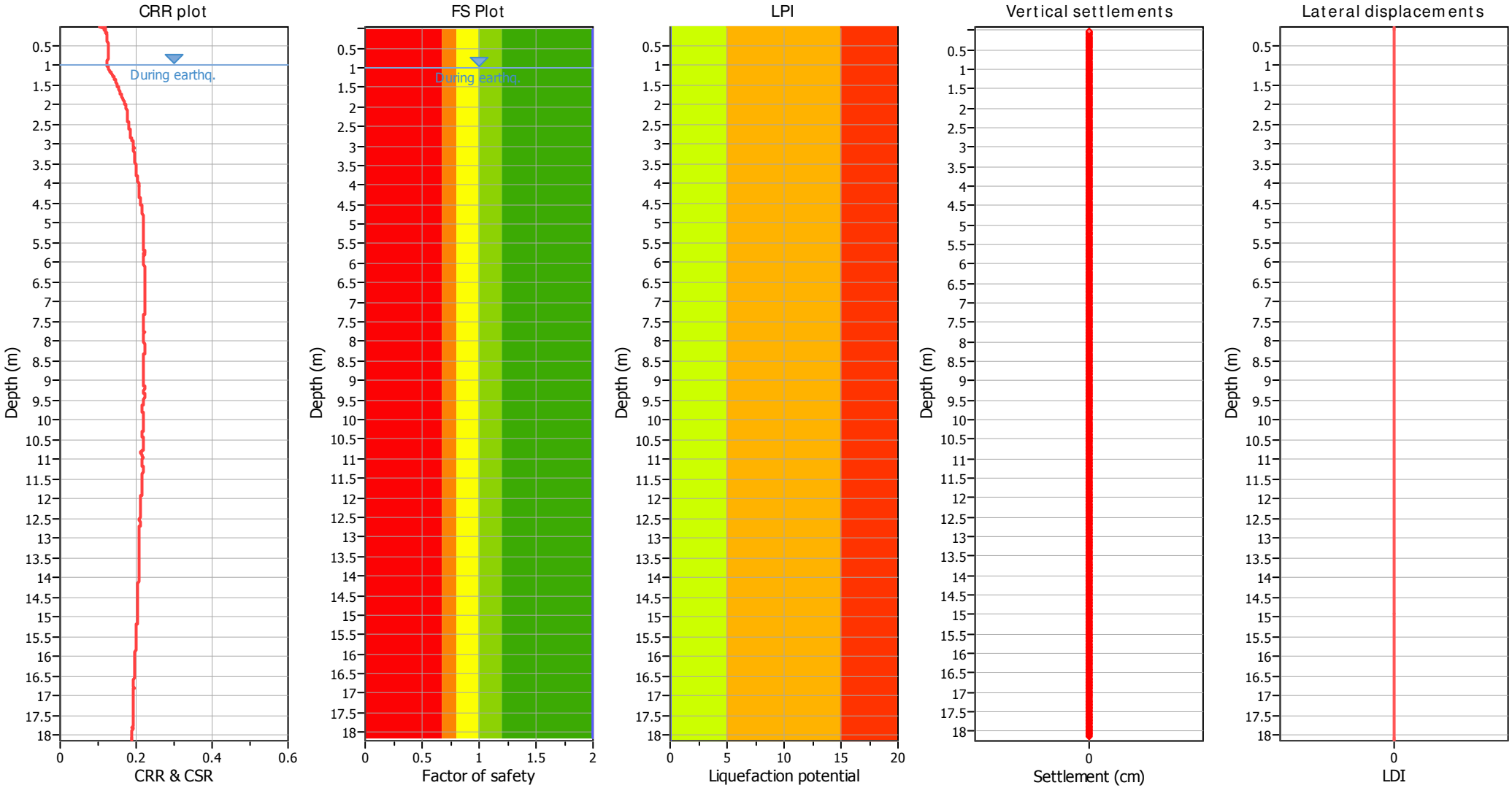
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	1.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.23	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	1.80 m	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	1.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.23	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	1.80 m	Fill height:	N/A	Limit depth:	N/A

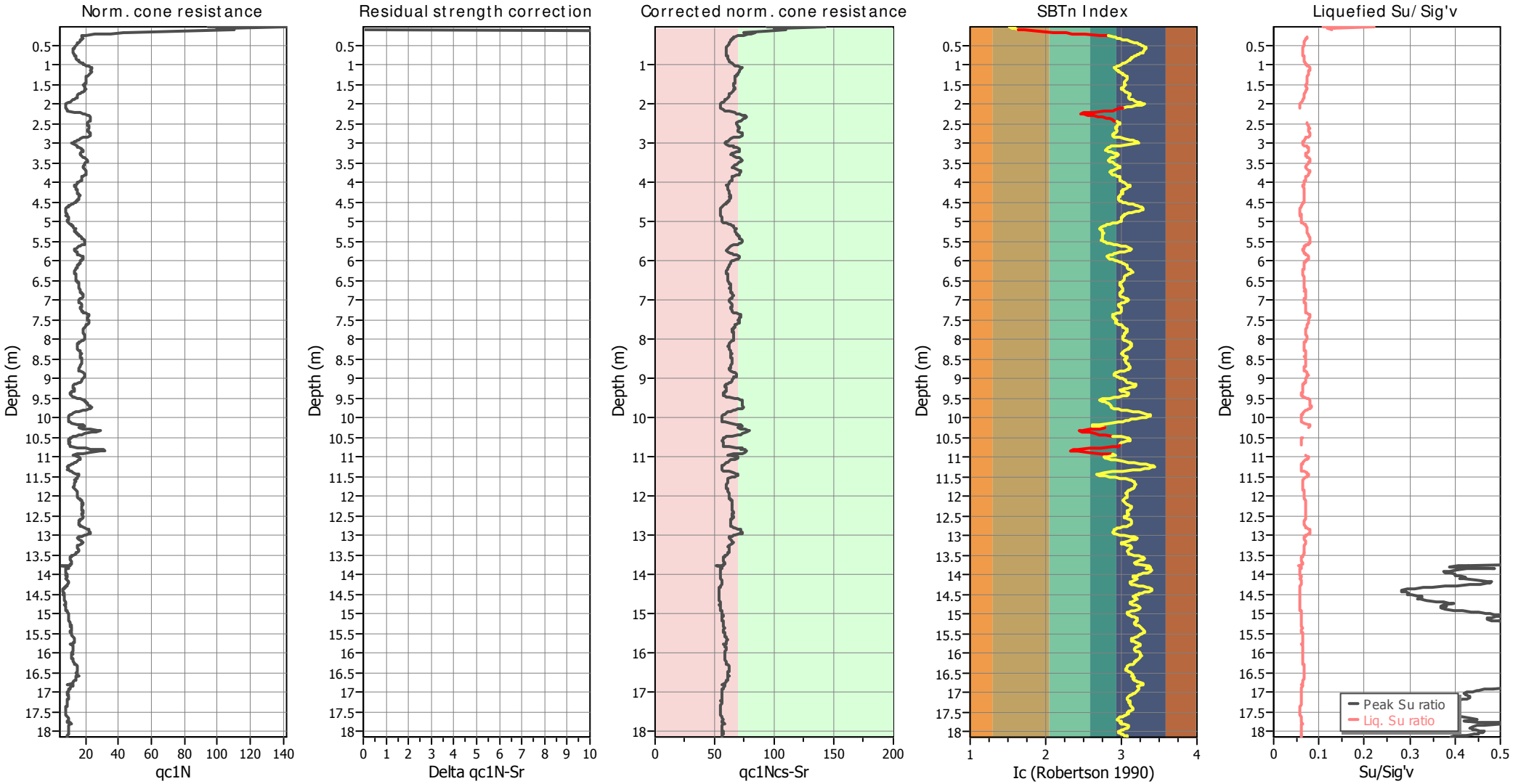
F.S. color scheme

- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

LPI color scheme

- Very high risk
- High risk
- Low risk

Check for strength loss plots (Idriss & Boulanger (2008))



Input parameters and analysis data

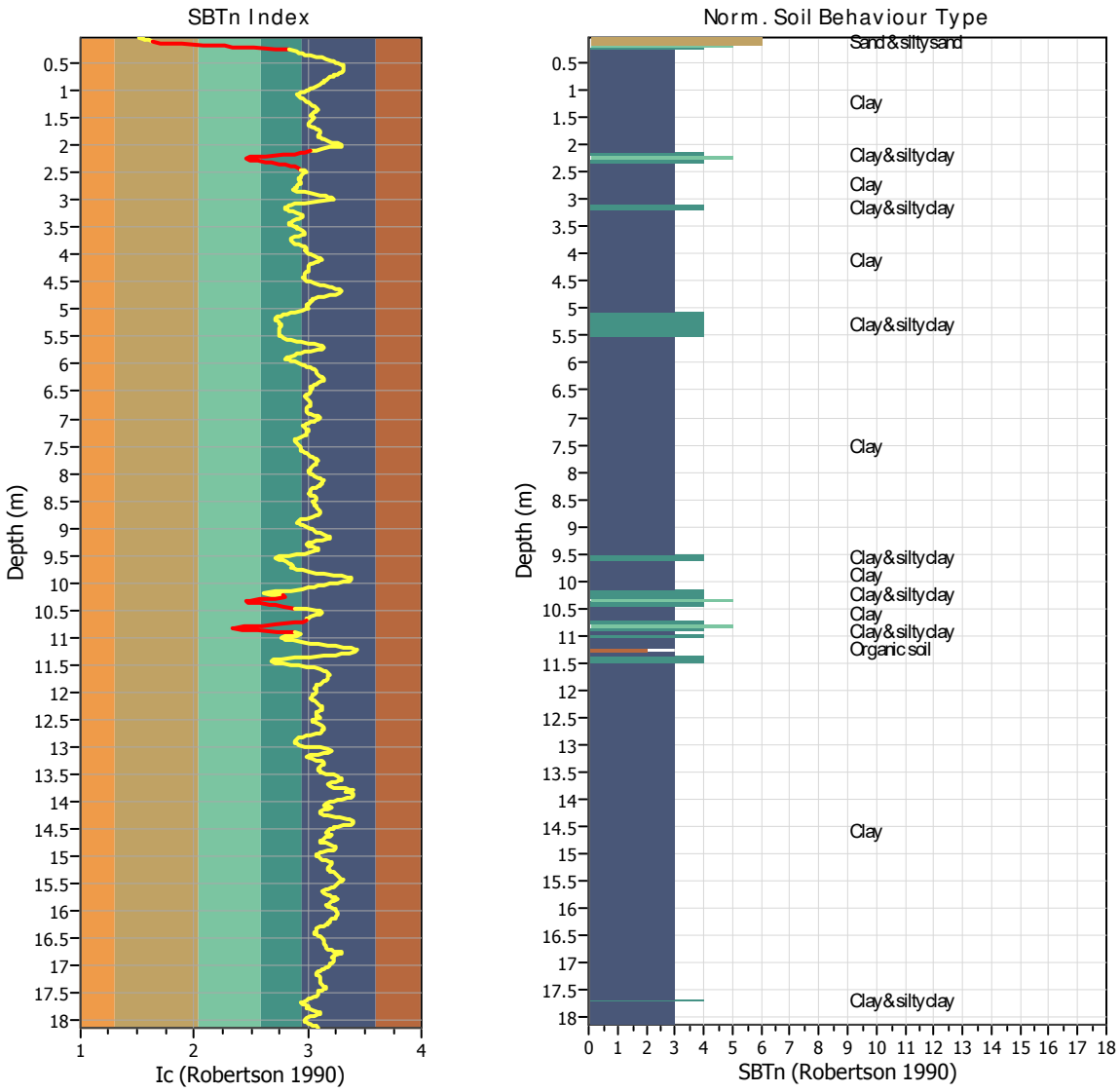
Analysis method:	B&I (2014)	Depth to GWT (erthq.):	1.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.23	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	1.80 m	Fill height:	N/A	Limit depth:	N/A

TRANSITION LAYER DETECTION ALGORITHM REPORT
Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vise-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between $1.80 < I_c < 3.0$) and a rate of change of I_c. Transitions typically occur when the rate of change of I_c is fast (i.e. delta I_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties		General statistics	
I_c minimum check value:	1.70	Total points in CPT file:	907
I_c maximum check value:	3.00	Total points excluded:	55
I_c change ratio value:	0.0100	Exclusion percentage:	6.06%
Minimum number of points in layer:	4	Number of layers detected:	7

Transition layer No	Number of points	Depth	SBT_n number	SBT_n description
Transition layer 1	9	Start depth: 0.12 (m)	6	Sand & silty sand
		End depth: 0.28 (m)	3	Clay
Transition layer 2	7	Start depth: 2.12 (m)	3	Clay
		End depth: 2.24 (m)	5	Silty sand & sandy silt
Transition layer 3	12	Start depth: 2.24 (m)	5	Silty sand & sandy silt
		End depth: 2.46 (m)	3	Clay
Transition layer 4	5	Start depth: 10.26 (m)	4	Clay & silty clay
		End depth: 10.34 (m)	5	Silty sand & sandy silt
Transition layer 5	8	Start depth: 10.34 (m)	5	Silty sand & sandy silt
		End depth: 10.48 (m)	3	Clay
Transition layer 6	8	Start depth: 10.70 (m)	3	Clay
		End depth: 10.84 (m)	5	Silty sand & sandy silt
Transition layer 7	6	Start depth: 10.84 (m)	5	Silty sand & sandy silt
		End depth: 10.94 (m)	3	Clay

Start depth: Depth where the transition layer begins
End depth: Depth where the transition layer ends

:: Field input data ::

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
1	0.03	5.62	11.15	32.12	3.51	16.90
2	0.04	8.47	25.79	32.86	3.06	17.40
3	0.07	6.51	18.71	22.34	3.70	17.23
4	0.08	5.97	18.07	23.75	4.35	17.04
5	0.10	6.26	18.29	22.03	5.03	17.29
6	0.12	6.56	31.88	20.43	5.00	17.39
7	0.14	4.70	26.31	14.77	10.37	17.58
8	0.17	2.68	39.38	9.72	15.43	17.37
9	0.18	2.55	25.42	8.68	21.61	17.28
10	0.20	2.12	28.37	7.57	24.14	17.06
11	0.22	1.54	27.18	4.98	31.68	17.10
12	0.24	1.20	35.80	3.88	40.77	17.15
13	0.26	1.05	40.35	2.46	48.05	17.27
14	0.28	1.03	44.11	1.66	51.79	17.35
15	0.30	1.02	47.41	0.80	52.98	17.46
16	0.32	1.08	52.86	-0.12	54.96	17.60
17	0.34	1.05	62.58	-2.03	56.84	17.74
18	0.36	1.04	67.48	-3.69	60.43	17.85
19	0.38	0.98	73.64	-62.52	63.29	17.93
20	0.40	0.97	79.03	-60.86	67.15	18.01
21	0.42	0.93	87.79	-58.89	70.38	18.10
22	0.44	0.91	95.36	-66.58	73.73	18.17
23	0.46	0.88	99.37	-66.09	75.50	18.21
24	0.48	0.88	98.06	-63.51	76.97	18.22
25	0.50	0.85	99.80	-59.57	78.15	18.21
26	0.52	0.82	99.78	-58.95	80.28	18.19
27	0.54	0.78	97.23	-57.54	81.94	18.15
28	0.56	0.76	94.54	-57.66	82.58	18.11
29	0.58	0.76	90.48	-53.23	82.55	18.06
30	0.60	0.74	88.25	-47.82	82.12	18.03
31	0.62	0.74	86.43	-44.00	82.26	18.00
32	0.64	0.73	85.06	-36.80	81.96	17.97
33	0.66	0.72	81.61	-31.51	80.82	17.92
34	0.68	0.74	76.90	-24.92	79.32	17.87
35	0.70	0.74	73.71	-26.77	77.36	17.84
36	0.72	0.77	73.43	-19.20	75.83	17.83
37	0.74	0.79	73.37	-12.80	74.65	17.83
38	0.76	0.79	73.12	-17.66	73.14	17.83
39	0.78	0.83	71.31	-24.74	71.44	17.81
40	0.80	0.85	66.89	-30.46	69.79	17.77
41	0.82	0.84	65.01	-27.38	68.68	17.72
42	0.84	0.84	62.74	-27.51	68.28	17.70
43	0.86	0.85	63.03	-21.60	67.16	17.69
44	0.88	0.89	63.42	-13.66	66.33	17.73
45	0.90	0.91	66.22	-8.25	65.52	17.77
46	0.92	0.93	68.78	-6.71	63.72	17.83
47	0.94	1.04	69.33	-6.46	61.66	17.87
48	0.97	1.08	70.10	-2.77	59.46	17.91

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
49	0.98	1.11	71.70	-5.42	58.59	17.94
50	1.01	1.14	73.94	-4.80	57.85	17.99
51	1.02	1.18	76.47	0.92	56.39	18.05
52	1.04	1.29	79.84	9.35	54.51	18.12
53	1.06	1.37	82.30	10.46	52.95	18.18
54	1.08	1.41	84.71	-4.55	52.57	18.22
55	1.10	1.40	87.46	-18.40	53.35	18.27
56	1.13	1.38	93.13	-19.26	54.50	18.32
57	1.14	1.38	96.56	-8.92	55.43	18.37
58	1.16	1.39	100.02	-3.63	56.18	18.42
59	1.19	1.39	105.75	-1.35	57.22	18.46
60	1.20	1.36	109.24	-1.97	58.26	18.50
61	1.22	1.36	111.10	-1.97	59.32	18.51
62	1.24	1.32	111.42	-9.17	60.17	18.52
63	1.26	1.29	111.38	-4.98	61.36	18.50
64	1.28	1.25	110.10	1.72	62.33	18.48
65	1.30	1.22	109.33	11.02	63.30	18.46
66	1.32	1.19	108.49	10.03	63.98	18.45
67	1.34	1.17	107.11	14.09	64.34	18.43
68	1.36	1.17	105.92	19.14	64.13	18.42
69	1.38	1.19	105.09	33.17	63.52	18.40
70	1.40	1.19	101.97	35.57	62.45	18.36
71	1.42	1.20	95.24	29.42	61.41	18.31
72	1.44	1.19	90.91	27.45	60.58	18.25
73	1.46	1.18	88.76	30.89	60.73	18.22
74	1.48	1.14	88.63	35.57	61.22	18.20
75	1.50	1.12	87.16	35.14	61.82	18.17
76	1.52	1.11	85.26	34.77	61.70	18.15
77	1.54	1.13	84.36	39.82	61.41	18.14
78	1.56	1.12	83.30	43.63	60.59	18.13
79	1.58	1.16	82.92	45.29	59.83	18.12
80	1.60	1.17	81.37	46.46	58.90	18.11
81	1.62	1.18	80.15	44.18	58.77	18.10
82	1.64	1.15	80.34	44.31	59.33	18.09
83	1.66	1.12	80.92	43.88	60.75	18.08
84	1.68	1.07	80.72	41.48	62.42	18.06
85	1.70	1.02	79.22	39.75	64.12	18.02
86	1.72	0.97	75.91	50.89	65.36	17.96
87	1.74	0.93	72.06	58.58	66.51	17.90
88	1.76	0.89	70.20	64.74	66.63	17.83
89	1.78	0.89	65.40	75.26	66.28	17.77
90	1.80	0.89	62.99	82.22	65.11	17.72
91	1.82	0.90	60.97	93.23	64.80	17.67
92	1.84	0.86	58.40	89.11	64.66	17.61
93	1.86	0.84	53.98	76.62	65.85	17.51
94	1.88	0.76	50.04	58.52	67.10	17.38
95	1.90	0.71	44.04	41.23	68.94	17.26
96	1.92	0.68	43.08	67.94	70.79	17.16

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
97	1.94	0.62	40.97	67.82	73.44	17.07
98	1.96	0.55	37.41	74.89	77.39	16.94
99	1.98	0.48	34.14	94.95	80.77	16.79
100	2.01	0.45	31.00	99.69	81.53	16.63
101	2.02	0.45	25.62	106.28	78.42	16.43
102	2.04	0.46	19.98	108.18	72.75	16.16
103	2.06	0.47	14.59	108.92	67.50	15.84
104	2.08	0.45	10.94	110.09	63.16	15.52
105	2.10	0.45	9.18	111.57	60.13	15.25
106	2.12	0.45	7.48	114.03	56.91	15.09
107	2.14	0.49	7.16	116.55	53.94	14.99
108	2.16	0.51	6.90	119.08	51.15	14.97
109	2.18	0.54	6.65	120.92	44.60	14.99
110	2.21	0.77	6.45	127.69	36.97	15.03
111	2.22	0.97	6.13	132.98	30.63	15.08
112	2.24	1.09	6.10	124.86	28.65	15.31
113	2.26	1.17	9.69	111.32	30.28	15.81
114	2.28	1.23	17.06	46.15	33.55	16.36
115	2.30	1.29	25.49	49.35	36.81	16.81
116	2.32	1.34	34.01	48.74	39.73	17.16
117	2.34	1.35	43.01	51.51	42.96	17.48
118	2.36	1.37	56.98	63.02	46.19	17.74
119	2.38	1.38	68.32	65.23	49.01	17.95
120	2.40	1.37	76.01	55.69	50.87	18.07
121	2.42	1.38	79.28	53.66	52.84	18.14
122	2.44	1.31	83.92	50.77	54.58	18.18
123	2.46	1.27	84.98	55.63	56.53	18.19
124	2.48	1.24	84.97	60.86	57.20	18.17
125	2.50	1.23	81.86	58.15	56.87	18.14
126	2.52	1.25	78.34	60.68	56.01	18.11
127	2.54	1.27	78.59	56.18	55.20	18.10
128	2.56	1.28	78.07	52.43	54.70	18.10
129	2.58	1.29	77.33	54.65	54.29	18.09
130	2.60	1.29	76.53	79.02	53.54	18.07
131	2.62	1.32	73.87	61.05	53.27	18.06
132	2.64	1.31	75.40	49.17	53.50	18.07
133	2.66	1.28	77.86	58.46	54.49	18.09
134	2.68	1.27	79.04	77.60	54.73	18.11
135	2.70	1.31	79.23	86.89	54.25	18.12
136	2.72	1.33	78.88	94.15	52.86	18.12
137	2.74	1.38	76.66	99.45	52.13	18.12
138	2.76	1.37	78.00	96.37	51.67	18.12
139	2.78	1.37	78.13	86.34	51.42	18.11
140	2.80	1.38	73.51	91.32	50.64	18.06
141	2.82	1.39	69.69	71.51	50.46	17.99
142	2.84	1.30	66.49	44.06	52.46	17.94
143	2.86	1.14	67.80	42.28	56.58	17.90
144	2.88	1.02	69.65	47.82	61.74	17.89

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
145	2.92	0.95	72.35	45.72	66.25	17.90
146	2.92	0.89	74.34	77.85	69.51	17.90
147	2.94	0.85	74.02	96.86	71.87	17.87
148	2.97	0.80	71.10	120.68	74.30	17.80
149	2.99	0.72	66.13	110.77	75.55	17.68
150	3.00	0.70	56.71	128.92	73.44	17.54
151	3.02	0.77	49.02	145.35	65.20	17.34
152	3.05	0.90	35.63	152.43	57.10	17.13
153	3.06	0.92	29.06	145.54	50.88	16.85
154	3.08	0.90	23.64	126.52	49.32	16.70
155	3.10	0.88	25.21	100.62	48.50	16.73
156	3.12	1.00	29.89	121.54	47.32	16.88
157	3.14	1.11	32.42	145.29	46.11	17.03
158	3.16	1.12	34.98	142.40	45.66	17.14
159	3.18	1.15	37.89	134.95	46.68	17.24
160	3.20	1.15	41.83	104.18	48.04	17.33
161	3.22	1.12	44.65	101.35	50.40	17.41
162	3.24	1.06	47.70	88.18	52.67	17.45
163	3.26	1.03	48.24	105.29	54.97	17.50
164	3.28	1.02	52.38	84.86	55.70	17.55
165	3.30	1.06	54.20	102.71	55.62	17.61
166	3.32	1.11	55.77	98.40	54.91	17.65
167	3.34	1.12	56.54	79.88	53.60	17.66
168	3.36	1.18	54.26	71.08	51.95	17.66
169	3.38	1.24	53.91	88.25	49.95	17.66
170	3.40	1.27	53.97	88.74	48.56	17.69
171	3.42	1.34	56.56	91.20	47.80	17.73
172	3.44	1.35	57.59	91.69	47.73	17.78
173	3.46	1.34	59.99	90.71	48.91	17.81
174	3.49	1.28	62.90	86.40	50.80	17.84
175	3.50	1.24	64.37	57.17	51.99	17.86
176	3.52	1.27	63.44	65.60	52.67	17.88
177	3.54	1.26	67.38	67.20	53.40	17.93
178	3.56	1.24	72.44	71.45	55.02	17.99
179	3.58	1.22	75.29	63.57	56.37	18.03
180	3.60	1.20	75.71	80.49	56.99	18.03
181	3.62	1.19	73.97	79.51	56.73	18.02
182	3.64	1.22	73.88	87.20	55.71	18.01
183	3.66	1.26	72.34	96.25	53.60	17.98
184	3.68	1.32	65.61	87.02	51.27	17.93
185	3.70	1.35	62.02	93.78	49.44	17.87
186	3.72	1.36	61.95	96.12	48.97	17.86
187	3.74	1.34	62.62	103.26	49.35	17.86
188	3.76	1.32	63.32	103.63	49.86	17.87
189	3.78	1.32	63.71	104.00	50.30	17.88
190	3.80	1.32	65.11	104.62	51.22	17.92
191	3.82	1.29	69.79	104.86	52.91	17.97
192	3.84	1.24	73.67	104.86	55.23	18.01

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
193	3.86	1.19	75.27	105.17	56.98	18.01
194	3.88	1.15	72.50	145.17	57.55	18.00
195	3.90	1.18	71.99	130.46	57.17	17.96
196	3.92	1.17	69.33	131.82	56.79	17.94
197	3.94	1.15	68.31	132.92	57.19	17.89
198	3.96	1.09	64.33	125.48	58.01	17.83
199	3.98	1.05	62.47	125.72	59.31	17.79
200	4.00	1.02	63.24	126.58	60.55	17.78
201	4.02	1.00	64.33	126.65	62.58	17.78
202	4.05	0.94	65.03	124.92	64.44	17.78
203	4.06	0.91	65.06	125.11	66.37	17.76
204	4.08	0.89	64.42	124.80	66.76	17.75
205	4.10	0.91	63.39	125.91	66.38	17.73
206	4.12	0.92	61.95	128.92	64.81	17.71
207	4.14	0.95	60.41	130.89	63.31	17.70
208	4.16	0.97	59.35	131.88	61.73	17.68
209	4.18	0.99	58.07	132.31	60.37	17.67
210	4.20	1.02	57.14	133.11	59.32	17.66
211	4.22	1.02	57.07	135.75	58.58	17.66
212	4.24	1.03	57.01	136.18	58.72	17.67
213	4.26	1.02	58.77	136.49	59.22	17.69
214	4.28	1.01	60.40	137.17	59.35	17.73
215	4.30	1.06	62.19	139.45	58.62	17.77
216	4.32	1.11	62.99	141.66	57.39	17.80
217	4.34	1.13	63.03	142.65	56.68	17.80
218	4.36	1.12	62.13	142.71	56.69	17.79
219	4.38	1.10	61.71	143.69	56.44	17.76
220	4.40	1.11	58.09	143.82	56.21	17.72
221	4.42	1.09	56.33	143.32	55.78	17.66
222	4.44	1.07	54.18	142.95	56.13	17.62
223	4.46	1.03	52.45	141.72	57.15	17.58
224	4.48	0.99	52.86	140.80	58.26	17.55
225	4.50	0.97	51.87	139.26	60.16	17.54
226	4.52	0.91	52.70	138.09	62.39	17.54
227	4.54	0.86	54.81	137.97	65.86	17.52
228	4.56	0.79	53.79	137.48	68.95	17.49
229	4.58	0.74	50.97	136.74	72.00	17.41
230	4.60	0.68	47.95	136.06	74.27	17.31
231	4.62	0.64	45.29	135.82	76.75	17.23
232	4.64	0.61	43.34	135.75	78.87	17.11
233	4.66	0.55	37.86	135.51	80.15	16.98
234	4.68	0.54	34.17	135.51	80.14	16.82
235	4.70	0.52	29.46	135.38	78.88	16.68
236	4.72	0.51	26.93	135.94	76.13	16.54
237	4.74	0.54	23.54	136.74	72.97	16.39
238	4.76	0.54	19.95	137.11	68.44	16.24
239	4.78	0.57	17.64	137.35	65.01	16.11
240	4.80	0.58	16.46	137.54	62.44	16.04

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
241	4.82	0.58	16.14	137.60	61.25	15.99
242	4.84	0.59	15.62	137.60	61.65	15.97
243	4.86	0.56	15.82	137.78	59.98	16.01
244	4.88	0.66	16.97	123.08	59.79	16.11
245	4.90	0.65	19.31	126.65	58.23	16.19
246	4.92	0.66	18.67	130.58	58.42	16.21
247	4.94	0.67	18.03	133.85	57.98	16.17
248	4.96	0.64	17.35	131.63	58.23	16.14
249	4.98	0.64	17.54	132.74	58.99	16.13
250	5.00	0.63	17.87	138.03	57.77	16.08
251	5.02	0.66	15.14	142.28	55.29	15.99
252	5.04	0.68	13.16	146.71	51.56	15.90
253	5.06	0.74	13.57	154.15	48.82	15.89
254	5.08	0.79	14.12	160.98	46.94	15.96
255	5.10	0.82	14.69	163.38	45.47	16.00
256	5.12	0.86	14.60	165.17	43.89	16.02
257	5.14	0.91	14.12	166.89	42.31	16.03
258	5.16	0.95	14.37	168.18	41.19	16.09
259	5.19	1.00	16.30	169.97	41.09	16.15
260	5.20	0.97	16.14	169.97	41.72	16.24
261	5.22	0.97	18.03	170.34	42.90	16.33
262	5.24	0.98	20.69	172.98	43.18	16.41
263	5.26	1.02	19.69	173.60	43.34	16.51
264	5.28	1.05	22.70	175.20	43.65	16.62
265	5.30	1.07	26.58	179.75	43.79	16.73
266	5.32	1.12	25.88	180.86	43.62	16.83
267	5.34	1.16	28.18	183.88	43.42	16.92
268	5.36	1.18	32.06	196.06	43.11	17.01
269	5.38	1.25	32.16	197.97	42.82	17.10
270	5.40	1.30	34.62	199.08	42.67	17.19
271	5.42	1.31	38.82	201.11	42.76	17.28
272	5.44	1.36	39.49	198.58	42.82	17.37
273	5.46	1.42	43.11	196.86	42.63	17.46
274	5.48	1.44	46.32	196.06	42.94	17.57
275	5.50	1.49	51.35	193.23	43.87	17.68
276	5.52	1.48	56.92	185.35	45.05	17.78
277	5.54	1.47	60.44	175.45	46.89	17.89
278	5.56	1.45	68.16	167.45	48.86	17.99
279	5.58	1.44	75.50	164.25	51.84	18.10
280	5.60	1.33	82.39	158.65	54.76	18.17
281	5.62	1.30	86.17	151.26	58.67	18.23
282	5.64	1.22	93.15	147.69	62.21	18.27
283	5.66	1.13	95.42	148.00	65.79	18.26
284	5.68	1.06	91.13	145.91	67.96	18.20
285	5.70	1.02	83.69	146.03	68.27	18.10
286	5.72	1.00	74.97	148.25	67.17	17.99
287	5.74	1.01	69.46	154.58	64.62	17.88
288	5.76	1.05	62.67	159.82	60.56	17.76

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
289	5.78	1.12	52.32	161.11	56.72	17.63
290	5.80	1.12	47.99	161.60	53.90	17.52
291	5.82	1.13	46.61	162.71	52.64	17.47
292	5.84	1.16	45.52	164.92	50.82	17.42
293	5.86	1.22	41.17	165.17	48.14	17.42
294	5.89	1.37	43.60	161.78	46.57	17.49
295	5.90	1.41	50.59	160.43	46.39	17.63
296	5.92	1.42	56.13	159.69	47.67	17.75
297	5.94	1.41	59.98	161.66	49.18	17.83
298	5.96	1.37	63.34	160.18	50.94	17.90
299	5.98	1.35	67.31	156.55	53.32	17.97
300	6.01	1.30	74.59	154.09	55.05	18.04
301	6.02	1.33	77.63	153.17	57.09	18.11
302	6.04	1.27	81.54	155.02	58.28	18.15
303	6.06	1.27	84.68	157.23	59.88	18.19
304	6.08	1.26	86.76	156.62	61.02	18.22
305	6.10	1.23	88.52	156.25	62.65	18.22
306	6.12	1.17	87.91	156.31	63.70	18.20
307	6.14	1.17	83.81	154.22	64.17	18.15
308	6.16	1.15	79.86	152.80	63.84	18.09
309	6.18	1.13	76.82	151.94	64.36	18.05
310	6.21	1.09	76.46	152.37	65.23	18.03
311	6.22	1.08	77.04	152.74	66.49	18.02
312	6.25	1.05	77.17	153.91	67.52	18.02
313	6.26	1.04	77.81	155.14	68.30	18.02
314	6.28	1.03	78.25	156.49	68.82	18.02
315	6.30	1.03	78.32	157.42	68.32	18.01
316	6.32	1.06	75.05	158.40	66.80	17.98
317	6.34	1.09	70.72	159.45	64.82	17.93
318	6.36	1.09	66.65	160.86	63.33	17.87
319	6.38	1.08	63.66	160.80	62.18	17.81
320	6.40	1.11	61.04	160.31	61.04	17.78
321	6.42	1.13	60.62	159.75	60.51	17.77
322	6.44	1.11	61.65	159.32	60.47	17.79
323	6.46	1.13	63.53	160.12	60.77	17.81
324	6.48	1.13	63.60	160.49	60.50	17.82
325	6.50	1.15	62.86	159.38	60.25	17.83
326	6.52	1.17	64.49	159.45	59.62	17.85
327	6.54	1.20	65.58	159.63	58.67	17.88
328	6.56	1.26	66.51	160.12	57.60	17.91
329	6.58	1.28	67.18	159.82	56.92	17.94
330	6.60	1.29	68.78	159.08	56.83	17.97
331	6.62	1.31	71.57	158.40	57.25	18.01
332	6.64	1.31	74.74	157.17	57.99	18.06
333	6.66	1.30	77.46	156.74	59.13	18.10
334	6.68	1.29	80.83	157.66	59.72	18.14
335	6.70	1.32	82.59	158.22	59.86	18.18
336	6.72	1.34	84.16	157.97	59.64	18.21

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
337	6.74	1.35	86.27	159.14	59.84	18.23
338	6.76	1.34	86.91	160.12	59.87	18.24
339	6.78	1.36	85.63	160.68	59.12	18.23
340	6.80	1.40	82.68	160.49	57.88	18.22
341	6.82	1.43	82.72	160.06	57.22	18.23
342	6.84	1.43	86.43	159.69	57.16	18.28
343	6.86	1.49	93.44	156.68	57.26	18.35
344	6.88	1.53	96.90	157.78	57.80	18.42
345	6.90	1.50	102.67	158.46	58.61	18.47
346	6.92	1.50	105.01	158.34	60.39	18.50
347	6.94	1.43	107.64	157.48	62.43	18.51
348	6.96	1.35	108.15	156.92	64.49	18.49
349	6.98	1.32	105.20	157.72	65.54	18.46
350	7.00	1.31	100.91	158.83	65.07	18.40
351	7.02	1.32	94.75	159.02	64.06	18.34
352	7.04	1.31	89.24	159.57	62.27	18.27
353	7.06	1.36	83.92	159.26	60.57	18.22
354	7.08	1.38	82.03	159.45	58.57	18.20
355	7.10	1.45	81.93	159.88	57.23	18.20
356	7.12	1.47	81.03	160.31	56.02	18.20
357	7.14	1.50	80.61	159.20	55.98	18.21
358	7.16	1.47	83.37	158.09	56.75	18.23
359	7.18	1.44	85.77	157.85	58.07	18.26
360	7.20	1.43	88.23	159.51	58.81	18.28
361	7.22	1.45	89.55	161.05	58.68	18.31
362	7.24	1.49	91.24	161.78	58.11	18.34
363	7.26	1.53	92.91	161.91	57.88	18.37
364	7.28	1.52	95.95	161.97	58.00	18.41
365	7.30	1.55	100.09	162.22	57.93	18.45
366	7.32	1.60	101.43	163.02	56.61	18.49
367	7.34	1.71	100.43	164.00	54.54	18.50
368	7.36	1.80	99.66	164.55	52.53	18.51
369	7.38	1.85	99.53	164.86	51.31	18.52
370	7.40	1.87	99.31	164.92	51.02	18.53
371	7.42	1.85	100.52	164.80	51.39	18.54
372	7.44	1.83	102.19	164.55	51.91	18.55
373	7.46	1.85	104.69	163.26	52.62	18.60
374	7.48	1.86	112.89	162.77	53.30	18.65
375	7.50	1.86	116.83	162.77	53.93	18.71
376	7.52	1.90	120.61	162.34	54.07	18.74
377	7.54	1.92	121.95	162.89	53.90	18.77
378	7.56	1.93	123.14	162.28	53.88	18.78
379	7.58	1.92	122.78	161.29	54.03	18.78
380	7.60	1.90	121.82	160.37	55.03	18.77
381	7.62	1.81	123.96	158.65	56.51	18.77
382	7.64	1.77	127.39	156.98	58.05	18.78
383	7.66	1.76	127.26	153.78	59.15	18.79
384	7.68	1.72	127.97	152.06	60.17	18.79

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
385	7.70	1.67	130.17	150.34	61.48	18.79
386	7.72	1.64	131.20	149.05	62.82	18.80
387	7.74	1.60	132.57	147.94	63.68	18.79
388	7.76	1.60	131.29	147.51	64.26	18.79
389	7.78	1.59	131.67	146.83	64.11	18.78
390	7.80	1.61	130.52	146.58	64.02	18.77
391	7.82	1.59	127.79	145.60	63.10	18.74
392	7.84	1.63	120.81	144.18	62.27	18.72
393	7.86	1.66	122.28	143.32	61.33	18.71
394	7.88	1.67	123.08	142.52	60.80	18.72
395	7.90	1.70	122.09	141.72	60.52	18.72
396	7.92	1.69	121.10	140.98	59.96	18.71
397	7.94	1.72	119.59	140.18	59.73	18.71
398	7.96	1.72	119.46	139.82	59.26	18.70
399	7.98	1.73	118.37	138.58	59.19	18.69
400	8.00	1.71	116.26	137.23	59.59	18.68
401	8.02	1.66	116.32	136.00	60.88	18.65
402	8.04	1.57	114.75	134.58	62.91	18.62
403	8.07	1.48	112.83	133.54	64.78	18.58
404	8.08	1.44	109.04	132.80	65.91	18.52
405	8.10	1.40	102.44	132.00	66.62	18.47
406	8.12	1.36	100.78	131.38	67.45	18.42
407	8.14	1.32	98.31	131.63	68.04	18.38
408	8.16	1.31	94.91	133.35	67.73	18.34
409	8.18	1.34	92.51	133.91	66.90	18.32
410	8.20	1.34	91.26	133.97	65.92	18.30
411	8.22	1.36	89.43	133.91	65.63	18.28
412	8.24	1.34	88.53	134.15	65.00	18.27
413	8.26	1.38	87.66	135.08	63.75	18.26
414	8.28	1.45	86.13	136.12	61.78	18.27
415	8.30	1.50	86.03	136.55	60.60	18.28
416	8.32	1.49	87.79	136.74	59.80	18.29
417	8.34	1.54	86.83	137.29	59.66	18.30
418	8.36	1.54	88.59	137.54	59.04	18.32
419	8.38	1.57	89.07	137.42	59.49	18.34
420	8.40	1.54	92.40	137.17	60.37	18.38
421	8.42	1.53	97.50	136.98	62.13	18.42
422	8.44	1.50	102.30	137.11	63.24	18.47
423	8.47	1.53	105.80	138.15	63.58	18.52
424	8.48	1.57	108.62	138.34	63.09	18.55
425	8.50	1.60	109.80	138.46	62.24	18.57
426	8.52	1.64	108.74	138.58	61.76	18.58
427	8.54	1.63	109.32	138.34	62.00	18.58
428	8.56	1.58	110.18	138.15	62.40	18.58
429	8.58	1.61	109.42	138.34	62.80	18.58
430	8.60	1.61	110.41	138.28	63.09	18.60
431	8.62	1.59	115.73	138.15	63.81	18.63
432	8.64	1.60	118.58	138.09	64.60	18.65

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
433	8.66	1.58	118.07	137.72	65.34	18.66
434	8.68	1.54	117.94	137.60	66.01	18.63
435	8.70	1.51	113.64	138.15	66.49	18.60
436	8.72	1.49	109.38	137.97	66.43	18.54
437	8.74	1.46	102.55	138.03	65.89	18.47
438	8.76	1.46	96.21	138.15	65.43	18.40
439	8.78	1.43	93.07	138.46	63.86	18.34
440	8.80	1.49	85.73	139.08	61.36	18.27
441	8.82	1.57	77.91	139.45	57.21	18.20
442	8.84	1.70	73.90	140.68	54.46	18.17
443	8.86	1.71	75.50	140.80	52.86	18.19
444	8.88	1.78	78.96	140.74	52.81	18.23
445	8.90	1.79	81.97	140.68	52.65	18.29
446	8.92	1.83	84.60	140.49	53.18	18.35
447	8.94	1.83	91.91	140.00	54.14	18.42
448	8.96	1.81	97.06	140.00	55.79	18.49
449	8.98	1.78	102.86	140.18	57.45	18.54
450	9.00	1.76	107.00	140.06	59.51	18.57
451	9.02	1.66	108.31	140.06	61.07	18.58
452	9.04	1.65	108.34	140.43	62.24	18.57
453	9.06	1.63	106.67	140.25	62.76	18.55
454	9.09	1.59	105.23	140.06	63.97	18.50
455	9.10	1.46	96.83	138.95	66.47	18.41
456	9.13	1.31	91.74	138.28	69.22	18.28
457	9.14	1.22	82.09	137.78	71.85	18.17
458	9.16	1.15	78.02	137.78	72.87	18.07
459	9.18	1.13	73.89	139.02	72.90	17.99
460	9.20	1.14	68.02	140.49	71.08	17.90
461	9.22	1.16	61.71	142.58	67.86	17.79
462	9.24	1.20	53.51	145.66	64.15	17.66
463	9.26	1.23	47.29	147.14	60.70	17.53
464	9.28	1.25	43.22	147.51	58.51	17.41
465	9.30	1.23	38.77	147.20	57.51	17.32
466	9.32	1.21	37.97	146.95	58.83	17.26
467	9.34	1.10	38.90	146.46	61.08	17.24
468	9.36	1.06	38.48	146.28	63.85	17.22
469	9.38	1.03	38.26	146.15	65.14	17.21
470	9.40	1.02	38.10	146.34	65.16	17.18
471	9.42	1.05	36.46	147.45	63.18	17.14
472	9.44	1.10	33.10	147.88	59.57	17.07
473	9.47	1.18	30.63	148.62	56.30	17.04
474	9.48	1.23	31.53	149.60	52.35	17.04
475	9.50	1.41	31.25	153.11	48.40	17.09
476	9.52	1.58	31.18	155.51	43.35	17.09
477	9.54	1.76	27.69	156.06	40.94	17.18
478	9.56	1.84	35.86	156.55	40.79	17.35
479	9.58	1.88	45.00	156.74	42.86	17.63
480	9.60	1.94	55.99	157.35	44.98	17.87

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
481	9.62	1.97	66.15	158.22	46.66	18.08
482	9.64	2.04	76.91	159.02	48.00	18.25
483	9.66	2.09	85.47	160.06	49.15	18.41
484	9.68	2.14	97.93	163.51	49.71	18.51
485	9.70	2.19	99.34	164.18	49.76	18.59
486	9.72	2.25	102.03	164.68	49.44	18.64
487	9.74	2.30	107.96	164.92	50.20	18.72
488	9.76	2.26	120.36	164.62	52.30	18.80
489	9.78	2.15	129.49	164.00	55.51	18.86
490	9.80	2.00	132.05	162.89	59.13	18.85
491	9.82	1.81	127.81	162.03	63.71	18.81
492	9.84	1.59	128.81	159.02	69.09	18.74
493	9.86	1.39	123.42	157.35	75.34	18.65
494	9.88	1.21	113.81	156.12	80.67	18.52
495	9.91	1.10	104.16	155.38	85.09	18.37
496	9.92	1.00	92.37	155.75	87.78	18.23
497	9.94	0.95	85.45	156.92	88.39	18.07
498	9.96	0.93	71.96	158.58	86.76	17.90
499	9.98	0.91	59.17	159.20	82.74	17.66
500	10.00	0.92	46.16	159.45	78.07	17.42
501	10.02	0.93	38.28	159.75	72.99	17.18
502	10.04	0.95	31.91	160.37	68.25	16.95
503	10.06	0.96	24.41	160.80	64.70	16.74
504	10.08	0.94	22.55	160.37	62.09	16.58
505	10.10	0.96	21.40	160.37	59.32	16.51
506	10.12	1.05	19.51	161.78	55.53	16.46
507	10.14	1.13	18.77	162.58	48.82	16.47
508	10.16	1.45	19.19	164.62	41.23	16.50
509	10.18	1.82	17.71	166.40	36.14	16.64
510	10.20	1.96	22.17	165.60	35.86	16.87
511	10.22	1.84	30.92	163.32	39.62	17.13
512	10.24	1.66	36.72	160.80	44.93	17.34
513	10.26	1.58	42.39	160.98	45.59	17.38
514	10.28	1.82	34.51	162.46	41.26	17.41
515	10.30	2.28	35.79	165.78	34.56	17.43
516	10.32	2.74	37.49	167.94	30.08	17.48
517	10.34	2.93	34.00	167.08	28.50	17.47
518	10.36	2.68	33.20	163.57	29.80	17.46
519	10.38	2.37	37.59	160.55	33.87	17.41
520	10.40	1.92	34.65	155.57	38.13	17.35
521	10.42	1.80	32.08	156.62	41.56	17.17
522	10.44	1.58	26.54	154.46	44.95	17.08
523	10.46	1.38	30.74	153.11	50.85	17.10
524	10.48	1.24	38.08	153.72	58.09	17.22
525	10.50	1.13	40.55	161.29	63.31	17.27
526	10.52	1.08	38.46	167.08	65.84	17.21
527	10.54	1.04	34.24	169.29	66.82	17.11
528	10.56	0.99	32.76	170.46	67.28	17.00

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
529	10.58	0.97	30.17	172.98	66.49	16.89
530	10.60	0.98	25.55	177.42	63.70	16.73
531	10.62	1.01	21.32	180.86	60.38	16.56
532	10.64	1.02	19.40	184.68	58.51	16.46
533	10.66	1.01	19.50	186.89	57.69	16.42
534	10.68	1.02	19.08	188.31	57.73	16.43
535	10.70	1.03	20.14	190.95	57.20	16.47
536	10.72	1.07	20.94	195.26	55.62	16.51
537	10.74	1.16	20.30	198.40	50.81	16.61
538	10.76	1.47	23.16	203.14	41.64	16.72
539	10.78	2.08	22.00	209.66	34.68	16.86
540	10.80	2.35	23.66	201.54	27.73	16.97
541	10.82	3.12	24.05	205.72	24.69	17.08
542	10.84	3.20	25.84	206.71	23.84	17.21
543	10.86	2.95	30.52	204.37	27.08	17.32
544	10.88	2.37	34.40	195.45	33.15	17.41
545	10.90	1.92	39.23	187.63	41.73	17.46
546	10.92	1.54	43.08	182.46	50.69	17.46
547	10.94	1.28	42.57	190.65	54.02	17.28
548	10.96	1.37	25.36	212.37	51.67	17.07
549	10.98	1.50	24.95	228.12	46.03	16.88
550	11.00	1.59	26.48	229.91	44.33	16.98
551	11.02	1.68	30.58	229.78	44.82	17.15
552	11.04	1.68	36.86	228.06	46.20	17.32
553	11.06	1.67	40.58	226.65	49.70	17.52
554	11.08	1.59	52.05	222.28	53.90	17.71
555	11.10	1.52	61.08	220.18	59.76	17.90
556	11.13	1.41	72.20	217.29	65.37	18.04
557	11.14	1.33	79.83	215.08	71.52	18.14
558	11.16	1.22	87.26	213.29	77.23	18.21
559	11.18	1.14	91.17	211.51	82.97	18.22
560	11.20	1.05	91.13	210.71	87.84	18.21
561	11.22	0.98	90.46	210.89	91.54	18.17
562	11.24	0.95	86.68	212.68	92.84	18.10
563	11.26	0.94	79.27	215.20	90.71	17.99
564	11.28	0.97	66.81	218.40	86.24	17.81
565	11.30	0.97	52.80	219.45	81.47	17.56
566	11.32	0.93	40.66	220.18	76.36	17.29
567	11.34	0.96	32.58	222.71	69.18	16.97
568	11.36	1.06	21.72	227.32	59.94	16.67
569	11.38	1.19	16.78	232.68	50.71	16.36
570	11.40	1.32	13.96	236.92	44.10	16.21
571	11.42	1.48	13.48	241.78	40.06	16.20
572	11.44	1.61	15.27	243.63	39.40	16.42
573	11.46	1.65	21.65	243.08	41.15	16.71
574	11.48	1.62	27.22	241.85	45.12	17.04
575	11.50	1.58	36.67	240.74	48.98	17.28
576	11.52	1.56	42.35	239.38	53.11	17.51

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
577	11.54	1.52	51.73	238.34	57.58	17.73
578	11.56	1.47	65.67	237.72	62.13	17.92
579	11.58	1.44	73.01	237.66	66.12	18.08
580	11.60	1.43	81.76	237.72	68.26	18.18
581	11.62	1.44	85.06	237.78	69.66	18.26
582	11.64	1.45	90.57	237.60	70.60	18.30
583	11.66	1.42	91.59	237.42	71.44	18.31
584	11.68	1.39	87.52	237.05	71.89	18.27
585	11.70	1.38	84.00	236.74	71.77	18.22
586	11.72	1.35	79.67	236.49	71.34	18.16
587	11.74	1.35	76.24	236.18	71.20	18.11
588	11.76	1.33	74.54	235.57	70.86	18.08
589	11.78	1.34	73.58	235.75	70.35	18.07
590	11.80	1.38	73.85	231.82	69.13	18.08
591	11.82	1.44	75.93	232.43	67.99	18.11
592	11.84	1.46	76.22	233.05	66.79	18.13
593	11.86	1.50	76.64	233.78	65.64	18.15
594	11.88	1.55	76.76	234.03	64.21	18.16
595	11.90	1.60	76.25	233.91	63.22	18.17
596	11.92	1.61	76.96	233.60	62.87	18.18
597	11.94	1.60	78.11	233.23	63.18	18.19
598	11.96	1.59	78.97	232.92	63.57	18.20
599	11.98	1.59	79.04	232.86	63.66	18.20
600	12.00	1.60	79.10	233.17	63.45	18.21
601	12.02	1.63	80.32	233.17	63.17	18.23
602	12.04	1.64	81.28	232.80	62.65	18.25
603	12.06	1.69	83.04	233.11	61.77	18.28
604	12.08	1.75	83.74	233.66	60.75	18.33
605	12.10	1.82	88.87	234.58	60.17	18.40
606	12.12	1.88	96.33	235.38	60.37	18.49
607	12.14	1.91	104.24	235.38	60.95	18.59
608	12.16	1.95	113.11	236.18	61.94	18.68
609	12.18	1.94	119.78	236.06	63.12	18.76
610	12.21	1.93	127.27	236.12	64.34	18.82
611	12.22	1.94	132.94	236.06	65.44	18.87
612	12.24	1.93	138.16	235.38	66.54	18.91
613	12.26	1.90	142.29	235.20	67.31	18.93
614	12.28	1.90	139.92	235.38	67.76	18.93
615	12.30	1.89	139.18	235.14	67.63	18.91
616	12.32	1.88	135.75	235.38	67.27	18.89
617	12.34	1.90	131.61	236.37	66.37	18.86
618	12.36	1.94	129.59	236.74	65.15	18.85
619	12.38	1.99	128.98	237.23	64.09	18.85
620	12.40	2.02	129.53	237.85	63.36	18.86
621	12.42	2.03	129.59	237.91	63.72	18.85
622	12.44	1.94	127.72	236.98	64.77	18.84
623	12.46	1.89	128.04	236.49	65.51	18.82
624	12.48	1.92	125.09	237.35	64.71	18.80

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
625	12.50	2.00	121.50	239.02	62.95	18.78
626	12.52	2.04	117.84	240.74	61.56	18.75
627	12.54	2.03	114.45	240.74	61.33	18.73
628	12.56	1.98	113.84	238.71	62.55	18.72
629	12.58	1.89	117.78	236.86	64.64	18.72
630	12.60	1.82	119.83	236.49	66.83	18.73
631	12.62	1.78	120.37	237.23	67.85	18.73
632	12.64	1.79	119.54	237.97	68.45	18.72
633	12.66	1.75	117.93	238.03	68.33	18.70
634	12.68	1.76	115.18	238.46	68.25	18.67
635	12.70	1.76	112.23	237.91	67.65	18.66
636	12.72	1.78	112.00	238.46	66.98	18.64
637	12.74	1.80	109.21	240.74	65.63	18.62
638	12.76	1.86	105.21	241.35	63.50	18.60
639	12.78	1.96	102.51	242.28	60.31	18.57
640	12.80	2.10	96.85	244.18	57.54	18.57
641	12.82	2.18	98.46	245.11	54.99	18.58
642	12.84	2.32	101.37	247.32	53.52	18.63
643	12.86	2.41	104.45	248.80	52.34	18.67
644	12.88	2.45	106.05	249.66	51.91	18.70
645	12.90	2.46	107.59	249.72	51.52	18.72
646	12.92	2.53	108.87	250.09	51.30	18.74
647	12.94	2.54	109.92	249.85	51.75	18.76
648	12.96	2.43	111.78	247.51	53.57	18.76
649	12.99	2.26	113.86	244.06	56.64	18.76
650	13.01	2.12	117.97	241.85	60.84	18.79
651	13.02	1.96	128.67	239.82	66.14	18.84
652	13.04	1.76	137.92	237.78	71.34	18.87
653	13.06	1.68	138.66	236.68	74.25	18.87
654	13.08	1.71	134.78	236.98	73.65	18.85
655	13.10	1.79	131.48	237.48	71.71	18.83
656	13.12	1.82	128.17	238.65	68.44	18.78
657	13.14	1.94	113.91	241.48	64.66	18.70
658	13.16	2.01	100.03	243.32	60.18	18.59
659	13.18	2.10	92.08	245.05	58.07	18.49
660	13.20	2.00	88.46	242.71	58.01	18.44
661	13.22	1.93	90.09	240.98	60.79	18.43
662	13.24	1.77	93.55	239.02	64.01	18.44
663	13.26	1.70	96.56	237.78	67.15	18.45
664	13.28	1.65	96.50	237.29	68.44	18.45
665	13.30	1.66	95.86	237.17	68.66	18.45
666	13.32	1.69	97.30	238.09	68.09	18.45
667	13.34	1.71	95.92	239.02	67.03	18.45
668	13.36	1.75	93.29	239.94	65.67	18.41
669	13.39	1.76	87.33	240.31	64.38	18.37
670	13.40	1.75	83.65	239.82	64.31	18.32
671	13.42	1.69	84.06	239.63	65.04	18.28
672	13.44	1.64	81.28	239.26	65.82	18.24

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
673	13.46	1.62	76.34	238.71	65.54	18.15
674	13.48	1.59	68.04	237.42	67.19	18.10
675	13.51	1.43	73.75	235.45	70.51	18.07
676	13.52	1.33	75.22	234.40	75.30	18.07
677	13.54	1.27	73.94	233.54	78.01	18.04
678	13.56	1.23	70.90	232.31	80.04	18.00
679	13.58	1.18	71.19	231.32	81.34	17.97
680	13.60	1.18	70.87	232.55	81.20	17.94
681	13.62	1.20	65.61	233.11	79.59	17.87
682	13.64	1.20	58.44	233.23	76.37	17.78
683	13.66	1.26	54.47	233.91	73.40	17.70
684	13.68	1.29	52.19	234.09	71.08	17.67
685	13.70	1.31	52.58	234.15	70.81	17.67
686	13.72	1.29	54.95	233.29	72.42	17.70
687	13.74	1.23	57.45	232.12	75.34	17.75
688	13.76	1.19	61.36	231.02	84.24	17.34
689	13.78	0.49	12.10	201.11	87.19	17.34
690	13.80	1.13	59.33	205.05	89.07	17.30
691	13.83	1.10	58.08	204.25	83.72	17.70
692	13.84	1.03	56.35	203.26	86.74	17.64
693	13.86	0.94	53.27	204.18	89.05	17.56
694	13.88	0.95	49.55	204.37	89.74	17.44
695	13.90	0.92	42.47	204.31	89.14	17.31
696	13.92	0.87	38.50	205.23	88.06	17.15
697	13.94	0.88	33.98	205.91	85.60	17.03
698	13.96	0.92	30.71	207.32	80.75	16.89
699	13.98	0.96	25.91	207.45	77.68	16.77
700	14.00	0.92	24.69	207.20	75.51	16.64
701	14.02	0.92	21.81	209.17	73.17	16.51
702	14.04	0.97	18.16	209.85	70.14	16.40
703	14.06	0.98	18.19	209.60	68.88	16.39
704	14.08	0.98	21.17	209.29	70.88	16.49
705	14.10	0.95	23.35	208.98	73.54	16.63
706	14.12	0.96	26.27	210.34	73.49	16.70
707	14.14	1.03	25.31	213.66	70.84	16.74
708	14.16	1.11	24.96	217.54	68.07	16.71
709	14.18	1.08	23.52	217.11	66.57	16.68
710	14.20	1.09	22.55	217.05	66.06	16.63
711	14.22	1.10	22.20	216.86	66.47	16.61
712	14.24	1.04	22.68	216.00	68.31	16.63
713	14.26	1.00	24.03	215.38	71.61	16.67
714	14.28	0.97	25.86	214.65	76.00	16.73
715	14.30	0.89	27.69	213.78	80.01	16.77
716	14.32	0.87	27.82	213.11	84.68	16.77
717	14.34	0.81	28.01	212.62	87.05	16.74
718	14.36	0.79	25.93	212.49	89.35	16.66
719	14.38	0.76	23.52	211.94	90.07	16.53
720	14.40	0.73	21.06	212.00	90.15	16.40

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
721	14.42	0.73	18.88	212.49	87.44	16.25
722	14.44	0.76	15.58	213.48	82.50	16.06
723	14.46	0.78	12.28	213.97	77.99	15.87
724	14.48	0.77	11.35	214.03	75.73	15.71
725	14.50	0.76	10.59	213.97	74.87	15.62
726	14.52	0.77	9.82	214.09	72.62	15.55
727	14.54	0.82	9.14	214.34	70.68	15.55
728	14.56	0.83	10.52	214.46	69.99	15.62
729	14.58	0.83	11.39	214.40	71.39	15.73
730	14.60	0.82	12.06	214.34	72.48	15.76
731	14.62	0.81	11.58	214.15	73.45	15.76
732	14.64	0.80	11.52	214.34	72.13	15.74
733	14.66	0.86	11.33	214.95	70.56	15.78
734	14.68	0.89	12.36	215.88	68.14	15.82
735	14.70	0.92	12.23	216.12	66.92	15.90
736	14.72	0.96	13.45	216.43	66.03	15.96
737	14.74	0.97	14.09	216.68	66.20	16.05
738	14.76	0.97	15.21	216.55	69.97	16.12
739	14.78	0.84	17.03	217.35	71.91	16.27
740	14.81	0.98	20.23	218.89	74.67	16.40
741	14.82	0.94	21.77	218.40	74.76	16.52
742	14.84	0.91	22.79	218.15	76.92	16.55
743	14.86	0.91	22.41	219.20	77.18	16.54
744	14.88	0.93	21.38	220.86	74.68	16.49
745	14.90	0.98	19.37	221.66	70.88	16.41
746	14.92	1.03	17.38	222.46	67.66	16.35
747	14.94	1.04	17.76	223.08	65.66	16.34
748	14.96	1.08	18.50	224.06	64.50	16.38
749	14.98	1.12	18.95	224.74	63.97	16.46
750	15.00	1.13	20.90	225.05	64.22	16.55
751	15.02	1.14	22.95	225.35	65.29	16.69
752	15.04	1.18	26.93	225.60	66.46	16.84
753	15.06	1.19	30.03	225.60	67.79	16.96
754	15.08	1.17	31.64	225.23	70.34	17.06
755	15.10	1.13	35.64	224.98	72.62	17.13
756	15.12	1.13	36.76	225.72	74.25	17.18
757	15.14	1.13	36.38	225.91	74.51	17.20
758	15.16	1.13	37.08	226.58	73.89	17.21
759	15.18	1.18	38.01	227.32	72.91	17.26
760	15.20	1.22	39.58	228.00	71.86	17.31
761	15.22	1.24	41.21	228.68	71.30	17.37
762	15.24	1.28	43.55	229.35	71.27	17.45
763	15.27	1.31	47.91	229.60	71.98	17.55
764	15.28	1.31	52.55	229.85	73.19	17.66
765	15.30	1.32	57.33	230.03	74.96	17.76
766	15.32	1.31	61.68	230.15	76.20	17.84
767	15.34	1.33	64.85	230.28	77.15	17.91
768	15.36	1.34	68.02	230.34	77.86	17.97

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
769	15.38	1.34	71.74	230.28	79.00	18.02
770	15.40	1.32	75.07	230.65	80.11	18.07
771	15.42	1.33	77.18	230.83	81.26	18.10
772	15.44	1.30	77.34	230.83	81.72	18.10
773	15.46	1.31	76.73	231.02	81.18	18.10
774	15.48	1.36	75.35	231.88	79.68	18.10
775	15.50	1.39	75.57	232.37	77.99	18.09
776	15.52	1.41	74.23	232.86	76.75	18.08
777	15.54	1.43	72.46	233.11	76.08	18.07
778	15.56	1.42	71.63	233.29	75.31	18.05
779	15.58	1.44	70.63	233.78	73.98	18.03
780	15.60	1.50	67.84	234.58	71.85	18.01
781	15.62	1.55	66.40	235.75	69.50	18.00
782	15.64	1.60	65.95	237.05	67.86	18.01
783	15.66	1.64	67.65	237.48	67.46	18.04
784	15.68	1.63	71.33	237.23	68.61	18.10
785	15.70	1.58	75.65	236.43	70.61	18.15
786	15.72	1.56	78.66	236.31	72.64	18.18
787	15.74	1.53	80.07	236.25	73.84	18.20
788	15.76	1.52	80.10	236.00	76.72	18.15
789	15.78	1.29	72.26	236.43	77.27	18.14
790	15.80	1.49	80.05	238.09	77.64	18.12
791	15.82	1.47	76.59	237.72	75.18	18.14
792	15.84	1.48	72.90	237.85	73.97	18.08
793	15.86	1.50	68.13	238.52	72.07	18.02
794	15.88	1.54	64.86	238.40	70.63	17.98
795	15.90	1.54	64.86	237.66	70.51	17.97
796	15.92	1.51	67.07	237.78	71.41	18.00
797	15.94	1.50	68.99	237.85	72.93	18.03
798	15.96	1.48	72.55	237.66	74.73	18.08
799	15.98	1.44	76.49	237.23	76.34	18.12
800	16.00	1.45	77.73	237.54	77.14	18.14
801	16.02	1.46	77.09	237.66	77.59	18.14
802	16.04	1.41	76.13	237.17	77.57	18.11
803	16.07	1.42	73.50	237.23	77.92	18.09
804	16.08	1.41	72.67	236.98	77.51	18.06
805	16.10	1.41	71.29	237.29	77.07	18.04
806	16.13	1.43	69.59	237.78	76.02	18.03
807	16.14	1.46	69.46	238.28	74.92	18.03
808	16.16	1.49	70.68	238.77	73.88	18.04
809	16.18	1.51	69.97	239.51	73.07	18.06
810	16.20	1.55	71.25	239.88	72.26	18.07
811	16.22	1.57	72.73	240.55	71.58	18.11
812	16.24	1.61	74.36	240.98	71.08	18.14
813	16.26	1.63	76.15	241.42	70.46	18.17
814	16.28	1.67	77.27	242.46	69.02	18.18
815	16.30	1.75	75.38	243.82	66.42	18.19
816	16.32	1.87	74.13	246.52	64.08	18.19

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
817	16.34	1.89	74.29	247.02	63.40	18.20
818	16.36	1.84	76.02	245.91	63.45	18.21
819	16.38	1.88	75.51	246.58	63.32	18.21
820	16.40	1.90	73.68	247.75	62.47	18.19
821	16.43	1.91	72.40	247.32	62.11	18.18
822	16.44	1.91	72.88	245.66	63.15	18.20
823	16.46	1.83	78.42	244.55	64.69	18.24
824	16.48	1.82	81.59	244.12	66.56	18.29
825	16.50	1.81	83.96	244.12	67.44	18.32
826	16.52	1.81	86.62	245.29	68.18	18.36
827	16.54	1.82	89.63	246.09	68.98	18.41
828	16.57	1.82	95.11	247.02	68.27	18.44
829	16.58	1.93	91.62	250.89	68.74	18.45
830	16.60	1.79	92.54	248.55	68.96	18.43
831	16.63	1.77	91.42	248.92	70.21	18.40
832	16.64	1.78	86.97	248.62	70.10	18.36
833	16.66	1.74	83.80	247.94	69.89	18.31
834	16.68	1.72	82.23	247.82	70.32	18.28
835	16.70	1.69	80.98	246.95	71.67	18.26
836	16.72	1.60	81.52	245.78	73.65	18.24
837	16.74	1.55	81.65	245.72	75.85	18.23
838	16.76	1.51	80.65	246.22	80.28	18.09
839	16.79	1.14	61.78	248.00	80.12	18.05
840	16.80	1.51	74.43	252.31	78.99	17.99
841	16.83	1.51	69.53	252.74	74.62	18.05
842	16.84	1.50	66.39	252.68	74.17	17.96
843	16.86	1.43	59.86	252.74	74.66	17.83
844	16.88	1.33	51.40	251.94	75.31	17.67
845	16.90	1.28	46.27	252.25	75.72	17.50
846	16.92	1.23	40.15	251.82	75.52	17.37
847	16.94	1.21	37.68	252.37	74.63	17.24
848	16.96	1.21	33.45	252.92	73.31	17.12
849	16.98	1.20	29.58	253.05	72.31	17.00
850	17.00	1.16	28.01	251.88	72.15	16.90
851	17.03	1.13	26.63	253.85	71.60	16.81
852	17.04	1.16	23.94	254.52	70.07	16.73
853	17.06	1.17	22.05	254.89	68.32	16.62
854	17.08	1.15	20.42	255.57	66.85	16.55
855	17.10	1.18	19.55	256.55	65.75	16.49
856	17.12	1.19	18.82	257.97	64.59	16.44
857	17.14	1.18	17.82	259.38	63.83	16.37
858	17.16	1.17	16.16	259.51	63.65	16.31
859	17.19	1.16	16.54	259.82	64.30	16.29
860	17.20	1.13	16.99	259.94	65.82	16.30
861	17.23	1.10	16.96	260.80	66.65	16.30
862	17.24	1.11	16.64	261.97	66.48	16.27
863	17.26	1.12	15.85	262.15	65.88	16.24
864	17.28	1.11	15.62	262.46	66.13	16.21

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
865	17.31	1.08	15.65	264.80	66.45	16.19
866	17.32	1.09	15.05	266.71	66.69	16.17
867	17.34	1.08	14.86	268.06	66.75	16.15
868	17.36	1.07	15.11	269.60	67.54	16.13
869	17.38	1.03	14.57	268.98	68.54	16.10
870	17.40	1.01	13.90	270.40	69.54	16.04
871	17.42	0.99	13.26	271.75	69.89	15.97
872	17.44	0.98	12.43	272.80	68.76	15.88
873	17.46	1.01	10.95	276.49	66.92	15.78
874	17.48	1.01	10.15	277.11	64.88	15.68
875	17.50	1.01	9.35	278.58	64.56	15.62
876	17.52	0.99	9.42	280.49	64.50	15.59
877	17.54	1.00	9.58	283.94	64.61	15.60
878	17.56	1.02	9.61	285.91	63.49	15.60
879	17.58	1.04	9.04	289.42	62.13	15.57
880	17.60	1.06	8.81	295.08	60.52	15.58
881	17.62	1.11	9.65	302.09	59.32	15.63
882	17.64	1.14	9.97	306.77	57.51	15.70
883	17.66	1.22	10.16	311.32	55.95	15.74
884	17.68	1.25	10.26	313.60	54.83	15.76
885	17.70	1.24	10.23	313.60	55.24	15.78
886	17.72	1.21	10.81	313.60	56.92	15.83
887	17.74	1.16	11.80	315.20	58.57	15.88
888	17.76	1.16	11.77	317.05	58.39	16.11
889	17.78	1.41	17.97	312.98	57.49	16.40
890	17.80	1.48	22.14	303.63	58.52	16.66
891	17.82	1.34	24.22	309.29	61.46	16.75
892	17.84	1.27	23.74	312.06	64.85	16.74
893	17.86	1.24	23.26	317.54	65.74	16.69
894	17.88	1.22	21.24	320.86	65.57	16.60
895	17.90	1.21	19.06	322.77	64.49	16.47
896	17.92	1.20	16.85	325.85	62.21	16.32
897	17.94	1.25	14.09	328.55	59.83	16.16
898	17.96	1.24	12.62	329.05	58.04	16.06
899	17.98	1.25	12.97	330.22	56.89	16.02
900	18.00	1.30	12.59	332.00	56.03	16.02
901	18.02	1.30	12.46	333.97	56.03	16.02
902	18.04	1.24	12.78	330.15	57.83	16.10
903	18.06	1.23	15.57	335.02	58.55	16.16
904	18.08	1.30	14.57	340.86	59.48	16.17
905	18.10	1.19	13.29	336.49	60.63	16.12
906	18.12	1.13	14.41	335.51	63.24	16.10
907	18.14	1.13	14.57	339.82	64.49	16.13

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (m)
q_c:	Measured cone resistance (MPa)
f_s:	Sleeve friction resistance (kPa)
u:	Pore pressure (kPa)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (kN/m^3)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1	0.03	0.51	0.00	0.51	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
2	0.04	0.68	0.00	0.68	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
3	0.07	1.20	0.00	1.20	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
4	0.08	1.37	0.00	1.37	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
5	0.10	1.71	0.00	1.71	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
6	0.12	2.06	0.00	2.06	1.00	0.150	1.43	0.105	1.10	1.00	2.000	Yes
7	0.14	2.41	0.00	2.41	1.00	0.150	1.43	0.105	1.10	1.00	2.000	Yes
8	0.17	2.93	0.00	2.93	1.00	0.150	1.43	0.105	1.10	1.00	2.000	Yes
9	0.18	3.11	0.00	3.11	1.00	0.150	1.43	0.105	1.10	1.00	2.000	Yes
10	0.20	3.45	0.00	3.45	1.00	0.150	1.43	0.105	1.10	1.00	2.000	Yes
11	0.22	3.79	0.00	3.79	1.00	0.150	1.43	0.105	1.10	1.00	2.000	Yes
12	0.24	4.13	0.00	4.13	1.00	0.150	1.43	0.105	1.10	1.00	2.000	Yes
13	0.26	4.48	0.00	4.48	1.00	0.150	1.43	0.105	1.10	1.00	2.000	Yes
14	0.28	4.83	0.00	4.83	1.00	0.150	1.43	0.105	1.10	1.00	2.000	Yes
15	0.30	5.18	0.00	5.18	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
16	0.32	5.53	0.00	5.53	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
17	0.34	5.88	0.00	5.88	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
18	0.36	6.24	0.00	6.24	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
19	0.38	6.60	0.00	6.60	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
20	0.40	6.96	0.00	6.96	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
21	0.42	7.32	0.00	7.32	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
22	0.44	7.68	0.00	7.68	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
23	0.46	8.05	0.00	8.05	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
24	0.48	8.41	0.00	8.41	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
25	0.50	8.78	0.00	8.78	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
26	0.52	9.14	0.00	9.14	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
27	0.54	9.50	0.00	9.50	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
28	0.56	9.86	0.00	9.86	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
29	0.58	10.23	0.00	10.23	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
30	0.60	10.59	0.00	10.59	1.00	0.150	1.43	0.105	1.10	1.00	2.000	No
31	0.62	10.95	0.00	10.95	1.00	0.149	1.43	0.105	1.10	1.00	2.000	No
32	0.64	11.31	0.00	11.31	1.00	0.149	1.43	0.105	1.10	1.00	2.000	No
33	0.66	11.66	0.00	11.66	1.00	0.149	1.43	0.105	1.10	1.00	2.000	No
34	0.68	12.02	0.00	12.02	1.00	0.149	1.43	0.105	1.10	1.00	2.000	No
35	0.70	12.38	0.00	12.38	1.00	0.149	1.43	0.105	1.10	1.00	2.000	No
36	0.72	12.74	0.00	12.74	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
37	0.74	13.09	0.00	13.09	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
38	0.76	13.45	0.00	13.45	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
39	0.78	13.80	0.00	13.80	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
40	0.80	14.16	0.00	14.16	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
41	0.82	14.51	0.00	14.51	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
42	0.84	14.87	0.00	14.87	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
43	0.86	15.22	0.00	15.22	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
44	0.88	15.58	0.00	15.58	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
45	0.90	15.93	0.00	15.93	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
46	0.92	16.29	0.00	16.29	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
47	0.94	16.65	0.00	16.65	1.00	0.149	1.43	0.104	1.10	1.00	2.000	No
48	0.97	17.18	0.00	17.18	0.99	0.149	1.43	0.104	1.10	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
49	0.98	17.36	0.00	17.36	0.99	0.149	1.43	0.104	1.10	1.00	2.000	No
50	1.01	17.90	0.10	17.80	0.99	0.149	1.43	0.105	1.10	1.00	0.124	No
51	1.02	18.08	0.20	17.89	0.99	0.150	1.43	0.105	1.10	1.00	0.125	No
52	1.04	18.45	0.39	18.05	0.99	0.152	1.43	0.106	1.10	1.00	0.126	No
53	1.06	18.81	0.59	18.22	0.99	0.153	1.43	0.107	1.10	1.00	0.126	No
54	1.08	19.17	0.78	18.39	0.99	0.155	1.43	0.108	1.10	1.00	0.128	No
55	1.10	19.54	0.98	18.56	0.99	0.156	1.43	0.109	1.10	1.00	0.129	No
56	1.13	20.09	1.28	18.81	0.99	0.158	1.43	0.111	1.10	1.00	0.131	No
57	1.14	20.27	1.37	18.90	0.99	0.159	1.43	0.111	1.10	1.00	0.131	No
58	1.16	20.64	1.57	19.07	0.99	0.161	1.43	0.112	1.10	1.00	0.132	No
59	1.19	21.19	1.86	19.33	0.99	0.163	1.43	0.114	1.10	1.00	0.134	No
60	1.20	21.38	1.96	19.42	0.99	0.163	1.43	0.114	1.10	1.00	0.135	No
61	1.22	21.75	2.16	19.59	0.99	0.165	1.43	0.115	1.10	1.00	0.136	No
62	1.24	22.12	2.35	19.77	0.99	0.166	1.43	0.116	1.10	1.00	0.137	No
63	1.26	22.49	2.55	19.94	0.99	0.167	1.43	0.117	1.10	1.00	0.138	No
64	1.28	22.86	2.75	20.11	0.99	0.168	1.43	0.118	1.10	1.00	0.139	No
65	1.30	23.23	2.94	20.29	0.99	0.169	1.43	0.119	1.10	1.00	0.140	No
66	1.32	23.60	3.14	20.46	0.99	0.171	1.43	0.119	1.10	1.00	0.142	No
67	1.34	23.97	3.34	20.63	0.99	0.172	1.43	0.120	1.10	1.00	0.143	No
68	1.36	24.33	3.53	20.80	0.99	0.173	1.43	0.121	1.10	1.00	0.144	No
69	1.38	24.70	3.73	20.97	0.99	0.174	1.43	0.122	1.10	1.00	0.144	No
70	1.40	25.07	3.92	21.15	0.99	0.175	1.43	0.123	1.10	1.00	0.145	No
71	1.42	25.44	4.12	21.32	0.99	0.176	1.43	0.123	1.10	1.00	0.146	No
72	1.44	25.80	4.32	21.48	0.99	0.177	1.43	0.124	1.10	1.00	0.147	No
73	1.46	26.17	4.51	21.65	0.99	0.178	1.43	0.125	1.10	1.00	0.148	No
74	1.48	26.53	4.71	21.82	0.99	0.179	1.43	0.126	1.10	1.00	0.149	No
75	1.50	26.89	4.91	21.99	0.99	0.180	1.43	0.126	1.10	1.00	0.150	No
76	1.52	27.26	5.10	22.15	0.99	0.181	1.43	0.127	1.10	1.00	0.151	No
77	1.54	27.62	5.30	22.32	0.99	0.182	1.43	0.128	1.10	1.00	0.152	No
78	1.56	27.98	5.49	22.49	0.99	0.183	1.43	0.128	1.10	1.00	0.153	No
79	1.58	28.34	5.69	22.65	0.99	0.184	1.43	0.129	1.10	1.00	0.153	No
80	1.60	28.71	5.89	22.82	0.99	0.185	1.43	0.130	1.10	1.00	0.154	No
81	1.62	29.07	6.08	22.99	0.99	0.186	1.43	0.130	1.10	1.00	0.155	No
82	1.64	29.43	6.28	23.15	0.98	0.187	1.43	0.131	1.10	1.00	0.155	No
83	1.66	29.79	6.47	23.32	0.98	0.188	1.43	0.132	1.10	1.00	0.156	No
84	1.68	30.15	6.67	23.48	0.98	0.189	1.43	0.132	1.10	1.00	0.157	No
85	1.70	30.51	6.87	23.65	0.98	0.190	1.43	0.133	1.10	1.00	0.158	No
86	1.72	30.87	7.06	23.81	0.98	0.191	1.43	0.133	1.10	1.00	0.159	No
87	1.74	31.23	7.26	23.97	0.98	0.191	1.43	0.134	1.10	1.00	0.160	No
88	1.76	31.59	7.46	24.13	0.98	0.192	1.43	0.135	1.10	1.00	0.161	No
89	1.78	31.94	7.65	24.29	0.98	0.193	1.43	0.135	1.10	1.00	0.162	No
90	1.80	32.30	7.85	24.45	0.98	0.194	1.43	0.136	1.10	1.00	0.163	No
91	1.82	32.65	8.04	24.61	0.98	0.195	1.43	0.136	1.10	1.00	0.163	No
92	1.84	33.00	8.24	24.76	0.98	0.196	1.43	0.137	1.10	1.00	0.164	No
93	1.86	33.35	8.44	24.92	0.98	0.196	1.43	0.137	1.10	1.00	0.165	No
94	1.88	33.70	8.63	25.07	0.98	0.197	1.43	0.138	1.10	1.00	0.166	No
95	1.90	34.05	8.83	25.22	0.98	0.198	1.43	0.139	1.10	1.00	0.167	No
96	1.92	34.39	9.03	25.36	0.98	0.199	1.43	0.139	1.10	1.00	0.167	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
97	1.94	34.73	9.22	25.51	0.98	0.199	1.43	0.140	1.10	1.00	0.168	No
98	1.96	35.07	9.42	25.65	0.98	0.200	1.43	0.140	1.10	1.00	0.169	No
99	1.98	35.40	9.61	25.79	0.98	0.201	1.43	0.141	1.10	1.00	0.170	No
100	2.01	35.90	9.91	26.00	0.98	0.202	1.43	0.141	1.10	1.00	0.171	No
101	2.02	36.07	10.01	26.06	0.98	0.202	1.43	0.142	1.10	1.00	0.172	No
102	2.04	36.39	10.20	26.19	0.98	0.203	1.43	0.142	1.10	1.00	0.172	No
103	2.06	36.71	10.40	26.31	0.98	0.204	1.43	0.143	1.10	1.00	0.173	No
104	2.08	37.02	10.59	26.42	0.98	0.205	1.43	0.143	1.10	1.00	0.174	No
105	2.10	37.32	10.79	26.53	0.98	0.206	1.43	0.144	1.10	1.00	0.174	No
106	2.12	37.63	10.99	26.64	0.98	0.206	1.43	0.144	1.10	1.00	2.000	Yes
107	2.14	37.93	11.18	26.74	0.98	0.207	1.43	0.145	1.10	1.00	2.000	Yes
108	2.16	38.22	11.38	26.84	0.98	0.208	1.43	0.145	1.10	1.00	2.000	Yes
109	2.18	38.52	11.58	26.95	0.98	0.209	1.43	0.146	1.10	1.00	2.000	Yes
110	2.21	38.98	11.87	27.11	0.98	0.210	1.43	0.147	1.10	1.00	2.000	Yes
111	2.22	39.13	11.97	27.16	0.98	0.210	1.43	0.147	1.10	1.00	2.000	Yes
112	2.24	39.43	12.16	27.27	0.97	0.211	1.43	0.148	1.10	1.00	2.000	Yes
113	2.26	39.75	12.36	27.39	0.97	0.211	1.43	0.148	1.10	1.00	2.000	Yes
114	2.28	40.08	12.56	27.52	0.97	0.212	1.43	0.148	1.10	1.00	2.000	Yes
115	2.30	40.41	12.75	27.66	0.97	0.213	1.43	0.149	1.10	1.00	2.000	Yes
116	2.32	40.76	12.95	27.81	0.97	0.213	1.43	0.149	1.10	1.00	2.000	Yes
117	2.34	41.10	13.15	27.96	0.97	0.214	1.43	0.150	1.10	1.00	2.000	Yes
118	2.36	41.46	13.34	28.12	0.97	0.214	1.43	0.150	1.10	1.00	2.000	Yes
119	2.38	41.82	13.54	28.28	0.97	0.215	1.43	0.150	1.10	1.00	2.000	Yes
120	2.40	42.18	13.73	28.45	0.97	0.216	1.43	0.151	1.10	1.00	2.000	Yes
121	2.42	42.54	13.93	28.61	0.97	0.216	1.43	0.151	1.10	1.00	2.000	Yes
122	2.44	42.91	14.13	28.78	0.97	0.217	1.43	0.152	1.10	1.00	2.000	Yes
123	2.46	43.27	14.32	28.95	0.97	0.217	1.43	0.152	1.10	1.00	2.000	Yes
124	2.48	43.63	14.52	29.11	0.97	0.217	1.43	0.152	1.10	1.00	0.180	No
125	2.50	44.00	14.72	29.28	0.97	0.218	1.43	0.153	1.10	1.00	0.181	No
126	2.52	44.36	14.91	29.45	0.97	0.218	1.43	0.153	1.10	1.00	0.181	No
127	2.54	44.72	15.11	29.61	0.97	0.219	1.43	0.153	1.10	1.00	0.181	No
128	2.56	45.08	15.30	29.78	0.97	0.219	1.43	0.154	1.10	1.00	0.181	No
129	2.58	45.44	15.50	29.94	0.97	0.220	1.43	0.154	1.10	1.00	0.182	No
130	2.60	45.81	15.70	30.11	0.97	0.220	1.43	0.154	1.10	1.00	0.182	No
131	2.62	46.17	15.89	30.28	0.97	0.221	1.43	0.155	1.10	1.00	0.182	No
132	2.64	46.53	16.09	30.44	0.97	0.221	1.43	0.155	1.10	1.00	0.183	No
133	2.66	46.89	16.28	30.61	0.97	0.222	1.43	0.155	1.10	1.00	0.183	No
134	2.68	47.25	16.48	30.77	0.97	0.222	1.43	0.155	1.10	1.00	0.184	No
135	2.70	47.62	16.68	30.94	0.97	0.222	1.43	0.156	1.10	1.00	0.184	No
136	2.72	47.98	16.87	31.10	0.97	0.223	1.43	0.156	1.10	1.00	0.184	No
137	2.74	48.34	17.07	31.27	0.97	0.223	1.43	0.156	1.10	1.00	0.184	No
138	2.76	48.70	17.27	31.44	0.97	0.224	1.43	0.157	1.10	1.00	0.185	No
139	2.78	49.06	17.46	31.60	0.97	0.224	1.43	0.157	1.10	1.00	0.185	No
140	2.80	49.43	17.66	31.77	0.97	0.224	1.43	0.157	1.10	1.00	0.185	No
141	2.82	49.79	17.85	31.93	0.96	0.225	1.43	0.157	1.10	1.00	0.186	No
142	2.84	50.14	18.05	32.09	0.96	0.225	1.43	0.158	1.10	1.00	0.187	No
143	2.86	50.50	18.25	32.26	0.96	0.226	1.43	0.158	1.10	1.00	0.188	No
144	2.88	50.86	18.44	32.42	0.96	0.226	1.43	0.158	1.10	1.00	0.189	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
145	2.92	51.58	18.84	32.74	0.96	0.227	1.43	0.159	1.10	1.00	0.190	No
146	2.92	51.58	18.84	32.74	0.96	0.227	1.43	0.159	1.10	1.00	0.191	No
147	2.94	51.93	19.03	32.90	0.96	0.227	1.43	0.159	1.10	1.00	0.191	No
148	2.97	52.47	19.33	33.14	0.96	0.228	1.43	0.159	1.09	1.00	0.192	No
149	2.99	52.82	19.52	33.30	0.96	0.228	1.43	0.160	1.09	1.00	0.193	No
150	3.00	53.00	19.62	33.38	0.96	0.228	1.43	0.160	1.09	1.00	0.194	No
151	3.02	53.34	19.82	33.53	0.96	0.229	1.43	0.160	1.09	1.00	0.194	No
152	3.05	53.86	20.11	33.75	0.96	0.229	1.43	0.160	1.09	1.00	0.193	No
153	3.06	54.03	20.21	33.82	0.96	0.229	1.43	0.161	1.09	1.00	0.193	No
154	3.08	54.36	20.40	33.95	0.96	0.230	1.43	0.161	1.09	1.00	0.194	No
155	3.10	54.69	20.60	34.09	0.96	0.230	1.43	0.161	1.09	1.00	0.195	No
156	3.12	55.03	20.80	34.23	0.96	0.231	1.43	0.161	1.09	1.00	0.194	No
157	3.14	55.37	20.99	34.38	0.96	0.231	1.43	0.162	1.10	1.00	0.194	No
158	3.16	55.72	21.19	34.53	0.96	0.231	1.43	0.162	1.09	1.00	0.194	No
159	3.18	56.06	21.39	34.67	0.96	0.232	1.43	0.162	1.10	1.00	0.194	No
160	3.20	56.41	21.58	34.82	0.96	0.232	1.43	0.162	1.09	1.00	0.194	No
161	3.22	56.75	21.78	34.98	0.96	0.232	1.43	0.163	1.09	1.00	0.195	No
162	3.24	57.10	21.97	35.13	0.96	0.233	1.43	0.163	1.09	1.00	0.196	No
163	3.26	57.45	22.17	35.28	0.96	0.233	1.43	0.163	1.09	1.00	0.196	No
164	3.28	57.80	22.37	35.44	0.96	0.233	1.43	0.163	1.09	1.00	0.196	No
165	3.30	58.16	22.56	35.59	0.96	0.234	1.43	0.163	1.09	1.00	0.196	No
166	3.32	58.51	22.76	35.75	0.96	0.234	1.43	0.164	1.09	1.00	0.196	No
167	3.34	58.86	22.96	35.91	0.96	0.234	1.43	0.164	1.09	1.00	0.197	No
168	3.36	59.22	23.15	36.06	0.95	0.234	1.43	0.164	1.09	1.00	0.197	No
169	3.38	59.57	23.35	36.22	0.95	0.235	1.43	0.164	1.09	1.00	0.197	No
170	3.40	59.92	23.54	36.38	0.95	0.235	1.43	0.164	1.09	1.00	0.197	No
171	3.42	60.28	23.74	36.54	0.95	0.235	1.43	0.165	1.09	1.00	0.196	No
172	3.44	60.63	23.94	36.70	0.95	0.235	1.43	0.165	1.09	1.00	0.197	No
173	3.46	60.99	24.13	36.86	0.95	0.236	1.43	0.165	1.09	1.00	0.197	No
174	3.49	61.52	24.43	37.10	0.95	0.236	1.43	0.165	1.09	1.00	0.198	No
175	3.50	61.70	24.53	37.18	0.95	0.236	1.43	0.165	1.09	1.00	0.198	No
176	3.52	62.06	24.72	37.34	0.95	0.237	1.43	0.166	1.09	1.00	0.198	No
177	3.54	62.42	24.92	37.50	0.95	0.237	1.43	0.166	1.09	1.00	0.199	No
178	3.56	62.78	25.11	37.67	0.95	0.237	1.43	0.166	1.09	1.00	0.199	No
179	3.58	63.14	25.31	37.83	0.95	0.237	1.43	0.166	1.09	1.00	0.199	No
180	3.60	63.50	25.51	37.99	0.95	0.237	1.43	0.166	1.09	1.00	0.200	No
181	3.62	63.86	25.70	38.16	0.95	0.238	1.43	0.166	1.09	1.00	0.200	No
182	3.64	64.22	25.90	38.32	0.95	0.238	1.43	0.167	1.09	1.00	0.200	No
183	3.66	64.58	26.09	38.49	0.95	0.238	1.43	0.167	1.09	1.00	0.200	No
184	3.68	64.94	26.29	38.65	0.95	0.238	1.43	0.167	1.09	1.00	0.200	No
185	3.70	65.30	26.49	38.81	0.95	0.239	1.43	0.167	1.09	1.00	0.200	No
186	3.72	65.65	26.68	38.97	0.95	0.239	1.43	0.167	1.09	1.00	0.201	No
187	3.74	66.01	26.88	39.13	0.95	0.239	1.43	0.167	1.09	1.00	0.201	No
188	3.76	66.37	27.08	39.29	0.95	0.239	1.43	0.167	1.09	1.00	0.201	No
189	3.78	66.73	27.27	39.45	0.95	0.239	1.43	0.168	1.09	1.00	0.202	No
190	3.80	67.09	27.47	39.62	0.95	0.240	1.43	0.168	1.08	1.00	0.202	No
191	3.82	67.44	27.66	39.78	0.95	0.240	1.43	0.168	1.08	1.00	0.202	No
192	3.84	67.80	27.86	39.94	0.95	0.240	1.43	0.168	1.08	1.00	0.203	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
193	3.86	68.16	28.06	40.11	0.95	0.240	1.43	0.168	1.08	1.00	0.203	No
194	3.88	68.52	28.25	40.27	0.94	0.240	1.43	0.168	1.08	1.00	0.204	No
195	3.90	68.88	28.45	40.44	0.94	0.241	1.43	0.168	1.08	1.00	0.204	No
196	3.92	69.24	28.65	40.60	0.94	0.241	1.43	0.169	1.08	1.00	0.204	No
197	3.94	69.60	28.84	40.76	0.94	0.241	1.43	0.169	1.08	1.00	0.205	No
198	3.96	69.96	29.04	40.92	0.94	0.241	1.43	0.169	1.08	1.00	0.205	No
199	3.98	70.31	29.23	41.08	0.94	0.241	1.43	0.169	1.08	1.00	0.206	No
200	4.00	70.67	29.43	41.24	0.94	0.241	1.43	0.169	1.08	1.00	0.206	No
201	4.02	71.02	29.63	41.40	0.94	0.242	1.43	0.169	1.08	1.00	0.207	No
202	4.05	71.56	29.92	41.64	0.94	0.242	1.43	0.169	1.08	1.00	0.208	No
203	4.06	71.74	30.02	41.72	0.94	0.242	1.43	0.169	1.08	1.00	0.208	No
204	4.08	72.09	30.21	41.88	0.94	0.242	1.43	0.170	1.07	1.00	0.208	No
205	4.10	72.44	30.41	42.03	0.94	0.242	1.43	0.170	1.07	1.00	0.208	No
206	4.12	72.80	30.61	42.19	0.94	0.243	1.43	0.170	1.07	1.00	0.209	No
207	4.14	73.15	30.80	42.35	0.94	0.243	1.43	0.170	1.07	1.00	0.209	No
208	4.16	73.51	31.00	42.51	0.94	0.243	1.43	0.170	1.07	1.00	0.209	No
209	4.18	73.86	31.20	42.66	0.94	0.243	1.43	0.170	1.07	1.00	0.209	No
210	4.20	74.21	31.39	42.82	0.94	0.243	1.43	0.170	1.07	1.00	0.209	No
211	4.22	74.57	31.59	42.98	0.94	0.243	1.43	0.170	1.07	1.00	0.209	No
212	4.24	74.92	31.78	43.14	0.94	0.244	1.43	0.170	1.07	1.00	0.209	No
213	4.26	75.27	31.98	43.29	0.94	0.244	1.43	0.171	1.07	1.00	0.209	No
214	4.28	75.63	32.18	43.45	0.94	0.244	1.43	0.171	1.07	1.00	0.210	No
215	4.30	75.98	32.37	43.61	0.94	0.244	1.43	0.171	1.07	1.00	0.209	No
216	4.32	76.34	32.57	43.77	0.94	0.244	1.43	0.171	1.07	1.00	0.209	No
217	4.34	76.70	32.77	43.93	0.94	0.244	1.43	0.171	1.07	1.00	0.209	No
218	4.36	77.05	32.96	44.09	0.94	0.244	1.43	0.171	1.07	1.00	0.210	No
219	4.38	77.41	33.16	44.25	0.93	0.245	1.43	0.171	1.07	1.00	0.210	No
220	4.40	77.76	33.35	44.41	0.93	0.245	1.43	0.171	1.07	1.00	0.210	No
221	4.42	78.11	33.55	44.56	0.93	0.245	1.43	0.171	1.07	1.00	0.210	No
222	4.44	78.47	33.75	44.72	0.93	0.245	1.43	0.171	1.07	1.00	0.211	No
223	4.46	78.82	33.94	44.88	0.93	0.245	1.43	0.172	1.07	1.00	0.211	No
224	4.48	79.17	34.14	45.03	0.93	0.245	1.43	0.172	1.07	1.00	0.212	No
225	4.50	79.52	34.34	45.18	0.93	0.245	1.43	0.172	1.07	1.00	0.212	No
226	4.52	79.87	34.53	45.34	0.93	0.245	1.43	0.172	1.07	1.00	0.213	No
227	4.54	80.22	34.73	45.49	0.93	0.246	1.43	0.172	1.07	1.00	0.213	No
228	4.56	80.57	34.92	45.65	0.93	0.246	1.43	0.172	1.07	1.00	0.214	No
229	4.58	80.92	35.12	45.80	0.93	0.246	1.43	0.172	1.07	1.00	0.214	No
230	4.60	81.27	35.32	45.95	0.93	0.246	1.43	0.172	1.06	1.00	0.215	No
231	4.62	81.61	35.51	46.10	0.93	0.246	1.43	0.172	1.06	1.00	0.215	No
232	4.64	81.95	35.71	46.24	0.93	0.246	1.43	0.172	1.06	1.00	0.216	No
233	4.66	82.29	35.90	46.39	0.93	0.246	1.43	0.173	1.06	1.00	0.216	No
234	4.68	82.63	36.10	46.53	0.93	0.247	1.43	0.173	1.06	1.00	0.216	No
235	4.70	82.96	36.30	46.66	0.93	0.247	1.43	0.173	1.06	1.00	0.217	No
236	4.72	83.29	36.49	46.80	0.93	0.247	1.43	0.173	1.06	1.00	0.217	No
237	4.74	83.62	36.69	46.93	0.93	0.247	1.43	0.173	1.06	1.00	0.217	No
238	4.76	83.95	36.89	47.06	0.93	0.247	1.43	0.173	1.06	1.00	0.217	No
239	4.78	84.27	37.08	47.19	0.93	0.247	1.43	0.173	1.06	1.00	0.217	No
240	4.80	84.59	37.28	47.31	0.93	0.248	1.43	0.173	1.06	1.00	0.217	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
241	4.82	84.91	37.47	47.43	0.93	0.248	1.43	0.173	1.06	1.00	0.218	No
242	4.84	85.23	37.67	47.56	0.93	0.248	1.43	0.174	1.06	1.00	0.218	No
243	4.86	85.55	37.87	47.68	0.93	0.248	1.43	0.174	1.06	1.00	0.218	No
244	4.88	85.87	38.06	47.81	0.92	0.248	1.43	0.174	1.06	1.00	0.218	No
245	4.90	86.19	38.26	47.93	0.92	0.248	1.43	0.174	1.06	1.00	0.218	No
246	4.92	86.52	38.46	48.06	0.92	0.249	1.43	0.174	1.06	1.00	0.218	No
247	4.94	86.84	38.65	48.19	0.92	0.249	1.43	0.174	1.06	1.00	0.218	No
248	4.96	87.16	38.85	48.32	0.92	0.249	1.43	0.174	1.06	1.00	0.219	No
249	4.98	87.49	39.04	48.44	0.92	0.249	1.43	0.174	1.06	1.00	0.219	No
250	5.00	87.81	39.24	48.57	0.92	0.249	1.43	0.174	1.06	1.00	0.219	No
251	5.02	88.13	39.44	48.69	0.92	0.249	1.43	0.175	1.06	1.00	0.219	No
252	5.04	88.45	39.63	48.81	0.92	0.250	1.43	0.175	1.06	1.00	0.219	No
253	5.06	88.76	39.83	48.93	0.92	0.250	1.43	0.175	1.06	1.00	0.219	No
254	5.08	89.08	40.02	49.06	0.92	0.250	1.43	0.175	1.06	1.00	0.219	No
255	5.10	89.40	40.22	49.18	0.92	0.250	1.43	0.175	1.06	1.00	0.219	No
256	5.12	89.72	40.42	49.31	0.92	0.250	1.43	0.175	1.06	1.00	0.219	No
257	5.14	90.04	40.61	49.43	0.92	0.250	1.43	0.175	1.06	1.00	0.219	No
258	5.16	90.37	40.81	49.56	0.92	0.250	1.43	0.175	1.06	1.00	0.219	No
259	5.19	90.85	41.10	49.75	0.92	0.251	1.43	0.175	1.06	1.00	0.219	No
260	5.20	91.01	41.20	49.81	0.92	0.251	1.43	0.176	1.06	1.00	0.219	No
261	5.22	91.34	41.40	49.94	0.92	0.251	1.43	0.176	1.06	1.00	0.219	No
262	5.24	91.67	41.59	50.07	0.92	0.251	1.43	0.176	1.06	1.00	0.220	No
263	5.26	92.00	41.79	50.21	0.92	0.251	1.43	0.176	1.06	1.00	0.219	No
264	5.28	92.33	41.99	50.34	0.92	0.251	1.43	0.176	1.06	1.00	0.219	No
265	5.30	92.66	42.18	50.48	0.92	0.251	1.43	0.176	1.06	1.00	0.219	No
266	5.32	93.00	42.38	50.62	0.92	0.251	1.43	0.176	1.06	1.00	0.219	No
267	5.34	93.34	42.58	50.76	0.92	0.252	1.43	0.176	1.06	1.00	0.219	No
268	5.36	93.68	42.77	50.91	0.91	0.252	1.43	0.176	1.06	1.00	0.219	No
269	5.38	94.02	42.97	51.05	0.91	0.252	1.43	0.176	1.06	1.00	0.219	No
270	5.40	94.37	43.16	51.20	0.91	0.252	1.43	0.176	1.06	1.00	0.219	No
271	5.42	94.71	43.36	51.35	0.91	0.252	1.43	0.176	1.06	1.00	0.219	No
272	5.44	95.06	43.56	51.50	0.91	0.252	1.43	0.176	1.06	1.00	0.218	No
273	5.46	95.41	43.75	51.66	0.91	0.252	1.43	0.176	1.06	1.00	0.218	No
274	5.48	95.76	43.95	51.81	0.91	0.252	1.43	0.176	1.06	1.00	0.218	No
275	5.50	96.11	44.15	51.97	0.91	0.252	1.43	0.176	1.06	1.00	0.218	No
276	5.52	96.47	44.34	52.13	0.91	0.252	1.43	0.176	1.06	1.00	0.218	No
277	5.54	96.83	44.54	52.29	0.91	0.252	1.43	0.176	1.06	1.00	0.218	No
278	5.56	97.19	44.73	52.45	0.91	0.252	1.43	0.177	1.06	1.00	0.218	No
279	5.58	97.55	44.93	52.62	0.91	0.252	1.43	0.177	1.06	1.00	0.218	No
280	5.60	97.91	45.13	52.79	0.91	0.252	1.43	0.177	1.06	1.00	0.219	No
281	5.62	98.28	45.32	52.95	0.91	0.252	1.43	0.177	1.06	1.00	0.219	No
282	5.64	98.64	45.52	53.12	0.91	0.252	1.43	0.177	1.06	1.00	0.220	No
283	5.66	99.01	45.71	53.29	0.91	0.252	1.43	0.177	1.06	1.00	0.220	No
284	5.68	99.37	45.91	53.46	0.91	0.252	1.43	0.177	1.05	1.00	0.221	No
285	5.70	99.73	46.11	53.63	0.91	0.252	1.43	0.177	1.05	1.00	0.221	No
286	5.72	100.09	46.30	53.79	0.91	0.252	1.43	0.177	1.05	1.00	0.221	No
287	5.74	100.45	46.50	53.95	0.91	0.252	1.43	0.177	1.05	1.00	0.221	No
288	5.76	100.81	46.70	54.11	0.91	0.252	1.43	0.177	1.05	1.00	0.221	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
289	5.78	101.16	46.89	54.27	0.91	0.252	1.43	0.177	1.05	1.00	0.221	No
290	5.80	101.51	47.09	54.42	0.91	0.252	1.43	0.177	1.05	1.00	0.221	No
291	5.82	101.86	47.28	54.57	0.90	0.252	1.43	0.177	1.05	1.00	0.221	No
292	5.84	102.21	47.48	54.73	0.90	0.252	1.43	0.177	1.05	1.00	0.221	No
293	5.86	102.55	47.68	54.88	0.90	0.253	1.43	0.177	1.05	1.00	0.221	No
294	5.89	103.08	47.97	55.11	0.90	0.253	1.43	0.177	1.05	1.00	0.220	No
295	5.90	103.26	48.07	55.19	0.90	0.253	1.43	0.177	1.05	1.00	0.220	No
296	5.92	103.61	48.27	55.35	0.90	0.253	1.43	0.177	1.05	1.00	0.220	No
297	5.94	103.97	48.46	55.51	0.90	0.253	1.43	0.177	1.05	1.00	0.220	No
298	5.96	104.33	48.66	55.67	0.90	0.253	1.43	0.177	1.05	1.00	0.220	No
299	5.98	104.68	48.85	55.83	0.90	0.253	1.43	0.177	1.05	1.00	0.220	No
300	6.01	105.23	49.15	56.08	0.90	0.253	1.43	0.177	1.05	1.00	0.221	No
301	6.02	105.41	49.25	56.16	0.90	0.253	1.43	0.177	1.05	1.00	0.221	No
302	6.04	105.77	49.44	56.33	0.90	0.253	1.43	0.177	1.05	1.00	0.221	No
303	6.06	106.13	49.64	56.50	0.90	0.253	1.43	0.177	1.05	1.00	0.221	No
304	6.08	106.50	49.83	56.66	0.90	0.253	1.43	0.177	1.05	1.00	0.221	No
305	6.10	106.86	50.03	56.83	0.90	0.253	1.43	0.177	1.05	1.00	0.221	No
306	6.12	107.23	50.23	57.00	0.90	0.253	1.43	0.177	1.05	1.00	0.222	No
307	6.14	107.59	50.42	57.17	0.90	0.253	1.43	0.177	1.05	1.00	0.222	No
308	6.16	107.95	50.62	57.33	0.90	0.253	1.43	0.177	1.05	1.00	0.222	No
309	6.18	108.31	50.82	57.50	0.90	0.253	1.43	0.177	1.05	1.00	0.222	No
310	6.21	108.85	51.11	57.74	0.90	0.253	1.43	0.177	1.05	1.00	0.223	No
311	6.22	109.03	51.21	57.83	0.90	0.253	1.43	0.177	1.05	1.00	0.223	No
312	6.25	109.57	51.50	58.07	0.90	0.253	1.43	0.177	1.05	1.00	0.223	No
313	6.26	109.75	51.60	58.15	0.89	0.253	1.43	0.177	1.05	1.00	0.223	No
314	6.28	110.11	51.80	58.32	0.89	0.253	1.43	0.177	1.05	1.00	0.223	No
315	6.30	110.48	51.99	58.48	0.89	0.253	1.43	0.177	1.05	1.00	0.223	No
316	6.32	110.83	52.19	58.65	0.89	0.252	1.43	0.177	1.05	1.00	0.223	No
317	6.34	111.19	52.39	58.81	0.89	0.252	1.43	0.177	1.05	1.00	0.223	No
318	6.36	111.55	52.58	58.97	0.89	0.252	1.43	0.177	1.05	1.00	0.223	No
319	6.38	111.91	52.78	59.13	0.89	0.252	1.43	0.177	1.05	1.00	0.223	No
320	6.40	112.26	52.97	59.29	0.89	0.252	1.43	0.177	1.05	1.00	0.223	No
321	6.42	112.62	53.17	59.45	0.89	0.252	1.43	0.177	1.05	1.00	0.223	No
322	6.44	112.97	53.37	59.61	0.89	0.252	1.43	0.177	1.05	1.00	0.223	No
323	6.46	113.33	53.56	59.77	0.89	0.252	1.43	0.177	1.05	1.00	0.223	No
324	6.48	113.69	53.76	59.93	0.89	0.252	1.43	0.177	1.04	1.00	0.223	No
325	6.50	114.04	53.96	60.09	0.89	0.252	1.43	0.177	1.04	1.00	0.223	No
326	6.52	114.40	54.15	60.25	0.89	0.252	1.43	0.177	1.04	1.00	0.223	No
327	6.54	114.76	54.35	60.41	0.89	0.252	1.43	0.177	1.04	1.00	0.223	No
328	6.56	115.12	54.54	60.57	0.89	0.252	1.43	0.177	1.04	1.00	0.222	No
329	6.58	115.47	54.74	60.73	0.89	0.252	1.43	0.177	1.04	1.00	0.222	No
330	6.60	115.83	54.94	60.90	0.89	0.252	1.43	0.177	1.04	1.00	0.222	No
331	6.62	116.19	55.13	61.06	0.89	0.252	1.43	0.177	1.04	1.00	0.222	No
332	6.64	116.56	55.33	61.23	0.89	0.252	1.43	0.177	1.04	1.00	0.222	No
333	6.66	116.92	55.52	61.39	0.89	0.252	1.43	0.177	1.04	1.00	0.222	No
334	6.68	117.28	55.72	61.56	0.89	0.252	1.43	0.177	1.04	1.00	0.223	No
335	6.70	117.64	55.92	61.73	0.89	0.252	1.43	0.177	1.04	1.00	0.222	No
336	6.72	118.01	56.11	61.89	0.88	0.252	1.43	0.177	1.04	1.00	0.222	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
337	6.74	118.37	56.31	62.06	0.88	0.252	1.43	0.176	1.04	1.00	0.222	No
338	6.76	118.74	56.51	62.23	0.88	0.252	1.43	0.176	1.04	1.00	0.222	No
339	6.78	119.10	56.70	62.40	0.88	0.252	1.43	0.176	1.04	1.00	0.222	No
340	6.80	119.47	56.90	62.57	0.88	0.252	1.43	0.176	1.04	1.00	0.222	No
341	6.82	119.83	57.09	62.74	0.88	0.252	1.43	0.176	1.04	1.00	0.222	No
342	6.84	120.20	57.29	62.91	0.88	0.252	1.43	0.176	1.04	1.00	0.222	No
343	6.86	120.56	57.49	63.08	0.88	0.252	1.43	0.176	1.04	1.00	0.222	No
344	6.88	120.93	57.68	63.25	0.88	0.252	1.43	0.176	1.04	1.00	0.221	No
345	6.90	121.30	57.88	63.42	0.88	0.252	1.43	0.176	1.04	1.00	0.222	No
346	6.92	121.67	58.08	63.60	0.88	0.252	1.43	0.176	1.04	1.00	0.222	No
347	6.94	122.04	58.27	63.77	0.88	0.252	1.43	0.176	1.04	1.00	0.222	No
348	6.96	122.41	58.47	63.94	0.88	0.252	1.43	0.176	1.04	1.00	0.222	No
349	6.98	122.78	58.66	64.12	0.88	0.252	1.43	0.176	1.04	1.00	0.223	No
350	7.00	123.15	58.86	64.29	0.88	0.252	1.43	0.176	1.04	1.00	0.223	No
351	7.02	123.52	59.06	64.46	0.88	0.251	1.43	0.176	1.04	1.00	0.223	No
352	7.04	123.88	59.25	64.63	0.88	0.251	1.43	0.176	1.04	1.00	0.223	No
353	7.06	124.25	59.45	64.80	0.88	0.251	1.43	0.176	1.04	1.00	0.223	No
354	7.08	124.61	59.64	64.96	0.88	0.251	1.43	0.176	1.04	1.00	0.222	No
355	7.10	124.97	59.84	65.13	0.88	0.251	1.43	0.176	1.04	1.00	0.222	No
356	7.12	125.34	60.04	65.30	0.88	0.251	1.43	0.176	1.04	1.00	0.222	No
357	7.14	125.70	60.23	65.47	0.88	0.251	1.43	0.176	1.04	1.00	0.222	No
358	7.16	126.07	60.43	65.64	0.87	0.251	1.43	0.176	1.04	1.00	0.222	No
359	7.18	126.43	60.63	65.81	0.87	0.251	1.43	0.176	1.04	1.00	0.222	No
360	7.20	126.80	60.82	65.98	0.87	0.251	1.43	0.176	1.04	1.00	0.222	No
361	7.22	127.16	61.02	66.15	0.87	0.251	1.43	0.176	1.04	1.00	0.222	No
362	7.24	127.53	61.21	66.32	0.87	0.251	1.43	0.176	1.04	1.00	0.222	No
363	7.26	127.90	61.41	66.49	0.87	0.251	1.43	0.176	1.04	1.00	0.222	No
364	7.28	128.27	61.61	66.66	0.87	0.251	1.43	0.176	1.04	1.00	0.222	No
365	7.30	128.63	61.80	66.83	0.87	0.251	1.43	0.176	1.04	1.00	0.222	No
366	7.32	129.00	62.00	67.01	0.87	0.251	1.43	0.175	1.04	1.00	0.221	No
367	7.34	129.37	62.20	67.18	0.87	0.251	1.43	0.175	1.04	1.00	0.221	No
368	7.36	129.74	62.39	67.35	0.87	0.251	1.43	0.175	1.04	1.00	0.220	No
369	7.38	130.12	62.59	67.53	0.87	0.251	1.43	0.175	1.04	1.00	0.220	No
370	7.40	130.49	62.78	67.70	0.87	0.250	1.43	0.175	1.04	1.00	0.220	No
371	7.42	130.86	62.98	67.88	0.87	0.250	1.43	0.175	1.04	1.00	0.220	No
372	7.44	131.23	63.18	68.05	0.87	0.250	1.43	0.175	1.04	1.00	0.220	No
373	7.46	131.60	63.37	68.23	0.87	0.250	1.43	0.175	1.04	1.00	0.220	No
374	7.48	131.97	63.57	68.40	0.87	0.250	1.43	0.175	1.04	1.00	0.220	No
375	7.50	132.35	63.77	68.58	0.87	0.250	1.43	0.175	1.04	1.00	0.220	No
376	7.52	132.72	63.96	68.76	0.87	0.250	1.43	0.175	1.04	1.00	0.220	No
377	7.54	133.10	64.16	68.94	0.87	0.250	1.43	0.175	1.04	1.00	0.219	No
378	7.56	133.47	64.35	69.12	0.87	0.250	1.43	0.175	1.04	1.00	0.219	No
379	7.58	133.85	64.55	69.30	0.87	0.250	1.43	0.175	1.04	1.00	0.219	No
380	7.60	134.22	64.75	69.48	0.86	0.250	1.43	0.175	1.03	1.00	0.219	No
381	7.62	134.60	64.94	69.66	0.86	0.250	1.43	0.175	1.03	1.00	0.220	No
382	7.64	134.97	65.14	69.84	0.86	0.250	1.43	0.175	1.03	1.00	0.220	No
383	7.66	135.35	65.33	70.02	0.86	0.249	1.43	0.175	1.03	1.00	0.220	No
384	7.68	135.73	65.53	70.20	0.86	0.249	1.43	0.175	1.03	1.00	0.221	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
385	7.70	136.10	65.73	70.38	0.86	0.249	1.43	0.174	1.03	1.00	0.221	No
386	7.72	136.48	65.92	70.55	0.86	0.249	1.43	0.174	1.03	1.00	0.221	No
387	7.74	136.85	66.12	70.73	0.86	0.249	1.43	0.174	1.03	1.00	0.221	No
388	7.76	137.23	66.32	70.91	0.86	0.249	1.43	0.174	1.03	1.00	0.221	No
389	7.78	137.61	66.51	71.09	0.86	0.249	1.43	0.174	1.03	1.00	0.221	No
390	7.80	137.98	66.71	71.27	0.86	0.249	1.43	0.174	1.03	1.00	0.221	No
391	7.82	138.36	66.90	71.45	0.86	0.249	1.43	0.174	1.03	1.00	0.221	No
392	7.84	138.73	67.10	71.63	0.86	0.249	1.43	0.174	1.03	1.00	0.221	No
393	7.86	139.10	67.30	71.81	0.86	0.249	1.43	0.174	1.03	1.00	0.221	No
394	7.88	139.48	67.49	71.99	0.86	0.249	1.43	0.174	1.03	1.00	0.221	No
395	7.90	139.85	67.69	72.16	0.86	0.248	1.43	0.174	1.03	1.00	0.220	No
396	7.92	140.23	67.89	72.34	0.86	0.248	1.43	0.174	1.03	1.00	0.221	No
397	7.94	140.60	68.08	72.52	0.86	0.248	1.43	0.174	1.03	1.00	0.220	No
398	7.96	140.98	68.28	72.70	0.86	0.248	1.43	0.174	1.03	1.00	0.220	No
399	7.98	141.35	68.47	72.88	0.86	0.248	1.43	0.174	1.03	1.00	0.220	No
400	8.00	141.72	68.67	73.05	0.86	0.248	1.43	0.174	1.03	1.00	0.220	No
401	8.02	142.10	68.87	73.23	0.85	0.248	1.43	0.174	1.03	1.00	0.221	No
402	8.04	142.47	69.06	73.41	0.85	0.248	1.43	0.174	1.03	1.00	0.221	No
403	8.07	143.03	69.36	73.67	0.85	0.248	1.43	0.173	1.03	1.00	0.222	No
404	8.08	143.21	69.45	73.76	0.85	0.248	1.43	0.173	1.03	1.00	0.222	No
405	8.10	143.58	69.65	73.93	0.85	0.248	1.43	0.173	1.03	1.00	0.222	No
406	8.12	143.95	69.85	74.10	0.85	0.248	1.43	0.173	1.03	1.00	0.222	No
407	8.14	144.32	70.04	74.27	0.85	0.247	1.43	0.173	1.03	1.00	0.222	No
408	8.16	144.68	70.24	74.44	0.85	0.247	1.43	0.173	1.03	1.00	0.222	No
409	8.18	145.05	70.44	74.61	0.85	0.247	1.43	0.173	1.03	1.00	0.222	No
410	8.20	145.42	70.63	74.78	0.85	0.247	1.43	0.173	1.03	1.00	0.222	No
411	8.22	145.78	70.83	74.95	0.85	0.247	1.43	0.173	1.03	1.00	0.222	No
412	8.24	146.15	71.02	75.12	0.85	0.247	1.43	0.173	1.03	1.00	0.222	No
413	8.26	146.51	71.22	75.29	0.85	0.247	1.43	0.173	1.03	1.00	0.222	No
414	8.28	146.88	71.42	75.46	0.85	0.247	1.43	0.173	1.03	1.00	0.222	No
415	8.30	147.24	71.61	75.63	0.85	0.247	1.43	0.173	1.03	1.00	0.221	No
416	8.32	147.61	71.81	75.80	0.85	0.247	1.43	0.173	1.03	1.00	0.221	No
417	8.34	147.97	72.01	75.97	0.85	0.247	1.43	0.173	1.03	1.00	0.221	No
418	8.36	148.34	72.20	76.14	0.85	0.247	1.43	0.173	1.03	1.00	0.221	No
419	8.38	148.71	72.40	76.31	0.85	0.247	1.43	0.173	1.03	1.00	0.221	No
420	8.40	149.08	72.59	76.48	0.85	0.246	1.43	0.173	1.02	1.00	0.221	No
421	8.42	149.44	72.79	76.65	0.85	0.246	1.43	0.172	1.02	1.00	0.221	No
422	8.44	149.81	72.99	76.83	0.84	0.246	1.43	0.172	1.02	1.00	0.221	No
423	8.47	150.37	73.28	77.09	0.84	0.246	1.43	0.172	1.02	1.00	0.221	No
424	8.48	150.55	73.38	77.18	0.84	0.246	1.43	0.172	1.02	1.00	0.221	No
425	8.50	150.93	73.58	77.35	0.84	0.246	1.43	0.172	1.02	1.00	0.221	No
426	8.52	151.30	73.77	77.53	0.84	0.246	1.43	0.172	1.02	1.00	0.220	No
427	8.54	151.67	73.97	77.70	0.84	0.246	1.43	0.172	1.02	1.00	0.220	No
428	8.56	152.04	74.16	77.88	0.84	0.246	1.43	0.172	1.02	1.00	0.221	No
429	8.58	152.41	74.36	78.05	0.84	0.246	1.43	0.172	1.02	1.00	0.220	No
430	8.60	152.78	74.56	78.23	0.84	0.246	1.43	0.172	1.02	1.00	0.220	No
431	8.62	153.16	74.75	78.40	0.84	0.246	1.43	0.172	1.02	1.00	0.220	No
432	8.64	153.53	74.95	78.58	0.84	0.245	1.43	0.172	1.02	1.00	0.220	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
433	8.66	153.90	75.14	78.76	0.84	0.245	1.43	0.172	1.02	1.00	0.220	No
434	8.68	154.28	75.34	78.94	0.84	0.245	1.43	0.172	1.02	1.00	0.221	No
435	8.70	154.65	75.54	79.11	0.84	0.245	1.43	0.172	1.02	1.00	0.221	No
436	8.72	155.02	75.73	79.29	0.84	0.245	1.43	0.172	1.02	1.00	0.221	No
437	8.74	155.39	75.93	79.46	0.84	0.245	1.43	0.171	1.02	1.00	0.221	No
438	8.76	155.76	76.13	79.63	0.84	0.245	1.43	0.171	1.02	1.00	0.221	No
439	8.78	156.12	76.32	79.80	0.84	0.245	1.43	0.171	1.02	1.00	0.221	No
440	8.80	156.49	76.52	79.97	0.84	0.245	1.43	0.171	1.02	1.00	0.221	No
441	8.82	156.85	76.71	80.14	0.84	0.245	1.43	0.171	1.02	1.00	0.220	No
442	8.84	157.22	76.91	80.31	0.84	0.245	1.43	0.171	1.02	1.00	0.220	No
443	8.86	157.58	77.11	80.47	0.83	0.244	1.43	0.171	1.02	1.00	0.220	No
444	8.88	157.94	77.30	80.64	0.83	0.244	1.43	0.171	1.02	1.00	0.219	No
445	8.90	158.31	77.50	80.81	0.83	0.244	1.43	0.171	1.02	1.00	0.219	No
446	8.92	158.68	77.70	80.98	0.83	0.244	1.43	0.171	1.02	1.00	0.219	No
447	8.94	159.05	77.89	81.15	0.83	0.244	1.43	0.171	1.02	1.00	0.219	No
448	8.96	159.41	78.09	81.33	0.83	0.244	1.43	0.171	1.02	1.00	0.219	No
449	8.98	159.79	78.28	81.50	0.83	0.244	1.43	0.171	1.02	1.00	0.219	No
450	9.00	160.16	78.48	81.68	0.83	0.244	1.43	0.171	1.02	1.00	0.219	No
451	9.02	160.53	78.68	81.85	0.83	0.244	1.43	0.171	1.02	1.00	0.219	No
452	9.04	160.90	78.87	82.03	0.83	0.244	1.43	0.171	1.02	1.00	0.219	No
453	9.06	161.27	79.07	82.20	0.83	0.244	1.43	0.170	1.02	1.00	0.219	No
454	9.09	161.83	79.36	82.46	0.83	0.243	1.43	0.170	1.02	1.00	0.220	No
455	9.10	162.01	79.46	82.55	0.83	0.243	1.43	0.170	1.02	1.00	0.220	No
456	9.13	162.56	79.76	82.80	0.83	0.243	1.43	0.170	1.02	1.00	0.221	No
457	9.14	162.74	79.85	82.89	0.83	0.243	1.43	0.170	1.02	1.00	0.221	No
458	9.16	163.10	80.05	83.05	0.83	0.243	1.43	0.170	1.02	1.00	0.221	No
459	9.18	163.46	80.25	83.22	0.83	0.243	1.43	0.170	1.02	1.00	0.221	No
460	9.20	163.82	80.44	83.38	0.83	0.243	1.43	0.170	1.02	1.00	0.221	No
461	9.22	164.18	80.64	83.54	0.83	0.243	1.43	0.170	1.02	1.00	0.221	No
462	9.24	164.53	80.83	83.69	0.83	0.243	1.43	0.170	1.02	1.00	0.221	No
463	9.26	164.88	81.03	83.85	0.83	0.243	1.43	0.170	1.02	1.00	0.221	No
464	9.28	165.23	81.23	84.00	0.83	0.243	1.43	0.170	1.02	1.00	0.221	No
465	9.30	165.57	81.42	84.15	0.82	0.243	1.43	0.170	1.02	1.00	0.221	No
466	9.32	165.92	81.62	84.30	0.82	0.242	1.43	0.170	1.02	1.00	0.221	No
467	9.34	166.26	81.82	84.45	0.82	0.242	1.43	0.170	1.02	1.00	0.221	No
468	9.36	166.61	82.01	84.60	0.82	0.242	1.43	0.170	1.01	1.00	0.222	No
469	9.38	166.95	82.21	84.74	0.82	0.242	1.43	0.170	1.01	1.00	0.222	No
470	9.40	167.30	82.40	84.89	0.82	0.242	1.43	0.170	1.01	1.00	0.222	No
471	9.42	167.64	82.60	85.04	0.82	0.242	1.43	0.170	1.01	1.00	0.222	No
472	9.44	167.98	82.80	85.18	0.82	0.242	1.43	0.169	1.01	1.00	0.221	No
473	9.47	168.49	83.09	85.40	0.82	0.242	1.43	0.169	1.01	1.00	0.221	No
474	9.48	168.66	83.19	85.47	0.82	0.242	1.43	0.169	1.01	1.00	0.221	No
475	9.50	169.00	83.39	85.62	0.82	0.242	1.43	0.169	1.01	1.00	0.220	No
476	9.52	169.34	83.58	85.76	0.82	0.242	1.43	0.169	1.01	1.00	0.220	No
477	9.54	169.69	83.78	85.91	0.82	0.242	1.43	0.169	1.01	1.00	0.219	No
478	9.56	170.04	83.97	86.06	0.82	0.242	1.43	0.169	1.01	1.00	0.219	No
479	9.58	170.39	84.17	86.22	0.82	0.242	1.43	0.169	1.01	1.00	0.218	No
480	9.60	170.75	84.37	86.38	0.82	0.242	1.43	0.169	1.01	1.00	0.218	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
481	9.62	171.11	84.56	86.54	0.82	0.241	1.43	0.169	1.01	1.00	0.218	No
482	9.64	171.47	84.76	86.71	0.82	0.241	1.43	0.169	1.01	1.00	0.217	No
483	9.66	171.84	84.95	86.89	0.82	0.241	1.43	0.169	1.01	1.00	0.217	No
484	9.68	172.21	85.15	87.06	0.82	0.241	1.43	0.169	1.01	1.00	0.216	No
485	9.70	172.58	85.35	87.24	0.81	0.241	1.43	0.169	1.01	1.00	0.216	No
486	9.72	172.96	85.54	87.41	0.81	0.241	1.43	0.169	1.01	1.00	0.216	No
487	9.74	173.33	85.74	87.59	0.81	0.241	1.43	0.169	1.01	1.00	0.215	No
488	9.76	173.71	85.94	87.77	0.81	0.241	1.43	0.168	1.01	1.00	0.215	No
489	9.78	174.08	86.13	87.95	0.81	0.241	1.43	0.168	1.01	1.00	0.216	No
490	9.80	174.46	86.33	88.13	0.81	0.240	1.43	0.168	1.01	1.00	0.217	No
491	9.82	174.84	86.52	88.31	0.81	0.240	1.43	0.168	1.01	1.00	0.217	No
492	9.84	175.21	86.72	88.49	0.81	0.240	1.43	0.168	1.01	1.00	0.218	No
493	9.86	175.58	86.92	88.67	0.81	0.240	1.43	0.168	1.01	1.00	0.219	No
494	9.88	175.95	87.11	88.84	0.81	0.240	1.43	0.168	1.01	1.00	0.220	No
495	9.91	176.51	87.41	89.10	0.81	0.240	1.43	0.168	1.01	1.00	0.220	No
496	9.92	176.69	87.51	89.18	0.81	0.240	1.43	0.168	1.01	1.00	0.221	No
497	9.94	177.05	87.70	89.35	0.81	0.240	1.43	0.168	1.01	1.00	0.221	No
498	9.96	177.41	87.90	89.51	0.81	0.240	1.43	0.168	1.01	1.00	0.221	No
499	9.98	177.76	88.09	89.67	0.81	0.240	1.43	0.168	1.01	1.00	0.221	No
500	10.00	178.11	88.29	89.82	0.81	0.239	1.43	0.168	1.01	1.00	0.221	No
501	10.02	178.45	88.49	89.97	0.81	0.239	1.43	0.168	1.01	1.00	0.221	No
502	10.04	178.79	88.68	90.11	0.81	0.239	1.43	0.168	1.01	1.00	0.220	No
503	10.06	179.13	88.88	90.25	0.81	0.239	1.43	0.167	1.01	1.00	0.220	No
504	10.08	179.46	89.07	90.38	0.81	0.239	1.43	0.167	1.01	1.00	0.220	No
505	10.10	179.79	89.27	90.52	0.81	0.239	1.43	0.167	1.01	1.00	0.220	No
506	10.12	180.12	89.47	90.65	0.80	0.239	1.43	0.167	1.01	1.00	0.220	No
507	10.14	180.45	89.66	90.78	0.80	0.239	1.43	0.167	1.01	1.00	0.220	No
508	10.16	180.78	89.86	90.92	0.80	0.239	1.43	0.167	1.01	1.00	0.219	No
509	10.18	181.11	90.06	91.05	0.80	0.239	1.43	0.167	1.01	1.00	0.218	No
510	10.20	181.45	90.25	91.19	0.80	0.239	1.43	0.167	1.01	1.00	0.217	No
511	10.22	181.79	90.45	91.34	0.80	0.239	1.43	0.167	1.01	1.00	0.217	No
512	10.24	182.14	90.64	91.49	0.80	0.239	1.43	0.167	1.01	1.00	0.218	No
513	10.26	182.48	90.84	91.64	0.80	0.239	1.43	0.167	1.01	1.00	2.000	Yes
514	10.28	182.83	91.04	91.80	0.80	0.239	1.43	0.167	1.01	1.00	2.000	Yes
515	10.30	183.18	91.23	91.95	0.80	0.238	1.43	0.167	1.01	1.00	2.000	Yes
516	10.32	183.53	91.43	92.10	0.80	0.238	1.43	0.167	1.01	1.00	2.000	Yes
517	10.34	183.88	91.63	92.25	0.80	0.238	1.43	0.167	1.01	1.00	2.000	Yes
518	10.36	184.23	91.82	92.41	0.80	0.238	1.43	0.167	1.01	1.00	2.000	Yes
519	10.38	184.58	92.02	92.56	0.80	0.238	1.43	0.167	1.01	1.00	2.000	Yes
520	10.40	184.92	92.21	92.71	0.80	0.238	1.43	0.167	1.01	1.00	2.000	Yes
521	10.42	185.27	92.41	92.86	0.80	0.238	1.43	0.167	1.01	1.00	2.000	Yes
522	10.44	185.61	92.61	93.00	0.80	0.238	1.43	0.167	1.01	1.00	2.000	Yes
523	10.46	185.95	92.80	93.15	0.80	0.238	1.43	0.166	1.01	1.00	2.000	Yes
524	10.48	186.30	93.00	93.30	0.80	0.238	1.43	0.166	1.01	1.00	2.000	Yes
525	10.50	186.64	93.19	93.45	0.80	0.238	1.43	0.166	1.01	1.00	0.219	No
526	10.52	186.98	93.39	93.59	0.80	0.238	1.43	0.166	1.01	1.00	0.219	No
527	10.54	187.33	93.59	93.74	0.79	0.237	1.43	0.166	1.01	1.00	0.219	No
528	10.56	187.67	93.78	93.88	0.79	0.237	1.43	0.166	1.01	1.00	0.219	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
529	10.58	188.00	93.98	94.02	0.79	0.237	1.43	0.166	1.01	1.00	0.219	No
530	10.60	188.34	94.18	94.16	0.79	0.237	1.43	0.166	1.01	1.00	0.219	No
531	10.62	188.67	94.37	94.30	0.79	0.237	1.43	0.166	1.01	1.00	0.219	No
532	10.64	189.00	94.57	94.43	0.79	0.237	1.43	0.166	1.01	1.00	0.219	No
533	10.66	189.33	94.76	94.56	0.79	0.237	1.43	0.166	1.01	1.00	0.219	No
534	10.68	189.66	94.96	94.70	0.79	0.237	1.43	0.166	1.01	1.00	0.219	No
535	10.70	189.99	95.16	94.83	0.79	0.237	1.43	0.166	1.01	1.00	2.000	Yes
536	10.72	190.32	95.35	94.96	0.79	0.237	1.43	0.166	1.01	1.00	2.000	Yes
537	10.74	190.65	95.55	95.10	0.79	0.237	1.43	0.166	1.01	1.00	2.000	Yes
538	10.76	190.98	95.75	95.24	0.79	0.237	1.43	0.166	1.01	1.00	2.000	Yes
539	10.78	191.32	95.94	95.38	0.79	0.237	1.43	0.166	1.01	1.00	2.000	Yes
540	10.80	191.66	96.14	95.52	0.79	0.237	1.43	0.166	1.01	1.00	2.000	Yes
541	10.82	192.00	96.33	95.67	0.79	0.236	1.43	0.166	1.01	1.00	2.000	Yes
542	10.84	192.34	96.53	95.81	0.79	0.236	1.43	0.165	1.01	1.00	2.000	Yes
543	10.86	192.69	96.73	95.96	0.79	0.236	1.43	0.165	1.01	1.00	2.000	Yes
544	10.88	193.04	96.92	96.12	0.79	0.236	1.43	0.165	1.00	1.00	2.000	Yes
545	10.90	193.39	97.12	96.27	0.79	0.236	1.43	0.165	1.00	1.00	2.000	Yes
546	10.92	193.74	97.32	96.42	0.79	0.236	1.43	0.165	1.00	1.00	2.000	Yes
547	10.94	194.08	97.51	96.57	0.79	0.236	1.43	0.165	1.00	1.00	2.000	Yes
548	10.96	194.42	97.71	96.72	0.78	0.236	1.43	0.165	1.00	1.00	0.217	No
549	10.98	194.76	97.90	96.86	0.78	0.236	1.43	0.165	1.00	1.00	0.217	No
550	11.00	195.10	98.10	97.00	0.78	0.236	1.43	0.165	1.00	1.00	0.217	No
551	11.02	195.45	98.30	97.15	0.78	0.236	1.43	0.165	1.00	1.00	0.216	No
552	11.04	195.79	98.49	97.30	0.78	0.236	1.43	0.165	1.00	1.00	0.216	No
553	11.06	196.14	98.69	97.45	0.78	0.235	1.43	0.165	1.00	1.00	0.216	No
554	11.08	196.50	98.88	97.61	0.78	0.235	1.43	0.165	1.00	1.00	0.216	No
555	11.10	196.85	99.08	97.77	0.78	0.235	1.43	0.165	1.00	1.00	0.216	No
556	11.13	197.40	99.38	98.02	0.78	0.235	1.43	0.165	1.00	1.00	0.217	No
557	11.14	197.58	99.47	98.10	0.78	0.235	1.43	0.164	1.00	1.00	0.217	No
558	11.16	197.94	99.67	98.27	0.78	0.235	1.43	0.164	1.00	1.00	0.217	No
559	11.18	198.31	99.87	98.44	0.78	0.235	1.43	0.164	1.00	1.00	0.217	No
560	11.20	198.67	100.06	98.61	0.78	0.235	1.43	0.164	1.00	1.00	0.218	No
561	11.22	199.03	100.26	98.77	0.78	0.235	1.43	0.164	1.00	1.00	0.218	No
562	11.24	199.39	100.45	98.94	0.78	0.234	1.43	0.164	1.00	1.00	0.218	No
563	11.26	199.75	100.65	99.10	0.78	0.234	1.43	0.164	1.00	1.00	0.218	No
564	11.28	200.11	100.85	99.26	0.78	0.234	1.43	0.164	1.00	1.00	0.218	No
565	11.30	200.46	101.04	99.42	0.78	0.234	1.43	0.164	1.00	1.00	0.217	No
566	11.32	200.81	101.24	99.57	0.78	0.234	1.43	0.164	1.00	1.00	0.218	No
567	11.34	201.15	101.44	99.71	0.78	0.234	1.43	0.164	1.00	1.00	0.217	No
568	11.36	201.48	101.63	99.85	0.78	0.234	1.43	0.164	1.00	1.00	0.217	No
569	11.38	201.81	101.83	99.98	0.77	0.234	1.43	0.164	1.00	1.00	0.217	No
570	11.40	202.13	102.02	100.11	0.77	0.234	1.43	0.164	1.00	1.00	0.217	No
571	11.42	202.46	102.22	100.24	0.77	0.234	1.43	0.164	1.00	1.00	0.216	No
572	11.44	202.78	102.42	100.37	0.77	0.234	1.43	0.164	1.00	1.00	0.216	No
573	11.46	203.12	102.61	100.51	0.77	0.234	1.43	0.163	1.00	1.00	0.215	No
574	11.48	203.46	102.81	100.65	0.77	0.233	1.43	0.163	1.00	1.00	0.215	No
575	11.50	203.81	103.01	100.80	0.77	0.233	1.43	0.163	1.00	1.00	0.215	No
576	11.52	204.16	103.20	100.95	0.77	0.233	1.43	0.163	1.00	1.00	0.215	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
577	11.54	204.51	103.40	101.11	0.77	0.233	1.43	0.163	1.00	1.00	0.215	No
578	11.56	204.87	103.59	101.27	0.77	0.233	1.43	0.163	1.00	1.00	0.215	No
579	11.58	205.23	103.79	101.44	0.77	0.233	1.43	0.163	1.00	1.00	0.215	No
580	11.60	205.59	103.99	101.61	0.77	0.233	1.43	0.163	1.00	1.00	0.215	No
581	11.62	205.96	104.18	101.78	0.77	0.233	1.43	0.163	1.00	1.00	0.215	No
582	11.64	206.33	104.38	101.95	0.77	0.233	1.43	0.163	1.00	1.00	0.215	No
583	11.66	206.69	104.57	102.12	0.77	0.232	1.43	0.163	1.00	1.00	0.215	No
584	11.68	207.06	104.77	102.29	0.77	0.232	1.43	0.163	1.00	1.00	0.215	No
585	11.70	207.42	104.97	102.45	0.77	0.232	1.43	0.163	1.00	1.00	0.215	No
586	11.72	207.78	105.16	102.62	0.77	0.232	1.43	0.162	1.00	1.00	0.215	No
587	11.74	208.15	105.36	102.79	0.77	0.232	1.43	0.162	1.00	1.00	0.215	No
588	11.76	208.51	105.56	102.95	0.77	0.232	1.43	0.162	1.00	1.00	0.215	No
589	11.78	208.87	105.75	103.12	0.77	0.232	1.43	0.162	1.00	1.00	0.215	No
590	11.80	209.23	105.95	103.28	0.76	0.232	1.43	0.162	1.00	1.00	0.215	No
591	11.82	209.59	106.14	103.45	0.76	0.232	1.43	0.162	1.00	1.00	0.214	No
592	11.84	209.96	106.34	103.62	0.76	0.231	1.43	0.162	1.00	1.00	0.214	No
593	11.86	210.32	106.54	103.78	0.76	0.231	1.43	0.162	1.00	1.00	0.214	No
594	11.88	210.68	106.73	103.95	0.76	0.231	1.43	0.162	1.00	1.00	0.214	No
595	11.90	211.05	106.93	104.12	0.76	0.231	1.43	0.162	1.00	1.00	0.214	No
596	11.92	211.41	107.13	104.28	0.76	0.231	1.43	0.162	1.00	1.00	0.213	No
597	11.94	211.77	107.32	104.45	0.76	0.231	1.43	0.162	1.00	1.00	0.213	No
598	11.96	212.14	107.52	104.62	0.76	0.231	1.43	0.161	1.00	1.00	0.213	No
599	11.98	212.50	107.71	104.79	0.76	0.231	1.43	0.161	1.00	1.00	0.213	No
600	12.00	212.86	107.91	104.95	0.76	0.230	1.43	0.161	1.00	1.00	0.213	No
601	12.02	213.23	108.11	105.12	0.76	0.230	1.43	0.161	1.00	1.00	0.213	No
602	12.04	213.59	108.30	105.29	0.76	0.230	1.43	0.161	1.00	1.00	0.213	No
603	12.06	213.96	108.50	105.46	0.76	0.230	1.43	0.161	1.00	1.00	0.213	No
604	12.08	214.33	108.69	105.63	0.76	0.230	1.43	0.161	1.00	1.00	0.212	No
605	12.10	214.69	108.89	105.80	0.76	0.230	1.43	0.161	1.00	1.00	0.212	No
606	12.12	215.06	109.09	105.98	0.76	0.230	1.43	0.161	1.00	1.00	0.212	No
607	12.14	215.44	109.28	106.15	0.76	0.230	1.43	0.161	1.00	1.00	0.211	No
608	12.16	215.81	109.48	106.33	0.76	0.229	1.43	0.161	1.00	1.00	0.211	No
609	12.18	216.19	109.68	106.51	0.76	0.229	1.43	0.161	1.00	1.00	0.211	No
610	12.21	216.75	109.97	106.78	0.76	0.229	1.43	0.160	1.00	1.00	0.211	No
611	12.22	216.94	110.07	106.87	0.75	0.229	1.43	0.160	1.00	1.00	0.211	No
612	12.24	217.32	110.26	107.05	0.75	0.229	1.43	0.160	1.00	1.00	0.211	No
613	12.26	217.70	110.46	107.23	0.75	0.229	1.43	0.160	0.99	1.00	0.211	No
614	12.28	218.07	110.66	107.42	0.75	0.229	1.43	0.160	0.99	1.00	0.211	No
615	12.30	218.45	110.85	107.60	0.75	0.229	1.43	0.160	0.99	1.00	0.211	No
616	12.32	218.83	111.05	107.78	0.75	0.228	1.43	0.160	0.99	1.00	0.211	No
617	12.34	219.21	111.25	107.96	0.75	0.228	1.43	0.160	0.99	1.00	0.211	No
618	12.36	219.58	111.44	108.14	0.75	0.228	1.43	0.160	0.99	1.00	0.210	No
619	12.38	219.96	111.64	108.32	0.75	0.228	1.43	0.160	0.99	1.00	0.210	No
620	12.40	220.34	111.83	108.50	0.75	0.228	1.43	0.160	0.99	1.00	0.210	No
621	12.42	220.72	112.03	108.69	0.75	0.228	1.43	0.159	0.99	1.00	0.210	No
622	12.44	221.09	112.23	108.87	0.75	0.228	1.43	0.159	0.99	1.00	0.210	No
623	12.46	221.47	112.42	109.05	0.75	0.227	1.43	0.159	0.99	1.00	0.210	No
624	12.48	221.84	112.62	109.23	0.75	0.227	1.43	0.159	0.99	1.00	0.210	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
625	12.50	222.22	112.82	109.41	0.75	0.227	1.43	0.159	0.99	1.00	0.210	No
626	12.52	222.60	113.01	109.58	0.75	0.227	1.43	0.159	0.99	1.00	0.209	No
627	12.54	222.97	113.21	109.76	0.75	0.227	1.43	0.159	0.99	1.00	0.209	No
628	12.56	223.34	113.40	109.94	0.75	0.227	1.43	0.159	0.99	1.00	0.209	No
629	12.58	223.72	113.60	110.12	0.75	0.227	1.43	0.159	0.99	1.00	0.210	No
630	12.60	224.09	113.80	110.30	0.75	0.227	1.43	0.159	0.99	1.00	0.210	No
631	12.62	224.47	113.99	110.48	0.75	0.226	1.43	0.158	0.99	1.00	0.210	No
632	12.64	224.84	114.19	110.65	0.74	0.226	1.43	0.158	0.99	1.00	0.210	No
633	12.66	225.22	114.38	110.83	0.74	0.226	1.43	0.158	0.99	1.00	0.210	No
634	12.68	225.59	114.58	111.01	0.74	0.226	1.43	0.158	0.99	1.00	0.210	No
635	12.70	225.96	114.78	111.19	0.74	0.226	1.43	0.158	0.99	1.00	0.210	No
636	12.72	226.34	114.97	111.36	0.74	0.226	1.43	0.158	0.99	1.00	0.209	No
637	12.74	226.71	115.17	111.54	0.74	0.226	1.43	0.158	0.99	1.00	0.209	No
638	12.76	227.08	115.37	111.71	0.74	0.226	1.43	0.158	0.99	1.00	0.209	No
639	12.78	227.45	115.56	111.89	0.74	0.225	1.43	0.158	0.99	1.00	0.209	No
640	12.80	227.82	115.76	112.06	0.74	0.225	1.43	0.158	0.99	1.00	0.208	No
641	12.82	228.19	115.95	112.24	0.74	0.225	1.43	0.158	0.99	1.00	0.208	No
642	12.84	228.57	116.15	112.42	0.74	0.225	1.43	0.158	0.99	1.00	0.207	No
643	12.86	228.94	116.35	112.59	0.74	0.225	1.43	0.157	0.99	1.00	0.207	No
644	12.88	229.31	116.54	112.77	0.74	0.225	1.43	0.157	0.99	1.00	0.206	No
645	12.90	229.69	116.74	112.95	0.74	0.225	1.43	0.157	0.99	1.00	0.206	No
646	12.92	230.06	116.94	113.13	0.74	0.224	1.43	0.157	0.99	1.00	0.206	No
647	12.94	230.44	117.13	113.31	0.74	0.224	1.43	0.157	0.99	1.00	0.206	No
648	12.96	230.81	117.33	113.49	0.74	0.224	1.43	0.157	0.99	1.00	0.206	No
649	12.99	231.38	117.62	113.76	0.74	0.224	1.43	0.157	0.99	1.00	0.207	No
650	13.01	231.75	117.82	113.93	0.74	0.224	1.43	0.157	0.99	1.00	0.207	No
651	13.02	231.94	117.92	114.03	0.74	0.224	1.43	0.157	0.99	1.00	0.208	No
652	13.04	232.32	118.11	114.21	0.74	0.224	1.43	0.157	0.99	1.00	0.208	No
653	13.06	232.70	118.31	114.39	0.74	0.224	1.43	0.156	0.99	1.00	0.208	No
654	13.08	233.07	118.50	114.57	0.73	0.223	1.43	0.156	0.99	1.00	0.208	No
655	13.10	233.45	118.70	114.75	0.73	0.223	1.43	0.156	0.99	1.00	0.208	No
656	13.12	233.83	118.90	114.93	0.73	0.223	1.43	0.156	0.99	1.00	0.208	No
657	13.14	234.20	119.09	115.11	0.73	0.223	1.43	0.156	0.99	1.00	0.207	No
658	13.16	234.57	119.29	115.28	0.73	0.223	1.43	0.156	0.99	1.00	0.207	No
659	13.18	234.94	119.49	115.45	0.73	0.223	1.43	0.156	0.99	1.00	0.206	No
660	13.20	235.31	119.68	115.63	0.73	0.223	1.43	0.156	0.99	1.00	0.207	No
661	13.22	235.68	119.88	115.80	0.73	0.223	1.43	0.156	0.99	1.00	0.207	No
662	13.24	236.05	120.07	115.97	0.73	0.222	1.43	0.156	0.99	1.00	0.207	No
663	13.26	236.42	120.27	116.15	0.73	0.222	1.43	0.156	0.99	1.00	0.207	No
664	13.28	236.78	120.47	116.32	0.73	0.222	1.43	0.156	0.99	1.00	0.207	No
665	13.30	237.15	120.66	116.49	0.73	0.222	1.43	0.155	0.99	1.00	0.207	No
666	13.32	237.52	120.86	116.66	0.73	0.222	1.43	0.155	0.99	1.00	0.207	No
667	13.34	237.89	121.06	116.84	0.73	0.222	1.43	0.155	0.99	1.00	0.207	No
668	13.36	238.26	121.25	117.01	0.73	0.222	1.43	0.155	0.99	1.00	0.207	No
669	13.39	238.81	121.55	117.27	0.73	0.221	1.43	0.155	0.99	1.00	0.207	No
670	13.40	238.99	121.64	117.35	0.73	0.221	1.43	0.155	0.99	1.00	0.207	No
671	13.42	239.36	121.84	117.52	0.73	0.221	1.43	0.155	0.99	1.00	0.207	No
672	13.44	239.72	122.04	117.69	0.73	0.221	1.43	0.155	0.99	1.00	0.207	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
673	13.46	240.09	122.23	117.86	0.73	0.221	1.43	0.155	0.99	1.00	0.207	No
674	13.48	240.45	122.43	118.02	0.73	0.221	1.43	0.155	0.99	1.00	0.207	No
675	13.51	240.99	122.72	118.27	0.72	0.221	1.43	0.155	0.99	1.00	0.207	No
676	13.52	241.17	122.82	118.35	0.72	0.221	1.43	0.154	0.99	1.00	0.207	No
677	13.54	241.53	123.02	118.52	0.72	0.221	1.43	0.154	0.99	1.00	0.207	No
678	13.56	241.89	123.21	118.68	0.72	0.220	1.43	0.154	0.99	1.00	0.207	No
679	13.58	242.25	123.41	118.84	0.72	0.220	1.43	0.154	0.99	1.00	0.207	No
680	13.60	242.61	123.61	119.01	0.72	0.220	1.43	0.154	0.99	1.00	0.207	No
681	13.62	242.97	123.80	119.17	0.72	0.220	1.43	0.154	0.99	1.00	0.207	No
682	13.64	243.32	124.00	119.33	0.72	0.220	1.43	0.154	0.99	1.00	0.207	No
683	13.66	243.68	124.19	119.48	0.72	0.220	1.43	0.154	0.99	1.00	0.207	No
684	13.68	244.03	124.39	119.64	0.72	0.220	1.43	0.154	0.99	1.00	0.207	No
685	13.70	244.39	124.59	119.80	0.72	0.220	1.43	0.154	0.99	1.00	0.207	No
686	13.72	244.74	124.78	119.96	0.72	0.220	1.43	0.154	0.99	1.00	0.207	No
687	13.74	245.09	124.98	120.12	0.72	0.219	1.43	0.154	0.99	1.00	0.207	No
688	13.76	245.44	125.18	120.27	0.72	0.219	1.43	0.154	0.99	1.00	0.207	No
689	13.78	245.79	125.37	120.42	0.72	0.219	1.43	0.153	0.99	1.00	0.208	No
690	13.80	246.13	125.57	120.57	0.72	0.219	1.43	0.153	0.99	1.00	0.207	No
691	13.83	246.67	125.86	120.80	0.72	0.219	1.43	0.153	0.99	1.00	0.207	No
692	13.84	246.84	125.96	120.88	0.72	0.219	1.43	0.153	0.99	1.00	0.207	No
693	13.86	247.19	126.16	121.04	0.72	0.219	1.43	0.153	0.99	1.00	0.207	No
694	13.88	247.54	126.35	121.19	0.72	0.219	1.43	0.153	0.99	1.00	0.207	No
695	13.90	247.89	126.55	121.34	0.72	0.219	1.43	0.153	0.99	1.00	0.207	No
696	13.92	248.23	126.75	121.49	0.72	0.218	1.43	0.153	0.99	1.00	0.207	No
697	13.94	248.57	126.94	121.63	0.71	0.218	1.43	0.153	0.99	1.00	0.207	No
698	13.96	248.91	127.14	121.77	0.71	0.218	1.43	0.153	0.99	1.00	0.207	No
699	13.98	249.24	127.33	121.91	0.71	0.218	1.43	0.153	0.99	1.00	0.206	No
700	14.00	249.58	127.53	122.05	0.71	0.218	1.43	0.153	0.99	1.00	0.206	No
701	14.02	249.91	127.73	122.18	0.71	0.218	1.43	0.153	0.99	1.00	0.206	No
702	14.04	250.24	127.92	122.31	0.71	0.218	1.43	0.153	0.98	1.00	0.206	No
703	14.06	250.56	128.12	122.45	0.71	0.218	1.43	0.152	0.98	1.00	0.206	No
704	14.08	250.89	128.31	122.58	0.71	0.218	1.43	0.152	0.98	1.00	0.206	No
705	14.10	251.23	128.51	122.71	0.71	0.218	1.43	0.152	0.98	1.00	0.206	No
706	14.12	251.56	128.71	122.85	0.71	0.218	1.43	0.152	0.98	1.00	0.206	No
707	14.14	251.89	128.90	122.99	0.71	0.217	1.43	0.152	0.98	1.00	0.206	No
708	14.16	252.23	129.10	123.13	0.71	0.217	1.43	0.152	0.98	1.00	0.205	No
709	14.18	252.56	129.30	123.27	0.71	0.217	1.43	0.152	0.98	1.00	0.205	No
710	14.20	252.90	129.49	123.40	0.71	0.217	1.43	0.152	0.98	1.00	0.205	No
711	14.22	253.23	129.69	123.54	0.71	0.217	1.43	0.152	0.98	1.00	0.205	No
712	14.24	253.56	129.88	123.68	0.71	0.217	1.43	0.152	0.98	1.00	0.205	No
713	14.26	253.89	130.08	123.81	0.71	0.217	1.43	0.152	0.98	1.00	0.205	No
714	14.28	254.23	130.28	123.95	0.71	0.217	1.43	0.152	0.98	1.00	0.205	No
715	14.30	254.56	130.47	124.09	0.71	0.217	1.43	0.152	0.98	1.00	0.205	No
716	14.32	254.90	130.67	124.23	0.71	0.217	1.43	0.152	0.98	1.00	0.205	No
717	14.34	255.23	130.87	124.37	0.71	0.217	1.43	0.152	0.98	1.00	0.205	No
718	14.36	255.57	131.06	124.50	0.71	0.216	1.43	0.151	0.98	1.00	0.205	No
719	14.38	255.90	131.26	124.64	0.70	0.216	1.43	0.151	0.98	1.00	0.205	No
720	14.40	256.23	131.45	124.77	0.70	0.216	1.43	0.151	0.98	1.00	0.205	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
721	14.42	256.55	131.65	124.90	0.70	0.216	1.43	0.151	0.98	1.00	0.205	No
722	14.44	256.87	131.85	125.03	0.70	0.216	1.43	0.151	0.98	1.00	0.205	No
723	14.46	257.19	132.04	125.15	0.70	0.216	1.43	0.151	0.98	1.00	0.205	No
724	14.48	257.50	132.24	125.26	0.70	0.216	1.43	0.151	0.98	1.00	0.205	No
725	14.50	257.82	132.44	125.38	0.70	0.216	1.43	0.151	0.98	1.00	0.205	No
726	14.52	258.13	132.63	125.50	0.70	0.216	1.43	0.151	0.98	1.00	0.205	No
727	14.54	258.44	132.83	125.61	0.70	0.216	1.43	0.151	0.98	1.00	0.205	No
728	14.56	258.75	133.02	125.73	0.70	0.216	1.43	0.151	0.98	1.00	0.205	No
729	14.58	259.06	133.22	125.84	0.70	0.216	1.43	0.151	0.98	1.00	0.205	No
730	14.60	259.38	133.42	125.96	0.70	0.215	1.43	0.151	0.98	1.00	0.205	No
731	14.62	259.69	133.61	126.08	0.70	0.215	1.43	0.151	0.98	1.00	0.205	No
732	14.64	260.01	133.81	126.20	0.70	0.215	1.43	0.151	0.98	1.00	0.205	No
733	14.66	260.33	134.00	126.32	0.70	0.215	1.43	0.151	0.98	1.00	0.204	No
734	14.68	260.64	134.20	126.44	0.70	0.215	1.43	0.151	0.98	1.00	0.204	No
735	14.70	260.96	134.40	126.56	0.70	0.215	1.43	0.151	0.98	1.00	0.204	No
736	14.72	261.28	134.59	126.69	0.70	0.215	1.43	0.150	0.98	1.00	0.204	No
737	14.74	261.60	134.79	126.81	0.70	0.215	1.43	0.150	0.98	1.00	0.204	No
738	14.76	261.92	134.99	126.94	0.70	0.215	1.43	0.150	0.98	1.00	0.204	No
739	14.78	262.25	135.18	127.07	0.70	0.215	1.43	0.150	0.98	1.00	0.204	No
740	14.81	262.74	135.48	127.26	0.70	0.215	1.43	0.150	0.98	1.00	0.204	No
741	14.82	262.90	135.57	127.33	0.69	0.215	1.43	0.150	0.98	1.00	0.204	No
742	14.84	263.24	135.77	127.47	0.69	0.214	1.43	0.150	0.98	1.00	0.204	No
743	14.86	263.57	135.97	127.60	0.69	0.214	1.43	0.150	0.98	1.00	0.204	No
744	14.88	263.90	136.16	127.73	0.69	0.214	1.43	0.150	0.98	1.00	0.204	No
745	14.90	264.22	136.36	127.87	0.69	0.214	1.43	0.150	0.98	1.00	0.203	No
746	14.92	264.55	136.56	128.00	0.69	0.214	1.43	0.150	0.98	1.00	0.203	No
747	14.94	264.88	136.75	128.13	0.69	0.214	1.43	0.150	0.98	1.00	0.203	No
748	14.96	265.21	136.95	128.26	0.69	0.214	1.43	0.150	0.98	1.00	0.203	No
749	14.98	265.53	137.14	128.39	0.69	0.214	1.43	0.150	0.98	1.00	0.203	No
750	15.00	265.87	137.34	128.53	0.69	0.214	1.43	0.150	0.98	1.00	0.203	No
751	15.02	266.20	137.54	128.66	0.69	0.214	1.43	0.149	0.98	1.00	0.203	No
752	15.04	266.54	137.73	128.80	0.69	0.213	1.43	0.149	0.98	1.00	0.202	No
753	15.06	266.88	137.93	128.95	0.69	0.213	1.43	0.149	0.98	1.00	0.202	No
754	15.08	267.22	138.12	129.09	0.69	0.213	1.43	0.149	0.98	1.00	0.202	No
755	15.10	267.56	138.32	129.24	0.69	0.213	1.43	0.149	0.98	1.00	0.202	No
756	15.12	267.90	138.52	129.39	0.69	0.213	1.43	0.149	0.98	1.00	0.202	No
757	15.14	268.25	138.71	129.53	0.69	0.213	1.43	0.149	0.98	1.00	0.202	No
758	15.16	268.59	138.91	129.68	0.69	0.213	1.43	0.149	0.98	1.00	0.202	No
759	15.18	268.94	139.11	129.83	0.69	0.213	1.43	0.149	0.98	1.00	0.202	No
760	15.20	269.28	139.30	129.98	0.69	0.213	1.43	0.149	0.98	1.00	0.202	No
761	15.22	269.63	139.50	130.13	0.69	0.213	1.43	0.149	0.98	1.00	0.202	No
762	15.24	269.98	139.69	130.28	0.69	0.212	1.43	0.149	0.98	1.00	0.201	No
763	15.27	270.51	139.99	130.52	0.68	0.212	1.43	0.149	0.98	1.00	0.201	No
764	15.28	270.68	140.09	130.60	0.68	0.212	1.43	0.149	0.98	1.00	0.201	No
765	15.30	271.04	140.28	130.75	0.68	0.212	1.43	0.148	0.98	1.00	0.201	No
766	15.32	271.39	140.48	130.92	0.68	0.212	1.43	0.148	0.98	1.00	0.201	No
767	15.34	271.75	140.68	131.08	0.68	0.212	1.43	0.148	0.98	1.00	0.201	No
768	15.36	272.11	140.87	131.24	0.68	0.212	1.43	0.148	0.98	1.00	0.201	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
769	15.38	272.47	141.07	131.40	0.68	0.212	1.43	0.148	0.98	1.00	0.201	No
770	15.40	272.83	141.26	131.57	0.68	0.211	1.43	0.148	0.98	1.00	0.201	No
771	15.42	273.20	141.46	131.74	0.68	0.211	1.43	0.148	0.98	1.00	0.200	No
772	15.44	273.56	141.66	131.90	0.68	0.211	1.43	0.148	0.98	1.00	0.200	No
773	15.46	273.92	141.85	132.07	0.68	0.211	1.43	0.148	0.98	1.00	0.200	No
774	15.48	274.28	142.05	132.23	0.68	0.211	1.43	0.148	0.98	1.00	0.200	No
775	15.50	274.64	142.25	132.40	0.68	0.211	1.43	0.148	0.98	1.00	0.200	No
776	15.52	275.01	142.44	132.56	0.68	0.211	1.43	0.148	0.98	1.00	0.200	No
777	15.54	275.37	142.64	132.73	0.68	0.211	1.43	0.147	0.98	1.00	0.200	No
778	15.56	275.73	142.83	132.89	0.68	0.210	1.43	0.147	0.98	1.00	0.200	No
779	15.58	276.09	143.03	133.06	0.68	0.210	1.43	0.147	0.98	1.00	0.200	No
780	15.60	276.45	143.23	133.22	0.68	0.210	1.43	0.147	0.98	1.00	0.199	No
781	15.62	276.81	143.42	133.39	0.68	0.210	1.43	0.147	0.98	1.00	0.199	No
782	15.64	277.17	143.62	133.55	0.68	0.210	1.43	0.147	0.98	1.00	0.199	No
783	15.66	277.53	143.81	133.71	0.68	0.210	1.43	0.147	0.98	1.00	0.199	No
784	15.68	277.89	144.01	133.88	0.68	0.210	1.43	0.147	0.98	1.00	0.199	No
785	15.70	278.25	144.21	134.05	0.68	0.210	1.43	0.147	0.98	1.00	0.199	No
786	15.72	278.62	144.40	134.21	0.68	0.210	1.43	0.147	0.98	1.00	0.199	No
787	15.74	278.98	144.60	134.38	0.67	0.209	1.43	0.147	0.98	1.00	0.199	No
788	15.76	279.34	144.80	134.55	0.67	0.209	1.43	0.146	0.98	1.00	0.199	No
789	15.78	279.71	144.99	134.72	0.67	0.209	1.43	0.146	0.98	1.00	0.199	No
790	15.80	280.07	145.19	134.88	0.67	0.209	1.43	0.146	0.98	1.00	0.198	No
791	15.82	280.43	145.38	135.05	0.67	0.209	1.43	0.146	0.98	1.00	0.198	No
792	15.84	280.79	145.58	135.21	0.67	0.209	1.43	0.146	0.98	1.00	0.198	No
793	15.86	281.15	145.78	135.38	0.67	0.209	1.43	0.146	0.98	1.00	0.198	No
794	15.88	281.51	145.97	135.54	0.67	0.209	1.43	0.146	0.98	1.00	0.198	No
795	15.90	281.87	146.17	135.70	0.67	0.208	1.43	0.146	0.98	1.00	0.198	No
796	15.92	282.23	146.37	135.87	0.67	0.208	1.43	0.146	0.98	1.00	0.198	No
797	15.94	282.59	146.56	136.03	0.67	0.208	1.43	0.146	0.98	1.00	0.198	No
798	15.96	282.96	146.76	136.20	0.67	0.208	1.43	0.146	0.98	1.00	0.198	No
799	15.98	283.32	146.95	136.36	0.67	0.208	1.43	0.146	0.98	1.00	0.198	No
800	16.00	283.68	147.15	136.53	0.67	0.208	1.43	0.145	0.98	1.00	0.198	No
801	16.02	284.04	147.35	136.70	0.67	0.208	1.43	0.145	0.98	1.00	0.197	No
802	16.04	284.41	147.54	136.86	0.67	0.208	1.43	0.145	0.98	1.00	0.197	No
803	16.07	284.95	147.84	137.11	0.67	0.207	1.43	0.145	0.97	1.00	0.197	No
804	16.08	285.13	147.93	137.19	0.67	0.207	1.43	0.145	0.97	1.00	0.197	No
805	16.10	285.49	148.13	137.36	0.67	0.207	1.43	0.145	0.97	1.00	0.197	No
806	16.13	286.03	148.43	137.61	0.67	0.207	1.43	0.145	0.97	1.00	0.197	No
807	16.14	286.21	148.52	137.69	0.67	0.207	1.43	0.145	0.97	1.00	0.197	No
808	16.16	286.57	148.72	137.85	0.67	0.207	1.43	0.145	0.97	1.00	0.197	No
809	16.18	286.93	148.92	138.02	0.67	0.207	1.43	0.145	0.97	1.00	0.197	No
810	16.20	287.29	149.11	138.18	0.66	0.207	1.43	0.145	0.97	1.00	0.196	No
811	16.22	287.66	149.31	138.35	0.66	0.207	1.43	0.145	0.97	1.00	0.196	No
812	16.24	288.02	149.50	138.52	0.66	0.206	1.43	0.144	0.97	1.00	0.196	No
813	16.26	288.38	149.70	138.68	0.66	0.206	1.43	0.144	0.97	1.00	0.196	No
814	16.28	288.75	149.90	138.85	0.66	0.206	1.43	0.144	0.97	1.00	0.196	No
815	16.30	289.11	150.09	139.02	0.66	0.206	1.43	0.144	0.97	1.00	0.196	No
816	16.32	289.47	150.29	139.19	0.66	0.206	1.43	0.144	0.97	1.00	0.195	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
817	16.34	289.84	150.49	139.35	0.66	0.206	1.43	0.144	0.97	1.00	0.195	No
818	16.36	290.20	150.68	139.52	0.66	0.206	1.43	0.144	0.97	1.00	0.195	No
819	16.38	290.57	150.88	139.69	0.66	0.206	1.43	0.144	0.97	1.00	0.195	No
820	16.40	290.93	151.07	139.86	0.66	0.205	1.43	0.144	0.97	1.00	0.195	No
821	16.43	291.48	151.37	140.11	0.66	0.205	1.43	0.144	0.97	1.00	0.195	No
822	16.44	291.66	151.47	140.19	0.66	0.205	1.43	0.144	0.97	1.00	0.195	No
823	16.46	292.02	151.66	140.36	0.66	0.205	1.43	0.144	0.97	1.00	0.195	No
824	16.48	292.39	151.86	140.53	0.66	0.205	1.43	0.143	0.97	1.00	0.195	No
825	16.50	292.76	152.06	140.70	0.66	0.205	1.43	0.143	0.97	1.00	0.194	No
826	16.52	293.12	152.25	140.87	0.66	0.205	1.43	0.143	0.97	1.00	0.194	No
827	16.54	293.49	152.45	141.04	0.66	0.205	1.43	0.143	0.97	1.00	0.194	No
828	16.57	294.04	152.74	141.30	0.66	0.204	1.43	0.143	0.97	1.00	0.194	No
829	16.58	294.23	152.84	141.39	0.66	0.204	1.43	0.143	0.97	1.00	0.194	No
830	16.60	294.60	153.04	141.56	0.66	0.204	1.43	0.143	0.97	1.00	0.194	No
831	16.63	295.15	153.33	141.82	0.66	0.204	1.43	0.143	0.97	1.00	0.194	No
832	16.64	295.33	153.43	141.90	0.66	0.204	1.43	0.143	0.97	1.00	0.194	No
833	16.66	295.70	153.62	142.07	0.66	0.204	1.43	0.143	0.97	1.00	0.194	No
834	16.68	296.06	153.82	142.24	0.65	0.204	1.43	0.143	0.97	1.00	0.194	No
835	16.70	296.43	154.02	142.41	0.65	0.204	1.43	0.143	0.97	1.00	0.194	No
836	16.72	296.79	154.21	142.58	0.65	0.203	1.43	0.142	0.97	1.00	0.194	No
837	16.74	297.16	154.41	142.75	0.65	0.203	1.43	0.142	0.97	1.00	0.194	No
838	16.76	297.52	154.61	142.91	0.65	0.203	1.43	0.142	0.97	1.00	0.194	No
839	16.79	298.06	154.90	143.16	0.65	0.203	1.43	0.142	0.97	1.00	0.194	No
840	16.80	298.24	155.00	143.24	0.65	0.203	1.43	0.142	0.97	1.00	0.194	No
841	16.83	298.78	155.29	143.49	0.65	0.203	1.43	0.142	0.97	1.00	0.194	No
842	16.84	298.96	155.39	143.57	0.65	0.203	1.43	0.142	0.97	1.00	0.194	No
843	16.86	299.32	155.59	143.73	0.65	0.203	1.43	0.142	0.97	1.00	0.194	No
844	16.88	299.67	155.78	143.89	0.65	0.203	1.43	0.142	0.97	1.00	0.194	No
845	16.90	300.02	155.98	144.04	0.65	0.202	1.43	0.142	0.97	1.00	0.194	No
846	16.92	300.37	156.18	144.20	0.65	0.202	1.43	0.142	0.97	1.00	0.194	No
847	16.94	300.71	156.37	144.34	0.65	0.202	1.43	0.142	0.97	1.00	0.194	No
848	16.96	301.06	156.57	144.49	0.65	0.202	1.43	0.141	0.97	1.00	0.194	No
849	16.98	301.40	156.76	144.63	0.65	0.202	1.43	0.141	0.97	1.00	0.194	No
850	17.00	301.74	156.96	144.78	0.65	0.202	1.43	0.141	0.97	1.00	0.194	No
851	17.03	302.24	157.25	144.99	0.65	0.202	1.43	0.141	0.97	1.00	0.193	No
852	17.04	302.41	157.35	145.05	0.65	0.202	1.43	0.141	0.97	1.00	0.193	No
853	17.06	302.74	157.55	145.19	0.65	0.202	1.43	0.141	0.97	1.00	0.193	No
854	17.08	303.07	157.74	145.33	0.65	0.202	1.43	0.141	0.97	1.00	0.193	No
855	17.10	303.40	157.94	145.46	0.65	0.201	1.43	0.141	0.97	1.00	0.193	No
856	17.12	303.73	158.14	145.59	0.65	0.201	1.43	0.141	0.97	1.00	0.193	No
857	17.14	304.06	158.33	145.72	0.65	0.201	1.43	0.141	0.97	1.00	0.193	No
858	17.16	304.38	158.53	145.85	0.64	0.201	1.43	0.141	0.97	1.00	0.193	No
859	17.19	304.87	158.82	146.05	0.64	0.201	1.43	0.141	0.97	1.00	0.193	No
860	17.20	305.03	158.92	146.11	0.64	0.201	1.43	0.141	0.97	1.00	0.193	No
861	17.23	305.52	159.22	146.31	0.64	0.201	1.43	0.141	0.97	1.00	0.193	No
862	17.24	305.69	159.31	146.37	0.64	0.201	1.43	0.141	0.97	1.00	0.193	No
863	17.26	306.01	159.51	146.50	0.64	0.201	1.43	0.141	0.97	1.00	0.193	No
864	17.28	306.33	159.71	146.63	0.64	0.201	1.43	0.140	0.97	1.00	0.193	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
865	17.31	306.82	160.00	146.82	0.64	0.201	1.43	0.140	0.97	1.00	0.193	No
866	17.32	306.98	160.10	146.88	0.64	0.200	1.43	0.140	0.97	1.00	0.193	No
867	17.34	307.31	160.30	147.01	0.64	0.200	1.43	0.140	0.97	1.00	0.192	No
868	17.36	307.63	160.49	147.14	0.64	0.200	1.43	0.140	0.97	1.00	0.192	No
869	17.38	307.95	160.69	147.26	0.64	0.200	1.43	0.140	0.97	1.00	0.192	No
870	17.40	308.27	160.88	147.39	0.64	0.200	1.43	0.140	0.97	1.00	0.192	No
871	17.42	308.59	161.08	147.51	0.64	0.200	1.43	0.140	0.97	1.00	0.192	No
872	17.44	308.91	161.28	147.63	0.64	0.200	1.43	0.140	0.97	1.00	0.192	No
873	17.46	309.22	161.47	147.75	0.64	0.200	1.43	0.140	0.97	1.00	0.192	No
874	17.48	309.54	161.67	147.87	0.64	0.200	1.43	0.140	0.97	1.00	0.192	No
875	17.50	309.85	161.87	147.98	0.64	0.200	1.43	0.140	0.97	1.00	0.192	No
876	17.52	310.16	162.06	148.10	0.64	0.200	1.43	0.140	0.97	1.00	0.192	No
877	17.54	310.47	162.26	148.22	0.64	0.200	1.43	0.140	0.97	1.00	0.192	No
878	17.56	310.79	162.45	148.33	0.64	0.199	1.43	0.140	0.97	1.00	0.192	No
879	17.58	311.10	162.65	148.45	0.64	0.199	1.43	0.140	0.97	1.00	0.192	No
880	17.60	311.41	162.85	148.56	0.64	0.199	1.43	0.139	0.97	1.00	0.192	No
881	17.62	311.72	163.04	148.68	0.64	0.199	1.43	0.139	0.97	1.00	0.191	No
882	17.64	312.03	163.24	148.80	0.64	0.199	1.43	0.139	0.97	1.00	0.191	No
883	17.66	312.35	163.43	148.92	0.63	0.199	1.43	0.139	0.97	1.00	0.191	No
884	17.68	312.66	163.63	149.03	0.63	0.199	1.43	0.139	0.97	1.00	0.191	No
885	17.70	312.98	163.83	149.15	0.63	0.199	1.43	0.139	0.97	1.00	0.191	No
886	17.72	313.30	164.02	149.27	0.63	0.199	1.43	0.139	0.97	1.00	0.191	No
887	17.74	313.61	164.22	149.40	0.63	0.199	1.43	0.139	0.97	1.00	0.191	No
888	17.76	313.94	164.42	149.52	0.63	0.199	1.43	0.139	0.97	1.00	0.191	No
889	17.78	314.27	164.61	149.65	0.63	0.199	1.43	0.139	0.97	1.00	0.190	No
890	17.80	314.60	164.81	149.79	0.63	0.198	1.43	0.139	0.97	1.00	0.190	No
891	17.82	314.93	165.00	149.93	0.63	0.198	1.43	0.139	0.97	1.00	0.190	No
892	17.84	315.27	165.20	150.07	0.63	0.198	1.43	0.139	0.97	1.00	0.190	No
893	17.86	315.60	165.40	150.21	0.63	0.198	1.43	0.139	0.97	1.00	0.190	No
894	17.88	315.93	165.59	150.34	0.63	0.198	1.43	0.139	0.97	1.00	0.190	No
895	17.90	316.26	165.79	150.47	0.63	0.198	1.43	0.139	0.97	1.00	0.190	No
896	17.92	316.59	165.99	150.60	0.63	0.198	1.43	0.138	0.97	1.00	0.190	No
897	17.94	316.91	166.18	150.73	0.63	0.198	1.43	0.138	0.97	1.00	0.190	No
898	17.96	317.23	166.38	150.86	0.63	0.198	1.43	0.138	0.97	1.00	0.190	No
899	17.98	317.55	166.57	150.98	0.63	0.198	1.43	0.138	0.97	1.00	0.190	No
900	18.00	317.88	166.77	151.11	0.63	0.198	1.43	0.138	0.97	1.00	0.190	No
901	18.02	318.20	166.97	151.23	0.63	0.197	1.43	0.138	0.97	1.00	0.190	No
902	18.04	318.52	167.16	151.35	0.63	0.197	1.43	0.138	0.97	1.00	0.190	No
903	18.06	318.84	167.36	151.48	0.63	0.197	1.43	0.138	0.97	1.00	0.190	No
904	18.08	319.16	167.55	151.61	0.63	0.197	1.43	0.138	0.97	1.00	0.190	No
905	18.10	319.49	167.75	151.74	0.63	0.197	1.43	0.138	0.97	1.00	0.190	No
906	18.12	319.81	167.95	151.86	0.63	0.197	1.43	0.138	0.97	1.00	0.190	No
907	18.14	320.13	168.14	151.99	0.63	0.197	1.43	0.138	0.97	1.00	0.190	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition

Abbreviations

Depth: Depth from free surface, at which CPT was performed (m)
σ_v: Total overburden pressure at test point (kPa)
u_0: Water pressure at test point (kPa)
σ_v': Effective overburden pressure based on GWT during earthquake (kPa)
r_d: Nonlinear shear mass factor
CSR: Cyclic Stress Ratio
MSF: Magnitude Scaling Factor
CSR_{eq}: CSR adjusted for M=7.5
K_σ: Effective overburden stress factor
CSR^*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1	0.03	6.57	0.00	1.55	0.51	1.70	94.22	0.00	94.22	4.000	No	No	2.00
2	0.04	7.82	0.00	1.52	0.42	1.70	142.13	0.00	142.13	4.000	No	No	2.00
3	0.07	6.99	0.00	1.56	0.48	1.70	109.24	0.00	109.24	4.000	No	No	2.00
4	0.08	6.25	0.00	1.60	0.50	1.70	100.13	0.00	100.13	4.000	No	No	2.00
5	0.10	6.27	0.00	1.64	0.49	1.70	105.00	0.00	105.00	4.000	No	No	2.00
6	0.12	5.84	0.00	1.71	0.48	1.70	110.14	0.00	110.14	4.000	Yes	No	2.00
7	0.14	4.65	14.92	1.90	0.50	1.70	78.78	21.05	99.82	4.000	Yes	No	2.00
8	0.17	3.31	29.99	2.09	0.52	1.70	44.98	44.38	89.36	4.000	Yes	No	2.00
9	0.18	2.45	45.02	2.28	0.50	1.70	42.80	55.09	97.89	4.000	Yes	No	2.00
10	0.20	2.07	50.43	2.34	0.52	1.70	35.50	55.58	91.08	4.000	Yes	No	2.00
11	0.22	1.62	64.76	2.52	0.54	1.70	25.77	57.07	82.84	4.000	Yes	No	2.00
12	0.24	1.26	79.47	2.71	0.55	1.70	20.21	0.00	20.21	4.000	Yes	Yes	2.00
13	0.26	1.09	89.81	2.84	0.56	1.70	17.58	0.00	17.58	4.000	Yes	Yes	2.00
14	0.28	1.03	94.73	2.90	0.56	1.70	17.26	0.00	17.26	4.000	Yes	Yes	2.00
15	0.30	1.04	96.25	2.92	0.56	1.70	17.10	0.00	17.10	4.000	No	Yes	2.00
16	0.32	1.05	98.73	2.95	0.55	1.70	18.15	0.00	18.15	4.000	No	Yes	2.00
17	0.34	1.06	100.00	2.98	0.55	1.70	17.55	0.00	17.55	4.000	No	Yes	2.00
18	0.36	1.02	100.00	3.03	0.55	1.70	17.53	0.00	17.53	4.000	No	Yes	2.00
19	0.38	0.99	100.00	3.07	0.56	1.70	16.52	0.00	16.52	4.000	No	Yes	2.00
20	0.40	0.95	100.00	3.12	0.56	1.70	16.29	0.00	16.29	4.000	No	Yes	2.00
21	0.42	0.92	100.00	3.17	0.56	1.70	15.59	0.00	15.59	4.000	No	Yes	2.00
22	0.44	0.89	100.00	3.21	0.56	1.70	15.25	0.00	15.25	4.000	No	Yes	2.00
23	0.46	0.88	100.00	3.23	0.56	1.70	14.79	0.00	14.79	4.000	No	Yes	2.00
24	0.48	0.86	100.00	3.25	0.56	1.70	14.80	0.00	14.80	4.000	No	Yes	2.00
25	0.50	0.84	100.00	3.26	0.57	1.70	14.27	0.00	14.27	4.000	No	Yes	2.00
26	0.52	0.80	100.00	3.29	0.57	1.70	13.81	0.00	13.81	4.000	No	Yes	2.00
27	0.54	0.77	100.00	3.31	0.57	1.70	13.01	0.00	13.01	4.000	No	Yes	2.00
28	0.56	0.75	100.00	3.32	0.57	1.70	12.67	0.00	12.67	4.000	No	Yes	2.00
29	0.58	0.74	100.00	3.32	0.57	1.70	12.73	0.00	12.73	4.000	No	Yes	2.00
30	0.60	0.74	100.00	3.31	0.57	1.70	12.43	0.00	12.43	4.000	No	Yes	2.00
31	0.62	0.73	100.00	3.31	0.57	1.70	12.40	0.00	12.40	4.000	No	Yes	2.00
32	0.64	0.72	100.00	3.31	0.57	1.70	12.22	0.00	12.22	4.000	No	Yes	2.00
33	0.66	0.73	100.00	3.30	0.57	1.70	12.15	0.00	12.15	4.000	No	Yes	2.00
34	0.68	0.73	100.00	3.28	0.57	1.70	12.47	0.00	12.47	4.000	No	Yes	2.00
35	0.70	0.75	100.00	3.25	0.57	1.70	12.43	0.00	12.43	4.000	No	Yes	2.00
36	0.72	0.76	100.00	3.24	0.57	1.70	12.92	0.00	12.92	4.000	No	Yes	2.00
37	0.74	0.78	100.00	3.22	0.57	1.70	13.32	0.00	13.32	4.000	No	Yes	2.00
38	0.76	0.80	100.00	3.20	0.57	1.70	13.29	0.00	13.29	4.000	No	Yes	2.00
39	0.78	0.82	100.00	3.18	0.57	1.70	14.00	0.00	14.00	4.000	No	Yes	2.00
40	0.80	0.83	100.00	3.16	0.57	1.70	14.25	0.00	14.25	4.000	No	Yes	2.00
41	0.82	0.84	100.00	3.14	0.57	1.70	14.02	0.00	14.02	4.000	No	Yes	2.00
42	0.84	0.84	100.00	3.14	0.57	1.70	14.17	0.00	14.17	4.000	No	Yes	2.00
43	0.86	0.85	100.00	3.12	0.57	1.70	14.21	0.00	14.21	4.000	No	Yes	2.00
44	0.88	0.88	100.00	3.11	0.56	1.70	14.86	0.00	14.86	4.000	No	Yes	2.00
45	0.90	0.91	100.00	3.10	0.56	1.70	15.29	0.00	15.29	4.000	No	Yes	2.00
46	0.92	0.96	100.00	3.08	0.56	1.70	15.59	0.00	15.59	4.000	No	Yes	2.00
47	0.94	1.01	100.00	3.05	0.55	1.70	17.38	0.00	17.38	4.000	No	Yes	2.00
48	0.97	1.07	100.00	3.01	0.55	1.70	18.05	0.00	18.05	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
49	0.98	1.11	100.00	3.00	0.55	1.70	18.64	0.00	18.64	4.000	No	Yes	2.00
50	1.01	1.14	100.00	2.99	0.55	1.70	19.07	0.00	19.07	4.000	No	Yes	2.00
51	1.02	1.20	100.00	2.97	0.55	1.70	19.85	0.00	19.85	4.000	No	Yes	2.00
52	1.04	1.28	98.18	2.94	0.54	1.70	21.70	0.00	21.70	4.000	No	Yes	2.00
53	1.06	1.36	96.22	2.92	0.54	1.70	23.00	0.00	23.00	4.000	No	Yes	2.00
54	1.08	1.39	95.73	2.91	0.53	1.70	23.58	0.00	23.58	4.000	No	Yes	2.00
55	1.10	1.39	96.72	2.92	0.53	1.70	23.50	0.00	23.50	4.000	No	Yes	2.00
56	1.13	1.38	98.16	2.94	0.54	1.70	23.14	0.00	23.14	4.000	No	Yes	2.00
57	1.14	1.38	99.31	2.95	0.54	1.70	23.09	0.00	23.09	4.000	No	Yes	2.00
58	1.16	1.38	100.00	2.97	0.53	1.70	23.36	0.00	23.36	4.000	No	Yes	2.00
59	1.19	1.38	100.00	2.98	0.53	1.70	23.27	0.00	23.27	4.000	No	Yes	2.00
60	1.20	1.37	100.00	3.00	0.54	1.70	22.75	0.00	22.75	4.000	No	Yes	2.00
61	1.22	1.34	100.00	3.01	0.54	1.70	22.82	0.00	22.82	4.000	No	Yes	2.00
62	1.24	1.32	100.00	3.02	0.54	1.70	22.17	0.00	22.17	4.000	No	Yes	2.00
63	1.26	1.29	100.00	3.04	0.54	1.70	21.65	0.00	21.65	4.000	No	Yes	2.00
64	1.28	1.25	100.00	3.06	0.54	1.70	20.92	0.00	20.92	4.000	No	Yes	2.00
65	1.30	1.22	100.00	3.07	0.54	1.70	20.51	0.00	20.51	4.000	No	Yes	2.00
66	1.32	1.20	100.00	3.08	0.55	1.70	19.98	0.00	19.98	4.000	No	Yes	2.00
67	1.34	1.18	100.00	3.08	0.55	1.70	19.69	0.00	19.69	4.000	No	Yes	2.00
68	1.36	1.18	100.00	3.08	0.55	1.70	19.71	0.00	19.71	4.000	No	Yes	2.00
69	1.38	1.19	100.00	3.07	0.55	1.70	19.88	0.00	19.88	4.000	No	Yes	2.00
70	1.40	1.20	100.00	3.06	0.55	1.70	19.98	0.00	19.98	4.000	No	Yes	2.00
71	1.42	1.20	100.00	3.04	0.55	1.70	20.12	0.00	20.12	4.000	No	Yes	2.00
72	1.44	1.20	100.00	3.03	0.55	1.70	19.94	0.00	19.94	4.000	No	Yes	2.00
73	1.46	1.18	100.00	3.03	0.55	1.70	19.81	0.00	19.81	4.000	No	Yes	2.00
74	1.48	1.16	100.00	3.04	0.55	1.70	19.20	0.00	19.20	4.000	No	Yes	2.00
75	1.50	1.13	100.00	3.05	0.55	1.70	18.87	0.00	18.87	4.000	No	Yes	2.00
76	1.52	1.13	100.00	3.05	0.55	1.70	18.66	0.00	18.66	4.000	No	Yes	2.00
77	1.54	1.13	100.00	3.04	0.55	1.70	18.92	0.00	18.92	4.000	No	Yes	2.00
78	1.56	1.15	100.00	3.03	0.55	1.70	18.82	0.00	18.82	4.000	No	Yes	2.00
79	1.58	1.16	100.00	3.02	0.55	1.70	19.47	0.00	19.47	4.000	No	Yes	2.00
80	1.60	1.18	100.00	3.01	0.55	1.70	19.61	0.00	19.61	4.000	No	Yes	2.00
81	1.62	1.18	100.00	3.00	0.55	1.70	19.74	0.00	19.74	4.000	No	Yes	2.00
82	1.64	1.16	100.00	3.01	0.55	1.70	19.37	0.00	19.37	4.000	No	Yes	2.00
83	1.66	1.12	100.00	3.03	0.55	1.70	18.82	0.00	18.82	4.000	No	Yes	2.00
84	1.68	1.08	100.00	3.06	0.55	1.70	17.94	0.00	17.94	4.000	No	Yes	2.00
85	1.70	1.03	100.00	3.08	0.56	1.70	17.18	0.00	17.18	4.000	No	Yes	2.00
86	1.72	0.99	100.00	3.10	0.56	1.70	16.27	0.00	16.27	4.000	No	Yes	2.00
87	1.74	0.94	100.00	3.11	0.56	1.70	15.63	0.00	15.63	4.000	No	Yes	2.00
88	1.76	0.92	100.00	3.12	0.56	1.70	14.99	0.00	14.99	4.000	No	Yes	2.00
89	1.78	0.91	100.00	3.11	0.56	1.70	15.01	0.00	15.01	4.000	No	Yes	2.00
90	1.80	0.91	100.00	3.09	0.56	1.70	14.96	0.00	14.96	4.000	No	Yes	2.00
91	1.82	0.90	100.00	3.09	0.56	1.70	15.07	0.00	15.07	4.000	No	Yes	2.00
92	1.84	0.89	100.00	3.09	0.57	1.70	14.51	0.00	14.51	4.000	No	Yes	2.00
93	1.86	0.84	100.00	3.11	0.57	1.70	14.11	0.00	14.11	4.000	No	Yes	2.00
94	1.88	0.78	100.00	3.12	0.57	1.70	12.81	0.00	12.81	4.000	No	Yes	2.00
95	1.90	0.73	100.00	3.15	0.57	1.70	11.91	0.00	11.91	4.000	No	Yes	2.00
96	1.92	0.68	100.00	3.17	0.58	1.70	11.41	0.00	11.41	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
97	1.94	0.63	100.00	3.21	0.58	1.70	10.39	0.00	10.39	4.000	No	Yes	2.00
98	1.96	0.57	100.00	3.26	0.59	1.70	9.30	0.00	9.30	4.000	No	Yes	2.00
99	1.98	0.51	100.00	3.30	0.59	1.70	8.05	0.00	8.05	4.000	No	Yes	2.00
100	2.01	0.48	100.00	3.31	0.59	1.70	7.54	0.00	7.54	4.000	No	Yes	2.00
101	2.02	0.48	100.00	3.27	0.59	1.70	7.61	0.00	7.61	4.000	No	Yes	2.00
102	2.04	0.48	100.00	3.20	0.59	1.70	7.73	0.00	7.73	4.000	No	Yes	2.00
103	2.06	0.48	100.00	3.13	0.59	1.70	7.84	0.00	7.84	4.000	No	Yes	2.00
104	2.08	0.48	100.00	3.07	0.59	1.70	7.61	0.00	7.61	4.000	No	Yes	2.00
105	2.10	0.47	100.00	3.02	0.59	1.70	7.56	0.00	7.56	4.000	No	Yes	2.00
106	2.12	0.49	100.00	2.98	0.59	1.70	7.52	0.00	7.52	4.000	Yes	Yes	2.00
107	2.14	0.50	97.47	2.93	0.59	1.70	8.19	0.00	8.19	4.000	Yes	Yes	2.00
108	2.16	0.53	93.91	2.89	0.59	1.70	8.50	0.00	8.50	4.000	Yes	Yes	2.00
109	2.18	0.63	85.05	2.78	0.59	1.70	9.01	0.00	9.01	4.000	Yes	Yes	2.00
110	2.21	0.79	73.61	2.63	0.58	1.70	12.99	0.00	12.99	4.000	Yes	Yes	2.00
111	2.22	0.97	62.91	2.50	0.57	1.70	16.27	53.95	70.22	4.000	Yes	No	2.00
112	2.24	1.10	59.28	2.45	0.57	1.70	18.34	53.68	72.02	4.000	Yes	No	2.00
113	2.26	1.18	62.27	2.49	0.56	1.70	19.55	54.74	74.29	4.000	Yes	No	2.00
114	2.28	1.24	68.00	2.56	0.55	1.70	20.65	56.26	76.91	4.000	Yes	No	2.00
115	2.30	1.30	73.34	2.63	0.55	1.70	21.72	0.00	21.72	4.000	Yes	Yes	2.00
116	2.32	1.34	77.90	2.69	0.54	1.70	22.46	0.00	22.46	4.000	Yes	Yes	2.00
117	2.34	1.36	82.71	2.75	0.54	1.70	22.62	0.00	22.62	4.000	Yes	Yes	2.00
118	2.36	1.38	87.27	2.80	0.54	1.70	23.04	0.00	23.04	4.000	Yes	Yes	2.00
119	2.38	1.39	91.10	2.85	0.54	1.70	23.20	0.00	23.20	4.000	Yes	Yes	2.00
120	2.40	1.39	93.54	2.88	0.54	1.70	23.03	0.00	23.03	4.000	Yes	Yes	2.00
121	2.42	1.36	96.07	2.91	0.54	1.70	23.14	0.00	23.14	4.000	Yes	Yes	2.00
122	2.44	1.33	98.26	2.94	0.54	1.70	21.99	0.00	21.99	4.000	Yes	Yes	2.00
123	2.46	1.28	100.00	2.97	0.54	1.70	21.30	0.00	21.30	4.000	Yes	Yes	2.00
124	2.48	1.26	100.00	2.98	0.54	1.70	20.74	0.00	20.74	4.000	No	Yes	2.00
125	2.50	1.25	100.00	2.98	0.54	1.70	20.72	0.00	20.72	4.000	No	Yes	2.00
126	2.52	1.26	100.00	2.96	0.54	1.70	21.01	0.00	21.01	4.000	No	Yes	2.00
127	2.54	1.28	99.03	2.95	0.54	1.70	21.28	0.00	21.28	4.000	No	Yes	2.00
128	2.56	1.29	98.41	2.94	0.54	1.70	21.53	0.00	21.53	4.000	No	Yes	2.00
129	2.58	1.30	97.90	2.94	0.54	1.70	21.71	0.00	21.71	4.000	No	Yes	2.00
130	2.60	1.31	96.95	2.92	0.54	1.70	21.61	0.00	21.61	4.000	No	Yes	2.00
131	2.62	1.32	96.62	2.92	0.54	1.69	22.10	0.00	22.10	4.000	No	Yes	2.00
132	2.64	1.31	96.91	2.92	0.54	1.69	21.81	0.00	21.81	4.000	No	Yes	2.00
133	2.66	1.30	98.15	2.94	0.54	1.69	21.36	0.00	21.36	4.000	No	Yes	2.00
134	2.68	1.30	98.45	2.94	0.54	1.69	21.08	0.00	21.08	4.000	No	Yes	2.00
135	2.70	1.32	97.85	2.94	0.54	1.68	21.66	0.00	21.66	4.000	No	Yes	2.00
136	2.72	1.36	96.10	2.91	0.54	1.68	21.97	0.00	21.97	4.000	No	Yes	2.00
137	2.74	1.38	95.18	2.90	0.54	1.67	22.74	0.00	22.74	4.000	No	Yes	2.00
138	2.76	1.39	94.58	2.89	0.54	1.67	22.53	0.00	22.53	4.000	No	Yes	2.00
139	2.78	1.39	94.26	2.89	0.54	1.66	22.53	0.00	22.53	4.000	No	Yes	2.00
140	2.80	1.40	93.25	2.88	0.54	1.66	22.64	0.00	22.64	4.000	No	Yes	2.00
141	2.82	1.37	93.01	2.88	0.54	1.65	22.65	0.00	22.65	4.000	No	Yes	2.00
142	2.84	1.29	95.59	2.91	0.54	1.66	21.24	0.00	21.24	4.000	No	Yes	2.00
143	2.86	1.16	100.00	2.97	0.55	1.66	18.77	0.00	18.77	4.000	No	Yes	2.00
144	2.88	1.05	100.00	3.05	0.56	1.67	16.90	0.00	16.90	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
145	2.92	0.97	100.00	3.11	0.56	1.67	15.67	0.00	15.67	4.000	No	Yes	2.00
146	2.92	0.91	100.00	3.15	0.56	1.68	14.65	0.00	14.65	4.000	No	Yes	2.00
147	2.94	0.87	100.00	3.19	0.57	1.68	14.06	0.00	14.06	4.000	No	Yes	2.00
148	2.97	0.81	100.00	3.22	0.57	1.67	13.28	0.00	13.28	4.000	No	Yes	2.00
149	2.99	0.76	100.00	3.23	0.57	1.68	11.88	0.00	11.88	4.000	No	Yes	2.00
150	3.00	0.75	100.00	3.21	0.58	1.68	11.57	0.00	11.57	4.000	No	Yes	2.00
151	3.02	0.82	100.00	3.10	0.57	1.67	12.68	0.00	12.68	4.000	No	Yes	2.00
152	3.05	0.89	100.00	2.98	0.56	1.65	14.72	0.00	14.72	4.000	No	Yes	2.00
153	3.06	0.94	93.56	2.88	0.56	1.65	14.98	0.00	14.98	4.000	No	Yes	2.00
154	3.08	0.93	91.52	2.86	0.57	1.65	14.66	0.00	14.66	4.000	No	Yes	2.00
155	3.10	0.95	90.42	2.84	0.57	1.65	14.38	0.00	14.38	4.000	No	Yes	2.00
156	3.12	1.02	88.82	2.82	0.56	1.64	16.12	0.00	16.12	4.000	No	Yes	2.00
157	3.14	1.10	87.16	2.80	0.56	1.63	17.90	0.00	17.90	4.000	No	Yes	2.00
158	3.16	1.15	86.54	2.79	0.56	1.62	17.90	0.00	17.90	4.000	No	Yes	2.00
159	3.18	1.16	87.95	2.81	0.55	1.62	18.32	0.00	18.32	4.000	No	Yes	2.00
160	3.20	1.16	89.80	2.83	0.55	1.61	18.38	0.00	18.38	4.000	No	Yes	2.00
161	3.22	1.13	92.93	2.87	0.55	1.61	17.84	0.00	17.84	4.000	No	Yes	2.00
162	3.24	1.09	95.86	2.91	0.56	1.61	16.88	0.00	16.88	4.000	No	Yes	2.00
163	3.26	1.06	98.74	2.95	0.56	1.61	16.42	0.00	16.42	4.000	No	Yes	2.00
164	3.28	1.06	99.64	2.96	0.56	1.61	16.21	0.00	16.21	4.000	No	Yes	2.00
165	3.30	1.08	99.54	2.96	0.56	1.60	16.80	0.00	16.80	4.000	No	Yes	2.00
166	3.32	1.11	98.67	2.95	0.55	1.60	17.47	0.00	17.47	4.000	No	Yes	2.00
167	3.34	1.15	97.03	2.93	0.55	1.59	17.54	0.00	17.54	4.000	No	Yes	2.00
168	3.36	1.19	94.94	2.90	0.55	1.59	18.45	0.00	18.45	4.000	No	Yes	2.00
169	3.38	1.25	92.35	2.87	0.55	1.58	19.28	0.00	19.28	4.000	No	Yes	2.00
170	3.40	1.30	90.50	2.84	0.55	1.58	19.80	0.00	19.80	4.000	No	Yes	2.00
171	3.42	1.34	89.47	2.83	0.55	1.57	20.69	0.00	20.69	4.000	No	Yes	2.00
172	3.44	1.36	89.39	2.83	0.55	1.57	20.92	0.00	20.92	4.000	No	Yes	2.00
173	3.46	1.34	90.97	2.85	0.55	1.56	20.73	0.00	20.73	4.000	No	Yes	2.00
174	3.49	1.30	93.45	2.88	0.55	1.56	19.69	0.00	19.69	4.000	No	Yes	2.00
175	3.50	1.27	94.99	2.90	0.55	1.56	19.07	0.00	19.07	4.000	No	Yes	2.00
176	3.52	1.27	95.86	2.91	0.55	1.56	19.47	0.00	19.47	4.000	No	Yes	2.00
177	3.54	1.27	96.78	2.92	0.55	1.55	19.31	0.00	19.31	4.000	No	Yes	2.00
178	3.56	1.25	98.81	2.95	0.55	1.55	18.95	0.00	18.95	4.000	No	Yes	2.00
179	3.58	1.23	100.00	2.97	0.55	1.55	18.63	0.00	18.63	4.000	No	Yes	2.00
180	3.60	1.22	100.00	2.98	0.55	1.55	18.38	0.00	18.38	4.000	No	Yes	2.00
181	3.62	1.22	100.00	2.97	0.55	1.55	18.23	0.00	18.23	4.000	No	Yes	2.00
182	3.64	1.25	99.65	2.96	0.55	1.54	18.63	0.00	18.63	4.000	No	Yes	2.00
183	3.66	1.29	97.03	2.93	0.55	1.54	19.17	0.00	19.17	4.000	No	Yes	2.00
184	3.68	1.33	94.07	2.89	0.55	1.53	19.95	0.00	19.95	4.000	No	Yes	2.00
185	3.70	1.36	91.67	2.86	0.55	1.53	20.31	0.00	20.31	4.000	No	Yes	2.00
186	3.72	1.37	91.04	2.85	0.55	1.52	20.40	0.00	20.40	4.000	No	Yes	2.00
187	3.74	1.36	91.55	2.86	0.55	1.52	20.11	0.00	20.11	4.000	No	Yes	2.00
188	3.76	1.35	92.23	2.87	0.55	1.52	19.80	0.00	19.80	4.000	No	Yes	2.00
189	3.78	1.34	92.80	2.87	0.55	1.52	19.76	0.00	19.76	4.000	No	Yes	2.00
190	3.80	1.33	94.00	2.89	0.55	1.52	19.71	0.00	19.71	4.000	No	Yes	2.00
191	3.82	1.30	96.17	2.91	0.55	1.51	19.22	0.00	19.22	4.000	No	Yes	2.00
192	3.84	1.26	99.07	2.95	0.55	1.51	18.54	0.00	18.54	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
193	3.86	1.22	100.00	2.98	0.55	1.51	17.72	0.00	17.72	4.000	No	Yes	2.00
194	3.88	1.20	100.00	2.99	0.56	1.51	17.14	0.00	17.14	4.000	No	Yes	2.00
195	3.90	1.19	100.00	2.98	0.55	1.51	17.52	0.00	17.52	4.000	No	Yes	2.00
196	3.92	1.19	100.00	2.97	0.55	1.51	17.38	0.00	17.38	4.000	No	Yes	2.00
197	3.94	1.16	100.00	2.98	0.56	1.50	17.09	0.00	17.09	4.000	No	Yes	2.00
198	3.96	1.12	100.00	2.99	0.56	1.51	16.15	0.00	16.15	4.000	No	Yes	2.00
199	3.98	1.08	100.00	3.01	0.56	1.50	15.66	0.00	15.66	4.000	No	Yes	2.00
200	4.00	1.05	100.00	3.03	0.56	1.50	15.10	0.00	15.10	4.000	No	Yes	2.00
201	4.02	1.01	100.00	3.06	0.56	1.50	14.83	0.00	14.83	4.000	No	Yes	2.00
202	4.05	0.98	100.00	3.09	0.57	1.50	13.89	0.00	13.89	4.000	No	Yes	2.00
203	4.06	0.94	100.00	3.11	0.57	1.50	13.54	0.00	13.54	4.000	No	Yes	2.00
204	4.08	0.93	100.00	3.12	0.57	1.50	13.14	0.00	13.14	4.000	No	Yes	2.00
205	4.10	0.93	100.00	3.11	0.57	1.50	13.37	0.00	13.37	4.000	No	Yes	2.00
206	4.12	0.95	100.00	3.09	0.57	1.49	13.50	0.00	13.50	4.000	No	Yes	2.00
207	4.14	0.97	100.00	3.07	0.57	1.49	14.00	0.00	14.00	4.000	No	Yes	2.00
208	4.16	1.00	100.00	3.05	0.57	1.49	14.20	0.00	14.20	4.000	No	Yes	2.00
209	4.18	1.02	100.00	3.03	0.57	1.48	14.46	0.00	14.46	4.000	No	Yes	2.00
210	4.20	1.04	100.00	3.01	0.56	1.48	14.85	0.00	14.85	4.000	No	Yes	2.00
211	4.22	1.05	100.00	3.00	0.56	1.48	14.89	0.00	14.89	4.000	No	Yes	2.00
212	4.24	1.05	100.00	3.00	0.56	1.47	14.99	0.00	14.99	4.000	No	Yes	2.00
213	4.26	1.05	100.00	3.01	0.56	1.47	14.83	0.00	14.83	4.000	No	Yes	2.00
214	4.28	1.06	100.00	3.01	0.56	1.47	14.70	0.00	14.70	4.000	No	Yes	2.00
215	4.30	1.09	100.00	3.00	0.56	1.46	15.35	0.00	15.35	4.000	No	Yes	2.00
216	4.32	1.13	100.00	2.98	0.56	1.46	15.94	0.00	15.94	4.000	No	Yes	2.00
217	4.34	1.15	100.00	2.97	0.56	1.46	16.20	0.00	16.20	4.000	No	Yes	2.00
218	4.36	1.14	100.00	2.97	0.56	1.45	16.04	0.00	16.04	4.000	No	Yes	2.00
219	4.38	1.14	100.00	2.97	0.56	1.45	15.72	0.00	15.72	4.000	No	Yes	2.00
220	4.40	1.13	100.00	2.97	0.56	1.45	15.85	0.00	15.85	4.000	No	Yes	2.00
221	4.42	1.12	99.74	2.96	0.56	1.45	15.56	0.00	15.56	4.000	No	Yes	2.00
222	4.44	1.09	100.00	2.96	0.56	1.45	15.24	0.00	15.24	4.000	No	Yes	2.00
223	4.46	1.06	100.00	2.98	0.56	1.45	14.76	0.00	14.76	4.000	No	Yes	2.00
224	4.48	1.02	100.00	3.00	0.57	1.45	14.06	0.00	14.06	4.000	No	Yes	2.00
225	4.50	0.98	100.00	3.02	0.57	1.44	13.84	0.00	13.84	4.000	No	Yes	2.00
226	4.52	0.94	100.00	3.06	0.57	1.44	13.00	0.00	13.00	4.000	No	Yes	2.00
227	4.54	0.88	100.00	3.11	0.57	1.44	12.30	0.00	12.30	4.000	No	Yes	2.00
228	4.56	0.83	100.00	3.15	0.58	1.45	11.25	0.00	11.25	4.000	No	Yes	2.00
229	4.58	0.76	100.00	3.19	0.58	1.45	10.61	0.00	10.61	4.000	No	Yes	2.00
230	4.60	0.72	100.00	3.22	0.58	1.45	9.72	0.00	9.72	4.000	No	Yes	2.00
231	4.62	0.67	100.00	3.25	0.59	1.45	9.18	0.00	9.18	4.000	No	Yes	2.00
232	4.64	0.63	100.00	3.27	0.59	1.45	8.64	0.00	8.64	4.000	No	Yes	2.00
233	4.66	0.59	100.00	3.29	0.59	1.45	7.84	0.00	7.84	4.000	No	Yes	2.00
234	4.68	0.56	100.00	3.29	0.59	1.45	7.67	0.00	7.67	4.000	No	Yes	2.00
235	4.70	0.55	100.00	3.27	0.59	1.44	7.43	0.00	7.43	4.000	No	Yes	2.00
236	4.72	0.55	100.00	3.24	0.59	1.44	7.32	0.00	7.32	4.000	No	Yes	2.00
237	4.74	0.56	100.00	3.20	0.59	1.44	7.66	0.00	7.66	4.000	No	Yes	2.00
238	4.76	0.58	100.00	3.14	0.59	1.44	7.62	0.00	7.62	4.000	No	Yes	2.00
239	4.78	0.59	100.00	3.09	0.59	1.43	8.06	0.00	8.06	4.000	No	Yes	2.00
240	4.80	0.61	100.00	3.06	0.59	1.43	8.18	0.00	8.18	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
241	4.82	0.61	100.00	3.04	0.59	1.43	8.24	0.00	8.24	4.000	No	Yes	2.00
242	4.84	0.60	100.00	3.05	0.59	1.43	8.30	0.00	8.30	4.000	No	Yes	2.00
243	4.86	0.63	100.00	3.02	0.59	1.43	7.84	0.00	7.84	4.000	No	Yes	2.00
244	4.88	0.65	100.00	3.02	0.59	1.42	9.29	0.00	9.29	4.000	No	Yes	2.00
245	4.90	0.68	100.00	3.00	0.59	1.42	9.09	0.00	9.09	4.000	No	Yes	2.00
246	4.92	0.69	100.00	3.00	0.59	1.42	9.27	0.00	9.27	4.000	No	Yes	2.00
247	4.94	0.68	100.00	2.99	0.58	1.41	9.32	0.00	9.32	4.000	No	Yes	2.00
248	4.96	0.68	100.00	3.00	0.59	1.41	8.96	0.00	8.96	4.000	No	Yes	2.00
249	4.98	0.66	100.00	3.01	0.59	1.41	8.89	0.00	8.89	4.000	No	Yes	2.00
250	5.00	0.67	100.00	2.99	0.59	1.41	8.81	0.00	8.81	4.000	No	Yes	2.00
251	5.02	0.69	99.13	2.95	0.59	1.41	9.22	0.00	9.22	4.000	No	Yes	2.00
252	5.04	0.73	94.44	2.89	0.59	1.41	9.46	0.00	9.46	4.000	No	Yes	2.00
253	5.06	0.77	90.85	2.85	0.58	1.40	10.25	0.00	10.25	4.000	No	Yes	2.00
254	5.08	0.82	88.30	2.82	0.58	1.40	10.90	0.00	10.90	4.000	No	Yes	2.00
255	5.10	0.86	86.28	2.79	0.58	1.40	11.33	0.00	11.33	4.000	No	Yes	2.00
256	5.12	0.90	84.04	2.76	0.58	1.39	11.79	0.00	11.79	4.000	No	Yes	2.00
257	5.14	0.94	81.76	2.73	0.58	1.39	12.50	0.00	12.50	4.000	No	Yes	2.00
258	5.16	0.98	80.10	2.71	0.58	1.39	12.95	0.00	12.95	4.000	No	Yes	2.00
259	5.19	1.00	79.96	2.71	0.57	1.38	13.61	0.00	13.61	4.000	No	Yes	2.00
260	5.20	1.01	80.88	2.72	0.58	1.38	13.26	0.00	13.26	4.000	No	Yes	2.00
261	5.22	1.01	82.61	2.75	0.57	1.38	13.23	0.00	13.23	4.000	No	Yes	2.00
262	5.24	1.03	83.01	2.75	0.57	1.38	13.40	0.00	13.40	4.000	No	Yes	2.00
263	5.26	1.05	83.25	2.75	0.57	1.38	13.85	0.00	13.85	4.000	No	Yes	2.00
264	5.28	1.08	83.70	2.76	0.57	1.37	14.20	0.00	14.20	4.000	No	Yes	2.00
265	5.30	1.11	83.89	2.76	0.57	1.37	14.42	0.00	14.42	4.000	No	Yes	2.00
266	5.32	1.15	83.65	2.76	0.57	1.37	15.07	0.00	15.07	4.000	No	Yes	2.00
267	5.34	1.19	83.37	2.75	0.57	1.36	15.60	0.00	15.60	4.000	No	Yes	2.00
268	5.36	1.24	82.91	2.75	0.57	1.36	15.83	0.00	15.83	4.000	No	Yes	2.00
269	5.38	1.28	82.49	2.74	0.56	1.36	16.79	0.00	16.79	4.000	No	Yes	2.00
270	5.40	1.32	82.27	2.74	0.56	1.35	17.31	0.00	17.31	4.000	No	Yes	2.00
271	5.42	1.36	82.40	2.74	0.56	1.35	17.40	0.00	17.40	4.000	No	Yes	2.00
272	5.44	1.40	82.50	2.74	0.56	1.35	18.07	0.00	18.07	4.000	No	Yes	2.00
273	5.46	1.45	82.22	2.74	0.55	1.34	18.80	0.00	18.80	4.000	No	Yes	2.00
274	5.48	1.49	82.68	2.75	0.55	1.34	19.10	0.00	19.10	4.000	No	Yes	2.00
275	5.50	1.51	84.02	2.76	0.55	1.34	19.64	0.00	19.64	4.000	No	Yes	2.00
276	5.52	1.52	85.69	2.78	0.55	1.34	19.54	0.00	19.54	4.000	No	Yes	2.00
277	5.54	1.50	88.23	2.82	0.55	1.33	19.35	0.00	19.35	4.000	No	Yes	2.00
278	5.56	1.49	90.89	2.85	0.55	1.33	19.10	0.00	19.10	4.000	No	Yes	2.00
279	5.58	1.44	94.80	2.90	0.55	1.33	18.90	0.00	18.90	4.000	No	Yes	2.00
280	5.60	1.39	98.49	2.94	0.55	1.33	17.51	0.00	17.51	4.000	No	Yes	2.00
281	5.62	1.31	100.00	3.00	0.56	1.33	17.00	0.00	17.00	4.000	No	Yes	2.00
282	5.64	1.24	100.00	3.05	0.56	1.33	15.95	0.00	15.95	4.000	No	Yes	2.00
283	5.66	1.17	100.00	3.10	0.56	1.33	14.84	0.00	14.84	4.000	No	Yes	2.00
284	5.68	1.10	100.00	3.13	0.57	1.33	13.94	0.00	13.94	4.000	No	Yes	2.00
285	5.70	1.06	100.00	3.14	0.57	1.33	13.38	0.00	13.38	4.000	No	Yes	2.00
286	5.72	1.04	100.00	3.12	0.57	1.33	13.15	0.00	13.15	4.000	No	Yes	2.00
287	5.74	1.05	100.00	3.09	0.57	1.33	13.21	0.00	13.21	4.000	No	Yes	2.00
288	5.76	1.09	100.00	3.03	0.57	1.32	13.74	0.00	13.74	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
289	5.78	1.13	100.00	2.97	0.56	1.32	14.57	0.00	14.57	4.000	No	Yes	2.00
290	5.80	1.16	97.41	2.93	0.57	1.32	14.55	0.00	14.55	4.000	No	Yes	2.00
291	5.82	1.17	95.83	2.91	0.57	1.32	14.70	0.00	14.70	4.000	No	Yes	2.00
292	5.84	1.20	93.49	2.88	0.56	1.31	15.09	0.00	15.09	4.000	No	Yes	2.00
293	5.86	1.28	89.94	2.84	0.56	1.31	15.71	0.00	15.71	4.000	No	Yes	2.00
294	5.89	1.36	87.80	2.81	0.56	1.30	17.57	0.00	17.57	4.000	No	Yes	2.00
295	5.90	1.43	87.55	2.81	0.56	1.30	18.06	0.00	18.06	4.000	No	Yes	2.00
296	5.92	1.45	89.29	2.83	0.55	1.30	18.27	0.00	18.27	4.000	No	Yes	2.00
297	5.94	1.43	91.33	2.85	0.55	1.30	18.06	0.00	18.06	4.000	No	Yes	2.00
298	5.96	1.41	93.63	2.88	0.56	1.30	17.56	0.00	17.56	4.000	No	Yes	2.00
299	5.98	1.37	96.68	2.92	0.56	1.29	17.21	0.00	17.21	4.000	No	Yes	2.00
300	6.01	1.36	98.84	2.95	0.56	1.29	16.59	0.00	16.59	4.000	No	Yes	2.00
301	6.02	1.33	100.00	2.98	0.56	1.29	16.98	0.00	16.98	4.000	No	Yes	2.00
302	6.04	1.32	100.00	3.00	0.56	1.29	16.22	0.00	16.22	4.000	No	Yes	2.00
303	6.06	1.30	100.00	3.02	0.56	1.29	16.20	0.00	16.20	4.000	No	Yes	2.00
304	6.08	1.29	100.00	3.04	0.56	1.29	16.05	0.00	16.05	4.000	No	Yes	2.00
305	6.10	1.25	100.00	3.06	0.56	1.29	15.61	0.00	15.61	4.000	No	Yes	2.00
306	6.12	1.22	100.00	3.08	0.56	1.29	14.82	0.00	14.82	4.000	No	Yes	2.00
307	6.14	1.19	100.00	3.08	0.56	1.28	14.82	0.00	14.82	4.000	No	Yes	2.00
308	6.16	1.18	100.00	3.08	0.57	1.28	14.53	0.00	14.53	4.000	No	Yes	2.00
309	6.18	1.15	100.00	3.08	0.57	1.28	14.27	0.00	14.27	4.000	No	Yes	2.00
310	6.21	1.13	100.00	3.10	0.57	1.28	13.77	0.00	13.77	4.000	No	Yes	2.00
311	6.22	1.10	100.00	3.11	0.57	1.28	13.58	0.00	13.58	4.000	No	Yes	2.00
312	6.25	1.08	100.00	3.13	0.57	1.28	13.20	0.00	13.20	4.000	No	Yes	2.00
313	6.26	1.07	100.00	3.14	0.57	1.28	13.08	0.00	13.08	4.000	No	Yes	2.00
314	6.28	1.06	100.00	3.15	0.57	1.28	13.03	0.00	13.03	4.000	No	Yes	2.00
315	6.30	1.07	100.00	3.14	0.57	1.27	12.89	0.00	12.89	4.000	No	Yes	2.00
316	6.32	1.09	100.00	3.12	0.57	1.27	13.26	0.00	13.26	4.000	No	Yes	2.00
317	6.34	1.11	100.00	3.09	0.57	1.27	13.66	0.00	13.66	4.000	No	Yes	2.00
318	6.36	1.12	100.00	3.07	0.57	1.27	13.57	0.00	13.57	4.000	No	Yes	2.00
319	6.38	1.12	100.00	3.05	0.57	1.27	13.55	0.00	13.55	4.000	No	Yes	2.00
320	6.40	1.14	100.00	3.04	0.57	1.26	13.78	0.00	13.78	4.000	No	Yes	2.00
321	6.42	1.15	100.00	3.03	0.57	1.26	14.02	0.00	14.02	4.000	No	Yes	2.00
322	6.44	1.16	100.00	3.03	0.57	1.26	13.83	0.00	13.83	4.000	No	Yes	2.00
323	6.46	1.16	100.00	3.03	0.57	1.26	14.07	0.00	14.07	4.000	No	Yes	2.00
324	6.48	1.17	100.00	3.03	0.57	1.26	14.04	0.00	14.04	4.000	No	Yes	2.00
325	6.50	1.18	100.00	3.03	0.57	1.25	14.19	0.00	14.19	4.000	No	Yes	2.00
326	6.52	1.20	100.00	3.02	0.57	1.25	14.40	0.00	14.40	4.000	No	Yes	2.00
327	6.54	1.24	100.00	3.00	0.56	1.25	14.83	0.00	14.83	4.000	No	Yes	2.00
328	6.56	1.28	100.00	2.99	0.56	1.25	15.46	0.00	15.46	4.000	No	Yes	2.00
329	6.58	1.31	100.00	2.98	0.56	1.24	15.75	0.00	15.75	4.000	No	Yes	2.00
330	6.60	1.33	100.00	2.98	0.56	1.24	15.87	0.00	15.87	4.000	No	Yes	2.00
331	6.62	1.34	100.00	2.98	0.56	1.24	16.07	0.00	16.07	4.000	No	Yes	2.00
332	6.64	1.34	100.00	2.99	0.56	1.24	16.04	0.00	16.04	4.000	No	Yes	2.00
333	6.66	1.33	100.00	3.01	0.56	1.24	15.91	0.00	15.91	4.000	No	Yes	2.00
334	6.68	1.34	100.00	3.02	0.56	1.24	15.72	0.00	15.72	4.000	No	Yes	2.00
335	6.70	1.35	100.00	3.02	0.56	1.23	16.11	0.00	16.11	4.000	No	Yes	2.00
336	6.72	1.37	100.00	3.02	0.56	1.23	16.34	0.00	16.34	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
337	6.74	1.38	100.00	3.02	0.56	1.23	16.40	0.00	16.40	4.000	No	Yes	2.00
338	6.76	1.38	100.00	3.02	0.56	1.23	16.27	0.00	16.27	4.000	No	Yes	2.00
339	6.78	1.40	100.00	3.01	0.56	1.23	16.44	0.00	16.44	4.000	No	Yes	2.00
340	6.80	1.43	100.00	2.99	0.56	1.22	16.91	0.00	16.91	4.000	No	Yes	2.00
341	6.82	1.45	100.00	2.98	0.56	1.22	17.28	0.00	17.28	4.000	No	Yes	2.00
342	6.84	1.49	100.00	2.98	0.56	1.22	17.28	0.00	17.28	4.000	No	Yes	2.00
343	6.86	1.52	100.00	2.98	0.55	1.22	17.95	0.00	17.95	4.000	No	Yes	2.00
344	6.88	1.54	100.00	2.99	0.55	1.22	18.40	0.00	18.40	4.000	No	Yes	2.00
345	6.90	1.54	100.00	3.00	0.55	1.21	18.02	0.00	18.02	4.000	No	Yes	2.00
346	6.92	1.51	100.00	3.03	0.55	1.21	17.91	0.00	17.91	4.000	No	Yes	2.00
347	6.94	1.46	100.00	3.06	0.56	1.21	17.14	0.00	17.14	4.000	No	Yes	2.00
348	6.96	1.40	100.00	3.09	0.56	1.21	16.15	0.00	16.15	4.000	No	Yes	2.00
349	6.98	1.36	100.00	3.10	0.56	1.21	15.76	0.00	15.76	4.000	No	Yes	2.00
350	7.00	1.35	100.00	3.09	0.56	1.21	15.63	0.00	15.63	4.000	No	Yes	2.00
351	7.02	1.34	100.00	3.08	0.56	1.21	15.68	0.00	15.68	4.000	No	Yes	2.00
352	7.04	1.36	100.00	3.06	0.56	1.21	15.60	0.00	15.60	4.000	No	Yes	2.00
353	7.06	1.38	100.00	3.03	0.56	1.20	16.13	0.00	16.13	4.000	No	Yes	2.00
354	7.08	1.43	100.00	3.00	0.56	1.20	16.41	0.00	16.41	4.000	No	Yes	2.00
355	7.10	1.46	100.00	2.98	0.56	1.20	17.12	0.00	17.12	4.000	No	Yes	2.00
356	7.12	1.50	100.00	2.96	0.55	1.20	17.39	0.00	17.39	4.000	No	Yes	2.00
357	7.14	1.51	99.99	2.96	0.55	1.20	17.69	0.00	17.69	4.000	No	Yes	2.00
358	7.16	1.50	100.00	2.97	0.56	1.20	17.31	0.00	17.31	4.000	No	Yes	2.00
359	7.18	1.48	100.00	2.99	0.56	1.19	16.93	0.00	16.93	4.000	No	Yes	2.00
360	7.20	1.47	100.00	3.00	0.56	1.19	16.84	0.00	16.84	4.000	No	Yes	2.00
361	7.22	1.49	100.00	3.00	0.56	1.19	17.01	0.00	17.01	4.000	No	Yes	2.00
362	7.24	1.52	100.00	2.99	0.55	1.19	17.52	0.00	17.52	4.000	No	Yes	2.00
363	7.26	1.55	100.00	2.99	0.55	1.19	17.90	0.00	17.90	4.000	No	Yes	2.00
364	7.28	1.57	100.00	2.99	0.55	1.19	17.82	0.00	17.82	4.000	No	Yes	2.00
365	7.30	1.59	100.00	2.99	0.55	1.18	18.12	0.00	18.12	4.000	No	Yes	2.00
366	7.32	1.65	100.00	2.97	0.55	1.18	18.69	0.00	18.69	4.000	No	Yes	2.00
367	7.34	1.73	98.21	2.94	0.55	1.18	19.86	0.00	19.86	4.000	No	Yes	2.00
368	7.36	1.82	95.68	2.91	0.54	1.18	20.85	0.00	20.85	4.000	No	Yes	2.00
369	7.38	1.87	94.12	2.89	0.54	1.17	21.46	0.00	21.46	4.000	No	Yes	2.00
370	7.40	1.89	93.74	2.88	0.54	1.17	21.69	0.00	21.69	4.000	No	Yes	2.00
371	7.42	1.88	94.22	2.89	0.54	1.17	21.41	0.00	21.41	4.000	No	Yes	2.00
372	7.44	1.88	94.89	2.90	0.54	1.17	21.12	0.00	21.12	4.000	No	Yes	2.00
373	7.46	1.88	95.79	2.91	0.54	1.17	21.35	0.00	21.35	4.000	No	Yes	2.00
374	7.48	1.89	96.66	2.92	0.54	1.17	21.43	0.00	21.43	4.000	No	Yes	2.00
375	7.50	1.90	97.44	2.93	0.54	1.17	21.35	0.00	21.35	4.000	No	Yes	2.00
376	7.52	1.92	97.63	2.93	0.54	1.16	21.76	0.00	21.76	4.000	No	Yes	2.00
377	7.54	1.95	97.41	2.93	0.54	1.16	21.97	0.00	21.97	4.000	No	Yes	2.00
378	7.56	1.96	97.39	2.93	0.54	1.16	22.14	0.00	22.14	4.000	No	Yes	2.00
379	7.58	1.95	97.57	2.93	0.54	1.16	21.98	0.00	21.98	4.000	No	Yes	2.00
380	7.60	1.91	98.81	2.95	0.54	1.16	21.73	0.00	21.73	4.000	No	Yes	2.00
381	7.62	1.86	100.00	2.97	0.54	1.16	20.70	0.00	20.70	4.000	No	Yes	2.00
382	7.64	1.81	100.00	2.99	0.55	1.16	20.17	0.00	20.17	4.000	No	Yes	2.00
383	7.66	1.78	100.00	3.01	0.55	1.15	20.00	0.00	20.00	4.000	No	Yes	2.00
384	7.68	1.75	100.00	3.02	0.55	1.15	19.53	0.00	19.53	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
385	7.70	1.71	100.00	3.04	0.55	1.15	19.05	0.00	19.05	4.000	No	Yes	2.00
386	7.72	1.67	100.00	3.06	0.55	1.15	18.65	0.00	18.65	4.000	No	Yes	2.00
387	7.74	1.64	100.00	3.08	0.55	1.15	18.22	0.00	18.22	4.000	No	Yes	2.00
388	7.76	1.63	100.00	3.08	0.55	1.15	18.11	0.00	18.11	4.000	No	Yes	2.00
389	7.78	1.63	100.00	3.08	0.55	1.15	18.03	0.00	18.03	4.000	No	Yes	2.00
390	7.80	1.63	100.00	3.08	0.55	1.15	18.26	0.00	18.26	4.000	No	Yes	2.00
391	7.82	1.64	100.00	3.07	0.55	1.15	18.00	0.00	18.00	4.000	No	Yes	2.00
392	7.84	1.66	100.00	3.06	0.55	1.14	18.40	0.00	18.40	4.000	No	Yes	2.00
393	7.86	1.68	100.00	3.04	0.55	1.14	18.69	0.00	18.69	4.000	No	Yes	2.00
394	7.88	1.71	100.00	3.03	0.55	1.14	18.80	0.00	18.80	4.000	No	Yes	2.00
395	7.90	1.72	100.00	3.03	0.55	1.14	19.14	0.00	19.14	4.000	No	Yes	2.00
396	7.92	1.73	100.00	3.02	0.55	1.14	18.96	0.00	18.96	4.000	No	Yes	2.00
397	7.94	1.74	100.00	3.02	0.55	1.14	19.25	0.00	19.25	4.000	No	Yes	2.00
398	7.96	1.75	100.00	3.01	0.55	1.13	19.25	0.00	19.25	4.000	No	Yes	2.00
399	7.98	1.75	100.00	3.01	0.55	1.13	19.38	0.00	19.38	4.000	No	Yes	2.00
400	8.00	1.73	100.00	3.02	0.55	1.13	19.10	0.00	19.10	4.000	No	Yes	2.00
401	8.02	1.68	100.00	3.04	0.55	1.13	18.53	0.00	18.53	4.000	No	Yes	2.00
402	8.04	1.60	100.00	3.06	0.55	1.13	17.55	0.00	17.55	4.000	No	Yes	2.00
403	8.07	1.53	100.00	3.09	0.56	1.13	16.53	0.00	16.53	4.000	No	Yes	2.00
404	8.08	1.47	100.00	3.11	0.56	1.13	16.08	0.00	16.08	4.000	No	Yes	2.00
405	8.10	1.43	100.00	3.12	0.56	1.13	15.59	0.00	15.59	4.000	No	Yes	2.00
406	8.12	1.38	100.00	3.13	0.56	1.13	15.08	0.00	15.08	4.000	No	Yes	2.00
407	8.14	1.35	100.00	3.13	0.56	1.13	14.62	0.00	14.62	4.000	No	Yes	2.00
408	8.16	1.35	100.00	3.13	0.57	1.12	14.57	0.00	14.57	4.000	No	Yes	2.00
409	8.18	1.36	100.00	3.12	0.56	1.12	14.81	0.00	14.81	4.000	No	Yes	2.00
410	8.20	1.37	100.00	3.11	0.56	1.12	14.86	0.00	14.86	4.000	No	Yes	2.00
411	8.22	1.37	100.00	3.10	0.56	1.12	15.07	0.00	15.07	4.000	No	Yes	2.00
412	8.24	1.39	100.00	3.09	0.56	1.12	14.79	0.00	14.79	4.000	No	Yes	2.00
413	8.26	1.42	100.00	3.08	0.56	1.12	15.19	0.00	15.19	4.000	No	Yes	2.00
414	8.28	1.47	100.00	3.05	0.56	1.12	15.99	0.00	15.99	4.000	No	Yes	2.00
415	8.30	1.51	100.00	3.03	0.56	1.11	16.53	0.00	16.53	4.000	No	Yes	2.00
416	8.32	1.54	100.00	3.02	0.56	1.11	16.41	0.00	16.41	4.000	No	Yes	2.00
417	8.34	1.55	100.00	3.02	0.56	1.11	16.90	0.00	16.90	4.000	No	Yes	2.00
418	8.36	1.58	100.00	3.01	0.56	1.11	16.90	0.00	16.90	4.000	No	Yes	2.00
419	8.38	1.58	100.00	3.01	0.56	1.11	17.21	0.00	17.21	4.000	No	Yes	2.00
420	8.40	1.57	100.00	3.03	0.56	1.11	16.86	0.00	16.86	4.000	No	Yes	2.00
421	8.42	1.55	100.00	3.05	0.56	1.11	16.66	0.00	16.66	4.000	No	Yes	2.00
422	8.44	1.54	100.00	3.07	0.56	1.11	16.33	0.00	16.33	4.000	No	Yes	2.00
423	8.47	1.56	100.00	3.07	0.56	1.10	16.66	0.00	16.66	4.000	No	Yes	2.00
424	8.48	1.59	100.00	3.07	0.56	1.10	17.11	0.00	17.11	4.000	No	Yes	2.00
425	8.50	1.63	100.00	3.05	0.56	1.10	17.34	0.00	17.34	4.000	No	Yes	2.00
426	8.52	1.65	100.00	3.05	0.55	1.10	17.80	0.00	17.80	4.000	No	Yes	2.00
427	8.54	1.65	100.00	3.05	0.55	1.10	17.71	0.00	17.71	4.000	No	Yes	2.00
428	8.56	1.64	100.00	3.06	0.56	1.10	17.11	0.00	17.11	4.000	No	Yes	2.00
429	8.58	1.63	100.00	3.06	0.55	1.10	17.41	0.00	17.41	4.000	No	Yes	2.00
430	8.60	1.63	100.00	3.07	0.56	1.09	17.34	0.00	17.34	4.000	No	Yes	2.00
431	8.62	1.63	100.00	3.08	0.56	1.09	17.17	0.00	17.17	4.000	No	Yes	2.00
432	8.64	1.62	100.00	3.09	0.56	1.09	17.26	0.00	17.26	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
433	8.66	1.60	100.00	3.10	0.56	1.09	17.01	0.00	17.01	4.000	No	Yes	2.00
434	8.68	1.57	100.00	3.11	0.56	1.09	16.53	0.00	16.53	4.000	No	Yes	2.00
435	8.70	1.54	100.00	3.11	0.56	1.09	16.26	0.00	16.26	4.000	No	Yes	2.00
436	8.72	1.51	100.00	3.11	0.56	1.09	15.99	0.00	15.99	4.000	No	Yes	2.00
437	8.74	1.50	100.00	3.11	0.56	1.09	15.62	0.00	15.62	4.000	No	Yes	2.00
438	8.76	1.48	100.00	3.10	0.56	1.09	15.65	0.00	15.65	4.000	No	Yes	2.00
439	8.78	1.49	100.00	3.08	0.56	1.08	15.32	0.00	15.32	4.000	No	Yes	2.00
440	8.80	1.52	100.00	3.04	0.56	1.08	15.93	0.00	15.93	4.000	No	Yes	2.00
441	8.82	1.62	100.00	2.98	0.56	1.08	16.73	0.00	16.73	4.000	No	Yes	2.00
442	8.84	1.69	98.11	2.94	0.55	1.08	18.17	0.00	18.17	4.000	No	Yes	2.00
443	8.86	1.76	96.10	2.91	0.55	1.08	18.23	0.00	18.23	4.000	No	Yes	2.00
444	8.88	1.79	96.04	2.91	0.55	1.08	18.88	0.00	18.88	4.000	No	Yes	2.00
445	8.90	1.83	95.84	2.91	0.55	1.08	19.06	0.00	19.06	4.000	No	Yes	2.00
446	8.92	1.85	96.50	2.92	0.55	1.07	19.36	0.00	19.36	4.000	No	Yes	2.00
447	8.94	1.85	97.71	2.93	0.55	1.07	19.44	0.00	19.44	4.000	No	Yes	2.00
448	8.96	1.84	99.76	2.96	0.55	1.07	19.17	0.00	19.17	4.000	No	Yes	2.00
449	8.98	1.81	100.00	2.98	0.55	1.07	18.78	0.00	18.78	4.000	No	Yes	2.00
450	9.00	1.76	100.00	3.02	0.55	1.07	18.56	0.00	18.56	4.000	No	Yes	2.00
451	9.02	1.71	100.00	3.04	0.55	1.07	17.50	0.00	17.50	4.000	No	Yes	2.00
452	9.04	1.67	100.00	3.05	0.56	1.07	17.36	0.00	17.36	4.000	No	Yes	2.00
453	9.06	1.65	100.00	3.06	0.56	1.07	17.22	0.00	17.22	4.000	No	Yes	2.00
454	9.09	1.59	100.00	3.08	0.56	1.07	16.72	0.00	16.72	4.000	No	Yes	2.00
455	9.10	1.48	100.00	3.11	0.56	1.07	15.33	0.00	15.33	4.000	No	Yes	2.00
456	9.13	1.36	100.00	3.15	0.57	1.07	13.75	0.00	13.75	4.000	No	Yes	2.00
457	9.14	1.25	100.00	3.19	0.57	1.07	12.85	0.00	12.85	4.000	No	Yes	2.00
458	9.16	1.20	100.00	3.20	0.57	1.06	12.07	0.00	12.07	4.000	No	Yes	2.00
459	9.18	1.17	100.00	3.20	0.57	1.06	11.91	0.00	11.91	4.000	No	Yes	2.00
460	9.20	1.17	100.00	3.18	0.57	1.06	11.91	0.00	11.91	4.000	No	Yes	2.00
461	9.22	1.20	100.00	3.13	0.57	1.06	12.17	0.00	12.17	4.000	No	Yes	2.00
462	9.24	1.23	100.00	3.08	0.57	1.06	12.59	0.00	12.59	4.000	No	Yes	2.00
463	9.26	1.26	100.00	3.03	0.57	1.06	12.87	0.00	12.87	4.000	No	Yes	2.00
464	9.28	1.27	100.00	3.00	0.57	1.06	13.08	0.00	13.08	4.000	No	Yes	2.00
465	9.30	1.26	100.00	2.99	0.57	1.06	12.80	0.00	12.80	4.000	No	Yes	2.00
466	9.32	1.21	100.00	3.01	0.57	1.06	12.62	0.00	12.62	4.000	No	Yes	2.00
467	9.34	1.16	100.00	3.04	0.58	1.06	11.49	0.00	11.49	4.000	No	Yes	2.00
468	9.36	1.10	100.00	3.08	0.58	1.05	11.07	0.00	11.07	4.000	No	Yes	2.00
469	9.38	1.07	100.00	3.10	0.58	1.05	10.72	0.00	10.72	4.000	No	Yes	2.00
470	9.40	1.06	100.00	3.10	0.58	1.05	10.57	0.00	10.57	4.000	No	Yes	2.00
471	9.42	1.08	100.00	3.07	0.58	1.05	10.85	0.00	10.85	4.000	No	Yes	2.00
472	9.44	1.14	100.00	3.02	0.58	1.05	11.45	0.00	11.45	4.000	No	Yes	2.00
473	9.47	1.20	100.00	2.97	0.57	1.05	12.19	0.00	12.19	4.000	No	Yes	2.00
474	9.48	1.30	95.45	2.91	0.57	1.05	12.72	0.00	12.72	4.000	No	Yes	2.00
475	9.50	1.44	90.29	2.84	0.57	1.05	14.56	0.00	14.56	4.000	No	Yes	2.00
476	9.52	1.61	83.26	2.75	0.56	1.05	16.27	0.00	16.27	4.000	No	Yes	2.00
477	9.54	1.76	79.73	2.71	0.56	1.04	18.14	0.00	18.14	4.000	No	Yes	2.00
478	9.56	1.86	79.51	2.71	0.56	1.04	18.95	0.00	18.95	4.000	No	Yes	2.00
479	9.58	1.92	82.55	2.74	0.55	1.04	19.29	0.00	19.29	4.000	No	Yes	2.00
480	9.60	1.96	85.59	2.78	0.55	1.04	19.93	0.00	19.93	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
481	9.62	2.02	87.92	2.81	0.55	1.04	20.22	0.00	20.22	4.000	No	Yes	2.00
482	9.64	2.07	89.74	2.83	0.55	1.04	20.93	0.00	20.93	4.000	No	Yes	2.00
483	9.66	2.12	91.29	2.85	0.54	1.04	21.36	0.00	21.36	4.000	No	Yes	2.00
484	9.68	2.17	92.03	2.86	0.54	1.04	21.87	0.00	21.87	4.000	No	Yes	2.00
485	9.70	2.22	92.09	2.86	0.54	1.03	22.33	0.00	22.33	4.000	No	Yes	2.00
486	9.72	2.28	91.67	2.86	0.54	1.03	22.93	0.00	22.93	4.000	No	Yes	2.00
487	9.74	2.30	92.67	2.87	0.54	1.03	23.41	0.00	23.41	4.000	No	Yes	2.00
488	9.76	2.27	95.39	2.90	0.54	1.03	23.02	0.00	23.02	4.000	No	Yes	2.00
489	9.78	2.17	99.41	2.96	0.54	1.03	21.83	0.00	21.83	4.000	No	Yes	2.00
490	9.80	2.02	100.00	3.01	0.54	1.03	20.28	0.00	20.28	4.000	No	Yes	2.00
491	9.82	1.83	100.00	3.08	0.55	1.03	18.42	0.00	18.42	4.000	No	Yes	2.00
492	9.84	1.63	100.00	3.15	0.56	1.03	16.10	0.00	16.10	4.000	No	Yes	2.00
493	9.86	1.43	100.00	3.23	0.57	1.03	14.13	0.00	14.13	4.000	No	Yes	2.00
494	9.88	1.27	100.00	3.30	0.57	1.03	12.29	0.00	12.29	4.000	No	Yes	2.00
495	9.91	1.13	100.00	3.35	0.58	1.03	11.12	0.00	11.12	4.000	No	Yes	2.00
496	9.92	1.05	100.00	3.38	0.58	1.03	10.10	0.00	10.10	4.000	No	Yes	2.00
497	9.94	0.99	100.00	3.39	0.58	1.02	9.62	0.00	9.62	4.000	No	Yes	2.00
498	9.96	0.96	100.00	3.37	0.58	1.02	9.39	0.00	9.39	4.000	No	Yes	2.00
499	9.98	0.95	100.00	3.32	0.59	1.02	9.23	0.00	9.23	4.000	No	Yes	2.00
500	10.00	0.95	100.00	3.26	0.59	1.02	9.27	0.00	9.27	4.000	No	Yes	2.00
501	10.02	0.96	100.00	3.20	0.58	1.02	9.35	0.00	9.35	4.000	No	Yes	2.00
502	10.04	0.98	100.00	3.14	0.58	1.02	9.56	0.00	9.56	4.000	No	Yes	2.00
503	10.06	0.98	100.00	3.09	0.58	1.02	9.64	0.00	9.64	4.000	No	Yes	2.00
504	10.08	0.99	100.00	3.05	0.58	1.02	9.50	0.00	9.50	4.000	No	Yes	2.00
505	10.10	1.02	100.00	3.01	0.58	1.02	9.66	0.00	9.66	4.000	No	Yes	2.00
506	10.12	1.08	99.43	2.96	0.58	1.02	10.58	0.00	10.58	4.000	No	Yes	2.00
507	10.14	1.25	90.84	2.85	0.58	1.02	11.37	0.00	11.37	4.000	No	Yes	2.00
508	10.16	1.50	80.16	2.71	0.57	1.01	14.54	0.00	14.54	4.000	No	Yes	2.00
509	10.18	1.77	72.27	2.62	0.56	1.01	18.17	0.00	18.17	4.000	No	Yes	2.00
510	10.20	1.90	71.81	2.61	0.56	1.01	19.57	0.00	19.57	4.000	No	Yes	2.00
511	10.22	1.85	77.73	2.68	0.56	1.01	18.38	0.00	18.38	4.000	No	Yes	2.00
512	10.24	1.73	85.52	2.78	0.56	1.01	16.59	0.00	16.59	4.000	No	Yes	2.00
513	10.26	1.72	86.44	2.79	0.56	1.01	15.76	0.00	15.76	4.000	Yes	Yes	2.00
514	10.28	1.93	80.21	2.72	0.56	1.01	18.12	0.00	18.12	4.000	Yes	Yes	2.00
515	10.30	2.32	69.68	2.58	0.55	1.01	22.72	57.18	79.89	4.000	Yes	No	2.00
516	10.32	2.69	61.91	2.49	0.54	1.01	27.28	56.84	84.12	4.000	Yes	No	2.00
517	10.34	2.82	59.00	2.45	0.53	1.01	29.11	56.61	85.71	4.000	Yes	No	2.00
518	10.36	2.69	61.40	2.48	0.54	1.01	26.62	56.53	83.15	4.000	Yes	No	2.00
519	10.38	2.36	68.53	2.57	0.54	1.00	23.51	57.19	80.69	4.000	Yes	No	2.00
520	10.40	2.06	75.44	2.66	0.56	1.00	19.02	0.00	19.02	4.000	Yes	Yes	2.00
521	10.42	1.80	80.65	2.72	0.56	1.00	17.79	0.00	17.79	4.000	Yes	Yes	2.00
522	10.44	1.62	85.54	2.78	0.57	1.00	15.62	0.00	15.62	4.000	Yes	Yes	2.00
523	10.46	1.43	93.53	2.88	0.57	1.00	13.68	0.00	13.68	4.000	Yes	Yes	2.00
524	10.48	1.28	100.00	2.99	0.57	1.00	12.28	0.00	12.28	4.000	Yes	Yes	2.00
525	10.50	1.18	100.00	3.07	0.58	1.00	11.11	0.00	11.11	4.000	No	Yes	2.00
526	10.52	1.11	100.00	3.11	0.58	1.00	10.69	0.00	10.69	4.000	No	Yes	2.00
527	10.54	1.07	100.00	3.12	0.58	1.00	10.20	0.00	10.20	4.000	No	Yes	2.00
528	10.56	1.03	100.00	3.12	0.58	1.00	9.71	0.00	9.71	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
529	10.58	1.02	100.00	3.11	0.58	1.00	9.55	0.00	9.55	4.000	No	Yes	2.00
530	10.60	1.02	100.00	3.08	0.58	1.00	9.68	0.00	9.68	4.000	No	Yes	2.00
531	10.62	1.04	100.00	3.03	0.58	1.00	9.90	0.00	9.90	4.000	No	Yes	2.00
532	10.64	1.05	100.00	3.00	0.58	0.99	10.01	0.00	10.01	4.000	No	Yes	2.00
533	10.66	1.05	100.00	2.99	0.58	0.99	9.89	0.00	9.89	4.000	No	Yes	2.00
534	10.68	1.06	100.00	2.99	0.58	0.99	10.04	0.00	10.04	4.000	No	Yes	2.00
535	10.70	1.08	100.00	2.98	0.58	0.99	10.10	0.00	10.10	4.000	Yes	Yes	2.00
536	10.72	1.12	99.55	2.96	0.58	0.99	10.46	0.00	10.46	4.000	Yes	Yes	2.00
537	10.74	1.27	93.47	2.88	0.58	0.99	11.31	0.00	11.31	4.000	Yes	Yes	2.00
538	10.76	1.61	80.76	2.72	0.57	0.99	14.38	0.00	14.38	4.000	Yes	Yes	2.00
539	10.78	2.01	69.88	2.59	0.55	0.99	20.32	56.52	76.84	4.000	Yes	No	2.00
540	10.80	2.56	57.56	2.43	0.55	0.99	22.93	54.50	77.42	4.000	Yes	No	2.00
541	10.82	2.93	51.56	2.36	0.53	0.99	30.40	54.64	85.04	4.000	Yes	No	2.00
542	10.84	3.13	49.81	2.34	0.53	0.99	31.18	54.19	85.37	4.000	Yes	No	2.00
543	10.86	2.88	56.31	2.42	0.53	0.99	28.70	55.73	84.44	4.000	Yes	No	2.00
544	10.88	2.45	67.32	2.55	0.55	0.99	23.02	56.81	79.83	4.000	Yes	No	2.00
545	10.90	1.98	80.90	2.72	0.56	0.99	18.65	0.00	18.65	4.000	Yes	Yes	2.00
546	10.92	1.62	93.31	2.88	0.57	0.98	15.00	0.00	15.00	4.000	Yes	Yes	2.00
547	10.94	1.44	97.56	2.93	0.57	0.98	12.45	0.00	12.45	4.000	Yes	Yes	2.00
548	10.96	1.43	94.58	2.89	0.57	0.98	13.29	0.00	13.29	4.000	No	Yes	2.00
549	10.98	1.53	87.04	2.80	0.57	0.98	14.51	0.00	14.51	4.000	No	Yes	2.00
550	11.00	1.64	84.67	2.77	0.57	0.98	15.39	0.00	15.39	4.000	No	Yes	2.00
551	11.02	1.70	85.36	2.78	0.56	0.98	16.29	0.00	16.29	4.000	No	Yes	2.00
552	11.04	1.72	87.29	2.80	0.56	0.98	16.20	0.00	16.20	4.000	No	Yes	2.00
553	11.06	1.69	92.01	2.86	0.56	0.98	16.14	0.00	16.14	4.000	No	Yes	2.00
554	11.08	1.64	97.41	2.93	0.56	0.98	15.36	0.00	15.36	4.000	No	Yes	2.00
555	11.10	1.55	100.00	3.02	0.56	0.98	14.61	0.00	14.61	4.000	No	Yes	2.00
556	11.13	1.46	100.00	3.10	0.57	0.98	13.59	0.00	13.59	4.000	No	Yes	2.00
557	11.14	1.36	100.00	3.18	0.57	0.97	12.81	0.00	12.81	4.000	No	Yes	2.00
558	11.16	1.27	100.00	3.25	0.58	0.97	11.73	0.00	11.73	4.000	No	Yes	2.00
559	11.18	1.18	100.00	3.32	0.58	0.97	10.92	0.00	10.92	4.000	No	Yes	2.00
560	11.20	1.10	100.00	3.38	0.58	0.97	10.06	0.00	10.06	4.000	No	Yes	2.00
561	11.22	1.03	100.00	3.42	0.58	0.97	9.39	0.00	9.39	4.000	No	Yes	2.00
562	11.24	1.00	100.00	3.43	0.59	0.97	9.05	0.00	9.05	4.000	No	Yes	2.00
563	11.26	0.99	100.00	3.41	0.59	0.97	9.01	0.00	9.01	4.000	No	Yes	2.00
564	11.28	1.00	100.00	3.36	0.59	0.97	9.24	0.00	9.24	4.000	No	Yes	2.00
565	11.30	1.00	100.00	3.30	0.59	0.97	9.29	0.00	9.29	4.000	No	Yes	2.00
566	11.32	1.00	100.00	3.24	0.59	0.97	8.89	0.00	8.89	4.000	No	Yes	2.00
567	11.34	1.03	100.00	3.15	0.59	0.97	9.19	0.00	9.19	4.000	No	Yes	2.00
568	11.36	1.11	100.00	3.02	0.58	0.97	10.06	0.00	10.06	4.000	No	Yes	2.00
569	11.38	1.24	93.33	2.88	0.58	0.96	11.30	0.00	11.30	4.000	No	Yes	2.00
570	11.40	1.38	84.34	2.77	0.58	0.96	12.59	0.00	12.59	4.000	No	Yes	2.00
571	11.42	1.52	78.41	2.69	0.57	0.96	14.03	0.00	14.03	4.000	No	Yes	2.00
572	11.44	1.63	77.39	2.68	0.57	0.96	15.30	0.00	15.30	4.000	No	Yes	2.00
573	11.46	1.68	80.04	2.71	0.57	0.96	15.69	0.00	15.69	4.000	No	Yes	2.00
574	11.48	1.66	85.78	2.78	0.57	0.96	15.39	0.00	15.39	4.000	No	Yes	2.00
575	11.50	1.63	91.05	2.85	0.57	0.96	14.96	0.00	14.96	4.000	No	Yes	2.00
576	11.52	1.60	96.42	2.92	0.56	0.96	14.81	0.00	14.81	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
577	11.54	1.56	100.00	2.99	0.57	0.96	14.42	0.00	14.42	4.000	No	Yes	2.00
578	11.56	1.52	100.00	3.05	0.57	0.96	13.88	0.00	13.88	4.000	No	Yes	2.00
579	11.58	1.49	100.00	3.11	0.57	0.96	13.60	0.00	13.60	4.000	No	Yes	2.00
580	11.60	1.48	100.00	3.14	0.57	0.96	13.47	0.00	13.47	4.000	No	Yes	2.00
581	11.62	1.48	100.00	3.16	0.57	0.96	13.55	0.00	13.55	4.000	No	Yes	2.00
582	11.64	1.48	100.00	3.17	0.57	0.96	13.67	0.00	13.67	4.000	No	Yes	2.00
583	11.66	1.47	100.00	3.18	0.57	0.95	13.37	0.00	13.37	4.000	No	Yes	2.00
584	11.68	1.44	100.00	3.19	0.57	0.95	13.06	0.00	13.06	4.000	No	Yes	2.00
585	11.70	1.42	100.00	3.18	0.57	0.95	12.94	0.00	12.94	4.000	No	Yes	2.00
586	11.72	1.41	100.00	3.18	0.57	0.95	12.72	0.00	12.72	4.000	No	Yes	2.00
587	11.74	1.39	100.00	3.18	0.57	0.95	12.66	0.00	12.66	4.000	No	Yes	2.00
588	11.76	1.39	100.00	3.17	0.57	0.95	12.43	0.00	12.43	4.000	No	Yes	2.00
589	11.78	1.39	100.00	3.17	0.57	0.95	12.57	0.00	12.57	4.000	No	Yes	2.00
590	11.80	1.43	100.00	3.15	0.57	0.95	12.88	0.00	12.88	4.000	No	Yes	2.00
591	11.82	1.47	100.00	3.13	0.57	0.95	13.43	0.00	13.43	4.000	No	Yes	2.00
592	11.84	1.51	100.00	3.12	0.57	0.95	13.64	0.00	13.64	4.000	No	Yes	2.00
593	11.86	1.55	100.00	3.10	0.57	0.95	14.04	0.00	14.04	4.000	No	Yes	2.00
594	11.88	1.60	100.00	3.08	0.57	0.95	14.45	0.00	14.45	4.000	No	Yes	2.00
595	11.90	1.63	100.00	3.07	0.56	0.95	14.88	0.00	14.88	4.000	No	Yes	2.00
596	11.92	1.65	100.00	3.06	0.56	0.94	14.98	0.00	14.98	4.000	No	Yes	2.00
597	11.94	1.65	100.00	3.07	0.56	0.94	14.89	0.00	14.89	4.000	No	Yes	2.00
598	11.96	1.64	100.00	3.07	0.56	0.94	14.81	0.00	14.81	4.000	No	Yes	2.00
599	11.98	1.64	100.00	3.07	0.56	0.94	14.78	0.00	14.78	4.000	No	Yes	2.00
600	12.00	1.65	100.00	3.07	0.56	0.94	14.89	0.00	14.89	4.000	No	Yes	2.00
601	12.02	1.67	100.00	3.07	0.56	0.94	15.12	0.00	15.12	4.000	No	Yes	2.00
602	12.04	1.70	100.00	3.06	0.56	0.94	15.21	0.00	15.21	4.000	No	Yes	2.00
603	12.06	1.74	100.00	3.05	0.56	0.94	15.70	0.00	15.70	4.000	No	Yes	2.00
604	12.08	1.80	100.00	3.03	0.56	0.94	16.25	0.00	16.25	4.000	No	Yes	2.00
605	12.10	1.86	100.00	3.02	0.56	0.94	16.87	0.00	16.87	4.000	No	Yes	2.00
606	12.12	1.92	100.00	3.03	0.55	0.94	17.37	0.00	17.37	4.000	No	Yes	2.00
607	12.14	1.96	100.00	3.04	0.55	0.94	17.61	0.00	17.61	4.000	No	Yes	2.00
608	12.16	1.98	100.00	3.05	0.55	0.94	18.00	0.00	18.00	4.000	No	Yes	2.00
609	12.18	1.99	100.00	3.07	0.55	0.94	17.89	0.00	17.89	4.000	No	Yes	2.00
610	12.21	1.99	100.00	3.08	0.55	0.93	17.80	0.00	17.80	4.000	No	Yes	2.00
611	12.22	1.98	100.00	3.10	0.55	0.93	17.91	0.00	17.91	4.000	No	Yes	2.00
612	12.24	1.97	100.00	3.11	0.55	0.93	17.76	0.00	17.76	4.000	No	Yes	2.00
613	12.26	1.96	100.00	3.13	0.55	0.93	17.48	0.00	17.48	4.000	No	Yes	2.00
614	12.28	1.94	100.00	3.13	0.55	0.93	17.48	0.00	17.48	4.000	No	Yes	2.00
615	12.30	1.94	100.00	3.13	0.56	0.93	17.34	0.00	17.34	4.000	No	Yes	2.00
616	12.32	1.94	100.00	3.12	0.56	0.93	17.25	0.00	17.25	4.000	No	Yes	2.00
617	12.34	1.95	100.00	3.11	0.55	0.93	17.40	0.00	17.40	4.000	No	Yes	2.00
618	12.36	1.99	100.00	3.10	0.55	0.93	17.75	0.00	17.75	4.000	No	Yes	2.00
619	12.38	2.03	100.00	3.08	0.55	0.93	18.18	0.00	18.18	4.000	No	Yes	2.00
620	12.40	2.06	100.00	3.07	0.55	0.93	18.47	0.00	18.47	4.000	No	Yes	2.00
621	12.42	2.05	100.00	3.08	0.55	0.93	18.59	0.00	18.59	4.000	No	Yes	2.00
622	12.44	2.00	100.00	3.09	0.55	0.92	17.69	0.00	17.69	4.000	No	Yes	2.00
623	12.46	1.96	100.00	3.10	0.56	0.92	17.19	0.00	17.19	4.000	No	Yes	2.00
624	12.48	1.98	100.00	3.09	0.55	0.92	17.51	0.00	17.51	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
625	12.50	2.03	100.00	3.06	0.55	0.92	18.18	0.00	18.18	4.000	No	Yes	2.00
626	12.52	2.07	100.00	3.04	0.55	0.92	18.53	0.00	18.53	4.000	No	Yes	2.00
627	12.54	2.06	100.00	3.04	0.55	0.92	18.44	0.00	18.44	4.000	No	Yes	2.00
628	12.56	2.01	100.00	3.06	0.55	0.92	17.94	0.00	17.94	4.000	No	Yes	2.00
629	12.58	1.94	100.00	3.09	0.56	0.92	17.11	0.00	17.11	4.000	No	Yes	2.00
630	12.60	1.88	100.00	3.12	0.56	0.92	16.49	0.00	16.49	4.000	No	Yes	2.00
631	12.62	1.84	100.00	3.13	0.56	0.92	16.09	0.00	16.09	4.000	No	Yes	2.00
632	12.64	1.82	100.00	3.14	0.56	0.92	16.20	0.00	16.20	4.000	No	Yes	2.00
633	12.66	1.82	100.00	3.14	0.56	0.92	15.80	0.00	15.80	4.000	No	Yes	2.00
634	12.68	1.80	100.00	3.14	0.56	0.91	15.91	0.00	15.91	4.000	No	Yes	2.00
635	12.70	1.81	100.00	3.13	0.56	0.91	15.85	0.00	15.85	4.000	No	Yes	2.00
636	12.72	1.83	100.00	3.12	0.56	0.91	16.02	0.00	16.02	4.000	No	Yes	2.00
637	12.74	1.86	100.00	3.10	0.56	0.91	16.20	0.00	16.20	4.000	No	Yes	2.00
638	12.76	1.92	100.00	3.07	0.56	0.91	16.73	0.00	16.73	4.000	No	Yes	2.00
639	12.78	2.02	100.00	3.03	0.55	0.91	17.60	0.00	17.60	4.000	No	Yes	2.00
640	12.80	2.12	100.00	2.99	0.55	0.91	18.86	0.00	18.86	4.000	No	Yes	2.00
641	12.82	2.25	98.77	2.95	0.55	0.91	19.57	0.00	19.57	4.000	No	Yes	2.00
642	12.84	2.35	96.93	2.92	0.54	0.91	20.88	0.00	20.88	4.000	No	Yes	2.00
643	12.86	2.44	95.44	2.91	0.54	0.91	21.63	0.00	21.63	4.000	No	Yes	2.00
644	12.88	2.49	94.89	2.90	0.54	0.91	22.04	0.00	22.04	4.000	No	Yes	2.00
645	12.90	2.53	94.39	2.89	0.54	0.91	22.12	0.00	22.12	4.000	No	Yes	2.00
646	12.92	2.56	94.11	2.89	0.54	0.91	22.66	0.00	22.66	4.000	No	Yes	2.00
647	12.94	2.55	94.68	2.90	0.54	0.91	22.76	0.00	22.76	4.000	No	Yes	2.00
648	12.96	2.46	96.99	2.92	0.54	0.91	21.77	0.00	21.77	4.000	No	Yes	2.00
649	12.99	2.32	100.00	2.97	0.55	0.91	20.19	0.00	20.19	4.000	No	Yes	2.00
650	13.01	2.16	100.00	3.03	0.55	0.90	18.92	0.00	18.92	4.000	No	Yes	2.00
651	13.02	2.00	100.00	3.11	0.55	0.90	17.49	0.00	17.49	4.000	No	Yes	2.00
652	13.04	1.85	100.00	3.18	0.56	0.90	15.63	0.00	15.63	4.000	No	Yes	2.00
653	13.06	1.76	100.00	3.22	0.56	0.90	14.92	0.00	14.92	4.000	No	Yes	2.00
654	13.08	1.77	100.00	3.21	0.56	0.90	15.21	0.00	15.21	4.000	No	Yes	2.00
655	13.10	1.82	100.00	3.18	0.56	0.90	15.84	0.00	15.84	4.000	No	Yes	2.00
656	13.12	1.89	100.00	3.14	0.56	0.90	16.10	0.00	16.10	4.000	No	Yes	2.00
657	13.14	1.97	100.00	3.09	0.56	0.90	17.15	0.00	17.15	4.000	No	Yes	2.00
658	13.16	2.06	100.00	3.02	0.55	0.90	17.78	0.00	17.78	4.000	No	Yes	2.00
659	13.18	2.08	100.00	2.99	0.55	0.90	18.60	0.00	18.60	4.000	No	Yes	2.00
660	13.20	2.06	100.00	2.99	0.55	0.90	17.70	0.00	17.70	4.000	No	Yes	2.00
661	13.22	1.95	100.00	3.03	0.56	0.90	17.05	0.00	17.05	4.000	No	Yes	2.00
662	13.24	1.85	100.00	3.08	0.56	0.89	15.58	0.00	15.58	4.000	No	Yes	2.00
663	13.26	1.75	100.00	3.12	0.56	0.89	14.98	0.00	14.98	4.000	No	Yes	2.00
664	13.28	1.72	100.00	3.14	0.57	0.89	14.53	0.00	14.53	4.000	No	Yes	2.00
665	13.30	1.71	100.00	3.14	0.56	0.89	14.60	0.00	14.60	4.000	No	Yes	2.00
666	13.32	1.73	100.00	3.14	0.56	0.89	14.84	0.00	14.84	4.000	No	Yes	2.00
667	13.34	1.76	100.00	3.12	0.56	0.89	14.99	0.00	14.99	4.000	No	Yes	2.00
668	13.36	1.79	100.00	3.10	0.56	0.89	15.37	0.00	15.37	4.000	No	Yes	2.00
669	13.39	1.80	100.00	3.08	0.56	0.89	15.41	0.00	15.41	4.000	No	Yes	2.00
670	13.40	1.78	100.00	3.08	0.56	0.89	15.36	0.00	15.36	4.000	No	Yes	2.00
671	13.42	1.74	100.00	3.09	0.56	0.89	14.77	0.00	14.77	4.000	No	Yes	2.00
672	13.44	1.70	100.00	3.10	0.57	0.89	14.32	0.00	14.32	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
673	13.46	1.66	100.00	3.10	0.57	0.89	14.14	0.00	14.14	4.000	No	Yes	2.00
674	13.48	1.59	100.00	3.12	0.57	0.88	13.84	0.00	13.84	4.000	No	Yes	2.00
675	13.51	1.50	100.00	3.17	0.57	0.88	12.42	0.00	12.42	4.000	No	Yes	2.00
676	13.52	1.39	100.00	3.23	0.58	0.88	11.59	0.00	11.59	4.000	No	Yes	2.00
677	13.54	1.32	100.00	3.26	0.58	0.88	11.03	0.00	11.03	4.000	No	Yes	2.00
678	13.56	1.27	100.00	3.29	0.58	0.88	10.65	0.00	10.65	4.000	No	Yes	2.00
679	13.58	1.24	100.00	3.30	0.58	0.88	10.25	0.00	10.25	4.000	No	Yes	2.00
680	13.60	1.23	100.00	3.30	0.58	0.88	10.18	0.00	10.18	4.000	No	Yes	2.00
681	13.62	1.24	100.00	3.28	0.58	0.88	10.43	0.00	10.43	4.000	No	Yes	2.00
682	13.64	1.27	100.00	3.24	0.58	0.88	10.35	0.00	10.35	4.000	No	Yes	2.00
683	13.66	1.30	100.00	3.21	0.58	0.88	10.88	0.00	10.88	4.000	No	Yes	2.00
684	13.68	1.33	100.00	3.18	0.58	0.88	11.18	0.00	11.18	4.000	No	Yes	2.00
685	13.70	1.34	100.00	3.17	0.58	0.88	11.30	0.00	11.30	4.000	No	Yes	2.00
686	13.72	1.32	100.00	3.19	0.58	0.87	11.09	0.00	11.09	4.000	No	Yes	2.00
687	13.74	1.28	100.00	3.23	0.58	0.87	10.61	0.00	10.61	4.000	No	Yes	2.00
688	13.76	1.01	100.00	3.34	0.58	0.87	10.24	0.00	10.24	4.000	No	Yes	2.00
689	13.78	0.98	100.00	3.37	0.61	0.87	4.20	0.00	4.20	4.000	No	Yes	2.00
690	13.80	0.95	100.00	3.39	0.58	0.87	9.68	0.00	9.68	4.000	No	Yes	2.00
691	13.83	1.13	100.00	3.33	0.58	0.87	9.43	0.00	9.43	4.000	No	Yes	2.00
692	13.84	1.07	100.00	3.37	0.59	0.87	8.84	0.00	8.84	4.000	No	Yes	2.00
693	13.86	1.01	100.00	3.39	0.59	0.87	8.07	0.00	8.07	4.000	No	Yes	2.00
694	13.88	0.98	100.00	3.40	0.59	0.87	8.09	0.00	8.09	4.000	No	Yes	2.00
695	13.90	0.95	100.00	3.39	0.59	0.87	7.84	0.00	7.84	4.000	No	Yes	2.00
696	13.92	0.93	100.00	3.38	0.59	0.87	7.44	0.00	7.44	4.000	No	Yes	2.00
697	13.94	0.93	100.00	3.35	0.59	0.86	7.49	0.00	7.49	4.000	No	Yes	2.00
698	13.96	0.96	100.00	3.30	0.59	0.86	7.87	0.00	7.87	4.000	No	Yes	2.00
699	13.98	0.98	100.00	3.26	0.59	0.86	8.19	0.00	8.19	4.000	No	Yes	2.00
700	14.00	0.98	100.00	3.23	0.59	0.86	7.84	0.00	7.84	4.000	No	Yes	2.00
701	14.02	0.98	100.00	3.20	0.59	0.86	7.86	0.00	7.86	4.000	No	Yes	2.00
702	14.04	1.00	100.00	3.16	0.59	0.86	8.30	0.00	8.30	4.000	No	Yes	2.00
703	14.06	1.02	100.00	3.15	0.59	0.86	8.33	0.00	8.33	4.000	No	Yes	2.00
704	14.08	1.01	100.00	3.17	0.59	0.86	8.33	0.00	8.33	4.000	No	Yes	2.00
705	14.10	1.00	100.00	3.21	0.59	0.86	8.07	0.00	8.07	4.000	No	Yes	2.00
706	14.12	1.02	100.00	3.21	0.59	0.86	8.13	0.00	8.13	4.000	No	Yes	2.00
707	14.14	1.08	100.00	3.17	0.59	0.86	8.79	0.00	8.79	4.000	No	Yes	2.00
708	14.16	1.12	100.00	3.14	0.58	0.86	9.40	0.00	9.40	4.000	No	Yes	2.00
709	14.18	1.13	100.00	3.12	0.59	0.86	9.14	0.00	9.14	4.000	No	Yes	2.00
710	14.20	1.13	100.00	3.11	0.59	0.86	9.22	0.00	9.22	4.000	No	Yes	2.00
711	14.22	1.12	100.00	3.11	0.58	0.86	9.33	0.00	9.33	4.000	No	Yes	2.00
712	14.24	1.09	100.00	3.14	0.59	0.86	8.83	0.00	8.83	4.000	No	Yes	2.00
713	14.26	1.05	100.00	3.18	0.59	0.86	8.49	0.00	8.49	4.000	No	Yes	2.00
714	14.28	1.00	100.00	3.24	0.59	0.86	8.23	0.00	8.23	4.000	No	Yes	2.00
715	14.30	0.95	100.00	3.29	0.59	0.86	7.52	0.00	7.52	4.000	No	Yes	2.00
716	14.32	0.90	100.00	3.34	0.59	0.85	7.34	0.00	7.34	4.000	No	Yes	2.00
717	14.34	0.87	100.00	3.37	0.59	0.85	6.84	0.00	6.84	4.000	No	Yes	2.00
718	14.36	0.83	100.00	3.40	0.60	0.85	6.66	0.00	6.66	4.000	No	Yes	2.00
719	14.38	0.80	100.00	3.40	0.60	0.85	6.37	0.00	6.37	4.000	No	Yes	2.00
720	14.40	0.78	100.00	3.41	0.60	0.85	6.13	0.00	6.13	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
721	14.42	0.78	100.00	3.37	0.60	0.85	6.09	0.00	6.09	4.000	No	Yes	2.00
722	14.44	0.80	100.00	3.32	0.60	0.85	6.36	0.00	6.36	4.000	No	Yes	2.00
723	14.46	0.81	100.00	3.26	0.60	0.85	6.56	0.00	6.56	4.000	No	Yes	2.00
724	14.48	0.81	100.00	3.23	0.60	0.85	6.48	0.00	6.48	4.000	No	Yes	2.00
725	14.50	0.81	100.00	3.22	0.60	0.85	6.36	0.00	6.36	4.000	No	Yes	2.00
726	14.52	0.82	100.00	3.20	0.60	0.85	6.46	0.00	6.46	4.000	No	Yes	2.00
727	14.54	0.85	100.00	3.17	0.59	0.85	6.83	0.00	6.83	4.000	No	Yes	2.00
728	14.56	0.87	100.00	3.16	0.59	0.85	6.99	0.00	6.99	4.000	No	Yes	2.00
729	14.58	0.87	100.00	3.18	0.59	0.85	6.97	0.00	6.97	4.000	No	Yes	2.00
730	14.60	0.86	100.00	3.19	0.59	0.85	6.83	0.00	6.83	4.000	No	Yes	2.00
731	14.62	0.85	100.00	3.21	0.60	0.85	6.79	0.00	6.79	4.000	No	Yes	2.00
732	14.64	0.87	100.00	3.19	0.60	0.85	6.67	0.00	6.67	4.000	No	Yes	2.00
733	14.66	0.89	100.00	3.17	0.59	0.85	7.16	0.00	7.16	4.000	No	Yes	2.00
734	14.68	0.93	100.00	3.14	0.59	0.85	7.46	0.00	7.46	4.000	No	Yes	2.00
735	14.70	0.97	100.00	3.12	0.59	0.85	7.69	0.00	7.69	4.000	No	Yes	2.00
736	14.72	0.99	100.00	3.11	0.59	0.85	8.00	0.00	8.00	4.000	No	Yes	2.00
737	14.74	1.01	100.00	3.11	0.59	0.85	8.12	0.00	8.12	4.000	No	Yes	2.00
738	14.76	0.97	100.00	3.16	0.59	0.85	8.10	0.00	8.10	4.000	No	Yes	2.00
739	14.78	0.97	100.00	3.19	0.59	0.84	6.96	0.00	6.96	4.000	No	Yes	2.00
740	14.81	0.96	100.00	3.22	0.59	0.84	8.17	0.00	8.17	4.000	No	Yes	2.00
741	14.82	0.99	100.00	3.22	0.59	0.84	7.83	0.00	7.83	4.000	No	Yes	2.00
742	14.84	0.96	100.00	3.25	0.59	0.84	7.56	0.00	7.56	4.000	No	Yes	2.00
743	14.86	0.96	100.00	3.25	0.59	0.84	7.59	0.00	7.59	4.000	No	Yes	2.00
744	14.88	0.98	100.00	3.22	0.59	0.84	7.70	0.00	7.70	4.000	No	Yes	2.00
745	14.90	1.02	100.00	3.17	0.59	0.84	8.13	0.00	8.13	4.000	No	Yes	2.00
746	14.92	1.06	100.00	3.13	0.59	0.84	8.53	0.00	8.53	4.000	No	Yes	2.00
747	14.94	1.09	100.00	3.10	0.59	0.84	8.64	0.00	8.64	4.000	No	Yes	2.00
748	14.96	1.13	100.00	3.09	0.59	0.84	8.95	0.00	8.95	4.000	No	Yes	2.00
749	14.98	1.16	100.00	3.08	0.58	0.84	9.33	0.00	9.33	4.000	No	Yes	2.00
750	15.00	1.18	100.00	3.08	0.58	0.84	9.37	0.00	9.37	4.000	No	Yes	2.00
751	15.02	1.20	100.00	3.10	0.58	0.84	9.44	0.00	9.44	4.000	No	Yes	2.00
752	15.04	1.21	100.00	3.11	0.58	0.84	9.81	0.00	9.81	4.000	No	Yes	2.00
753	15.06	1.23	100.00	3.13	0.58	0.84	9.84	0.00	9.84	4.000	No	Yes	2.00
754	15.08	1.21	100.00	3.17	0.58	0.84	9.69	0.00	9.69	4.000	No	Yes	2.00
755	15.10	1.19	100.00	3.20	0.58	0.84	9.35	0.00	9.35	4.000	No	Yes	2.00
756	15.12	1.17	100.00	3.22	0.58	0.84	9.33	0.00	9.33	4.000	No	Yes	2.00
757	15.14	1.18	100.00	3.22	0.58	0.84	9.32	0.00	9.32	4.000	No	Yes	2.00
758	15.16	1.19	100.00	3.21	0.58	0.84	9.35	0.00	9.35	4.000	No	Yes	2.00
759	15.18	1.22	100.00	3.20	0.58	0.84	9.74	0.00	9.74	4.000	No	Yes	2.00
760	15.20	1.26	100.00	3.19	0.58	0.84	10.08	0.00	10.08	4.000	No	Yes	2.00
761	15.22	1.29	100.00	3.18	0.58	0.84	10.25	0.00	10.25	4.000	No	Yes	2.00
762	15.24	1.32	100.00	3.18	0.58	0.84	10.52	0.00	10.52	4.000	No	Yes	2.00
763	15.27	1.34	100.00	3.19	0.58	0.83	10.80	0.00	10.80	4.000	No	Yes	2.00
764	15.28	1.36	100.00	3.20	0.58	0.83	10.77	0.00	10.77	4.000	No	Yes	2.00
765	15.30	1.36	100.00	3.23	0.58	0.83	10.86	0.00	10.86	4.000	No	Yes	2.00
766	15.32	1.36	100.00	3.24	0.58	0.83	10.77	0.00	10.77	4.000	No	Yes	2.00
767	15.34	1.37	100.00	3.25	0.58	0.83	10.90	0.00	10.90	4.000	No	Yes	2.00
768	15.36	1.38	100.00	3.26	0.58	0.83	11.00	0.00	11.00	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
769	15.38	1.38	100.00	3.28	0.58	0.83	10.99	0.00	10.99	4.000	No	Yes	2.00
770	15.40	1.38	100.00	3.29	0.58	0.83	10.86	0.00	10.86	4.000	No	Yes	2.00
771	15.42	1.37	100.00	3.30	0.58	0.83	10.91	0.00	10.91	4.000	No	Yes	2.00
772	15.44	1.36	100.00	3.31	0.58	0.83	10.68	0.00	10.68	4.000	No	Yes	2.00
773	15.46	1.37	100.00	3.30	0.58	0.83	10.71	0.00	10.71	4.000	No	Yes	2.00
774	15.48	1.40	100.00	3.28	0.58	0.83	11.10	0.00	11.10	4.000	No	Yes	2.00
775	15.50	1.43	100.00	3.26	0.58	0.83	11.40	0.00	11.40	4.000	No	Yes	2.00
776	15.52	1.46	100.00	3.25	0.58	0.83	11.52	0.00	11.52	4.000	No	Yes	2.00
777	15.54	1.46	100.00	3.24	0.58	0.83	11.67	0.00	11.67	4.000	No	Yes	2.00
778	15.56	1.48	100.00	3.23	0.58	0.83	11.58	0.00	11.58	4.000	No	Yes	2.00
779	15.58	1.50	100.00	3.21	0.58	0.83	11.78	0.00	11.78	4.000	No	Yes	2.00
780	15.60	1.54	100.00	3.19	0.57	0.83	12.21	0.00	12.21	4.000	No	Yes	2.00
781	15.62	1.60	100.00	3.15	0.57	0.83	12.63	0.00	12.63	4.000	No	Yes	2.00
782	15.64	1.64	100.00	3.13	0.57	0.83	13.08	0.00	13.08	4.000	No	Yes	2.00
783	15.66	1.67	100.00	3.13	0.57	0.83	13.40	0.00	13.40	4.000	No	Yes	2.00
784	15.68	1.67	100.00	3.14	0.57	0.83	13.31	0.00	13.31	4.000	No	Yes	2.00
785	15.70	1.64	100.00	3.17	0.57	0.83	12.90	0.00	12.90	4.000	No	Yes	2.00
786	15.72	1.60	100.00	3.20	0.57	0.82	12.68	0.00	12.68	4.000	No	Yes	2.00
787	15.74	1.58	100.00	3.21	0.57	0.82	12.43	0.00	12.43	4.000	No	Yes	2.00
788	15.76	1.49	100.00	3.25	0.57	0.82	12.36	0.00	12.36	4.000	No	Yes	2.00
789	15.78	1.48	100.00	3.25	0.58	0.82	10.46	0.00	10.46	4.000	No	Yes	2.00
790	15.80	1.47	100.00	3.26	0.57	0.82	12.10	0.00	12.10	4.000	No	Yes	2.00
791	15.82	1.53	100.00	3.23	0.57	0.82	11.93	0.00	11.93	4.000	No	Yes	2.00
792	15.84	1.53	100.00	3.21	0.57	0.82	12.00	0.00	12.00	4.000	No	Yes	2.00
793	15.86	1.55	100.00	3.19	0.57	0.82	12.15	0.00	12.15	4.000	No	Yes	2.00
794	15.88	1.57	100.00	3.17	0.57	0.82	12.43	0.00	12.43	4.000	No	Yes	2.00
795	15.90	1.57	100.00	3.17	0.57	0.82	12.44	0.00	12.44	4.000	No	Yes	2.00
796	15.92	1.56	100.00	3.18	0.57	0.82	12.16	0.00	12.16	4.000	No	Yes	2.00
797	15.94	1.54	100.00	3.20	0.57	0.82	12.11	0.00	12.11	4.000	No	Yes	2.00
798	15.96	1.52	100.00	3.22	0.57	0.82	11.95	0.00	11.95	4.000	No	Yes	2.00
799	15.98	1.50	100.00	3.24	0.58	0.82	11.61	0.00	11.61	4.000	No	Yes	2.00
800	16.00	1.50	100.00	3.25	0.58	0.82	11.64	0.00	11.64	4.000	No	Yes	2.00
801	16.02	1.49	100.00	3.26	0.58	0.82	11.72	0.00	11.72	4.000	No	Yes	2.00
802	16.04	1.48	100.00	3.26	0.58	0.81	11.33	0.00	11.33	4.000	No	Yes	2.00
803	16.07	1.46	100.00	3.26	0.58	0.81	11.41	0.00	11.41	4.000	No	Yes	2.00
804	16.08	1.46	100.00	3.26	0.58	0.81	11.29	0.00	11.29	4.000	No	Yes	2.00
805	16.10	1.46	100.00	3.25	0.58	0.81	11.28	0.00	11.28	4.000	No	Yes	2.00
806	16.13	1.48	100.00	3.24	0.58	0.81	11.43	0.00	11.43	4.000	No	Yes	2.00
807	16.14	1.51	100.00	3.22	0.58	0.81	11.73	0.00	11.73	4.000	No	Yes	2.00
808	16.16	1.54	100.00	3.21	0.57	0.81	11.90	0.00	11.90	4.000	No	Yes	2.00
809	16.18	1.56	100.00	3.20	0.57	0.81	12.12	0.00	12.12	4.000	No	Yes	2.00
810	16.20	1.59	100.00	3.19	0.57	0.81	12.37	0.00	12.37	4.000	No	Yes	2.00
811	16.22	1.62	100.00	3.18	0.57	0.81	12.57	0.00	12.57	4.000	No	Yes	2.00
812	16.24	1.65	100.00	3.18	0.57	0.81	12.87	0.00	12.87	4.000	No	Yes	2.00
813	16.26	1.68	100.00	3.17	0.57	0.81	13.05	0.00	13.05	4.000	No	Yes	2.00
814	16.28	1.73	100.00	3.15	0.57	0.81	13.32	0.00	13.32	4.000	No	Yes	2.00
815	16.30	1.81	100.00	3.11	0.57	0.81	14.02	0.00	14.02	4.000	No	Yes	2.00
816	16.32	1.89	100.00	3.08	0.56	0.81	14.99	0.00	14.99	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
817	16.34	1.92	100.00	3.07	0.56	0.81	15.13	0.00	15.13	4.000	No	Yes	2.00
818	16.36	1.92	100.00	3.07	0.56	0.81	14.69	0.00	14.69	4.000	No	Yes	2.00
819	16.38	1.93	100.00	3.07	0.56	0.81	15.05	0.00	15.05	4.000	No	Yes	2.00
820	16.40	1.95	100.00	3.06	0.56	0.81	15.20	0.00	15.20	4.000	No	Yes	2.00
821	16.43	1.96	100.00	3.05	0.56	0.81	15.21	0.00	15.21	4.000	No	Yes	2.00
822	16.44	1.93	100.00	3.07	0.56	0.81	15.20	0.00	15.20	4.000	No	Yes	2.00
823	16.46	1.90	100.00	3.09	0.56	0.81	14.60	0.00	14.60	4.000	No	Yes	2.00
824	16.48	1.87	100.00	3.11	0.57	0.81	14.51	0.00	14.51	4.000	No	Yes	2.00
825	16.50	1.86	100.00	3.13	0.57	0.81	14.37	0.00	14.37	4.000	No	Yes	2.00
826	16.52	1.86	100.00	3.14	0.57	0.80	14.41	0.00	14.41	4.000	No	Yes	2.00
827	16.54	1.86	100.00	3.15	0.57	0.80	14.42	0.00	14.42	4.000	No	Yes	2.00
828	16.57	1.90	100.00	3.14	0.57	0.80	14.40	0.00	14.40	4.000	No	Yes	2.00
829	16.58	1.90	100.00	3.14	0.56	0.80	15.34	0.00	15.34	4.000	No	Yes	2.00
830	16.60	1.88	100.00	3.15	0.57	0.80	14.19	0.00	14.19	4.000	No	Yes	2.00
831	16.63	1.83	100.00	3.16	0.57	0.80	13.99	0.00	13.99	4.000	No	Yes	2.00
832	16.64	1.81	100.00	3.16	0.57	0.80	14.06	0.00	14.06	4.000	No	Yes	2.00
833	16.66	1.79	100.00	3.16	0.57	0.80	13.72	0.00	13.72	4.000	No	Yes	2.00
834	16.68	1.77	100.00	3.17	0.57	0.80	13.58	0.00	13.58	4.000	No	Yes	2.00
835	16.70	1.72	100.00	3.18	0.57	0.80	13.35	0.00	13.35	4.000	No	Yes	2.00
836	16.72	1.66	100.00	3.21	0.57	0.80	12.58	0.00	12.58	4.000	No	Yes	2.00
837	16.74	1.60	100.00	3.24	0.57	0.80	12.16	0.00	12.16	4.000	No	Yes	2.00
838	16.76	1.45	100.00	3.29	0.58	0.80	11.87	0.00	11.87	4.000	No	Yes	2.00
839	16.79	1.44	100.00	3.29	0.59	0.79	8.88	0.00	8.88	4.000	No	Yes	2.00
840	16.80	1.44	100.00	3.27	0.58	0.79	11.85	0.00	11.85	4.000	No	Yes	2.00
841	16.83	1.56	100.00	3.22	0.58	0.79	11.82	0.00	11.82	4.000	No	Yes	2.00
842	16.84	1.53	100.00	3.21	0.58	0.79	11.71	0.00	11.71	4.000	No	Yes	2.00
843	16.86	1.47	100.00	3.22	0.58	0.79	11.20	0.00	11.20	4.000	No	Yes	2.00
844	16.88	1.40	100.00	3.23	0.58	0.79	10.35	0.00	10.35	4.000	No	Yes	2.00
845	16.90	1.33	100.00	3.23	0.58	0.79	9.97	0.00	9.97	4.000	No	Yes	2.00
846	16.92	1.29	100.00	3.23	0.58	0.79	9.58	0.00	9.58	4.000	No	Yes	2.00
847	16.94	1.27	100.00	3.22	0.58	0.79	9.42	0.00	9.42	4.000	No	Yes	2.00
848	16.96	1.26	100.00	3.20	0.58	0.79	9.38	0.00	9.38	4.000	No	Yes	2.00
849	16.98	1.24	100.00	3.19	0.59	0.79	9.30	0.00	9.30	4.000	No	Yes	2.00
850	17.00	1.21	100.00	3.19	0.59	0.79	9.02	0.00	9.02	4.000	No	Yes	2.00
851	17.03	1.20	100.00	3.18	0.59	0.79	8.79	0.00	8.79	4.000	No	Yes	2.00
852	17.04	1.21	100.00	3.16	0.59	0.79	8.99	0.00	8.99	4.000	No	Yes	2.00
853	17.06	1.21	100.00	3.14	0.59	0.79	9.08	0.00	9.08	4.000	No	Yes	2.00
854	17.08	1.22	100.00	3.12	0.59	0.78	8.91	0.00	8.91	4.000	No	Yes	2.00
855	17.10	1.23	100.00	3.10	0.59	0.78	9.17	0.00	9.17	4.000	No	Yes	2.00
856	17.12	1.24	100.00	3.09	0.59	0.78	9.20	0.00	9.20	4.000	No	Yes	2.00
857	17.14	1.23	100.00	3.08	0.59	0.78	9.14	0.00	9.14	4.000	No	Yes	2.00
858	17.16	1.22	100.00	3.07	0.59	0.78	9.07	0.00	9.07	4.000	No	Yes	2.00
859	17.19	1.21	100.00	3.08	0.59	0.78	8.96	0.00	8.96	4.000	No	Yes	2.00
860	17.20	1.18	100.00	3.10	0.59	0.78	8.70	0.00	8.70	4.000	No	Yes	2.00
861	17.23	1.16	100.00	3.12	0.59	0.78	8.44	0.00	8.44	4.000	No	Yes	2.00
862	17.24	1.16	100.00	3.11	0.59	0.78	8.59	0.00	8.59	4.000	No	Yes	2.00
863	17.26	1.17	100.00	3.11	0.59	0.78	8.61	0.00	8.61	4.000	No	Yes	2.00
864	17.28	1.16	100.00	3.11	0.59	0.78	8.53	0.00	8.53	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
865	17.31	1.14	100.00	3.11	0.59	0.78	8.33	0.00	8.33	4.000	No	Yes	2.00
866	17.32	1.14	100.00	3.12	0.59	0.78	8.35	0.00	8.35	4.000	No	Yes	2.00
867	17.34	1.13	100.00	3.12	0.59	0.78	8.30	0.00	8.30	4.000	No	Yes	2.00
868	17.36	1.11	100.00	3.13	0.59	0.78	8.22	0.00	8.22	4.000	No	Yes	2.00
869	17.38	1.09	100.00	3.14	0.59	0.78	7.93	0.00	7.93	4.000	No	Yes	2.00
870	17.40	1.06	100.00	3.15	0.59	0.78	7.73	0.00	7.73	4.000	No	Yes	2.00
871	17.42	1.04	100.00	3.16	0.59	0.78	7.55	0.00	7.55	4.000	No	Yes	2.00
872	17.44	1.04	100.00	3.14	0.59	0.78	7.48	0.00	7.48	4.000	No	Yes	2.00
873	17.46	1.05	100.00	3.12	0.59	0.78	7.71	0.00	7.71	4.000	No	Yes	2.00
874	17.48	1.07	100.00	3.09	0.59	0.78	7.76	0.00	7.76	4.000	No	Yes	2.00
875	17.50	1.06	100.00	3.09	0.59	0.78	7.76	0.00	7.76	4.000	No	Yes	2.00
876	17.52	1.06	100.00	3.09	0.59	0.77	7.55	0.00	7.55	4.000	No	Yes	2.00
877	17.54	1.06	100.00	3.09	0.59	0.77	7.67	0.00	7.67	4.000	No	Yes	2.00
878	17.56	1.08	100.00	3.07	0.59	0.77	7.76	0.00	7.76	4.000	No	Yes	2.00
879	17.58	1.10	100.00	3.05	0.59	0.77	7.94	0.00	7.94	4.000	No	Yes	2.00
880	17.60	1.13	100.00	3.03	0.59	0.77	8.10	0.00	8.10	4.000	No	Yes	2.00
881	17.62	1.16	100.00	3.01	0.59	0.77	8.50	0.00	8.50	4.000	No	Yes	2.00
882	17.64	1.22	100.00	2.99	0.59	0.77	8.72	0.00	8.72	4.000	No	Yes	2.00
883	17.66	1.26	99.95	2.96	0.58	0.77	9.34	0.00	9.34	4.000	No	Yes	2.00
884	17.68	1.30	98.57	2.94	0.58	0.77	9.52	0.00	9.52	4.000	No	Yes	2.00
885	17.70	1.29	99.08	2.95	0.58	0.77	9.44	0.00	9.44	4.000	No	Yes	2.00
886	17.72	1.27	100.00	2.98	0.59	0.77	9.24	0.00	9.24	4.000	No	Yes	2.00
887	17.74	1.24	100.00	3.00	0.59	0.77	8.88	0.00	8.88	4.000	No	Yes	2.00
888	17.76	1.31	100.00	3.00	0.59	0.77	8.84	0.00	8.84	4.000	No	Yes	2.00
889	17.78	1.41	100.00	2.99	0.58	0.77	10.76	0.00	10.76	4.000	No	Yes	2.00
890	17.80	1.47	100.00	3.00	0.58	0.77	11.32	0.00	11.32	4.000	No	Yes	2.00
891	17.82	1.42	100.00	3.04	0.58	0.77	10.18	0.00	10.18	4.000	No	Yes	2.00
892	17.84	1.35	100.00	3.09	0.58	0.77	9.69	0.00	9.69	4.000	No	Yes	2.00
893	17.86	1.31	100.00	3.10	0.58	0.77	9.45	0.00	9.45	4.000	No	Yes	2.00
894	17.88	1.29	100.00	3.10	0.58	0.77	9.32	0.00	9.32	4.000	No	Yes	2.00
895	17.90	1.28	100.00	3.09	0.59	0.77	9.16	0.00	9.16	4.000	No	Yes	2.00
896	17.92	1.28	100.00	3.05	0.59	0.77	9.14	0.00	9.14	4.000	No	Yes	2.00
897	17.94	1.29	100.00	3.02	0.58	0.77	9.46	0.00	9.46	4.000	No	Yes	2.00
898	17.96	1.31	100.00	2.99	0.58	0.77	9.40	0.00	9.40	4.000	No	Yes	2.00
899	17.98	1.33	100.00	2.98	0.58	0.77	9.45	0.00	9.45	4.000	No	Yes	2.00
900	18.00	1.35	100.00	2.96	0.58	0.77	9.85	0.00	9.85	4.000	No	Yes	2.00
901	18.02	1.35	100.00	2.96	0.58	0.77	9.90	0.00	9.90	4.000	No	Yes	2.00
902	18.04	1.33	100.00	2.99	0.58	0.77	9.42	0.00	9.42	4.000	No	Yes	2.00
903	18.06	1.33	100.00	3.00	0.58	0.77	9.35	0.00	9.35	4.000	No	Yes	2.00
904	18.08	1.31	100.00	3.01	0.58	0.77	9.86	0.00	9.86	4.000	No	Yes	2.00
905	18.10	1.27	100.00	3.03	0.59	0.77	8.97	0.00	8.97	4.000	No	Yes	2.00
906	18.12	1.21	100.00	3.07	0.59	0.77	8.50	0.00	8.50	4.000	No	Yes	2.00
907	18.14	1.20	100.00	3.09	0.59	0.76	8.55	0.00	8.55	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS

Abbreviations

Depth: Depth from free surface, at which CPT was performed (m)
q_t: Total cone resistance
FC: Fines content (%)
I_c: Soil behavior type index
m: Stress exponent
C_N: Overburden correction factor
q_{c1N}: Normalized and adjusted cone resistance
Δq_{c1N}: Cone resistance correction factor due to fines
$q_{c1N,cs}$: Normalized and adjusted cone resistance
$CRR_{7.5}$: Cyclic resistance ratio for M_w=7.5
FS: Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
0.03	2.00	0.00	9.99	0.01	0.00	0.04	2.00	0.00	9.98	0.01	0.00
0.07	2.00	0.00	9.97	0.03	0.00	0.08	2.00	0.00	9.96	0.01	0.00
0.10	2.00	0.00	9.95	0.02	0.00	0.12	2.00	0.00	9.94	0.02	0.00
0.14	2.00	0.00	9.93	0.02	0.00	0.17	2.00	0.00	9.91	0.03	0.00
0.18	2.00	0.00	9.91	0.01	0.00	0.20	2.00	0.00	9.90	0.02	0.00
0.22	2.00	0.00	9.89	0.02	0.00	0.24	2.00	0.00	9.88	0.02	0.00
0.26	2.00	0.00	9.87	0.02	0.00	0.28	2.00	0.00	9.86	0.02	0.00
0.30	2.00	0.00	9.85	0.02	0.00	0.32	2.00	0.00	9.84	0.02	0.00
0.34	2.00	0.00	9.83	0.02	0.00	0.36	2.00	0.00	9.82	0.02	0.00
0.38	2.00	0.00	9.81	0.02	0.00	0.40	2.00	0.00	9.80	0.02	0.00
0.42	2.00	0.00	9.79	0.02	0.00	0.44	2.00	0.00	9.78	0.02	0.00
0.46	2.00	0.00	9.77	0.02	0.00	0.48	2.00	0.00	9.76	0.02	0.00
0.50	2.00	0.00	9.75	0.02	0.00	0.52	2.00	0.00	9.74	0.02	0.00
0.54	2.00	0.00	9.73	0.02	0.00	0.56	2.00	0.00	9.72	0.02	0.00
0.58	2.00	0.00	9.71	0.02	0.00	0.60	2.00	0.00	9.70	0.02	0.00
0.62	2.00	0.00	9.69	0.02	0.00	0.64	2.00	0.00	9.68	0.02	0.00
0.66	2.00	0.00	9.67	0.02	0.00	0.68	2.00	0.00	9.66	0.02	0.00
0.70	2.00	0.00	9.65	0.02	0.00	0.72	2.00	0.00	9.64	0.02	0.00
0.74	2.00	0.00	9.63	0.02	0.00	0.76	2.00	0.00	9.62	0.02	0.00
0.78	2.00	0.00	9.61	0.02	0.00	0.80	2.00	0.00	9.60	0.02	0.00
0.82	2.00	0.00	9.59	0.02	0.00	0.84	2.00	0.00	9.58	0.02	0.00
0.86	2.00	0.00	9.57	0.02	0.00	0.88	2.00	0.00	9.56	0.02	0.00
0.90	2.00	0.00	9.55	0.02	0.00	0.92	2.00	0.00	9.54	0.02	0.00
0.94	2.00	0.00	9.53	0.02	0.00	0.97	2.00	0.00	9.52	0.03	0.00
0.98	2.00	0.00	9.51	0.01	0.00	1.01	2.00	0.00	9.49	0.03	0.00
1.02	2.00	0.00	9.49	0.01	0.00	1.04	2.00	0.00	9.48	0.02	0.00
1.06	2.00	0.00	9.47	0.02	0.00	1.08	2.00	0.00	9.46	0.02	0.00
1.10	2.00	0.00	9.45	0.02	0.00	1.13	2.00	0.00	9.44	0.03	0.00
1.14	2.00	0.00	9.43	0.01	0.00	1.16	2.00	0.00	9.42	0.02	0.00
1.19	2.00	0.00	9.41	0.03	0.00	1.20	2.00	0.00	9.40	0.01	0.00
1.22	2.00	0.00	9.39	0.02	0.00	1.24	2.00	0.00	9.38	0.02	0.00
1.26	2.00	0.00	9.37	0.02	0.00	1.28	2.00	0.00	9.36	0.02	0.00
1.30	2.00	0.00	9.35	0.02	0.00	1.32	2.00	0.00	9.34	0.02	0.00
1.34	2.00	0.00	9.33	0.02	0.00	1.36	2.00	0.00	9.32	0.02	0.00
1.38	2.00	0.00	9.31	0.02	0.00	1.40	2.00	0.00	9.30	0.02	0.00
1.42	2.00	0.00	9.29	0.02	0.00	1.44	2.00	0.00	9.28	0.02	0.00
1.46	2.00	0.00	9.27	0.02	0.00	1.48	2.00	0.00	9.26	0.02	0.00
1.50	2.00	0.00	9.25	0.02	0.00	1.52	2.00	0.00	9.24	0.02	0.00
1.54	2.00	0.00	9.23	0.02	0.00	1.56	2.00	0.00	9.22	0.02	0.00
1.58	2.00	0.00	9.21	0.02	0.00	1.60	2.00	0.00	9.20	0.02	0.00
1.62	2.00	0.00	9.19	0.02	0.00	1.64	2.00	0.00	9.18	0.02	0.00
1.66	2.00	0.00	9.17	0.02	0.00	1.68	2.00	0.00	9.16	0.02	0.00
1.70	2.00	0.00	9.15	0.02	0.00	1.72	2.00	0.00	9.14	0.02	0.00
1.74	2.00	0.00	9.13	0.02	0.00	1.76	2.00	0.00	9.12	0.02	0.00
1.78	2.00	0.00	9.11	0.02	0.00	1.80	2.00	0.00	9.10	0.02	0.00
1.82	2.00	0.00	9.09	0.02	0.00	1.84	2.00	0.00	9.08	0.02	0.00
1.86	2.00	0.00	9.07	0.02	0.00	1.88	2.00	0.00	9.06	0.02	0.00
1.90	2.00	0.00	9.05	0.02	0.00	1.92	2.00	0.00	9.04	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
1.94	2.00	0.00	9.03	0.02	0.00	1.96	2.00	0.00	9.02	0.02	0.00
1.98	2.00	0.00	9.01	0.02	0.00	2.01	2.00	0.00	8.99	0.03	0.00
2.02	2.00	0.00	8.99	0.01	0.00	2.04	2.00	0.00	8.98	0.02	0.00
2.06	2.00	0.00	8.97	0.02	0.00	2.08	2.00	0.00	8.96	0.02	0.00
2.10	2.00	0.00	8.95	0.02	0.00	2.12	2.00	0.00	8.94	0.02	0.00
2.14	2.00	0.00	8.93	0.02	0.00	2.16	2.00	0.00	8.92	0.02	0.00
2.18	2.00	0.00	8.91	0.02	0.00	2.21	2.00	0.00	8.90	0.03	0.00
2.22	2.00	0.00	8.89	0.01	0.00	2.24	2.00	0.00	8.88	0.02	0.00
2.26	2.00	0.00	8.87	0.02	0.00	2.28	2.00	0.00	8.86	0.02	0.00
2.30	2.00	0.00	8.85	0.02	0.00	2.32	2.00	0.00	8.84	0.02	0.00
2.34	2.00	0.00	8.83	0.02	0.00	2.36	2.00	0.00	8.82	0.02	0.00
2.38	2.00	0.00	8.81	0.02	0.00	2.40	2.00	0.00	8.80	0.02	0.00
2.42	2.00	0.00	8.79	0.02	0.00	2.44	2.00	0.00	8.78	0.02	0.00
2.46	2.00	0.00	8.77	0.02	0.00	2.48	2.00	0.00	8.76	0.02	0.00
2.50	2.00	0.00	8.75	0.02	0.00	2.52	2.00	0.00	8.74	0.02	0.00
2.54	2.00	0.00	8.73	0.02	0.00	2.56	2.00	0.00	8.72	0.02	0.00
2.58	2.00	0.00	8.71	0.02	0.00	2.60	2.00	0.00	8.70	0.02	0.00
2.62	2.00	0.00	8.69	0.02	0.00	2.64	2.00	0.00	8.68	0.02	0.00
2.66	2.00	0.00	8.67	0.02	0.00	2.68	2.00	0.00	8.66	0.02	0.00
2.70	2.00	0.00	8.65	0.02	0.00	2.72	2.00	0.00	8.64	0.02	0.00
2.74	2.00	0.00	8.63	0.02	0.00	2.76	2.00	0.00	8.62	0.02	0.00
2.78	2.00	0.00	8.61	0.02	0.00	2.80	2.00	0.00	8.60	0.02	0.00
2.82	2.00	0.00	8.59	0.02	0.00	2.84	2.00	0.00	8.58	0.02	0.00
2.86	2.00	0.00	8.57	0.02	0.00	2.88	2.00	0.00	8.56	0.02	0.00
2.92	2.00	0.00	8.54	0.04	0.00	2.92	2.00	0.00	8.54	0.00	0.00
2.94	2.00	0.00	8.53	0.02	0.00	2.97	2.00	0.00	8.52	0.03	0.00
2.99	2.00	0.00	8.51	0.02	0.00	3.00	2.00	0.00	8.50	0.01	0.00
3.02	2.00	0.00	8.49	0.02	0.00	3.05	2.00	0.00	8.48	0.03	0.00
3.06	2.00	0.00	8.47	0.01	0.00	3.08	2.00	0.00	8.46	0.02	0.00
3.10	2.00	0.00	8.45	0.02	0.00	3.12	2.00	0.00	8.44	0.02	0.00
3.14	2.00	0.00	8.43	0.02	0.00	3.16	2.00	0.00	8.42	0.02	0.00
3.18	2.00	0.00	8.41	0.02	0.00	3.20	2.00	0.00	8.40	0.02	0.00
3.22	2.00	0.00	8.39	0.02	0.00	3.24	2.00	0.00	8.38	0.02	0.00
3.26	2.00	0.00	8.37	0.02	0.00	3.28	2.00	0.00	8.36	0.02	0.00
3.30	2.00	0.00	8.35	0.02	0.00	3.32	2.00	0.00	8.34	0.02	0.00
3.34	2.00	0.00	8.33	0.02	0.00	3.36	2.00	0.00	8.32	0.02	0.00
3.38	2.00	0.00	8.31	0.02	0.00	3.40	2.00	0.00	8.30	0.02	0.00
3.42	2.00	0.00	8.29	0.02	0.00	3.44	2.00	0.00	8.28	0.02	0.00
3.46	2.00	0.00	8.27	0.02	0.00	3.49	2.00	0.00	8.26	0.03	0.00
3.50	2.00	0.00	8.25	0.01	0.00	3.52	2.00	0.00	8.24	0.02	0.00
3.54	2.00	0.00	8.23	0.02	0.00	3.56	2.00	0.00	8.22	0.02	0.00
3.58	2.00	0.00	8.21	0.02	0.00	3.60	2.00	0.00	8.20	0.02	0.00
3.62	2.00	0.00	8.19	0.02	0.00	3.64	2.00	0.00	8.18	0.02	0.00
3.66	2.00	0.00	8.17	0.02	0.00	3.68	2.00	0.00	8.16	0.02	0.00
3.70	2.00	0.00	8.15	0.02	0.00	3.72	2.00	0.00	8.14	0.02	0.00
3.74	2.00	0.00	8.13	0.02	0.00	3.76	2.00	0.00	8.12	0.02	0.00
3.78	2.00	0.00	8.11	0.02	0.00	3.80	2.00	0.00	8.10	0.02	0.00
3.82	2.00	0.00	8.09	0.02	0.00	3.84	2.00	0.00	8.08	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
3.86	2.00	0.00	8.07	0.02	0.00	3.88	2.00	0.00	8.06	0.02	0.00
3.90	2.00	0.00	8.05	0.02	0.00	3.92	2.00	0.00	8.04	0.02	0.00
3.94	2.00	0.00	8.03	0.02	0.00	3.96	2.00	0.00	8.02	0.02	0.00
3.98	2.00	0.00	8.01	0.02	0.00	4.00	2.00	0.00	8.00	0.02	0.00
4.02	2.00	0.00	7.99	0.02	0.00	4.05	2.00	0.00	7.98	0.03	0.00
4.06	2.00	0.00	7.97	0.01	0.00	4.08	2.00	0.00	7.96	0.02	0.00
4.10	2.00	0.00	7.95	0.02	0.00	4.12	2.00	0.00	7.94	0.02	0.00
4.14	2.00	0.00	7.93	0.02	0.00	4.16	2.00	0.00	7.92	0.02	0.00
4.18	2.00	0.00	7.91	0.02	0.00	4.20	2.00	0.00	7.90	0.02	0.00
4.22	2.00	0.00	7.89	0.02	0.00	4.24	2.00	0.00	7.88	0.02	0.00
4.26	2.00	0.00	7.87	0.02	0.00	4.28	2.00	0.00	7.86	0.02	0.00
4.30	2.00	0.00	7.85	0.02	0.00	4.32	2.00	0.00	7.84	0.02	0.00
4.34	2.00	0.00	7.83	0.02	0.00	4.36	2.00	0.00	7.82	0.02	0.00
4.38	2.00	0.00	7.81	0.02	0.00	4.40	2.00	0.00	7.80	0.02	0.00
4.42	2.00	0.00	7.79	0.02	0.00	4.44	2.00	0.00	7.78	0.02	0.00
4.46	2.00	0.00	7.77	0.02	0.00	4.48	2.00	0.00	7.76	0.02	0.00
4.50	2.00	0.00	7.75	0.02	0.00	4.52	2.00	0.00	7.74	0.02	0.00
4.54	2.00	0.00	7.73	0.02	0.00	4.56	2.00	0.00	7.72	0.02	0.00
4.58	2.00	0.00	7.71	0.02	0.00	4.60	2.00	0.00	7.70	0.02	0.00
4.62	2.00	0.00	7.69	0.02	0.00	4.64	2.00	0.00	7.68	0.02	0.00
4.66	2.00	0.00	7.67	0.02	0.00	4.68	2.00	0.00	7.66	0.02	0.00
4.70	2.00	0.00	7.65	0.02	0.00	4.72	2.00	0.00	7.64	0.02	0.00
4.74	2.00	0.00	7.63	0.02	0.00	4.76	2.00	0.00	7.62	0.02	0.00
4.78	2.00	0.00	7.61	0.02	0.00	4.80	2.00	0.00	7.60	0.02	0.00
4.82	2.00	0.00	7.59	0.02	0.00	4.84	2.00	0.00	7.58	0.02	0.00
4.86	2.00	0.00	7.57	0.02	0.00	4.88	2.00	0.00	7.56	0.02	0.00
4.90	2.00	0.00	7.55	0.02	0.00	4.92	2.00	0.00	7.54	0.02	0.00
4.94	2.00	0.00	7.53	0.02	0.00	4.96	2.00	0.00	7.52	0.02	0.00
4.98	2.00	0.00	7.51	0.02	0.00	5.00	2.00	0.00	7.50	0.02	0.00
5.02	2.00	0.00	7.49	0.02	0.00	5.04	2.00	0.00	7.48	0.02	0.00
5.06	2.00	0.00	7.47	0.02	0.00	5.08	2.00	0.00	7.46	0.02	0.00
5.10	2.00	0.00	7.45	0.02	0.00	5.12	2.00	0.00	7.44	0.02	0.00
5.14	2.00	0.00	7.43	0.02	0.00	5.16	2.00	0.00	7.42	0.02	0.00
5.19	2.00	0.00	7.41	0.03	0.00	5.20	2.00	0.00	7.40	0.01	0.00
5.22	2.00	0.00	7.39	0.02	0.00	5.24	2.00	0.00	7.38	0.02	0.00
5.26	2.00	0.00	7.37	0.02	0.00	5.28	2.00	0.00	7.36	0.02	0.00
5.30	2.00	0.00	7.35	0.02	0.00	5.32	2.00	0.00	7.34	0.02	0.00
5.34	2.00	0.00	7.33	0.02	0.00	5.36	2.00	0.00	7.32	0.02	0.00
5.38	2.00	0.00	7.31	0.02	0.00	5.40	2.00	0.00	7.30	0.02	0.00
5.42	2.00	0.00	7.29	0.02	0.00	5.44	2.00	0.00	7.28	0.02	0.00
5.46	2.00	0.00	7.27	0.02	0.00	5.48	2.00	0.00	7.26	0.02	0.00
5.50	2.00	0.00	7.25	0.02	0.00	5.52	2.00	0.00	7.24	0.02	0.00
5.54	2.00	0.00	7.23	0.02	0.00	5.56	2.00	0.00	7.22	0.02	0.00
5.58	2.00	0.00	7.21	0.02	0.00	5.60	2.00	0.00	7.20	0.02	0.00
5.62	2.00	0.00	7.19	0.02	0.00	5.64	2.00	0.00	7.18	0.02	0.00
5.66	2.00	0.00	7.17	0.02	0.00	5.68	2.00	0.00	7.16	0.02	0.00
5.70	2.00	0.00	7.15	0.02	0.00	5.72	2.00	0.00	7.14	0.02	0.00
5.74	2.00	0.00	7.13	0.02	0.00	5.76	2.00	0.00	7.12	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
5.78	2.00	0.00	7.11	0.02	0.00	5.80	2.00	0.00	7.10	0.02	0.00
5.82	2.00	0.00	7.09	0.02	0.00	5.84	2.00	0.00	7.08	0.02	0.00
5.86	2.00	0.00	7.07	0.02	0.00	5.89	2.00	0.00	7.06	0.03	0.00
5.90	2.00	0.00	7.05	0.01	0.00	5.92	2.00	0.00	7.04	0.02	0.00
5.94	2.00	0.00	7.03	0.02	0.00	5.96	2.00	0.00	7.02	0.02	0.00
5.98	2.00	0.00	7.01	0.02	0.00	6.01	2.00	0.00	7.00	0.03	0.00
6.02	2.00	0.00	6.99	0.01	0.00	6.04	2.00	0.00	6.98	0.02	0.00
6.06	2.00	0.00	6.97	0.02	0.00	6.08	2.00	0.00	6.96	0.02	0.00
6.10	2.00	0.00	6.95	0.02	0.00	6.12	2.00	0.00	6.94	0.02	0.00
6.14	2.00	0.00	6.93	0.02	0.00	6.16	2.00	0.00	6.92	0.02	0.00
6.18	2.00	0.00	6.91	0.02	0.00	6.21	2.00	0.00	6.90	0.03	0.00
6.22	2.00	0.00	6.89	0.01	0.00	6.25	2.00	0.00	6.88	0.03	0.00
6.26	2.00	0.00	6.87	0.01	0.00	6.28	2.00	0.00	6.86	0.02	0.00
6.30	2.00	0.00	6.85	0.02	0.00	6.32	2.00	0.00	6.84	0.02	0.00
6.34	2.00	0.00	6.83	0.02	0.00	6.36	2.00	0.00	6.82	0.02	0.00
6.38	2.00	0.00	6.81	0.02	0.00	6.40	2.00	0.00	6.80	0.02	0.00
6.42	2.00	0.00	6.79	0.02	0.00	6.44	2.00	0.00	6.78	0.02	0.00
6.46	2.00	0.00	6.77	0.02	0.00	6.48	2.00	0.00	6.76	0.02	0.00
6.50	2.00	0.00	6.75	0.02	0.00	6.52	2.00	0.00	6.74	0.02	0.00
6.54	2.00	0.00	6.73	0.02	0.00	6.56	2.00	0.00	6.72	0.02	0.00
6.58	2.00	0.00	6.71	0.02	0.00	6.60	2.00	0.00	6.70	0.02	0.00
6.62	2.00	0.00	6.69	0.02	0.00	6.64	2.00	0.00	6.68	0.02	0.00
6.66	2.00	0.00	6.67	0.02	0.00	6.68	2.00	0.00	6.66	0.02	0.00
6.70	2.00	0.00	6.65	0.02	0.00	6.72	2.00	0.00	6.64	0.02	0.00
6.74	2.00	0.00	6.63	0.02	0.00	6.76	2.00	0.00	6.62	0.02	0.00
6.78	2.00	0.00	6.61	0.02	0.00	6.80	2.00	0.00	6.60	0.02	0.00
6.82	2.00	0.00	6.59	0.02	0.00	6.84	2.00	0.00	6.58	0.02	0.00
6.86	2.00	0.00	6.57	0.02	0.00	6.88	2.00	0.00	6.56	0.02	0.00
6.90	2.00	0.00	6.55	0.02	0.00	6.92	2.00	0.00	6.54	0.02	0.00
6.94	2.00	0.00	6.53	0.02	0.00	6.96	2.00	0.00	6.52	0.02	0.00
6.98	2.00	0.00	6.51	0.02	0.00	7.00	2.00	0.00	6.50	0.02	0.00
7.02	2.00	0.00	6.49	0.02	0.00	7.04	2.00	0.00	6.48	0.02	0.00
7.06	2.00	0.00	6.47	0.02	0.00	7.08	2.00	0.00	6.46	0.02	0.00
7.10	2.00	0.00	6.45	0.02	0.00	7.12	2.00	0.00	6.44	0.02	0.00
7.14	2.00	0.00	6.43	0.02	0.00	7.16	2.00	0.00	6.42	0.02	0.00
7.18	2.00	0.00	6.41	0.02	0.00	7.20	2.00	0.00	6.40	0.02	0.00
7.22	2.00	0.00	6.39	0.02	0.00	7.24	2.00	0.00	6.38	0.02	0.00
7.26	2.00	0.00	6.37	0.02	0.00	7.28	2.00	0.00	6.36	0.02	0.00
7.30	2.00	0.00	6.35	0.02	0.00	7.32	2.00	0.00	6.34	0.02	0.00
7.34	2.00	0.00	6.33	0.02	0.00	7.36	2.00	0.00	6.32	0.02	0.00
7.38	2.00	0.00	6.31	0.02	0.00	7.40	2.00	0.00	6.30	0.02	0.00
7.42	2.00	0.00	6.29	0.02	0.00	7.44	2.00	0.00	6.28	0.02	0.00
7.46	2.00	0.00	6.27	0.02	0.00	7.48	2.00	0.00	6.26	0.02	0.00
7.50	2.00	0.00	6.25	0.02	0.00	7.52	2.00	0.00	6.24	0.02	0.00
7.54	2.00	0.00	6.23	0.02	0.00	7.56	2.00	0.00	6.22	0.02	0.00
7.58	2.00	0.00	6.21	0.02	0.00	7.60	2.00	0.00	6.20	0.02	0.00
7.62	2.00	0.00	6.19	0.02	0.00	7.64	2.00	0.00	6.18	0.02	0.00
7.66	2.00	0.00	6.17	0.02	0.00	7.68	2.00	0.00	6.16	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
7.70	2.00	0.00	6.15	0.02	0.00	7.72	2.00	0.00	6.14	0.02	0.00
7.74	2.00	0.00	6.13	0.02	0.00	7.76	2.00	0.00	6.12	0.02	0.00
7.78	2.00	0.00	6.11	0.02	0.00	7.80	2.00	0.00	6.10	0.02	0.00
7.82	2.00	0.00	6.09	0.02	0.00	7.84	2.00	0.00	6.08	0.02	0.00
7.86	2.00	0.00	6.07	0.02	0.00	7.88	2.00	0.00	6.06	0.02	0.00
7.90	2.00	0.00	6.05	0.02	0.00	7.92	2.00	0.00	6.04	0.02	0.00
7.94	2.00	0.00	6.03	0.02	0.00	7.96	2.00	0.00	6.02	0.02	0.00
7.98	2.00	0.00	6.01	0.02	0.00	8.00	2.00	0.00	6.00	0.02	0.00
8.02	2.00	0.00	5.99	0.02	0.00	8.04	2.00	0.00	5.98	0.02	0.00
8.07	2.00	0.00	5.97	0.03	0.00	8.08	2.00	0.00	5.96	0.01	0.00
8.10	2.00	0.00	5.95	0.02	0.00	8.12	2.00	0.00	5.94	0.02	0.00
8.14	2.00	0.00	5.93	0.02	0.00	8.16	2.00	0.00	5.92	0.02	0.00
8.18	2.00	0.00	5.91	0.02	0.00	8.20	2.00	0.00	5.90	0.02	0.00
8.22	2.00	0.00	5.89	0.02	0.00	8.24	2.00	0.00	5.88	0.02	0.00
8.26	2.00	0.00	5.87	0.02	0.00	8.28	2.00	0.00	5.86	0.02	0.00
8.30	2.00	0.00	5.85	0.02	0.00	8.32	2.00	0.00	5.84	0.02	0.00
8.34	2.00	0.00	5.83	0.02	0.00	8.36	2.00	0.00	5.82	0.02	0.00
8.38	2.00	0.00	5.81	0.02	0.00	8.40	2.00	0.00	5.80	0.02	0.00
8.42	2.00	0.00	5.79	0.02	0.00	8.44	2.00	0.00	5.78	0.02	0.00
8.47	2.00	0.00	5.77	0.03	0.00	8.48	2.00	0.00	5.76	0.01	0.00
8.50	2.00	0.00	5.75	0.02	0.00	8.52	2.00	0.00	5.74	0.02	0.00
8.54	2.00	0.00	5.73	0.02	0.00	8.56	2.00	0.00	5.72	0.02	0.00
8.58	2.00	0.00	5.71	0.02	0.00	8.60	2.00	0.00	5.70	0.02	0.00
8.62	2.00	0.00	5.69	0.02	0.00	8.64	2.00	0.00	5.68	0.02	0.00
8.66	2.00	0.00	5.67	0.02	0.00	8.68	2.00	0.00	5.66	0.02	0.00
8.70	2.00	0.00	5.65	0.02	0.00	8.72	2.00	0.00	5.64	0.02	0.00
8.74	2.00	0.00	5.63	0.02	0.00	8.76	2.00	0.00	5.62	0.02	0.00
8.78	2.00	0.00	5.61	0.02	0.00	8.80	2.00	0.00	5.60	0.02	0.00
8.82	2.00	0.00	5.59	0.02	0.00	8.84	2.00	0.00	5.58	0.02	0.00
8.86	2.00	0.00	5.57	0.02	0.00	8.88	2.00	0.00	5.56	0.02	0.00
8.90	2.00	0.00	5.55	0.02	0.00	8.92	2.00	0.00	5.54	0.02	0.00
8.94	2.00	0.00	5.53	0.02	0.00	8.96	2.00	0.00	5.52	0.02	0.00
8.98	2.00	0.00	5.51	0.02	0.00	9.00	2.00	0.00	5.50	0.02	0.00
9.02	2.00	0.00	5.49	0.02	0.00	9.04	2.00	0.00	5.48	0.02	0.00
9.06	2.00	0.00	5.47	0.02	0.00	9.09	2.00	0.00	5.46	0.03	0.00
9.10	2.00	0.00	5.45	0.01	0.00	9.13	2.00	0.00	5.43	0.03	0.00
9.14	2.00	0.00	5.43	0.01	0.00	9.16	2.00	0.00	5.42	0.02	0.00
9.18	2.00	0.00	5.41	0.02	0.00	9.20	2.00	0.00	5.40	0.02	0.00
9.22	2.00	0.00	5.39	0.02	0.00	9.24	2.00	0.00	5.38	0.02	0.00
9.26	2.00	0.00	5.37	0.02	0.00	9.28	2.00	0.00	5.36	0.02	0.00
9.30	2.00	0.00	5.35	0.02	0.00	9.32	2.00	0.00	5.34	0.02	0.00
9.34	2.00	0.00	5.33	0.02	0.00	9.36	2.00	0.00	5.32	0.02	0.00
9.38	2.00	0.00	5.31	0.02	0.00	9.40	2.00	0.00	5.30	0.02	0.00
9.42	2.00	0.00	5.29	0.02	0.00	9.44	2.00	0.00	5.28	0.02	0.00
9.47	2.00	0.00	5.27	0.03	0.00	9.48	2.00	0.00	5.26	0.01	0.00
9.50	2.00	0.00	5.25	0.02	0.00	9.52	2.00	0.00	5.24	0.02	0.00
9.54	2.00	0.00	5.23	0.02	0.00	9.56	2.00	0.00	5.22	0.02	0.00
9.58	2.00	0.00	5.21	0.02	0.00	9.60	2.00	0.00	5.20	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
9.62	2.00	0.00	5.19	0.02	0.00	9.64	2.00	0.00	5.18	0.02	0.00
9.66	2.00	0.00	5.17	0.02	0.00	9.68	2.00	0.00	5.16	0.02	0.00
9.70	2.00	0.00	5.15	0.02	0.00	9.72	2.00	0.00	5.14	0.02	0.00
9.74	2.00	0.00	5.13	0.02	0.00	9.76	2.00	0.00	5.12	0.02	0.00
9.78	2.00	0.00	5.11	0.02	0.00	9.80	2.00	0.00	5.10	0.02	0.00
9.82	2.00	0.00	5.09	0.02	0.00	9.84	2.00	0.00	5.08	0.02	0.00
9.86	2.00	0.00	5.07	0.02	0.00	9.88	2.00	0.00	5.06	0.02	0.00
9.91	2.00	0.00	5.05	0.03	0.00	9.92	2.00	0.00	5.04	0.01	0.00
9.94	2.00	0.00	5.03	0.02	0.00	9.96	2.00	0.00	5.02	0.02	0.00
9.98	2.00	0.00	5.01	0.02	0.00	10.00	2.00	0.00	5.00	0.02	0.00
10.02	2.00	0.00	4.99	0.02	0.00	10.04	2.00	0.00	4.98	0.02	0.00
10.06	2.00	0.00	4.97	0.02	0.00	10.08	2.00	0.00	4.96	0.02	0.00
10.10	2.00	0.00	4.95	0.02	0.00	10.12	2.00	0.00	4.94	0.02	0.00
10.14	2.00	0.00	4.93	0.02	0.00	10.16	2.00	0.00	4.92	0.02	0.00
10.18	2.00	0.00	4.91	0.02	0.00	10.20	2.00	0.00	4.90	0.02	0.00
10.22	2.00	0.00	4.89	0.02	0.00	10.24	2.00	0.00	4.88	0.02	0.00
10.26	2.00	0.00	4.87	0.02	0.00	10.28	2.00	0.00	4.86	0.02	0.00
10.30	2.00	0.00	4.85	0.02	0.00	10.32	2.00	0.00	4.84	0.02	0.00
10.34	2.00	0.00	4.83	0.02	0.00	10.36	2.00	0.00	4.82	0.02	0.00
10.38	2.00	0.00	4.81	0.02	0.00	10.40	2.00	0.00	4.80	0.02	0.00
10.42	2.00	0.00	4.79	0.02	0.00	10.44	2.00	0.00	4.78	0.02	0.00
10.46	2.00	0.00	4.77	0.02	0.00	10.48	2.00	0.00	4.76	0.02	0.00
10.50	2.00	0.00	4.75	0.02	0.00	10.52	2.00	0.00	4.74	0.02	0.00
10.54	2.00	0.00	4.73	0.02	0.00	10.56	2.00	0.00	4.72	0.02	0.00
10.58	2.00	0.00	4.71	0.02	0.00	10.60	2.00	0.00	4.70	0.02	0.00
10.62	2.00	0.00	4.69	0.02	0.00	10.64	2.00	0.00	4.68	0.02	0.00
10.66	2.00	0.00	4.67	0.02	0.00	10.68	2.00	0.00	4.66	0.02	0.00
10.70	2.00	0.00	4.65	0.02	0.00	10.72	2.00	0.00	4.64	0.02	0.00
10.74	2.00	0.00	4.63	0.02	0.00	10.76	2.00	0.00	4.62	0.02	0.00
10.78	2.00	0.00	4.61	0.02	0.00	10.80	2.00	0.00	4.60	0.02	0.00
10.82	2.00	0.00	4.59	0.02	0.00	10.84	2.00	0.00	4.58	0.02	0.00
10.86	2.00	0.00	4.57	0.02	0.00	10.88	2.00	0.00	4.56	0.02	0.00
10.90	2.00	0.00	4.55	0.02	0.00	10.92	2.00	0.00	4.54	0.02	0.00
10.94	2.00	0.00	4.53	0.02	0.00	10.96	2.00	0.00	4.52	0.02	0.00
10.98	2.00	0.00	4.51	0.02	0.00	11.00	2.00	0.00	4.50	0.02	0.00
11.02	2.00	0.00	4.49	0.02	0.00	11.04	2.00	0.00	4.48	0.02	0.00
11.06	2.00	0.00	4.47	0.02	0.00	11.08	2.00	0.00	4.46	0.02	0.00
11.10	2.00	0.00	4.45	0.02	0.00	11.13	2.00	0.00	4.43	0.03	0.00
11.14	2.00	0.00	4.43	0.01	0.00	11.16	2.00	0.00	4.42	0.02	0.00
11.18	2.00	0.00	4.41	0.02	0.00	11.20	2.00	0.00	4.40	0.02	0.00
11.22	2.00	0.00	4.39	0.02	0.00	11.24	2.00	0.00	4.38	0.02	0.00
11.26	2.00	0.00	4.37	0.02	0.00	11.28	2.00	0.00	4.36	0.02	0.00
11.30	2.00	0.00	4.35	0.02	0.00	11.32	2.00	0.00	4.34	0.02	0.00
11.34	2.00	0.00	4.33	0.02	0.00	11.36	2.00	0.00	4.32	0.02	0.00
11.38	2.00	0.00	4.31	0.02	0.00	11.40	2.00	0.00	4.30	0.02	0.00
11.42	2.00	0.00	4.29	0.02	0.00	11.44	2.00	0.00	4.28	0.02	0.00
11.46	2.00	0.00	4.27	0.02	0.00	11.48	2.00	0.00	4.26	0.02	0.00
11.50	2.00	0.00	4.25	0.02	0.00	11.52	2.00	0.00	4.24	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
11.54	2.00	0.00	4.23	0.02	0.00	11.56	2.00	0.00	4.22	0.02	0.00
11.58	2.00	0.00	4.21	0.02	0.00	11.60	2.00	0.00	4.20	0.02	0.00
11.62	2.00	0.00	4.19	0.02	0.00	11.64	2.00	0.00	4.18	0.02	0.00
11.66	2.00	0.00	4.17	0.02	0.00	11.68	2.00	0.00	4.16	0.02	0.00
11.70	2.00	0.00	4.15	0.02	0.00	11.72	2.00	0.00	4.14	0.02	0.00
11.74	2.00	0.00	4.13	0.02	0.00	11.76	2.00	0.00	4.12	0.02	0.00
11.78	2.00	0.00	4.11	0.02	0.00	11.80	2.00	0.00	4.10	0.02	0.00
11.82	2.00	0.00	4.09	0.02	0.00	11.84	2.00	0.00	4.08	0.02	0.00
11.86	2.00	0.00	4.07	0.02	0.00	11.88	2.00	0.00	4.06	0.02	0.00
11.90	2.00	0.00	4.05	0.02	0.00	11.92	2.00	0.00	4.04	0.02	0.00
11.94	2.00	0.00	4.03	0.02	0.00	11.96	2.00	0.00	4.02	0.02	0.00
11.98	2.00	0.00	4.01	0.02	0.00	12.00	2.00	0.00	4.00	0.02	0.00
12.02	2.00	0.00	3.99	0.02	0.00	12.04	2.00	0.00	3.98	0.02	0.00
12.06	2.00	0.00	3.97	0.02	0.00	12.08	2.00	0.00	3.96	0.02	0.00
12.10	2.00	0.00	3.95	0.02	0.00	12.12	2.00	0.00	3.94	0.02	0.00
12.14	2.00	0.00	3.93	0.02	0.00	12.16	2.00	0.00	3.92	0.02	0.00
12.18	2.00	0.00	3.91	0.02	0.00	12.21	2.00	0.00	3.90	0.03	0.00
12.22	2.00	0.00	3.89	0.01	0.00	12.24	2.00	0.00	3.88	0.02	0.00
12.26	2.00	0.00	3.87	0.02	0.00	12.28	2.00	0.00	3.86	0.02	0.00
12.30	2.00	0.00	3.85	0.02	0.00	12.32	2.00	0.00	3.84	0.02	0.00
12.34	2.00	0.00	3.83	0.02	0.00	12.36	2.00	0.00	3.82	0.02	0.00
12.38	2.00	0.00	3.81	0.02	0.00	12.40	2.00	0.00	3.80	0.02	0.00
12.42	2.00	0.00	3.79	0.02	0.00	12.44	2.00	0.00	3.78	0.02	0.00
12.46	2.00	0.00	3.77	0.02	0.00	12.48	2.00	0.00	3.76	0.02	0.00
12.50	2.00	0.00	3.75	0.02	0.00	12.52	2.00	0.00	3.74	0.02	0.00
12.54	2.00	0.00	3.73	0.02	0.00	12.56	2.00	0.00	3.72	0.02	0.00
12.58	2.00	0.00	3.71	0.02	0.00	12.60	2.00	0.00	3.70	0.02	0.00
12.62	2.00	0.00	3.69	0.02	0.00	12.64	2.00	0.00	3.68	0.02	0.00
12.66	2.00	0.00	3.67	0.02	0.00	12.68	2.00	0.00	3.66	0.02	0.00
12.70	2.00	0.00	3.65	0.02	0.00	12.72	2.00	0.00	3.64	0.02	0.00
12.74	2.00	0.00	3.63	0.02	0.00	12.76	2.00	0.00	3.62	0.02	0.00
12.78	2.00	0.00	3.61	0.02	0.00	12.80	2.00	0.00	3.60	0.02	0.00
12.82	2.00	0.00	3.59	0.02	0.00	12.84	2.00	0.00	3.58	0.02	0.00
12.86	2.00	0.00	3.57	0.02	0.00	12.88	2.00	0.00	3.56	0.02	0.00
12.90	2.00	0.00	3.55	0.02	0.00	12.92	2.00	0.00	3.54	0.02	0.00
12.94	2.00	0.00	3.53	0.02	0.00	12.96	2.00	0.00	3.52	0.02	0.00
12.99	2.00	0.00	3.51	0.03	0.00	13.01	2.00	0.00	3.50	0.02	0.00
13.02	2.00	0.00	3.49	0.01	0.00	13.04	2.00	0.00	3.48	0.02	0.00
13.06	2.00	0.00	3.47	0.02	0.00	13.08	2.00	0.00	3.46	0.02	0.00
13.10	2.00	0.00	3.45	0.02	0.00	13.12	2.00	0.00	3.44	0.02	0.00
13.14	2.00	0.00	3.43	0.02	0.00	13.16	2.00	0.00	3.42	0.02	0.00
13.18	2.00	0.00	3.41	0.02	0.00	13.20	2.00	0.00	3.40	0.02	0.00
13.22	2.00	0.00	3.39	0.02	0.00	13.24	2.00	0.00	3.38	0.02	0.00
13.26	2.00	0.00	3.37	0.02	0.00	13.28	2.00	0.00	3.36	0.02	0.00
13.30	2.00	0.00	3.35	0.02	0.00	13.32	2.00	0.00	3.34	0.02	0.00
13.34	2.00	0.00	3.33	0.02	0.00	13.36	2.00	0.00	3.32	0.02	0.00
13.39	2.00	0.00	3.31	0.03	0.00	13.40	2.00	0.00	3.30	0.01	0.00
13.42	2.00	0.00	3.29	0.02	0.00	13.44	2.00	0.00	3.28	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
13.46	2.00	0.00	3.27	0.02	0.00	13.48	2.00	0.00	3.26	0.02	0.00
13.51	2.00	0.00	3.25	0.03	0.00	13.52	2.00	0.00	3.24	0.01	0.00
13.54	2.00	0.00	3.23	0.02	0.00	13.56	2.00	0.00	3.22	0.02	0.00
13.58	2.00	0.00	3.21	0.02	0.00	13.60	2.00	0.00	3.20	0.02	0.00
13.62	2.00	0.00	3.19	0.02	0.00	13.64	2.00	0.00	3.18	0.02	0.00
13.66	2.00	0.00	3.17	0.02	0.00	13.68	2.00	0.00	3.16	0.02	0.00
13.70	2.00	0.00	3.15	0.02	0.00	13.72	2.00	0.00	3.14	0.02	0.00
13.74	2.00	0.00	3.13	0.02	0.00	13.76	2.00	0.00	3.12	0.02	0.00
13.78	2.00	0.00	3.11	0.02	0.00	13.80	2.00	0.00	3.10	0.02	0.00
13.83	2.00	0.00	3.09	0.03	0.00	13.84	2.00	0.00	3.08	0.01	0.00
13.86	2.00	0.00	3.07	0.02	0.00	13.88	2.00	0.00	3.06	0.02	0.00
13.90	2.00	0.00	3.05	0.02	0.00	13.92	2.00	0.00	3.04	0.02	0.00
13.94	2.00	0.00	3.03	0.02	0.00	13.96	2.00	0.00	3.02	0.02	0.00
13.98	2.00	0.00	3.01	0.02	0.00	14.00	2.00	0.00	3.00	0.02	0.00
14.02	2.00	0.00	2.99	0.02	0.00	14.04	2.00	0.00	2.98	0.02	0.00
14.06	2.00	0.00	2.97	0.02	0.00	14.08	2.00	0.00	2.96	0.02	0.00
14.10	2.00	0.00	2.95	0.02	0.00	14.12	2.00	0.00	2.94	0.02	0.00
14.14	2.00	0.00	2.93	0.02	0.00	14.16	2.00	0.00	2.92	0.02	0.00
14.18	2.00	0.00	2.91	0.02	0.00	14.20	2.00	0.00	2.90	0.02	0.00
14.22	2.00	0.00	2.89	0.02	0.00	14.24	2.00	0.00	2.88	0.02	0.00
14.26	2.00	0.00	2.87	0.02	0.00	14.28	2.00	0.00	2.86	0.02	0.00
14.30	2.00	0.00	2.85	0.02	0.00	14.32	2.00	0.00	2.84	0.02	0.00
14.34	2.00	0.00	2.83	0.02	0.00	14.36	2.00	0.00	2.82	0.02	0.00
14.38	2.00	0.00	2.81	0.02	0.00	14.40	2.00	0.00	2.80	0.02	0.00
14.42	2.00	0.00	2.79	0.02	0.00	14.44	2.00	0.00	2.78	0.02	0.00
14.46	2.00	0.00	2.77	0.02	0.00	14.48	2.00	0.00	2.76	0.02	0.00
14.50	2.00	0.00	2.75	0.02	0.00	14.52	2.00	0.00	2.74	0.02	0.00
14.54	2.00	0.00	2.73	0.02	0.00	14.56	2.00	0.00	2.72	0.02	0.00
14.58	2.00	0.00	2.71	0.02	0.00	14.60	2.00	0.00	2.70	0.02	0.00
14.62	2.00	0.00	2.69	0.02	0.00	14.64	2.00	0.00	2.68	0.02	0.00
14.66	2.00	0.00	2.67	0.02	0.00	14.68	2.00	0.00	2.66	0.02	0.00
14.70	2.00	0.00	2.65	0.02	0.00	14.72	2.00	0.00	2.64	0.02	0.00
14.74	2.00	0.00	2.63	0.02	0.00	14.76	2.00	0.00	2.62	0.02	0.00
14.78	2.00	0.00	2.61	0.02	0.00	14.81	2.00	0.00	2.60	0.03	0.00
14.82	2.00	0.00	2.59	0.01	0.00	14.84	2.00	0.00	2.58	0.02	0.00
14.86	2.00	0.00	2.57	0.02	0.00	14.88	2.00	0.00	2.56	0.02	0.00
14.90	2.00	0.00	2.55	0.02	0.00	14.92	2.00	0.00	2.54	0.02	0.00
14.94	2.00	0.00	2.53	0.02	0.00	14.96	2.00	0.00	2.52	0.02	0.00
14.98	2.00	0.00	2.51	0.02	0.00	15.00	2.00	0.00	2.50	0.02	0.00
15.02	2.00	0.00	2.49	0.02	0.00	15.04	2.00	0.00	2.48	0.02	0.00
15.06	2.00	0.00	2.47	0.02	0.00	15.08	2.00	0.00	2.46	0.02	0.00
15.10	2.00	0.00	2.45	0.02	0.00	15.12	2.00	0.00	2.44	0.02	0.00
15.14	2.00	0.00	2.43	0.02	0.00	15.16	2.00	0.00	2.42	0.02	0.00
15.18	2.00	0.00	2.41	0.02	0.00	15.20	2.00	0.00	2.40	0.02	0.00
15.22	2.00	0.00	2.39	0.02	0.00	15.24	2.00	0.00	2.38	0.02	0.00
15.27	2.00	0.00	2.37	0.03	0.00	15.28	2.00	0.00	2.36	0.01	0.00
15.30	2.00	0.00	2.35	0.02	0.00	15.32	2.00	0.00	2.34	0.02	0.00
15.34	2.00	0.00	2.33	0.02	0.00	15.36	2.00	0.00	2.32	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
15.38	2.00	0.00	2.31	0.02	0.00	15.40	2.00	0.00	2.30	0.02	0.00
15.42	2.00	0.00	2.29	0.02	0.00	15.44	2.00	0.00	2.28	0.02	0.00
15.46	2.00	0.00	2.27	0.02	0.00	15.48	2.00	0.00	2.26	0.02	0.00
15.50	2.00	0.00	2.25	0.02	0.00	15.52	2.00	0.00	2.24	0.02	0.00
15.54	2.00	0.00	2.23	0.02	0.00	15.56	2.00	0.00	2.22	0.02	0.00
15.58	2.00	0.00	2.21	0.02	0.00	15.60	2.00	0.00	2.20	0.02	0.00
15.62	2.00	0.00	2.19	0.02	0.00	15.64	2.00	0.00	2.18	0.02	0.00
15.66	2.00	0.00	2.17	0.02	0.00	15.68	2.00	0.00	2.16	0.02	0.00
15.70	2.00	0.00	2.15	0.02	0.00	15.72	2.00	0.00	2.14	0.02	0.00
15.74	2.00	0.00	2.13	0.02	0.00	15.76	2.00	0.00	2.12	0.02	0.00
15.78	2.00	0.00	2.11	0.02	0.00	15.80	2.00	0.00	2.10	0.02	0.00
15.82	2.00	0.00	2.09	0.02	0.00	15.84	2.00	0.00	2.08	0.02	0.00
15.86	2.00	0.00	2.07	0.02	0.00	15.88	2.00	0.00	2.06	0.02	0.00
15.90	2.00	0.00	2.05	0.02	0.00	15.92	2.00	0.00	2.04	0.02	0.00
15.94	2.00	0.00	2.03	0.02	0.00	15.96	2.00	0.00	2.02	0.02	0.00
15.98	2.00	0.00	2.01	0.02	0.00	16.00	2.00	0.00	2.00	0.02	0.00
16.02	2.00	0.00	1.99	0.02	0.00	16.04	2.00	0.00	1.98	0.02	0.00
16.07	2.00	0.00	1.97	0.03	0.00	16.08	2.00	0.00	1.96	0.01	0.00
16.10	2.00	0.00	1.95	0.02	0.00	16.13	2.00	0.00	1.94	0.03	0.00
16.14	2.00	0.00	1.93	0.01	0.00	16.16	2.00	0.00	1.92	0.02	0.00
16.18	2.00	0.00	1.91	0.02	0.00	16.20	2.00	0.00	1.90	0.02	0.00
16.22	2.00	0.00	1.89	0.02	0.00	16.24	2.00	0.00	1.88	0.02	0.00
16.26	2.00	0.00	1.87	0.02	0.00	16.28	2.00	0.00	1.86	0.02	0.00
16.30	2.00	0.00	1.85	0.02	0.00	16.32	2.00	0.00	1.84	0.02	0.00
16.34	2.00	0.00	1.83	0.02	0.00	16.36	2.00	0.00	1.82	0.02	0.00
16.38	2.00	0.00	1.81	0.02	0.00	16.40	2.00	0.00	1.80	0.02	0.00
16.43	2.00	0.00	1.79	0.03	0.00	16.44	2.00	0.00	1.78	0.01	0.00
16.46	2.00	0.00	1.77	0.02	0.00	16.48	2.00	0.00	1.76	0.02	0.00
16.50	2.00	0.00	1.75	0.02	0.00	16.52	2.00	0.00	1.74	0.02	0.00
16.54	2.00	0.00	1.73	0.02	0.00	16.57	2.00	0.00	1.72	0.03	0.00
16.58	2.00	0.00	1.71	0.01	0.00	16.60	2.00	0.00	1.70	0.02	0.00
16.63	2.00	0.00	1.69	0.03	0.00	16.64	2.00	0.00	1.68	0.01	0.00
16.66	2.00	0.00	1.67	0.02	0.00	16.68	2.00	0.00	1.66	0.02	0.00
16.70	2.00	0.00	1.65	0.02	0.00	16.72	2.00	0.00	1.64	0.02	0.00
16.74	2.00	0.00	1.63	0.02	0.00	16.76	2.00	0.00	1.62	0.02	0.00
16.79	2.00	0.00	1.61	0.03	0.00	16.80	2.00	0.00	1.60	0.01	0.00
16.83	2.00	0.00	1.59	0.03	0.00	16.84	2.00	0.00	1.58	0.01	0.00
16.86	2.00	0.00	1.57	0.02	0.00	16.88	2.00	0.00	1.56	0.02	0.00
16.90	2.00	0.00	1.55	0.02	0.00	16.92	2.00	0.00	1.54	0.02	0.00
16.94	2.00	0.00	1.53	0.02	0.00	16.96	2.00	0.00	1.52	0.02	0.00
16.98	2.00	0.00	1.51	0.02	0.00	17.00	2.00	0.00	1.50	0.02	0.00
17.03	2.00	0.00	1.49	0.03	0.00	17.04	2.00	0.00	1.48	0.01	0.00
17.06	2.00	0.00	1.47	0.02	0.00	17.08	2.00	0.00	1.46	0.02	0.00
17.10	2.00	0.00	1.45	0.02	0.00	17.12	2.00	0.00	1.44	0.02	0.00
17.14	2.00	0.00	1.43	0.02	0.00	17.16	2.00	0.00	1.42	0.02	0.00
17.19	2.00	0.00	1.41	0.03	0.00	17.20	2.00	0.00	1.40	0.01	0.00
17.23	2.00	0.00	1.39	0.03	0.00	17.24	2.00	0.00	1.38	0.01	0.00
17.26	2.00	0.00	1.37	0.02	0.00	17.28	2.00	0.00	1.36	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
17.31	2.00	0.00	1.35	0.03	0.00	17.32	2.00	0.00	1.34	0.01	0.00
17.34	2.00	0.00	1.33	0.02	0.00	17.36	2.00	0.00	1.32	0.02	0.00
17.38	2.00	0.00	1.31	0.02	0.00	17.40	2.00	0.00	1.30	0.02	0.00
17.42	2.00	0.00	1.29	0.02	0.00	17.44	2.00	0.00	1.28	0.02	0.00
17.46	2.00	0.00	1.27	0.02	0.00	17.48	2.00	0.00	1.26	0.02	0.00
17.50	2.00	0.00	1.25	0.02	0.00	17.52	2.00	0.00	1.24	0.02	0.00
17.54	2.00	0.00	1.23	0.02	0.00	17.56	2.00	0.00	1.22	0.02	0.00
17.58	2.00	0.00	1.21	0.02	0.00	17.60	2.00	0.00	1.20	0.02	0.00
17.62	2.00	0.00	1.19	0.02	0.00	17.64	2.00	0.00	1.18	0.02	0.00
17.66	2.00	0.00	1.17	0.02	0.00	17.68	2.00	0.00	1.16	0.02	0.00
17.70	2.00	0.00	1.15	0.02	0.00	17.72	2.00	0.00	1.14	0.02	0.00
17.74	2.00	0.00	1.13	0.02	0.00	17.76	2.00	0.00	1.12	0.02	0.00
17.78	2.00	0.00	1.11	0.02	0.00	17.80	2.00	0.00	1.10	0.02	0.00
17.82	2.00	0.00	1.09	0.02	0.00	17.84	2.00	0.00	1.08	0.02	0.00
17.86	2.00	0.00	1.07	0.02	0.00	17.88	2.00	0.00	1.06	0.02	0.00
17.90	2.00	0.00	1.05	0.02	0.00	17.92	2.00	0.00	1.04	0.02	0.00
17.94	2.00	0.00	1.03	0.02	0.00	17.96	2.00	0.00	1.02	0.02	0.00
17.98	2.00	0.00	1.01	0.02	0.00	18.00	2.00	0.00	1.00	0.02	0.00
18.02	2.00	0.00	0.99	0.02	0.00	18.04	2.00	0.00	0.98	0.02	0.00
18.06	2.00	0.00	0.97	0.02	0.00	18.08	2.00	0.00	0.96	0.02	0.00
18.10	2.00	0.00	0.95	0.02	0.00	18.12	2.00	0.00	0.94	0.02	0.00
18.14	2.00	0.00	0.93	0.02	0.00						

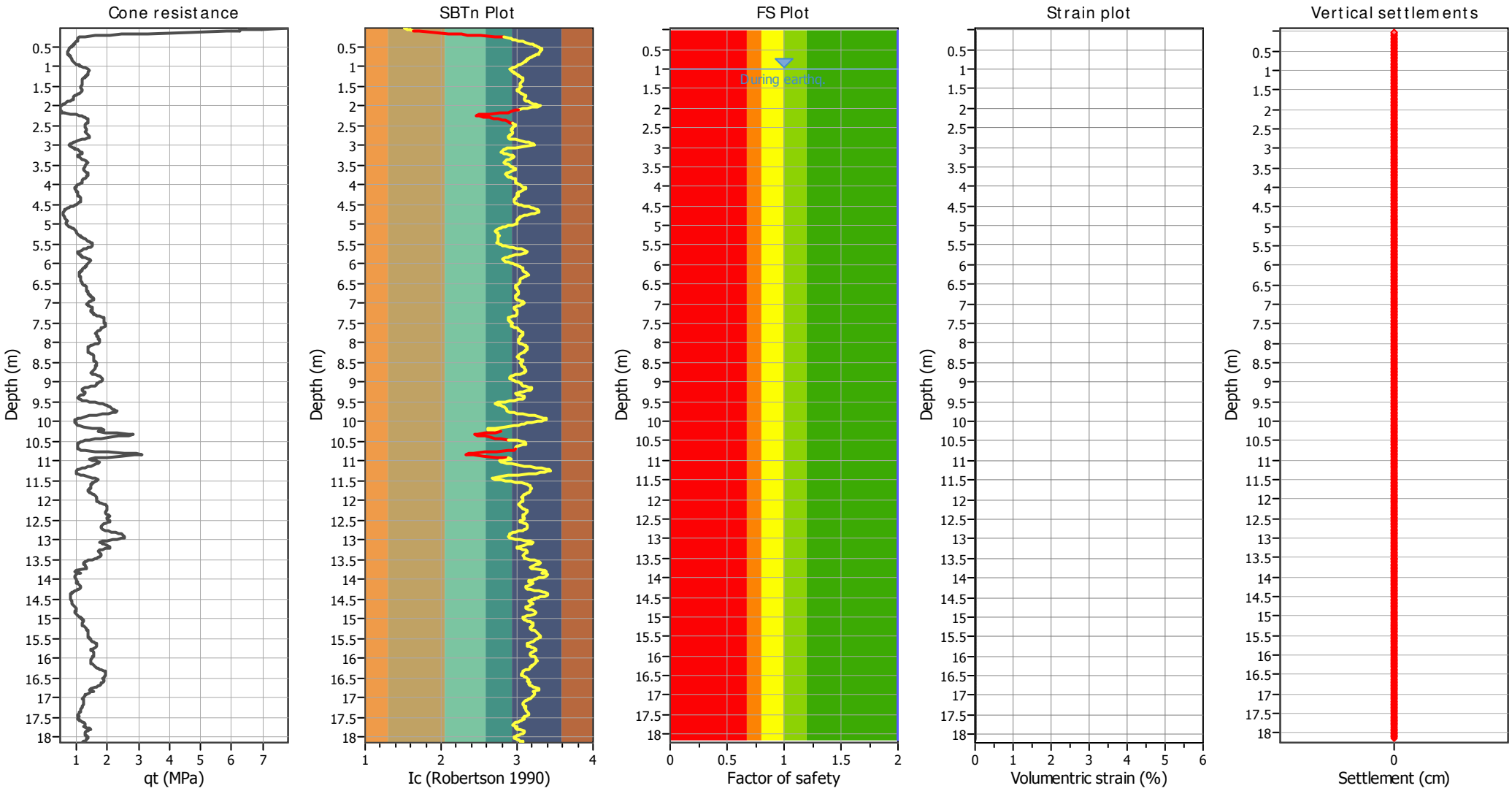
Overall liquefaction potential: 0.00

LPI = 0.00 - Liquefaction risk very low
LPI between 0.00 and 5.00 - Liquefaction risk low
LPI between 5.00 and 15.00 - Liquefaction risk high
LPI > 15.00 - Liquefaction risk very high

Abbreviations

FS: Calculated factor of safety for test point
F_L: 1 - FS
w_z: Function value of the extend of soil liquefaction according to depth
d_z: Layer thickness (m)
LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

q_t:	Total cone resistance (cone resistance q_c corrected for pore water effects)
I_c:	Soil Behaviour Type Index
FS:	Calculated Factor of Safety against liquefaction
Volumentric strain:	Post-liquefaction volumentric strain

:: Post-earthquake settlement due to soil liquefaction ::

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
1.01	19.07	2.00	0.00	1.00	0.00	1.02	19.85	2.00	0.00	1.00	0.00
1.04	21.70	2.00	0.00	1.00	0.00	1.06	23.00	2.00	0.00	1.00	0.00
1.08	23.58	2.00	0.00	1.00	0.00	1.10	23.50	2.00	0.00	1.00	0.00
1.13	23.14	2.00	0.00	1.00	0.00	1.14	23.09	2.00	0.00	1.00	0.00
1.16	23.36	2.00	0.00	1.00	0.00	1.19	23.27	2.00	0.00	1.00	0.00
1.20	22.75	2.00	0.00	1.00	0.00	1.22	22.82	2.00	0.00	1.00	0.00
1.24	22.17	2.00	0.00	1.00	0.00	1.26	21.65	2.00	0.00	1.00	0.00
1.28	20.92	2.00	0.00	1.00	0.00	1.30	20.51	2.00	0.00	1.00	0.00
1.32	19.98	2.00	0.00	1.00	0.00	1.34	19.69	2.00	0.00	1.00	0.00
1.36	19.71	2.00	0.00	1.00	0.00	1.38	19.88	2.00	0.00	1.00	0.00
1.40	19.98	2.00	0.00	1.00	0.00	1.42	20.12	2.00	0.00	1.00	0.00
1.44	19.94	2.00	0.00	1.00	0.00	1.46	19.81	2.00	0.00	1.00	0.00
1.48	19.20	2.00	0.00	1.00	0.00	1.50	18.87	2.00	0.00	1.00	0.00
1.52	18.66	2.00	0.00	1.00	0.00	1.54	18.92	2.00	0.00	1.00	0.00
1.56	18.82	2.00	0.00	1.00	0.00	1.58	19.47	2.00	0.00	1.00	0.00
1.60	19.61	2.00	0.00	1.00	0.00	1.62	19.74	2.00	0.00	1.00	0.00
1.64	19.37	2.00	0.00	1.00	0.00	1.66	18.82	2.00	0.00	1.00	0.00
1.68	17.94	2.00	0.00	1.00	0.00	1.70	17.18	2.00	0.00	1.00	0.00
1.72	16.27	2.00	0.00	1.00	0.00	1.74	15.63	2.00	0.00	1.00	0.00
1.76	14.99	2.00	0.00	1.00	0.00	1.78	15.01	2.00	0.00	1.00	0.00
1.80	14.96	2.00	0.00	1.00	0.00	1.82	15.07	2.00	0.00	1.00	0.00
1.84	14.51	2.00	0.00	1.00	0.00	1.86	14.11	2.00	0.00	1.00	0.00
1.88	12.81	2.00	0.00	1.00	0.00	1.90	11.91	2.00	0.00	1.00	0.00
1.92	11.41	2.00	0.00	1.00	0.00	1.94	10.39	2.00	0.00	1.00	0.00
1.96	9.30	2.00	0.00	1.00	0.00	1.98	8.05	2.00	0.00	1.00	0.00
2.01	7.54	2.00	0.00	1.00	0.00	2.02	7.61	2.00	0.00	1.00	0.00
2.04	7.73	2.00	0.00	1.00	0.00	2.06	7.84	2.00	0.00	1.00	0.00
2.08	7.61	2.00	0.00	1.00	0.00	2.10	7.56	2.00	0.00	1.00	0.00
2.12	7.52	2.00	0.00	1.00	0.00	2.14	8.19	2.00	0.00	1.00	0.00
2.16	8.50	2.00	0.00	1.00	0.00	2.18	9.01	2.00	0.00	1.00	0.00
2.21	12.99	2.00	0.00	1.00	0.00	2.22	70.22	2.00	0.00	1.00	0.00
2.24	72.02	2.00	0.00	1.00	0.00	2.26	74.29	2.00	0.00	1.00	0.00
2.28	76.91	2.00	0.00	1.00	0.00	2.30	21.72	2.00	0.00	1.00	0.00
2.32	22.46	2.00	0.00	1.00	0.00	2.34	22.62	2.00	0.00	1.00	0.00
2.36	23.04	2.00	0.00	1.00	0.00	2.38	23.20	2.00	0.00	1.00	0.00
2.40	23.03	2.00	0.00	1.00	0.00	2.42	23.14	2.00	0.00	1.00	0.00
2.44	21.99	2.00	0.00	1.00	0.00	2.46	21.30	2.00	0.00	1.00	0.00
2.48	20.74	2.00	0.00	1.00	0.00	2.50	20.72	2.00	0.00	1.00	0.00
2.52	21.01	2.00	0.00	1.00	0.00	2.54	21.28	2.00	0.00	1.00	0.00
2.56	21.53	2.00	0.00	1.00	0.00	2.58	21.71	2.00	0.00	1.00	0.00
2.60	21.61	2.00	0.00	1.00	0.00	2.62	22.10	2.00	0.00	1.00	0.00
2.64	21.81	2.00	0.00	1.00	0.00	2.66	21.36	2.00	0.00	1.00	0.00
2.68	21.08	2.00	0.00	1.00	0.00	2.70	21.66	2.00	0.00	1.00	0.00
2.72	21.97	2.00	0.00	1.00	0.00	2.74	22.74	2.00	0.00	1.00	0.00
2.76	22.53	2.00	0.00	1.00	0.00	2.78	22.53	2.00	0.00	1.00	0.00
2.80	22.64	2.00	0.00	1.00	0.00	2.82	22.65	2.00	0.00	1.00	0.00
2.84	21.24	2.00	0.00	1.00	0.00	2.86	18.77	2.00	0.00	1.00	0.00
2.88	16.90	2.00	0.00	1.00	0.00	2.92	15.67	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
2.92	14.65	2.00	0.00	1.00	0.00	2.94	14.06	2.00	0.00	1.00	0.00
2.97	13.28	2.00	0.00	1.00	0.00	2.99	11.88	2.00	0.00	1.00	0.00
3.00	11.57	2.00	0.00	1.00	0.00	3.02	12.68	2.00	0.00	1.00	0.00
3.05	14.72	2.00	0.00	1.00	0.00	3.06	14.98	2.00	0.00	1.00	0.00
3.08	14.66	2.00	0.00	1.00	0.00	3.10	14.38	2.00	0.00	1.00	0.00
3.12	16.12	2.00	0.00	1.00	0.00	3.14	17.90	2.00	0.00	1.00	0.00
3.16	17.90	2.00	0.00	1.00	0.00	3.18	18.32	2.00	0.00	1.00	0.00
3.20	18.38	2.00	0.00	1.00	0.00	3.22	17.84	2.00	0.00	1.00	0.00
3.24	16.88	2.00	0.00	1.00	0.00	3.26	16.42	2.00	0.00	1.00	0.00
3.28	16.21	2.00	0.00	1.00	0.00	3.30	16.80	2.00	0.00	1.00	0.00
3.32	17.47	2.00	0.00	1.00	0.00	3.34	17.54	2.00	0.00	1.00	0.00
3.36	18.45	2.00	0.00	1.00	0.00	3.38	19.28	2.00	0.00	1.00	0.00
3.40	19.80	2.00	0.00	1.00	0.00	3.42	20.69	2.00	0.00	1.00	0.00
3.44	20.92	2.00	0.00	1.00	0.00	3.46	20.73	2.00	0.00	1.00	0.00
3.49	19.69	2.00	0.00	1.00	0.00	3.50	19.07	2.00	0.00	1.00	0.00
3.52	19.47	2.00	0.00	1.00	0.00	3.54	19.31	2.00	0.00	1.00	0.00
3.56	18.95	2.00	0.00	1.00	0.00	3.58	18.63	2.00	0.00	1.00	0.00
3.60	18.38	2.00	0.00	1.00	0.00	3.62	18.23	2.00	0.00	1.00	0.00
3.64	18.63	2.00	0.00	1.00	0.00	3.66	19.17	2.00	0.00	1.00	0.00
3.68	19.95	2.00	0.00	1.00	0.00	3.70	20.31	2.00	0.00	1.00	0.00
3.72	20.40	2.00	0.00	1.00	0.00	3.74	20.11	2.00	0.00	1.00	0.00
3.76	19.80	2.00	0.00	1.00	0.00	3.78	19.76	2.00	0.00	1.00	0.00
3.80	19.71	2.00	0.00	1.00	0.00	3.82	19.22	2.00	0.00	1.00	0.00
3.84	18.54	2.00	0.00	1.00	0.00	3.86	17.72	2.00	0.00	1.00	0.00
3.88	17.14	2.00	0.00	1.00	0.00	3.90	17.52	2.00	0.00	1.00	0.00
3.92	17.38	2.00	0.00	1.00	0.00	3.94	17.09	2.00	0.00	1.00	0.00
3.96	16.15	2.00	0.00	1.00	0.00	3.98	15.66	2.00	0.00	1.00	0.00
4.00	15.10	2.00	0.00	1.00	0.00	4.02	14.83	2.00	0.00	1.00	0.00
4.05	13.89	2.00	0.00	1.00	0.00	4.06	13.54	2.00	0.00	1.00	0.00
4.08	13.14	2.00	0.00	1.00	0.00	4.10	13.37	2.00	0.00	1.00	0.00
4.12	13.50	2.00	0.00	1.00	0.00	4.14	14.00	2.00	0.00	1.00	0.00
4.16	14.20	2.00	0.00	1.00	0.00	4.18	14.46	2.00	0.00	1.00	0.00
4.20	14.85	2.00	0.00	1.00	0.00	4.22	14.89	2.00	0.00	1.00	0.00
4.24	14.99	2.00	0.00	1.00	0.00	4.26	14.83	2.00	0.00	1.00	0.00
4.28	14.70	2.00	0.00	1.00	0.00	4.30	15.35	2.00	0.00	1.00	0.00
4.32	15.94	2.00	0.00	1.00	0.00	4.34	16.20	2.00	0.00	1.00	0.00
4.36	16.04	2.00	0.00	1.00	0.00	4.38	15.72	2.00	0.00	1.00	0.00
4.40	15.85	2.00	0.00	1.00	0.00	4.42	15.56	2.00	0.00	1.00	0.00
4.44	15.24	2.00	0.00	1.00	0.00	4.46	14.76	2.00	0.00	1.00	0.00
4.48	14.06	2.00	0.00	1.00	0.00	4.50	13.84	2.00	0.00	1.00	0.00
4.52	13.00	2.00	0.00	1.00	0.00	4.54	12.30	2.00	0.00	1.00	0.00
4.56	11.25	2.00	0.00	1.00	0.00	4.58	10.61	2.00	0.00	1.00	0.00
4.60	9.72	2.00	0.00	1.00	0.00	4.62	9.18	2.00	0.00	1.00	0.00
4.64	8.64	2.00	0.00	1.00	0.00	4.66	7.84	2.00	0.00	1.00	0.00
4.68	7.67	2.00	0.00	1.00	0.00	4.70	7.43	2.00	0.00	1.00	0.00
4.72	7.32	2.00	0.00	1.00	0.00	4.74	7.66	2.00	0.00	1.00	0.00
4.76	7.62	2.00	0.00	1.00	0.00	4.78	8.06	2.00	0.00	1.00	0.00
4.80	8.18	2.00	0.00	1.00	0.00	4.82	8.24	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
4.84	8.30	2.00	0.00	1.00	0.00	4.86	7.84	2.00	0.00	1.00	0.00
4.88	9.29	2.00	0.00	1.00	0.00	4.90	9.09	2.00	0.00	1.00	0.00
4.92	9.27	2.00	0.00	1.00	0.00	4.94	9.32	2.00	0.00	1.00	0.00
4.96	8.96	2.00	0.00	1.00	0.00	4.98	8.89	2.00	0.00	1.00	0.00
5.00	8.81	2.00	0.00	1.00	0.00	5.02	9.22	2.00	0.00	1.00	0.00
5.04	9.46	2.00	0.00	1.00	0.00	5.06	10.25	2.00	0.00	1.00	0.00
5.08	10.90	2.00	0.00	1.00	0.00	5.10	11.33	2.00	0.00	1.00	0.00
5.12	11.79	2.00	0.00	1.00	0.00	5.14	12.50	2.00	0.00	1.00	0.00
5.16	12.95	2.00	0.00	1.00	0.00	5.19	13.61	2.00	0.00	1.00	0.00
5.20	13.26	2.00	0.00	1.00	0.00	5.22	13.23	2.00	0.00	1.00	0.00
5.24	13.40	2.00	0.00	1.00	0.00	5.26	13.85	2.00	0.00	1.00	0.00
5.28	14.20	2.00	0.00	1.00	0.00	5.30	14.42	2.00	0.00	1.00	0.00
5.32	15.07	2.00	0.00	1.00	0.00	5.34	15.60	2.00	0.00	1.00	0.00
5.36	15.83	2.00	0.00	1.00	0.00	5.38	16.79	2.00	0.00	1.00	0.00
5.40	17.31	2.00	0.00	1.00	0.00	5.42	17.40	2.00	0.00	1.00	0.00
5.44	18.07	2.00	0.00	1.00	0.00	5.46	18.80	2.00	0.00	1.00	0.00
5.48	19.10	2.00	0.00	1.00	0.00	5.50	19.64	2.00	0.00	1.00	0.00
5.52	19.54	2.00	0.00	1.00	0.00	5.54	19.35	2.00	0.00	1.00	0.00
5.56	19.10	2.00	0.00	1.00	0.00	5.58	18.90	2.00	0.00	1.00	0.00
5.60	17.51	2.00	0.00	1.00	0.00	5.62	17.00	2.00	0.00	1.00	0.00
5.64	15.95	2.00	0.00	1.00	0.00	5.66	14.84	2.00	0.00	1.00	0.00
5.68	13.94	2.00	0.00	1.00	0.00	5.70	13.38	2.00	0.00	1.00	0.00
5.72	13.15	2.00	0.00	1.00	0.00	5.74	13.21	2.00	0.00	1.00	0.00
5.76	13.74	2.00	0.00	1.00	0.00	5.78	14.57	2.00	0.00	1.00	0.00
5.80	14.55	2.00	0.00	1.00	0.00	5.82	14.70	2.00	0.00	1.00	0.00
5.84	15.09	2.00	0.00	1.00	0.00	5.86	15.71	2.00	0.00	1.00	0.00
5.89	17.57	2.00	0.00	1.00	0.00	5.90	18.06	2.00	0.00	1.00	0.00
5.92	18.27	2.00	0.00	1.00	0.00	5.94	18.06	2.00	0.00	1.00	0.00
5.96	17.56	2.00	0.00	1.00	0.00	5.98	17.21	2.00	0.00	1.00	0.00
6.01	16.59	2.00	0.00	1.00	0.00	6.02	16.98	2.00	0.00	1.00	0.00
6.04	16.22	2.00	0.00	1.00	0.00	6.06	16.20	2.00	0.00	1.00	0.00
6.08	16.05	2.00	0.00	1.00	0.00	6.10	15.61	2.00	0.00	1.00	0.00
6.12	14.82	2.00	0.00	1.00	0.00	6.14	14.82	2.00	0.00	1.00	0.00
6.16	14.53	2.00	0.00	1.00	0.00	6.18	14.27	2.00	0.00	1.00	0.00
6.21	13.77	2.00	0.00	1.00	0.00	6.22	13.58	2.00	0.00	1.00	0.00
6.25	13.20	2.00	0.00	1.00	0.00	6.26	13.08	2.00	0.00	1.00	0.00
6.28	13.03	2.00	0.00	1.00	0.00	6.30	12.89	2.00	0.00	1.00	0.00
6.32	13.26	2.00	0.00	1.00	0.00	6.34	13.66	2.00	0.00	1.00	0.00
6.36	13.57	2.00	0.00	1.00	0.00	6.38	13.55	2.00	0.00	1.00	0.00
6.40	13.78	2.00	0.00	1.00	0.00	6.42	14.02	2.00	0.00	1.00	0.00
6.44	13.83	2.00	0.00	1.00	0.00	6.46	14.07	2.00	0.00	1.00	0.00
6.48	14.04	2.00	0.00	1.00	0.00	6.50	14.19	2.00	0.00	1.00	0.00
6.52	14.40	2.00	0.00	1.00	0.00	6.54	14.83	2.00	0.00	1.00	0.00
6.56	15.46	2.00	0.00	1.00	0.00	6.58	15.75	2.00	0.00	1.00	0.00
6.60	15.87	2.00	0.00	1.00	0.00	6.62	16.07	2.00	0.00	1.00	0.00
6.64	16.04	2.00	0.00	1.00	0.00	6.66	15.91	2.00	0.00	1.00	0.00
6.68	15.72	2.00	0.00	1.00	0.00	6.70	16.11	2.00	0.00	1.00	0.00
6.72	16.34	2.00	0.00	1.00	0.00	6.74	16.40	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
6.76	16.27	2.00	0.00	1.00	0.00	6.78	16.44	2.00	0.00	1.00	0.00
6.80	16.91	2.00	0.00	1.00	0.00	6.82	17.28	2.00	0.00	1.00	0.00
6.84	17.28	2.00	0.00	1.00	0.00	6.86	17.95	2.00	0.00	1.00	0.00
6.88	18.40	2.00	0.00	1.00	0.00	6.90	18.02	2.00	0.00	1.00	0.00
6.92	17.91	2.00	0.00	1.00	0.00	6.94	17.14	2.00	0.00	1.00	0.00
6.96	16.15	2.00	0.00	1.00	0.00	6.98	15.76	2.00	0.00	1.00	0.00
7.00	15.63	2.00	0.00	1.00	0.00	7.02	15.68	2.00	0.00	1.00	0.00
7.04	15.60	2.00	0.00	1.00	0.00	7.06	16.13	2.00	0.00	1.00	0.00
7.08	16.41	2.00	0.00	1.00	0.00	7.10	17.12	2.00	0.00	1.00	0.00
7.12	17.39	2.00	0.00	1.00	0.00	7.14	17.69	2.00	0.00	1.00	0.00
7.16	17.31	2.00	0.00	1.00	0.00	7.18	16.93	2.00	0.00	1.00	0.00
7.20	16.84	2.00	0.00	1.00	0.00	7.22	17.01	2.00	0.00	1.00	0.00
7.24	17.52	2.00	0.00	1.00	0.00	7.26	17.90	2.00	0.00	1.00	0.00
7.28	17.82	2.00	0.00	1.00	0.00	7.30	18.12	2.00	0.00	1.00	0.00
7.32	18.69	2.00	0.00	1.00	0.00	7.34	19.86	2.00	0.00	1.00	0.00
7.36	20.85	2.00	0.00	1.00	0.00	7.38	21.46	2.00	0.00	1.00	0.00
7.40	21.69	2.00	0.00	1.00	0.00	7.42	21.41	2.00	0.00	1.00	0.00
7.44	21.12	2.00	0.00	1.00	0.00	7.46	21.35	2.00	0.00	1.00	0.00
7.48	21.43	2.00	0.00	1.00	0.00	7.50	21.35	2.00	0.00	1.00	0.00
7.52	21.76	2.00	0.00	1.00	0.00	7.54	21.97	2.00	0.00	1.00	0.00
7.56	22.14	2.00	0.00	1.00	0.00	7.58	21.98	2.00	0.00	1.00	0.00
7.60	21.73	2.00	0.00	1.00	0.00	7.62	20.70	2.00	0.00	1.00	0.00
7.64	20.17	2.00	0.00	1.00	0.00	7.66	20.00	2.00	0.00	1.00	0.00
7.68	19.53	2.00	0.00	1.00	0.00	7.70	19.05	2.00	0.00	1.00	0.00
7.72	18.65	2.00	0.00	1.00	0.00	7.74	18.22	2.00	0.00	1.00	0.00
7.76	18.11	2.00	0.00	1.00	0.00	7.78	18.03	2.00	0.00	1.00	0.00
7.80	18.26	2.00	0.00	1.00	0.00	7.82	18.00	2.00	0.00	1.00	0.00
7.84	18.40	2.00	0.00	1.00	0.00	7.86	18.69	2.00	0.00	1.00	0.00
7.88	18.80	2.00	0.00	1.00	0.00	7.90	19.14	2.00	0.00	1.00	0.00
7.92	18.96	2.00	0.00	1.00	0.00	7.94	19.25	2.00	0.00	1.00	0.00
7.96	19.25	2.00	0.00	1.00	0.00	7.98	19.38	2.00	0.00	1.00	0.00
8.00	19.10	2.00	0.00	1.00	0.00	8.02	18.53	2.00	0.00	1.00	0.00
8.04	17.55	2.00	0.00	1.00	0.00	8.07	16.53	2.00	0.00	1.00	0.00
8.08	16.08	2.00	0.00	1.00	0.00	8.10	15.59	2.00	0.00	1.00	0.00
8.12	15.08	2.00	0.00	1.00	0.00	8.14	14.62	2.00	0.00	1.00	0.00
8.16	14.57	2.00	0.00	1.00	0.00	8.18	14.81	2.00	0.00	1.00	0.00
8.20	14.86	2.00	0.00	1.00	0.00	8.22	15.07	2.00	0.00	1.00	0.00
8.24	14.79	2.00	0.00	1.00	0.00	8.26	15.19	2.00	0.00	1.00	0.00
8.28	15.99	2.00	0.00	1.00	0.00	8.30	16.53	2.00	0.00	1.00	0.00
8.32	16.41	2.00	0.00	1.00	0.00	8.34	16.90	2.00	0.00	1.00	0.00
8.36	16.90	2.00	0.00	1.00	0.00	8.38	17.21	2.00	0.00	1.00	0.00
8.40	16.86	2.00	0.00	1.00	0.00	8.42	16.66	2.00	0.00	1.00	0.00
8.44	16.33	2.00	0.00	1.00	0.00	8.47	16.66	2.00	0.00	1.00	0.00
8.48	17.11	2.00	0.00	1.00	0.00	8.50	17.34	2.00	0.00	1.00	0.00
8.52	17.80	2.00	0.00	1.00	0.00	8.54	17.71	2.00	0.00	1.00	0.00
8.56	17.11	2.00	0.00	1.00	0.00	8.58	17.41	2.00	0.00	1.00	0.00
8.60	17.34	2.00	0.00	1.00	0.00	8.62	17.17	2.00	0.00	1.00	0.00
8.64	17.26	2.00	0.00	1.00	0.00	8.66	17.01	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
8.68	16.53	2.00	0.00	1.00	0.00	8.70	16.26	2.00	0.00	1.00	0.00
8.72	15.99	2.00	0.00	1.00	0.00	8.74	15.62	2.00	0.00	1.00	0.00
8.76	15.65	2.00	0.00	1.00	0.00	8.78	15.32	2.00	0.00	1.00	0.00
8.80	15.93	2.00	0.00	1.00	0.00	8.82	16.73	2.00	0.00	1.00	0.00
8.84	18.17	2.00	0.00	1.00	0.00	8.86	18.23	2.00	0.00	1.00	0.00
8.88	18.88	2.00	0.00	1.00	0.00	8.90	19.06	2.00	0.00	1.00	0.00
8.92	19.36	2.00	0.00	1.00	0.00	8.94	19.44	2.00	0.00	1.00	0.00
8.96	19.17	2.00	0.00	1.00	0.00	8.98	18.78	2.00	0.00	1.00	0.00
9.00	18.56	2.00	0.00	1.00	0.00	9.02	17.50	2.00	0.00	1.00	0.00
9.04	17.36	2.00	0.00	1.00	0.00	9.06	17.22	2.00	0.00	1.00	0.00
9.09	16.72	2.00	0.00	1.00	0.00	9.10	15.33	2.00	0.00	1.00	0.00
9.13	13.75	2.00	0.00	1.00	0.00	9.14	12.85	2.00	0.00	1.00	0.00
9.16	12.07	2.00	0.00	1.00	0.00	9.18	11.91	2.00	0.00	1.00	0.00
9.20	11.91	2.00	0.00	1.00	0.00	9.22	12.17	2.00	0.00	1.00	0.00
9.24	12.59	2.00	0.00	1.00	0.00	9.26	12.87	2.00	0.00	1.00	0.00
9.28	13.08	2.00	0.00	1.00	0.00	9.30	12.80	2.00	0.00	1.00	0.00
9.32	12.62	2.00	0.00	1.00	0.00	9.34	11.49	2.00	0.00	1.00	0.00
9.36	11.07	2.00	0.00	1.00	0.00	9.38	10.72	2.00	0.00	1.00	0.00
9.40	10.57	2.00	0.00	1.00	0.00	9.42	10.85	2.00	0.00	1.00	0.00
9.44	11.45	2.00	0.00	1.00	0.00	9.47	12.19	2.00	0.00	1.00	0.00
9.48	12.72	2.00	0.00	1.00	0.00	9.50	14.56	2.00	0.00	1.00	0.00
9.52	16.27	2.00	0.00	1.00	0.00	9.54	18.14	2.00	0.00	1.00	0.00
9.56	18.95	2.00	0.00	1.00	0.00	9.58	19.29	2.00	0.00	1.00	0.00
9.60	19.93	2.00	0.00	1.00	0.00	9.62	20.22	2.00	0.00	1.00	0.00
9.64	20.93	2.00	0.00	1.00	0.00	9.66	21.36	2.00	0.00	1.00	0.00
9.68	21.87	2.00	0.00	1.00	0.00	9.70	22.33	2.00	0.00	1.00	0.00
9.72	22.93	2.00	0.00	1.00	0.00	9.74	23.41	2.00	0.00	1.00	0.00
9.76	23.02	2.00	0.00	1.00	0.00	9.78	21.83	2.00	0.00	1.00	0.00
9.80	20.28	2.00	0.00	1.00	0.00	9.82	18.42	2.00	0.00	1.00	0.00
9.84	16.10	2.00	0.00	1.00	0.00	9.86	14.13	2.00	0.00	1.00	0.00
9.88	12.29	2.00	0.00	1.00	0.00	9.91	11.12	2.00	0.00	1.00	0.00
9.92	10.10	2.00	0.00	1.00	0.00	9.94	9.62	2.00	0.00	1.00	0.00
9.96	9.39	2.00	0.00	1.00	0.00	9.98	9.23	2.00	0.00	1.00	0.00
10.00	9.27	2.00	0.00	1.00	0.00	10.02	9.35	2.00	0.00	1.00	0.00
10.04	9.56	2.00	0.00	1.00	0.00	10.06	9.64	2.00	0.00	1.00	0.00
10.08	9.50	2.00	0.00	1.00	0.00	10.10	9.66	2.00	0.00	1.00	0.00
10.12	10.58	2.00	0.00	1.00	0.00	10.14	11.37	2.00	0.00	1.00	0.00
10.16	14.54	2.00	0.00	1.00	0.00	10.18	18.17	2.00	0.00	1.00	0.00
10.20	19.57	2.00	0.00	1.00	0.00	10.22	18.38	2.00	0.00	1.00	0.00
10.24	16.59	2.00	0.00	1.00	0.00	10.26	15.76	2.00	0.00	1.00	0.00
10.28	18.12	2.00	0.00	1.00	0.00	10.30	79.89	2.00	0.00	1.00	0.00
10.32	84.12	2.00	0.00	1.00	0.00	10.34	85.71	2.00	0.00	1.00	0.00
10.36	83.15	2.00	0.00	1.00	0.00	10.38	80.69	2.00	0.00	1.00	0.00
10.40	19.02	2.00	0.00	1.00	0.00	10.42	17.79	2.00	0.00	1.00	0.00
10.44	15.62	2.00	0.00	1.00	0.00	10.46	13.68	2.00	0.00	1.00	0.00
10.48	12.28	2.00	0.00	1.00	0.00	10.50	11.11	2.00	0.00	1.00	0.00
10.52	10.69	2.00	0.00	1.00	0.00	10.54	10.20	2.00	0.00	1.00	0.00
10.56	9.71	2.00	0.00	1.00	0.00	10.58	9.55	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
10.60	9.68	2.00	0.00	1.00	0.00	10.62	9.90	2.00	0.00	1.00	0.00
10.64	10.01	2.00	0.00	1.00	0.00	10.66	9.89	2.00	0.00	1.00	0.00
10.68	10.04	2.00	0.00	1.00	0.00	10.70	10.10	2.00	0.00	1.00	0.00
10.72	10.46	2.00	0.00	1.00	0.00	10.74	11.31	2.00	0.00	1.00	0.00
10.76	14.38	2.00	0.00	1.00	0.00	10.78	76.84	2.00	0.00	1.00	0.00
10.80	77.42	2.00	0.00	1.00	0.00	10.82	85.04	2.00	0.00	1.00	0.00
10.84	85.37	2.00	0.00	1.00	0.00	10.86	84.44	2.00	0.00	1.00	0.00
10.88	79.83	2.00	0.00	1.00	0.00	10.90	18.65	2.00	0.00	1.00	0.00
10.92	15.00	2.00	0.00	1.00	0.00	10.94	12.45	2.00	0.00	1.00	0.00
10.96	13.29	2.00	0.00	1.00	0.00	10.98	14.51	2.00	0.00	1.00	0.00
11.00	15.39	2.00	0.00	1.00	0.00	11.02	16.29	2.00	0.00	1.00	0.00
11.04	16.20	2.00	0.00	1.00	0.00	11.06	16.14	2.00	0.00	1.00	0.00
11.08	15.36	2.00	0.00	1.00	0.00	11.10	14.61	2.00	0.00	1.00	0.00
11.13	13.59	2.00	0.00	1.00	0.00	11.14	12.81	2.00	0.00	1.00	0.00
11.16	11.73	2.00	0.00	1.00	0.00	11.18	10.92	2.00	0.00	1.00	0.00
11.20	10.06	2.00	0.00	1.00	0.00	11.22	9.39	2.00	0.00	1.00	0.00
11.24	9.05	2.00	0.00	1.00	0.00	11.26	9.01	2.00	0.00	1.00	0.00
11.28	9.24	2.00	0.00	1.00	0.00	11.30	9.29	2.00	0.00	1.00	0.00
11.32	8.89	2.00	0.00	1.00	0.00	11.34	9.19	2.00	0.00	1.00	0.00
11.36	10.06	2.00	0.00	1.00	0.00	11.38	11.30	2.00	0.00	1.00	0.00
11.40	12.59	2.00	0.00	1.00	0.00	11.42	14.03	2.00	0.00	1.00	0.00
11.44	15.30	2.00	0.00	1.00	0.00	11.46	15.69	2.00	0.00	1.00	0.00
11.48	15.39	2.00	0.00	1.00	0.00	11.50	14.96	2.00	0.00	1.00	0.00
11.52	14.81	2.00	0.00	1.00	0.00	11.54	14.42	2.00	0.00	1.00	0.00
11.56	13.88	2.00	0.00	1.00	0.00	11.58	13.60	2.00	0.00	1.00	0.00
11.60	13.47	2.00	0.00	1.00	0.00	11.62	13.55	2.00	0.00	1.00	0.00
11.64	13.67	2.00	0.00	1.00	0.00	11.66	13.37	2.00	0.00	1.00	0.00
11.68	13.06	2.00	0.00	1.00	0.00	11.70	12.94	2.00	0.00	1.00	0.00
11.72	12.72	2.00	0.00	1.00	0.00	11.74	12.66	2.00	0.00	1.00	0.00
11.76	12.43	2.00	0.00	1.00	0.00	11.78	12.57	2.00	0.00	1.00	0.00
11.80	12.88	2.00	0.00	1.00	0.00	11.82	13.43	2.00	0.00	1.00	0.00
11.84	13.64	2.00	0.00	1.00	0.00	11.86	14.04	2.00	0.00	1.00	0.00
11.88	14.45	2.00	0.00	1.00	0.00	11.90	14.88	2.00	0.00	1.00	0.00
11.92	14.98	2.00	0.00	1.00	0.00	11.94	14.89	2.00	0.00	1.00	0.00
11.96	14.81	2.00	0.00	1.00	0.00	11.98	14.78	2.00	0.00	1.00	0.00
12.00	14.89	2.00	0.00	1.00	0.00	12.02	15.12	2.00	0.00	1.00	0.00
12.04	15.21	2.00	0.00	1.00	0.00	12.06	15.70	2.00	0.00	1.00	0.00
12.08	16.25	2.00	0.00	1.00	0.00	12.10	16.87	2.00	0.00	1.00	0.00
12.12	17.37	2.00	0.00	1.00	0.00	12.14	17.61	2.00	0.00	1.00	0.00
12.16	18.00	2.00	0.00	1.00	0.00	12.18	17.89	2.00	0.00	1.00	0.00
12.21	17.80	2.00	0.00	1.00	0.00	12.22	17.91	2.00	0.00	1.00	0.00
12.24	17.76	2.00	0.00	1.00	0.00	12.26	17.48	2.00	0.00	1.00	0.00
12.28	17.48	2.00	0.00	1.00	0.00	12.30	17.34	2.00	0.00	1.00	0.00
12.32	17.25	2.00	0.00	1.00	0.00	12.34	17.40	2.00	0.00	1.00	0.00
12.36	17.75	2.00	0.00	1.00	0.00	12.38	18.18	2.00	0.00	1.00	0.00
12.40	18.47	2.00	0.00	1.00	0.00	12.42	18.59	2.00	0.00	1.00	0.00
12.44	17.69	2.00	0.00	1.00	0.00	12.46	17.19	2.00	0.00	1.00	0.00
12.48	17.51	2.00	0.00	1.00	0.00	12.50	18.18	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
12.52	18.53	2.00	0.00	1.00	0.00	12.54	18.44	2.00	0.00	1.00	0.00
12.56	17.94	2.00	0.00	1.00	0.00	12.58	17.11	2.00	0.00	1.00	0.00
12.60	16.49	2.00	0.00	1.00	0.00	12.62	16.09	2.00	0.00	1.00	0.00
12.64	16.20	2.00	0.00	1.00	0.00	12.66	15.80	2.00	0.00	1.00	0.00
12.68	15.91	2.00	0.00	1.00	0.00	12.70	15.85	2.00	0.00	1.00	0.00
12.72	16.02	2.00	0.00	1.00	0.00	12.74	16.20	2.00	0.00	1.00	0.00
12.76	16.73	2.00	0.00	1.00	0.00	12.78	17.60	2.00	0.00	1.00	0.00
12.80	18.86	2.00	0.00	1.00	0.00	12.82	19.57	2.00	0.00	1.00	0.00
12.84	20.88	2.00	0.00	1.00	0.00	12.86	21.63	2.00	0.00	1.00	0.00
12.88	22.04	2.00	0.00	1.00	0.00	12.90	22.12	2.00	0.00	1.00	0.00
12.92	22.66	2.00	0.00	1.00	0.00	12.94	22.76	2.00	0.00	1.00	0.00
12.96	21.77	2.00	0.00	1.00	0.00	12.99	20.19	2.00	0.00	1.00	0.00
13.01	18.92	2.00	0.00	1.00	0.00	13.02	17.49	2.00	0.00	1.00	0.00
13.04	15.63	2.00	0.00	1.00	0.00	13.06	14.92	2.00	0.00	1.00	0.00
13.08	15.21	2.00	0.00	1.00	0.00	13.10	15.84	2.00	0.00	1.00	0.00
13.12	16.10	2.00	0.00	1.00	0.00	13.14	17.15	2.00	0.00	1.00	0.00
13.16	17.78	2.00	0.00	1.00	0.00	13.18	18.60	2.00	0.00	1.00	0.00
13.20	17.70	2.00	0.00	1.00	0.00	13.22	17.05	2.00	0.00	1.00	0.00
13.24	15.58	2.00	0.00	1.00	0.00	13.26	14.98	2.00	0.00	1.00	0.00
13.28	14.53	2.00	0.00	1.00	0.00	13.30	14.60	2.00	0.00	1.00	0.00
13.32	14.84	2.00	0.00	1.00	0.00	13.34	14.99	2.00	0.00	1.00	0.00
13.36	15.37	2.00	0.00	1.00	0.00	13.39	15.41	2.00	0.00	1.00	0.00
13.40	15.36	2.00	0.00	1.00	0.00	13.42	14.77	2.00	0.00	1.00	0.00
13.44	14.32	2.00	0.00	1.00	0.00	13.46	14.14	2.00	0.00	1.00	0.00
13.48	13.84	2.00	0.00	1.00	0.00	13.51	12.42	2.00	0.00	1.00	0.00
13.52	11.59	2.00	0.00	1.00	0.00	13.54	11.03	2.00	0.00	1.00	0.00
13.56	10.65	2.00	0.00	1.00	0.00	13.58	10.25	2.00	0.00	1.00	0.00
13.60	10.18	2.00	0.00	1.00	0.00	13.62	10.43	2.00	0.00	1.00	0.00
13.64	10.35	2.00	0.00	1.00	0.00	13.66	10.88	2.00	0.00	1.00	0.00
13.68	11.18	2.00	0.00	1.00	0.00	13.70	11.30	2.00	0.00	1.00	0.00
13.72	11.09	2.00	0.00	1.00	0.00	13.74	10.61	2.00	0.00	1.00	0.00
13.76	10.24	2.00	0.00	1.00	0.00	13.78	4.20	2.00	0.00	1.00	0.00
13.80	9.68	2.00	0.00	1.00	0.00	13.83	9.43	2.00	0.00	1.00	0.00
13.84	8.84	2.00	0.00	1.00	0.00	13.86	8.07	2.00	0.00	1.00	0.00
13.88	8.09	2.00	0.00	1.00	0.00	13.90	7.84	2.00	0.00	1.00	0.00
13.92	7.44	2.00	0.00	1.00	0.00	13.94	7.49	2.00	0.00	1.00	0.00
13.96	7.87	2.00	0.00	1.00	0.00	13.98	8.19	2.00	0.00	1.00	0.00
14.00	7.84	2.00	0.00	1.00	0.00	14.02	7.86	2.00	0.00	1.00	0.00
14.04	8.30	2.00	0.00	1.00	0.00	14.06	8.33	2.00	0.00	1.00	0.00
14.08	8.33	2.00	0.00	1.00	0.00	14.10	8.07	2.00	0.00	1.00	0.00
14.12	8.13	2.00	0.00	1.00	0.00	14.14	8.79	2.00	0.00	1.00	0.00
14.16	9.40	2.00	0.00	1.00	0.00	14.18	9.14	2.00	0.00	1.00	0.00
14.20	9.22	2.00	0.00	1.00	0.00	14.22	9.33	2.00	0.00	1.00	0.00
14.24	8.83	2.00	0.00	1.00	0.00	14.26	8.49	2.00	0.00	1.00	0.00
14.28	8.23	2.00	0.00	1.00	0.00	14.30	7.52	2.00	0.00	1.00	0.00
14.32	7.34	2.00	0.00	1.00	0.00	14.34	6.84	2.00	0.00	1.00	0.00
14.36	6.66	2.00	0.00	1.00	0.00	14.38	6.37	2.00	0.00	1.00	0.00
14.40	6.13	2.00	0.00	1.00	0.00	14.42	6.09	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
14.44	6.36	2.00	0.00	1.00	0.00	14.46	6.56	2.00	0.00	1.00	0.00
14.48	6.48	2.00	0.00	1.00	0.00	14.50	6.36	2.00	0.00	1.00	0.00
14.52	6.46	2.00	0.00	1.00	0.00	14.54	6.83	2.00	0.00	1.00	0.00
14.56	6.99	2.00	0.00	1.00	0.00	14.58	6.97	2.00	0.00	1.00	0.00
14.60	6.83	2.00	0.00	1.00	0.00	14.62	6.79	2.00	0.00	1.00	0.00
14.64	6.67	2.00	0.00	1.00	0.00	14.66	7.16	2.00	0.00	1.00	0.00
14.68	7.46	2.00	0.00	1.00	0.00	14.70	7.69	2.00	0.00	1.00	0.00
14.72	8.00	2.00	0.00	1.00	0.00	14.74	8.12	2.00	0.00	1.00	0.00
14.76	8.10	2.00	0.00	1.00	0.00	14.78	6.96	2.00	0.00	1.00	0.00
14.81	8.17	2.00	0.00	1.00	0.00	14.82	7.83	2.00	0.00	1.00	0.00
14.84	7.56	2.00	0.00	1.00	0.00	14.86	7.59	2.00	0.00	1.00	0.00
14.88	7.70	2.00	0.00	1.00	0.00	14.90	8.13	2.00	0.00	1.00	0.00
14.92	8.53	2.00	0.00	1.00	0.00	14.94	8.64	2.00	0.00	1.00	0.00
14.96	8.95	2.00	0.00	1.00	0.00	14.98	9.33	2.00	0.00	1.00	0.00
15.00	9.37	2.00	0.00	1.00	0.00	15.02	9.44	2.00	0.00	1.00	0.00
15.04	9.81	2.00	0.00	1.00	0.00	15.06	9.84	2.00	0.00	1.00	0.00
15.08	9.69	2.00	0.00	1.00	0.00	15.10	9.35	2.00	0.00	1.00	0.00
15.12	9.33	2.00	0.00	1.00	0.00	15.14	9.32	2.00	0.00	1.00	0.00
15.16	9.35	2.00	0.00	1.00	0.00	15.18	9.74	2.00	0.00	1.00	0.00
15.20	10.08	2.00	0.00	1.00	0.00	15.22	10.25	2.00	0.00	1.00	0.00
15.24	10.52	2.00	0.00	1.00	0.00	15.27	10.80	2.00	0.00	1.00	0.00
15.28	10.77	2.00	0.00	1.00	0.00	15.30	10.86	2.00	0.00	1.00	0.00
15.32	10.77	2.00	0.00	1.00	0.00	15.34	10.90	2.00	0.00	1.00	0.00
15.36	11.00	2.00	0.00	1.00	0.00	15.38	10.99	2.00	0.00	1.00	0.00
15.40	10.86	2.00	0.00	1.00	0.00	15.42	10.91	2.00	0.00	1.00	0.00
15.44	10.68	2.00	0.00	1.00	0.00	15.46	10.71	2.00	0.00	1.00	0.00
15.48	11.10	2.00	0.00	1.00	0.00	15.50	11.40	2.00	0.00	1.00	0.00
15.52	11.52	2.00	0.00	1.00	0.00	15.54	11.67	2.00	0.00	1.00	0.00
15.56	11.58	2.00	0.00	1.00	0.00	15.58	11.78	2.00	0.00	1.00	0.00
15.60	12.21	2.00	0.00	1.00	0.00	15.62	12.63	2.00	0.00	1.00	0.00
15.64	13.08	2.00	0.00	1.00	0.00	15.66	13.40	2.00	0.00	1.00	0.00
15.68	13.31	2.00	0.00	1.00	0.00	15.70	12.90	2.00	0.00	1.00	0.00
15.72	12.68	2.00	0.00	1.00	0.00	15.74	12.43	2.00	0.00	1.00	0.00
15.76	12.36	2.00	0.00	1.00	0.00	15.78	10.46	2.00	0.00	1.00	0.00
15.80	12.10	2.00	0.00	1.00	0.00	15.82	11.93	2.00	0.00	1.00	0.00
15.84	12.00	2.00	0.00	1.00	0.00	15.86	12.15	2.00	0.00	1.00	0.00
15.88	12.43	2.00	0.00	1.00	0.00	15.90	12.44	2.00	0.00	1.00	0.00
15.92	12.16	2.00	0.00	1.00	0.00	15.94	12.11	2.00	0.00	1.00	0.00
15.96	11.95	2.00	0.00	1.00	0.00	15.98	11.61	2.00	0.00	1.00	0.00
16.00	11.64	2.00	0.00	1.00	0.00	16.02	11.72	2.00	0.00	1.00	0.00
16.04	11.33	2.00	0.00	1.00	0.00	16.07	11.41	2.00	0.00	1.00	0.00
16.08	11.29	2.00	0.00	1.00	0.00	16.10	11.28	2.00	0.00	1.00	0.00
16.13	11.43	2.00	0.00	1.00	0.00	16.14	11.73	2.00	0.00	1.00	0.00
16.16	11.90	2.00	0.00	1.00	0.00	16.18	12.12	2.00	0.00	1.00	0.00
16.20	12.37	2.00	0.00	1.00	0.00	16.22	12.57	2.00	0.00	1.00	0.00
16.24	12.87	2.00	0.00	1.00	0.00	16.26	13.05	2.00	0.00	1.00	0.00
16.28	13.32	2.00	0.00	1.00	0.00	16.30	14.02	2.00	0.00	1.00	0.00
16.32	14.99	2.00	0.00	1.00	0.00	16.34	15.13	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
16.36	14.69	2.00	0.00	1.00	0.00	16.38	15.05	2.00	0.00	1.00	0.00
16.40	15.20	2.00	0.00	1.00	0.00	16.43	15.21	2.00	0.00	1.00	0.00
16.44	15.20	2.00	0.00	1.00	0.00	16.46	14.60	2.00	0.00	1.00	0.00
16.48	14.51	2.00	0.00	1.00	0.00	16.50	14.37	2.00	0.00	1.00	0.00
16.52	14.41	2.00	0.00	1.00	0.00	16.54	14.42	2.00	0.00	1.00	0.00
16.57	14.40	2.00	0.00	1.00	0.00	16.58	15.34	2.00	0.00	1.00	0.00
16.60	14.19	2.00	0.00	1.00	0.00	16.63	13.99	2.00	0.00	1.00	0.00
16.64	14.06	2.00	0.00	1.00	0.00	16.66	13.72	2.00	0.00	1.00	0.00
16.68	13.58	2.00	0.00	1.00	0.00	16.70	13.35	2.00	0.00	1.00	0.00
16.72	12.58	2.00	0.00	1.00	0.00	16.74	12.16	2.00	0.00	1.00	0.00
16.76	11.87	2.00	0.00	1.00	0.00	16.79	8.88	2.00	0.00	1.00	0.00
16.80	11.85	2.00	0.00	1.00	0.00	16.83	11.82	2.00	0.00	1.00	0.00
16.84	11.71	2.00	0.00	1.00	0.00	16.86	11.20	2.00	0.00	1.00	0.00
16.88	10.35	2.00	0.00	1.00	0.00	16.90	9.97	2.00	0.00	1.00	0.00
16.92	9.58	2.00	0.00	1.00	0.00	16.94	9.42	2.00	0.00	1.00	0.00
16.96	9.38	2.00	0.00	1.00	0.00	16.98	9.30	2.00	0.00	1.00	0.00
17.00	9.02	2.00	0.00	1.00	0.00	17.03	8.79	2.00	0.00	1.00	0.00
17.04	8.99	2.00	0.00	1.00	0.00	17.06	9.08	2.00	0.00	1.00	0.00
17.08	8.91	2.00	0.00	1.00	0.00	17.10	9.17	2.00	0.00	1.00	0.00
17.12	9.20	2.00	0.00	1.00	0.00	17.14	9.14	2.00	0.00	1.00	0.00
17.16	9.07	2.00	0.00	1.00	0.00	17.19	8.96	2.00	0.00	1.00	0.00
17.20	8.70	2.00	0.00	1.00	0.00	17.23	8.44	2.00	0.00	1.00	0.00
17.24	8.59	2.00	0.00	1.00	0.00	17.26	8.61	2.00	0.00	1.00	0.00
17.28	8.53	2.00	0.00	1.00	0.00	17.31	8.33	2.00	0.00	1.00	0.00
17.32	8.35	2.00	0.00	1.00	0.00	17.34	8.30	2.00	0.00	1.00	0.00
17.36	8.22	2.00	0.00	1.00	0.00	17.38	7.93	2.00	0.00	1.00	0.00
17.40	7.73	2.00	0.00	1.00	0.00	17.42	7.55	2.00	0.00	1.00	0.00
17.44	7.48	2.00	0.00	1.00	0.00	17.46	7.71	2.00	0.00	1.00	0.00
17.48	7.76	2.00	0.00	1.00	0.00	17.50	7.76	2.00	0.00	1.00	0.00
17.52	7.55	2.00	0.00	1.00	0.00	17.54	7.67	2.00	0.00	1.00	0.00
17.56	7.76	2.00	0.00	1.00	0.00	17.58	7.94	2.00	0.00	1.00	0.00
17.60	8.10	2.00	0.00	1.00	0.00	17.62	8.50	2.00	0.00	1.00	0.00
17.64	8.72	2.00	0.00	1.00	0.00	17.66	9.34	2.00	0.00	1.00	0.00
17.68	9.52	2.00	0.00	1.00	0.00	17.70	9.44	2.00	0.00	1.00	0.00
17.72	9.24	2.00	0.00	1.00	0.00	17.74	8.88	2.00	0.00	1.00	0.00
17.76	8.84	2.00	0.00	1.00	0.00	17.78	10.76	2.00	0.00	1.00	0.00
17.80	11.32	2.00	0.00	1.00	0.00	17.82	10.18	2.00	0.00	1.00	0.00
17.84	9.69	2.00	0.00	1.00	0.00	17.86	9.45	2.00	0.00	1.00	0.00
17.88	9.32	2.00	0.00	1.00	0.00	17.90	9.16	2.00	0.00	1.00	0.00
17.92	9.14	2.00	0.00	1.00	0.00	17.94	9.46	2.00	0.00	1.00	0.00
17.96	9.40	2.00	0.00	1.00	0.00	17.98	9.45	2.00	0.00	1.00	0.00
18.00	9.85	2.00	0.00	1.00	0.00	18.02	9.90	2.00	0.00	1.00	0.00
18.04	9.42	2.00	0.00	1.00	0.00	18.06	9.35	2.00	0.00	1.00	0.00
18.08	9.86	2.00	0.00	1.00	0.00	18.10	8.97	2.00	0.00	1.00	0.00
18.12	8.50	2.00	0.00	1.00	0.00	18.14	8.55	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)

Total estimated settlement: 0.00

Abbreviations

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumentric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

:: Strength loss calculation Idriss & Boulanger (2008) ::

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.03	6.57	111.75	1.00	111.75	1.55	0.11	0.84
0.04	7.82	132.99	1.00	132.99	1.52	0.22	0.87
0.07	6.99	118.79	1.00	118.79	1.56	0.14	0.85
0.08	6.25	106.23	1.00	106.23	1.60	0.12	0.84
0.10	6.27	106.53	1.00	106.53	1.64	0.13	0.84
0.12	5.84	99.30	1.00	99.30	1.71	0.14	0.83
0.14	4.65	79.01	1.19	93.86	1.90	0.11	0.79
0.17	3.31	56.24	1.43	80.56	2.09	0.08	0.75
0.18	2.45	41.61	1.87	77.89	2.28	0.10	0.71
0.20	2.07	35.12	2.09	73.53	2.34	0.09	0.69
0.22	1.62	27.48	2.88	79.19	2.52	0.09	0.66
0.24	1.26	21.41	4.04	86.50	2.71	0.08	21.77
0.26	1.09	18.53	5.09	94.32	2.84	0.08	17.38
0.28	1.03	17.47	5.67	98.95	2.90	0.07	15.21
0.30	1.04	17.65	5.85	103.28	2.92	0.07	14.33
0.32	1.05	17.74	6.17	109.42	2.95	0.07	13.48
0.34	1.06	17.87	6.47	115.70	2.98	0.07	12.77
0.36	1.02	17.25	7.07	121.89	3.03	0.07	11.61
0.38	0.99	16.75	7.55	126.45	3.07	0.07	10.66
0.40	0.95	16.02	8.22	131.65	3.12	0.07	9.68
0.42	0.92	15.58	8.78	136.86	3.17	0.07	8.94
0.44	0.89	15.06	9.38	141.31	3.21	0.07	8.24
0.46	0.88	14.78	9.70	143.40	3.23	0.07	7.72
0.48	0.86	14.46	9.97	144.08	3.25	0.07	7.22
0.50	0.84	14.13	10.18	143.84	3.26	0.07	6.76
0.52	0.80	13.53	10.57	142.99	3.29	0.07	6.22
0.54	0.77	12.98	10.88	141.18	3.31	0.06	5.74
0.56	0.75	12.61	11.00	138.71	3.32	0.06	5.37
0.58	0.74	12.42	10.99	136.53	3.32	0.06	5.10
0.60	0.74	12.34	10.91	134.65	3.31	0.06	4.90
0.62	0.73	12.18	10.94	133.25	3.31	0.06	4.68
0.64	0.72	12.10	10.88	131.66	3.31	0.06	4.50
0.66	0.73	12.14	10.67	129.55	3.30	0.06	4.37
0.68	0.73	12.22	10.40	127.00	3.28	0.06	4.27
0.70	0.75	12.48	10.04	125.32	3.25	0.06	4.24
0.72	0.76	12.78	9.76	124.72	3.24	0.06	4.22
0.74	0.78	13.08	9.55	124.83	3.22	0.07	4.20
0.76	0.80	13.43	9.27	124.55	3.20	0.07	4.20
0.78	0.82	13.72	8.97	123.07	3.18	0.07	4.18
0.80	0.83	13.95	8.68	121.04	3.16	0.07	4.14
0.82	0.84	13.99	8.48	118.72	3.14	0.07	4.05
0.84	0.84	13.98	8.41	117.65	3.14	0.07	3.95
0.86	0.85	14.27	8.22	117.31	3.12	0.07	3.94
0.88	0.88	14.67	8.07	118.41	3.11	0.07	3.96
0.90	0.91	15.15	7.93	120.16	3.10	0.07	3.99
0.92	0.96	16.00	7.62	121.98	3.08	0.07	4.13
0.94	1.01	16.93	7.27	123.16	3.05	0.07	4.27
0.97	1.07	17.95	6.91	123.99	3.01	0.07	4.39

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.98	1.11	18.52	6.76	125.26	3.00	0.07	4.48
1.01	1.14	19.13	6.64	126.99	2.99	0.07	4.49
1.02	1.20	20.17	6.40	129.12	2.97	0.07	4.69
1.04	1.28	21.51	6.10	131.17	2.94	0.08	4.90
1.06	1.36	22.76	5.85	133.12	2.92	0.08	5.08
1.08	1.39	23.33	5.79	135.04	2.91	0.08	5.11
1.10	1.39	23.34	5.91	137.96	2.92	0.08	5.02
1.13	1.38	23.15	6.10	141.14	2.94	0.08	4.84
1.14	1.38	23.12	6.25	144.39	2.95	0.08	4.79
1.16	1.38	23.18	6.37	147.57	2.97	0.08	4.72
1.19	1.38	23.06	6.54	150.72	2.98	0.08	4.57
1.20	1.37	22.88	6.71	153.43	3.00	0.08	4.50
1.22	1.34	22.49	6.88	154.81	3.01	0.08	4.35
1.24	1.32	22.11	7.03	155.33	3.02	0.08	4.20
1.26	1.29	21.47	7.22	155.10	3.04	0.08	4.01
1.28	1.25	20.92	7.39	154.58	3.06	0.07	3.85
1.30	1.22	20.37	7.55	153.85	3.07	0.07	3.68
1.32	1.20	19.96	7.67	153.10	3.08	0.07	3.55
1.34	1.18	19.70	7.73	152.27	3.08	0.07	3.45
1.36	1.18	19.68	7.70	151.48	3.08	0.07	3.40
1.38	1.19	19.80	7.59	150.29	3.07	0.07	3.37
1.40	1.20	19.94	7.41	147.76	3.06	0.07	3.34
1.42	1.20	19.95	7.23	144.30	3.04	0.07	3.30
1.44	1.20	19.88	7.09	141.00	3.03	0.07	3.24
1.46	1.18	19.57	7.12	139.32	3.03	0.07	3.14
1.48	1.16	19.21	7.20	138.35	3.04	0.07	3.04
1.50	1.13	18.82	7.30	137.44	3.05	0.07	2.94
1.52	1.13	18.73	7.28	136.34	3.05	0.07	2.89
1.54	1.13	18.71	7.23	135.34	3.04	0.07	2.85
1.56	1.15	18.99	7.09	134.73	3.03	0.07	2.85
1.58	1.16	19.22	6.97	133.93	3.02	0.07	2.85
1.60	1.18	19.53	6.81	133.08	3.01	0.07	2.86
1.62	1.18	19.49	6.79	132.39	3.00	0.07	2.82
1.64	1.16	19.22	6.88	132.28	3.01	0.07	2.74
1.66	1.12	18.60	7.12	132.45	3.03	0.07	2.62
1.68	1.08	17.85	7.40	132.12	3.06	0.07	2.49
1.70	1.03	16.99	7.69	130.69	3.08	0.07	2.34
1.72	0.99	16.22	7.91	128.25	3.10	0.07	2.21
1.74	0.94	15.50	8.11	125.66	3.11	0.07	2.09
1.76	0.92	15.10	8.13	122.70	3.12	0.07	2.01
1.78	0.91	14.90	8.06	120.14	3.11	0.07	1.96
1.80	0.91	14.95	7.86	117.54	3.09	0.07	1.94
1.82	0.90	14.79	7.81	115.49	3.09	0.07	1.91
1.84	0.89	14.49	7.79	112.77	3.09	0.07	1.87
1.86	0.84	13.68	7.99	109.29	3.11	0.07	1.75
1.88	0.78	12.74	8.21	104.57	3.12	0.06	1.63
1.90	0.73	11.81	8.53	100.75	3.15	0.06	1.50
1.92	0.68	11.00	8.86	97.41	3.17	0.06	1.39

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
1.94	0.63	10.15	9.33	94.70	3.21	0.06	1.28
1.96	0.57	9.04	10.04	90.80	3.26	0.06	1.13
1.98	0.51	8.11	10.66	86.44	3.30	0.06	1.01
2.01	0.48	7.57	10.80	81.71	3.31	0.06	0.94
2.02	0.48	7.47	10.23	76.42	3.27	0.06	0.93
2.04	0.48	7.58	9.21	69.76	3.20	0.06	0.94
2.06	0.48	7.57	8.28	62.69	3.13	0.06	0.93
2.08	0.48	7.52	7.53	56.60	3.07	0.06	0.92
2.10	0.47	7.41	7.02	52.00	3.02	0.06	0.91
2.12	0.49	7.61	6.48	49.34	2.98	0.06	0.93
2.14	0.50	7.93	6.01	47.62	2.93	0.06	0.96
2.16	0.53	8.43	5.57	46.94	2.89	0.06	1.02
2.18	0.63	10.06	4.58	46.11	2.78	0.07	1.22
2.21	0.79	12.70	3.53	44.85	2.63	0.07	1.53
2.22	0.97	15.85	2.76	43.79	2.50	0.07	0.60
2.24	1.10	18.04	2.54	45.91	2.45	0.07	0.61
2.26	1.18	19.42	2.72	52.87	2.49	0.08	0.62
2.28	1.24	20.47	3.10	63.54	2.56	0.08	0.63
2.30	1.30	21.37	3.51	75.04	2.63	0.08	2.53
2.32	1.34	22.04	3.90	85.89	2.69	0.09	2.60
2.34	1.36	22.50	4.35	97.76	2.75	0.09	2.64
2.36	1.38	22.76	4.81	109.52	2.80	0.08	2.66
2.38	1.39	22.89	5.24	119.90	2.85	0.08	2.66
2.40	1.39	22.91	5.52	126.51	2.88	0.08	2.65
2.42	1.36	22.48	5.83	131.08	2.91	0.08	2.59
2.44	1.33	21.89	6.11	133.71	2.94	0.08	2.51
2.46	1.28	21.08	6.42	135.41	2.97	0.08	2.41
2.48	1.26	20.65	6.53	134.93	2.98	0.07	2.35
2.50	1.25	20.55	6.48	133.15	2.98	0.07	2.33
2.52	1.26	20.73	6.34	131.38	2.96	0.07	2.33
2.54	1.28	20.99	6.21	130.28	2.95	0.08	2.35
2.56	1.29	21.21	6.13	129.95	2.94	0.08	2.37
2.58	1.30	21.34	6.06	129.34	2.94	0.08	2.37
2.60	1.31	21.56	5.94	128.10	2.92	0.08	2.39
2.62	1.32	21.62	5.90	127.53	2.92	0.08	2.38
2.64	1.31	21.55	5.94	127.93	2.92	0.08	2.37
2.66	1.30	21.25	6.09	129.47	2.94	0.08	2.32
2.68	1.30	21.28	6.13	130.53	2.94	0.08	2.32
2.70	1.32	21.59	6.06	130.74	2.94	0.08	2.34
2.72	1.36	22.26	5.83	129.90	2.91	0.08	2.40
2.74	1.38	22.63	5.72	129.44	2.90	0.08	2.43
2.76	1.39	22.87	5.65	129.15	2.89	0.08	2.45
2.78	1.39	22.87	5.61	128.26	2.89	0.08	2.44
2.80	1.40	22.93	5.49	125.84	2.88	0.08	2.43
2.82	1.37	22.45	5.46	122.58	2.88	0.08	2.37
2.84	1.29	21.03	5.77	121.34	2.91	0.08	2.21
2.86	1.16	18.94	6.43	121.81	2.97	0.07	1.98
2.88	1.05	16.96	7.29	123.61	3.05	0.07	1.77

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
2.92	0.97	15.53	8.06	125.17	3.11	0.07	1.61
2.92	0.91	14.60	8.63	125.98	3.15	0.07	1.51
2.94	0.87	13.84	9.05	125.25	3.19	0.07	1.43
2.97	0.81	12.92	9.48	122.50	3.22	0.07	1.32
2.99	0.76	12.09	9.71	117.33	3.23	0.06	1.23
3.00	0.75	11.92	9.33	111.20	3.21	0.06	1.21
3.02	0.82	13.01	7.88	102.52	3.10	0.06	1.32
3.05	0.89	14.27	6.52	92.99	2.98	0.07	1.44
3.06	0.94	14.98	5.52	82.75	2.88	0.07	1.51
3.08	0.93	14.81	5.28	78.24	2.86	0.07	1.49
3.10	0.95	15.21	5.16	78.48	2.84	0.07	1.52
3.12	1.02	16.45	4.98	81.92	2.82	0.08	1.64
3.14	1.10	17.81	4.80	85.53	2.80	0.08	1.77
3.16	1.15	18.68	4.74	88.45	2.79	0.08	1.85
3.18	1.16	18.84	4.89	92.08	2.81	0.08	1.86
3.20	1.16	18.82	5.09	95.76	2.83	0.08	1.85
3.22	1.13	18.27	5.45	99.53	2.87	0.08	1.79
3.24	1.09	17.57	5.80	102.00	2.91	0.07	1.72
3.26	1.06	16.98	6.17	104.78	2.95	0.07	1.65
3.28	1.06	17.00	6.29	106.94	2.96	0.07	1.65
3.30	1.08	17.42	6.27	109.32	2.96	0.07	1.68
3.32	1.11	17.94	6.16	110.55	2.95	0.07	1.73
3.34	1.15	18.56	5.95	110.43	2.93	0.07	1.78
3.36	1.19	19.26	5.69	109.63	2.90	0.08	1.84
3.38	1.25	20.16	5.38	108.49	2.87	0.08	1.92
3.40	1.30	21.07	5.17	108.91	2.84	0.08	2.00
3.42	1.34	21.74	5.05	109.87	2.83	0.08	2.06
3.44	1.36	22.14	5.04	111.67	2.83	0.08	2.09
3.46	1.34	21.80	5.22	113.84	2.85	0.08	2.05
3.49	1.30	21.09	5.51	116.23	2.88	0.08	1.97
3.50	1.27	20.62	5.70	117.45	2.90	0.08	1.92
3.52	1.27	20.48	5.80	118.86	2.91	0.08	1.90
3.54	1.27	20.49	5.92	121.28	2.92	0.08	1.90
3.56	1.25	20.20	6.18	124.82	2.95	0.07	1.86
3.58	1.23	19.89	6.40	127.25	2.97	0.07	1.83
3.60	1.22	19.66	6.50	127.72	2.98	0.07	1.80
3.62	1.22	19.72	6.46	127.32	2.97	0.07	1.80
3.64	1.25	20.08	6.29	126.30	2.96	0.07	1.83
3.66	1.29	20.79	5.95	123.72	2.93	0.07	1.89
3.68	1.33	21.48	5.59	119.99	2.89	0.08	1.94
3.70	1.36	22.00	5.30	116.62	2.86	0.08	1.98
3.72	1.37	22.11	5.23	115.65	2.85	0.08	1.98
3.74	1.36	21.96	5.29	116.11	2.86	0.08	1.96
3.76	1.35	21.75	5.37	116.74	2.87	0.08	1.94
3.78	1.34	21.63	5.43	117.55	2.87	0.08	1.92
3.80	1.33	21.44	5.58	119.59	2.89	0.08	1.90
3.82	1.30	21.00	5.84	122.71	2.91	0.08	1.85
3.84	1.26	20.25	6.21	125.84	2.95	0.07	1.78

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
3.86	1.22	19.51	6.50	126.75	2.98	0.07	1.71
3.88	1.20	19.17	6.59	126.32	2.99	0.07	1.67
3.90	1.19	19.10	6.53	124.65	2.98	0.07	1.66
3.92	1.19	19.09	6.47	123.44	2.97	0.07	1.66
3.94	1.16	18.57	6.53	121.29	2.98	0.07	1.61
3.96	1.12	17.91	6.67	119.36	2.99	0.07	1.54
3.98	1.08	17.14	6.88	117.92	3.01	0.07	1.47
4.00	1.05	16.64	7.09	117.93	3.03	0.07	1.42
4.02	1.01	15.97	7.43	118.64	3.06	0.07	1.36
4.05	0.98	15.37	7.75	119.08	3.09	0.07	1.30
4.06	0.94	14.72	8.08	118.95	3.11	0.07	1.25
4.08	0.93	14.53	8.15	118.43	3.12	0.07	1.23
4.10	0.93	14.54	8.08	117.56	3.11	0.07	1.23
4.12	0.95	14.91	7.81	116.50	3.09	0.07	1.25
4.14	0.97	15.27	7.56	115.38	3.07	0.07	1.28
4.16	1.00	15.68	7.29	114.27	3.05	0.07	1.31
4.18	1.02	16.05	7.06	113.29	3.03	0.07	1.34
4.20	1.04	16.36	6.88	112.58	3.01	0.07	1.36
4.22	1.05	16.60	6.76	112.24	3.00	0.07	1.37
4.24	1.05	16.62	6.78	112.74	3.00	0.07	1.37
4.26	1.05	16.57	6.87	113.77	3.01	0.07	1.36
4.28	1.06	16.75	6.89	115.34	3.01	0.07	1.37
4.30	1.09	17.23	6.77	116.58	3.00	0.07	1.41
4.32	1.13	17.87	6.56	117.30	2.98	0.07	1.45
4.34	1.15	18.18	6.45	117.24	2.97	0.07	1.48
4.36	1.14	18.12	6.45	116.86	2.97	0.07	1.47
4.38	1.14	18.00	6.41	115.37	2.97	0.07	1.45
4.40	1.13	17.83	6.37	113.61	2.97	0.07	1.43
4.42	1.12	17.66	6.30	111.27	2.96	0.07	1.42
4.44	1.09	17.23	6.36	109.54	2.96	0.07	1.38
4.46	1.06	16.63	6.52	108.52	2.98	0.07	1.33
4.48	1.02	16.08	6.71	107.83	3.00	0.07	1.28
4.50	0.98	15.37	7.02	107.95	3.02	0.07	1.22
4.52	0.94	14.67	7.40	108.53	3.06	0.06	1.16
4.54	0.88	13.63	7.99	108.94	3.11	0.06	1.07
4.56	0.83	12.67	8.53	108.07	3.15	0.06	0.99
4.58	0.76	11.62	9.07	105.45	3.19	0.06	0.91
4.60	0.72	10.79	9.48	102.31	3.22	0.06	0.84
4.62	0.67	10.01	9.93	99.32	3.25	0.06	0.78
4.64	0.63	9.26	10.31	95.46	3.27	0.06	0.72
4.66	0.59	8.65	10.55	91.28	3.29	0.06	0.67
4.68	0.56	8.17	10.55	86.16	3.29	0.06	0.63
4.70	0.55	7.96	10.31	82.15	3.27	0.06	0.61
4.72	0.55	7.97	9.81	78.24	3.24	0.06	0.61
4.74	0.56	8.06	9.25	74.52	3.20	0.06	0.62
4.76	0.58	8.37	8.44	70.68	3.14	0.06	0.64
4.78	0.59	8.59	7.85	67.42	3.09	0.06	0.66
4.80	0.61	8.85	7.41	65.57	3.06	0.06	0.67

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
4.82	0.61	8.96	7.21	64.54	3.04	0.06	0.68
4.84	0.60	8.82	7.27	64.18	3.05	0.06	0.67
4.86	0.63	9.25	6.99	64.68	3.02	0.06	0.70
4.88	0.65	9.57	6.96	66.63	3.02	0.06	0.72
4.90	0.68	10.16	6.70	68.11	3.00	0.06	0.77
4.92	0.69	10.20	6.73	68.65	3.00	0.06	0.77
4.94	0.68	10.16	6.66	67.66	2.99	0.06	0.76
4.96	0.68	10.01	6.70	67.08	3.00	0.06	0.75
4.98	0.66	9.81	6.83	66.99	3.01	0.06	0.73
5.00	0.67	9.94	6.63	65.85	2.99	0.06	0.74
5.02	0.69	10.20	6.22	63.46	2.95	0.06	0.76
5.04	0.73	10.82	5.63	60.92	2.89	0.06	0.80
5.06	0.77	11.55	5.21	60.15	2.85	0.07	0.85
5.08	0.82	12.36	4.92	60.85	2.82	0.07	0.91
5.10	0.86	13.00	4.71	61.21	2.79	0.07	0.96
5.12	0.90	13.58	4.48	60.82	2.76	0.07	1.01
5.14	0.94	14.16	4.25	60.23	2.73	0.07	1.06
5.16	0.98	14.84	4.10	60.81	2.71	0.07	1.11
5.19	1.00	15.12	4.08	61.76	2.71	0.07	1.13
5.20	1.01	15.28	4.17	63.74	2.72	0.07	1.14
5.22	1.01	15.25	4.34	66.15	2.75	0.07	1.14
5.24	1.03	15.51	4.38	67.86	2.75	0.07	1.15
5.26	1.05	15.91	4.40	70.00	2.75	0.07	1.18
5.28	1.08	16.35	4.44	72.64	2.76	0.07	1.21
5.30	1.11	16.86	4.46	75.26	2.76	0.07	1.25
5.32	1.15	17.43	4.44	77.39	2.76	0.08	1.29
5.34	1.19	18.01	4.41	79.43	2.75	0.08	1.34
5.36	1.24	18.70	4.37	81.66	2.75	0.08	1.39
5.38	1.28	19.39	4.33	83.88	2.74	0.08	1.44
5.40	1.32	20.02	4.30	86.18	2.74	0.08	1.49
5.42	1.36	20.55	4.32	88.70	2.74	0.08	1.53
5.44	1.40	21.15	4.33	91.52	2.74	0.08	1.57
5.46	1.45	21.82	4.30	93.81	2.74	0.08	1.62
5.48	1.49	22.48	4.34	97.63	2.75	0.08	1.67
5.50	1.51	22.83	4.48	102.20	2.76	0.08	1.69
5.52	1.52	22.99	4.65	106.82	2.78	0.08	1.69
5.54	1.50	22.85	4.92	112.36	2.82	0.08	1.67
5.56	1.49	22.69	5.21	118.25	2.85	0.08	1.65
5.58	1.44	22.07	5.67	125.20	2.90	0.08	1.59
5.60	1.39	21.30	6.14	130.70	2.94	0.07	1.52
5.62	1.31	19.98	6.78	135.37	3.00	0.07	1.43
5.64	1.24	18.79	7.37	138.46	3.05	0.07	1.34
5.66	1.17	17.45	7.98	139.26	3.10	0.07	1.25
5.68	1.10	16.33	8.36	136.49	3.13	0.07	1.17
5.70	1.06	15.59	8.41	131.13	3.14	0.07	1.11
5.72	1.04	15.26	8.22	125.46	3.12	0.07	1.09
5.74	1.05	15.41	7.78	119.85	3.09	0.07	1.10
5.76	1.09	16.00	7.09	113.46	3.03	0.07	1.14

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
5.78	1.13	16.55	6.45	106.85	2.97	0.07	1.18
5.80	1.16	16.91	6.00	101.47	2.93	0.07	1.21
5.82	1.17	17.05	5.80	98.90	2.91	0.07	1.22
5.84	1.20	17.43	5.52	96.13	2.88	0.07	1.26
5.86	1.28	18.47	5.10	94.27	2.84	0.07	1.34
5.89	1.36	19.55	4.87	95.22	2.81	0.08	1.43
5.90	1.43	20.59	4.84	99.72	2.81	0.08	1.50
5.92	1.45	20.85	5.03	104.92	2.83	0.08	1.52
5.94	1.43	20.71	5.26	109.00	2.85	0.08	1.50
5.96	1.41	20.35	5.53	112.60	2.88	0.07	1.47
5.98	1.37	19.84	5.91	117.18	2.92	0.07	1.42
6.01	1.36	19.59	6.18	121.12	2.95	0.07	1.40
6.02	1.33	19.17	6.51	124.92	2.98	0.07	1.37
6.04	1.32	18.98	6.71	127.40	3.00	0.07	1.36
6.06	1.30	18.57	6.98	129.57	3.02	0.07	1.33
6.08	1.29	18.29	7.17	131.13	3.04	0.07	1.31
6.10	1.25	17.70	7.44	131.71	3.06	0.07	1.26
6.12	1.22	17.16	7.62	130.77	3.08	0.07	1.23
6.14	1.19	16.68	7.70	128.46	3.08	0.07	1.19
6.16	1.18	16.42	7.64	125.56	3.08	0.07	1.17
6.18	1.15	15.97	7.73	123.52	3.08	0.07	1.14
6.21	1.13	15.54	7.88	122.51	3.10	0.07	1.11
6.22	1.10	15.11	8.10	122.41	3.11	0.07	1.08
6.25	1.08	14.78	8.28	122.42	3.13	0.07	1.06
6.26	1.07	14.56	8.42	122.56	3.14	0.06	1.04
6.28	1.06	14.41	8.51	122.64	3.15	0.06	1.03
6.30	1.07	14.47	8.42	121.86	3.14	0.06	1.03
6.32	1.09	14.71	8.15	119.98	3.12	0.07	1.05
6.34	1.11	14.98	7.81	117.00	3.09	0.07	1.07
6.36	1.12	15.08	7.56	113.95	3.07	0.07	1.08
6.38	1.12	15.11	7.36	111.26	3.05	0.07	1.08
6.40	1.14	15.27	7.17	109.51	3.04	0.07	1.09
6.42	1.15	15.37	7.08	108.83	3.03	0.07	1.10
6.44	1.16	15.46	7.07	109.40	3.03	0.07	1.10
6.46	1.16	15.45	7.12	110.09	3.03	0.07	1.10
6.48	1.17	15.58	7.08	110.30	3.03	0.07	1.11
6.50	1.18	15.69	7.04	110.44	3.03	0.07	1.12
6.52	1.20	15.99	6.93	110.85	3.02	0.07	1.14
6.54	1.24	16.48	6.77	111.68	3.00	0.07	1.18
6.56	1.28	17.01	6.60	112.23	2.99	0.07	1.22
6.58	1.31	17.41	6.49	112.91	2.98	0.07	1.24
6.60	1.33	17.63	6.47	114.09	2.98	0.07	1.26
6.62	1.34	17.72	6.54	115.93	2.98	0.07	1.27
6.64	1.34	17.71	6.66	118.03	2.99	0.07	1.27
6.66	1.33	17.55	6.85	120.23	3.01	0.07	1.25
6.68	1.34	17.56	6.95	122.01	3.02	0.07	1.25
6.70	1.35	17.71	6.97	123.49	3.02	0.07	1.27
6.72	1.37	17.97	6.94	124.63	3.02	0.07	1.28

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
6.74	1.38	18.01	6.97	125.51	3.02	0.07	1.29
6.76	1.38	18.03	6.97	125.71	3.02	0.07	1.29
6.78	1.40	18.21	6.85	124.71	3.01	0.07	1.30
6.80	1.43	18.59	6.64	123.53	2.99	0.07	1.33
6.82	1.45	18.90	6.54	123.54	2.98	0.07	1.35
6.84	1.49	19.29	6.53	125.90	2.98	0.07	1.38
6.86	1.52	19.71	6.54	128.99	2.98	0.07	1.41
6.88	1.54	19.98	6.63	132.49	2.99	0.07	1.43
6.90	1.54	19.94	6.77	134.90	3.00	0.07	1.42
6.92	1.51	19.41	7.06	137.08	3.03	0.07	1.39
6.94	1.46	18.64	7.40	138.05	3.06	0.07	1.33
6.96	1.40	17.77	7.76	137.81	3.09	0.07	1.27
6.98	1.36	17.15	7.94	136.14	3.10	0.07	1.23
7.00	1.35	16.95	7.86	133.15	3.09	0.07	1.21
7.02	1.34	16.87	7.68	129.59	3.08	0.07	1.20
7.04	1.36	17.04	7.38	125.74	3.06	0.07	1.22
7.06	1.38	17.31	7.09	122.73	3.03	0.07	1.24
7.08	1.43	17.88	6.76	120.87	3.00	0.07	1.28
7.10	1.46	18.36	6.54	120.00	2.98	0.07	1.31
7.12	1.50	18.84	6.34	119.45	2.96	0.07	1.35
7.14	1.51	18.89	6.33	119.65	2.96	0.07	1.35
7.16	1.50	18.68	6.46	120.67	2.97	0.07	1.33
7.18	1.48	18.33	6.68	122.36	2.99	0.07	1.31
7.20	1.47	18.19	6.80	123.65	3.00	0.07	1.30
7.22	1.49	18.41	6.78	124.74	3.00	0.07	1.31
7.24	1.52	18.80	6.68	125.61	2.99	0.07	1.34
7.26	1.55	19.10	6.64	126.87	2.99	0.07	1.36
7.28	1.57	19.31	6.66	128.65	2.99	0.07	1.38
7.30	1.59	19.59	6.65	130.32	2.99	0.07	1.40
7.32	1.65	20.36	6.44	131.03	2.97	0.07	1.45
7.34	1.73	21.40	6.10	130.58	2.94	0.07	1.53
7.36	1.82	22.42	5.78	129.66	2.91	0.08	1.60
7.38	1.87	23.06	5.59	128.92	2.89	0.08	1.65
7.40	1.89	23.24	5.55	128.87	2.88	0.08	1.67
7.42	1.88	23.09	5.60	129.39	2.89	0.08	1.65
7.44	1.88	22.96	5.69	130.52	2.90	0.08	1.64
7.46	1.88	22.97	5.80	133.10	2.91	0.08	1.64
7.48	1.89	23.05	5.90	136.07	2.92	0.08	1.65
7.50	1.90	23.18	6.00	139.16	2.93	0.08	1.66
7.52	1.92	23.36	6.03	140.78	2.93	0.08	1.67
7.54	1.95	23.64	6.00	141.80	2.93	0.08	1.69
7.56	1.96	23.69	6.00	142.05	2.93	0.08	1.69
7.58	1.95	23.57	6.02	141.89	2.93	0.08	1.68
7.60	1.91	22.98	6.18	142.02	2.95	0.08	1.64
7.62	1.86	22.26	6.42	142.90	2.97	0.07	1.59
7.64	1.81	21.56	6.67	143.88	2.99	0.07	1.54
7.66	1.78	21.08	6.85	144.51	3.01	0.07	1.51
7.68	1.75	20.63	7.02	144.89	3.02	0.07	1.47

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
7.70	1.71	20.08	7.24	145.45	3.04	0.07	1.43
7.72	1.67	19.56	7.47	146.10	3.06	0.07	1.40
7.74	1.64	19.18	7.62	146.09	3.08	0.07	1.37
7.76	1.63	18.92	7.72	145.97	3.08	0.07	1.35
7.78	1.63	18.91	7.69	145.44	3.08	0.07	1.35
7.80	1.63	18.84	7.68	144.64	3.08	0.07	1.35
7.82	1.64	18.96	7.52	142.53	3.07	0.07	1.35
7.84	1.66	19.09	7.38	140.87	3.06	0.07	1.36
7.86	1.68	19.37	7.22	139.85	3.04	0.07	1.38
7.88	1.71	19.63	7.13	139.94	3.03	0.07	1.40
7.90	1.72	19.71	7.08	139.56	3.03	0.07	1.41
7.92	1.73	19.85	6.99	138.75	3.02	0.07	1.42
7.94	1.74	19.87	6.95	138.10	3.02	0.07	1.42
7.96	1.75	20.00	6.87	137.43	3.01	0.07	1.43
7.98	1.75	19.92	6.86	136.65	3.01	0.07	1.42
8.00	1.73	19.62	6.93	135.92	3.02	0.07	1.40
8.02	1.68	18.91	7.14	135.10	3.04	0.07	1.35
8.04	1.60	17.93	7.49	134.25	3.06	0.07	1.28
8.07	1.53	16.98	7.81	132.53	3.09	0.07	1.21
8.08	1.47	16.25	8.00	129.99	3.11	0.07	1.16
8.10	1.43	15.68	8.12	127.42	3.12	0.07	1.12
8.12	1.38	15.13	8.27	125.07	3.13	0.07	1.08
8.14	1.35	14.73	8.37	123.36	3.13	0.07	1.05
8.16	1.35	14.62	8.32	121.61	3.13	0.07	1.04
8.18	1.36	14.70	8.17	120.13	3.12	0.07	1.05
8.20	1.37	14.87	8.00	118.98	3.11	0.07	1.06
8.22	1.37	14.84	7.95	118.06	3.10	0.07	1.06
8.24	1.39	14.95	7.84	117.25	3.09	0.07	1.07
8.26	1.42	15.27	7.63	116.52	3.08	0.07	1.09
8.28	1.47	15.90	7.29	115.96	3.05	0.07	1.14
8.30	1.51	16.33	7.10	115.89	3.03	0.07	1.17
8.32	1.54	16.65	6.96	115.92	3.02	0.07	1.19
8.34	1.55	16.77	6.94	116.35	3.02	0.07	1.20
8.36	1.58	17.04	6.84	116.49	3.01	0.07	1.22
8.38	1.58	17.01	6.91	117.54	3.01	0.07	1.21
8.40	1.57	16.90	7.06	119.26	3.03	0.07	1.21
8.42	1.55	16.56	7.35	121.78	3.05	0.07	1.18
8.44	1.54	16.48	7.54	124.26	3.07	0.07	1.18
8.47	1.56	16.61	7.60	126.21	3.07	0.07	1.19
8.48	1.59	16.98	7.52	127.61	3.07	0.07	1.21
8.50	1.63	17.37	7.37	128.07	3.05	0.07	1.24
8.52	1.65	17.57	7.29	128.09	3.05	0.07	1.25
8.54	1.65	17.46	7.33	128.03	3.05	0.07	1.25
8.56	1.64	17.30	7.40	128.02	3.06	0.07	1.24
8.58	1.63	17.15	7.47	128.08	3.06	0.07	1.23
8.60	1.63	17.16	7.52	128.98	3.07	0.07	1.23
8.62	1.63	17.08	7.64	130.51	3.08	0.07	1.22
8.64	1.62	16.94	7.77	131.72	3.09	0.07	1.21

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
8.66	1.60	16.69	7.90	131.93	3.10	0.07	1.19
8.68	1.57	16.32	8.02	130.85	3.11	0.07	1.17
8.70	1.54	15.93	8.10	129.08	3.11	0.07	1.14
8.72	1.51	15.59	8.09	126.12	3.11	0.07	1.11
8.74	1.50	15.35	8.00	122.76	3.11	0.07	1.10
8.76	1.48	15.10	7.92	119.53	3.10	0.07	1.08
8.78	1.49	15.19	7.65	116.21	3.08	0.07	1.09
8.80	1.52	15.57	7.22	112.48	3.04	0.07	1.11
8.82	1.62	16.57	6.54	108.31	2.98	0.07	1.18
8.84	1.69	17.38	6.09	105.82	2.94	0.07	1.24
8.86	1.76	18.13	5.83	105.77	2.91	0.07	1.29
8.88	1.79	18.43	5.83	107.39	2.91	0.08	1.32
8.90	1.83	18.82	5.80	109.17	2.91	0.08	1.34
8.92	1.85	19.00	5.88	111.79	2.92	0.08	1.36
8.94	1.85	19.02	6.04	114.82	2.93	0.07	1.36
8.96	1.84	18.79	6.30	118.45	2.96	0.07	1.34
8.98	1.81	18.46	6.57	121.33	2.98	0.07	1.32
9.00	1.76	17.85	6.91	123.40	3.02	0.07	1.27
9.02	1.71	17.33	7.17	124.31	3.04	0.07	1.24
9.04	1.67	16.83	7.37	124.11	3.05	0.07	1.20
9.06	1.65	16.54	7.46	123.41	3.06	0.07	1.18
9.09	1.59	15.79	7.67	121.04	3.08	0.07	1.13
9.10	1.48	14.57	8.10	117.96	3.11	0.07	1.04
9.13	1.36	13.17	8.58	113.01	3.15	0.07	0.94
9.14	1.25	12.03	9.05	108.82	3.19	0.06	0.86
9.16	1.20	11.37	9.23	104.90	3.20	0.06	0.81
9.18	1.17	11.03	9.23	101.84	3.20	0.06	0.79
9.20	1.17	11.06	8.91	98.48	3.18	0.06	0.79
9.22	1.20	11.29	8.34	94.17	3.13	0.06	0.81
9.24	1.23	11.62	7.70	89.45	3.08	0.06	0.83
9.26	1.26	11.93	7.11	84.86	3.03	0.06	0.85
9.28	1.27	11.99	6.75	80.93	3.00	0.06	0.86
9.30	1.26	11.89	6.58	78.30	2.99	0.06	0.85
9.32	1.21	11.33	6.80	77.04	3.01	0.06	0.81
9.34	1.16	10.71	7.18	76.88	3.04	0.06	0.77
9.36	1.10	10.04	7.65	76.81	3.08	0.06	0.72
9.38	1.07	9.72	7.87	76.45	3.10	0.06	0.69
9.40	1.06	9.63	7.87	75.82	3.10	0.06	0.69
9.42	1.08	9.88	7.53	74.39	3.07	0.06	0.71
9.44	1.14	10.43	6.92	72.24	3.02	0.06	0.75
9.47	1.20	11.06	6.39	70.65	2.97	0.06	0.79
9.48	1.30	12.15	5.75	69.88	2.91	0.07	0.87
9.50	1.44	13.53	5.14	69.61	2.84	0.07	0.97
9.52	1.61	15.37	4.40	67.62	2.75	0.08	1.10
9.54	1.76	16.85	4.06	68.47	2.71	0.08	1.21
9.56	1.86	17.88	4.04	72.29	2.71	0.08	1.28
9.58	1.92	18.50	4.33	80.13	2.74	0.08	1.33
9.60	1.96	18.95	4.64	87.85	2.78	0.08	1.36

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.62	2.02	19.51	4.88	95.28	2.81	0.08	1.40
9.64	2.07	20.00	5.08	101.67	2.83	0.08	1.43
9.66	2.12	20.56	5.26	108.13	2.85	0.08	1.47
9.68	2.17	21.04	5.34	112.41	2.86	0.08	1.50
9.70	2.22	21.56	5.35	115.37	2.86	0.08	1.54
9.72	2.28	22.07	5.30	117.01	2.86	0.08	1.58
9.74	2.30	22.29	5.42	120.79	2.87	0.08	1.59
9.76	2.27	21.90	5.75	125.82	2.90	0.08	1.56
9.78	2.17	20.80	6.26	130.18	2.96	0.08	1.49
9.80	2.02	19.20	6.85	131.53	3.01	0.07	1.37
9.82	1.83	17.22	7.62	131.23	3.08	0.07	1.23
9.84	1.63	15.09	8.56	129.14	3.15	0.07	1.08
9.86	1.43	12.98	9.67	125.54	3.23	0.07	0.93
9.88	1.27	11.27	10.64	119.97	3.30	0.06	0.81
9.91	1.13	9.88	11.46	113.23	3.35	0.06	0.71
9.92	1.05	8.97	11.97	107.37	3.38	0.06	0.64
9.94	0.99	8.37	12.08	101.17	3.39	0.06	0.60
9.96	0.96	8.07	11.77	95.06	3.37	0.06	0.58
9.98	0.95	7.95	11.03	87.66	3.32	0.06	0.57
10.00	0.95	7.93	10.17	80.65	3.26	0.06	0.57
10.02	0.96	8.04	9.25	74.32	3.20	0.06	0.57
10.04	0.98	8.16	8.41	68.57	3.14	0.06	0.58
10.06	0.98	8.20	7.79	63.87	3.09	0.06	0.59
10.08	0.99	8.22	7.35	60.42	3.05	0.06	0.59
10.10	1.02	8.53	6.88	58.74	3.01	0.06	0.61
10.12	1.08	9.16	6.26	57.35	2.96	0.06	0.65
10.14	1.25	10.80	5.21	56.24	2.85	0.07	0.77
10.16	1.50	13.35	4.10	54.77	2.71	0.08	0.95
10.18	1.77	16.10	3.43	55.14	2.62	0.08	1.15
10.20	1.90	17.38	3.39	58.91	2.61	0.08	1.24
10.22	1.85	16.84	3.88	65.36	2.68	0.08	1.20
10.24	1.73	15.55	4.63	71.96	2.78	0.08	1.11
10.26	1.72	15.45	4.73	72.99	2.79	0.08	1.10
10.28	1.93	17.50	4.11	71.88	2.72	0.08	1.25
10.30	2.32	21.36	3.23	68.93	2.58	0.08	0.63
10.32	2.69	25.03	2.70	67.60	2.49	0.09	0.65
10.34	2.82	26.32	2.53	66.55	2.45	0.09	0.65
10.36	2.69	25.04	2.67	66.83	2.48	0.09	0.65
10.38	2.36	21.63	3.14	67.99	2.57	0.09	0.63
10.40	2.06	18.65	3.68	68.72	2.66	0.08	1.33
10.42	1.80	16.00	4.15	66.37	2.72	0.08	1.14
10.44	1.62	14.20	4.63	65.76	2.78	0.08	1.01
10.46	1.43	12.34	5.52	68.13	2.88	0.07	0.88
10.48	1.28	10.83	6.68	72.36	2.99	0.06	0.77
10.50	1.18	9.84	7.55	74.30	3.07	0.06	0.70
10.52	1.11	9.15	7.99	73.07	3.11	0.06	0.65
10.54	1.07	8.68	8.16	70.80	3.12	0.06	0.62
10.56	1.03	8.29	8.24	68.34	3.12	0.06	0.59

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
10.58	1.02	8.12	8.10	65.79	3.11	0.06	0.58
10.60	1.02	8.18	7.62	62.34	3.08	0.06	0.58
10.62	1.04	8.34	7.06	58.85	3.03	0.06	0.60
10.64	1.05	8.41	6.75	56.72	3.00	0.06	0.60
10.66	1.05	8.45	6.61	55.88	2.99	0.06	0.60
10.68	1.06	8.48	6.62	56.13	2.99	0.06	0.61
10.70	1.08	8.67	6.53	56.63	2.98	0.06	0.62
10.72	1.12	9.09	6.28	57.04	2.96	0.06	0.65
10.74	1.27	10.51	5.51	57.92	2.88	0.07	0.75
10.76	1.61	13.79	4.16	57.37	2.72	0.08	0.98
10.78	2.01	17.66	3.24	57.26	2.59	0.08	0.61
10.80	2.56	23.01	2.45	56.31	2.43	0.08	0.64
10.82	2.93	26.62	2.15	57.11	2.36	0.08	0.66
10.84	3.13	28.53	2.07	58.96	2.34	0.08	0.66
10.86	2.88	26.03	2.38	61.96	2.42	0.09	0.65
10.88	2.45	21.81	3.06	66.66	2.55	0.08	0.63
10.90	1.98	17.21	4.17	71.79	2.72	0.08	1.23
10.92	1.62	13.68	5.49	75.14	2.88	0.07	0.98
10.94	1.44	11.92	6.02	71.74	2.93	0.07	0.85
10.96	1.43	11.78	5.65	66.52	2.89	0.07	0.84
10.98	1.53	12.78	4.79	61.20	2.80	0.07	0.91
11.00	1.64	13.77	4.54	62.55	2.77	0.08	0.98
11.02	1.70	14.32	4.61	66.03	2.78	0.08	1.02
11.04	1.72	14.54	4.81	70.02	2.80	0.08	1.04
11.06	1.69	14.21	5.34	75.88	2.86	0.07	1.01
11.08	1.64	13.66	6.00	81.98	2.93	0.07	0.98
11.10	1.55	12.81	6.96	89.12	3.02	0.07	0.92
11.13	1.46	11.96	7.91	94.55	3.10	0.07	0.85
11.14	1.36	11.01	8.99	98.95	3.18	0.06	0.79
11.16	1.27	10.13	10.01	101.40	3.25	0.06	0.72
11.18	1.18	9.22	11.07	102.02	3.32	0.06	0.66
11.20	1.10	8.45	11.98	101.18	3.38	0.06	0.60
11.22	1.03	7.83	12.68	99.24	3.42	0.06	0.56
11.24	1.00	7.48	12.92	96.71	3.43	0.06	0.53
11.26	0.99	7.43	12.52	93.03	3.41	0.06	0.53
11.28	1.00	7.51	11.68	87.67	3.36	0.06	0.54
11.30	1.00	7.47	10.79	80.58	3.30	0.06	0.53
11.32	1.00	7.45	9.86	73.40	3.24	0.06	0.53
11.34	1.03	7.70	8.57	65.99	3.15	0.06	0.55
11.36	1.11	8.48	6.99	59.25	3.02	0.06	0.61
11.38	1.24	9.59	5.50	52.69	2.88	0.07	0.68
11.40	1.38	10.91	4.51	49.18	2.77	0.07	0.78
11.42	1.52	12.23	3.94	48.22	2.69	0.07	0.87
11.44	1.63	13.24	3.85	51.00	2.68	0.08	0.94
11.46	1.68	13.66	4.09	55.88	2.71	0.08	0.97
11.48	1.66	13.51	4.66	62.87	2.78	0.08	0.96
11.50	1.63	13.18	5.23	68.95	2.85	0.07	0.94
11.52	1.60	12.85	5.87	75.45	2.92	0.07	0.92

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
11.54	1.56	12.49	6.60	82.35	2.99	0.07	0.89
11.56	1.52	12.08	7.35	88.86	3.05	0.07	0.86
11.58	1.49	11.77	8.04	94.58	3.11	0.07	0.84
11.60	1.48	11.65	8.41	98.00	3.14	0.07	0.83
11.62	1.48	11.67	8.66	100.99	3.16	0.07	0.83
11.64	1.48	11.62	8.82	102.55	3.17	0.07	0.83
11.66	1.47	11.46	8.97	102.79	3.18	0.07	0.82
11.68	1.44	11.21	9.05	101.48	3.19	0.06	0.80
11.70	1.42	10.99	9.03	99.29	3.18	0.06	0.79
11.72	1.41	10.86	8.95	97.22	3.18	0.06	0.78
11.74	1.39	10.68	8.93	95.41	3.18	0.06	0.76
11.76	1.39	10.63	8.87	94.24	3.17	0.06	0.76
11.78	1.39	10.68	8.78	93.79	3.17	0.06	0.76
11.80	1.43	10.99	8.56	94.14	3.15	0.06	0.79
11.82	1.47	11.32	8.36	94.70	3.13	0.07	0.81
11.84	1.51	11.68	8.15	95.28	3.12	0.07	0.83
11.86	1.55	12.00	7.95	95.46	3.10	0.07	0.86
11.88	1.60	12.39	7.71	95.50	3.08	0.07	0.88
11.90	1.63	12.67	7.54	95.55	3.07	0.07	0.91
11.92	1.65	12.80	7.48	95.75	3.06	0.07	0.91
11.94	1.65	12.77	7.53	96.18	3.07	0.07	0.91
11.96	1.64	12.70	7.60	96.48	3.07	0.07	0.91
11.98	1.64	12.69	7.61	96.59	3.07	0.07	0.91
12.00	1.65	12.77	7.58	96.79	3.07	0.07	0.91
12.02	1.67	12.90	7.53	97.15	3.07	0.07	0.92
12.04	1.70	13.14	7.44	97.82	3.06	0.07	0.94
12.06	1.74	13.49	7.29	98.40	3.05	0.07	0.96
12.08	1.80	14.00	7.12	99.71	3.03	0.07	1.00
12.10	1.86	14.52	7.02	101.98	3.02	0.07	1.04
12.12	1.92	14.94	7.06	105.42	3.03	0.07	1.07
12.14	1.96	15.28	7.16	109.35	3.04	0.07	1.09
12.16	1.98	15.43	7.32	113.00	3.05	0.07	1.10
12.18	1.99	15.48	7.52	116.45	3.07	0.07	1.11
12.21	1.99	15.43	7.73	119.25	3.08	0.07	1.10
12.22	1.98	15.39	7.92	121.85	3.10	0.07	1.10
12.24	1.97	15.27	8.11	123.83	3.11	0.07	1.09
12.26	1.96	15.12	8.24	124.65	3.13	0.07	1.08
12.28	1.94	14.98	8.32	124.65	3.13	0.07	1.07
12.30	1.94	14.89	8.30	123.64	3.13	0.07	1.06
12.32	1.94	14.86	8.24	122.39	3.12	0.07	1.06
12.34	1.95	14.97	8.08	121.00	3.11	0.07	1.07
12.36	1.99	15.25	7.87	120.03	3.10	0.07	1.09
12.38	2.03	15.57	7.69	119.71	3.08	0.07	1.11
12.40	2.06	15.82	7.56	119.66	3.07	0.07	1.13
12.42	2.05	15.66	7.62	119.37	3.08	0.07	1.12
12.44	2.00	15.25	7.80	118.99	3.09	0.07	1.09
12.46	1.96	14.90	7.93	118.19	3.10	0.07	1.06
12.48	1.98	15.04	7.79	117.24	3.09	0.07	1.07

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
12.50	2.03	15.44	7.49	115.73	3.06	0.07	1.10
12.52	2.07	15.72	7.26	114.08	3.04	0.07	1.12
12.54	2.06	15.63	7.22	112.84	3.04	0.07	1.12
12.56	2.01	15.18	7.43	112.72	3.06	0.07	1.08
12.58	1.94	14.56	7.78	113.35	3.09	0.07	1.04
12.60	1.88	13.98	8.16	114.07	3.12	0.07	1.00
12.62	1.84	13.69	8.34	114.15	3.13	0.07	0.98
12.64	1.82	13.47	8.44	113.71	3.14	0.07	0.96
12.66	1.82	13.40	8.42	112.86	3.14	0.07	0.96
12.68	1.80	13.28	8.41	111.69	3.14	0.07	0.95
12.70	1.81	13.34	8.30	110.77	3.13	0.07	0.95
12.72	1.83	13.42	8.19	109.85	3.12	0.07	0.96
12.74	1.86	13.68	7.95	108.81	3.10	0.07	0.98
12.76	1.92	14.16	7.59	107.39	3.07	0.07	1.01
12.78	2.02	14.96	7.05	105.43	3.03	0.07	1.07
12.80	2.12	15.82	6.59	104.22	2.99	0.07	1.13
12.82	2.25	16.81	6.17	103.80	2.95	0.07	1.20
12.84	2.35	17.65	5.94	104.80	2.92	0.08	1.26
12.86	2.44	18.39	5.75	105.78	2.91	0.08	1.31
12.88	2.49	18.75	5.68	106.61	2.90	0.08	1.34
12.90	2.53	19.05	5.62	107.16	2.89	0.08	1.36
12.92	2.56	19.26	5.59	107.65	2.89	0.08	1.38
12.94	2.55	19.13	5.66	108.28	2.90	0.08	1.37
12.96	2.46	18.37	5.95	109.22	2.92	0.08	1.31
12.99	2.32	17.17	6.44	110.60	2.97	0.07	1.23
13.01	2.16	15.86	7.14	113.15	3.03	0.07	1.13
13.02	2.00	14.47	8.04	116.35	3.11	0.07	1.03
13.04	1.85	13.24	8.95	118.52	3.18	0.07	0.95
13.06	1.76	12.53	9.48	118.75	3.22	0.07	0.90
13.08	1.77	12.59	9.37	117.90	3.21	0.07	0.90
13.10	1.82	12.94	9.02	116.70	3.18	0.07	0.92
13.12	1.89	13.52	8.44	114.12	3.14	0.07	0.97
13.14	1.97	14.10	7.79	109.77	3.09	0.07	1.01
13.16	2.06	14.85	7.03	104.31	3.02	0.07	1.06
13.18	2.08	15.00	6.68	100.14	2.99	0.07	1.07
13.20	2.06	14.77	6.67	98.45	2.99	0.07	1.05
13.22	1.95	13.84	7.13	98.65	3.03	0.07	0.99
13.24	1.85	13.01	7.67	99.81	3.08	0.07	0.93
13.26	1.75	12.24	8.22	100.54	3.12	0.07	0.87
13.28	1.72	11.93	8.44	100.71	3.14	0.07	0.85
13.30	1.71	11.88	8.48	100.74	3.14	0.07	0.85
13.32	1.73	12.01	8.38	100.65	3.14	0.07	0.86
13.34	1.76	12.24	8.20	100.28	3.12	0.07	0.87
13.36	1.79	12.40	7.96	98.73	3.10	0.07	0.89
13.39	1.80	12.50	7.74	96.70	3.08	0.07	0.89
13.40	1.78	12.32	7.72	95.13	3.08	0.07	0.88
13.42	1.74	11.97	7.85	94.00	3.09	0.07	0.86
13.44	1.70	11.60	7.99	92.64	3.10	0.07	0.83

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
13.46	1.66	11.31	7.94	89.81	3.10	0.07	0.81
13.48	1.59	10.74	8.22	88.28	3.12	0.07	0.77
13.51	1.50	9.95	8.81	87.64	3.17	0.06	0.71
13.52	1.39	9.10	9.66	87.97	3.23	0.06	0.65
13.54	1.32	8.56	10.16	86.94	3.26	0.06	0.61
13.56	1.27	8.15	10.53	85.78	3.29	0.06	0.58
13.58	1.24	7.89	10.77	84.92	3.30	0.06	0.56
13.60	1.23	7.82	10.74	83.96	3.30	0.06	0.56
13.62	1.24	7.84	10.44	81.90	3.28	0.06	0.56
13.64	1.27	8.05	9.86	79.31	3.24	0.06	0.57
13.66	1.30	8.27	9.32	77.06	3.21	0.06	0.59
13.68	1.33	8.55	8.91	76.13	3.18	0.06	0.61
13.70	1.34	8.60	8.86	76.22	3.17	0.06	0.61
13.72	1.32	8.42	9.15	77.05	3.19	0.06	0.60
13.74	1.28	8.10	9.67	78.34	3.23	0.06	0.58
13.76	1.01	6.01	11.31	67.89	3.34	0.06	0.43
13.78	0.98	5.71	11.86	67.69	3.37	0.05	0.41
13.80	0.95	5.45	12.21	66.56	3.39	0.06	0.39
13.83	1.13	6.84	11.21	76.64	3.33	0.06	0.49
13.84	1.07	6.36	11.77	74.82	3.37	0.06	0.45
13.86	1.01	5.95	12.21	72.60	3.39	0.06	0.42
13.88	0.98	5.64	12.34	69.62	3.40	0.06	0.40
13.90	0.95	5.45	12.22	66.60	3.39	0.06	0.39
13.92	0.93	5.27	12.02	63.32	3.38	0.06	0.38
13.94	0.93	5.27	11.56	60.97	3.35	0.06	0.38
13.96	0.96	5.50	10.66	58.58	3.30	0.06	0.39
13.98	0.98	5.60	10.10	56.51	3.26	0.06	0.40
14.00	0.98	5.59	9.70	54.24	3.23	0.06	0.40
14.02	0.98	5.62	9.28	52.17	3.20	0.06	0.40
14.04	1.00	5.77	8.74	50.40	3.16	0.06	0.41
14.06	1.02	5.90	8.52	50.28	3.15	0.06	0.42
14.08	1.01	5.83	8.87	51.74	3.17	0.06	0.42
14.10	1.00	5.77	9.35	53.89	3.21	0.06	0.41
14.12	1.02	5.90	9.34	55.08	3.21	0.06	0.42
14.14	1.08	6.29	8.87	55.80	3.17	0.06	0.45
14.16	1.12	6.59	8.38	55.25	3.14	0.06	0.47
14.18	1.13	6.72	8.12	54.54	3.12	0.06	0.48
14.20	1.13	6.70	8.03	53.74	3.11	0.06	0.48
14.22	1.12	6.60	8.10	53.44	3.11	0.06	0.47
14.24	1.09	6.38	8.42	53.71	3.14	0.06	0.46
14.26	1.05	6.05	9.00	54.45	3.18	0.06	0.43
14.28	1.00	5.65	9.79	55.35	3.24	0.06	0.40
14.30	0.95	5.30	10.52	55.82	3.29	0.06	0.38
14.32	0.90	4.89	11.39	55.65	3.34	0.06	0.35
14.34	0.87	4.63	11.83	54.76	3.37	0.06	0.33
14.36	0.83	4.34	12.26	53.18	3.40	0.06	0.31
14.38	0.80	4.12	12.40	51.09	3.40	0.06	0.29
14.40	0.78	3.95	12.41	49.00	3.41	0.06	0.28

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
14.42	0.78	3.94	11.90	46.95	3.37	0.06	0.28
14.44	0.80	4.07	10.98	44.69	3.32	0.06	0.29
14.46	0.81	4.18	10.15	42.47	3.26	0.06	0.30
14.48	0.81	4.18	9.74	40.71	3.23	0.06	0.30
14.50	0.81	4.15	9.59	39.75	3.22	0.06	0.30
14.52	0.82	4.25	9.18	39.00	3.20	0.06	0.30
14.54	0.85	4.43	8.84	39.15	3.17	0.06	0.32
14.56	0.87	4.58	8.71	39.89	3.16	0.06	0.33
14.58	0.87	4.57	8.96	41.00	3.18	0.06	0.33
14.60	0.86	4.51	9.16	41.32	3.19	0.06	0.32
14.62	0.85	4.42	9.33	41.26	3.21	0.06	0.32
14.64	0.87	4.52	9.09	41.08	3.19	0.06	0.32
14.66	0.89	4.71	8.82	41.53	3.17	0.06	0.34
14.68	0.93	5.01	8.39	42.03	3.14	0.06	0.36
14.70	0.97	5.25	8.18	42.96	3.12	0.06	0.38
14.72	0.99	5.45	8.02	43.69	3.11	0.06	0.39
14.74	1.01	5.56	8.05	44.79	3.11	0.06	0.40
14.76	0.97	5.25	8.71	45.76	3.16	0.06	0.38
14.78	0.97	5.27	9.06	47.69	3.19	0.06	0.38
14.81	0.96	5.18	9.55	49.50	3.22	0.06	0.37
14.82	0.99	5.36	9.57	51.26	3.22	0.06	0.38
14.84	0.96	5.18	9.96	51.63	3.25	0.06	0.37
14.86	0.96	5.14	10.00	51.46	3.25	0.06	0.37
14.88	0.98	5.31	9.55	50.71	3.22	0.06	0.38
14.90	1.02	5.58	8.87	49.53	3.17	0.06	0.40
14.92	1.06	5.86	8.31	48.63	3.13	0.06	0.42
14.94	1.09	6.09	7.96	48.48	3.10	0.06	0.44
14.96	1.13	6.32	7.76	49.06	3.09	0.06	0.45
14.98	1.16	6.53	7.67	50.09	3.08	0.06	0.47
15.00	1.18	6.67	7.71	51.44	3.08	0.06	0.48
15.02	1.20	6.81	7.89	53.73	3.10	0.06	0.49
15.04	1.21	6.94	8.10	56.19	3.11	0.06	0.50
15.06	1.23	7.01	8.33	58.37	3.13	0.06	0.50
15.08	1.21	6.87	8.78	60.32	3.17	0.06	0.49
15.10	1.19	6.72	9.18	61.69	3.20	0.06	0.48
15.12	1.17	6.61	9.47	62.59	3.22	0.06	0.47
15.14	1.18	6.60	9.52	62.86	3.22	0.06	0.47
15.16	1.19	6.72	9.41	63.20	3.21	0.06	0.48
15.18	1.22	6.94	9.23	64.03	3.20	0.06	0.50
15.20	1.26	7.19	9.05	65.06	3.19	0.06	0.51
15.22	1.29	7.41	8.95	66.33	3.18	0.06	0.53
15.24	1.32	7.62	8.94	68.11	3.18	0.06	0.54
15.27	1.34	7.76	9.07	70.35	3.19	0.06	0.55
15.28	1.36	7.86	9.28	72.95	3.20	0.06	0.56
15.30	1.36	7.84	9.60	75.32	3.23	0.06	0.56
15.32	1.36	7.87	9.83	77.37	3.24	0.06	0.56
15.34	1.37	7.91	10.00	79.10	3.25	0.06	0.57
15.36	1.38	7.97	10.13	80.70	3.26	0.06	0.57

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
15.38	1.38	7.95	10.34	82.20	3.28	0.06	0.57
15.40	1.38	7.92	10.54	83.48	3.29	0.06	0.57
15.42	1.37	7.82	10.75	84.12	3.30	0.06	0.56
15.44	1.36	7.77	10.84	84.25	3.31	0.06	0.56
15.46	1.37	7.83	10.74	84.02	3.30	0.06	0.56
15.48	1.40	8.03	10.46	83.99	3.28	0.06	0.57
15.50	1.43	8.26	10.15	83.85	3.26	0.06	0.59
15.52	1.46	8.42	9.93	83.54	3.25	0.06	0.60
15.54	1.46	8.46	9.80	82.96	3.24	0.06	0.60
15.56	1.48	8.53	9.67	82.43	3.23	0.06	0.61
15.58	1.50	8.68	9.43	81.81	3.21	0.06	0.62
15.60	1.54	8.97	9.04	81.17	3.19	0.06	0.64
15.62	1.60	9.34	8.63	80.59	3.15	0.06	0.67
15.64	1.64	9.67	8.34	80.68	3.13	0.06	0.69
15.66	1.67	9.86	8.27	81.53	3.13	0.07	0.70
15.68	1.67	9.80	8.47	83.04	3.14	0.07	0.70
15.70	1.64	9.59	8.82	84.62	3.17	0.06	0.69
15.72	1.60	9.34	9.18	85.74	3.20	0.06	0.67
15.74	1.58	9.17	9.40	86.24	3.21	0.06	0.66
15.76	1.49	8.54	9.92	84.69	3.25	0.06	0.61
15.78	1.48	8.44	10.02	84.55	3.25	0.06	0.60
15.80	1.47	8.31	10.09	83.87	3.26	0.06	0.59
15.82	1.53	8.75	9.64	84.35	3.23	0.06	0.62
15.84	1.53	8.76	9.42	82.53	3.21	0.06	0.63
15.86	1.55	8.89	9.08	80.77	3.19	0.06	0.64
15.88	1.57	9.01	8.83	79.52	3.17	0.06	0.64
15.90	1.57	9.01	8.81	79.31	3.17	0.06	0.64
15.92	1.56	8.91	8.97	79.88	3.18	0.06	0.64
15.94	1.54	8.76	9.24	80.96	3.20	0.06	0.63
15.96	1.52	8.60	9.56	82.24	3.22	0.06	0.61
15.98	1.50	8.46	9.85	83.37	3.24	0.06	0.60
16.00	1.50	8.39	10.00	83.92	3.25	0.06	0.60
16.02	1.49	8.31	10.08	83.74	3.26	0.06	0.59
16.04	1.48	8.24	10.08	83.02	3.26	0.06	0.59
16.07	1.46	8.11	10.14	82.18	3.26	0.06	0.58
16.08	1.46	8.09	10.06	81.44	3.26	0.06	0.58
16.10	1.46	8.09	9.99	80.83	3.25	0.06	0.58
16.13	1.48	8.21	9.79	80.41	3.24	0.06	0.59
16.14	1.51	8.39	9.59	80.46	3.22	0.06	0.60
16.16	1.54	8.57	9.41	80.64	3.21	0.06	0.61
16.18	1.56	8.75	9.26	81.01	3.20	0.06	0.62
16.20	1.59	8.93	9.12	81.42	3.19	0.06	0.64
16.22	1.62	9.14	9.00	82.20	3.18	0.06	0.65
16.24	1.65	9.32	8.91	83.02	3.18	0.06	0.67
16.26	1.68	9.53	8.80	83.80	3.17	0.06	0.68
16.28	1.73	9.84	8.54	84.08	3.15	0.07	0.70
16.30	1.81	10.38	8.09	83.96	3.11	0.07	0.74
16.32	1.89	10.87	7.69	83.59	3.08	0.07	0.78

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
16.34	1.92	11.06	7.57	83.69	3.07	0.07	0.79
16.36	1.92	11.07	7.58	83.87	3.07	0.07	0.79
16.38	1.93	11.08	7.56	83.73	3.07	0.07	0.79
16.40	1.95	11.22	7.41	83.14	3.06	0.07	0.80
16.43	1.96	11.25	7.35	82.66	3.05	0.07	0.80
16.44	1.93	11.08	7.53	83.37	3.07	0.07	0.79
16.46	1.90	10.87	7.79	84.73	3.09	0.07	0.78
16.48	1.87	10.64	8.11	86.30	3.11	0.07	0.76
16.50	1.86	10.58	8.27	87.45	3.13	0.07	0.76
16.52	1.86	10.55	8.40	88.56	3.14	0.07	0.75
16.54	1.86	10.55	8.54	90.10	3.15	0.07	0.75
16.57	1.90	10.80	8.41	90.84	3.14	0.07	0.77
16.58	1.90	10.74	8.49	91.20	3.14	0.07	0.77
16.60	1.88	10.62	8.53	90.59	3.15	0.07	0.76
16.63	1.83	10.25	8.75	89.69	3.16	0.07	0.73
16.64	1.81	10.12	8.73	88.37	3.16	0.07	0.72
16.66	1.79	10.00	8.70	86.96	3.16	0.07	0.71
16.68	1.77	9.80	8.77	85.95	3.17	0.07	0.70
16.70	1.72	9.47	9.01	85.38	3.18	0.07	0.68
16.72	1.66	9.07	9.37	84.97	3.21	0.06	0.65
16.74	1.60	8.66	9.76	84.53	3.24	0.06	0.62
16.76	1.45	7.63	10.57	80.62	3.29	0.06	0.54
16.79	1.44	7.54	10.54	79.44	3.29	0.06	0.54
16.80	1.44	7.53	10.34	77.82	3.27	0.06	0.54
16.83	1.56	8.30	9.54	79.24	3.22	0.06	0.59
16.84	1.53	8.12	9.46	76.86	3.21	0.06	0.58
16.86	1.47	7.71	9.55	73.62	3.22	0.06	0.55
16.88	1.40	7.23	9.67	69.84	3.23	0.06	0.52
16.90	1.33	6.77	9.74	65.96	3.23	0.06	0.48
16.92	1.29	6.51	9.70	63.17	3.23	0.06	0.47
16.94	1.27	6.34	9.54	60.53	3.22	0.06	0.45
16.96	1.26	6.26	9.31	58.29	3.20	0.06	0.45
16.98	1.24	6.15	9.13	56.10	3.19	0.06	0.44
17.00	1.21	5.98	9.10	54.42	3.19	0.06	0.43
17.03	1.20	5.89	9.00	53.01	3.18	0.06	0.42
17.04	1.21	5.91	8.73	51.58	3.16	0.06	0.42
17.06	1.21	5.94	8.42	50.01	3.14	0.06	0.42
17.08	1.22	5.98	8.16	48.86	3.12	0.06	0.43
17.10	1.23	6.02	7.97	47.98	3.10	0.06	0.43
17.12	1.24	6.08	7.77	47.26	3.09	0.06	0.43
17.14	1.23	6.05	7.64	46.25	3.08	0.06	0.43
17.16	1.22	5.98	7.61	45.53	3.07	0.06	0.43
17.19	1.21	5.85	7.72	45.20	3.08	0.06	0.42
17.20	1.18	5.68	7.98	45.34	3.10	0.06	0.41
17.23	1.16	5.57	8.13	45.29	3.12	0.06	0.40
17.24	1.16	5.55	8.10	44.93	3.11	0.06	0.40
17.26	1.17	5.57	8.00	44.52	3.11	0.06	0.40
17.28	1.16	5.49	8.04	44.17	3.11	0.06	0.39

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
17.31	1.14	5.42	8.09	43.86	3.11	0.06	0.39
17.32	1.14	5.36	8.14	43.58	3.12	0.06	0.38
17.34	1.13	5.33	8.15	43.38	3.12	0.06	0.38
17.36	1.11	5.21	8.28	43.14	3.13	0.06	0.37
17.38	1.09	5.05	8.46	42.72	3.14	0.06	0.36
17.40	1.06	4.86	8.63	41.98	3.15	0.06	0.35
17.42	1.04	4.73	8.70	41.17	3.16	0.06	0.34
17.44	1.04	4.73	8.50	40.19	3.14	0.06	0.34
17.46	1.05	4.79	8.18	39.15	3.12	0.06	0.34
17.48	1.07	4.87	7.82	38.07	3.09	0.06	0.35
17.50	1.06	4.82	7.77	37.45	3.09	0.06	0.34
17.52	1.06	4.80	7.76	37.20	3.09	0.06	0.34
17.54	1.06	4.80	7.78	37.30	3.09	0.06	0.34
17.56	1.08	4.91	7.58	37.21	3.07	0.06	0.35
17.58	1.10	5.03	7.35	36.96	3.05	0.06	0.36
17.60	1.13	5.23	7.08	37.06	3.03	0.06	0.37
17.62	1.16	5.45	6.88	37.51	3.01	0.06	0.39
17.64	1.22	5.79	6.58	38.14	2.99	0.06	0.41
17.66	1.26	6.07	6.33	38.44	2.96	0.06	0.43
17.68	1.30	6.27	6.15	38.57	2.94	0.06	0.45
17.70	1.29	6.24	6.21	38.80	2.95	0.06	0.45
17.72	1.27	6.07	6.49	39.34	2.98	0.06	0.43
17.74	1.24	5.90	6.76	39.86	3.00	0.06	0.42
17.76	1.31	6.31	6.73	42.44	3.00	0.06	0.45
17.78	1.41	6.97	6.58	45.83	2.99	0.06	0.50
17.80	1.47	7.32	6.75	49.45	3.00	0.06	0.52
17.82	1.42	7.03	7.24	50.91	3.04	0.06	0.50
17.84	1.35	6.52	7.82	51.00	3.09	0.06	0.47
17.86	1.31	6.29	7.97	50.12	3.10	0.06	0.45
17.88	1.29	6.15	7.94	48.82	3.10	0.06	0.44
17.90	1.28	6.06	7.76	47.02	3.09	0.06	0.43
17.92	1.28	6.10	7.37	44.96	3.05	0.06	0.44
17.94	1.29	6.17	6.97	42.96	3.02	0.06	0.44
17.96	1.31	6.25	6.67	41.69	2.99	0.06	0.45
17.98	1.33	6.35	6.48	41.18	2.98	0.06	0.45
18.00	1.35	6.49	6.34	41.14	2.96	0.06	0.46
18.02	1.35	6.47	6.34	41.06	2.96	0.06	0.46
18.04	1.33	6.34	6.64	42.04	2.99	0.06	0.45
18.06	1.33	6.33	6.75	42.73	3.00	0.06	0.45
18.08	1.31	6.20	6.91	42.85	3.01	0.06	0.44
18.10	1.27	5.97	7.10	42.40	3.03	0.06	0.43
18.12	1.21	5.59	7.54	42.18	3.07	0.06	0.40
18.14	1.20	5.49	7.76	42.58	3.09	0.06	0.39

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

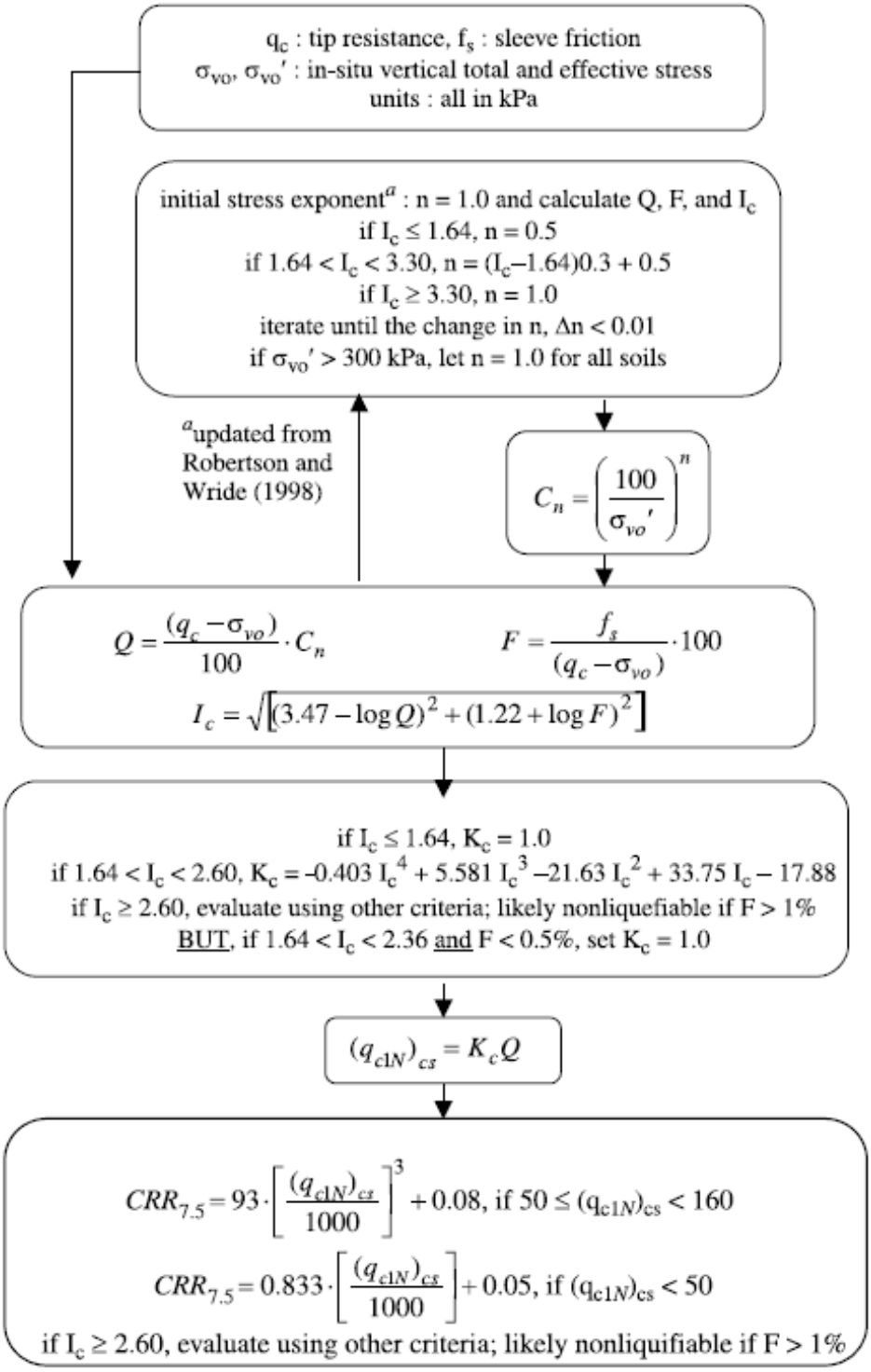
Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$

Abbreviations

q_t:	Total cone resistance
K_c:	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c:	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

Procedure for the evaluation of soil liquefaction resistance, NCEER (1998)

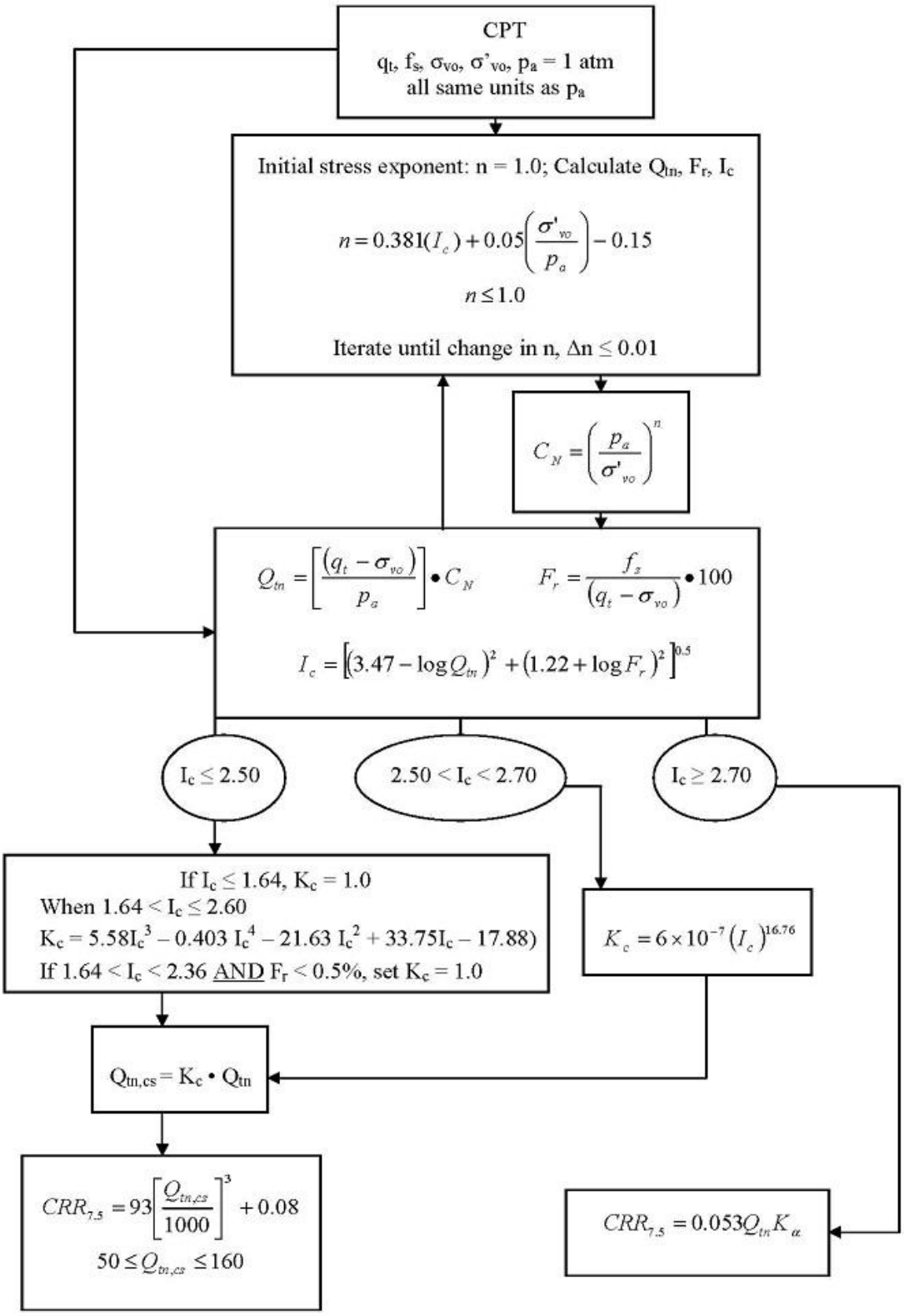
Calculation of soil resistance against liquefaction is performed according to the Robertson & Wride (1998) procedure. The procedure used in the software, slightly differs from the one originally published in NCEER-97-0022 (Proceedings of the NCEER Workshop on Evaluation of Liquefaction Resistance of Soils). The revised procedure is presented below in the form of a flowchart[1]:



[1] "Estimating liquefaction-induced ground settlements from CPT for level ground", G. Zhang, P.K. Robertson, and R.W.I. Brachman

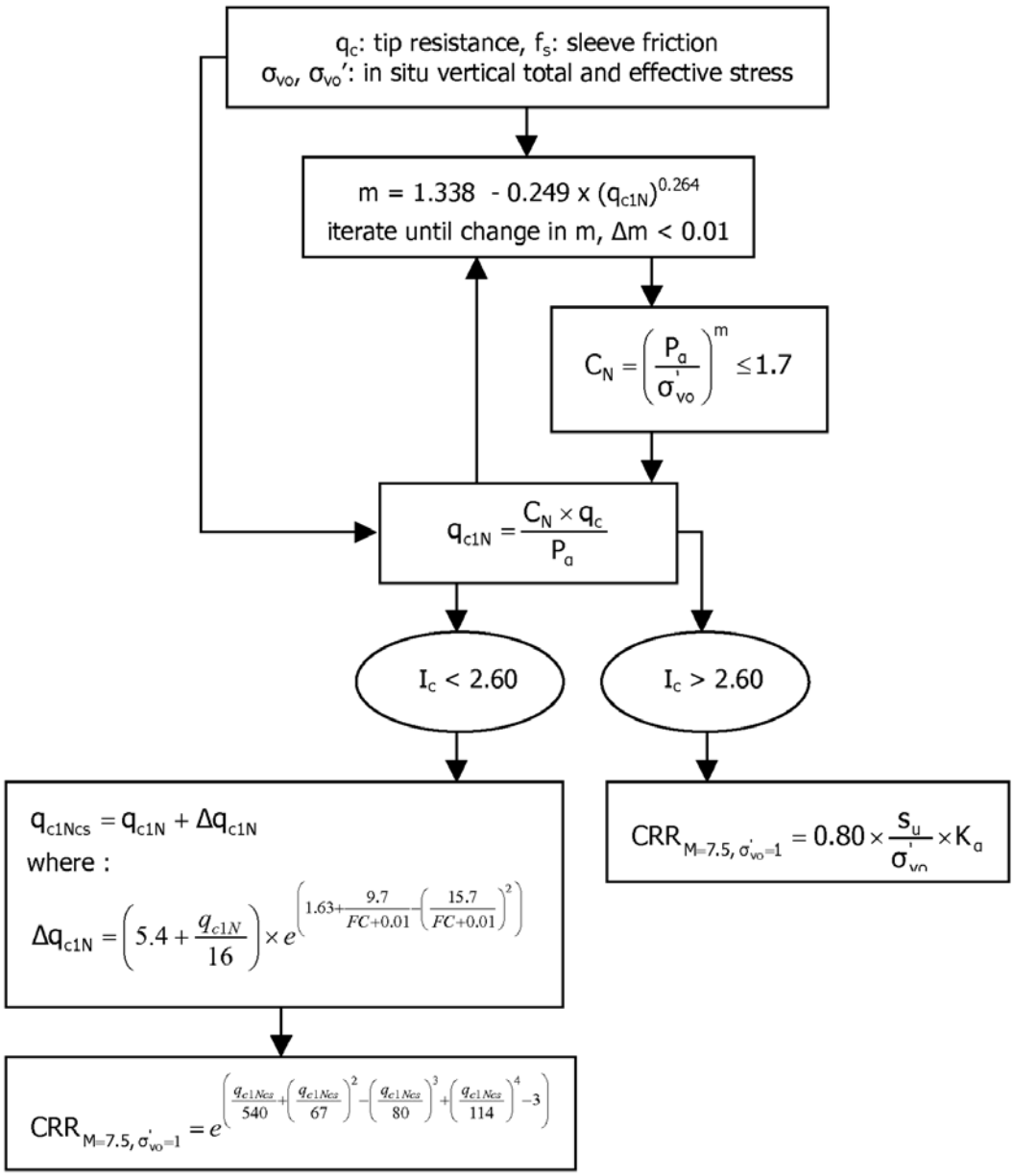
Procedure for the evaluation of soil liquefaction resistance (all soils), Robertson (2010)

Calculation of soil resistance against liquefaction is performed according to the Robertson & Wride (1998) procedure. This procedure used in the software, slightly differs from the one originally published in NCEER-97-0022 (Proceedings of the NCEER Workshop on Evaluation of Liquefaction Resistance of Soils). The revised procedure is presented below in the form of a flowchart[1]:

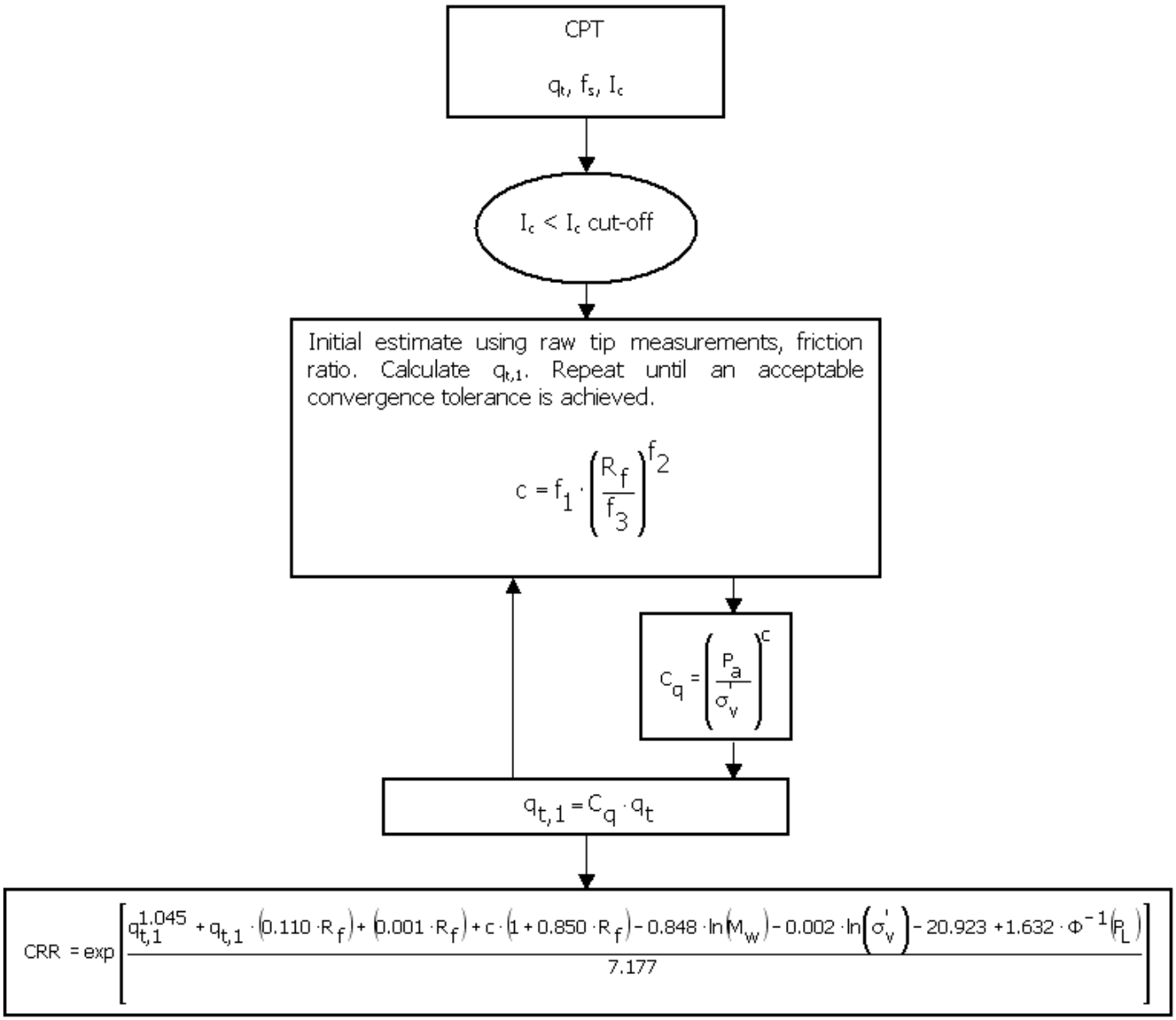


[1] P.K. Robertson, 2009. "Performance based earthquake design using the CPT", Keynote Lecture, International Conference on Performance-based Design in Earthquake Geotechnical Engineering – from case history to practice, IS-Tokyo, June 2009

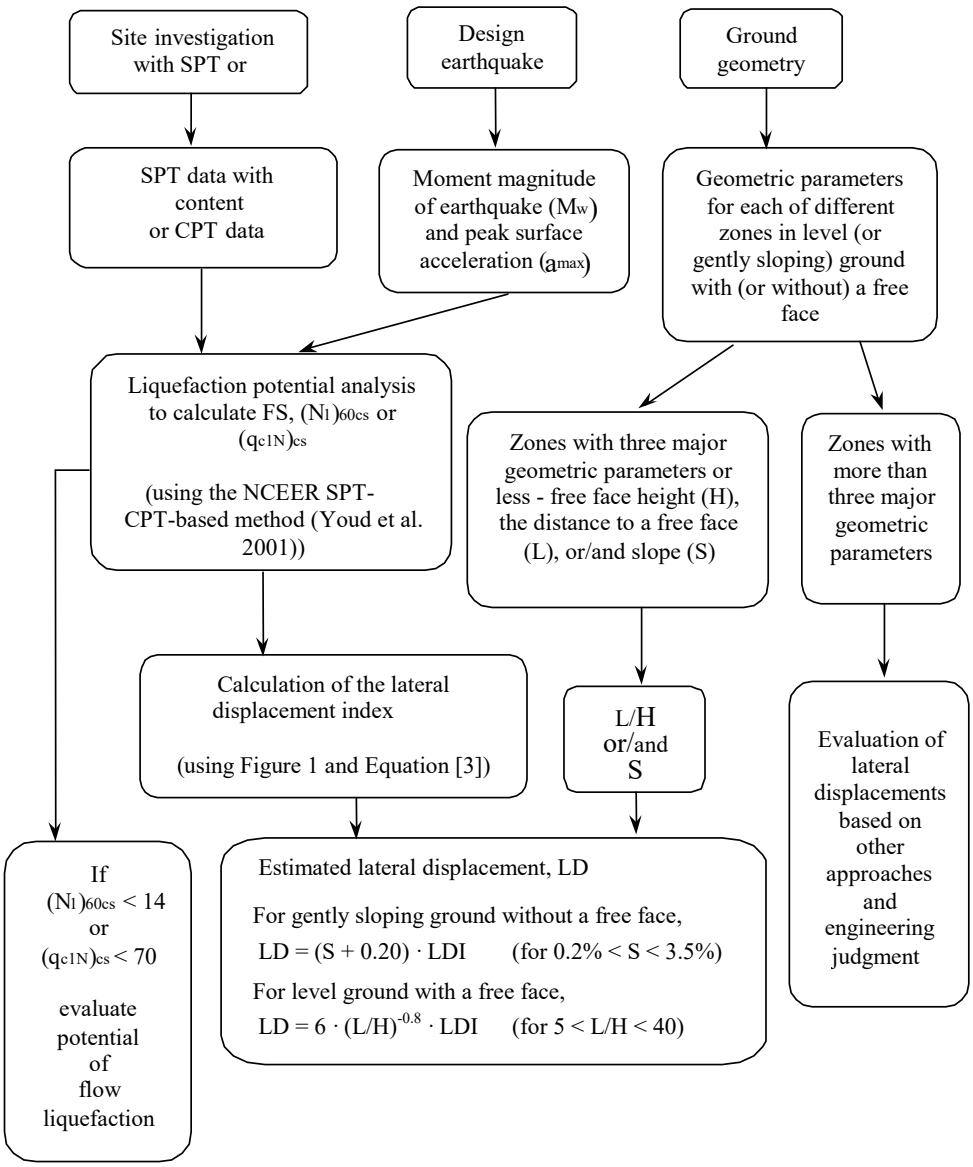
Procedure for the evaluation of soil liquefaction resistance, Idriss & Boulanger (2008)



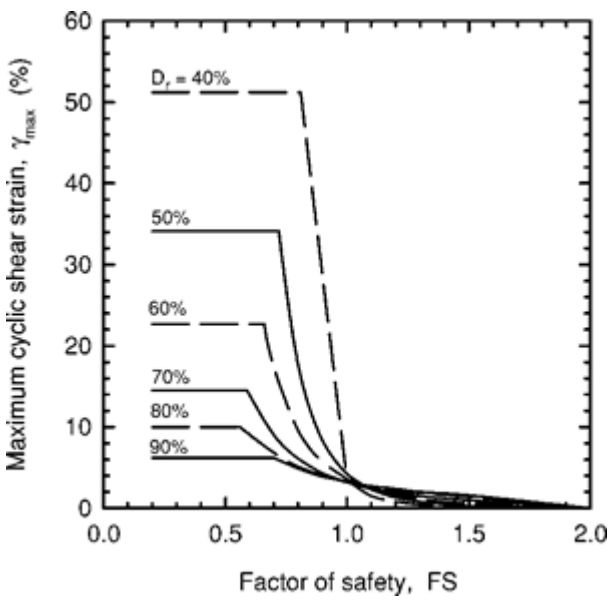
Procedure for the evaluation of soil liquefaction resistance (sandy soils), Moss et al. (2006)



Procedure for the evaluation of liquefaction-induced lateral spreading displacements



[1] Flow chart illustrating major steps in estimating liquefaction-induced lateral spreading displacements using the proposed approach



[1] Figure 1

$$LDI = \int_0^{z_{max}} \gamma_{max} dz$$

[1] Equation [3]

[1] "Estimating liquefaction-induced ground settlements from CPT for level ground", G. Zhang, P.K. Robertson, and R.W.I. Brachman

Procedure for the estimation of seismic induced settlements in dry sands

Average shear stress, τ_{av}

$$\tau_{av} = CSR^{*} \cdot \sigma_{v0}' = 0.65 \cdot \frac{a_{max}}{g} \cdot \sigma_{v0} \cdot r_a$$

Estimate small shear strain modulus, G_0

$$G_0 = 0.0188 \cdot \left[10^{(0.55 I_c + 1.68)}\right] \cdot (q_t - \sigma_v)$$

Estimate shear strain amplitude, γ

(based on Pradel (1998))

$$\gamma = \left[\frac{1 + \alpha \cdot e^{bR}}{1 + \alpha}\right] \cdot R \cdot 100 \ (\%)$$

$$R = \frac{\tau_{av}}{G_0} \text{ (Note } \tau_{av} \text{ and } G_0 \text{ same units)}$$

$$\alpha = 0.0389 \cdot \left(\frac{\sigma_v}{p_a}\right) + 0.124$$

$$b = 6400 \cdot \left(\frac{\sigma_v}{p_a}\right)$$

Estimate volumetric strain in 15 cycles

$$\varepsilon_{vol(15)} = \gamma \cdot \left[\frac{(N_1)_{60,cs}}{20}\right]^{-1.20}$$

$$(N_1)_{60,cs} = \frac{Q_{tn,cs}}{8.5 \cdot \left[1 - \frac{I_c}{4.6}\right]}$$

Volumetric strain in design earthquake

$$\Sigma_{vol} = \varepsilon_{vol(15)} \cdot \left[\frac{N_c}{15}\right]^{0.45}$$

$$N_c = (M - 4)^{2.17}$$

Seismic settlement, s

$$s = 2 \cdot \int_0^{GWT} \Sigma_{vol} \cdot dz$$

Robertson, P.K. and Lisheng, S., 2010, "Estimation of seismic compression in dry soils using the CPT" FIFTH INTERNATIONAL CONFERENCE ON RECENT ADVANCES IN GEOTECHNICAL EARTHQUAKE ENGINEERING AND SOIL DYNAMICS, Symposium in honor of professor I. M. Idriss, San Diego, CA

Liquefaction Potential Index (LPI) calculation procedure

Calculation of the Liquefaction Potential Index (LPI) is used to interpret the liquefaction assessment calculations in terms of severity over depth. The calculation procedure is based on the methology developed by Iwasaki (1982) and is adopted by AFPS.

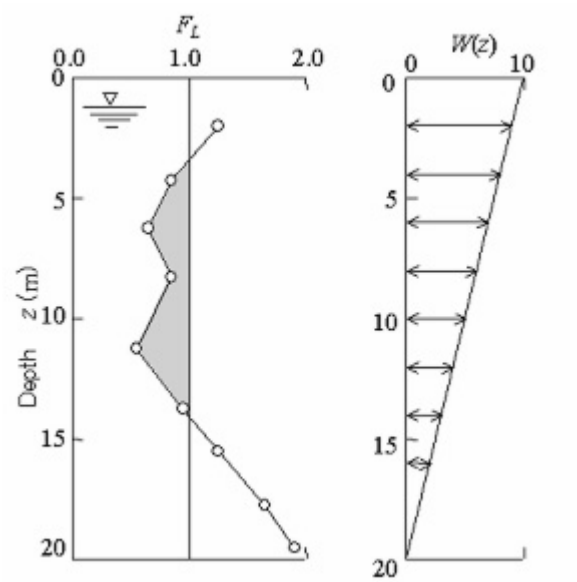
To estimate the severity of liquefaction extent at a given site, LPI is calculated based on the following equation:

$$\text{LPI} = \int_0^{20} (10 - 0{,}5_Z) \times F_L \times d_z$$

where:
F_L = 1 - F.S. when F.S. less than 1
F_L = 0 when F.S. greater than 1
z depth of measurment in meters

Values of LPI range between zero (0) when no test point is characterized as liquefiable and 100 when all points are characterized as susceptible to liquefaction. Iwasaki proposed four (4) discrete categories based on the numeric value of LPI:

- LPI = 0 : Liquefaction risk is very low
- 0 < LPI <= 5 : Liquefaction risk is low
- 5 < LPI <= 15 : Liquefaction risk is high
- LPI > 15 : Liquefaction risk is very high



Graphical presentation of the LPI calculation procedure

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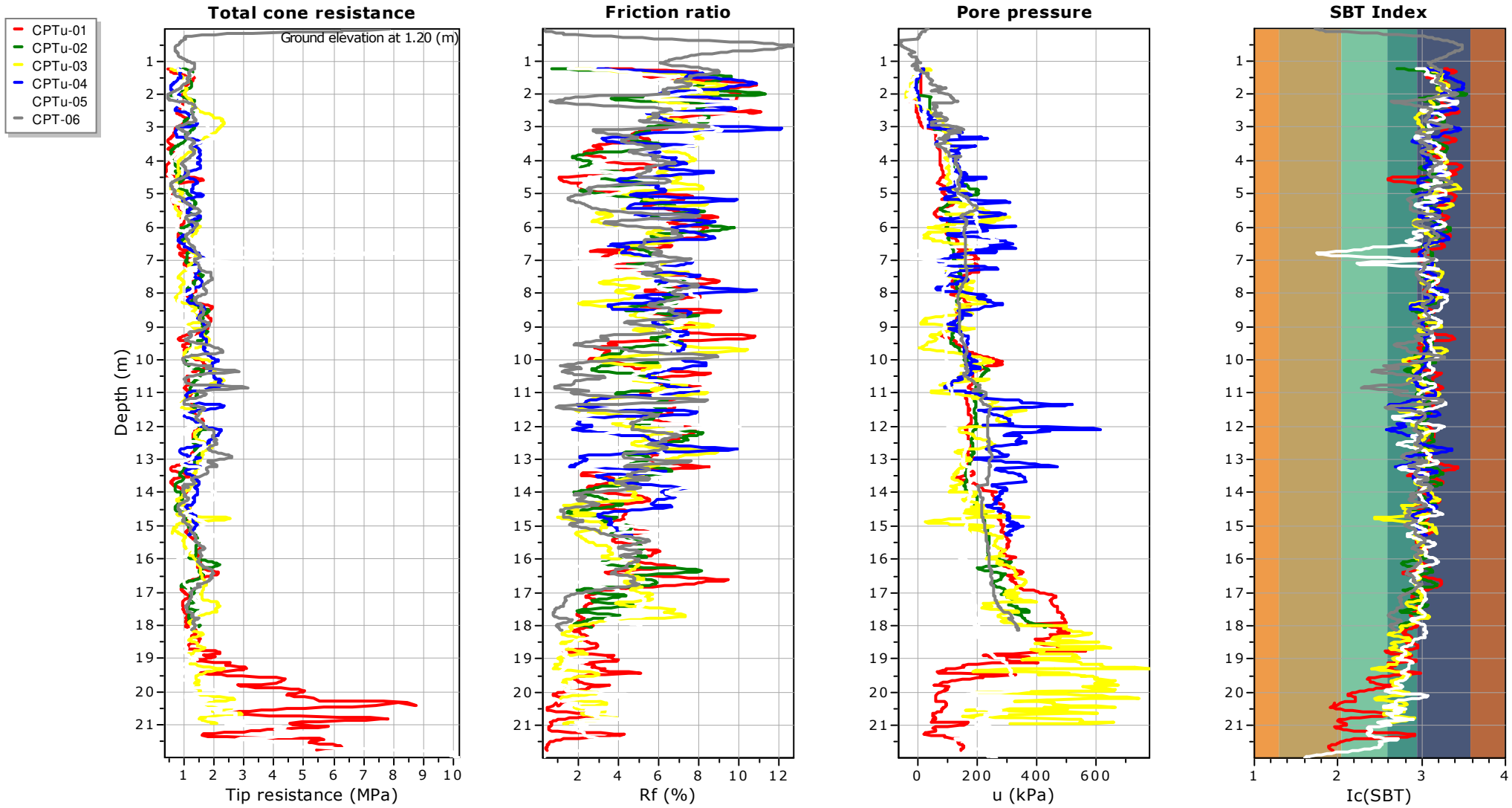
Location:

Overlay basic interpretation plots



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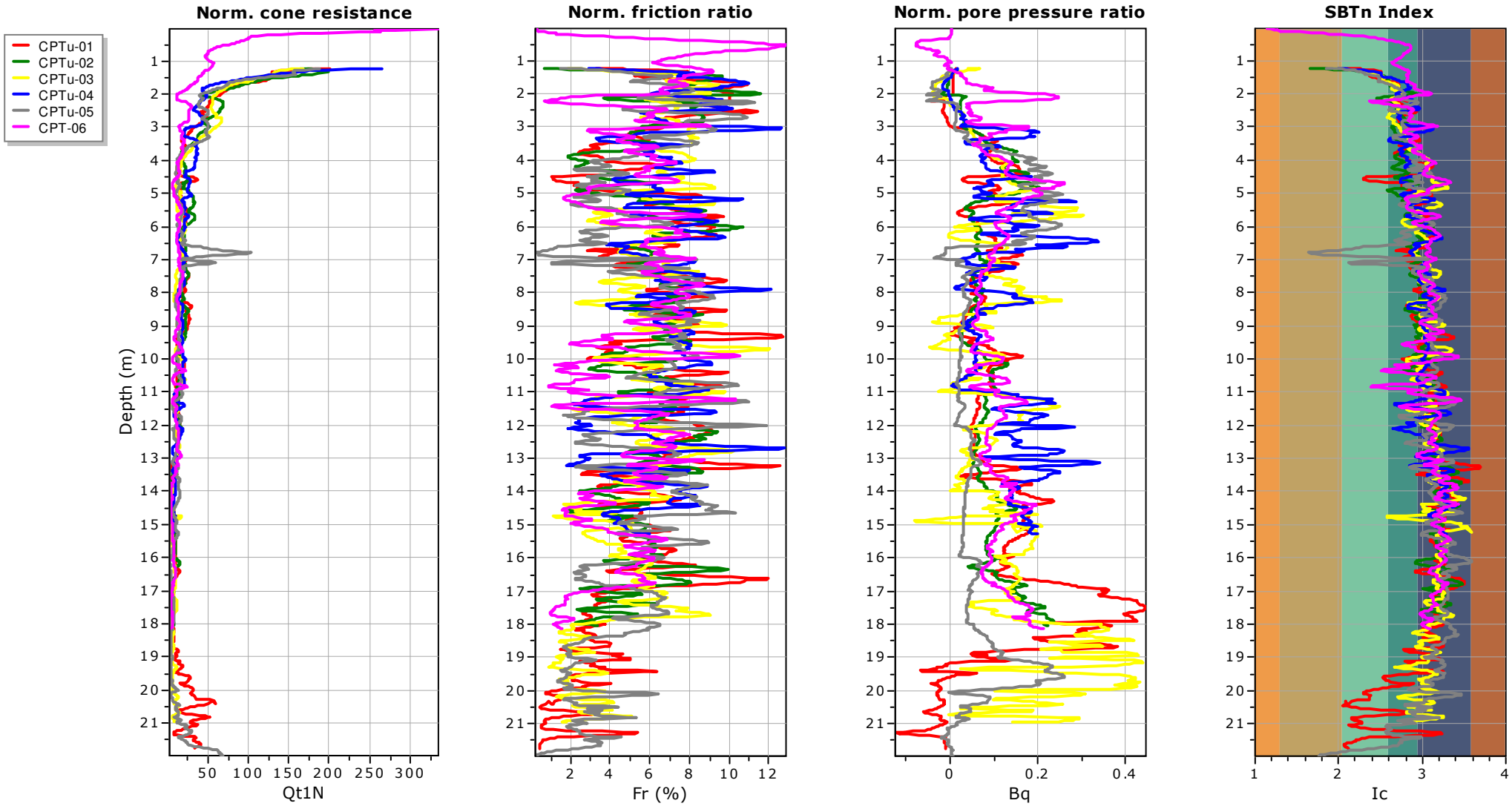
Project:
Location:

Normalized basic plots



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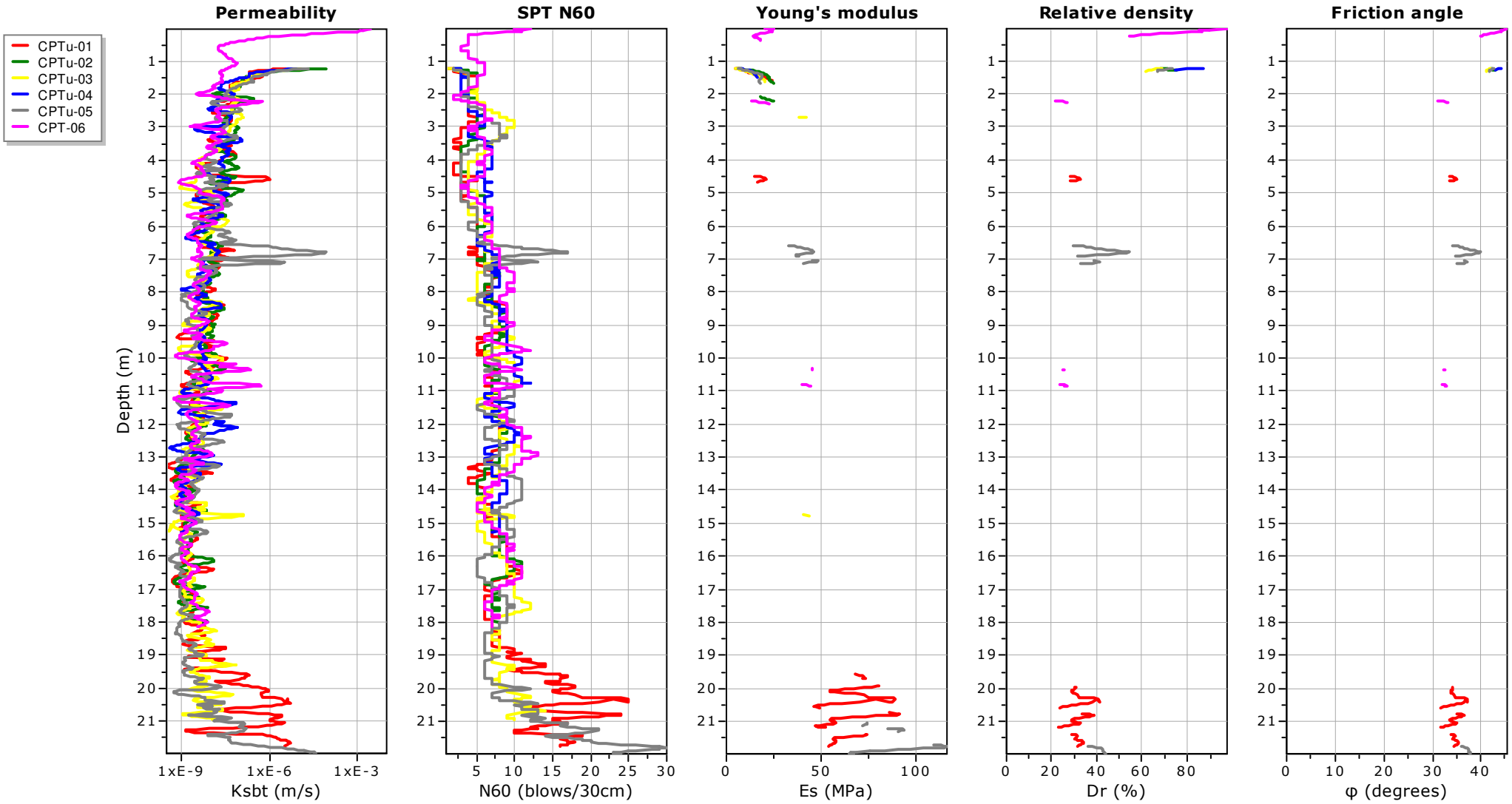
Location:

Overlay estimation plots (1)



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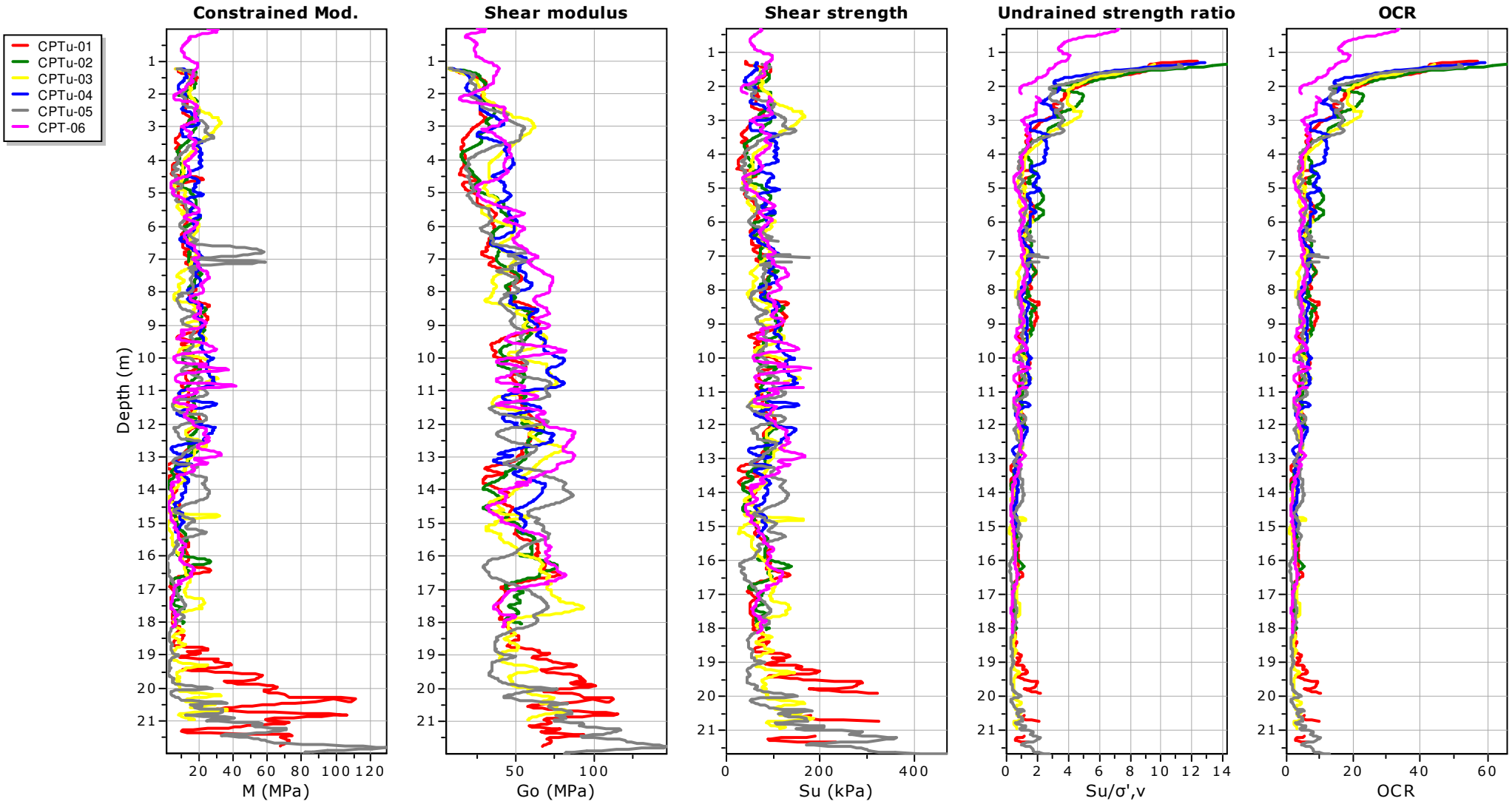
Project:
Location:

Overlay estimation plots (2)



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Project:
Location:

Overlay estimation plots (3)